

# Environmental Science Processes & Impacts

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## Environmental Impact

Municipal wastewater treatment plants (WWTPs) act as a major barrier to reduce the release of endocrine disrupting chemicals (EDCs) into the environment. The co-existence of free and conjugated estrogens and the interference from complex matrices often lead to largely variable detected concentrations and sometimes even negative removal efficiencies of typical EDCs in WWTPs. In this study, a highly selective and sensitive method was developed for simultaneous extraction, elution, and detection of 12 EDCs (including 6 conjugated estrogens) in both wastewater and sludge with enhanced sample pretreatment and UPLC-MS/MS. By using the developed method, the behavior of target EDCs in a local anaerobic/anoxic/oxic treatment plant was clarified. This study helps to better understand the behavior and fate of typical EDCs (particularly conjugates) in WWTPs.

Submission to E.S.P.I.

By Zhu et al.

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11 4 **Simultaneous detection of endocrine disrupting chemicals including**  
12 **conjugates in municipal wastewater and sludge with enhanced sample**  
13 **pretreatment and UPLC-MS/MS**  
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**ABSTRACT**

The co-existence of free and conjugated estrogens and the interference from complex matrices often lead to largely variable detected concentrations and sometimes even negative removal efficiencies of typical endocrine disrupting chemicals (EDCs) in wastewater treatment plants (WWTPs). In this study, a highly selective and sensitive method was developed for simultaneous extraction, elution, and detection of 12 EDCs (i.e., 4 free estrogens, 6 conjugated estrogens, and 2 phenolic compounds) in municipal wastewater and sludge. Sample pretreatment and ultra performance liquid chromatography-tandem mass spectrometry detection were optimized to improve the detection selectivity and sensitivity. Results indicate that the additional purification process was highly effective in reducing the matrix interference, and the limits of quantification reached as low as 0.04–2.2 ng L<sup>-1</sup> in wastewater and 0.05–4.9 ng g<sup>-1</sup> in sludge for all target EDCs. The developed method was successfully applied to explore the behavior of target EDCs in a local WWTP. The conjugates occupied a considerable portion (4.3–76.9% in molar ratio) of each related estrogen in the influent. Most of the target EDCs could not be completely removed in WWTPs, thus posing a potential threat to aquatic ecosystems.

**Keywords:** Endocrine disrupting chemicals; Conjugates; Wastewater treatment plant; Enhanced sample pretreatment; UPLC-MS/MS

## 1. Introduction

Endocrine disrupting chemicals (EDCs), typically steroidal estrogens including estrone (E1), 17 $\beta$ -estradiol (E2), estriol (E3), and 17 $\alpha$ -ethynylestradiol (EE2) and endocrine disrupting phenolic compounds including bisphenol A (BPA) and 4-nonylphenol (NP), have drawn much attention in recent years because they may alter the normal hormone functions and physiological status in wildlife and humans.<sup>1</sup> In China, about 790,000 tons of BPA and 41,000 tons of NP were produced and consumed in 2011 (Chinese Statistical Bureau, <http://www.stats.gov.cn>), and over 10.6 tons of natural estrogens (converted to E2 equivalent) are excreted by humans, livestock, and poultry every year.<sup>2</sup> As a consequence, these compounds have been widely detected in China's surface waters at concentration levels approximately ranging from 1 ng L<sup>-1</sup> (E3) to 33  $\mu$ g L<sup>-1</sup> (NP),<sup>3</sup> which may induce potential ecological risks such as decreasing fertility and causing feminization in fish.<sup>4</sup>

Municipal wastewater treatment plants (WWTPs) act as a major barrier to reduce the release of EDCs into the environment.<sup>5</sup> The occurrence, behavior and fate of EDCs in WWTPs have been extensively investigated.<sup>6,7</sup> However, most of the previous researches only focused on free estrogens and often reported largely variable detected concentrations and sometimes even negative removal efficiencies in WWTPs.<sup>8,9</sup> The reason behind lies in that estrogens are excreted primarily in sulfate and glucuronide conjugated forms in urine and feces, which can readily be transformed to free forms in biological wastewater treatment processes.<sup>10</sup> As a result, an underestimation of removal efficiency will inevitably occur if the conjugated forms

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4 64 occupy a considerable portion of the total estrogens.<sup>8</sup> This necessitates the detection  
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6 65 of conjugated estrogens in WWTPs when investigating the behavior and fate of  
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9 66 EDCs.

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11 A number of analytical methods have been developed to identify and quantify  
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14 68 typical EDCs in municipal wastewater and sludge;<sup>11</sup> however, few methods have  
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16 69 achieved simultaneous extraction and detection of both free and conjugated estrogens.  
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19 70 Conjugated estrogens cannot be directly analyzed by gas chromatography and mass  
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21 71 spectrometry (GC-MS) or bioassays but need to undergo an enzymatic or acidic  
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24 72 hydrolysis to free forms prior to analysis.<sup>12,13</sup> This renders the detection methods  
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27 73 rather complicated and cannot differentiate the original forms of conjugated estrogens.

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29 74 Recently, ultra performance liquid chromatography-tandem mass spectrometry  
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31 75 (UPLC-MS/MS) has become a major means to detect free and conjugated estrogens in  
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34 76 wastewater, sludge and other environmental matrices;<sup>14-16</sup> however, most of the  
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36 77 earlier developed methods had to detect free and conjugated estrogens separately,<sup>15</sup> or  
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39 78 were not able to extract glucuronide conjugates simultaneously.<sup>14</sup> In addition, LC is  
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41 79 more easily interfered by sample matrix than GC, which considerably reduces the  
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44 80 detection sensitivity.<sup>17</sup> Although using tandem mass can reduce the possibility of false  
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47 81 positives and thus increase the detection selectivity, co-eluted impurities from sample  
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49 82 pretreatment process may significantly suppress the ionization of target analytes.<sup>18</sup>  
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52 83 Hence, much effort has been put to reduce matrix interference through improving  
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54 84 sample pretreatment (e.g., applying extra rinsing steps and/or purification cartridges)  
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57 85 to further clean up samples.<sup>15,19</sup> However, these approaches are usually designated for  
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86 a single group of EDCs (e.g., conjugates).

87 Therefore, this study aimed to develop a highly selective and sensitive method  
88 for simultaneous detection of 12 EDCs (including 4 free estrogens, 6 conjugated  
89 estrogens, BPA, and NP) in municipal wastewater and sludge. Both sample  
90 pretreatment and UPLC-MS/MS detection were optimized to simultaneously extract,  
91 elute, and detect all target EDCs with minimized matrix interference, which  
92 significantly improved the detection selectivity and sensitivity. The calibration  
93 linearity, method recovery, and limit of quantification (LOQ) were all assessed for  
94 method validation. Afterwards, the developed method was applied to explore the  
95 behavior of target EDCs (particularly conjugates) in a WWTP located in Beijing,  
96 China.

