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## Ohmic Contact of Indium Oxide as Transparent Electrode to n-type Indium Phosphide

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## Abstract

Ohmic contacts to n-type indium phosphide (n-InP) with indium oxide ( $In_2O_3$ ), a transparent conducting oxide (TCO), have been achieved. Hydrogen plasma surface pretreatment of the n-InP substrates (H<sub>2</sub>-cleaned n-InP) prior to the deposition of  $In_2O_3$  films, is the key to achieve Ohmic contact. Oxygen flow rate during the  $In_2O_3$  film deposition, which equivalently determines its doping level, is the main tuning parameter for  $In_2O_3$  thin films growth. Rapid thermal annealing process (RTP) at different temperatures was found to have little effects on the Ohmic contact type.

**Keywords:** Ohmic contact, In<sub>2</sub>O<sub>3</sub> thin film, n-type InP, surface pretreatment, annealing process

## **1. Introduction**

Transparent high-conductivity Ohmic contacts are of primary importance for optoelectronic devices, such as high electron mobility transistors [1], light emitting diodes (LEDs) [2] and solar cells [3]. Although the large band gaps usually associated with optical transparency preclude the possibility of high conductivity in many transparent materials, a number of metal oxides, known as transparent conducting oxides (TCOs), possess the unique properties of being both transparent and highly conductive [4].

Compared with the majority of TCOs, indium oxide (IO) as a binary compound TCO does not need extrinsic doping and has the advantage of ease of tuning the chemical composition during film deposition. What's more, the superiority of IO films over tin oxide  $(SnO_2)$  films as transparent electrodes is largely due to the higher mobility in IO [5]. IO films prepared by various techniques have mobility in the range of 10-75 cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup>, with carrier concentration around  $10^{19}$ - $10^{20}$  cm<sup>-3</sup> [5]. The optical transmittance of IO films in the visible and near-IR regions is about 75%-90% [6-8]. Additionally, the refractive index of IO films in the visible region ranges between 1.9 and 2.08 [8, 9]. The low refractive index of IO relative to InP (n~3.2) also possesses the possibility that IO could be used as a conducting waveguide cladding material for current injection into high refractive index contrast nanophotonic devices [10, 11]. A critical concern for these applications, however, is the electrical properties across the interface between the IO films and InP substrates. The contact should be Ohmic

and the resistance should be minimized [12, 13].

Generally, in order to achieve Ohmic contact between a TCO film and an n-type nondegenerate semiconductor, it is required that the Fermi level of the TCO ( $\phi_{IO}$ ) be less than that of the semiconductor ( $\phi_{InP}$ ) [14, 15]. For the donor-doped n-InP substrates used in this study (n=7.00×10<sup>17</sup> cm<sup>-3</sup>), the Fermi level (E<sub>F</sub>) is estimated to be 0.39 eV below the conduction band minimum (E<sub>c</sub>) by using Equation 1, shown as follows,

$$E_F = E_c - k_b T \cdot \ln(\frac{n}{n}) \tag{1}$$

where  $k_b$  is the Boltzmann constant; T is the room temperature (300 K);  $n_i$  is the intrinsic carrier concentration of InP as  $1.317 \times 10^7$  cm<sup>-3</sup> [16]. We know that the work function is defined as the energy difference between the vacuum level and the Fermi level, which for an n-type semiconductor can be also written as  $x + (E_c-E_f)$ . Therefore,  $\phi_{InP}$  is estimated to be 4.77 eV, where the electron affinity x of InP is 4.38 eV [16]. For In<sub>2</sub>O<sub>3</sub> films, the work function was reported as 4.6-4.7 eV for as-deposited films by D.C. magnetron sputtering [17], 4.88 eV and very close to 5 eV for films prepared by means of reactive evaporation [7,18,19]. But In<sub>2</sub>O<sub>3</sub> film still poses great possibility to form Ohmic contact to n-InP. First, we know the work function of In<sub>2</sub>O<sub>3</sub> films depends critically on the preparation method and process parameters. Second, in our study, in order to achieve Ohmic contact between the In<sub>2</sub>O<sub>3</sub> film and the n-InP substrate, H<sub>2</sub> or O<sub>2</sub> plasma surface pretreatments were done on n-InP substrates, which have been verified to change the effective surface work function of ITO [20-22]. Actually, our previous results [23] have shown that Ohmic contact of CdO to n-InP can be achieved by eliminating the interfacial oxide layer with H<sub>2</sub> plasma surface treatment on the substrate prior to film deposition and low interfacial contact resistance of  $(6.8\pm2.8)\times10^{-6}$  $\Omega$ ·cm<sup>2</sup> was obtained. However, CdO is toxic and pose a great threat to the environment. In<sub>2</sub>O<sub>3</sub> is a promising alternative to form Ohmic contact to n-InP.

