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1	Nb-doped $VO_x/CeO_2$ catalyst for NH <sub>3</sub> -SCR of NO <sub>x</sub> at low					
2	temperatures					
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## 13 Abstract

The promotion effect of Nb addition to  $VO_r/CeO_2$  catalyst for the selective catalytic 14 15 reduction of NO<sub>x</sub> by NH<sub>3</sub> was fully investigated.  $VO_x/CeO_2$  and NbO<sub>x</sub> doped VO<sub>x</sub>/CeO<sub>2</sub> catalysts were characterized by N<sub>2</sub> physisorption, XRD, H<sub>2</sub>-TPR and 16 NH<sub>3</sub>-TPD. The results showed that the addition of Nb could significantly promote the 17 SCR activity of the  $VO_x/CeO_2$  catalyst, especially in the low temperature range. 18  $VO_x/CeO_2$  with 30 wt.% NbO<sub>x</sub> catalyst showed the best catalytic performance and 19 better SO<sub>2</sub>/H<sub>2</sub>O tolerance than VO<sub>x</sub>/CeO<sub>2</sub> catalyst. 30Nb-1VO<sub>x</sub>/CeO<sub>2</sub> also exhibited 20 21 higher NH<sub>3</sub>-SCR activity than 3V<sub>2</sub>O<sub>5</sub>-WO<sub>3</sub>/TiO<sub>2</sub>. The lower crystallinity, the stronger 22 redox capability and the more Brønsted acid sites of the Nb-VO<sub>x</sub>/CeO<sub>2</sub> catalyst were all responsible for the more excellent NH<sub>3</sub>-SCR performance. Based on kinetic 23 experiments and in situ DRIFTS results, it was concluded that the 24 Langmuir-Hinshelwood mechanism existed for selective catalytic reduction of NO 25 over Nb-VO<sub>x</sub>/CeO<sub>2</sub>, in which adsorbed NO<sub>x</sub> species reacted with adsorbed NH<sub>3</sub> to 26 27 finally form N<sub>2</sub> and H<sub>2</sub>O.

#### 28 Keywords

Selective catalytic reduction of NO<sub>x</sub> with NH<sub>3</sub>; Low temperature activity;
Vanadium-cerium catalyst; Niobium oxide

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# 32 **1 Introduction**

Nitrogen oxides (NO and NO<sub>2</sub>), which result from automobile exhaust gas and 33 34 industrial combustion of fossil fuels, have been major pollutants for air pollution.<sup>1</sup> They contribute to a variety of environmentally harmful effects such as 35 photochemical smog, acid rain, and haze formation.<sup>2</sup> The selective catalytic reduction 36 of  $NO_x$  with  $NH_3$  ( $NH_3$ -SCR) in the presence of excess oxygen is now the most 37 efficient technology for the removal of nitrogen oxides from stationary sources.<sup>2, 3</sup> 38 V<sub>2</sub>O<sub>5</sub>-WO<sub>3</sub>(MoO<sub>3</sub>)/TiO<sub>2</sub> has been widely applied as an industrial catalyst for several 39 decades. <sup>4, 5</sup> However, some problems still remain for V<sub>2</sub>O<sub>5</sub>-WO<sub>3</sub>(MoO<sub>3</sub>)/TiO<sub>2</sub>, such 40 as the relatively narrow operating temperature window of 300-400 °C, low N<sub>2</sub> 41 selectivity and high conversion of SO<sub>2</sub> to SO<sub>3</sub> at high temperatures. <sup>4, 6, 7</sup> Besides, the 42 high concentration of ash containing K<sub>2</sub>O, CaO, As<sub>2</sub>O<sub>3</sub> in the flue gas reduces the 43 performance and longevity of V<sub>2</sub>O<sub>5</sub>-WO<sub>3</sub>(MoO<sub>3</sub>)/TiO<sub>2</sub> catalysts.<sup>8,9</sup> These could be 44 avoided by locating the SCR unit downstream of the electrostatic precipitator unit and 45 even downstream of the desulfurizer, through the development of a highly efficient 46 low temperature SCR system. 47

In our previous study, we have developed a  $VO_x/CeO_2$  catalyst, prepared by a homogeneous precipitation method, showing excellent NH<sub>3</sub>-SCR activity, N<sub>2</sub> selectivity and SO<sub>2</sub> durability. <sup>10</sup> However, the catalytic activity was not high enough for the application in the deNO<sub>x</sub> process of exhaust gas with low temperature, such as the flue gas after dust removal and desulfurization from coal-fired power plants.

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Therefore, it is very necessary to modify this vanadium-cerium catalyst to improvethe low temperature activity, which is crucial for its practical utilization.

55 Niobium compound materials are of current interest as important catalysts for various reactions, such as the removal of nitrogen oxides, the hydrogenation and 56 oxidative dehydrogenation of alkanes, acting as a catalyst promoter, catalyst support 57 or solid acid catalyst. <sup>11</sup> It was reported that when the niobium oxides were introduced 58 into V<sub>2</sub>O<sub>5</sub>/TiO<sub>2</sub> catalysts, the conversion of NO in NH<sub>3</sub>-SCR reaction increased 2-4 59 times at low temperatures. <sup>12</sup> The addition of Nb to  $MnO_r$ -CeO<sub>2</sub> was also found to be 60 very effective in improving the NH<sub>3</sub>-SCR activity and N<sub>2</sub> selectivity.  $^{13, 14}$  Mn<sub>2</sub>Nb<sub>1</sub>O<sub>x</sub> 61 catalyst exhibited higher NH<sub>3</sub>-SCR activity than MnO<sub>x</sub> catalyst. <sup>15</sup> In addition, it was 62 reported that the introduction of the third main group element (such as Mn, Fe, Co, 63 Mo) could also improve the activity, stability or SO<sub>2</sub> durability of the SCR catalysts. 64 <sup>16-19</sup> Therefore, based on our V-Ce catalyst, we can add other elements to adjust its 65 physicochemical properties, expecting to enhance the low temperature SCR activity. 66