## 97 **2. Materials and methods**

### 98 *2.1. Chemicals*

99 E1, E2, E3, EE2, and BPA standards were purchased from Dr. Ehrenstorfer  
100 GmbH (Augsburg, Germany; purity > 99.0%), and 4-NP (> 95.0%, CAS 25154-52-3)  
101 was from Tokyo Kasei Kogyo Co. (Tokyo, Japan). Sodium salts of 6 conjugated  
102 estrogens (> 95% purity), including estrone 3- $\beta$ -D-glucuronide (E1-3G),  $\beta$ -estradiol  
103 3- $\beta$ -D-glucuronide (E2-3G),  $\beta$ -estradiol 17- $\beta$ -D-glucuronide (E2-17G), estrone  
104 3-sulfate (E1-3S),  $\beta$ -estradiol 3-sulfate (E2-3S), and estriol 3-sulfate (E3-3S) were  
105 purchased from Sigma Aldrich China (Shanghai, China). Three surrogate standards,  
106 including E2-d<sub>2</sub> ( $\geq$  98%), BPA-d<sub>16</sub> ( $\geq$  98%), and E2-3S-d<sub>4</sub> (50% Tris), were supplied  
107 by CDN Isotopes (Quebec, Canada).

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4 108 High performance liquid chromatography (HPLC) grade methanol (MeOH),  
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6 109 methyl *t*-butyl ether (MTBE), acetonitrile (ACN), dichloromethane (DCM), and  
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9 110 acetone (ACE) were purchased from Fisher Scientific (Geel, Belgium). Milli-Q (MQ)  
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11 111 water was produced with a Millipore purification system (Advantage A10, Millipore,  
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13 112 Bedford, US). HPLC grade ammonia (25% NH<sub>4</sub>OH in water, by weight) was  
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15 113 purchased from Sigma Aldrich China. The stock solutions of target EDCs and  
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17 114 surrogate standards were individually prepared by dissolving each compound in  
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19 115 MeOH at a concentration of 1000 mg L<sup>-1</sup> and stored at -20°C in refrigerator.  
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21 116 Na<sub>2</sub>EDTA-McIlvaine buffer (MB) was prepared by dissolving 21.00 g citric acid  
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23 117 monohydrate, 17.75 g Na<sub>2</sub>HPO<sub>4</sub>, and 60.50 g Na<sub>2</sub>EDTA·2H<sub>2</sub>O in 1.625 L of deionized  
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25 118 water, with the pH adjusted to 4.00 ± 0.05.<sup>20</sup>

## 31 32 119 2.2. Sample collection

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34 120 Wastewater and sludge samples were collected from a municipal WWTP located  
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36 121 in Beijing, China, which primarily adopts an anaerobic/anoxic/oxic (A/A/O)  
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38 122 biological treatment process. The sampling points are illustrated in Fig. S1, except  
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40 123 digested sludge samples which were collected from a sludge digestion tank. The  
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42 124 samples of excess sludge and digested sludge were grabbed three times on a sampling  
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44 125 day (i.e., in the morning, noon, and evening) and mixed together. All other samples  
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46 126 were acquired as the flow-proportional (24 h) mixture by using electronic  
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48 127 auto-samplers (SD900, Hach, Loveland, CO, US). The samples were stored in 4 L  
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50 128 amber glass bottles, in which 1% MeOH (v/v) was pre-added to inhibit microbial  
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52 129 activity, and transported immediately to laboratory.

### 130 2.3. Sample pretreatment

131 The sample pretreatment procedures were optimized stepwise, as detailed in Fig.  
132 1. Wastewater samples, including the influent, mixed liquor from each treatment unit  
133 of the A/A/O process, and effluent, were centrifuged at 6000 revolutions per minute  
134 (rpm) for 10 min. The supernatant (400 mL each) was adjusted to pH 3.0 with 40%  
135 H<sub>2</sub>SO<sub>4</sub> (v/v), filtered through GF/F glass microfiber filters (0.7 μm, Whatman, UK),  
136 spiked with the surrogate standard solutions (i.e., 50 ng L<sup>-1</sup> E2-3S-d<sub>4</sub>, 100 ng L<sup>-1</sup>  
137 E2-d<sub>2</sub>, and 200 ng L<sup>-1</sup> BPA-d<sub>16</sub>), stored at 4 °C in refrigerator, and subjected to  
138 solid-phase extraction (SPE) within 24 h.

#### 139 Fig. 1

140 Sludge samples (i.e., excess and digested) were centrifuged at 6000 rpm for 10  
141 min to collect solid particles. The solid particles, as well as the mixed liquor  
142 suspended solids from each treatment unit of the A/A/O process, were freeze-dried  
143 under vacuum (FD-1-50, Boyikang, China), homogenized using a mortar and pestle,  
144 and sieved to obtain the desired particles (diameter ≤ 0.5 mm). One gram of the  
145 sieved particles was weighted and placed into a 10 mL glass centrifuge tube, spiked  
146 with the surrogate standard solutions (i.e., 20 ng g<sup>-1</sup> E2-3S-d<sub>4</sub>, 40 ng g<sup>-1</sup> E2-d<sub>2</sub>, and 80  
147 ng g<sup>-1</sup> BPA-d<sub>16</sub>), vortexed vigorously to mix the surrogate standards with the sludge  
148 particles, and subjected to ultrasonic solvent extraction (USE). Each sample was  
149 added with a test extraction solvent (5 mL, as detailed in Section 3.2), vortexed  
150 vigorously, ultrasonicated for 10 min, and centrifuged at 5000 rpm for 8 min to collect  
151 the supernatant. The USE was continuously performed for three times, and the

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4 152 supernatants were mixed together, diluted to a total volume of 400 mL with MQ water,  
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6 153 filtrated through GF/F glass microfiber filters, adjusted to pH 3.0 with 40% H<sub>2</sub>SO<sub>4</sub>  
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9 154 (v/v), stored at 4 °C in refrigerator, and subjected to SPE within 24 h

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11 155 An Oasis HLB cartridge (500 mg/6 mL, Waters), after being activated by 5 mL  
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14 156 each of MTBE, MeOH, and MQ water, was applied to concentrate the  
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16 157 above-pretreated wastewater or sludge sample at a flow rate of 3–5 mL min<sup>-1</sup>.  
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18 158 Thereafter, the cartridge was sequentially rinsed with 5 mL each of 10% MeOH  
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21 159 aqueous solution, MQ water (pH 3.0), 2:10:88 NH<sub>4</sub>OH/MeOH/MQ water (v/v/v, pH  
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24 160 11.0), and 30% MeOH aqueous solution to eliminate impurities from sample matrix,  
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26 161 and then was dried under vacuum.

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29 162 Before elution, a Sep-pak C18 cartridge (500 mg/6 mL, Waters), pre-activated by  
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31 163 5 mL of the test eluent, was connected below the dried HLB cartridge to further clean  
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34 164 the impurities. For sludge samples, 0.5 g Al<sub>2</sub>O<sub>3</sub> and 1.0 g Na<sub>2</sub>SO<sub>4</sub> were sequentially  
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36 165 packed into its headspace to retain the co-eluted impurities and dehydrate the eluate  
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39 166 from the HLB cartridge, respectively. Nie et al.<sup>21</sup> reported a post-SPE cleanup  
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41 167 procedure by using a laboratory-made glass column, which was filled with anhydrous  
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44 168 Na<sub>2</sub>SO<sub>4</sub>, neutral Al<sub>2</sub>O<sub>3</sub>, and silica gel from top to bottom, to reduce the co-eluted  
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46 169 impurities. Afterwards, the HLB cartridge was eluted with 2 × 4 mL of a selected  
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49 170 eluent. The eluates were collected into a 10 mL conical-bottomed glass tube, placed in  
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52 171 a water bath at 35 °C, and dried under a gentle stream of N<sub>2</sub>. The dried residue was  
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54 172 immediately reconstituted with 200 μL of 9:1 MQ water/MeOH (v/v) for  
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56 173 UPLC-MS/MS detection.  
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## 174 2.4. UPLC-MS/MS analysis

