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Selective catalytic reduction of NO by NH3 over CuO-CeO2 in the presence of SO²

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Abstract:

 $SO₂$ induced deactivation of selective catalytic reduction of NO over CuO-CeO₂ was studied. In the case of reaction under low O_2 concentration of 1.0 vol%, SO_2 severely deactivated the catalyst at 240 °C with a surface S atomic concentration as low as 1.34 %. However, the deactivated catalyst could be reactivated during online NO reduction under 5.0 vol% O_2 without decreasing the surface S concentration of catalyst, which could be attributed to the involvement of $NO₂$ into the reactions. $NO₂$ could promote the NO removal through three reaction routes: fast SCR reaction; reaction between $NO₂$ and NH₃, and reaction between $NO₂$ and NH₄⁺. Especially under conditions of 10% O_2 , the reaction between NO₂ and NH₃/NH₄⁺ induced the formation of extra $NH_{X\leq 3}$ species which promoted the decomposition of surface deposited sulfate to SO_2 with the assistance of Ce_2O_3 , thus suppressed the accumulation of sulfate on the catalyst surface, and finally suppressed the $SO₂$ induced catalyst deactivation.

Keywords: Selective catalytic reduction; NO_X ; $SO₂$ deactivation; $CeO₂$; sulfate decomposition

Nitrogen oxides (NO_x) are the main reason for the formation of acid rain and photochemical smog, which are harmful for the ecosystem and humanity. Selective catalytic reduction (SCR) is the dominant technology to control the NO_X emission from stationary sources including power boilers and combustion furnaces [1, 2]. Traditional $V_2O_5-WO_3/TiO_2$ catalysts have been widely employed at high temperature but with several defects, such as high toxicity of active components, high activity for SO_2 oxidation, and formation of N₂O at high temperature [3-5], which stimulated the continuing efforts to develop high performance catalysts. Among them, the development of low temperature active catalysts, which could be installed after the dust removal facility, is highly desired. MnO_X, CuO_X , CeO_X and their composites are typically studied transition metal oxides as promising low temperature SCR catalysts [6-12]. Especially, ceria is found to promote NO removal via the redox cycle between Ce^{4+} and Ce^{3+} [10, 13-15], and Cu^{2+} species in the $CeO₂$ matrix is more catalytically active than Cu^{2+} in the CuO matrix [12, 16], and the synergistic effect between Cu and Ce species was also reported to improve the oxygen activation and NO_X adsorption over Cu-CeO_X and CuO-CeO₂-TiO₂ catalysts [17-19].

Flue gases always contain small concentrations of SO_2 even after desulphurization. The SO_2 induced catalyst deactivation is still the main barrier for the application of low temperature active SCR systems [6, 8, 20-23]. In fact, the influences of $SO₂$ on the NO removal over low temperature SCR catalysts have been studied extensively, and it is well accepted that the catalyst deactivation was mainly due to the deposition of ammonia sulfate/sulfites which covered the active sites of the catalyst at low temperature [22]. Recent results found that the fast SCR reaction involved $NO₂$ was less affected by $SO₂$ deactivation than the standard SCR [24], and the presence of large amounts of NO could destabilize the ammonium nitrates and decomposed them at lower temperatures [25]. Also, oxygen in the NO-containing stream was found to play an important role in the NO conversion and selectivity of the SCR reaction, which promote the formation of $NO₂$ and accelerate of the SCR reaction [26-29]. Moreover, the addition of $CeO₂$ into the catalysts was also reported to play in important role for the promotion of resistance to $SO₂$ induced catalyst deactivation [11, 30]. However, further studies are still expected to pursue the possibility for the de-NO_X at low temperature in the presence of SO_2 .