In this paper, we present results for optical and electrical properties of indium oxide  $(In_2O_3)$  thin films deposited by ion beam assisted deposition (IAD). The electrical contact properties across the interface between the contact material,  $In_2O_3$ , and the semiconductor, n-InP are investigated. The oxygen partial pressure during deposition is the main tuning parameter for  $In_2O_3$  films growth. Effects of oxygen partial pressure during deposition on microstructure and surface morphology, grain size and surface roughness, optical and electrical properties of  $In_2O_3$  films were ever systematically reported [24-26]. While, in our study,  $In_2O_3$  films will be used as cladding electrodes and therefore optical and electrical properties of bulk  $In_2O_3$  films and especially the interfacial electrical contact properties are our big concern. In addition, we know, in InP based photonic device fabrication, rapid thermal annealing processes (RTP) are often required. So, it is also necessary to investigate what effect RTP would have on the interfacial contact properties between  $In_2O_3$  and InP.

## 2. Experimental

## 2.1 Film preparation

In<sub>2</sub>O<sub>3</sub> thin films were prepared at room temperature using Ion-Assisted Deposition (IAD, ION TECH, INC, USA) with In<sub>2</sub>O<sub>3</sub> target (99.99% pure, Kurt J. Lesker company). IAD consists of a main ion source and an assisted ion source. The main beam will sputter out In<sub>2</sub>O<sub>3</sub> from the target, while the assistant beam directed toward the substrate will provide additional kinetic energy to the sputtered In<sub>2</sub>O<sub>3</sub>, increasing the film surface energy without further heating. Therefore, thin films prepared by IAD possess good adhesiveness without additional substrate heating. In addition, cooling water running in the back of the sample further stabilizes the local temperature during deposition and does not exceed 50°C.

Properties of  $In_2O_3$  are strongly dependent on its doping level, which are mainly oxygen vacancies. The oxygen partial pressure, which is controlled by the oxygen flow rate of the assistant beam during deposition, is therefore the main tuning parameter for  $In_2O_3$  thin films growth. Oxygen flow rates of 0 sccm, 3 sccm, 5 sccm, and 7 sccm were used and the deposited corresponding thin films are referred to as  $In_2O_3$ -0,  $In_2O_3$ -3,  $In_2O_3$ -5, and  $In_2O_3$ -7 respectively. Deposition time is 60 min and the working pressure is  $4.5 \times 10^{-4}$  Torr. The film thickness is about 100 nm, which is tested by an alpha-step 200 from Tencor Instruments. Other detailed parameters of  $In_2O_3$  deposition are listed in Table 1.

## 2.2 Bulk In<sub>2</sub>O<sub>3</sub> properties measurement

Bulk material properties of In<sub>2</sub>O<sub>3</sub> were characterized using thin films deposited on commercial glass slides. Electrical properties were carried out using Hall Effect

measurements with films of Van der Pauw geometry. For optical properties, transmittance and reflectance spectra were measured in the spectral range from 200 nm to 2000 nm using a UV/Vis/IR Perkin-Elmer lambda 1050 spectrophotometer with the integrating sphere in the dual beam mode. Microstructure of the as-deposited In<sub>2</sub>O<sub>3</sub>-3 film was examined using scanning electron microscope (SEM, Hitachi S4800) and an RIGAKU: ATX-G x-ray diffractometer.

## 2.3 Contact patterns fabrication and Electrical contact properties measurement

Interfacial properties are characterized using the In<sub>2</sub>O<sub>3</sub> thin films deposited on n-type InP substrates (n=7.00×10<sup>17</sup> cm<sup>-3</sup>). Prior to deposition, all InP substrates were first solvent cleaned in 3 minutes of ultrasonic bath sequentially in acetone, IPA (Isopropyl Alcohol), and then deionized water; substrates cleaned by this method are referred to as solvent-cleaned samples. Some substrates were further cleaned by reactive ion etching (RIE) in Oxygen and others in Hydrogen (O<sub>2</sub> or H<sub>2</sub>, 50 mtorr, 100 W, 1 min). Samples received surface treatments of RIE plasma cleaning are referred to as O<sub>2</sub>-cleaned or H<sub>2</sub>-cleaned. It should be noted that all samples were directly put into IAD apparatus right after ex-situ pretreatments. B. Anthony's study [27] showed that H plasma clean can protect the wafer from contamination for up to 15 min in ambient air. So measures were taken to shorten the elapse to be less than 10 min.. ANTHONY