67 In this study, a series of  $M-VO_x/CeO_2$  catalysts (M = Mn, Fe, Co, Nb, Mo) were prepared by the homogeneous precipitation method and were applied to the 68 low-temperature NH<sub>3</sub>-SCR reaction. The addition of Nb could significantly promote 69 the SCR activity over the VO<sub>x</sub>/CeO<sub>2</sub> catalyst. Among the catalysts with different 70 NbO<sub>x</sub> contents,  $VO_x/CeO_2$  with 30 wt.% NbO<sub>x</sub> catalyst showed the best catalytic 71 performance and better SO<sub>2</sub>/H<sub>2</sub>O tolerance compared to VO<sub>x</sub>/CeO<sub>2</sub> catalyst. The 72 lower crystallinity, the stronger redox capability and the more Brønsted acid sites of 73 the Nb-VO<sub>x</sub>/CeO<sub>2</sub> catalyst were all responsible for its higher SCR activity. 74

# 75 **2 Experiments**

76 2.1 Catalyst synthesis and activity tests

The  $VO_x/CeO_2$  oxide catalysts were prepared by a homogeneous precipitation 77 method. Aqueous solutions of NH<sub>4</sub>VO<sub>3</sub> (H<sub>2</sub>C<sub>2</sub>O<sub>4</sub> was added to facilitate the 78 dissolution of NH<sub>4</sub>VO<sub>3</sub>) and Ce(NO<sub>3</sub>)<sub>2</sub> were mixed with the desired molar ratios (the 79 mass ratio of vanadium oxide was controlled at 1 wt.%). An excess of aqueous urea 80 solution was then added to the mixed solution. The solution was heated to 90  $\,$   ${\rm C}$  and 81 held there for 12 h under vigorous stirring. After filtration and washing with deionized 82 water, the resulting precipitate was dried at 100 °C overnight and subsequently 83 calcined at 350 °C for 3 h in air. M-VO<sub>x</sub>/CeO<sub>2</sub> catalysts (the mass ratio of MO<sub>x</sub> were 84 controlled at 30 wt.%) were also prepared by homogeneous precipitation methods 85 using Mn(NO<sub>3</sub>)<sub>2</sub>, Co(NO<sub>3</sub>)<sub>3</sub>, Fe(NO<sub>3</sub>)<sub>3</sub>, NbCl<sub>5</sub>, and (NH<sub>4</sub>)<sub>6</sub>Mo<sub>7</sub>O<sub>24</sub> as precursors, 86 respectively. Nb-VO<sub>x</sub>/CeO<sub>2</sub> catalysts with different Nb contents (10, 30, 50 wt.%) and 87 the unpromoted 3 wt.%  $VO_x/CeO_2$  catalyst were also prepared by the same method. 88 For comparison, the conventional 3 wt.% V<sub>2</sub>O<sub>5</sub>-10 wt.% WO<sub>3</sub>/TiO<sub>2</sub> and 1 wt.% 89 V<sub>2</sub>O<sub>5</sub>-10 wt.% WO<sub>3</sub>/TiO<sub>2</sub> were prepared by impregnation method using NH<sub>4</sub>VO<sub>3</sub>, 90 (NH<sub>4</sub>)<sub>10</sub>W<sub>12</sub>O<sub>41</sub>, H<sub>2</sub>C<sub>2</sub>O<sub>4</sub> 2H<sub>2</sub>O as precursors and anatase TiO<sub>2</sub> as support. After 91 impregnation, the excess water was removed in a rotary evaporator at 60 °C. The 92 samples dried at 100 °C overnight and then calcined at 500 °C for 3h in air condition. 93

Before NH<sub>3</sub>-SCR activity tests, the catalysts were pressed, crushed and sieved to
40-60 mesh. The SCR activity tests were carried out in a fixed-bed quartz flow reactor

at atmospheric pressure. The reaction conditions were controlled as follows: 500 ppm 96 NO, 500 ppm NH<sub>3</sub>, 5 vol.% O<sub>2</sub>, 100 ppm SO<sub>2</sub> (when used), N<sub>2</sub> balance. Under 97 98 ambient conditions, the total flow rate was 500 ml/min and the gas hourly space velocity (GHSV) was 50 000 h<sup>-1</sup>. The amount of catalysts used in activity tests was 99 100 0.6 ml (about 0.7 g). The effluent gas including NO, NH<sub>3</sub>, NO<sub>2</sub> and N<sub>2</sub>O was continuously analyzed by an FTIR spectrometer (Nicole Nexus 670) equipped with a 101 heated, low-volume multiple-path gas cell (2m). The FTIR spectra were collected 102 after the SCR reaction reached a steady state, and the  $NO_x$  conversion and  $N_2$ 103 104 selectivity were calculated as follows:

$$NO_{x}conversion = \left(1 - \frac{[NO]_{out} + [NO_{2}]_{out}}{[NO]_{in} + [NO_{2}]_{in}}\right) \times 100\%$$

$$N_{2}selectivity = \frac{[NO]_{in} + [NH_{3}]_{in} - [NO_{2}]_{out} - 2[N_{2}O]_{out}}{[NO]_{in} + [NH_{3}]_{in}} \times 100\%$$

# 105 2.2 Characterization of catalysts

The surface area and pore characterization of the catalysts were obtained from  $N_2$ 106 107 adsorption/desorption analysis at -196 °C using a Quantachrome Quadrasorb SI-MP. Prior to the  $N_2$  physisorption, the catalysts were degassed at 300 °C for 5 h. Surface 108 109 areas were determined by the BET equation in the 0.05-0.35 partial pressure range. 110 Pore volumes and average pore diameters were determined by the Barrett-Joyner-Halenda (BJH) method from the desorption branches of the isotherms. 111

Powder X-ray diffraction (XRD) measurements of the catalysts were carried out on a computerized PANalytical X'Pert Pro diffractometer with Cu K $\alpha$  ( $\lambda = 0.15406$  nm)

radiation. The data of  $2\theta$  from 10 to  $80^{\circ}$  were collected at  $8^{\circ}$ /min with the step size of 0.07°.

