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ARTICLE

## Synthesis of Functional xLaMn/KIT-6 and Feature of Hot Coal Gas Desulphurization

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To enhance the stability of sorbent during continuous desulphurization-regeneration cycles, KIT-6 with 3D pore channels was used as support for sorbents. A series of mesoporous xLaMn/KIT-6 sorbents with different La/Mn atomic ratios were fabricated by a sol-gel method and their desulphurization properties in hot coal gas were investigated at 700-850 °C. 3La97Mn/KIT-6 performed the best at 800 °C with breakthrough sulphur capacity of 11.56 g sulfur/100 g sorbent. The eight successive desulphurization (800 °C)-regeneration (600 °C) cycles revealed that 3La97Mn/ KIT-6 with endurable regeneration ability could obtain 80% of initial sulphur capacity. It indicated better desulphurization performance compared to pure 3La97Mn and 3La97Mn/MCM-41. The fresh and used xLaMn/KIT-6 sorbents were characterized by means of BET, XRD, HRTEM, XPS and H<sub>2</sub>-TPR techniques. The XRD patterns and HRTEM images of fresh and used 3La97Mn/KIT-6 verified that the utilization of KIT-6 suppressed effectively the aggregation of Mn<sub>2</sub>O<sub>3</sub> particles and improved the stability of sorbent.

### 1 Introduction

Due to the fact that more than 70% energy consumption relies on coal resources in China, the air pollution is induced which can be attributed to the by-product of fly ash, compounds of containing nitrogen and sulphur during the coal combustion. According to the report<sup>1</sup>, China had overtaken other nations in the worldwide as the largest emitter of SO<sub>2</sub> since 2005, which should be mainly attributed to the coal-derived power station. Therefore, a system named integrated gasification-combined cycle (IGCC) was developed to replace the traditional coal-derived power station to realize a high effective usage of coal resources and lower emission of contaminant. Furthermore, the H<sub>2</sub>S in coal-derived gas not only corrupt the pipeline or gas turbine and poison the catalysts (*e.g* Fischer-Tropsch synthesis<sup>2</sup>) for downstream process, but also can be a source of acid rain which threatens the environment and the human health. In the meantime, environmental legislations have been presented to limit the sulphur content in fossil-derived gas. So it is necessary to keep the emission of H<sub>2</sub>S below 100 ppmv in IGCC unit. Conventional gas-cleaning techniques at low temperature, such as amine scrubbers<sup>3</sup> and wet limestone<sup>4</sup> desulphurization, have been applied to remove the H<sub>2</sub>S in the coal gas, which are disadvantageous in energy saving due to the huge heat loss during gas cooling and reheating stage. Therefore, the desulphurization for hot coal gas is needed to improve the overall thermal efficiency from an energy saving point of view.

Recently, there are comprehensive reports concerning copper<sup>5-10</sup>, zinc<sup>11-14</sup>, manganese<sup>7, 10, 12, 15-20</sup>, ferric, calcium<sup>4, 21, 22</sup> and rare earth

element<sup>23-26</sup> used as based sorbents of hot coal gas desulphurization. According to the report of Westmoreland<sup>27, 28</sup>, MnO was stable in strong reducing environment and possessed promising potential for hot coal gas desulphurization in the temperature range of 400-1000 °C, which is superior to V<sub>2</sub>O<sub>5</sub>, CaO and ZnO due to high initial sulphidation rate. Although MnO has a relative lower desulphurization precision compared with zinc and ferric oxides, its high desulphurization efficiency with endurable regeneration ability and high sulphur capacity at 800-1000 °C have attracted considerable attention of researchers<sup>16, 17, 29</sup>. When copper, zinc, ferric, rare earth elements oxides were doped to Mn-based sorbents, the thermodynamic equilibrium efficiency reacted with H<sub>2</sub>S can increase remarkably. As report of Flytzani-Stephanopoulos<sup>26</sup>, Ce and La oxides were stable at higher than 800 °C and the ultra deep removal of H<sub>2</sub>S could be achieved.

Pure metal oxides as desulphurizers are confronted with the serious scientific problems, such as diffusion resistance, mechanical strength and sintering during hot coal gas desulfurization. Recently, many inert materials were used as support of metal oxides, such as TiO<sub>2</sub>, ZrO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub> and mesoporous MCM-41 and SBA-15. However, the utilization of the active particles was low due to low surface area and character of microporous or 1D channel of the support. In the meantime, the macroporous material, such as cordierite, indeed suffered from the pulverization and low utilization of sorbent because of the low surface area. Thus, there is significant interest to use novel support, such as MCM-48 or KIT-6. However, KIT-6 presented a superior performance in resistance to pore blockage due to its unique pore structure with three dimensional

channels, which have been applied in adsorption of CO<sub>2</sub>. In this study, the mesoporous silica KIT-6 with high surface area and large pore volume was synthesized using as the support of sorbents and this design could take advantage of unique pore structure of KIT-6 to improve the gas diffusion in reaction as well as the stability of the sorbent. A series of xLayMn/KIT-6 sorbents were prepared by a sol-gel method and their desulfurization activities were investigated on a quartz reactor. The properties of fresh and used sorbents were characterized by the means of BET, XRD, HR-TEM, XPS, FT-IR and H<sub>2</sub>-TPR techniques.

## 2 Experimental section

### 2.1 Synthesis of KIT-6 and xLayMn/KIT-6 Sorbents

Mesoporous KIT-6 was prepared according to the report of Kleitz *et al.*<sup>30</sup>, i.e. 9 g of pluronic P123 was dissolved in 325 g of deionized water (DW) and 17.4 g of HCl (37%) under vigorous stirring to form a clear and transparent solution. Subsequently, 9 g of butanol was added with stirring at 35 °C for 1 h. After 19.35 g of TEOS was added drop-wise to the aforementioned clear solution, this mixture was continuously stirred at 35 °C for another 24 h and then was transferred into a Teflon-lined stainless steel autoclave for hydrothermal synthesis at 100 °C for 24 h under static condition. After cooled down it to room temperature (RT), the white precipitate was filtered and dried at 100 °C for 24 h. Finally, the white powder was calcined in air at 550 °C for 6 h.

A series of xLayMn/KIT-6 sorbents with different La/Mn atomic ratios were prepared by means of a sol-gel method according to the report of Zhang *et al.*<sup>31</sup>. 0.32 g of La(NO<sub>3</sub>)<sub>3</sub>•6H<sub>2</sub>O was dissolved in 25 mL DW and 8.52 g of 50wt% Mn(NO<sub>3</sub>)<sub>2</sub> solution, followed by addition of 5 mL HNO<sub>3</sub> (6 mol/L). After the addition of 7.74 g of citric acid, 2 g of as-prepared KIT-6 support was added to the aforementioned solution. The mixture was kept at 60 °C until it became a viscous yellow gel and then aged at RT for two days. Finally, the gel was dried at 60 °C and calcined at 550 °C for 6 h to obtain dark brown 50wt%3La97Mn/KIT-6. A series of 50wt% xLayMn/KIT-6 sorbents were fabricated according to same procedure as 3La97Mn/KIT-6, which were denoted as 10La90Mn/KIT-6, 5La95Mn/KIT-6, 3La97Mn/KIT-6 and 100Mn/KIT-6, the numbers before La and Mn stood for the molar number in mixed metal oxides, respectively. The loadings of active metal oxides (La<sub>2</sub>O<sub>3</sub> and Mn<sub>2</sub>O<sub>3</sub>) for all samples was 50 wt%.

