

Analytical Methods

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2 **1 In-line single-phase extraction for direct determination of total iron in oils**
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4 **2 using CdTe quantum dots and a flow-batch system**
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Abstract

In this work, a novel method for direct determination of total iron in viscous samples (edible oils and biodiesel) is presented. Considering sensitivity and selectivity, the proposed method used in-line single-phase extraction and CdTe quantum dots (QDs). The method was automated employing a flow-batch system. The in-line single-phase extraction of iron consisted in the addition of a mixture of ethanol/chloroform (75:25, v/v) to dissolve the oil samples, followed by addition of an acid solution, HNO₃/HCl (3:1, v/v) to make the iron available. The analytical method was based on iron's capacity to establish surface interactions with CdTe QDs that result in a quenching of their fluorescent intensity proportional to the iron concentration. Various factors that may influence the fluorescence quenching of the iron, such as pH, sample volume, amount of the organic mixture, and acid solution concentration were studied. The maximum reproducibility of this fluorescence quenching occurred at pH 7.5. Phosphate buffered saline (PBS) 1.0 mol L⁻¹ was added before the reaction. Method validation and application to real samples showed that the analytical features of the developed method were quite satisfactory in terms of linearity ($r^2 = 0.997$), limit of detection (0.1 µg g⁻¹), precision (RSD < 1.6 %), and accuracy (recovery = 95.5 – 104.3 % range), when compared to others works in the literature. The proposed automatic method presented suitable robustness, a high sampling rate (79 h⁻¹), and lower waste generation per determination (0.900 mL), contributing to the basic principles of green chemistry.

Keywords: In-line single-phase extraction; Flow-batch system; CdTe quantum dots; Fluorescence determination of iron; Viscous matrices.

1. Introduction

Trace metallic elements are naturally present in oils due to two factors: (i) contamination from soil and fertilizers where the plant is grown, and (ii) contact with equipment during extraction, refining, and transportation. However, it is widely known that metals, although being present in low concentrations, have negative effects on the oxidative stability of both edible and non-edible oils. Iron, which has a catalytic effect on the autoxidation of both edible oils and biodiesel, is a common example of this problematic. Iron concentration is an important parameter for the quality control of oils, but due to their high organic contents, its accurate determination remains an analytical challenge.^{1,2}

Several methods have been developed and applied to the determination of iron in edible oils and biodiesel, usually using atomic absorption, x-ray fluorescence, or emission spectrometry.^{3,4} However, these methods have drawbacks including high cost, complex analyses, low sample throughput, and the necessary sample pretreatment methods to reduce matrix influences; these include dissolutions in organic toxic solvents, mineralization (calcination), acidic extraction, emulsification, sonication, and microwave digestion.⁵

Taking into account these disadvantages, a preferable iron determination may be explored using automated procedures based on the principles of flow analysis, which allows working with small volumes, saving both samples and reagents, and therefore contributing to green analytical chemistry.⁴ However, when it comes to oils, the physic-chemical characteristics of these matrices, such as high viscosity and elevated organic load, make them difficult for analysis in flow systems, especially when using in-line pretreatments.^{5,6}

An alternative to overcome such drawbacks is the use of a flow-batch system.⁷ Recently, our research group has developed a procedure for automatic spectrophotometric determination of Fe(III) in oils, (without external pretreatment) using methanol-chloroform and methyl isobutyl ketone as solvents.⁸ The system allowed us to obtain satisfactory figures of merit, and a high

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2 59 sampling frequency. However, the procedure might have been improved with respect to its
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4 60 sensitivity and selectivity, as well as for reducing its organic (toxic) solvents consumption.
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7 61 During the last decade, several sensitive and selective methods have been developed
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9 62 involving the use of cadmium telluride quantum dots (CdTe QDs).^{9,10} In most CdTe QD
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11 63 applications, the detection is based on signal quenching. More recently, attention has been
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13 64 focused on signal enhancement, mainly associated with QDs ability to sensitize distinct
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15 65 chemiluminescence systems.¹¹ When employing CdTe QDs in analyses involving oil matrices, it
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17 66 becomes necessary to solubilize the sample.
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21 67 These disadvantages can be overcome by a simple strategy to transform the viscous analyte
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23 68 medium into a single-phase alcohol medium. Ribeiro and Rocha¹² described a simple and fast
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25 69 procedure for the direct determination of free glycerol in biodiesel exploiting a single-phase
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27 70 system. The procedure employed consists in simultaneously dissolving biodiesel and an acetyl-
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29 71 acetone reagent with anhydrous ethanol. A similar strategy was reported by Shishov et al.¹³
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31 72 where isopropyl alcohol was used to produce a single-phase system for automated determination
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33 73 of calcium (II), and magnesium (II) with eriochrome black T as the indicator. Both procedures
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35 74 are fast, simple, and inexpensive, without requiring mechanical agitation or centrifugation steps.
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40 75 In this study for the first time, an automated method for direct determination of total iron in
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42 76 edible oils and biodiesel is proposed using in-line single-phase extraction, CdTe QDs, and a
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44 77 flow-batch system. The in-line single-phase extraction consists in the addition of an
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46 78 ethanol/chloroform mixture to dissolve the oil samples, followed by addition of an acid solution
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48 79 (HNO₃/HCl, 3:1) and buffer (1.0 mol L⁻¹ of pH 7.50 phosphate buffered saline) to bring forward
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50 80 the analyte. Iron's capacity to establish surface interactions with the CdTe QDs results in a
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52 81 quenching of the fluorescent intensity, which is proportional to the analyte concentration.
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2. Experimental

2.1 Reagents, solutions and samples

All reagents were of analytical grade, and freshly distilled and deionized water ($> 18 \text{ M}\Omega \text{ cm}^{-1}$) was used to prepare all solutions. The reagents were not subjected to any further purification.