The H<sub>2</sub>-TPR experiments were carried out on a Micromeritics Auto Chem 2920 chemisorption analyzer. The samples (30 mg) were pretreated at 300 °C in a flow of 20 vol.% O<sub>2</sub>/Ar (50 ml/min) for 0.5 h in a quartz reactor and cooled down to room temperature (30 °C) followed by Ar purging for 0.5 h. A 50 mL/min gas flow of 10% H<sub>2</sub> in Ar was then passed over the samples through a cold trap to the detector. The reduction temperature was raised at 10 °C min<sup>-1</sup> from 30 to 1000 °C.

122 2.3 NH<sub>3</sub>-TPD studies

NH<sub>3</sub>-TPD experiments were performed in the same instrument as the H<sub>2</sub>-TPR, 123 equipped with a quadrupole mass spectrometer (MKS Cirrus) to record the signals of 124 NH<sub>3</sub> (m/z = 17 for NH<sub>3</sub>, the interference of H<sub>2</sub>O was eliminated by using a cold trap 125 126 before the detector). Prior to TPD experiments, the samples (100 mg) were pretreated at 300 °C in a flow of 20 vol.% O<sub>2</sub>/Ar (50 ml/min) for 0.5 h and cooled down to room 127 temperature (30 °C). The samples were then exposed to a flow of 2500 ppm NH<sub>3</sub>/Ar 128 (50 ml/min) at 30 °C for 1 h, followed by Ar purging for another 1 h. Finally, the 129 temperature was raised to 600 °C in Ar flow at the rate of 10 °C min<sup>-1</sup>. 130

131 2.4 *In situ* DRIFTS studies

*In situ* DRIFTS experiments were performed on an FTIR spectrometer (Nicolet Nexus 670) equipped with a smart collector and an MCT/A detector cooled by liquid nitrogen. The reaction temperature was controlled precisely by an Omega

programmable temperature controller. Prior to each experiment, the sample was pretreated at 300 °C for 0.5 h in a flow of 20 vol.%  $O_2/N_2$  and then cooled down to 175 °C. The background spectra were collected in flowing  $N_2$  and automatically subtracted from the sample spectrum. The reaction conditions were controlled as follows: 200 ml/min total flow rate, 500 ppm NH<sub>3</sub> or/and 500 ppm NO + 5 vol.%  $O_2$ , and  $N_2$  balance. All spectra were recorded by accumulating 100 scans with a resolution of 4 cm<sup>-1</sup>.

142 **3 Results and Discussion** 

143 3.1 Catalytic performance

144 3.1.1 SCR activity over  $30M-1VO_x/CeO_2$ 

145 Fig. 1 shows the NO<sub>x</sub> conversion and N<sub>2</sub> selectivity over VO<sub>x</sub>/CeO<sub>2</sub> and doped  $VO_x/CeO_2$  catalysts. The  $VO_x/CeO_2$  catalyst presented 80% NO<sub>x</sub> conversion at 200 °C. 146 Mn doped VO<sub>x</sub>/CeO<sub>2</sub> exhibited nearly 100% NO<sub>x</sub> conversion at 100-200  $^{\circ}$ C, but the 147 NO<sub>x</sub> conversion decreased rapidly above 200 °C. It also showed lower N<sub>2</sub> selectivity 148 in the whole temperature that we investigated. NH<sub>3</sub>-SCR activities over Fe, Co and 149 Mo doped  $VO_x/CeO_2$  catalysts were all lower than that over  $VO_x/CeO_2$ . Among these 150 catalysts, Co doped  $VO_x/CeO_2$  catalyst presented the lowest  $NO_x$  conversion and the 151 maximal  $NO_x$  conversion was only 50%. Furthermore, the  $N_2$  selectivity over 152 Co-VO<sub>x</sub>/CeO<sub>2</sub> was rather low. Contrarily, Nb doped VO<sub>x</sub>/CeO<sub>2</sub> catalyst exhibited 153 higher catalytic performance than the VO<sub>x</sub>/CeO<sub>2</sub> catalyst. The addition of Nb 154 enhanced the NO<sub>x</sub> conversion and N<sub>2</sub> selectivity over VO<sub>x</sub>/CeO<sub>2</sub> simultaneously. It 155

showed 60% and 90% NO<sub>x</sub> conversion at 150 and 175 °C, respectively, and 100% N<sub>2</sub> selectivity was obtained in the temperature range of 100-350 °C. The best NH<sub>3</sub>-SCR activity was obtained over the Nb doped VO<sub>x</sub>/CeO<sub>2</sub> catalyst, therefore we chose Nb to further investigate the influence of doping amount on the catalyst structure and catalytic performance.

