# Journal of Materials Chemistry A

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# Journal of Materials Chemistry A

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# ARTICLE



of other TMPs with crystallizable controlling units.

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# **1. Introduction**

Thermo-sensitive polymer networks exhibiting a temperaturememory effect (TME)<sup>1-8</sup> typically exhibit a broad thermal transition  $\Delta T_{\text{trans}}^{9}$  or two overlapping thermal transitions, which could also exhibit multi-shape effects.<sup>10-12</sup> Temperaturememory polymers (TMPs) can memorize the temperature  $T_{\text{deform}}$  within  $\Delta T_{\text{trans}}$ , where they have been deformed during programming. The original shape of the programmed TMP is recalled when response temperatures  $T_{sw}$  are exceeded, whereby  $T_{\rm sw}$  are equal to or above  $T_{\rm deform}$ . The temperature interval  $\Delta T_{\text{trans}}$ , which can be either a glass  $(T_{\text{g}})$  or melting  $(T_{\text{m}})$ transition, can be considered as an ensemble of individual sharp transitions  $(T_{\text{trans},i})$ , whereby each single sharp transition can be utilized as reversible physical crosslinks for fixation of the temporary shape. In this context, first theoretical model approaches have recently been introduced for the description of amorphous TMPs.<sup>2, 13, 14</sup> Still, it is relevant to understand and experimentally confirm the mechanistic aspects of TME in polymers with crystallizable controlling units. One example for polymers having a broad  $\Delta T_{\rm m}$  and showing excellent temperature-memory properties over a temperature interval of up to 90 °C is crosslinked poly[ethylene-co-(vinyl acetate)] (cPEVA) comprising amorphous vinyl acetate (VA) segments and crystallizable polyethylene (PE) segments.<sup>4</sup> The broad  $\Delta T_m$ in cPEVA is a result of the sequence structure of the copolymer and in particular the distribution of PE segment lengths, which

are related to the thickness of the crystalline lamellae. The broadness of  $\Delta T_{\rm m}$  in cPEVA can be influenced by either the weight fraction of VA co-monomer or the crosslink density of the polymer network.

temperature might enable the prediction of the TME behavior and the knowledge based design

We hypothesized that the TME capability of cPEVA is enabled by specific nanostructures of the crystals, which remember the temperature of the deformation. Several contributions might influence the crystallizable controlling units when a temperature-memory creation procedure is applied, which consist of a deformation step at certain  $T_{deform}$  within  $\Delta T_m$ . First, the temperature  $(T_{deform})$  prior deformation could be considered as an isothermal treatment, permitting the variation of crystal dimensions. Second, the deformation step could lead into a rearrangement of the crystal structure (e.g. orientation of crystals) and third, the contribution of the cooling step when fixing the temporary shape will influence the nanostructure responsible for memorizing different  $T_{deform}$ s. These changes of the semi-crystalline nanostructure would be caused both by the temperature within the melting range and the deformation to the temporary shape.

In this study, we explored the nanostructural changes during temperature-memory programming and recovery for a series of cPEVAs with regard to the contribution of temperature treatment by means of specific annealing experiments as well as DSC analysis, the influence of the deformation step during temperature-memory creation procedure (TMCP) at different temperatures, and the contribution of the cooling step on the

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formed semi-crystalline nanostructure via *in situ* X-ray scattering techniques (small- and wide-angle X-ray scattering SAXS/WAXS). In this way, the effect of applying different  $T_{\text{deform}}$ s on the nanostructure of PE crystalline domains in programmed cPEVAs and therefore on the TME mechanism could be revealed.

In the following we describe the thermomechanical characterization of the cPEVA copolymer networks. Their nanostructure is explored by SAXS and WAXS and compared to theoretical dimensions. The thermal contribution to the TME is investigated by annealing experiments of non-deformed samples and analyzed by DSC. The contribution of the mechanical deformation at  $T_{deform}$  and the contribution of the cooling step to changes of the nanostructure of the crystallizable controlling units are investigated *in situ* by SAXS and WAXS. Finally, mechanisms at high and low  $T_{deform}$  are deduced from these experiments and temperature dependent pathways for the TME are presented.