175 An Agilent 1290 UPLC system, equipped with a BEH-C18 column (100 mm ×  
176 2.1 mm, 1.7 μm, Waters) at a constant temperature of 30 °C, was used for separation  
177 of target analytes. The injection volume was 10 μL. The mobile phases consisted of  
178 MQ water (A) and a mixed solvent of 1:1:8 MeOH/MQ water/ACN (v/v/v) (B), with  
179 each containing 7.5 mmol L<sup>-1</sup> NH<sub>4</sub>OH to improve the ionization efficiency in the  
180 tandem MS system. The mobile phases had a total flow rate of 0.2 mL min<sup>-1</sup> and a  
181 gradient elution program (time in min, % mobile phase B) as follows: (0, 10), (5, 40),  
182 (5.1, 50), (8, 50), (13, 70), (14, 100), (17, 100), (17.1, 10), and (21, 10). All 12 target  
183 EDCs could be eluted within 18 min.

184 An Agilent 6420 triple quadrupole MS, operated in the negative electrospray  
185 ionization (ESI(-)) mode with a capillary voltage of 3.5 kV, was used to detect target  
186 analytes. Multiple reaction monitoring (MRM) mode was adopted for data acquisition.  
187 The operational parameters of the tandem MS, including fragmentor voltage, and  
188 product ions and associated cone energies, were optimized for each analyte, as listed  
189 in [Table S1](#).

## 190 2.5. Method validation

191 The method was validated by measuring the calibration linearity, inter- and  
192 intra-day precisions, method recoveries, and LOQs. For each analyte, a 10-point  
193 calibration curve was established with concentrations ranging from 5 to 5000 ng L<sup>-1</sup>  
194 for NP and 0.5 to 500 ng L<sup>-1</sup> for all other analytes. The intra-day precision was  
195 evaluated by analyzing the target EDCs at three concentration levels (i.e., 5, 50 and

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4 196 500 ng L<sup>-1</sup>, spiked in MQ water) every four hours for three times under the routine  
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6 197 use of the developed method, and the inter-day precision was assessed by repeating  
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8 198 the intra-day analysis every two days for three times.

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11 199 To determine the method recoveries of target EDCs in wastewater, 200 µL of a  
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13 200 mixed standard solution prepared in MeOH (containing 50 µg L<sup>-1</sup> of each conjugate,  
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15 201 100 µg L<sup>-1</sup> of each free estrogen and BPA, and 1000 µg L<sup>-1</sup> of NP) was spiked into a  
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17 202 400 mL wastewater sample. To determine the method recoveries in sludge, certain  
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19 203 volumes (200 and 600 µL) of the above mixed standard solution were spiked into 1.0  
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21 204 g of the freeze-dried and sieved aerobic sludge (as reference matrix) to achieve the  
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23 205 low and high concentration levels, respectively. The spiked wastewater and sludge  
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25 206 samples, together with their raw samples (to measure the background concentrations  
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27 207 of target EDCs), were pretreated (Fig. 1) and analyzed by UPLC-MS/MS. The method  
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29 208 recovery of each analyte was calculated as follows:

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$$Recovery(\%) = \frac{C_{spi} - C_{raw}}{C_{std}} \times 100 \quad (1)$$
  
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40 210 where  $C_{spi}$ ,  $C_{raw}$  and  $C_{std}$  are the concentrations of a target analyte in the spiked sample,  
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42 211 raw sample and standard solution, respectively. The LOQ in wastewater or sludge was  
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44 212 determined separately by spiking a mixed standard solution into the SPE eluate,  
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46 213 which was then serially diluted to find an analyte concentration that provided a signal  
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48 214 to noise ratio of 10:1.<sup>22</sup>

### 53 215 **3. Results and discussion**

#### 54 216 *3.1. Optimization of UPLC-MS/MS operational parameters*

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4 217 The operational parameters of MS/MS were optimized under the ESI(-) mode by  
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6 218 directly injecting 1000  $\mu\text{g L}^{-1}$  standard solution of each analyte into the tandem MS.  
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9 219 Because of the instable ion fragmentations in the collision cell when the steroidal  
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11 220 rings were cleaved to form product ions, a “broad” selection mode (allowing ions with  
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13 221  $\pm 0.3$  m/z shift to enter the MS2 detector rather than the instrument default “unit”  
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15 222 selection mode with  $\pm 0.1$  m/z shift) was employed to identify the product ions of four  
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17 223 free estrogens (i.e., E1, E2, E3, EE2). For example, the 145.18 m/z ion was formed as  
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19 224 a major product ion from the fragmentation of E2 (Fig. S2a). Its signal peak could  
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21 225 alter by 0.2 m/z in the MS2 scan mode among different injections (e.g., between the  
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23 226 1<sup>st</sup> and 2<sup>nd</sup> injections), and alter by 0.1 m/z among different retention times in the  
24  
25 227 same injection (e.g., between the retention times of 3.642 and 3.706 min in the 2<sup>nd</sup>  
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27 228 injection) (Fig. S2b). Hence, the default “unit” selection mode may considerably  
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29 229 reduce the response of product ions. By using the “broad” selection mode, the  
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31 230 detection sensitivity of product ions could be enhanced by at least 4 folds.  
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39 231 Various UPLC conditions were tested to improve the resolution and sensitivity of  
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41 232 target EDCs. Relatively smooth alteration of mobile phase ratios was employed in the  
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43 233 first 13 min to achieve an effective separation of 11 analytes, and then the ratio of  
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45 234 mobile phase B was rapidly raised to elute NP. The total-ion MRM chromatogram of  
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47 235 12 EDCs is shown in Fig. 2. Except the three deuterated standards that were co-eluted  
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49 236 with their non-deuterated counterparts (i.e., E2-3S, BPA, and E2), all other EDCs  
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51 237 were well separated.  
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**Fig. 2**

## 239 3.2. USE optimization

240 It was reported that 1:1 MeOH/ACE (v/v) could efficiently extract free estrogens  
241 and phenolic EDCs from sludge in the USE process.<sup>21</sup> In addition, an acidic buffer  
242 (e.g., MB or citric acid (CA)) in combination with an organic solvent has also been  
243 proved efficient for extracting free estrogens from soils.<sup>23</sup> To extract conjugated  
244 estrogens from sludge, a mixed solvent of MeOH/DCM or MeOH/ACE was used in  
245 an accelerated solvent extraction (ASE) process,<sup>14,24</sup> however, the suitable extraction  
246 solvent for conjugates in the USE process has never been reported. In the present  
247 study, MeOH, MB, CA, and their pair-wise combinations (1:1 of MeOH/MB,  
248 MeOH/CA, and MeOH/ACE) were examined individually for simultaneous  
249 extraction of all 12 target EDCs from sludge.