Anhydrous ethanol and chloroform (Synth) were used to prepare a mixture of ethanol/chloroform (75:25 v/v) to dissolve the oil samples. To release the analyte nitric and hydrochloric acid (Merck) were used to prepare an acid solution (HNO_3/HCl , 3:1).

A 1.0 mol L^{-1} of pH 7.50 phosphate buffered saline (PBS) solution (compound of $13.76 \text{ mol L}^{-1} \text{ NaCl}$, $0.27 \text{ mol L}^{-1} \text{ KCl}$, $0.97 \text{ mol L}^{-1} \text{ Na}_2\text{HPO}_4 \cdot 12\text{H}_2\text{O}$, $0.15 \text{ mol L}^{-1} \text{ KH}_2\text{PO}_4$) was used in the experiments.

A $100 \mu\text{g g}^{-1}$ metal-organic iron standard was purchased from Quimlab (SRM 1079b NIST), and mineral oil (Sigma-Aldrich) was used for the dilutions of the metal-organic standard solution.

For the synthesis of the CdTe QDs the following reagents were used: sodium borohydride (NaBH_4 , 99%), tellurium powder (200 mesh, 99.8%), cadmium chloride hemi (pentahydrate) ($\text{CdCl}_2 \cdot 2.5 \text{ H}_2\text{O}$, 99%), and 3-mercaptopropionic acid (MPA, 99%) purchased from Sigma-Aldrich. To adjust the alkalinity of the reaction medium, a $1.0 \text{ mol L}^{-1} \text{ NaOH}$ solution was used.¹¹

The methodology was applied to six commercial edible oils (olive, soybean and sunflower), and six biodiesel samples (B100) originated from different feedstocks (soybean, sunflower, maize).

2.2 Apparatus

Measurements in the automatic flow-batch system were carried out by a multi-channel CCD spectrophotometer (model USB4000, Ocean Optics), with a tungsten-halogen light source (LS-1-LL, Ocean Optics), and two $100 \mu\text{m}$ i.d. optical fibers.

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2 109 To characterize the synthesized nanocrystals, the QD absorption spectra were obtained
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4 110 using a UV-Vis spectrophotometer (model 8453, Hewlett-Packard). The fluorescence
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6 111 measurements were performed with a spectrofluorimeter (model FL3-11, Fluorolog-3), equipped
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9 112 with a xenon discharge light source (450 W). The slits can vary from 1 to 20 nm. Those selected
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11 113 were 5 nm for excitation, and 10 nm for emission. A quartz fluorimetric cell with a 10 mm
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14 114 optical path, and 220 μL of internal volume (type 73.2 F-Q-10, Starna cells, USA) were used.

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16 115 For comparison purposes the oil samples were analyzed using a Shimadzu AA6800 atomic
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18 116 absorption spectrometer with a longitudinally heated graphite tube atomizer, equipped with a
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21 117 Shimadzu ASC-6100 auto-sampler, and pyrolytic-coated graphite tubes. Argon 99.996% was
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23 118 used as purge and protective gas. A single element hollow cathode lamp for iron (Hamamatsu
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26 119 Photonics, λ_{max} : 248.33 nm), operated at 4 mA was used as a light source. The monochromator
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28 120 spectral band pass (slit) was 0.7 nm.

32 122 2.3. Synthesis of CdTe QDs

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35 123 CdTe QDs were synthesized as previously described¹¹ with some modifications. Briefly,
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37 124 NaHTe solution was prepared by reaction between NaBH_4 (1×10^{-3} mol), and tellurium powder
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40 125 (0.4×10^{-3} mol) in N_2 saturated water (20 mL). The reaction mixture was heated to 80°C for 30
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42 126 min under N_2 flow to get an intense clear red solution. This NaHTe solution was stored for
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45 127 further use at room temperature still under the protection of N_2 .

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47 128 The NaHTe solution was then transferred to another flask containing CdCl_2 (4×10^{-3} mol)
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49 129 and MPA (7×10^{-3} mol) in a 100 mL N_2 saturated water solution. The pH of the solution was
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52 130 adjusted to 11.5 by adding 1.0 mol L^{-1} NaOH solution. The $\text{Cd}^{2+} : \text{Te}^{2-} : \text{MPA}$ molar ratio was
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54 131 fixed at 1 : 0.1 : 1.7. The CdTe QD's size was tuned by varying the heating time. In order to
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56 132 remove the contaminants, purification of the QDs was performed by precipitation in absolute
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59 133 ethanol. The precipitate fractions were subsequently centrifuged, vacuum dried, and kept in a
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134 refrigerator.

The nanocrystals size for the synthesized CdTe QDs was calculated as shown in Eq. (1):¹⁴

$$D = (9.8127 \times 10^{-7}) \lambda^3 - (1.7147 \times 10^{-3}) \lambda^2 + (1.0064) \lambda - 194.84 \quad (1)$$

where D is the diameter or size of the nanocrystals (nm) and λ is the wavelength of maximum absorbance corresponding to the first excitonic absorption peak of the crystal.

The CdTe QD aqueous solution molar concentration was determined by appraising the extinction coefficient (ϵ), calculated as shown in Eq. (2):¹⁴

$$\epsilon = 3450 \Delta E (D)^{2.4} \quad (2)$$

where ΔE is the transition energy corresponding to the first absorption peak expressed in eV. D (nm) is the size of the CdTe QDs. Knowing both ϵ and the absorbance peak of the nanocrystal solution; the molar concentration was calculated by applying the Lambert-Beer's law.