In this study, we found that the $SO₂$ induced catalyst deactivation could be suppressed at relatively low temperature of 240 $^{\circ}$ C via the reaction between NH₃ $(NH₄⁺)$ and $NO₂$ (oxidized from NO). Moreover, this reaction also induced the formation of $NH_{X\text{R}}$ species which promoted the decomposition of sulfate to SO_2 with the assistance of $Ce₂O₃$, thus suppressed the accumulation of ammonia sulfate on the catalyst surface.

2. Experimental

Traditional precipitation was applied to prepare the catalyst. Typically 6.0 mmol of cetyltrimethylammonium bromide was dissolved in 300 ml distilled water at ambient temperature, then 85 mmol of $Cu(NO₃)₂$ and 15 mmol of $Ce(NO₃)₃$ were added into the above solution under magnetic stirring. After 30 min of continue stirring, ammonium hydroxide was gradually added until the pH value of the mixed solution reached to 10, and the suspended solution was aged at 90 $^{\circ}$ C for 3 h. Finally, the precipitate was filtered, washed with distilled water, dried in the oven at 100°C over night, and then milled and calcined at 300 °C for 5 h for later use.

X-ray photoelectron spectroscopy (XPS) data were obtained using a Thermo ESCALAB 250. The X-ray source was an Al Kα radiation. All binding energies were referenced to a 284.8 eV C1s. The used TG analyzer was NETZSCH STA 449F3 and the heating rate was 10 °C/min.

NH3-temperature-programmed desorption (NH3-TPD) experiments were performed using 100 mg of each catalyst to determine their $NH₃$ adsorption ability. The sample was pretreated in a helium stream (30 ml/min) at 500 \degree C for 1 h, and then cooled to 60 °C. The pretreated sample was exposed to a mixed flow of 10% NH₃ in argon at a flow rate of 20 ml/min for 2 h at ambient temperature, and then heated from 100 °C to 800 °C at a heating rate of 10 °C/min. The NH₃-TPD data was recorded on-line by a mass-quadrupole detector (QIC 20).

FTIR experiments were performed on $CuO-CeO₂$ catalyst recorded with a Nicolet 5700 Fourier Transform spectrometer $(0.09 \text{ cm}^{-1} \text{ resolution})$. CuO-CeO₂ catalyst after each treatment was cooled to room temperature and then purged by N_2 for 1 hour. Then the powder samples were compressed in KBr-supporting disks to

obtain the IR spectra.

SCR activity measurements and NO oxidation experiments were performed as previous studies using 0.2 g catalyst pasted on three Al plates (4cm \times 10 cm) [6-8]. The inlet and outlet concentrations of NO, $NO₂$, $SO₂$, and $O₂$ were monitored by Testo AG testo 340.

Catalysts were deactivated/regenerated by 550 ppm NO, 550 ppm NH3, 200 ppm SO₂ when used under 150,000 h⁻¹ GHSV at 240 °C with different O₂ concentration. The SO₂ deactivated samples were expressed as $SD_[C](T)$, where T stood for the time (minute) on stream and $[C]$ stood for the O_2 concentration.

3. Results and discussion

3.1 Impacts of O2 and SO2 on Catalytic activity

NO conversion was significantly affected by oxygen concentration and temperature as shown in Fig. 1. The NO conversion increased from 32.2% to 40% and 45.2% with the increasing of oxygen concentration from 1.0 vol% to 5.0 vol% and 10.0 vol% at 160 °C, respectively. NO conversion was further promoted by temperature increasing and reached 53%, 65.6% , and 69.4% with 1.0 vol%, 5.0 vol% and 10.0 vol% of O_2 at 220 °C, respectively. For temperature at 240 °C or above, the NO conversion was reduced under O_2 concentration above 5% due to the side reaction of NH₃ over oxidation $[6-8]$.