# 2. Experimental

#### 2.1. Materials

Poly[ethylene-*co*-(vinyl acetate)]s (DuPont, Wilmington, USA) with vinyl acetate contents of 18 wt% and 28 wt% (data of supplier) and the thermosensitive initiator dicumyl peroxide (DCP) (Sigma-Aldrich, Taufkirchen, Germany) were used as received. Copolymer networks were prepared as described in reference,<sup>15</sup> i.e., PEVAs were mixed with 0.5, 1, or 2 wt% DCP in a twin-screw extruder (EuroPrismLab, Thermo Fisher Scientific, MA, USA) at 110 °C and 50 rpm. The obtained PEVA/DCP blends were compression molded into films with 1 mm thickness at 200 °C at 20 bar for 25 min.

#### 2.2. Thermogravimetric analysis (TGA)

TGA measurements were carried out on a TGA 209 (NETZSCH, Selb, Germany) in the temperature range from - 25 °C to 700 °C with a heating rate of 20 K·min<sup>-1</sup>. The composition of cPEVA was analyzed according to the weight loss of acetic acid groups observed in the temperature range from 300 °C to 410 °C,<sup>16</sup> where the vinyl acetate weight content (VAC) was calculated by **Equation (1)**.

$$VAC = \frac{w_1 \cdot \left(\frac{M_w(VA)}{M_w(-COOCH_3)}\right)}{w} \times 100$$
(1)

Here  $w_1$  is the weight loss attributed to the deacetylation of VA segments in the temperature range from 300 °C to 410 °C and w is total weight of cPEVA samples.  $M_w$  (VA) is the molar mass of VA and  $M_w$  (-COOCH<sub>3</sub>) the molar mass of the acetic acid groups. The sample ID cPEVAxx denotes the VAC as determined by TGA.

## 2.3. <sup>1</sup>H-NMR spectroscopy

<sup>1</sup>H-NMR spectroscopy recorded at 25 °C on a 500 MHz Advance spectrometer (Bruker, Karlsruhe, Germany) using tetramethylsilane (TMS) as internal standard. Experiments were performed at 500 MHz (<sup>1</sup>H) resonance frequency with the spectral width of 10000 Hz. Samples were dissolved in toluene $d_8$  at 50 °C for 18 h prior to the measurements. The assigned chemical shifts were: a) –COOCH<sub>3</sub>- (methylene protons near the carboxyl group,  $\delta = 1.8$  ppm), b) -CH- (methylene protons near the carboxyl group,  $\delta = 5.0$  ppm), and c) -CH<sub>2</sub>- (linear methylene protons,  $\delta = 1.3 - 1.6$  ppm) (see **Supplementary Information Figure S1**).

The <sup>1</sup>H-NMR data were used for calculation of the theoretical average segment length of PE sequences using the formula  $n_0 = 1 + 2F_e/F_v$ , where  $n_0$  is the segment length,  $F_e$  the ethylene mole fraction, and  $F_v$  the VA mole fraction.<sup>17</sup>

## 2.4. Swelling experiments

The gel content (*G*) was determined by gravimetric relation of the non-extracted reaction product to the purified polymer network. The purification procedure consisted of extraction with toluene at 50 °C for 24 h, removing all un-reacted fractions and drying the samples at 50 °C under vacuum until constant weight was reached (**Equation 2**). cPEVAs purified by extraction were used for determination of equilibrium swelling Q in toluene (**Equation 3**):

$$G = \frac{m_{extracted}}{m_{non-extracted}} \cdot 100 \tag{2}$$

$$Q = \left[1 + \frac{\rho_{polymer}}{\rho_{solvent}} \left(\frac{m_{swollen}}{m_{dried}} - 1\right)\right] \cdot 100 \tag{3}$$

Here  $m_{sw}$  and  $m_d$  represent the swollen and dry weights of the networks,  $\rho_{polymer}$  and  $\rho_{solvent}$  are the specific densities of the network and solvent respectively.