### 2.2 Characterization of Sorbents

Nitrogen adsorption isotherms of KIT-6, fresh and used 50wt% xLayMn/KIT-6 sorbents were obtained at 77 K on a domestic adsorption system<sup>32</sup>. Prior to the analysis, the samples were degassed at 200 °C for 2 h. BET surface area, pore volume and average pore diameter were calculated based on adsorption isotherm while pore size distribution was estimated by BJH (Barrett, Joyner & Halenda) method.

The small-angle X-ray diffraction (XRD) patterns of KIT-6, fresh and used sorbents were recorded with a Rigaku D/max 2500 vpc automatic diffractometer equipped with Ni filtered Cu K<sub>α</sub> radiation (20 kV, 30 mA). Wide-angle XRD patterns were measured with a PANalytical automatic diffractometer using Ni-filtered Cu K<sub>α</sub> radiation (λ = 0.15406 nm) at settings of 40 kV and 50 mA. The cell

parameters of all samples were calculated by the following equation:  $a_0 = \sqrt{6} \times d(211)$ . The pore wall thickness was estimated by the formula  $h = a_0/3.0919 - D/2^{33}$ ,  $D$  is the mesopore size calculated based on BJH method. The fine structures of fresh and used sorbents were investigated by HRTEM on a JEM-2100F electron microscopy operated at 200 kV. FT-IR spectra of fresh and regenerated 3La97Mn/KIT-6 at 600, 700 and 800 °C were collected on BIO-RAD FTS 3000 spectrophotometer.

The temperature-programmed reduction (TPR) experiments were performed using a TPR-2910 Micromeritics (USA) instrument, equipped with a thermal conductivity detector (TCD). 0.1995 g of samples was pretreated at 200 °C in argon (30 mL/min) for 60 min. After cooling to 60 °C in argon atmosphere, TPR profiles were taken from 60 to 900 °C (10 °C/min) in 10% H<sub>2</sub>/Ar mixed gas (30 mL/min) and the signals of hydrogen consumption were recorded using TCD.

The X-ray photoelectron spectroscopy (XPS) signals were obtained with a PHI-1600 ESCA spectrometer equipped with Al K<sub>α</sub> X-ray source (1486.6 eV). The binding energies (BEs) of the sample were calibrated with the contaminant C 1s line (284.6 eV).

### 2.3 Desulfurization and Regeneration Tests for Sorbents

The desulfurization performance of the sorbents for hot coal gas was investigated over a fixed-bed quartz tubular micro-reactor. The experimental setup was described in details elsewhere<sup>34</sup>. The inlet stream was controlled by mass flow controllers (D07-7B/ZM, Beijing Sevenstar Electronics Co., Ltd., China) at 180 mL/min. Typically, 0.5 g sorbent was packed into the reactor (i.d. 10 mm) and the reaction temperature was controlled by a K-type thermal-couple. The sorbents were first heated to the reaction temperature in N<sub>2</sub> at the rate of 10 °C/min and the simulated hot coal gas with composite of 66.44% N<sub>2</sub>, 13.84% H<sub>2</sub>, 19.36% CO and 0.36% H<sub>2</sub>S was then introduced to the reactor for desulfurization. The concentration of H<sub>2</sub>S in inlet and outlet gas was analyzed by iodometric titration method to obtain breakthrough curve of H<sub>2</sub>S and breakthrough sulphur capacity (the outlet H<sub>2</sub>S concentration of lower than 50 ppmv is defined as the breakthrough point). The performance of sorbents was evaluated by the breakthrough sulphur capacity (BSC) according to equation (1):

$$SC \left( \frac{\text{g of sulfur}}{100 \text{ g of sorbent}} \right) = WHSV \times \frac{M_s}{V_m} \times \left[ \int_0^t (C_{in} - C_{out}) dt \right] \times 10^{-4} \quad (1)$$

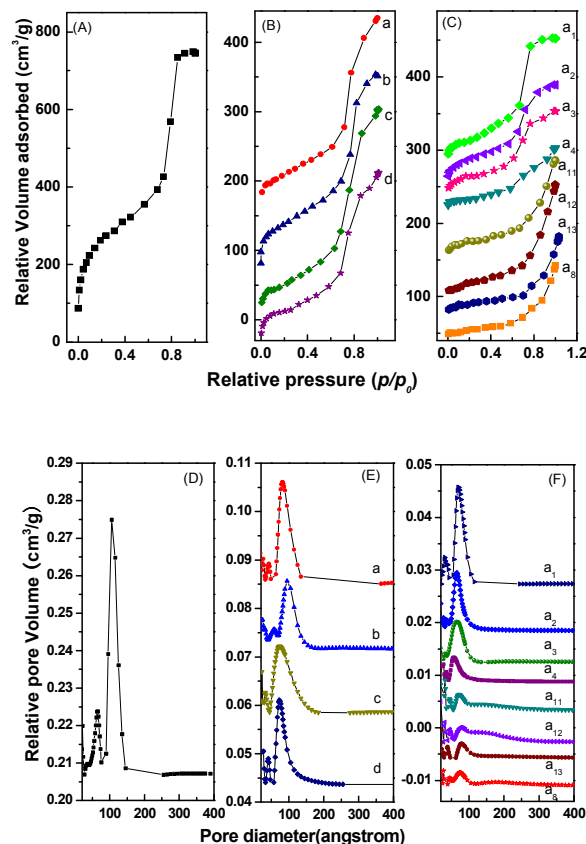
Where  $SC$  represents the effective sulphur capacity (g·S/100 g sorbents);  $WHSV$  is weight hour space velocity (L/(h·g));  $M$  is molecular weight of sulphur (g/mol);  $V_m$  is the molar volume of H<sub>2</sub>S at standard pressure and 25 °C (24.5 L/mol);  $C_{in}$  and  $C_{out}$  are the inlet and outlet concentration (ppmv) of H<sub>2</sub>S, respectively;  $t$  is the breakthrough time for desulphurization (h). The effective utilization of sorbent can be defined as the ratio of BSC with the theoretical sulphur capacity (TSC).

The regeneration temperature was optimized in the range of 600~800 °C over aforementioned reactor. The used sorbent was first heated to appointed temperature in N<sub>2</sub> (77 mL/min) at a rate of 10 °C/min and then regenerated in 5% O<sub>2</sub>/N<sub>2</sub> mixture (100 mL/min) until the concentration of SO<sub>2</sub> in exit could not be detected by KMnO<sub>4</sub> solution as a indicator. The regenerated samples were treated in the N<sub>2</sub> atmosphere for 1 h to keep the residual metal sulphate decomposing.

### 3 Results and discussion

#### 3.1 BET Analysis

To investigate the variation in structure of sorbents during the desulphurization and regeneration, the nitrogen adsorption isotherms and pore size distributions of KIT-6, fresh and used sorbents were shown in Fig. 1. It could be seen that KIT-6 exhibited type-IV curve defined by International Union of Pure and Applied Chemistry (IUPAC), which was characteristic of mesoporous materials. A sharp capillary condensation step in the range of  $p/p_0 = 0.7-0.9$  (Fig. 1A) and a narrow pore size distribution ( $D_p$ ) at approximately 10.6 nm (Fig. 1D) were observed, an indicative of the uniform large channels existed within KIT-6. As shown in Fig. 1B, the nitrogen adsorption isotherms of fresh sorbents did not vary remarkably, which indicated that the introduction of metal oxides did not destroy the characteristic of mesoporous KIT-6. However, compared with KIT-6, there was a decline in height of adsorption mutation (Fig. 1B-C) and the pore size distribution after the metal oxide was incorporated into KIT-6 or the sorbents used in hot coal gas desulphurization (Fig. 1E-F).