The O_2 concentration significantly affects SO_2 deactivation and regeneration behavior over CuO-CeO₂ catalyst as shown in Fig. 2. For a fresh catalyst with 57.3%

NO conversion at 240 °C (section A) under 1.0 vol[%] O_2 , the NO conversion decreased sharply to 8.7% within 1.5 h with 200 ppm $SO₂$ (section B). After the catalyst was regenerated during online SCR for 2 h with 5.0 vol⁹% O_2 (section C), the NO conversion recovered and reached 61.8%, however, SO_2 still deactivated the catalyst slightly and the NO conversion decreased to 50.9% in 1.5 h (section D). When the catalyst was worked again in 10.0 vol% O_2 (section E), the NO conversion recovered to 60.2% again, and SO_2 deactivation could be minimized (black line shown in section F). In summary, SO_2 deactivation is O_2 concentration dependent and high O_2 concentration can not only recover the deactivated catalyst, but also minimize $SO₂$ deactivation at relatively low temperature of 240 °C.

3.2 NO oxidation

The oxidation of NO to $NO₂$ was studied as shown in Fig. 3. Signal of $NO₂$ was not detected at 100-300 °C with 1.0 vol% oxygen. Once the oxygen concentration increased to 5.0 vol%, NO_2 was first detected at 160 °C and reached 180 ppm at 300 °C. Under 10.0 vol% O_2 , 260 ppm NO₂ was detected at 300 °C. All the results demonstrated that the catalytic oxidation of NO to $NO₂$ was $O₂$ concentration depended on O_2 concentration, which should be able to accelerate the SCR reaction especially at low temperatures $[29, 31]$. From Fig. 3, sufficient NO₂ was produced at 240 °C under O_2 concentration above 5.0 vol%.

3.3 NH3-TPD and NH3-TPO

The NH3-TPD technique was employed to determine the acidic sites in the

catalyst and its $NH₃$ adsorption behavior. As shown in Fig. 4a, the $NH₃$ desorption started at 100 °C and reached the maximum desorption at 215 °C and then decreased with further increasing the temperature, almost no NH₃ was desorbed at temperature above 300 °C. Evidently, NH₃ was adsorbed on the surface of CuO-CeO₂ during SCR of NO at 240 °C.

Fig. 4b shows the influence of O_2 on NH₃ oxidation. NH₃ oxidation started at 150 °C (9.7%) and enhanced with temperature and reached 41% at 300 °C under 1 vol% O_2 , indicating that NH₃ could be oxidized with a relative low O_2 concentration of 1 vol%. NH₃ oxidation, which was further promoted by high O_2 concentration, reached a conversion of 95.5% and 97.8% at 300 °C with 5 vol% and 10 vol% O_2 , respectively. Fig. 4b also shows the influence of O_2 concentration on NO and NO₂ selectivities from NH₃ oxidation. NO and NO₂ were not detected under 1 vol% O₂ at 100-300 °C. Under 5 vol% O_2 , NO was detected above 200 °C and reached 132 ppm at 300 \degree C with a NO selectivity of 24%, but NO₂ was not detected throughout the experiments. When the O_2 concentration increased to 10 vol%, not only NO was detected at 160 °C and reached 90 ppm at 300 °C, but $NO₂$ was also detected above 240 °C and reached 43 ppm at 300 °C, the selectivity of NO and NO₂ was 16.3% and 7.8%, respectively. In summary, a relatively low concentration of O_2 is sufficient to promote $NH₃$ activation, and high $O₂$ concentration promoted the over oxidation of NH₃ to NO (even NO₂), especially at temperature above 240 °C.

3.4 XPS analysis

Fig. 5 shows the XPS spectra of fresh and used CuO -CeO₂. The O 1s bands of the samples were shown in Fig. 5a, the binding energy at about 529.6 eV corresponded to the lattice oxygen (denoted as O_β), and the band at about 531.6 eV corresponded to the surface adsorbed oxygen (-OH) (denoted as $O₀$) [32], and the ratio of $O_{\alpha}/(O_{\alpha}+O_{\beta})$ over fresh CuO-CeO₂ was 45.9%. The lattice oxygen appeared as the adsorption sites for $SO₂$ and the adsorbed oxygen played an important role in the formation of sulfites/sulfates [33]. The ratio of $O_q/(O_q+O_p)$ increased to 60.9% and 76.3% over $SD_{[5%0}(300)]$ and $SD_{[10%0}(540)]$ after oxygen concentration increased during SO2 deactivation in Fig. 2. The increase of adsorbed oxygen suggested the deposition of sulfates [6, 8] and the strong adsorption of $NO₂$ as shown in Fig. 7.