250 The extraction efficiency of each target analyte is shown in Fig. 3. MeOH  
251 showed an acceptable extraction efficiency for most free estrogens (i.e., E1, E2, EE2)  
252 and phenolic compounds, but a low efficiency (< 50%) for E3 (relatively hydrophilic,  
253  $\log K_{ow} = 2.81$ ), E2-3G, E2-17G, and E3-3S. CA and MB were effective in extracting  
254 the conjugates but failed to extract the phenolic compounds (< 40%). Although 1:1  
255 MeOH/ACE was reported to be effective in extracting both free and conjugated  
256 estrogens in the ASE process,<sup>14</sup> it was ineffective in extracting most conjugates in the  
257 USE process. Both 1:1 MeOH/CA and 1:1 MeOH/MB could simultaneously extract  
258 most of the target EDCs with an acceptable efficiency (> 50%). Because 1:1  
259 MeOH/MB exhibited a better extraction efficiency for E1-3S, EE2 and NP, it was  
260 selected as the optimal extraction solvent in the USE process. Using this solvent, all

261 target EDCs could be extracted with an efficiency ranging from 57.1% to 109.4%.

262 **Fig. 3**

### 263 3.3. SPE optimization

264 HLB cartridge is commonly used in the SPE process because it contains both  
265 hydrophobic and hydrophilic units to retain a wide range of compounds. However,  
266 this advantage also makes it less selective in a complex matrix. In this regard, a  
267 four-step sequential rinsing procedure was developed to reduce the matrix  
268 interference (Fig. 1). The first three solvents with an increasing polarity (i.e., 10%  
269 MeOH, MQ water (pH 3.0), and 2:10:88 NH<sub>4</sub>OH/MeOH/MQ water (pH 11.0)) were  
270 used to rinse off the retained hydrophilic matrix compounds, while the fourth solvent  
271 (i.e., 30% MeOH) was used to rinse off the retained hydrophobic compounds.

272 After connection of a Sep-pak C18 cartridge to the rinsed and vacuum dried  
273 HLB cartridge, sequential elutions with 3:2 DCM/ACE (v/v), MeOH, and MeOH  
274 containing 5% NH<sub>4</sub>OH (by weight) were performed to determine the optimal eluent  
275 composition. The cumulative recoveries of each target analyte by different eluents are  
276 presented in Fig. 4. Results show that the first elution with DCM/ACE was effective  
277 for the free estrogens and phenolic compounds (recovery = 82–110%), but ineffective  
278 for the conjugates (recovery = 0–4%). The second elution with MeOH could elute  
279 most of the conjugates (recovery = 68–83%) and 16.8% of NP. However, the retained  
280 conjugates were resistant to further elution with a more polar eluent (i.e., MeOH  
281 containing 5% NH<sub>4</sub>OH), indicating a further increase in the eluent polarity was not  
282 necessary. Hence, a mixture of DCM/ACE and MeOH (3:2:5, v/v/v) was selected as

the optimal eluent in the SPE process.

**Fig. 4**

To evaluate the efficacy of the additional purification process (i.e., four-step sequential rinsing plus Sep-pak C18 cleanup), four different matrices, including the influent, effluent, aerobic sludge, and digested sludge collected from a local WWTP, were utilized to compare the matrix effects (ME%) between the purified and unpurified samples. The purified samples were spiked with 200  $\mu\text{L}$  of a mixed standard solution (100  $\mu\text{g L}^{-1}$  of each target analyte, prepared in MQ water) and subjected to the additional purification process (Fig. 1), whereas the unpurified samples were spiked identically but did not undergo the additional purification process. The ME% value was calculated as follows:

$$ME(\%) = \frac{A_{\text{spi}} - A_{\text{raw}}}{A_{\text{std}}} \quad (2)$$

where  $A_{\text{spi}}$ ,  $A_{\text{raw}}$  and  $A_{\text{std}}$  are the signal responses of a target analyte in the spiked sample, raw sample and standard solution, respectively. To reflect the real matrix interference (i.e., signal suppression or enhancement), surrogate standard correction was not adopted for the ME% calculation.

Fig. 5 shows that the additional purification process could obviously reduce the matrix interference for both wastewater and sludge samples. The ME% values of almost all target EDCs (except NP) in the unpurified samples were considerably lower than those in the purified samples, implying that both wastewater and sludge matrices severely suppressed the signal responses. On the contrary, the signal response of NP was significantly enhanced by the unpurified sludge matrix (ME% = 129–133). The

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4 305 total-ion MRM chromatograms of all target EDCs in the standard solution, unpurified  
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6 306 sludge sample, and purified sludge sample are comparatively illustrated in Fig. S3,  
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9 307 which demonstrates that the additional purification process was highly effective in  
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11 308 reducing the matrix interference.

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14 309 **Fig. 5**

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17 310 *3.4. Method validation*

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19 311 The calibration curve of each target analyte exhibited a good linearity ( $R^2 > 0.99$ )  
20  
21 312 over a broad concentration range (Table S1). The intra- and inter-day precisions are  
22  
23 313 expressed by the recovery and relative standard deviation (RSD) values of repeated  
24  
25 314 analyses. Table S2 shows that in the intra-day precision tests, the recoveries of target  
26  
27 315 analytes ranged from 86.3 to 110.7% for all three concentration levels, with RSD  
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29 316 values below 15%. Meanwhile, in the inter-day precision tests, the recoveries ranged  
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31 317 from 84.3 to 107.7%, with RSD values below 19%. Both intra- and inter-day  
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33 318 precisions confirmed the good repeatability of the developed method.

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39 319 As shown in Table 1, the majority of recovery efficiencies were within the range  
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41 320 of 70–120% and all the RSD values were below 20% (as recommended by the U.S.  
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43 321 EPA) in different test matrices, which ensures the accuracy and robustness of the  
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45 322 developed method. Only a few recovery efficiencies of E3 (130.9%), E1-3G  
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47 323 (48.5–66.5%), E2-17G (68.5% and 68.2%), and E1-3S (63.5%) in wastewater and  
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49 324 sludge exceeded the recommended range to some extent, but these recoveries were  
50  
51 325 quite stable as reflected by their RSD values (i.e., 2.9–13.4%). On the whole, the  
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53 326 recovery efficiency deviated farther from the ideal value (100%) as the sample matrix  
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327 became more complex (i.e., from MQ water to effluent, influent, and sludge).

328 **Table 1**

329 In MQ water, the LOQs of 12 target EDCs ranged from 0.03 to 1.1 ng L<sup>-1</sup>. In the  
330 influent and effluent, the LOQs were in the ranges of 0.07–2.2 and 0.04–1.4 ng L<sup>-1</sup>,  
331 respectively. Several earlier developed methods for detection of free or conjugated  
332 estrogens reported the LOQs of 0.5–30,<sup>10</sup> 0.4–3.0,<sup>15</sup> and 15–75 ng L<sup>-1</sup> <sup>25</sup> in the  
333 influent and effluent of WWTPs. In the sludge, the LOQs of free estrogens,  
334 conjugated estrogens, and NP were 0.5–3.4, 0.05–1.5, and 4.9 ng g<sup>-1</sup>, respectively;  
335 which are considerably lower than the previously reported values (i.e., 1.2–10.0,  
336 0.3–5.0, and 188.1 ng g<sup>-1</sup>, correspondingly).<sup>14,21,26</sup> This result demonstrates that the  
337 additional purification process could significantly improve the detection sensitivity,  
338 which makes the developed method well applicable to the detection of target EDCs in  
339 both wastewater and sludge of WWTPs.