#### 2.5. Differential scanning calorimetry (DSC)

DSC measurements were performed on a DSC 204 Phoenix (NETZSCH, Selb, Germany) applying a heating-coolingheating cycle at heating and cooling rates of 10 K·min<sup>-1</sup> between -100 and 150 °C. The melting temperatures of cPEVAs were obtained from the second heating run. Furthermore, the melting enthalpy related weight crystallinity  $(w_c)$  of cPEVAs was calculated from DSC endothermic curves obtained from second heating according to **Equation 4**.

$$w_c = \frac{\Delta H_m}{\Delta H^{100}} \cdot 100 \tag{4}$$

Here  $\Delta H_{\rm m}$  is the melting enthalpy, representing the area of the melting peak, and  $\Delta H_m^{100}$  is the specific melting enthalpy for a 100% crystalline PE segment (287.3 J·g<sup>-1</sup>).<sup>18</sup>

#### 2.6. Annealing experiments

For annealing the copolymer networks, samples were placed in the thermo-chamber of the tensile tester and were heated to 90 °C and then cooled towards 20 °C in steps of 10 °C at a rate of 5 °C  $\cdot$ min<sup>-1</sup>. The samples were kept for 2 h under isothermal conditions after each 10 °C cooling step at this particular

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temperature. Annealed specimens were analyzed using the first DSC heating run at 10 K  $\cdot$  min<sup>-1</sup> between -20 and 120 °C.

#### 2.7. Tensile tests

Tensile tests were performed on a Z1.0 (Zwick-Roell, Ulm, Germany) equipped with a thermo chamber and a temperature controller (Eurotherm e2408, Limburg, Germany) using standard test specimen (ISO 527-2/1BB) at a strain rate of 5 mm·min<sup>-1</sup>. Stress-strain curves were recorded at ambient temperature and at  $T_{\rm high}$  (100 °C for cPEVA20 and at 80 °C for cPEVA31). A pre-force of 50 mN was applied prior data recording. Young's modulus (*E*), elongation at break ( $\epsilon_{\rm b}$ ) and tensile strength ( $\sigma_{\rm b}$ ) were determined. Additionally, the obtained stress-strain data at  $T_{\rm high}$  were analyzed by Mooney-Rivlin equations for calculation of the crosslink density (v<sub>c</sub>) (**Equation 5** and 6) of cPEVAs.<sup>19, 20</sup>

$$\frac{\sigma_n}{\lambda - \lambda^{-2}} = 2C_1 + \frac{2C_2}{\lambda}$$
(5)  
$$v_c = \frac{2C_1}{RT}$$
(6)

Where  $\sigma_n$  is the tensile stress,  $\lambda$  is the strain rate,  $2C_1$  and  $2C_2$  are the Mooney-Rivlin constants, R is the gas constant (8.314 J·K<sup>-1</sup>·mol<sup>-1</sup>), and T is the absolute temperature.

#### 2.8. Cyclic, thermomechanical tensile tests

Testing machine and specimen dimensions were the same as described for tensile tests. Each test cycle consisted of a temperature-memory creation procedure (TMCP), where the temporary shape was created at  $T_{deform}$ , and a recovery module under stress-free conditions (see **Supplementary Information Figure S3a**). The first cycle was used as a preconditioning cycle to erase the thermomechanical history of the samples.

*TMCP-module*: The specimen was cooled from  $T_{high}$  to  $T_{deform}$  and deformed to an elongation  $\varepsilon_m = 150\%$ , where the strain was kept constant for 10 minutes to allow relaxation. Then the sample was cooled at 5 K·min<sup>-1</sup> to  $T_{low} = 0$  °C and equilibrated for 10 min under strain controlled conditions. Finally, the stress was removed and the elongation of the sample in the temporary shape  $\varepsilon_u$  was determined. The deformation temperatures ( $T_{deform}$ s) in subsequent cycles and were 90, 65, 40, 25, and 10 °C for cPEVA20 series and 70, 55, 40 25, and 10 °C for cPEVA31 series.

*Recovery module*: The recovery of the original shape was induced by heating the programmed sample to  $T_{\text{high}}$  with a heating rate of 2 K·min<sup>-1</sup> under stress-free conditions. After the completion of the recovery process  $\varepsilon_{p}$  was determined, as well as the switching temperature  $T_{\text{sw}}$ , which was obtained as inflection point in the strain-temperature recovery curve by help of first derivatives.