The complex spectrum of Ce 3d was deconvoluted into eight components in Fig. 5b, and those peaks detected at 882.8, 889.2, 898.7, 901.1, 908.2, and 917.6 eV represent the $3d^{10}4f^0$ initial electronic state corresponding to Ce^{4+} species [34]. And the peaks at 885.1 eV and 903.5 eV arise from Ce^{3+} species [35]. The results indicated that CeO₂ and Ce₂O₃ are both existed in CuO-CeO₂. The ratio of Ce³⁺/(Ce³⁺ + Ce⁴⁺) is calculated to be 21.7%, 16%, 9.9%, and 9.4% over fresh catalyst, $SD_{11\%1}(90)$, $SD_{[5\%]}(300)$, and $SD_{[10\%]}(540)$ respectively, which demonstrated that part of Ce³⁺ was oxidized to Ce^{4+} when O_2 and SO_2 concentrations were increased.

From the Cu 2p bands of the samples shown in Fig. 5c, the binding energy at 954 eV and 934 eV corresponded well with Cu^{2+} over fresh catalyst, $SD_{[1\%]}(90)$,

 $SD_{[5\%]}(300)$, and $SD_{[10\%]}(540)$ [36], which indicated that the sulfation of the catalyst did not change the chemical state of Cu^{2+} . According to our previous results, Cu^{2+} is the main active component at low temperatures [6-8], Cu^{2+} ions were ready to be reduced to $Cu⁺$ by SO₂ for SCR of NO over Fe-Cu/TiO₂-CNTs catalysts, and the Cu⁺ ions were active components at high temperatures. Here in this study, we found that for CuO-CeO₂, CeO₂ suppressed the Cu²⁺ reduction which could be attributed to the redox cycle between Ce^{4+} and Ce^{3+} [12, 16, 17], and thus Cu^{+} was not detected by XPS even after the catalyst was tested with SO_2 . As a result, the CuO-CeO₂ showed the potential to keep high NO removal activity even with SO_2 .

The S 2p bands of $SD_{[1\%]}(90)$, $SD_{[5\%]}(300)$, and $SD_{[10\%]}(540)$ samples were showed in Fig. 5d. The binding energy of S 2p concentrated at about 168.2-168.5 eV and 169.2-169.7 eV corresponded to S^{4+} and S^{6+} , respectively [35, 37]. It is also worth noting that, the surface atomic concentration of S was 1.34% over $SD_[1%0](90)$, which indicated that deposition of ammonia sulfate/sulfites at the catalyst surface occurred during NO reduction with SO_2 [6, 8, 21]. And a surface S concentration of 1.34% is sufficient to deactivate the catalyst. Interestingly, on the one hand, the deposited S species on catalyst surface increased to 3.13% over $SD_[5%0](300)$; on the other hand, the SO₂ induced catalyst deactivation weakened as shown in Fig. 2. This strongly suggested that the deactivation caused by sulfate/sulfites deposition could be minimized by increasing the O_2 concentration. Moreover, in the case of high O_2 concentration of 10.0 vol%, sulfate/sulfites deposition was also suppressed and the

surface S concentration reduced to 1.68% over $SD_[10%0](540)$, which should further suppress the $SO₂$ induced deactivation.

From Fig. 5d, the ratio of $S^{4+}/(S^{4+}+ S^{6+})$ over $SD_{[1\%]}(90)$, $SD_{[5\%]}(300)$, and $SD_{[10\%]}(540)$ was calculated to be 30.7%, 41.9%, and 60.6%, respectively. Normally, sulfites are ready to be oxidized to sulfates by O_2 . However, the ratio of $S^{4+}/(S^{4+}+S^{6+})$ decreased with $O₂$ concentration, which suggested the existence of an additional reaction to reduce S^{6+} to S^{4+} .