2.4. Flow-batch system

A schematic diagram of the flow-batch proposed is shown in Fig. 1. The homemade mixing chamber (MC) was built in PTFE (polytetrafluoroethylene). It has a total volume of 2.0 ml and three quartz windows (W1, W2, and W3) mounted at 180° and 90° from each other (1 cm optical path).

The flow-batch (FB) consists of five three-way solenoid valves (V_S , V_E , V_A , V_B , V_{QDs} , and V_w) model EW-01540-13 (Cole Parmer); polyethylene tubing connectors with 0.8 mm id; a peristaltic pump (PP) model 78002-00 (Ismatec), Fluor-elastomer pumping tubes with 1.0 mm i.d. were used for propelling all fluids.

The additions of the sample or standard solution (S), ethanol/chloroform solution (E), acid solution (A), PBS buffer solution (B), CdTe QDs solution (QDs) into the MC were performed switching ON valves V_S , V_E , V_A , V_B , V_{QDs} , respectively. A stirring bar (SB) performs the homogenization of the mixture in the MC under the action of the magnetic stirrer (MS) and the MC is emptied switching ON the valve V_w .

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2 160 Data acquisition, solenoid valves, peristaltic pump were computer controlled using an USB
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4 161 interface (USB6009, National Instruments) and software developed in LabVIEW 2013 (National
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11 164 **2.5. In-line operation procedure**

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14 165 Before starting the analytical procedure, working solutions for each channel are pumped
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16 166 for continuous recirculation to their respective reservoirs. Then the valves V_S , V_E , V_A , V_B and
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18 V_{QDs} are simultaneous switched ON for a time interval of 1.50 s, and the working solutions (S, E,
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21 168 Then immediately, the discard valve V_W is switched ON for 5.0 s and MC is emptied using the
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23 169 peristaltic pump (PP). This channels filling procedure is very important and must be carried out
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26 170 whenever there is a change of the working solutions in reservoir.
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30 172 The analyzer was operated as described in [Table 1](#) for the direct determination of iron in
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33 173 edible oils and biodiesel using a portable spectrofluorimeter for detection. As the rotation speed
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35 174 of the peristaltic pump is computer controlled, a flow rate of $18.1 \pm 1.2 \mu\text{L s}^{-1}$ ($n = 20$) was
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38 175 employed for the edible oil and biodiesel sampling (S) and of $148.2 \pm 1.3 \mu\text{L s}^{-1}$ ($n = 20$) was
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40 176 used for the ethanol/chloroform solution (E), acid solution (A), buffer solution (B), and CdTe
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42 177 QDs solution (QDs) of the MC. Stirring was constant inside MC during the whole process.
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45 178 However, after additions of the solutions extra time of 2 s was employed for homogenization
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47 179 (steps 2, 4, 6, and 8). This extra time allowed for a reproducible analytical response.
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49 180 The differing samples or standard solution (adding 25 μL by V_S), and the solvent
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51 181 ethanol/chloroform (adding 600 μL by V_E), were added simultaneously to the MC (step 1).
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54 182 Following, came acid, buffer, and CdTe QDs solutions (steps 3, 5, and 7, respectively), each
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56 183 added to the mixing chamber. Finally, the analytical signal was measured inside the MC (step 9),
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59 184 and all of its content was aspirated for waste (step 10, removing 900 μL by V_W).
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2 185 Afterwards, the system carried out a cleaning cycle, simultaneously adding ethanol/
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4 186 chloroform solution, and a new differing sample or standard (step 11); this procedure is
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7 187 necessary for cleaning of the MC, and for filling the channel between valve V_S and the MC with
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9 188 new sample or standard. The excess of the solutions in the MC were aspirated towards waste
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11 189 (step 12). The cleaning cycle was completed by addition of the acid solution (step 13),
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14 190 homogenization (step 14), and discard (step 15).

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16 191 During steps 2 through 10 shown in [Table 1](#), the sample was manually replaced by the new
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19 192 sample in the intake tube (recycled to the reservoir); this period of about 11 s is sufficient for this
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21 193 procedure. For in-line blank preparation, mineral oil was added through the valve V_S, and the
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23 194 methodology for analysis is similar to described for the sample and standard solution.

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28 196 2.6. Reference method

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30 197 For comparison, the proposed flow-batch system was evaluated against a graphite furnace
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33 198 atomic absorption spectrometer (GFAAS) method. The samples were mineralized at 550 °C as
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35 199 previously described.¹⁵ Ten grams (10 g) of sample (edible oils and biodiesel) were weighed
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38 200 directly into quartz crucibles. In sequence, 0.5 g of magnesium oxide was added. The mixture
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40 201 was calcinated gradually to 550 °C. (1 h at 100 °C, 1 h at 180 °C, 5 h at 250 °C, 1 h at 300 °C,
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42 202 and 2 h at 550 °C) in order to avoid sample loss. After cooling down carefully to room
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45 203 temperature, the ashes were dissolved directly in the crucible with small portions of an aqueous
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47 204 1.0 mol L⁻¹ H₂SO₄ solution (total volume 25 mL), and gradually transferred to a 50.0 mL
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49 205 volumetric flask. Standard solutions were prepared from 1.0 to 10.0 µg Kg⁻¹. The analytical
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51 206 signals (absorbance) were measured at a maximum absorbance of around 248.3 nm. The analysis
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54 207 of each sample was performed in triplicate and the concentrations were calculated from the
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56 208 analytical curve.

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60 210 3. Results and discussion

3.1. Analyte extraction

The determination method is based on the interaction of iron with CdTe QDs, reducing their photoluminescence emission by means of a quenching mechanism.¹⁶ To eliminate the procedure of iron extraction from viscous matrices to an aqueous medium, we carried out the reactions in an organic based media, a single-phase system.¹³ The criterion for the choice of the solvent and the mixing ratio was its ability to be well mixed with the edible oils and biodiesel in order to provide high repeatability.