161 3.1.2 SCR activity over Nb-1VO<sub>x</sub>/CeO<sub>2</sub> catalysts

The effect of NbO<sub>x</sub> addition amount to  $VO_x/CeO_2$  catalyst on NO<sub>x</sub> conversion was 162 shown in Fig. 2. 10 wt.% NbO<sub>x</sub> doped VO<sub>x</sub>/CeO<sub>2</sub> catalyst showed higher NH<sub>3</sub>-SCR 163 activity than unpromoted  $VO_x/CeO_2$  catalyst. The 30Nb- $VO_x/CeO_2$  catalyst presented 164 the best catalytic activity, over which NO<sub>x</sub> was completely reduced at about 175  $^{\circ}$ C. 165 Any further increase in Nb content resulted in a decline in activity. These indicated 166 that Nb content had a significant effect on the SCR activity over VO<sub>x</sub>/CeO<sub>2</sub> catalysts, 167 and 30 wt.% NbO<sub>x</sub> was optimal. Although, for the  $30Nb-VO_x/CeO_2$  catalyst, the 168 content of 1% V seems to be negligible comparing with 30% Nb, V indeed played an 169 important role in NH<sub>3</sub>-SCR reaction and 30Nb-VO<sub>x</sub>/CeO<sub>2</sub> exhibited much higher 170 catalytic activity than 30Nb/CeO<sub>2</sub> (as shown in Fig. S1). At lower than 175 °C, the 171 reaction rates normalized by surface area over 30Nb-VO<sub>x</sub>/CeO<sub>2</sub> was higher than that 172 over  $VO_x/CeO_2$  (as shown in Fig. S2). The highest reaction rate over  $30Nb-VO_x/CeO_2$ 173 was obtained at 175-350 °C. The lower reaction rates over 30Nb-VO<sub>x</sub>/CeO<sub>2</sub> than 174  $VO_x/CeO_2$  above 200 °C were due to its larger specific surface area and similar  $NO_x$ 175 conversion. 30Nb-1VO<sub>x</sub>/CeO<sub>2</sub> and 1VO<sub>x</sub>/CeO<sub>2</sub> catalyst were chosen as the model 176 catalysts to carry out further investigation, such as the effect of Nb on H<sub>2</sub>O/SO<sub>2</sub> 177

tolerance and the relationship between catalyst structure and catalytic activity.

To better evaluate the NH<sub>3</sub>-SCR activity over Nb-VO<sub>x</sub>/CeO<sub>2</sub> catalyst, we also 179 180 carried out the comparative SCR activity test over V<sub>2</sub>O<sub>5</sub>-WO<sub>3</sub>/TiO<sub>2</sub> (Fig. 3). 30 wt.% Nb-1VO<sub>x</sub>/CeO<sub>2</sub> exhibited higher NO<sub>x</sub> conversion than  $1VO_x/CeO_2$  and  $3VO_x/CeO_2$ . 181 However, there was not notable enhancement over 30Nb-3VO<sub>x</sub>/CeO<sub>2</sub> in contrast to 182  $3VO_x/CeO_2$  (as shown in Fig. S3). Compared to  $3VO_x/CeO_2$ , the  $30Nb-1VO_x/CeO_2$ 183 catalyst not only decreased the content of vanadium oxide, but also enhanced the 184 catalytic activity. The NH<sub>3</sub>-SCR performance over 30Nb-1VO<sub>x</sub>/CeO<sub>2</sub> catalyst was 185 186 also better than that over  $3V_2O_5$ -10WO<sub>3</sub>/TiO<sub>2</sub> and  $1V_2O_5$ -10WO<sub>3</sub>/TiO<sub>2</sub>. The NO<sub>x</sub> conversion over three catalysts at 175 °C was 96%, 63% and 15%, respectively. 187 Therefore,  $30Nb-1VO_x/CeO_2$  showed excellent NH<sub>3</sub>-SCR performance. 188

189 3.1.3 Influence of 
$$H_2O$$
 and  $SO_2$  on SCR activity

190 Fig. 4 shows the effect of SO<sub>2</sub> and H<sub>2</sub>O on the catalytic activity over  $1VO_x/CeO_2$ 191 and 30Nb-1VO<sub>x</sub>/CeO<sub>2</sub> catalysts at 250 °C. When 100 ppm SO<sub>2</sub> was introduced to the inlet gas, the NO<sub>x</sub> conversion over VO<sub>x</sub>/CeO<sub>2</sub> decreased to 24% in 48 h and could not 192 recover to the initial activity after the removal of SO<sub>2</sub>, which indicates that the 193 inhibiting effect of SO<sub>2</sub> on the SCR activity over the VO<sub>x</sub>/CeO<sub>2</sub> catalyst was severe 194 and irreversible. However, the  $SO_2$  inhibiting effect over Nb-VO<sub>x</sub>/CeO<sub>2</sub> was quite 195 different. The NO<sub>x</sub> conversion decreased slightly, and nearly 90% NO<sub>x</sub> conversion 196 was obtained in the presence of 100 ppm SO<sub>2</sub> for a 48 h test. The NH<sub>3</sub>-SCR 197 performance over VO<sub>x</sub>/CeO<sub>2</sub> catalysts after SO<sub>2</sub> poisoning for 48 h is shown in Fig. 198

199 S4. The activity over Nb-VO<sub>x</sub>/CeO<sub>2</sub> was still higher than that over VO<sub>x</sub>/CeO<sub>2</sub>. 95% 200 NO<sub>x</sub> conversion could be obtained on the Nb-VO<sub>x</sub>/CeO<sub>2</sub> catalyst at 250 °C and only 201 26% NO<sub>x</sub> conversion on VO<sub>x</sub>/CeO<sub>2</sub>. This proved again that the Nb-VO<sub>x</sub>/CeO<sub>2</sub> catalyst 202 showed higher SO<sub>2</sub> resistance than VO<sub>x</sub>/CeO<sub>2</sub>.