### 340 3.5. Method application

341 The developed method was applied to determine the concentrations of target  
342 EDCs along the A/A/O treatment process in a local WWTP. The major characteristics  
343 of the influent and effluent of this WWTP are shown in [Table S3](#). All target EDCs  
344 were detected in the influent with a maximum concentration of 333 ng L<sup>-1</sup> (E1) for  
345 free estrogens, 39.1 ng L<sup>-1</sup> (E3-3S) for conjugated estrogens, and 2319 ng L<sup>-1</sup> (NP)  
346 for phenolic compounds ([Table 2](#)). It should be noticed that the conjugates (sulfate  
347 plus glucuronide) occupied 4.3%, 76.9% and 25.5% (molar ratio) of the total E1, E2  
348 and E3, respectively, implying that a considerable portion of estrogens entered the

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4 349 WWTP in conjugated forms. Liu et al.<sup>27</sup> also reported similar conjugate  
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6 350 concentrations in the influent of a municipal WWTP located in Osaka, Japan, where  
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8 351 the concentrations of E1-3S/E1-3G and E3-3S were measured to range from 3.2 to  
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11 352 21.9 ng L<sup>-1</sup>. However, the conjugates in their study occupied 33.2% and 100.0%  
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14 353 (molar ratio) of the total E1 and E3, respectively. The different molar ratios could  
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16 354 partly arise from the different sampling seasons (i.e., April in this study and January  
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18 355 in their study) because the enzymatic hydrolysis of conjugated estrogens in sewer  
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21 356 pipes is promoted at an increased wastewater temperature.<sup>28</sup>  
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#### 24 **Table 2**

25  
26 358 After entering the anaerobic zone, E1, EE2, BPA, and NP were removed quite  
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28 359 effectively in wastewater but were found to be abundant in sludge, probably because  
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31 360 of their relatively high LogK<sub>ow</sub> values (> 3.0) which facilitated their absorption onto  
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34 361 sludge particles.<sup>7</sup> E2 exhibited an increased concentration in wastewater, which  
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36 362 probably arose from the effective transformation of E2-3G and E2-17G via  
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38 363 enzymes,<sup>10</sup> as evidenced by their negligible concentrations in both wastewater and  
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41 364 sludge. E2-3S was significantly distributed in sludge, whose release from sludge  
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44 365 might explain its increased concentration in wastewater. The concentrations of E3 and  
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46 366 E3-3S in wastewater maintained nearly constant after entering the anaerobic zone.

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48 367 In the anoxic and oxic zones, the concentrations of free estrogens and phenolic  
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51 368 compounds continuously decreased in wastewater and sludge, probably because of the  
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54 369 co-metabolic degradation by nitrifying bacteria.<sup>5</sup> The glucuronide conjugates were  
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57 370 rarely detected, while the sulfate conjugates appeared to persist in wastewater and  
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4 371 sludge although some decay was observed for E1-3S and E3-3S. It was reported that  
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6 372 more enzymes are usually present for glucuronide conjugates than for sulfate  
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9 373 conjugates in biological treatment processes.<sup>10</sup>

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11 374 In the effluent and excess sludge, only EE2 and the glucuronide conjugates were  
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13 375 completely removed. E1, E2, E3, and their sulfate conjugates were still detectable  
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15 376 with concentration ranges of 1.8–14.8 ng L<sup>-1</sup> and 0.4–16.1 ng g<sup>-1</sup> in the effluent and  
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17 377 excess sludge, respectively. A considerable amount of BPA and particularly NP would  
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19 378 be released into the environment through effluent discharge and sludge disposal. It is  
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21 379 seen that most of the target EDCs could not be completely removed by the wastewater  
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23 380 treatment processes, thus posing a potential threat to aquatic ecosystems. In addition,  
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25 381 the results demonstrate that the removal efficiency of estrogens can be significantly  
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27 382 underestimated if the conjugated forms are ignored. Taking E2 as example, its  
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29 383 removal efficiency was 58.0% if only considering the free form, but could reach 83.4%  
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31 384 if considering both the free and conjugated forms.

#### 385 **4. Conclusions**

386 This study developed a highly selective and sensitive method for simultaneous  
387 extraction, elution, and detection of 12 EDCs (i.e., 4 free estrogens, 6 conjugated  
388 estrogens, and 2 phenolic compounds) in both wastewater and sludge of WWTPs.

389 Based on the experimental results, the following conclusions can be drawn:

- 390 • 1:1 MeOH/MB and 3:2:5 DCM/ACE/MeOH (by volume) were the optimal  
391 extraction solvents in the USE and SPE processes, respectively. The additional  
392 purification process (i.e., four-step sequential rinsing plus Sep-Pak C18 cartridge

- cleanup) was highly effective in reducing the matrix interference.
- The LOQs of 12 target EDCs were in the ranges of 0.04–2.2 ng L<sup>-1</sup> and 0.05–4.9 ng g<sup>-1</sup> in the wastewater (i.e., influent and effluent) and sludge, respectively. The majority of recovery efficiencies were within the range of 70–120% and all RSD values were below 20%, which ensures the detection accuracy and precision.
  - The developed method was applied to explore the behavior of target EDCs in a local WWTP. All 12 target EDCs were detected in the influent, where the conjugates occupied a considerable portion (4.3–76.9% in molar ratio) of each related estrogen (i.e., E1, E2, and E3). Only EE2 and the glucuronide conjugates were completely removed in the effluent and excess sludge, while other studied EDCs were partially removed by the wastewater treatment processes.
  - Further research should be conducted to clarify the transformation mechanism of conjugated estrogens in WWTPs and assess the potential ecological risk of residual EDCs in the effluent and excess sludge.

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## Appendix A. Supplementary information

Supplementary data associated with this article can be found in the online version

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**Figure Captions**

- 467
- 468 Fig. 1 Schematic diagram of the optimized sample pretreatment procedures.
- 469 Fig. 2 Total-ion MRM chromatogram of 12 target EDCs and 3 surrogate standards.
- 470 Fig. 3 Extraction efficiencies of different solvents for 12 target EDCs in the  
471 ultrasonic solvent extraction process (ACE: acetone; CA: citric acid; MB:  
472 McIlvaine buffer; MeOH: methanol).
- 473 Fig. 4 Cumulative recoveries of sequential elutions with different solvents for 12  
474 target EDCs in the solid-phase extraction process (ACE: acetone; DCM:  
475 dichloromethane; MeOH: methanol).
- 476 Fig. 5 Matrix effects of 12 target EDCs detected with/without additional  
477 purification in spiked wastewater and sludge samples (P: purified; UP:  
478 unpurified).
- 479

**Table 1**

Recoveries and limits of quantification (LOQs) for 12 target EDCs in MQ water, wastewater, and sludge.