It worth highlighting that CdTe QDs are insoluble in ethanol and chloroform, and when precipitating they exhibit a pronounced decrease of fluorescence. However, we observe that the addition of HNO₃/HCl 3:1 (v/v) and PBS buffer solutions, and homogenization in the sequence presented in [Table 1](#) (1 to 8 steps) avoid CdTe QDs precipitation and a concomitant decrease of fluorescence.

The results shown in [Fig. 2a](#) suggest that anhydrous ethanol and chloroform mixing 75:25 (v/v) is the most suitable solvent for in-line dilution of viscous samples. The acid solution of HNO₃/HCl 3:1 (v/v) was the most effective for the extraction of all iron remnants in the sample ([Fig. 2b](#)). Using acid solution without direct organic extraction is not effective or reproducible due to formation of emulsions and/or non-mixing of the phases. In fact, the joining of the two extractions allowed greater data reproducibility.

3.2. Optimization of the reaction conditions

As previously reported in the literature,¹⁶ the larger CdTe QDs are not sufficiently sensitive to iron. However, in the study, smaller nanocrystals were clearly more sensitive to the metal, providing a significant decrease in fluorescence intensity. Thus, the size of 1.65 nm CdTe QDs was selected as the most adequate for iron determination.

When the CdTe QDs concentration was too low, the slope was gentle because the QDs did not quantitatively complex in the given concentration range of iron, in other words, the limited

CdTe cannot occupy all non-specific binding sites of coexisting iron in the system. In addition, it was found that at higher QD concentrations, the relative effect of quenching magnitude decreased by reason of the lower concentration, that is, a relatively higher concentration of iron would be needed to quench the luminescence of the CdTe QDs, a reduced sensitivity towards probing iron. Considering these factors, a QD concentration of $2.5 \times 10^{-4} \text{ mol L}^{-1}$ was adopted.

The effect of solution pH value on the fluorescent intensity was studied, and the results are shown in Fig. 3. It can be seen that the optimum range of pH was 7.0 to 8.0. If the pH is too low or too high, the relative fluorescence intensity is lower. The reason may be explained as follows: in acid medium, the fluorescence intensity decreases as a possible result of the deconstruction of the Fe(III)-MPA complex's annulus due to the protonation of the surface-binding thiolates.¹⁷ When the pH increases to above 8, the fluorescence intensity decrease may be due to the precipitation product ($\text{Fe}(\text{OH})_3$). In this work, in order to avoid iron precipitation, a pH of 7.5 was chosen to run the assay. This result is in agreement with other studies available in the literature.^{16,17}

3.3. Optimizatization of the proposed flow-batch method

The parameters of the proposed flow-batch method were evaluated in order to improve the sensitivity and reproducibility of the analytical signal. All the optimization studies were performed automatically in the proposed FB. The studied range and selected values as the best compromise between reproducibility and sensitivity are presented in Table 2. If needed, modifications of parameters may be re-studied and carried out by simply changing the operational parameters in the FB system control software.

3.4. Evaluation of interferences

The selectivity of the spectrofluorimetric method using CdTe QDs was investigated. Samples containing a fixed amount of iron ($50 \mu\text{g g}^{-1}$), and increasing concentrations of the

species under evaluation were analyzed using the developed methodology. A compound was considered “non-interfering” if the analytical signal variation was $\pm 5\%$ as compared to that obtained in its absence. Under the reaction parameters used, the results (Table 3) show that no significant interfering effect for the majority of the tested compounds was found. Under the system operating conditions, no interfering effect was observed.

3.5. Analytical features

For the determination of iron in viscous matrices using the proposed method, the regression equation was $A = -0.0797 + 0.0087 C$, where A is the analytical response for the fluorescence intensity signal (Eq. 3), and C is the iron concentration in $\mu\text{g g}^{-1}$ in the measuring solution. The squared linear correlation coefficient, r^2 was 0.997 ($n = 5$) in the range between 10.0 to 100.0 $\mu\text{g g}^{-1}$.

$$A = -\log P / P_0 \quad (3)$$

where P and P_0 are fluorescence intensity of standard solutions and blank, respectively.

The analytical curve was statistically validated by analysis of variance (ANOVA), showing no significant lack of fit in the proposed models at a 95% confidence level. The limit of detection (LOD), and the limit of quantification (LOQ) for both methods were estimated based on the criteria established by the International Union of Pure and Applied Chemistry (IUPAC).¹⁸ LOD and LOQ were evaluated as $3s_b / S$ and $10s_b / S$, respectively, where s_b is the standard deviation for 20 measurements of the blank and S is the slope of analytical curve. For the determination of iron the LOD and LOQ were 0.10 $\mu\text{g g}^{-1}$ and 0.34 $\mu\text{g g}^{-1}$, respectively.

Table 4 presents the results for the proposed FB system, and the reference method for the iron in viscous matrices. No statistically significant differences were observed between the results at a confidence level of 95% when applying the paired t -test. The relative standard

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2 289 deviation (RSD %) was less than 1.5 %, for iron, respectively, and it were obtained from five
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4 290 replicates.
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7 291 Recovery tests were also performed using four real samples of edible oils and biodiesel
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9 292 with mean values of analyte concentration equal 4.02 and 5.03 $\mu\text{g g}^{-1}$ for edible olive and
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12 293 soybean oil, respectively; and 1.05 and 2.98 $\mu\text{g g}^{-1}$ for soybean and sunflower biodiesels,
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14 294 respectively (see Table 5). For this purpose, 1.0 mL of standard solution with known
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17 295 concentrations of 10.0, 25.0, and 50.0 $\mu\text{g g}^{-1}$ of iron was added to 9.0 mL of each real sample,
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20 296 and spiked samples were analyzed using the proposed FB system. As can be seen in Table 5,
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22 297 good recoveries values (within the 95.5 – 104.3 % range) were obtained for the three analyzed
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24 298 samples.
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27 299 Table 6 presents selected analytical features of the proposed and other methods.^{4,6,8,16,19}
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29 300 Compared to other procedures, the proposed FBA system presents, in general, satisfactory
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31 301 parameters, such as; limit of detection, working range, smaller sample volumes, and relative
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34 302 standard deviation. Moreover, this method is fully automated; a simple in-line single-phase
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36 303 extraction is carried out for sample pretreatment.
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40 305 **Conclusion**