In order to examine the electrical contact properties, photolithography process was used

to define contact patterns for transmission line method measurements. Fabrication process flow is shown in Fig.1: linear arrays of 200 um by 200 um square pads with various gap distances apart (10-60 um gap in 10 um increment). Ti/Au (10 nm/300 nm) was then deposited by E-beam evaporation followed by a lift-off process to form metal contacts on In<sub>2</sub>O<sub>3</sub>. Finally, using the deposited metal pads as a self-alignment mask, the exposed In<sub>2</sub>O<sub>3</sub> film was removed using RIE in Methane/H<sub>2</sub>/Ar gases (CH<sub>4</sub>:H<sub>2</sub>:Ar=10:30:10 sccm, 50 mtorr, 200 W) to complete the fabrication process. The electrical current-voltage characteristics between In<sub>2</sub>O<sub>3</sub> films and InP substrates were measured by standard two-probe measurement method using a Kiethley 2400 source meter.

## 2.4 Annealing heat treatments detail

The annealing treatments were carried out using a Jet First 100/150 Rapid Thermal Process, at 360 °C, 400 °C and 450 °C, which are the temperatures chosen for device contact annealing. The annealing duration is 60 seconds, while the temperature was raised rapidly in 10 seconds in forming gas (20% H<sub>2</sub>, balance N<sub>2</sub>).

## 3. Results and discussion

## 3.1 Properties of bulk In<sub>2</sub>O<sub>3</sub>

The measured electrical and optical properties of bulk  $In_2O_3$  are concisely summarized in Table 2. From Table 2, we can tell with increasing the  $O_2$  flow rate during the film deposition, the carrier concentration decreases from  $8.53 \times 10^{19}$  to  $2 \times 10^{17}$  cm<sup>-3</sup>. Higher oxygen partial

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pressure during film deposition results in lower carrier concentration due to the reduction of oxygen vacancies. The Hall mobility of  $In_2O_3$  ranges from 13.1~29.3 cm<sup>2</sup>/V·s; the conductivity is highest at 355.5 S/cm for  $In_2O_3$ -0, while for  $In_2O_3$ -7 the conductivity is as small as 0.71 S/cm, which indicates that  $In_2O_3$ -7 is highly oxidized and low in oxygen vacancies.

We know that fiber-optic communication transmission windows around 1500 nm are most widely-used, which have the lowest attenuation losses and achieve the longest range. Therefore, in this study, the optical constants (refractive index n and absorption coefficient k) at 1550 nm are extracted from the transmittance and reflectance spectra, shown in Fig.2, corrected by the substrate transmittance and reflectance spectra employing the interference pattern resulted from multiple reflections in the film and the glass substrate. From Fig.2, we know that the optical transmittance of In<sub>2</sub>O<sub>3</sub> in the visible and near-IR regions is about 75%-90%, which is consistent with reported data [6, 7]. The high optical transparency of  $In_2O_3$  in the visible and near-IR regions is a direct consequence of its wide band gap (Eg ~ 3.0 eV) [28]. Additionally, the fundamental absorption edges of  $In_2O_3$  generally lie in the UV and shift to shorter wavelengths with lower O2 flow rate, due to the increasing carrier concentration. The refractive index in the visible region increases from 1.84 to 2.01 in dependence of the increasing O<sub>2</sub> flow rate during the deposition, because of the more sufficient oxidation. Optical loss at 1550 nm is highest for In<sub>2</sub>O<sub>3</sub>-0 at 2061cm<sup>-1</sup> and lowest for

 $In_2O_3$ -7 at 320.7cm<sup>-1</sup>, where higher loss at higher carrier concentration results from free carrier absorption and free carrier scattering.

The optical band gap of  $In_2O_3$  is estimated using the graph of  $(\alpha hv)^2$  versus hv [29] (as shown in Fig.3), where  $\alpha$ , the optical attenuation coefficient at energy hv, is extracted from the transmittance and reflectance spectra using the relation  $\alpha = -(1/d) \log(T/(1-R))$ , where *d* is the film thickness. From Fig.3, we can tell the optical band gap increases with the increasing carrier concentration. The optical band gap energy depends on the carrier concentration as a result of the band filling effect, also known as the Burstein-Moss shift [30]: the filling of excessive carrier in the conduction band leads to the increase of the optical band gap energy. To sum up, a trade-off relation is indicated for the engineering of the conductivity and the optical loss of bulk In<sub>2</sub>O<sub>3</sub> thin films.