4. Discussions

The deactivation of catalyst by SO_2 at low temperature is the main barrier for the application of low temperature SCR of NO [6, 8, 20-23], which was mainly due to the deposition of ammonia sulfate/sulfites. Over $CuO-CeO₂$ in this study, $SO₂$ also induced deposition of ammonia sulfate/sulfite and catalyst deactivation under 1.0 vol% O_2 as shown in Figs. 2 and 5d at 240 °C. Amazingly, under O_2 concentration above 5.0 vol% (especially 10.0 vol%), the SO_2 induced deactivation was weakened, though surface sulfate/sulfite deposition still occurred. From literature, introducing $NO₂$ into the reaction system, together with the adding of $CeO₂$ into the catalysts, was found to promote the tolerance SO_2 deactivation [24, 25, 30, 38]. Therefore it seems high concentration of O_2 and Ce species (in catalyst) could restrain the deactivation of catalyst by SO_2 ; accordingly, the related reactions involved in this system were analyzed and listed as below:

$$
2NO + O_2 \rightarrow 2NO_2 \tag{2}
$$

$$
NO + 2CuO-2CeO2 \rightarrow NO2 + Cu2O-2CeO2
$$
 (3)

$$
NO + NO2 + 2NH3 \rightarrow 2N2 + 3H2O
$$
 (4)

$$
6NO2 + 8NH3 \rightarrow 7N2 + 12H2O
$$
 (5)

$$
SO2 + 2NH3 + H2O \rightarrow (NH4)2SO3
$$
\n(6)

$$
2(NH_4)_2SO_3 + O_2 \to 2(NH_4)_2SO_4
$$
\n(7)

$$
Cu2O-2CeO2 \rightarrow 2CuO + Ce2O3
$$
 (8)

$$
Cu2O-Ce2O3+O2 \rightarrow 2CuO-2CeO2
$$
\n(9)

$$
4(NH_4)_2SO_4 + 2(4-x)NO_2 \rightarrow (4-x)N_2 + 4(NH_{X<3})_2SO_4 + 4(4-x)H_2O \qquad (10)
$$

$$
(NH_{X<3})_2SO_4 + (2-x)Ce_2O_3 \to N_2 + SO_2 + xH_2O + 2(2-x)CeO_2 \tag{11}
$$

Reaction (1) is the standard SCR reaction normally occurred at high temperatures, by which the lattice oxygen in the catalyst was also involved. Reactions (2) and (3) produced sufficient $NO₂$ which promoted the SCR reaction through the fast reaction (4) and/or reactions $(5) + (10)$ at low temperatures. At the same time SO₂ was also involved in reactions (6) and (7), which was proved by XPS as shown in Fig. 5d. The produced Cu₂O (normally only part of $Cu²⁺$ ions were reduced, here for simplification, we direct use Cu₂O as formulas of Cu_XO containing Cu⁺. Similarly, $Ce₂O₃$ was used as formulas of Ce_XO containing $Ce³⁺$ from reactions (1) and (3) was then oxidized by $CeO₂$ through reaction (8); as a result, $Cu⁺$ was not detected as shown in Fig. 5c. The reduced catalyst could also be oxidized by O_2 through reaction (9). In fact, reactions (9) and (11) explained the low Ce^{3+} ions detected over catalyst