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43 306 A novel method for direct determination of total iron in edible oils and biodiesel using in-
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45 307 line single-phase extraction, CdTe QDs and a flow-batch system was presented. The in-line
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48 308 single-phase extraction consisted in the addition of an ethanol/chloroform mixture (75:25) to
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50 309 dissolve the oils samples, followed by addition of an acid solution (HNO_3/HCl , 3:1) to make the
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53 310 iron available. The iron analyte establishes a surface interaction with the nano-crystals which
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55 311 results in a concentration proportional quenching of fluorescent intensity.
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57 312 When compared to other works reported in the literature^{4,6,16,19}, the proposed method
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59 313 presents satisfactory limits of detection, quantification, precision, and accuracy. Moreover, it
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314 also presented significant reductions in consumption of reagents (0.275 mL), organic solvents

(0.600 mL), and samples (0.025 mL). Therefore, it was possible to developed a good automatic method with high sample throughput (79 h^{-1}) and lower waste generation per determination (0.900 mL), contributing to the basic principles of green chemistry. All this permits suggesting the proposed method as a potentially useful alternative for determination of other analytes in viscous matrices.

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2 378 **FIGURE CAPTIONS**

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4 379 **Figure 1.** The flow-batch system manifold. Mixing-chamber (MC); quartz windows (W1, W2,
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7 380 W3); light source (tungsten lamp); spectrofluorimeter (USB4000); optical fiber (OP); three-way
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9 381 solenoid valves (V_S , V_E , V_A , V_B , V_{QDs} , and V_W); magnetic stirrer (MS); stirring bar (SB); sample
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11 382 or standard solution (S); ethanol/chloroform solution (E), acid solution (A), PBS buffer solution
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14 383 (B), CdTe QDs solution (QDs).

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17 384 **Figure 2.** Effect of the solvent extraction ratio.

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21 385 **Figure 3.** Effect of pH on the relative fluorescence intensity of system CdTe QDs 2.5×10^{-4}
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23 386 mol L⁻¹; 50 μg L⁻¹ of iron solution.

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Table 1

Operation steps of the flow-batch system for the direct determination of iron in edible oils and biodiesel.

Step	Event	Time (s)	Volume (μL)
1	Addition of the sample (V_S) ^a	1.4 ^b	25
	Addition of the solvent ethanol/chloroform (V_E) ^a	4.0	600
2	Homogenization	2.0	–
3	Addition of the acid solution (V_A)	0.7	100
4	Homogenization	2.0	–
5	Addition of the buffer solution (V_B)	0.7	100
6	Homogenization	2.0	–
7	Addition of the CdTe QDs solution (V_{QDs})	0.5	75
8	Homogenization	2.0	–
9	Measurements of the analytical signal	1.0	–
10	Waste (V_W) – emptying of MC	6.1	–
11 ^c	Addition of the ethanol/chloroform solution (V_E) ^a	4.0	600
	Addition of the new sample or standard (V_S) ^{a,d}	2.8	50
12 ^c	Waste (V_W) – emptying of MC	6.1	–
13 ^c	Addition of the acid solution (V_A)	6.1	900
14 ^c	Homogenization	2.0	–
15 ^c	Waste (V_W) – emptying of MC	6.1	–

^a Simultaneous addition.

^b Addition of edible oils or biodiesel.

^c Steps 11 to 15 belong to the cleaning cycles.

^d Sometimes necessary for filling the feed channel from valve VS to MC with the new sample or standard.

Table 2

Selected parameters of the FB system procedure for direct determination of iron in edible oils and biodiesel.

Parameter	Range	Selected value
Sample volume (μL) ^a	10 – 100	25
Ethanol/chloroform (75:25, v/v) (μL)	200 – 1000	600
HNO ₃ /HCl (3:1, v/v) (μL)	50 – 200	100
PBS buffer solution (μL)	50 – 200	100
CdTe QDs solution (μL)	50 – 200	50
Homogenization between additions (s)	1 – 10	2
Cleaning numbers	1 – 4	2
Total volume (μL)	500 – 1200	875

^a For both viscous samples (edible oils and biodiesel).

Table 3

Summary of the interference effects of possible ions on the peak height obtained from 50 $\mu\text{g g}^{-1}$ of iron solution.

Foreign ions	Tolerable concentration ratio ^a ($\mu\text{g L}^{-1}$)
Cd^{2+}	85
Zn^{2+}	65
Pb^{2+}	75
Cr^{2+}	80
Cu^{2+}	85
Ca^{2+}	70
Mg^{2+}	70

^a The concentration of an ion is considered to be interfered with when causing a relative error of more than $\pm 5\%$ with respect to the signal of iron alone.

Table 4

Results for the direct determination of iron in edible oils and biodiesel using the proposed flow-batch system, and atomic absorption as the comparative method ($\mu\text{g g}^{-1}$). Mean values and uncertainties are based on five analytical determinations.