When 5% H<sub>2</sub>O was introduced to the inlet gas, the NO<sub>x</sub> conversion over VO<sub>x</sub>/CeO<sub>2</sub> decreased rapidly to 56% and kept in 56% in 48 h test. The catalytic activity could recover to the original level after the removal of H<sub>2</sub>O, indicating that the poison of H<sub>2</sub>O was reversible. Meanwhile, H<sub>2</sub>O had no influence on the catalytic activity over Nb-VO<sub>x</sub>/CeO<sub>2</sub> catalyst and 100% NO<sub>x</sub> conversion was maintained all the time. Nb-VO<sub>x</sub>/CeO<sub>2</sub> exhibited much higher catalytic activity and stronger resistance to SO<sub>2</sub>/H<sub>2</sub>O than VO<sub>x</sub>/CeO<sub>2</sub>.

## 210 3.2 Catalyst Characterization

211  $3.2.1 \text{ N}_2$  physisorption

Table 1 shows the N<sub>2</sub> physisorption results of  $1VO_x/CeO_2$  and  $30Nb-1VO_x/CeO_2$ catalysts. Nb-VO<sub>x</sub>/CeO<sub>2</sub> catalyst presented larger specific surface area and pore volume than VO<sub>x</sub>/CeO<sub>2</sub>. The addition of Nb to VO<sub>x</sub>/CeO<sub>2</sub> resulted in bigger specific surface area and pore volume, which is beneficial to the enhancement of SCR activity.

216 3.2.2 XRD

The XRD patterns of  $1VO_x/CeO_2$  and  $30Nb-1VO_x/CeO_2$  catalysts are shown in Fig. 5. For both catalysts, all the peaks in the diffraction profiles attributed to  $CeO_2$  of a cubic fluorite structure (43-1002). No vanadium species and niobium species were

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detected, suggesting that V and Nb species were highly dispersed on the catalysts. The intensity of peaks of Nb doped catalyst was weaker than that of  $VO_x/CeO_2$ , indicating a loss of crystallinity. The deceasing crystallinity may contribute to the increase of surface area.

224 3.2.3 H<sub>2</sub>-TPR

The redox properties of 1VO<sub>x</sub>/CeO<sub>2</sub> and 30Nb-1VO<sub>x</sub>/CeO<sub>2</sub> catalysts were 225 investigated by H<sub>2</sub>-TPR and the spectra are shown in Fig. 6. There are three peaks at 226 380, 460 and 710 °C (740 °C) over 1VO<sub>x</sub>/CeO<sub>2</sub> and 30Nb-1VO<sub>x</sub>/CeO<sub>2</sub>. According to 227 the literatures  $^{10, 20}$ , the reduction peaks of surface Ce<sup>4+</sup> to Ce<sup>3+</sup> and the bulk Ce<sup>4+</sup> to 228 Ce<sup>3+</sup> were centered at 509 and 812 °C, respectively. The reduction peaks at 399, 523 229 and 766 °C over CeO<sub>2</sub> could be assigned to the reduction of surface oxygen species, 230 that of oxygen in deeper interior and that of oxygen in bulk, respectively.<sup>21</sup> The 231 reduction peak around 400-500 °C is due to the surface vanadium oxide, while high 232 temperature peak over 700 °C is assigned to the reduction of bulk vanadium oxide.<sup>22</sup> 233 Niobium oxide could be reduced at much higher temperature. <sup>15</sup> Therefore, the low 234 temperature peak at 380 °C and 460 °C could be due to the reduction of surface Ce<sup>4+</sup> 235 and  $V^{5+}$  and that in deeper interior, respectively. The TPR peak at 710 °C (740 °C) 236 could be attributed to the reduction of bulk Ce and V. Both V and Ce possessed redox 237 capability and acted as reactive sites to catalyze NH<sub>3</sub>-SCR reaction. The amount of H<sub>2</sub> 238 consumption of Nb-VO<sub>x</sub>/CeO<sub>2</sub> catalyst was higher than that of VO<sub>x</sub>/CeO<sub>2</sub> (1.15:1). 239 The intensity of the low temperature (380  $^{\circ}$ C) reduction peak of Nb-VO<sub>x</sub>/CeO<sub>2</sub> was 240 much stronger than that of  $VO_x/CeO_2$  (1.44:1). This could be due to the interaction of 241

V, Ce and Nb over Nb-VO<sub>x</sub>/CeO<sub>2</sub> catalyst resulting in better dispersion of vanadium species and stronger redox capability. The active temperature window in NH<sub>3</sub>-SCR reaction was between 150-400 °C. Stronger redox capability in this temperature range could enhance NH<sub>3</sub>-SCR performance. Therefore, Nb doped VO<sub>x</sub>/CeO<sub>2</sub> showed higher NH<sub>3</sub>-SCR activity.