 $SD_{[10\%]}(540)$ as shown in Fig. 5b. Compared to reaction (5), reaction (10) is also reasonable, which also produced $NH_{X\leq 3}$ species with high oxidability, thus reduced the surface S^{6+} concentration through reaction (11), especially under 10.0 vol% of O_2 , which produced sufficient $NO₂$ through reactions (2) and (3). Note that from the free Gibbs energy calculation, reduction of S^{6+} to S^{4+} through reaction (11) is energetically favored. As a result, the catalyst deactivation caused by sulfate deposition could be weakened or even minimized through reactions (8), (10) and (11). Here the direct oxidation of SO_2 to SO_3 was neglected because the low reaction temperature (below 240 °C). The fact that Cu⁺ was not detected by XPS from catalysts after SO_2 induced deactivation, together with the decrease of surface S concentration and increase of surface S^{4+} species as shown in Fig. 5, strongly supported our proposal. From Fig. 2, the catalyst regeneration under 10 vol% O_2 with NH₃ and NO only (in section E) was also shown, evidently the atmosphere with $NH_3 + NO + O_2$ showed the best effect for catalyst recovery, which strongly suggested that $NH₃ + NO + O₂$ produced new deoxidizer of NH_{X<3} to promote the reaction for S^{6+} to S^{4+} . Since NO₂ is a strong oxidizer compared to NO, the production of deoxidizer like $NH_{X\leq 3}$ as intermediate product is very reasonable [1], from the reactants involved in the above reactions, $NH_{X\leq 3}$ is the only deoxidizer possibly produced.

In order to further confirm our proposal, TGA curves were used to analysis the thermal stability of fresh catalyst and $SD_[10%]$ </sub>(540). As shown in Fig. 6, the TG curve of fresh catalyst almost showed no weight loss up to 600 °C. While for the TG curve

of $SD_{[10\%]}(540)$, a weight loss of approximately 5% and 2% was observed at 200-300 °C and 300-400 °C, which could be corresponded to the decomposition of ammonia sulfate and sulfite, respectively [39]. This is in good agreement with the calculated ratio of $S^{4+}/(S^{4+}+S^{6+})$ from $SD_{[10\%]}(540)$.

FTIR was also used to characterize the $CuO-CeO₂$ catalyst at different reaction stages. As shown in Fig. 7, peaks located at 1384 cm^{-1} and 1623 cm^{-1} attributed to the surface $NO₂$ ⁻ (monodentate nitrito) and $NO₃$ ⁻ (bidentate) were detected in all spectra, indicating the success adsorption of NO and $NO₂$, and a strong intensity of peak at 1623 cm⁻¹ (compared to the intensity of peak 1384 cm⁻¹) was observed in spectra –c and –e under reaction with SO_2 [40-42], indicating that surface NO_2 species increased with $SO₂$ introduction, which should be beneficial for NO removal. Also, peaks at 1050 cm⁻¹ (attributed to SO_4^2) and at 976 and 1150 (attributed SO_3^2) were detected in spectra –c and –e $[33, 43-47]$, indicating the deposition of sulfate/sulfite, in agreement with our XPS measurements. Note that the intensity of SO_3^2 peaks in spectrum-e was stronger than those in spectrum-c, which strongly supported our assumption of the existence of sulfate decomposition at low temperature as reactions -10 and -11 shown. By the way, a weak peak at 1050 cm⁻¹ could also be observed in spectra $-a$, $-b$, and $-d$, which could be caused by the trace SO_2 remained in the test system, the peaks located at 844 cm⁻¹ was attributed to the surface Cu^{2+} [47], however, the attribution of peak at 780 cm^{-1} is still not clear.

5 Conclusions

In summary, $CuO-CeO₂$ catalyst deactivation caused by the deposition of ammonia sulfate/sulfite could be online reactivated with 5.0 vol% O_2 at 240 °C, which was attributed to the reaction between NH_3/NH_4^+ and NO_2 . Under 10.0 vol% O_2 , the SO₂ deactivation was minimized, and the reaction between Ce₂O₃ + NH_X \leq 3 and ammonia sulfates overcame the accumulation of sulfate on the catalyst surface. The results obtained in this study provided a possibility to suppress the $SO₂$ induced catalyst deactivation at low temperatures, which should be important for the applications of low temperature SCR.