Samples		Proposed method		Reference method	
		Fe (III) $\pm t_{n-1} S/\sqrt{n^a}$	RSD % ^b	Fe (III) $\pm t_{n-1} S/\sqrt{n^a}$	RSD % ^b
Edible oils	Olive	3.96 \pm 0.06	1.45	4.02 \pm 0.05	0.88
		4.63 \pm 0.05	1.51	4.59 \pm 0.05	0.91
	Soybean	4.98 \pm 0.04	1.42	5.03 \pm 0.04	0.76
		3.41 \pm 0.05	1.36	3.38 \pm 0.03	0.81
Sunflower	2.55 \pm 0.06	1.15	2.59 \pm 0.04	1.09	
	5.11 \pm 0.05	1.32	5.14 \pm 0.03	0.95	
Biodiesel	Soybean	1.09 \pm 0.05	1.23	1.05 \pm 0.04	0.79
		4.58 \pm 0.04	1.51	4.61 \pm 0.03	0.63
	Sunflower	2.21 \pm 0.05	1.15	2.26 \pm 0.04	0.94
		2.94 \pm 0.05	1.32	2.98 \pm 0.03	0.85
	Maize	3.03 \pm 0.05	1.23	2.96 \pm 0.04	0.92
		2.05 \pm 0.04	1.51	1.99 \pm 0.05	0.65

^a Where n is the number of replicate measurements, t_{n-1} is the statistic parameter often called Student's t (with $n = 5$, at 95% level of confidence), and S is the standard deviation.

^b RSD: relative standard deviation.

Table 5

Recoveries of iron in edible oils and biodiesel (n = 5).

Samples ($\mu\text{g g}^{-1}$)		Recovery %		
		$10.0 (\mu\text{g g}^{-1}) \pm t_{n-1} S/\sqrt{n^a}$	$25.0 (\mu\text{g g}^{-1}) \pm t_{n-1} S/\sqrt{n^a}$	$50.0 (\mu\text{g g}^{-1}) \pm t_{n-1} S/\sqrt{n^a}$
Edible oil	Olive oil (4.02)	102.4 ± 2.1	98.5 ± 2.3	104.3 ± 2.4
	Soybean oil (5.03)	99.3 ± 2.4	95.5 ± 2.2	101.6 ± 2.2
Biodiesel	Soybean (1.05)	103.5 ± 2.2	102.5 ± 2.1	95.9 ± 2.3
	Sunflower (2.98)	98.7 ± 2.5	101.6 ± 2.4	103.4 ± 2.3

^a Where n is the number of replicate measurements, t_{n-1} is the statistical parameter often called Student's t (with $n = 5$, at 95% level of confidence), and s is the standard deviation.

Table 6

Comparison of the proposed method with previously reported methods for determination of iron in edible oils and biodiesel.

Detection technique	Analyte	Sample	Sample preparation	Fully automated technique	Sample amount	Working range (mg L ⁻¹)	LOD (µg g ⁻¹)	RSD%	Ref.
UV-Vis (with multivariate calibration)	Si, P, Fe, Al	Biodiesel	Microwave digestion	No	1.0 g	2 – 20	0.6	5.0	4
UV-Vis	Fe(III)	Edible oil	Organic solvents	Yes	150 µL	0.5 – 25	0.31	< 3.5	6
UV-Vis	Fe(III)	Edible and Mineral oils	Organic solvents	Yes	100 µL	0.1 – 1.0	0.02	< 1.6	8
Fluorescence	Fe	Biodiesel	Ultrasound-assisted	No	200 µL	6 – 100	1.25	< 2.6	16
AAS	Cu, Fe	Edible oil	Dry ashing	No	4 – 20 g	0 – 10	0.6	2	19
Fluorescence	Fe	Edible and biodiesel	In-line single phase extraction	Yes	25 µL	0.1 – 1.0	0.1	< 1.6	This work