247 3.2.4 NH<sub>3</sub>-TPD

Fig. 7 shows NH<sub>3</sub>-TPD results over 1VO<sub>x</sub>/CeO<sub>2</sub> and 30Nb-1VO<sub>x</sub>/CeO<sub>2</sub> catalysts 248 using the fragment of m/z = 17 to identify NH<sub>3</sub>. There were two NH<sub>3</sub> desorption peaks 249 around 100 and 250 °C on both catalysts. It is generally accepted that NH<sub>4</sub><sup>+</sup> ions 250 bound to Brønsted acid sites are less thermally stable than coordinated NH<sub>3</sub> molecules 251 bound to Lewis acid sites and desorb at lower temperatures. <sup>18, 23, 24</sup> Therefore, the 252 desorption peak at 100 °C could be ascribed to the desorption of physisorbed NH<sub>3</sub> and 253 the partial ionic NH<sub>4</sub><sup>+</sup> bound to the weak Brønsted acid sites, and the peak at 250 °C 254 could be assigned to the desorption of ionic  $NH_4^+$  bound to strong Br ønsted acid sites 255 and coordinated NH<sub>3</sub> bound to the Lewis acid sites. The amount of acid sites over 256 Nb-VO<sub>x</sub>/CeO<sub>2</sub> was remarkably larger than that of VO<sub>x</sub>/CeO<sub>2</sub> (1.68:1). It indicates that 257 Nb-VO<sub>x</sub>/CeO<sub>2</sub> catalyst presented more acid sites which could facilitate the adsorption 258 and activation of  $NH_3$  during catalytic reaction even in the presence of  $H_2O$  and  $SO_2$ 259 thus enhances the catalytic activity in NH<sub>3</sub>-SCR. In the presence of SO<sub>2</sub>, more acid 260 sites over Nb-VO<sub>x</sub>/CeO<sub>2</sub> catalyst inhibited the adsorption of SO<sub>2</sub> and the deposition of 261 262 sulfate thus enhanced the resistance to SO<sub>2</sub>. More acid sites could also promote the adsorption of NH<sub>3</sub> in the presence of H<sub>2</sub>O and weaken the competitive adsorption of 263

H<sub>2</sub>O with NH<sub>3</sub>. Furthermore, larger specific surface area was obtained over

Nb-VO<sub>x</sub>/CeO<sub>2</sub>. Therefore, Nb-VO<sub>x</sub>/CeO<sub>2</sub> catalyst showed stronger resistance to  $H_2O/SO_2$ .

267 3.3 In situ DRIFTS studies

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To investigate NH<sub>3</sub>/NO<sub>x</sub> adsorption on  $1VO_x/CeO_2$  and  $30Nb-1VO_x/CeO_2$  catalysts 268 together with the SCR reaction mechanism, in situ DRIFTS were conducted at 175 °C 269 and the results of NH<sub>3</sub> adsorption on VO<sub>x</sub>/CeO<sub>2</sub> and Nb-VO<sub>x</sub>/CeO<sub>2</sub> catalysts are 270 shown in Fig. 8A. After NH<sub>3</sub> adsorption and N<sub>2</sub> purge, both catalysts were covered by 271 different NH<sub>3</sub> species. The bands at 1423 and 1670 cm<sup>-1</sup> were assigned to asymmetric 272 and symmetric bending vibrations of ionic  $NH_4^+$  on Brønsted acid sites and the bands 273 at 1596 (1604) and 1147 (1200) cm<sup>-1</sup> were attributed to asymmetric and symmetric 274 275 bending vibrations of the N-H bonds in NH<sub>3</sub> coordinately linked to the Lewis acid sites. <sup>25-27</sup> Nb-VO<sub>x</sub>/CeO<sub>2</sub> catalyst provided more acid sites than VO<sub>x</sub>/CeO<sub>2</sub> (1.71:1), 276 especially the Brønsted acid sites, than  $VO_x/CeO_2$ , which was in well harmony with 277 the NH<sub>3</sub>-TPD results. As shown in our previous paper (Chemical Engineering Journal 278 250 (2014) 390-398)<sup>15</sup>, the NbO<sub>x</sub> itself did not show any NH<sub>3</sub>-SCR activity in the 279 whole temperature range that we investigated. However, the addition of Nb to 280  $1VO_x/CeO_2$  increased the surface acidity. Nb mainly played as acid sites for the 281 promotion of NH<sub>3</sub> adsorption in NH<sub>3</sub>-SCR reaction. 282

283 The *in situ* DRIFT spectra of NO + O<sub>2</sub> adsorption on  $1VO_x/CeO_2$  and 284 30Nb- $1VO_x/CeO_2$  catalysts at 175 °C were also conducted, and the results are shown

in Fig. 8B. When  $VO_x/CeO_2$  catalyst was exposed to NO + O<sub>2</sub>, bands assigned to 285 nitrate species were observed including monodentate nitrate (1540 and 1270 cm<sup>-1</sup>), 286 bridging nitrate (1215 and 1592 cm<sup>-1</sup>) and bidentate nitrate (1570 and 1243 cm<sup>-1</sup>).<sup>28-30</sup> 287 On the Nb-VO<sub>x</sub>/CeO<sub>2</sub> catalyst, the adsorption amount of NO<sub>x</sub> was larger than that on 288 the  $VO_x/CeO_2$  catalyst (1.67:1). The addition of Nb to the  $VO_x/CeO_2$  catalyst 289 increased the acidity but did not inhibit the adsorption of  $NO_x$  on the catalyst surface 290 simultaneously. It could be due to its stronger oxidation at low temperature and its 291 larger specific surface area. Therefore, the Nb-VO<sub>y</sub>/CeO<sub>2</sub> catalyst produced more 292 293 nitrate species than VO<sub>x</sub>/CeO<sub>2</sub>.

According to the Arrhenius equation, the activation energy over  $VO_x/CeO_2$  and Nb- $VO_x/CeO_2$  catalysts was calculated as 47 and 38 kJ/mol (as shown in Fig. S5). The interaction of V, Ce and Nb of the Nb- $VO_x/CeO_2$  catalyst decreased the activation energy of NO reduction and promote the NH<sub>3</sub>-SCR reaction.