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Figure Captions:

Fig.1. NO conversion over CuO-CeO₂, under 550 ppm of NO +550 ppm NH₃+ 1-10 vol % O_2 + Ar, at a total flow rate of 500 ml/min and a gas hourly space velocity (GHSV) of 150,000 h⁻¹ at 160, 180, 200, 220, and 240 °C.

Fig.2. Effects of O_2 on SO_2 deactivation and regeneration at 240 °C. Section-A: activity characterization of the fresh catalyst with 1 vol% O_2 ; section-B: deactivation by introducing 200 ppm SO_2 ; section-C: regeneration with 550 ppm NO, 550 ppm NH₃, 5 vol% O_2 , and Ar balance; section-D: deactivation again with 200 ppm SO_2 introducing; section-E: regeneration again with 550 ppm NO, 550 ppm $NH₃$, 10 vol% O_2 , and Ar balance; and section-F: catalyst deactivation with 200 ppm SO_2 . For comparison, the activity of catalyst after regeneration with 550 ppm $NO + 10.0$ vol⁹/₀ and 550 ppm $NH_3 + 10.0$ vol% in section -E was also shown in section-F (blue and red line, respectively).

Fig.3. NO oxidation under 550 ppm of NO + 1-10 vol % O_2 + Ar, at a total flow rate of 500 ml/min and a gas hourly space velocity (GHSV) of $150,000 \text{ h}^{-1}$.

Fig.4. (a) NH_3 -TPD pattern; and (b) NH_3 -TPO profiles of the catalyst.

Fig.5. XPS results of (a) O 1s, (b) Ce 3d, (c) Cu 2p, and (d)S 2p for (i) CuO-CeO₂, (ii) $SD_{[1\%]}(90)$, (iii) $SD_{[5\%]}(300)$, and (iv) $SD_{[10\%]}(540)$, respectively.

Fig.6. TG analysis at 10 °C/min for fresh catalyst and $SD_[10%]$ </sub> (540) .

Fig. 7. FTIR spectra of CuO-CeO₂ after 12 hours treatment at 240°C for (a) N₂ purging; (b) SCR test under 800 ppm NO, 800 ppm NH₃ and 5% O_2 ; (c) SCR test under 800 ppm NO, 800 ppm NH₃, 200ppm SO_2 and 5% O_2 ; (d) SCR test under 800 ppm NO, 800 ppm NH₃ and 10% O₂; and (e) SCR test under 800 ppm NO, 800 ppm NH₃, 200ppm SO₂ and 10% O₂.

Fig.1. NO conversion over CuO-CeO2, under 550 ppm of NO +550 ppm NH3+ 1-10 vol % O2 + Ar, at a total flow rate of 500 ml/min and a gas hourly space velocity (GHSV) of 150,000 h-1 at 160, 180, 200, 220, and 240 °C. 80x49mm (300 x 300 DPI)

Fig.3. NO oxidation under 550 ppm of NO + 1-10 vol % O2 + Ar, at a total flow rate of 500 ml/min and a gas hourly space velocity (GHSV) of 150,000 h-1 80x60mm (300 x 300 DPI)

80x114mm (300 x 300 DPI)

Fig.5. XPS results of (a) O 1s, (b) Ce 3d, (c) Cu 2p, and (d)S 2p for (i) CuO-CeO2, (ii) SD[1%](90), (iii) SD[5%](300), and (iv) SD[10%](540), respectively. 85x65mm (300 x 300 DPI)

Fig.6. TG analysis at 10 °C/min for fresh catalyst and SD[10%](540) 85x63mm (300 x 300 DPI)

85x127mm (300 x 300 DPI)

Reaction between NO_2 and NH_3/NH_4^+ induced the formation of $NH_{X\leq 3}$ species with high oxidability; $NH_{X<3}$ promoted the surface sulfate decomposition; high de-NO_X performance was achieved in the presence of $SO₂$ at low temperature.