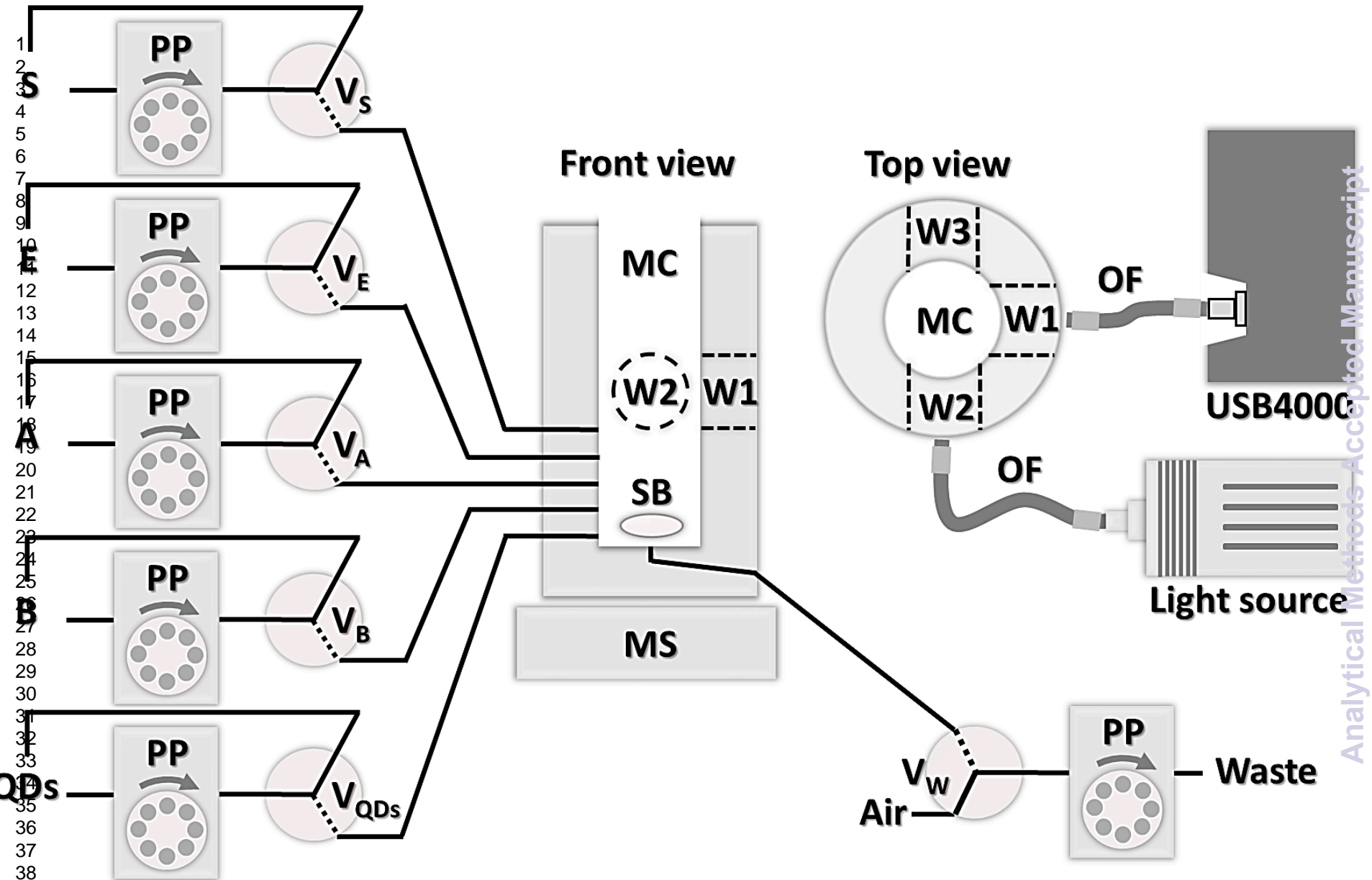


Fig. 1

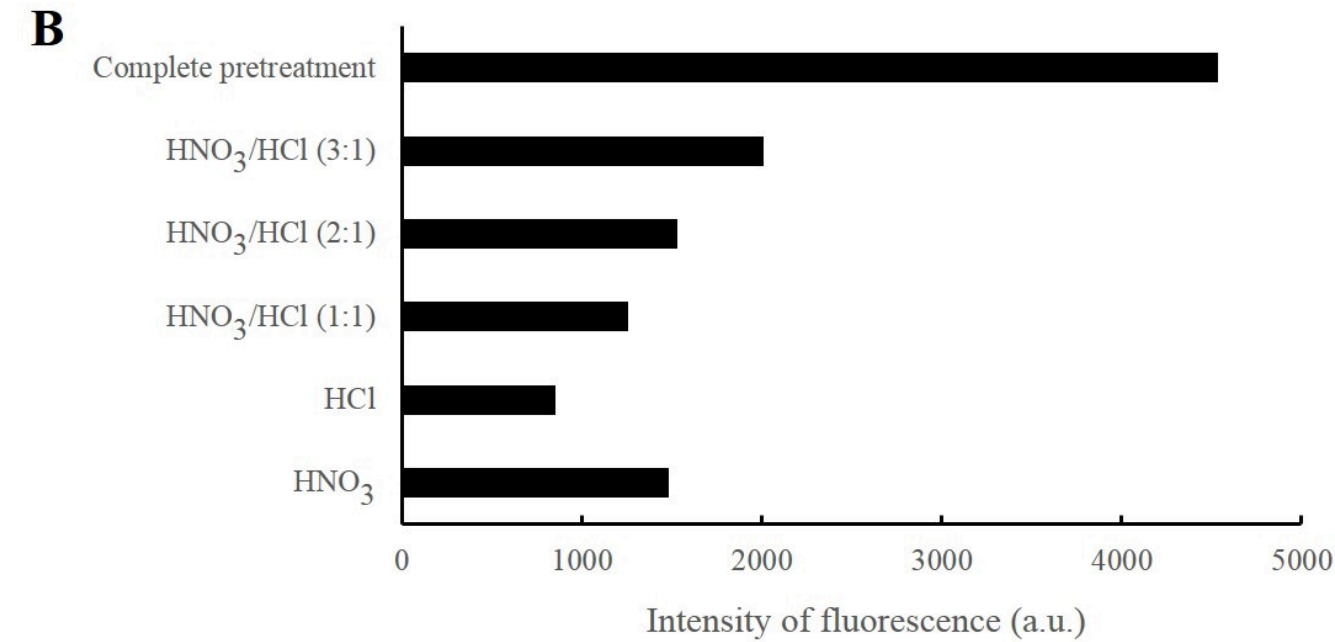
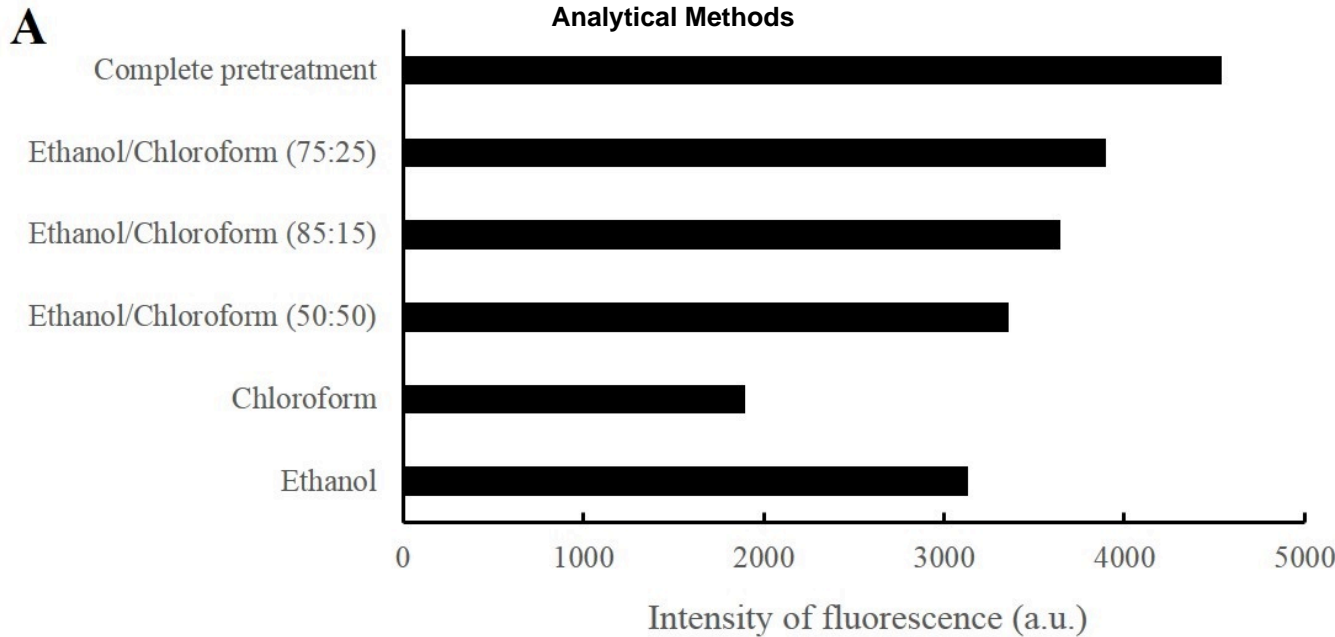