To investigate the reactivity of adsorbed NH<sub>3</sub> species in the SCR reaction on 298 30Nb-1VO<sub>x</sub>/CeO<sub>2</sub> catalysts, the *in situ* DRIFTS of reaction between pre-adsorbed 299  $NH_3$  and  $NO + O_2$  at 175 °C were recorded as a function of time (Fig. 9A). After  $NH_3$ 300 pre-adsorption and N<sub>2</sub> purge, the catalyst surface was covered by the adsorbed NH<sub>3</sub> 301 species. When NO +  $O_2$  was introduced, the intensity of the bands attributed to NH<sub>3</sub> 302 species decreased and disappeared after 10 min. At the same time, the bands assigned 303 to nitrate species (monodentate nitrate at 1540 cm<sup>-1</sup>, bridging nitrate at 1215, 1592 304 cm<sup>-1</sup> and bidentate nitrate at 1570, 1243 cm<sup>-1</sup>) appeared. This result suggested that 305 both ionic  $NH_4^+$  and coordinated  $NH_3$  could react with  $NO_x$  and participate in the 306

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NH<sub>3</sub>-SCR reactions. Fig. S6 showed the band intensities of adsorbed NH<sub>3</sub> species over VO<sub>x</sub>/CeO<sub>2</sub> and 30Nb-VO<sub>x</sub>/CeO<sub>2</sub> pretreated by exposure to NH<sub>3</sub> followed by exposure to NO + O<sub>2</sub> at 175 °C. The reactive rate of adsorbed NH<sub>3</sub> species with gas NO and O<sub>2</sub> over Nb-VO<sub>x</sub>/CeO<sub>2</sub> was much higher than that over VO<sub>x</sub>/CeO<sub>2</sub>. Therefore, more adsorbed NH<sub>3</sub> species on Nb-VO<sub>x</sub>/CeO<sub>2</sub> contributed to its better SCR activity. The reaction between the pre-adsorbed NO<sub>x</sub> and NH<sub>3</sub> on 30Nb-1VO<sub>x</sub>/CeO<sub>2</sub>

catalysts was also investigated by the *in situ* DRIFTS, and the results were shown in Fig. 9B. After NO + O<sub>2</sub> pre-adsorption and N<sub>2</sub> purge, Nb-VO<sub>x</sub>/CeO<sub>2</sub> catalyst surface was covered by various nitrate species. When NH<sub>3</sub> was introduced, the intensity of bridging nitrate decreased, which indicated that adsorbed NO<sub>x</sub> species could also react with NH<sub>3</sub>. NH<sub>3</sub> adsorbed species were observed at the band of 1427 cm<sup>-1</sup>.

318 The kinetic experiments were also carried out to investigate the reaction order and the tests met the condition of differential reactor model. The NO conversion data in 319 the kinetics test were in differential regime (conversion less than 20%) (as shown in 320 Fig. S7). A relative small particles size (40-60 mesh) and the volume hourly space 321 velocity (about 500 000 h<sup>-1</sup>)<sup>31</sup> ensured the elimination of internal and external 322 diffusion, respectively. The rates of NO conversion increased linearly with NO 323 concentration over 30Nb-1VO<sub>x</sub>/CeO<sub>2</sub> catalyst (as shown in Fig. S8), and the reaction 324 order for NO was calculated as 0.555. The reaction order for NO was lower than 1, 325 indicating the presence of Langmuir-Hinshelwood mechanism, which was in 326 327 agreement with DRIFTS results. In Fig. 9B, the intensity of the bands attributed to nitrate species weakened after exposure to NH<sub>3</sub> indicating that adsorbed NO<sub>x</sub> species 328

could react with adsorbed NH<sub>3</sub> to finally form  $N_2$  and  $H_2O$ . In our previous study <sup>10</sup>, 329 for the  $3VO_x/CeO_2$  catalysts pre-adsorbed NO<sub>x</sub> species, when NH<sub>3</sub> was introduced, 330 331 the intensity of the bands attributed to monodentate nitrate and bridging nitrate species decreased slightly. The amount of bidentate nitrate species increased markedly, 332 which may be due to the transformation of monodentate and bridging nitrate to 333 bidentate nitrate (Fig. 10<sup>10</sup> and Fig. S5<sup>10</sup>). The adsorbed nitrate species were mostly 334 inactive in the NH<sub>3</sub>-SCR reaction and therefore the 3VO<sub>x</sub>/CeO<sub>2</sub> catalysts mainly 335 followed the Eley-Rideal mechanism. 336

# 337 4 Conclusions

A systematic study on the effect of Nb addition to the  $VO_x/CeO_2$  catalyst for the 338 low-temperature NH<sub>3</sub>-SCR reaction was carried out. VO<sub>x</sub>/CeO<sub>2</sub> and Nb doped 339 340  $VO_x/CeO_2$  catalysts were prepared by homogeneous precipitation method and the SCR activity at low temperature was enhanced by the addition of Nb. The NH<sub>3</sub>-SCR 341 activity over 1% VO<sub>x</sub>/CeO<sub>2</sub> with 30 wt.% NbO<sub>x</sub> catalyst were higher than that over the 342 3%V<sub>2</sub>O<sub>5</sub>-WO<sub>3</sub>/CeO<sub>2</sub> catalyst. 30Nb-1VO<sub>x</sub>/CeO<sub>2</sub> showed higher catalytic activity than 343 1VO<sub>x</sub>/CeO<sub>2</sub> catalyst, due to the weaker crystallinity, the stronger redox capability and 344 the more Brønsted acid sites. The excellent  $SO_2/H_2O$  tolerance was also obtained over 345 30Nb-1VO<sub>x</sub>/CeO<sub>2</sub> catalyst. The Langmuir-Hinshelwood mechanism existed for 346 selective catalytic reduction of NO Over  $30Nb-1VO_x/CeO_2$ , in which adsorbed  $NO_x$ 347 species reacted with adsorbed NH<sub>3</sub> to finally form N<sub>2</sub> and H<sub>2</sub>O. 348