**Fig. 1** N<sub>2</sub> adsorption isotherms (A-C) and pore size distribution (D-F) of KIT-6 and fresh (a) 3La97Mn/KIT-6, (b) 5La95Mn/KIT-6, (c) 10La90Mn/KIT-6, and (d) 100Mn/KIT-6; (a<sub>1</sub>-a<sub>4</sub>) 3La97Mn/KIT-6 used at 700, 750, 800, 850 °C, respectively; (a<sub>11</sub>-a<sub>13</sub>) 3La97Mn/KIT-6 regenerated at 600, 700 and 800 °C after third cycles; (a<sub>8</sub>) 3La97Mn/KIT-6 regenerated at 600 °C after eighth cycles.

**Table 1.** Total pore volume ( $V_t$ ), Mesopore volume ( $V_{meso}$ ), Micropore volume ( $V_m$ ), Average pore diameter ( $D_a$ ) and BET surface area ( $S_{BET}$ ) of KIT-6, fresh and used xLayMn/KIT-6

| Sample         | $V_t$ (mm <sup>3</sup> /g) | $V_{meso}$ (mm <sup>3</sup> /g) | $V_m$ (mm <sup>3</sup> /g) | $D_a$ (nm) | $S_{BET}$ (m <sup>2</sup> /g) |
|----------------|----------------------------|---------------------------------|----------------------------|------------|-------------------------------|
| KIT-6          | 1093                       | 762                             | 331                        | 2.33       | 938                           |
| La3Mn97/KIT-6  | 381                        | 309                             | 72                         | 3.56       | 214                           |
| La5Mn95/KIT-6  | 395                        | 308                             | 87                         | 3.11       | 254                           |
| La10Mn90/KIT-6 | 414                        | 344                             | 70                         | 4.04       | 205                           |
| Mn100/KIT-6    | 336                        | 262                             | 74                         | 3.57       | 188                           |
| S-700-         | 254                        | 201                             | 53                         | 3.51       | 145                           |
| La3Mn97/KIT-6  | 197                        | 148                             | 49                         | 2.64       | 149                           |
| S-750-         | 163                        | 126                             | 37                         | 3.05       | 107                           |
| La3Mn97/KIT-6  | 113                        | 86                              | 27                         | 1.66       | 68                            |
| S-850-         | 177                        | 137                             | 40                         | 2.71       | 131                           |
| La3Mn97/KIT-6  | 117                        | 93                              | 24                         | 4.03       | 58                            |
| S-800-         | 224                        | 180                             | 44                         | 3.23       | 139                           |
| La10Mn90/KIT-6 | 162                        | 132                             | 30                         | 4          | 81                            |
| R-S-3-600-     | 176                        | 158                             | 18                         | 4.35       | 81                            |
| La3Mn97/KIT-6  | 100                        | 83                              | 17                         | 3.57       | 56                            |
| R-S-3-800-     | 111                        | 99                              | 12                         | 4.93       | 45                            |
| La3Mn97/KIT-6  |                            |                                 |                            |            |                               |

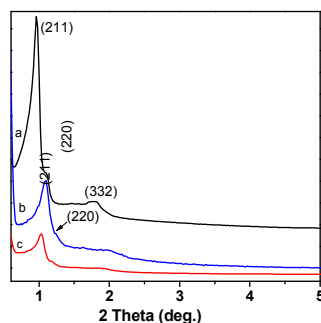
Notes: The physical parameters of all samples were calculated by BJH method.

As listed in Table 1,  $S_{BET}$  and  $V_t$  of KIT-6 were 938 m<sup>2</sup>/g and 1.093 cm<sup>3</sup>/g, respectively. Both  $S_{BET}$  and  $V_t$  of fresh sorbents decreased to 188-254 m<sup>2</sup>/g and 0.336-0.414 cm<sup>3</sup>/g, respectively due to the loadings of metal oxides in mesoporous channels of KIT-6. For used sorbents, after desulphurized at 700-850 °C, there was a drastic decline in both  $S_{BET}$  and  $V_t$  due to the replacement of metal oxides by metal sulphides with large molecular sizes (Table 1). Moreover, the  $S_{BET}$  and  $V_t$  of used sorbents decreased with the increment of desulphurization temperature. According to the report of Zhang *et al.*<sup>35</sup>, the increment of calcination temperature on mesoporous silica can enhance the polymerization degree of  $\equiv \text{Si-O-Si} \equiv$  bonds but with smaller pore diameter and lower surface area. After the 3La97Mn/KIT-6 underwent 8<sup>th</sup> desulphurization-regeneration cycles, approximately 30% of  $S_{BET}$  and  $V_t$  was still maintained, indicated the stability of mesoporous structure in sorbent, which was favourable to the diffusion of gas and heat in mesoporous channels of sorbents.

#### 3.2 XRD Analysis

Small-angle powder X-ray diffraction (XRD) patterns of KIT-6, fresh and used sorbents were shown in Fig. 2. The small angle XRD patterns of KIT-6 have three diffraction peaks at  $2\theta = 0.97, 1.1, 1.76^\circ$ , which was ascribed as the reflections of (211), (220), (332)

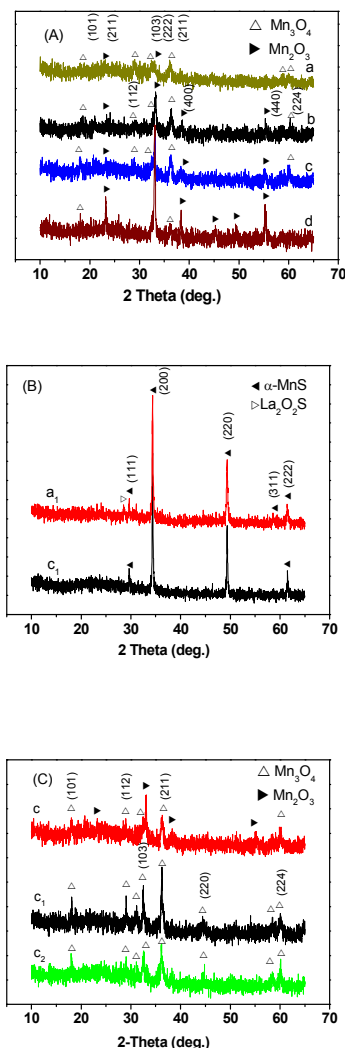




**Fig. 2** Small-angle XRD patterns of (a) KIT-6, (b) fresh and (c) used 3La97Mn/KIT-6.

planes in the discontinuous cubic Ia3d space group, respectively. As shown in Fig. 2b, the XRD patterns of fresh 3La97Mn/KIT-6 verified that the mesoporous cubic structure of KIT-6 was not destroyed after the loading of metal oxides. However, the reduction in intensity of XRD peaks could be attributed to a decrease in the electron density contrast upon the introduction of metal oxides into the mesoporous channels of KIT-6, and this behaviour was identical with the nitrogen adsorption results (Fig. 1B and 1E). The wall thickness (2.72 nm) can be calculated from the relationship ( $h = a_0/3.0919 - D_p/2$ ) of the unit cell parameter,  $a_0$  (20.79 nm) with the most probable diameter  $D_p$  (8.2 nm), based on the interplanar spacing,  $d$  ( $n\lambda = 2d\sin\theta$ ) estimated from the peak corresponding to (211) reflections in 3La97Mn/KIT-6, which was higher than that (2.1 nm) of KIT-6. This revealed that the enhancement of the pore wall thickness was due to the loading of metal oxides, resulting in better thermal stability. For 3La97Mn/KIT-6 after desulphurization at 800 °C, the pore wall thickness was 3.2 nm, which was attributed to the metal sulphides with large molecular size ( $r(S^{2-}) = 184$  pm,  $r(Mn^{2+}) = 80$  pm) substitution for metal oxides with small molecular size ( $r(O^{2-}) = 140$  pm,  $r(Mn^{3+}) = 66$  pm) on pore wall of mesoporous channels. However, the sharp peak at  $2\theta = 1.09^\circ$  indicated that the bicontinuous mesoporous network of sorbent was still preserved after desulphurization (Fig. 2c).