## 3.2 Microstructure of In<sub>2</sub>O<sub>3</sub> films

SEM and XRD spectrum of the as-deposited  $In_2O_3$ -3 film was shown in Fig.4. The SEM result shows that the as-deposited film prepared by IAD is smooth and dense with grain size about 50 nm. And the XRD result shows that the as-deposited film is already polycrystalline, but some amorphous contribution can not be excluded. Structures comprising amorphous and polycrystalline components are common for  $In_2O_3$  films annealed or processed below 200 °C [31]. Regarding  $In_2O_3$ , the film exhibits sharp crystalline peaks, which clearly correspond to the cubic structure of the mineral bixbyite ((JCPDS 6-0416). For  $In_2O_3$ , deposited at low

temperature, the predominant planes are (222) and (400) [32], which is the case here. A (100) or (111) preferred orientation has generally been reported in  $In_2O_3$  films which have been obtained by various techniques [8, 33, 34].

## 3.3 Interfacial electrical contact property

For interfacial electrical contact experiments, contacts to n-type InP substrates pretreated with standard solvent cleaning, O<sub>2</sub> cleaning and H<sub>2</sub> cleaning, from thin films of In<sub>2</sub>O<sub>3</sub>-0, In<sub>2</sub>O<sub>3</sub>-3, In<sub>2</sub>O<sub>3</sub>-5, and In<sub>2</sub>O<sub>3</sub>-7, were examined. Fig.5 shows I-V curves of the In<sub>2</sub>O<sub>3</sub> contact to n-InP of different  $O_2$  flow rates during  $In_2O_3$  deposition: (a) solvent-cleaned n-InP substrates; (b) O<sub>2</sub>-cleaned n-InP substrates; (c) H<sub>2</sub>-cleaned n-InP substrates. For solvent-cleaned substrates as shown in Fig.5 (a), Ohmic contact is shown for n-InP to In<sub>2</sub>O<sub>3</sub>-0 and In<sub>2</sub>O<sub>3</sub>-3 thin films, while Schottky behavior is shown for In<sub>2</sub>O<sub>3</sub>-5, and In<sub>2</sub>O<sub>3</sub>-7 contacts to n-InP. The difference in carrier concentration results in different Fermi energy and work function of the  $In_2O_3$  films, whereas the energy bands are predominately aligned for less oxidized, films with higher carrier concentration forming the Ohmic contact. However, for  $O_2$  plasma cleaned substrates, all film contacts to n-InP show Schottky behavior (seen in Fig.5 (b)). This implies that an interfacial oxide layer might exist between the film and the substrate for O<sub>2</sub> plasma pretreated samples [23]. If such oxide layer exists and causes the Schottky behavior, the removal of such layer could allow the formation of Ohmic contact. Then some substrates were treated by  $H_2$  plasma after standard solvent cleaning prior to  $In_2O_3$  film deposition. The

contact measurements of those samples are shown in Fig.5 (c). All In<sub>2</sub>O<sub>3</sub> films form Ohmic contact to n-InP substrates pre-treated using H<sub>2</sub> plasma.

Dynamic resistances of  $In_2O_3$  film contacts to  $H_2$ -cleaned InP substrates in terms of different O<sub>2</sub> flow rates during film deposition are listed in Fig.6, which are calculated from the I-V curves such as those in Fig.5 (c). It can be seen that the dynamic resistance shows a decreasing trend with the increasing O<sub>2</sub> flow rate. It should be noted that besides the In<sub>2</sub>O<sub>3</sub> film resistance and the In<sub>2</sub>O<sub>3</sub>/InP contact resistance, the dynamic resistance as calculated from I-V curves is the total resistance also including the resistances due to the probes, the metal pads, the InP substrate, and the probe/metal and the metal/  $In_2O_3$  interfaces but these resistances are not affected by the increasing O2 flow rate and the hydrogen pretreatment. In consideration of the decreasing conductivity of the In<sub>2</sub>O<sub>3</sub> films with the increasing O<sub>2</sub> flow rate, seen in Table 2, we can conclude that the dynamic In<sub>2</sub>O<sub>3</sub>/InP interfacial contact resistance decreases with tuning the O<sub>2</sub> flow rate from 0 sccm to 7 scccm, after hydrogen pretreatment. On the other hand, comparing with the dynamic resistances of  $In_2O_3$ -0 and In<sub>2</sub>O<sub>3</sub>-3 films contacts to solvent-cleaned InP substrates calculated from Fig.5 (a) as 2.46  $\Omega$ and 2.78  $\Omega$  separately, the dynamic resistances of those films contacts to H<sub>2</sub>-cleaned InP substrates are 2.12  $\Omega$  and 2.07  $\Omega$  separately, as shown in Fig.6. It means that the hydrogen plasma pretreatment is not only crucial for In2O3 films to form Ohmic contact with n-InP substrates but also good for improving the interfacial conductivity of the In<sub>2</sub>O<sub>3</sub>/InP contact.