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Catalysts	Specific surface	Pore diameter	Pore volume			
	area (m <sup>2</sup> /g)	(nm)	(cc/g)			
1VO <sub>x</sub> /CeO <sub>2</sub>	131.3	3.50	0.11			
30Nb-1VO <sub>x</sub> /CeO <sub>2</sub>	168.2	3.48	0.15			

Table 1 N<sub>2</sub> physisorption of VO<sub>x</sub>/CeO<sub>2</sub> and Nb-VO<sub>x</sub>/CeO<sub>2</sub> catalysts

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# **Figure Captions**

Fig. 1 The NO<sub>x</sub> conversion (A) and N<sub>2</sub> selectivity (B) over  $M-VO_x/CeO_2$  catalysts. 397 Reaction conditions:  $[NO] = [NH_3] = 500 \text{ ppm}, [O_2] = 5 \text{ vol. }\%, N_2 \text{ balance, total flow}$ 398 rate 500 ml/min and GHSV = 50 000  $h^{-1}$ . 399 Fig. 2 NH<sub>3</sub>-SCR activity over Nb-VO<sub>x</sub>/CeO<sub>2</sub> catalysts. Reaction conditions: [NO] =400  $[NH_3] = 500 \text{ ppm}, [O_2] = 5 \text{ vol. }\%, N_2 \text{ balance, total flow rate 500 ml/min and GHSV}$ 401  $= 50\ 000\ h^{-1}$ . 402 Fig. 3 NH<sub>3</sub>-SCR activity over VO<sub>x</sub>/CeO<sub>2</sub> and V<sub>2</sub>O<sub>5</sub>-WO<sub>3</sub>/TiO<sub>2</sub> catalysts. Reaction 403 conditions:  $[NO] = [NH_3] = 500$  ppm,  $[O_2] = 5$  vol. %, N<sub>2</sub> balance, total flow rate 500 404 ml/min and GHSV =  $50\ 000\ h^{-1}$ . 405 406 Fig. 4 Effect of SO<sub>2</sub> and H<sub>2</sub>O on NH<sub>3</sub>-SCR activity over VO<sub>x</sub>/CeO<sub>2</sub> and Nb-VO<sub>x</sub>/CeO<sub>2</sub>

- 407 catalysts at 250 °C. Reaction conditions:  $[NO] = [NH_3] = 500$  ppm,  $[SO_2] = 100$  ppm
- 408 (when used),  $[H_2O] = 5\%$  (when used),  $[O_2] = 5$  vol. %, N<sub>2</sub> balance, total flow rate
- 409 500 ml/min and GHSV = 50 000  $h^{-1}$ .
- 410 Fig. 5 XRD patterns of  $VO_x/CeO_2$  and  $Nb-VO_x/CeO_2$  catalysts.
- 411 Fig. 6 H<sub>2</sub>-TPR results over  $VO_x/CeO_2$  and Nb- $VO_x/CeO_2$  catalysts.
- 412 Fig. 7 NH<sub>3</sub>-TPD results over  $VO_x/CeO_2$  and Nb-VO<sub>x</sub>/CeO<sub>2</sub> catalysts.
- 413 Fig. 8 DRIFT spectra of 500 ppm  $NH_3$  adsorption (A) and 500 ppm NO + 5 vol.%  $O_2$
- 414 adsorption (B) on  $VO_x/CeO_2$  and  $Nb-VO_x/CeO_2$  catalysts.

- 415 Fig. 9 In situ DRIFT spectra over Nb-VO<sub>x</sub>/CeO<sub>2</sub> pretreated by exposure to NO + O<sub>2</sub>
- followed by exposure to  $NH_3$  at 175 °C (A), and by exposure to  $NH_3$  followed by
- 417 exposure to NO +  $O_2$  at 175 °C (B).
- 418





421 Reaction conditions:  $[NO] = [NH_3] = 500$  ppm,  $[O_2] = 5$  vol. %, N<sub>2</sub> balance, total flow

422

rate 500 ml/min and GHSV = 50 000  $h^{-1}$ .





432 Reaction conditions:  $[NO] = [NH_3] = 500$  ppm,  $[O_2] = 5$  vol. %, N<sub>2</sub> balance, total flow

433 rate 500 ml/min and GHSV = 50 000  $h^{-1}$ .



Fig. 4 Effect of SO<sub>2</sub> and H<sub>2</sub>O on NH<sub>3</sub>-SCR activity over VO<sub>x</sub>/CeO<sub>2</sub> and Nb-VO<sub>x</sub>/CeO<sub>2</sub> catalysts at 250 °C. Reaction conditions:  $[NO] = [NH_3] = 500$  ppm,  $[SO_2] = 100$  ppm (when used),  $[H_2O] = 5\%$  (when used),  $[O_2] = 5$  vol. %, N<sub>2</sub> balance, total flow rate 500 ml/min and GHSV = 50 000 h<sup>-1</sup>.





Fig. 5 XRD patterns of VO<sub>x</sub>/CeO<sub>2</sub> and Nb-VO<sub>x</sub>/CeO<sub>2</sub> catalysts.





445 Fig. 6 H<sub>2</sub>-TPR results over  $VO_x/CeO_2$  and Nb-VO<sub>x</sub>/CeO<sub>2</sub> catalysts.





448 Fig. 7 NH<sub>3</sub>-TPD results over VO<sub>x</sub>/CeO<sub>2</sub> and Nb-VO<sub>x</sub>/CeO<sub>2</sub> catalysts.





451 Fig. 8 DRIFT spectra of 500 ppm NH<sub>3</sub> adsorption (A) and 500 ppm NO + 5 vol.%  $O_2$ 

452 adsorption (B) on  $VO_x/CeO_2$  and  $Nb-VO_x/CeO_2$  catalysts.