The textural features of fresh, used and regenerated sorbents were investigated by wide-angle XRD. As shown in Fig. 3, there was no signal of silicates, which indicated that no reaction occurred between metal oxides and supports. For all fresh sorbents, the manganese oxides existed mainly in the form of  $Mn_2O_3$  [PDF#65-7467] and  $Mn_3O_4$  [PDF#18-0803] phases. For 100Mn/KIT-6, the peaks at  $23.14^\circ$ ,  $32.95^\circ$ ,  $38.23^\circ$ ,  $45.17^\circ$ ,  $49.35^\circ$  and  $55.18^\circ$  were assigned to  $Mn_2O_3$  phase [PDF#65-7467], while there were only weak peaks of  $Mn_3O_4$  [PDF#18-0803] at  $2\theta = 18.02^\circ$  and  $36.04^\circ$ . However, the diffraction peaks of  $Mn_2O_3$  became weak and widen (Fig. 3 A(b-d)) accompanied with transition from  $Mn_2O_3$  to  $Mn_3O_4$  with the increment of  $La_2O_3$  loading. The ionic radius of doped  $La^{3+}$  is between those of  $Mn^{3+}$  (0.066 nm) and  $O^{2-}$  (0.140 nm). Therefore, the  $La^{3+}$  ions (0.102 nm) can replace the  $Mn^{3+}$  sites, which further vary the close-packed of particles and increase the defects in the crystal structure.<sup>36</sup> In the meantime,  $MnO_x$  crystallite sizes reduced after the doping with  $La_2O_3$  due to segregation of the doped  $La^{3+}$



**Fig. 3** Wide-angle XRD patterns of (A) fresh and (B) sulphidized (a, a<sub>1</sub>) 10La90Mn/KIT-6, (b) fresh 5La95Mn/KIT-6, (c, c<sub>1</sub>) fresh and sulphidized 3La97Mn/KIT-6, (d) fresh 100Mn/KIT-6 and; (C) fresh and regenerated (c, c<sub>1</sub>, c<sub>2</sub>) 3La97Mn/KIT-6 after third cycles and eighth cycles, respectively.

ions at the grain boundary, which inhibited the aggregation of grains.<sup>37</sup> However, there was no La diffraction peak to be observed up to 10 wt% La loading. This indicated that  $La_2O_3$  presented in an amorphous state or very fine particles without the detection using of X-ray diffractometer.<sup>38</sup> The particles of  $MnO_x$  and  $La_2O_3$  lowered remarkably and were dispersed highly on the support as a result of the synergetic effects which will result in the variation of sorbent in the structural properties.<sup>39, 40</sup>

For used 10La90Mn/KIT-6, the peaks of  $La_2O_3$  at  $2\theta = 28.51^\circ$  and  $\alpha$ -MnS [PDF#65-0891] ( $2\theta = 29.62^\circ$ ,  $34.34^\circ$ ,  $49.35^\circ$ ,  $61.50^\circ$ ) were observed in XRD patterns. However, there was only  $\alpha$ -MnS [PDF#65-0891] phase to be detected in used 3La97Mn/KIT-6 (Fig. 3B(c<sub>1</sub>)) due to the low content of La species.

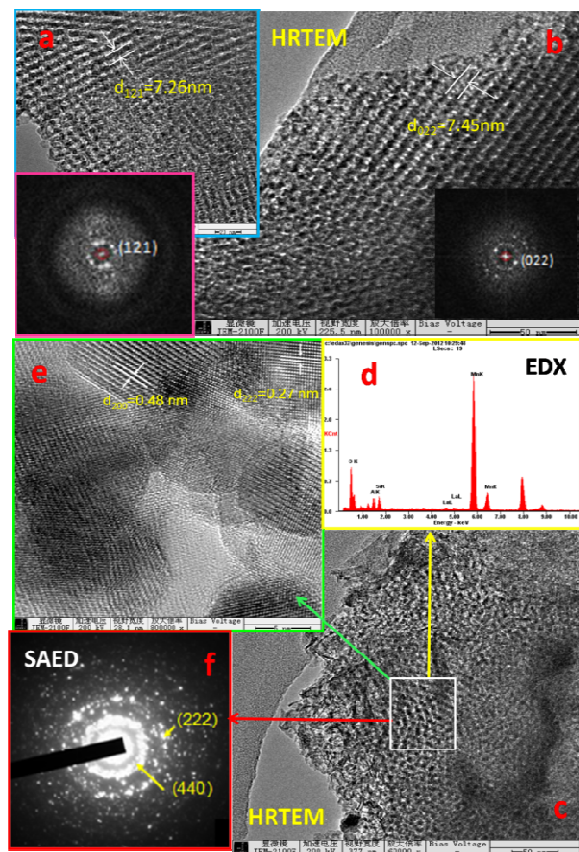
As for XRD patterns of 3La97Mn/KIT-6 regenerated at 600 °C for 3 and 8 times, respectively (Fig. 3C), there was a significant

variation in structure compared to fresh 3La97Mn/KIT-6 without the formation of sulphate. The peaks at  $2\theta = 18.02^\circ$ ,  $28.97^\circ$ ,  $32.41^\circ$ ,  $36.04^\circ$ ,  $44.37^\circ$ ,  $58.76^\circ$  and  $60.02^\circ$  were assigned to  $\text{Mn}_3\text{O}_4$  [PDF#18-0803], indicating that  $\text{Mn}_3\text{O}_4$  was the most stable spinel phase in regenerated sorbents, plausibly due to low oxygen atmosphere (6% v  $\text{O}_2/\text{N}_2$  mixture). However, there is no obvious change in intensity and width of the XRD peaks of 3La97Mn/KIT-6 regenerated at  $800^\circ\text{C}$  for 3<sup>rd</sup> and 8<sup>th</sup> cycles. In a word, the metal oxides can disperse again on the inner surface of KIT-6 during the regeneration treatments (Fig. 3C(c<sub>1</sub>,c<sub>2</sub>)), which was favourable to the multi-utilization of sorbent.