Fig.7 (a) shows the I-V curve measurements of the  $In_2O_3$ -3 contacts to H<sub>2</sub>-pretreated n-InP substrates in terms of different post-deposition rapid thermal processes (RTP) to investigate whether the annealing process will affect the ohmic contact property. It can be seen that the contact properties between In<sub>2</sub>O<sub>3</sub> and n-InP remain to be Ohmic after all the annealing heat treatments at 360 °C, 400 °C and 450 °C. This might be due to the carrier concentration remains unchanged (mainly oxygen vacancies). Meanwhile, the dynamic resistance of the  $In_2O_3$ -3 film/n-InP substrate samples were calculated, as plotted in Fig.7 (b). Comparing with that of the as-deposited sample at 2.07  $\Omega$ , the dynamic resistance first increases slowly to 2.3  $\Omega$  when the annealing temperature is lower than 400 °C and then increases sharply to 3.3  $\Omega$  with the temperature increased to 450 °C. Effects of annealing heat treatments at various temperatures, in different atmosphere or for different duration time on electrical properties of In<sub>2</sub>O<sub>3</sub> films were ever investigated [35-37]. Especially, Yuan's study of annealing on In<sub>2</sub>O<sub>3</sub> films in vacumm [35], Oh's study of annealing on Al-doped ZnO films in H<sub>2</sub> atmosphere [38] and Lin's study of annealing on In<sub>2</sub>O<sub>3</sub>:Sn films in N<sub>2</sub> atmosphere [39] have shown that grain size will increase and crystallite quality will be promoted after annealing process and the resistivity of bulk films will decrease, either due to the grain boundary scattering mechanism[35] or originating from the desorption of the negatively charged oxygen species from the grain boundary surfaces by the hydrogen treatment [38]. So resistivity of bulk  $In_2O_3$  films will get lower after annealed in  $H_2+N_2$  atmosphere. What is

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more, besides the bulk  $In_2O_3$  film resistance and the  $In_2O_3/InP$  contact resistance, the dynamic resistance includes resistance due to the probes, the metal pads, the InP substrate, and the probe/metal and the metal/  $In_2O_3$  interfaces that remains as a constant. Therefore, we can conclude that the  $In_2O_3/InP$  interfacial contact resistances first increase slowly with the increasing annealing temperature and then change sharply when the annealing temperature is high at 450 °C, which can be probably explained by the interfacial diffusion.

All results show that though the Ohmic contact of  $In_2O_3$  to n-InP is not only compatible to RTP but also the RTP is good for improving the quality of  $In_2O_3$  films, the conductivity of the  $In_2O_3/InP$  contacts will deteriorate drastically when the annealing temperature is too high, suggesting that choosing optimal annealing temperature is important in device contact heat treatments.

## 4. Conclusions

Ohmic contact of  $In_2O_3$  thin films prepared by IAD to n-type InP can be achieved with  $H_2$  plasma pre-treated substrates, which isn't obviously affected by tuning the oxygen flow rate during the film deposition or the post-deposition rapid thermal annealing processes. For optical and electrical properties, by tuning the ambient oxygen pressure during the film deposition, we obtained  $In_2O_3$  films with low optical loss (lowest at 320.7 cm<sup>-1</sup> for  $In_2O_3$ -7) at the 1550 nm wavelength range and reasonable conductivity (highest at 355.5 S/cm for  $In_2O_3$ -0). These results indicate the promising potential of  $In_2O_3$  thin films as transparent

electrodes for designing InP based optoelectronic devices for optical communication applications.