Analyte	<u>MQ water</u>		<u>Influent</u>		<u>Effluent</u>		<u>Sludge</u>		
	Recovery (RSD <sup>a</sup> ) %	LOQ (ng L <sup>-1</sup> )	Recovery (RSD) %	LOQ (ng L <sup>-1</sup> )	Recovery (RSD) %	LOQ (ng L <sup>-1</sup> )	LL <sup>b</sup> Recovery (RSD) %	HL <sup>b</sup> Recovery (RSD) %	LOQ (ng g <sup>-1</sup> )
E1	106.7 (1.8)	0.2	112.9 (13.8)	0.1	103.9 (3.9)	0.1	85.8 (5.0)	106.2 (10.6)	0.5
E2	103.5 (2.5)	0.6	97.8 (3.9)	0.6	101.7 (4.2)	0.5	94.4 (9.4)	96.2 (2.4)	1.9
E3	98.4 (3.6)	0.5	130.9 (4.5)	1.5	97.3 (9.2)	0.9	75.4 (5.5)	93.4 (2.0)	1.0
EE2	97.8 (2.6)	0.9	80.9 (4.6)	0.8	122.4 (0.7)	0.8	94.4 (10.4)	83.5 (8.3)	3.4
BPA	111.8 (3.7)	0.5	107.1 (18.7)	1.0	103.4 (1.5)	0.7	92.6 (17.0)	93.7 (7.7)	1.2
NP	84.5 (14.0)	1.0	78.5 (1.5)	2.2	80.6 (11.9)	0.7	101.1 (8.2)	77.6 (9.4)	4.9
E1-3G	99.1 (8.0)	0.3	48.5 (3.8)	1.0	61.2 (3.0)	0.6	66.5 (5.1)	59.7 (7.9)	0.4
E2-3G	92.1 (5.8)	0.3	92.3 (7.3)	0.7	86.2 (4.4)	0.5	71.4 (13.7)	62.8 (5.5)	0.7
E2-17G	88.7 (5.3)	1.1	92.8 (7.4)	1.7	81.6 (3.7)	1.4	68.5 (9.9)	68.2 (2.9)	1.5
E1-3S	86.6 (1.5)	0.03	76.9 (2.9)	0.07	89.4 (2.5)	0.05	63.5 (13.4)	83.3 (6.3)	0.07
E2-3S	99.7 (0.6)	0.03	83.2 (3.3)	0.07	98.5 (1.5)	0.04	76.3 (7.0)	79.9 (9.5)	0.05
E3-3S	98.9 (1.2)	0.04	114.9 (2.3)	0.08	84.8 (5.3)	0.07	92.1 (9.9)	90.3 (9.3)	0.07

<sup>a</sup> Relative standard deviation,  $n = 3$ .

<sup>b</sup> LL: low concentration level (10 ng g<sup>-1</sup> of each conjugated estrogen, 20 ng g<sup>-1</sup> of each free estrogen and BPA, and 200 ng g<sup>-1</sup> of NP); HL: high concentration level (30 ng g<sup>-1</sup> of each conjugated estrogen, 60 ng g<sup>-1</sup> of each free estrogen and BPA, and 600 ng g<sup>-1</sup> of NP).

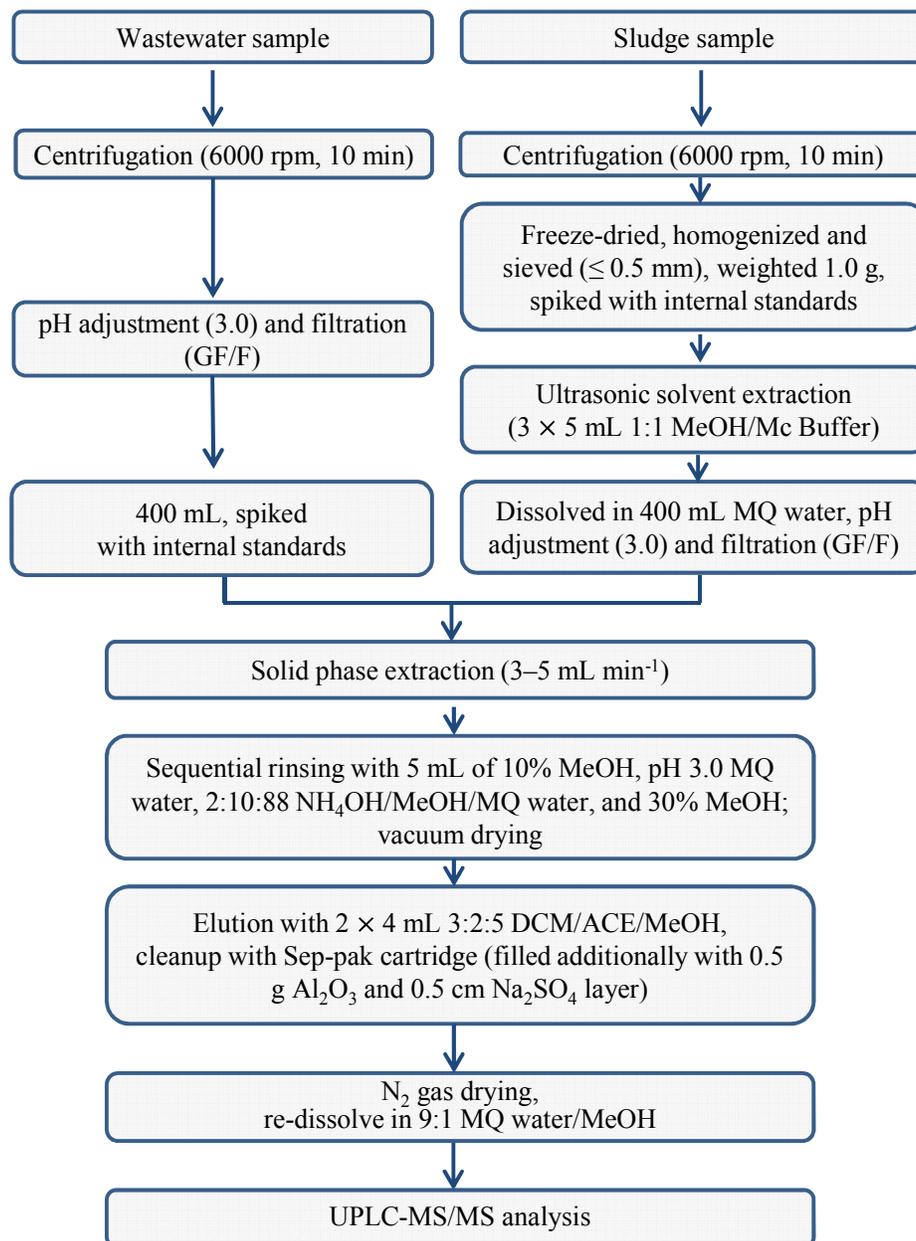
**Table 2**

Concentrations of 12 target EDCs in wastewater and sludge along the biological treatment process (A/A/O) in a local WWTP (April, 2013).