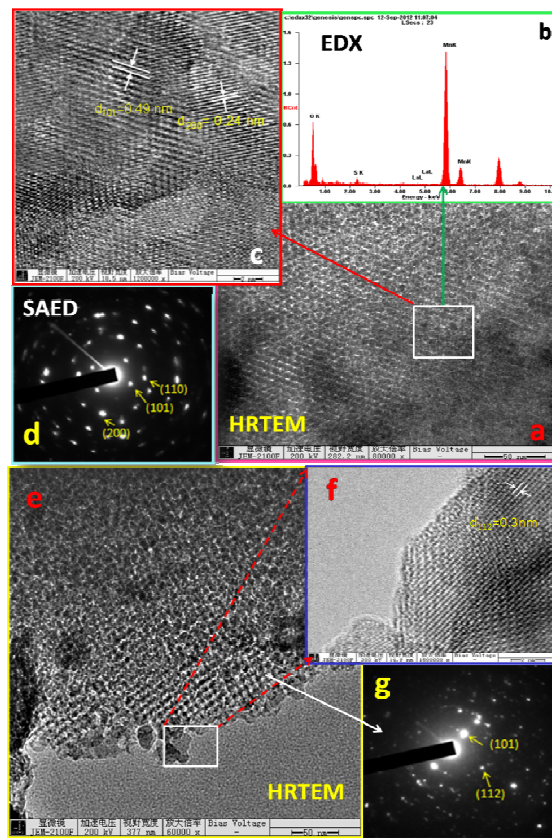
### 3.3 HRTEM Images of Sorbents

The fine structures of KIT-6, fresh, used and regenerated 3La97Mn/KIT-6 were investigated by means of HRTEM technique. As shown in Fig. 4a-b, the HRTEM images and corresponding FT diffraction patterns (inset of Fig. 4a-b) revealed that KIT-6 exhibited clear lattice fringes. The distance between two dark strips is about 7 ~ 8 nm, close to the results (8 ~ 9.1 nm) calculated by small-angle XRD ( $n\lambda = 2d\sin\theta$ ), an indicative of the highly ordered 3D pore

structures<sup>41</sup>. The HRTEM images of fresh 3La97Mn/KIT-6 illustrated that KIT-6 still remained the double gyroidal mesoporous structure and the active species of metal oxides were dispersed uniformly in the channel of KIT-6 after metal oxides,  $\text{Mn}_2\text{O}_3$  and  $\text{La}_2\text{O}_3$  loadings (Fig. 4c). It can be seen from the result of EDX analysis that Mn and La oxides were incorporated successfully with KIT-6 support. Small part of metal oxides were aggregated on the outer surface of KIT-6 and formed metal oxide particles with the diameter of 10-14 nm due to higher oxide loadings (50%)(Fig. 4e). As shown in Fig. 4e, the magnification HRTEM image of metal oxide crystallites revealed the existence of regular crystalline particles and the two  $d$ -spacing obtained by the distance between light-dark strips were 0.27 and 0.48 nm, corresponding to the (222) plane of cubic  $\text{Mn}_2\text{O}_3$  and the (101) plane of  $\text{Mn}_3\text{O}_4$  (JCPDS 18-0803), respectively. Fig. 4f showed the selected area electron diffraction (SAED) in this region. The light dots dispersed highly on diffusion concentric circles indicated that metal oxides existed mainly in polycrystalline particles with small amount of nanocrystallites. The crystal  $d$ -spacings estimated via SAED patterns were 0.25 and 0.16 nm, corresponding to the (222) and (440) plane of  $\text{Mn}_2\text{O}_3$  nanoparticles. Therefore, the phase analysis of fresh 3La97Mn/KIT-6 sorbent verified that active species existed in  $\text{Mn}_2\text{O}_3$  and  $\text{Mn}_3\text{O}_4$  mixed crystallites, similar to the results of XRD analysis (Fig. 3A(c)). Besides, there is no signal of  $\text{La}_2\text{O}_3$  in SAED images, plausible due to the loadings of trace  $\text{La}_2\text{O}_3$ .



**Fig. 4** HRTEM images of KIT-6, viewed from (a) [111], (b) [311] phase directions (inset: FT diffraction patterns); (c) HRTEM image (d)corresponding EDX analysis of fresh 3La97Mn/KIT-6; (e) HRTEM image (f) SAED patterns of  $\text{MnO}_x$  species of fresh 3La97Mn/KIT-6.



**Fig. 5** (a) HRTEM image and (b, d) corresponding EDX analysis and SAED patterns of 3La97Mn/KIT-6 after sulphidation at  $800^\circ\text{C}$ ; (c) HRTEM image of

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sulphides of 3La97Mn/KIT-6 after sulphidation at 800 °C; (e) HRTEM images of 3La97Mn/KIT-6 after regeneration, (f) HRTEM images and (g) the corresponding SAED patterns of regenerated metal oxides in 3La97Mn/KIT-6.

HRTEM image and EDX analysis of 3La97Mn/KIT-6 after sulphidation at 800 °C illustrated that the mesoporous silica KIT-6 framework still remained intact, indicating a hydrothermal stability of the support. Furthermore, there were no significant aggregations of metal sulphides to appear, indicating that the utilization of KIT-6 was effective to depress the aggregation of metal particles inside channels (Fig. 5a). SAED image revealed that the diffraction characteristics of polycrystallites reduced and the properties of crystals intensified remarkably. In the meantime, the symmetrical array of diffraction dots appeared. The crystal *d*-spacing calculated by diffraction dots in SAED image were 0.27 and 0.33 nm, corresponding to the (200) and (111) planes of cubic MnS crystallites, respectively, similar to the distance (0.24 nm) between two dark strips in magnification HRTEM image of MnS crystallites. Besides, we observed strong diffraction dots with the *d*-spacing of 0.49 nm on SAED pattern, attributed to the (101) planes of Mn<sub>3</sub>O<sub>4</sub> (JCPDS 18-0803) that did not react in 3La97Mn/KIT-6 sorbent although Mn<sub>3</sub>O<sub>4</sub> species were not detected in XRD patterns. In the meantime, the *d*-spacing (0.49 nm) of the (101) planes of Mn<sub>3</sub>O<sub>4</sub> was observed in magnification HRTEM image (Fig. 5c). In a word, the crystallites of MnS grew up and aggregated to a certain extent after sulphidation reaction compared to fresh 3La97Mn/KIT-6.

Fig. 5e-g presented the TEM/SAED analysis for 3La97Mn/KIT-6 regenerated for three cycles. Fig. 5e showed well-reserved 3D mesoporous framework of KIT-6, which facilitated the gas-solid reaction in sorbent through continuous desulphurization-regeneration cycles. The HRTEM image of regenerated particles was observed with *d*-spacing at 0.30 nm (Fig. 5f). The corresponding SAED patterns of active particles indicated that they contributed to (101) and (112) plane of Mn<sub>3</sub>O<sub>4</sub>, respectively.

### 3.4 H<sub>2</sub>-TPR Measurements

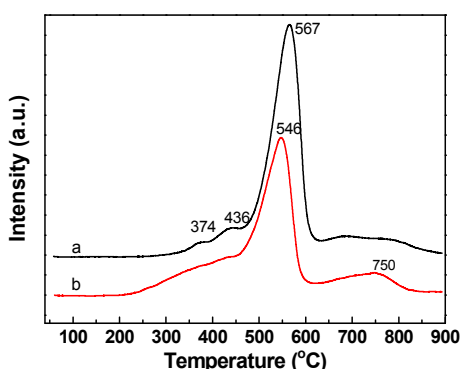


Fig. 6 TPR profiles of (a) 3La97Mn/KIT-6 and (b) 10La90Mn/KIT-6

As shown in Fig. 6, there are two minor reduction peaks in the range of 374–436 °C and a strong peak centred at 567 °C in H<sub>2</sub>-TPR profile of 3La97Mn/KIT-6. The former was ascribed to the reduction of partial Mn oxides on the surface of sorbent, and the latter was attributed to the reduction of Mn<sub>3</sub>O<sub>4</sub> and Mn<sub>2</sub>O<sub>3</sub> to MnO<sup>42,43</sup> according to the equation<sup>44</sup>,  $3\text{Mn}_2\text{O}_3 + \text{H}_2 = 2\text{Mn}_3\text{O}_4 + \text{H}_2\text{O}$ ,  $\text{Mn}_3\text{O}_4 + \text{H}_2 = 3\text{MnO} + \text{H}_2\text{O}$ . On the contrary, the H<sub>2</sub>-TPR peaks over 10La90Mn/KIT-6 shifted to low temperature region due to segregation action of La<sub>2</sub>O<sub>3</sub> species and two reduction peaks centred at 546 and 750 °C were ascribed to the reduction of Mn oxides to the MnO<sup>42, 43</sup> and reduction of partial MnO to Mn<sup>0</sup><sup>45</sup>. This suggested that Mn oxides were reduced more easily with increasing amounts of La<sub>2</sub>O<sub>3</sub> species, indicating that the active sites to react with H<sub>2</sub> enhanced due to the smaller sizes and better dispersion of the particles. In addition, the H<sub>2</sub> consumption over 3La97Mn/KIT-6 was higher than that over 10La90Mn/KIT-6, because the former existed mainly in Mn<sub>2</sub>O<sub>3</sub> and the latter in Mn<sub>3</sub>O<sub>4</sub> species (Fig. 3A), resulting in different H<sub>2</sub>-consumption contents between two sorbents.

