# RSC Advances



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#### RSC Advances **Page 2 of 33**



## **1. Introduction**

With the rapid development of industries, large quantities of wastewater containing heavy metals are discharged into the environment, which caused serious ecological, 26 environmental and healthy problems.<sup>1, 2</sup> Various methods, such as chemical precipitation, ion exchange, adsorption, membrane filtration, and electrochemical

# **Page 3 of 33 RSC Advances**



## RSC Advances **Page 4 of 33**

**RSC Advances Accepted Manuscript RSC Advances Accepted Manuscript**



## **2. Methods**

2.1. Biosorbent materials and chemicals

#### Page 5 of 33 **RSC Advances**



Three modifiers (sodium hydroxide (NaOH), acetic acid, ethylene diamine

2.3. Preparation of modified biosorbents

#### RSC Advances **Page 6 of 33**

**RSC Advances Accepted Manuscript RSC Advances Accepted Manuscript**

![](_page_6_Picture_134.jpeg)

#### 2.4. Experimental setup

![](_page_6_Picture_135.jpeg)

flowmeter and PVC pipes. The two PP plastic columns (8.0 cm diameter and 80 cm

length for each) packed with biosorbent giving a bed depth of 45 cm were employed

in series. Fig. 1 shows the schematic of the two-stage continuous system. Table 2 lists

- the operational parameters of pilot plant. The bed system was packed with *A. bisporus*
- (defined as Run 1); *P. cornucopiae* (defined as Run 2); *A. bisporus* and *P. cornucopiae*
- (defined as Run 3), respectively. The column I, and column II were defined as the
- column of the two-stage bed columns closing to the inlet and outlet, respectively.

## **Page 7 of 33 RSC Advances**

![](_page_7_Picture_124.jpeg)

2.5. Experimental procedure

![](_page_7_Picture_125.jpeg)

#### 133 2.6 Calculations

- 134 The Removal efficiency(%) can be calculated based on the inlet and the outlet
- 135 effluent concentrations as follows: $^{20}$

$$
Removal(\%) = \frac{(C_{in} - C_{out})}{C_{in}} \cdot 100
$$
\n(1)

136 where  $C_{in}$  (mg/L) and  $C_{out}$  (mg/L) are the influent and outlet effluent metal

- 137 concentrations, respectively.
- 138 The biosorption capacity of the target metal species was determined by the
- 139 concentration before and after absorption:

$$
q = \frac{t \cdot Q \cdot (C_{in} - C_{out})}{m} \tag{2}
$$

140 where t is the treatment time (h), Q is the flow rate  $(L h^{-1})$ , m is the total mass of the

141 biosorbent in the column (g).

#### 142 2.7 Theoretical models

The Bohart-Adams model was frequently applied for modeling the breakthrough 144 curves for metal ions' sorption.<sup>21, 22</sup> This model is used for the interpretation of the initial part of the breakthrough curve, and the mathematical expression of the model is as follows:

$$
\ln \frac{C_t}{C_i} = K_{BA} C_i t - K_{BA} N_0 \frac{Z}{\nu}
$$
\n<sup>(3)</sup>

147 Where 
$$
K_{BA}
$$
,  $N_0$ ,  $v$ ,  $Z$  were kinetic constant (L mg-1 h-1), biosorption capacity (mg

- 148 L-1), linear flow velocity (cm h-1), bed height (cm), respectively.
- 149 The Thomas model  $^{23}$  was frequently applied for describing the column
- 150 performance and predicting the breakthrough curve of metal sorption. This model
- 151 assumes that the adsorption process follows Langmuir kinetics of adsorption–

## **Page 9 of 33 RSC Advances**

![](_page_9_Picture_188.jpeg)

3.1 Effect of modification

![](_page_9_Picture_189.jpeg)

## RSC Advances **Page 10 of 33**

![](_page_10_Picture_154.jpeg)

## 3.2 Metal removal in *A. bisporus* columns

## **Page 11 of 33 RSC Advances**

![](_page_11_Picture_131.jpeg)

#### RSC Advances **Page 12 of 33**

![](_page_12_Picture_136.jpeg)

#### 3.3 Metal removal in *P. cornucopiae* columns

The effluent concentration profiles from column I in the two-stage system packed with *P. cornucopiae* are given in Fig. 5. The performances of this run are summarized at Table 4. At the operation of 45h and 50h, it was detected that the amount of 232 cadmium remaining in the outlet effluent was 0.113, and 0.264 mg  $L^{-1}$ , respectively, which continuously exceeded the emission limit values. Meanwhile, the concentrations of other heavy metals in the effluent from column II were all below

# **Page 13 of 33 RSC Advances**

![](_page_13_Picture_136.jpeg)

# RSC Advances **Page 14 of 33**

257 uptake by biosorbent.<sup>13</sup> The limitation in adsorption selectivity of biomass might be

![](_page_14_Picture_166.jpeg)