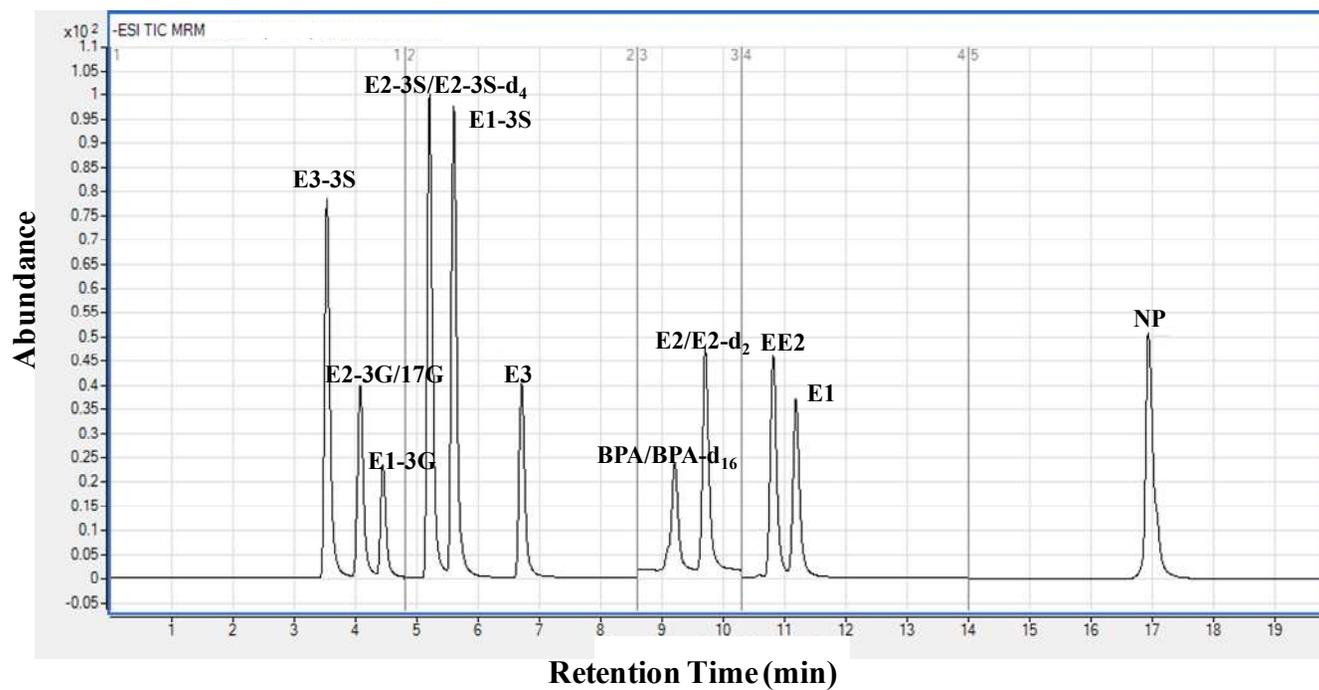
Analyte	<u>Influent</u>	<u>Anaerobic zone</u>		<u>Anoxic zone</u>		<u>Oxic zone</u>		<u>Effluent</u>	<u>Excess sludge</u>
	(ng L <sup>-1</sup> )	Wastewater (ng L <sup>-1</sup> )	Sludge (ng g <sup>-1</sup> )	Wastewater (ng L <sup>-1</sup> )	Sludge (ng g <sup>-1</sup> )	Wastewater (ng L <sup>-1</sup> )	Sludge (ng g <sup>-1</sup> )	(ng L <sup>-1</sup> )	(ng g <sup>-1</sup> )
E1	333 (4) <sup>a</sup>	159 (5)	53.6 (6.5)	54.0 (1.5)	38.7 (0.8)	16.3 (0.3)	17.9 (1.0)	14.8 (3.4)	16.1 (4.4)
E2	5.0 (0.7)	14.5 (1.0)	8.3 (0.7)	3.3 (0.5)	12.3 (1.4)	1.8 (0.4)	6.8 (0.1)	2.1 (0.3)	4.3 (0.5)
E3	89.0 (1.7)	84.8 (1.1)	42.6 (6.8)	37.0 (2.7)	25.0 (3.3)	6.7 (0.9)	3.9 (0.3)	2.1 (0.4)	1.9 (0.1)
EE2	28.6 (6.5)	<LOQ <sup>b</sup>	139 (3)	<LOQ	105 (16)	<LOQ	1.2 (0.7)	<LOQ	<LOQ
BPA	191 (10)	148 (7)	371 (58)	87.0 (10.8)	262 (39)	86.5 (8.9)	149 (10)	13.0 (0.6)	92.3 (5.1)
NP	2319 (17)	1496 (62)	13327 (3311)	917 (117)	6547 (16)	774 (56)	5983 (1437)	676 (11)	3579 (672)
E1-3G	3.6 (0.6)	<LOQ	<LOQ	<LOQ	<LOQ	<LOQ	<LOQ	<LOQ	<LOQ
E2-3G	13.3 (1.2)	1.2 (0.2)	<LOQ	1.0 (0.3)	<LOQ	0.9 (0.3)	<LOQ	<LOQ	<LOQ
E2-17G	10.5 (2.3)	<LOQ	<LOQ	<LOQ	<LOQ	<LOQ	<LOQ	<LOQ	<LOQ
E1-3S	16.5 (0.9)	9.0 (0.4)	<LOQ	3.4 (0.2)	<LOQ	1.6 (0.1)	<LOQ	1.9 (0.4)	0.7 (0.1)
E2-3S	2.7 (0.1)	9.2 (0.3)	10.2 (0.3)	1.8 (0.2)	13.3 (1.1)	1.3 (0.1)	17.3 (0.9)	1.8 (0.5)	11.0 (0.7)
E3-3S	39.1 (3.4)	39.0 (1.4)	1.3 (0.1)	8.5 (0.5)	0.7 (0.1)	5.0 (2.4)	0.7 (0.1)	2.0 (0.2)	0.4 (0.1)

<sup>a</sup> Mean concentration (SD),  $n = 3$ .

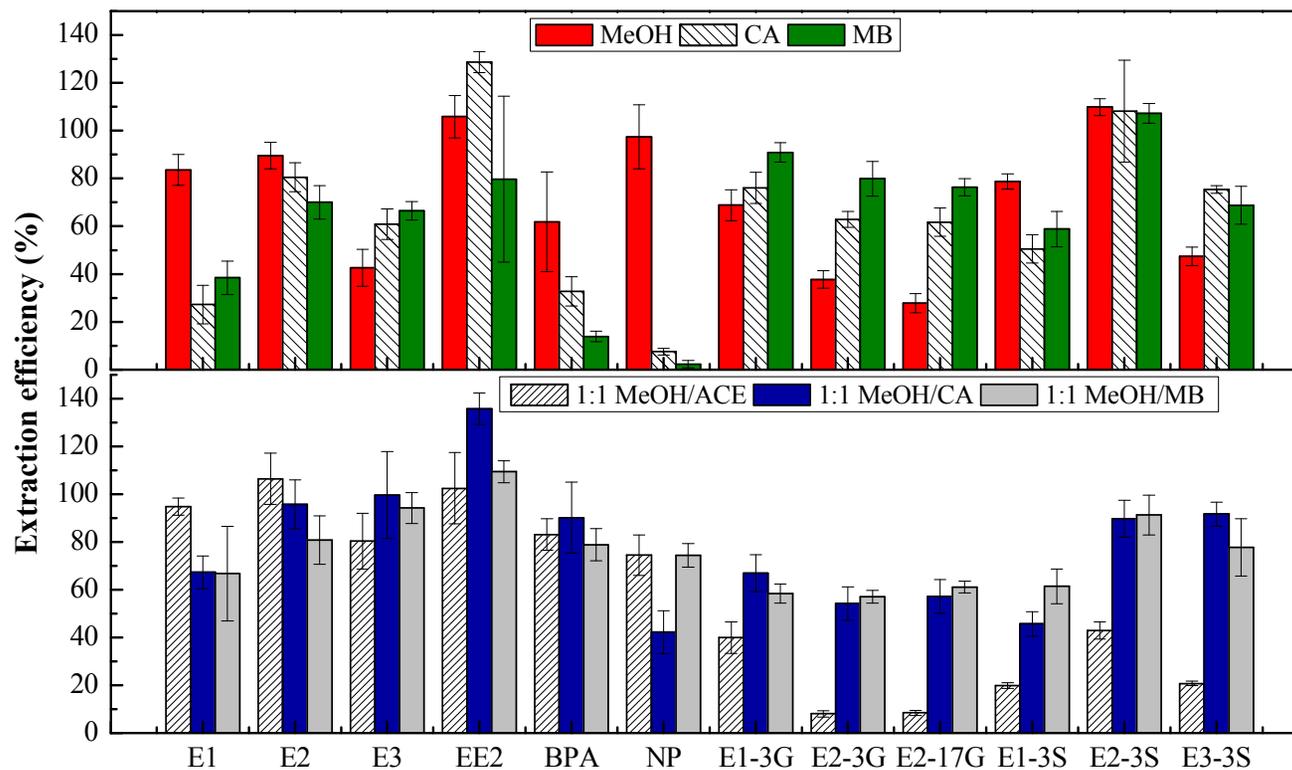
<sup>b</sup> The LOQs of target EDCs in wastewater and sludge are provided in [Table 1](#).