### 3.5 XPS Analysis

Fig. 7 showed the XPS spectra of Mn over fresh, used and regenerated 3La97Mn/KIT-6 sorbents. The binding energies (BEs) at 653.6 eV and 641.6 eV can be described to Mn 2p<sub>1/2</sub> and Mn 2p<sub>3/2</sub> in Mn<sub>2</sub>O<sub>3</sub> (Fig. 7A(a)). As shown in Fig. 7A, there was nearly no difference between Mn 2p peaks before and after desulphurization, i.e. it is difficult to identify the oxidation states of Mn.<sup>46</sup> According to report of Töpfer et al,<sup>47</sup> there was appreciable distinction in Mn3p peaks between Mn<sup>3+</sup> (49.5 eV) and Mn<sup>2+</sup> (48.2 eV) ions. Therefore, the spectra of Mn3p were collected in order to verify the chemical states of manganese. The broadening of the Mn3p peak in Fig. 7B revealed the different valence states of Mn in fresh 3La97Mn/KIT-6 sorbent, which had been verified by XRD analysis. After smoothing and background subtraction by a fitting of the Mn3p spectrum, there was approximately equal peak area of Mn<sup>3+</sup>/Mn<sup>2+</sup>, indicating the coexistence of both Mn<sup>3+</sup> and Mn<sup>2+</sup> ions. Fig. 7C showed that MnO<sub>x</sub>

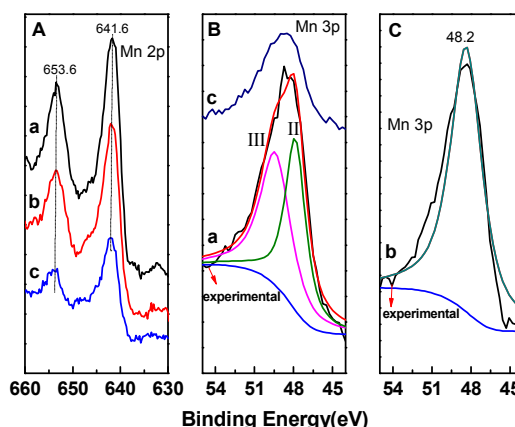


Fig. 7 Mn 2p (A) and Mn 3p (B-C) spectra of fresh (a), used (b) and regenerated (c) 3La97Mn/KIT-6 sorbents.



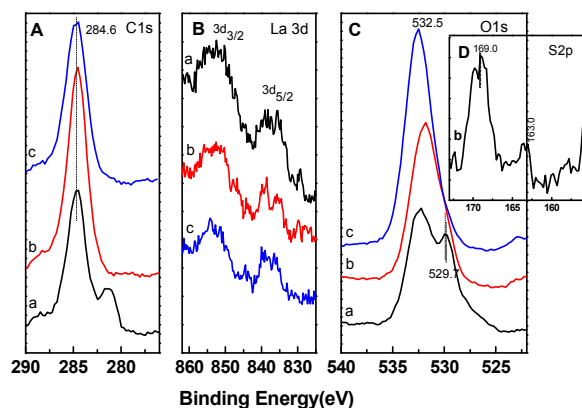


Fig. 8 C 1s (A), La 3d (B), O 1s (C) and S 2p (D) spectra of fresh (a), used (b) and regenerated (c) 3La97Mn/KIT-6 sorbents

was transformed into MnS after desulphurization with the BE values of 48.2 eV. After regeneration, MnS was transformed into  $\text{Mn}_3\text{O}_4$  (Fig. 7B(c)), which was consistent with XRD results (Fig. 3).

C 1s peaks (284.6 eV) in Fig. 8A originated from the contaminant carbon species and a shoulder peak at 281.2 eV in C 1s XPS spectra of fresh 3La1097Mn/KIT-6 (Fig. 8A(a)) correlated closely with the formation of carbides. This may stem from incomplete combustion of citric acid during the calcination of sorbent. The  $\text{La}3d_{5/2}$  BE is 835.5 eV, 16.8 eV apart from the  $\text{La}3d_{3/2}$  peak (Fig. 8B) in accord with that reported in literature.<sup>48</sup> It could be seen that there was no obvious variation between BEs of  $\text{La}3d_{5/2}$  and  $\text{La}3d_{3/2}$  before and after sulphidation, meaning that valence states of La remained constant. The peaks at 532.5 eV and 529.7 eV for fresh 3La97Mn/KIT-6 (Fig. 8C) were assigned to O 1s spectra in  $\text{SiO}_2$  and metal oxides, respectively. After sulphidation, the O 1s peak at 529.7 eV disappeared (Fig. 8C(b)) and the signal of S 2p at 163.0 eV occurred due to the transformation of metal oxides to metal sulphides (Fig. 8D). The peak at 169.0 eV was attributed to the signal of sulphate. The interaction of sulphides with the oxygen atoms on sorbent will result in the formation of sulphate.

### 3.6 Effect of La/Mn Atomic Ratios on Performance of Sorbents

The effect of different La/Mn atomic ratios on desulphurization performance of sorbents was shown in Fig. 9. It was worthwhile to note that 100Mn/KIT-6 showed the lowest sulphur capacity (8 g sulphur/100 g sorbent) with slowly deactivation rate (Fig. 9d). The gas-solid reaction between  $\text{H}_2\text{S}$  and  $\text{MeO}_x$  occurred first on the surface and then extended to the bulk phase. The low sulphur capacity was attributed to the high diffusion resistance of  $\text{H}_2\text{S}$  from surface to bulk due to the aggregation of  $\text{Mn}_2\text{O}_3$  particles in the absence of  $\text{La}_2\text{O}_3$  (Fig. 3A(d)). The doping of a small amount of  $\text{La}_2\text{O}_3$  in the Mn-based sorbent could decrease significantly the particle size and improve the dispersion of Mn species, which can expose more active sites and is favourable to the diffusion of  $\text{H}_2\text{S}$  within active particles. The desulphurization performance might be controlled by the number of the active centres and related to the amount of manganese oxide species having different surface