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## **Figure Captions:**

Fig.1 Schematic representation of the fabrication process used to define the electrical contact measurement pattern

Fig.2 Transmittance and reflectance spectra of In<sub>2</sub>O<sub>3</sub>-0, In<sub>2</sub>O<sub>3</sub>-3, In<sub>2</sub>O<sub>3</sub>-5 and In<sub>2</sub>O<sub>3</sub>-7

Fig.3 Graph of  $(\alpha hv)^2$  versus photon energy(eV)

Fig.4 SEM and XRD spectra of the as-deposited In<sub>2</sub>O<sub>3</sub>-3 film

Fig.5 I-V curve measurements of the  $In_2O_3$  contacts to n-InP of different  $O_2$  flow rates during film deposition: (a) solvent-cleaned n-InP substrates; (b)  $O_2$ -cleaned n-InP substrates; (c)  $H_2$ -cleaned n-InP substrates

Fig.6 Dynamic resistances of In<sub>2</sub>O<sub>3</sub> film contacts to H<sub>2</sub>-cleaned n-InP substrates in terms of different O<sub>2</sub> flow rates

Fig.7  $In_2O_3$ -3 contacts to  $H_2$ -cleaned n-InP substrates in terms of different post-deposition annealing temperatures, (a) I-V curve measurements; (b) Calculated dynamic resistances

Table 1 Parameters of In<sub>2</sub>O<sub>3</sub> films deposition by IAD

Table 2 Bulk material properties of In2O3 at different deposition conditions



Fig.1 Schematic representation of the fabrication process used to define the electrical contact measurement pattern



Fig.2 Transmittance and reflectance spectra of In<sub>2</sub>O<sub>3</sub>-0, In<sub>2</sub>O<sub>3</sub>-3, In<sub>2</sub>O<sub>3</sub>-5 and In<sub>2</sub>O<sub>3</sub>-7



Fig.3 Graph of  $(\alpha hv)^2$  versus photon energy(eV)



Fig.4 SEM and XRD spectra of the as-deposited In<sub>2</sub>O<sub>3</sub>-3 film



![](_page_24_Figure_3.jpeg)

![](_page_25_Figure_2.jpeg)

Fig.5 I-V curve measurements of the  $In_2O_3$  contacts to n-InP of different  $O_2$  flow rates during film deposition: (a) solvent-cleaned n-InP substrates; (b)  $O_2$ -cleaned n-InP substrates; (c)  $H_2$  -cleaned n-InP substrates

![](_page_26_Figure_2.jpeg)

Fig.6 Dynamic resistances of  $In_2O_3$  film contacts to  $H_2$ -cleaned n-InP substrates in terms of different  $O_2$  flow rates

![](_page_27_Figure_2.jpeg)

Fig.7 In<sub>2</sub>O<sub>3</sub>-3 contacts to H<sub>2</sub>-cleaned n-InP substrates in terms of different post-deposition annealing temperatures, (a) I-V curve measurements; (b) Calculated dynamic resistances.

Main Beam									
Forward Power (W)	Beam Voltage (V)	Accelerate Voltage (V)	Beam Current (mA)	Argon Neutron (sccm)	Argon Source (sccm)	Oxygen (sccm)			
200	1000	160	85	3	10	25			
Assisted Beam									
Forward Power (W)	Beam Voltage (V)	Accelerate Voltage (V)	Beam Current (mA)	Argon Neutron (sccm)	Argon Source (sccm)	Oxygen (sccm)			
110	150	100	31	3	10	0,3,5,7			

## Table 1 Parameters of $In_2O_3$ films deposition by IAD

Deposition Condition (O <sub>2</sub> flow rate)	0	3	5	7
Carrier Concentration (cm <sup>-3</sup> )	8.53×10 <sup>19</sup>	2.13×10 <sup>19</sup>	2×10 <sup>19</sup>	2×10 <sup>17</sup>
Conductivity (S/cm)	355.5	99.9	41.9	0.71
Hall Mobility (cm <sup>2</sup> /Vs)	26.1	29.3	13.1	21.5
Complex Refr.Ind.@1550nm (n+ik)	1.84+0.025i	1.952+0.0102i	1.9662+0.0071i	2.01+0.004i
Optical Loss@ 1550nm (cm <sup>-1</sup> )	2061.8	831.1	571.9	320.7
Optical Band Gap (eV)	3.75	3.7	3.68	3.65

Table 2 Bulk material properties of  $In_2O_3$  at different deposition conditions