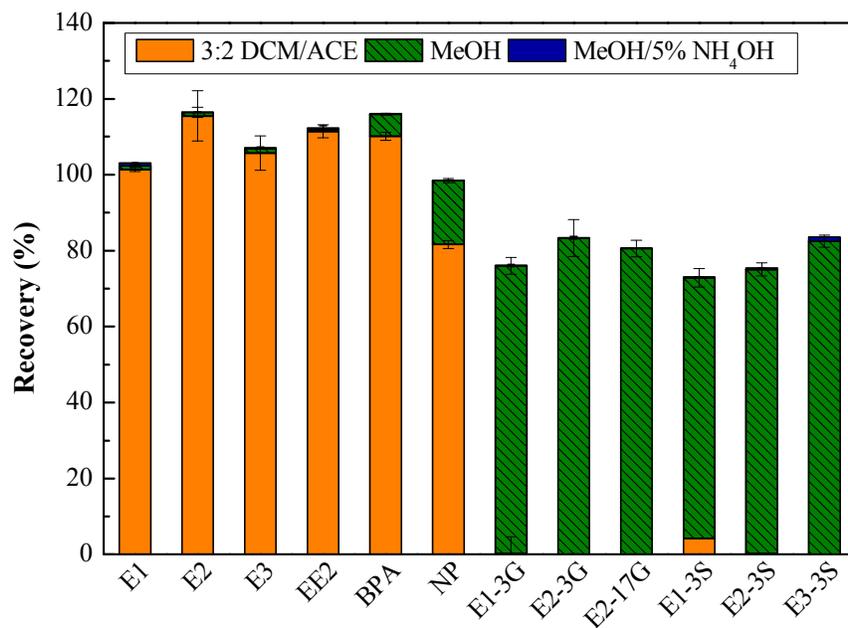
**Fig. 1.** Schematic diagram of the optimized sample pretreatment procedures.



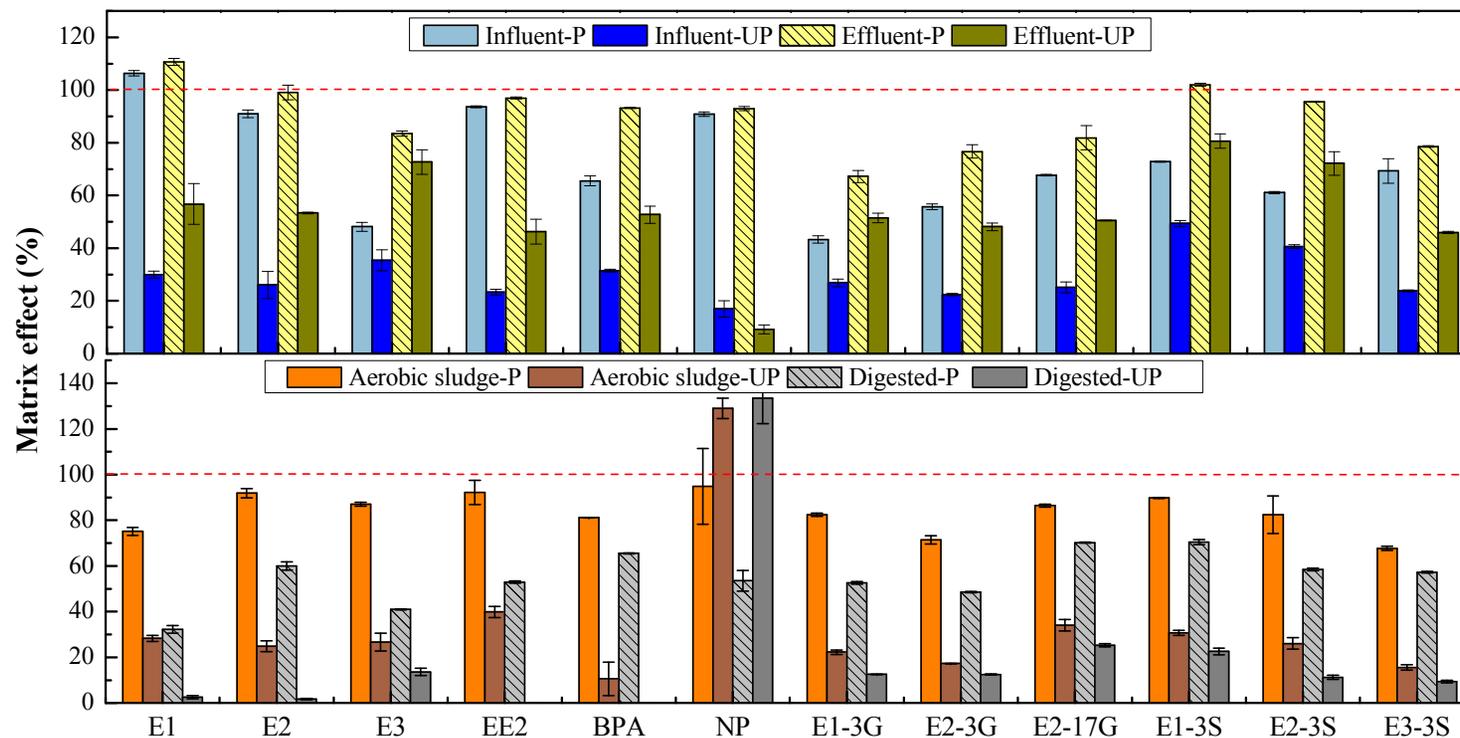
**Fig. 2.** Total-ion MRM chromatogram of 12 target EDCs and 3 surrogate standards.



**Fig. 3.** Extraction efficiencies of different solvents for 12 target EDCs in the ultrasonic solvent extraction process (ACE: acetone; CA: citric acid; MB: McIlvaine buffer; MeOH: methanol).



**Fig. 4.** Cumulative recoveries of sequential elutions with different solvents for 12 target EDCs in the solid-phase extraction process (ACE: acetone; DCM: dichloromethane; MeOH: methanol).



**Fig. 5.** Matrix effects of 12 target EDCs detected with/without additional purification in spiked wastewater and sludge samples (P: purified; UP: unpurified).