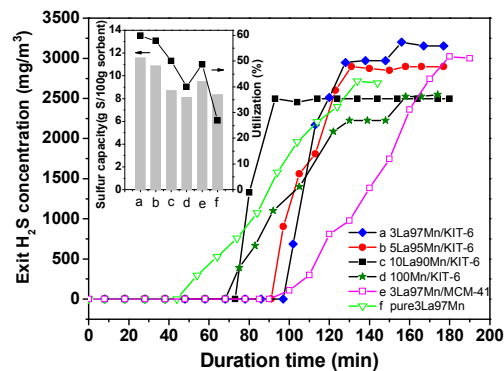


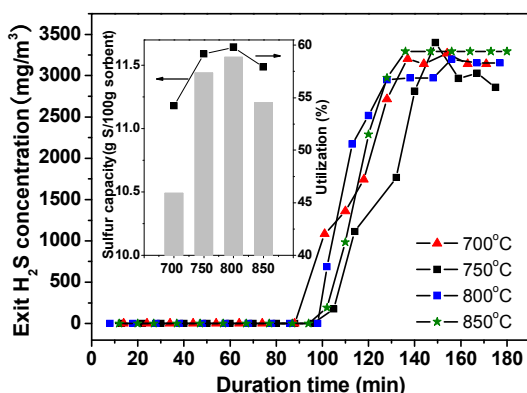
Fig. 9  $\text{H}_2\text{S}$  breakthrough curves for xLaMn/KIT-6 sorbents with different La/Mn ratios. (a) 3La97Mn/KIT-6, (b) 5La95Mn/KIT-6, (c) 10La90Mn/KIT-6, (d) 100Mn/KIT-6, (e) 3La97Mn/MCM-41 and (f) pure 3La97Mn. Reaction temperature: 800 °C; WHSV=21600 mL/(h·g); feed composition: 66.44%  $\text{N}_2$ , 13.84%  $\text{H}_2$ , 19.36%  $\text{CO}$ , 0.36%  $\text{H}_2\text{S}$ .

vacancies. However, the sulphur capacity of  $\text{La}_2\text{O}_3$  itself is low and the reaction rate with  $\text{H}_2\text{S}$  was slow. Therefore, the  $\text{H}_2\text{S}$  breakthrough sulphur capacity (BSC) over 3La97Mn/KIT-6, 5La95Mn/KIT-6 and 10La90Mn/KIT-6 decreased with incremental  $\text{La}_2\text{O}_3$  loadings. 3La97Mn/KIT-6 exhibited the highest sulphur capacity (11.56 g sulphur/100 g sorbents) with the utilization of about 60%. On the other hand, the XRD patterns of the sorbents also illustrated that  $\text{Mn}_2\text{O}_3$  transformed gradually into  $\text{Mn}_3\text{O}_4$  phase with the increase of  $\text{La}_2\text{O}_3$  species. Ko et al.<sup>49</sup> reported that the desulphurization performance of the  $\text{Mn}_2\text{O}_3$  was better than that of  $\text{Mn}_3\text{O}_4$  due to the reduction of  $\text{Mn}_2\text{O}_3$  during sulphur adsorption. The terrace occurrence in desulphurization curve of 10La90Mn/KIT-6 sorbent may originate from the catalytic action of  $\text{La}_2\text{O}_2\text{S}$  species to make decomposition of  $\text{H}_2\text{S}$  at high temperature, similar to the catalytic phenomenon of  $\text{Sm}_2\text{O}_3\text{S}^{50}$ . In addition, 3La97Mn/KIT-6 sorbent exhibited higher breakthrough sulphur capacity when compared with pure 3La97Mn and 3La97Mn/MCM-41. A poor desulphurization performance of the pure 3La97Mn sorbent (0.25 g) at 800 °C was due to the low surface area and pore volume (Table S1 and Fig. S1, Supplementary Information). The low deactivation rate (Fig. 9f) over pure 3La97Mn after breakthrough point meant that there was strong mass transfer limitation when  $\text{H}_2\text{S}$  contacted with MnOx in bulk due to the presence of larger  $\text{Mn}_2\text{O}_3$  particles, which was verified by XRD result (Fig. S2, Supplementary Information). Hence, the utilization of pure 3La97Mn sorbent decreased seriously. In the meantime, the desulphurization performance over 3La97Mn/MCM-41 with straight 1-D pore structure reduced slightly (Fig. 9e) due to both dispersion of  $\text{Mn}_2\text{O}_3$  particle over the framework and the diffusion resistance of  $\text{H}_2\text{S}$  molecules. The XRD result of 3La97Mn/MCM-41 (Fig. S2(b)) also verified the existence of large active species of  $\text{Mn}_2\text{O}_3$ . In a word, KIT-6 with 3D double gyroidal channel was outstanding candidate for hot coal gas desulphurization due to its special textural properties.

### 3.7 Effect of Desulphurization Temperature on Performance of 3La97Mn/KIT-6

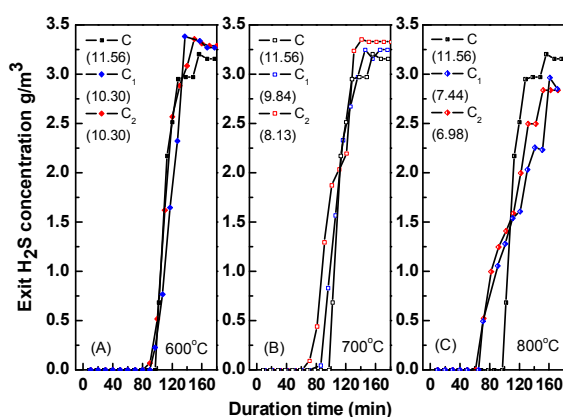
The effect of desulphurization temperature on the performance for hot coal gas desulphurization was investigated in the range of 700-





**Fig. 10** H<sub>2</sub>S breakthrough curves for 3La97Mn/KIT-6 sorbents at different sulphurization temperatures. WHSV=21600mL/(h·g); feed composition: 66.44% N<sub>2</sub>, 13.84% H<sub>2</sub>, 19.36% CO, 0.36% H<sub>2</sub>S.

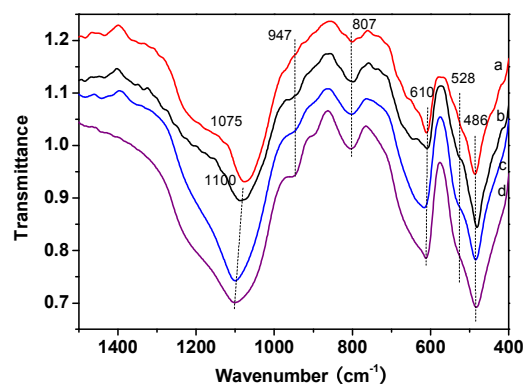
850 °C. As shown in Fig. 10, the breakthrough time and the corresponding sulphur uptake capacity over 3La97Mn/KIT-6 increased from 700 to 800 °C. According to the report of Bakker *et al.*<sup>1</sup>, the initial desulphurization reaction rate increased with the increasing reaction temperature. However, the desulphurization performance over 3La97Mn/KIT-6 declined slightly at 850 °C, plausible due to the serious deterioration of mesoporous silica framework. The  $S_{\text{BET}}$  (68 m<sup>2</sup>/g) and  $V_{\text{meso}}$  (86 mm<sup>3</sup>/g) of 3La97Mn/KIT-6 after desulphurized at 850 °C declined significantly (Table 1), which resulted in the rise of H<sub>2</sub>S diffusion resistance during the reactions. However, the HRTEM and BET results revealed that the double gyroidal mesoporous structure of 3La97Mn/KIT-6 remained intact (Fig. 5a). As a result, 800 °C was determined as the most feasible temperature.