Fig. 2

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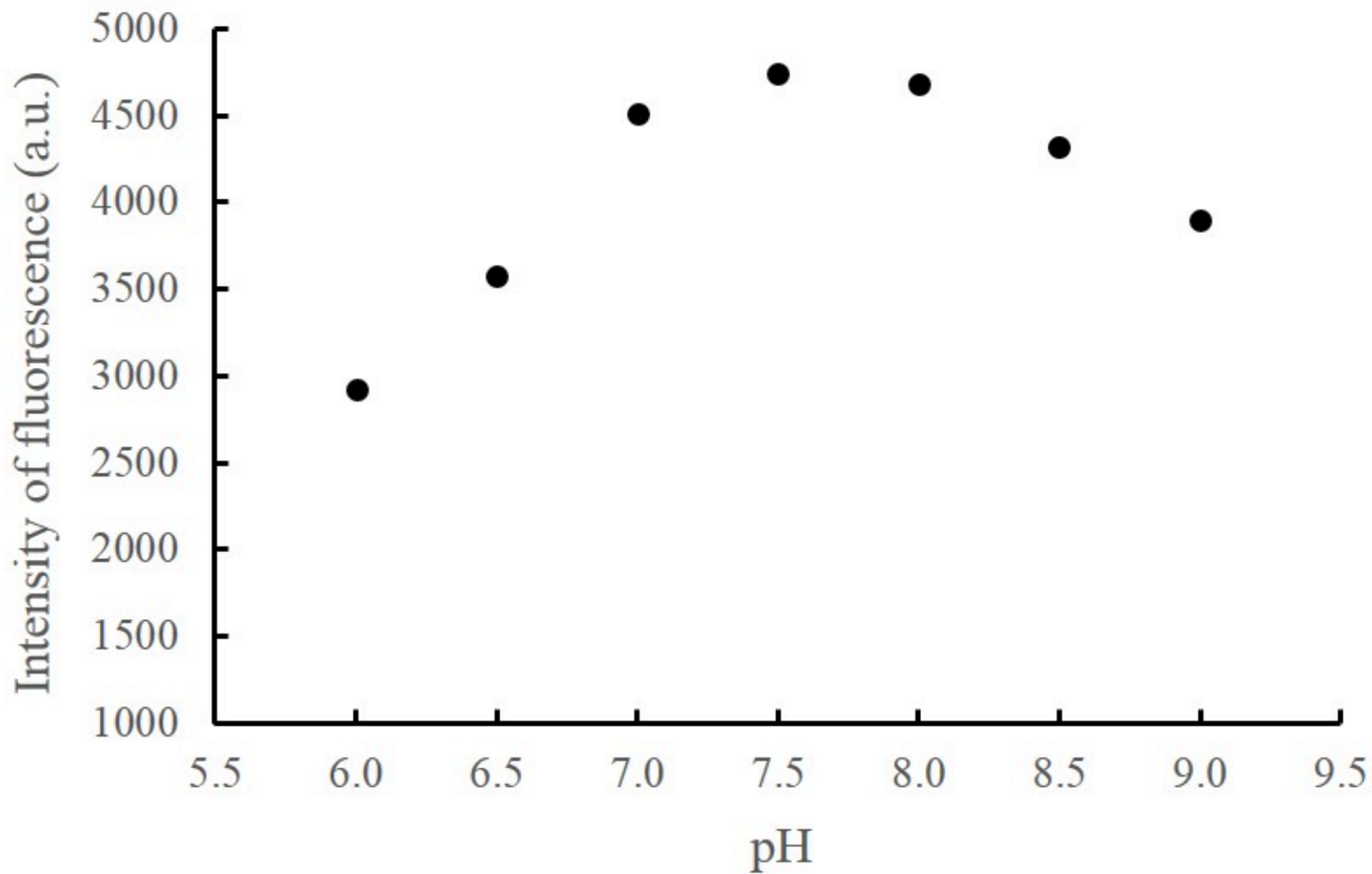


Fig. 3