#### Page 15 of 33 **RSC Advances**

- 278 between the Thomas rate constant  $(K_T)$  and uptake capacity  $(q_0)$  was observed.
- 279 Similar observation was reported by Bulgariu and Bulgariu.<sup>21</sup>
- 3.5 Metal removal in *A. bisporus* and *P. cornucopiae* columns

![](_page_15_Picture_157.jpeg)

- sorption on various metals among different sorbents might be the major reason. Our
- previous study and many other reports also mentioned the preference of mushroom
- 298 for metals.<sup>14, 17</sup> The profile of breakthrough curves obtained from packed bed column

#### **RSC Advances Page 16 of 33**

**RSC Advances Accepted Manuscript RSC Advances Accepted Manuscript**

studies was the shape of an "S".<sup>5, 12, 21, 31</sup> The low concentration of metals in the outlet effluent when the operation stopped indicated the vacant of some adsorption sites. Once the mixed biosorbents were applied, the metals could make full use of those adsorption sites, thus the total metal uptake of biosorbents increased.

3.6 Desorption and regeneration

The usefulness of a biosorbent depends not only on its biosorption capacity, but 305 also on the efficient regeneration and reuse. The Sorption – Desorption parameters listed in Table 7 showed that the desorption of *A. bisporus* was 85.29% after three cycles, while *P. cornucopiae* was approximately 80%. The biomass in the packed bed system can undergo cyclic biosorption-desorption cycles without additional operations, such as, centrifugation, filtration, and packing. In addition, the biomass 310 utilized in this study has been proved to have high efficiencies of desorption.<sup>18, 33</sup> Therefore, the requirement of fresh biosorbent is reduced, making the biosorption process more sustainable and cost effective. The exhausted biosorbents for the present system were put into a biogas digester for fermentation after being exhausted, and then the biogas residues were disposed of via landfill, while the biogas slurry was disposed of precipitation and flocculation for metal's extraction.

3.7 Implication for industrial application

The present study showed a good biosorption performance in a packed bed system containing multiple biosorbents. Thus, for making the utmost use of biosorbents and

## **Page 17 of 33 RSC Advances**

![](_page_17_Picture_129.jpeg)

## **4. Conclusions**

![](_page_17_Picture_130.jpeg)

## **Acknowledgements**

## **RSC Advances Page 18 of 33**

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# **Page 19 of 33 RSC Advances**

![](_page_19_Picture_279.jpeg)

# RSC Advances **Page 20 of 33**

![](_page_20_Picture_280.jpeg)

# **Page 21 of 33 RSC Advances**

![](_page_21_Picture_75.jpeg)

440	Table 1

441 Characteristics of industrial wastewater.

![](_page_22_Picture_92.jpeg)

443	Table 2

444 Small-sized pilot plant operational parameters.

![](_page_23_Picture_89.jpeg)

445 Notations: Column-*A*: the bed column packed with *A. bisporus*; Column-*P*: the bed

446 column packed with *P. cornucopiae.* 

# 448 Table 3

Effect of different modifiers on heavy metals biosorption capacity (mg  $g^{-1}$ ) by

450 mushrooms.

![](_page_24_Picture_83.jpeg)

![](_page_25_Picture_65.jpeg)

## 453 The performance of different runs.

![](_page_25_Picture_66.jpeg)

## 455 Table 5

456 Parameters of Bohart-Adams and Thomas models for the sorption of metal ions by

![](_page_26_Picture_130.jpeg)

![](_page_26_Picture_131.jpeg)

458 Notations: K<sub>BA</sub>, Bohart-Adams rate constant (L mg<sup>-1</sup> h<sup>-1</sup>); N<sub>0</sub>, saturation concentration

459 (mg l<sup>-1</sup>); K<sub>T</sub>, Thomas rate constant (L mg<sup>-1</sup> h<sup>-1</sup>); q<sub>0</sub>, equilibrium metal sorption (mg

460  $\text{g}^{-1}$ ); R<sup>2</sup>, correlation coefficient.

462	Table 6	

463 The performance of the bed column system packed with *A. bisporus* and *P.* 

464 *cornucopiae.*

![](_page_27_Picture_88.jpeg)

465

	467	Table 7
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468 Sorption – Desorption parameters.

![](_page_28_Picture_76.jpeg)

![](_page_29_Figure_3.jpeg)

![](_page_30_Figure_2.jpeg)

![](_page_31_Figure_2.jpeg)

482 Fig. 3 FTIR spectrums of *P. cornucopiae* (A) and modified *P. cornucopiae* (B)

![](_page_32_Figure_2.jpeg)

Fig. 4 Breakthrough profile of nickel, zinc and copper in the effluent from columnⅠ

in the system packing with *A. bisporus.* 

![](_page_33_Figure_2.jpeg)

Fig. 5 Breakthrough profile of cadmium, nickel, zinc in the effluent from columnⅠ in the system packing with *P. cornucopiae.*