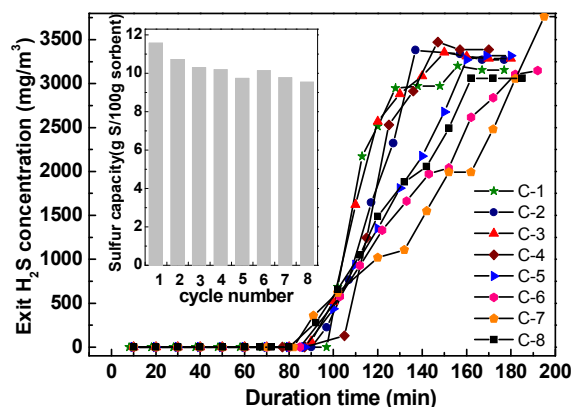
**Fig. 11** H<sub>2</sub>S breakthrough curves over (C) fresh and (C<sub>1</sub>, C<sub>2</sub>) regenerated 3La97Mn/KIT-6 sorbents. Desulphurization: 800 °C; WHSV=21600mL/(h·g); feed composition: 66.44% N<sub>2</sub>, 13.84% H<sub>2</sub>, 19.36% CO, 0.36% H<sub>2</sub>S. Regeneration: (A) 600 °C, (B) 700 °C, (C) 800 °C; WHSV = 7200 mL/(h·g); feed composition: 5% O<sub>2</sub>/N<sub>2</sub>. The data in parentheses in the upper left is the corresponding sulphur capacity (S/100g sorbent)

### 3.8 Effect of Regeneration Temperature on Properties of 3La97Mn/KIT-6

The effect of regeneration temperature on the properties of 3La97Mn/KIT-6 was shown in Fig. 11. During desulphurization (800 °C)-regeneration cycles based on the following equation:  $3\text{MnS} + 5\text{O}_2 = \text{Mn}_3\text{O}_4 + 3\text{SO}_2$  ( $\Delta H = -3298\text{KJ/mol}$ ). It can be seen that the regeneration reaction is exothermic, so it should be carried out at temperature as low as possible to avoid the sintering of the sorbents. The H<sub>2</sub>S breakthrough curves over 3La97Mn/KIT-6 regenerated at 600 °C almost kept unchangeable and about 89% of initial activity could be remained for 3<sup>rd</sup> cyclic regeneration (Fig. 11A). In the meantime, HRTEM images and  $S_{\text{BET}}$  of 3La97Mn/KIT-6 regenerated at this temperature verified the existence of mesoporous structure of 3La97Mn/KIT-6. However, the desulphurization performance of sorbents regenerated at 700 and 800 °C declined, especially at 800 °C. The breakthrough curve became smooth after breakthrough time point (Fig. 11C), because high temperature could induce the collapse of the mesoporous silica framework of sorbent, resulting in the decrease of  $S_{\text{BET}}$  and  $V_t$  (56 m<sup>2</sup>/g and 0.10 cm<sup>3</sup>/g) (Table 1). Besides, the FT-IR spectra (Fig. 12) of sorbents regenerated at 600-800 °C revealed that the bands (400-700 cm<sup>-1</sup>) ascribed to the asymmetry, bending and stretching vibration of Mn-O bonds in Mn<sub>2</sub>O<sub>3</sub> and Mn<sub>3</sub>O<sub>4</sub><sup>52,53</sup> did not vary significantly and the formation of little sulphates increased slightly with incremental regeneration temperature (the bands at 947 cm<sup>-1</sup> were attributed to the adsorption of SO<sub>4</sub><sup>2-</sup><sup>54</sup>). The bands at 1075 and 807 cm<sup>-1</sup> were ascribed to the asymmetric and symmetric stretching vibration of Si-O<sup>55</sup> for 3La97Mn/KIT-6, which was shifted to 1100 cm<sup>-1</sup> after regeneration due to the contract in the mean bond length<sup>56-58</sup> of Si-O-Mn in supported metal oxides during transformation from Mn<sub>2</sub>O<sub>3</sub> to Mn<sub>3</sub>O<sub>4</sub> (Fig. 3C(c<sub>1</sub>,c<sub>2</sub>)).



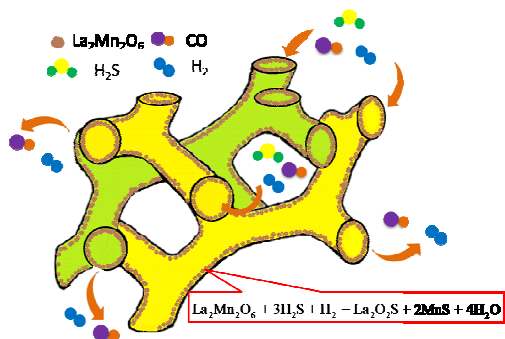
**Fig. 12** FT-IR spectra of fresh and regenerated sorbents. (a) fresh 3La97Mn/KIT-6, (b) 3La97Mn/KIT-6 regenerated at 600 °C for 3 cycles, (c) 3La97Mn/KIT-6 regenerated at 700 °C after 3 cycles, (d) 3La97Mn/KIT-6 regenerated at 800 °C after 3 cycles.



**Fig. 13**  $\text{H}_2\text{S}$  breakthrough curves for eighth desulphurization-regeneration cycles over 3La97Mn/KIT-6 sorbent (Inset is corresponding breakthrough sulfur capacity). Desulphurization: T-800 °C; WHSV=21600 mL/(h·g); feed composition: 66.44%  $\text{N}_2$ , 13.84%  $\text{H}_2$ , 19.36%  $\text{CO}$ , 0.36%  $\text{H}_2\text{S}$ . Regeneration: T-600 °C; WHSV=7200 mL/(h·g); feed composition: 5%  $\text{O}_2/\text{N}_2$ .

### 3.9 Successive Sulphurization-Regeneration Performance of 3La97Mn/KIT-6

In order to study the regeneration stability, mechanical strength and desulphurization performance of 3La97Mn/KIT-6 sorbents, eight desulphurization-regeneration cycle results and the corresponding sulphur uptake capacity were shown in Fig. 13. It can be seen that the BSC over fresh 3La97Mn/KIT-6 was 11.56 g sulphur /100 g sorbents, which was significantly higher than that over 50%wt  $\text{LaFeO}_3/\text{MCM-41}$  (5.58 g sulphur /100 g sorbents)<sup>59</sup> and the latter was used only at 500-550 °C. This indicated that the addition of Mn active species and the utilization of high stable mesoporous KIT-6 with double gyroidal structure (Scheme 1) increased remarkably the sulphur capacity of sorbent and improved the sulphidation performance at high temperature (800 °C). As shown in scheme 1, the 3D double gyroidal channel of KIT-6 constrained effectively the sintering of active La-Mn species as well as the pulverization of sorbents. Therefore, the performance of the sorbent after 9<sup>th</sup> cycle was highly stable with ca. 80% of the initial activity. The XRD results of 3La97Mn/KIT-6



**Scheme 1.** Scheme of stable xLa97Mn/KIT-6 with double gyroidal structure for hot coal gas desulphurization.

verified that the active La-Mn clusters still were dispersed highly on KIT-6 after 3<sup>rd</sup> and 8<sup>th</sup> regeneration cycles. The HRTEM images illustrated that mesoporous structure of KIT-6 remained intact (Fig. 5e-f) after successive desulphurization-regeneration.

## Conclusions

A series of xLa97Mn/KIT-6 were prepared by a sol-gel method. The 8<sup>th</sup> desulphurization-regeneration tests of 3La97Mn/KIT-6 indicated that 3La97Mn/KIT-6 performed well with stable regeneration ability. BET analysis, small-angle XRD and HRTEM images suggested that the mesoporous framework of 3La97Mn/KIT-6 was stable during cyclic regeneration tests. The utilization of KIT-6 ensured the highly dispersion of active particles and confined the migration of active particles during desulphurization-regeneration tests, which was essential for the regeneration of 3La97Mn/KIT-6.

## Acknowledgements

We gratefully acknowledge the joint financial support of National Natural Science Foundation of China and BAOSTEEL Group Corporation (Grant 50876122).

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