The extent, to which the applied deformation ( $\varepsilon_m$ ) could be fixed, was quantified by the shape fixity ratio  $R_f$ , which was calculated according to **Equation 7**. Similarly the ability of the material to recover its original shape was quantified by the shape recovery ratio  $R_r$  using **Equation 8**. **Supplementary Figure 3a** shows the schematic illustration of the TMCP and both recovery modules in a temperature–strain–stress 3D plot.

$$R_f(N) = \frac{\varepsilon_u(N)}{\varepsilon_m} \cdot 100 \tag{7}$$

$$R_r(N) = \frac{\varepsilon_u(N) - \varepsilon_p(N)}{\varepsilon_u(N) - \varepsilon_p(N-1)} \cdot 100 \quad (8)$$

#### 2.9. X-Ray scattering techniques

*Wide-angle X-ray Scattering*: WAXS measurements were performed on an X-ray diffraction system D8 Discover with a two-dimensional Hi-Star detector (105  $\mu$ m pixel size) from Bruker AXS (Karlruhe, Germany). The X-ray generator was operated at a voltage of 40 kV and a current of 40 mA on a copper anode. A graphite monochromator produced Cu-K<sub>a</sub> radiation (0.154 nm wavelength). A 3 pinhole collimator with an opening of 0.8 mm was used. The distance between sample and detector was 150 mm, calibrated with Corundum standard. *In situ* measurements during TMCP were performed using a custom-build stretching device, a heating gun, and a cooled nitrogen gas stream with 5 min exposure time per scattering pattern.

Integration of intensity vs scattering angle  $2\theta$  led to onedimensional curves for analysis. The peaks of the two phases (amorphous and crystalline) were fitted with Pearson VII functions. The crystallinity index ( $x_c$ ) was determined from the areas of crystalline and amorphous peaks using **Equation 9**.

$$x_c = \frac{A_{cryst}}{A_{cryst} + A_{amorph}} \cdot 100 \tag{9}$$

The average lateral crystal size  $(l_c)$  was calculated from the (110) reflection by the Scherrer method with  $k = 0.9.^{21}$  Integration of intensity versus azimuthal angle  $\chi$  data led into one-dimensional curves for analysis of the degree of crystal orientation.

Small-angle X-ray Scattering (SAXS): SAXS measurements were performed on a Nanostar diffractometer from Bruker AXS (Karlruhe, Germany) equipped with a two dimensional VANTEC-2000 detector (68 µm pixel size) using a monochromatic beam with a wavelength of 0.154 nm. The distance sample to detector was 1070 mm, the beam size 400 µm. In addition SAXS data with short exposure times were recorded at the µSpot beamline at BESSYII (Berlin, Germany) with a sample to detector distance of 810 mm and 0.15418 nm wavelength on a MAR-CCD detector (73.2 µm pixel size). Machine background weighted by the absorption factor was subtracted from the raw data. Invalid pixels (e.g. beam stop) were masked. The image was aligned, rotated, harmonized (assuming fiber-symmetry) and extrapolated towards high scattering vector  $\mathbf{s} = (s_1, s_2, s_3)$ . Thereafter, the data were projected on the fiber plane, multiplied by s<sup>2</sup> (Laplacian in real space), the background which occurred due to the non-ideal nature of the two-phase system was removed by spatial frequency filtering, and finally an interference function G(s)was obtained. From G(s) the chord distribution function CDF z(r) was calculated by Fourier transformation.<sup>22</sup> z(r) is the Laplacian of Vonk's multidimensional correlation function.<sup>23</sup> It visualizes size and arrangement of the nanodomains in the sample, e.g. long period, lamellae thickness and extension. The longitudinal long period (L) and the average crystal thickness  $d_{\rm c}$ were calculated from CDF analysis.<sup>24</sup>

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# 3. Results and discussion

## 3.1 Characterization of copolymer networks

Two series of crosslinked poly[ethylene-co-(vinyl acetate)] comprising two different vinyl acetate contents (VAC of 20 wt% and 31 wt%) and three different crosslink densities (achieved by crosslinking with dicumyl peroxide (DCP) weight contents of 0.5, 1, and 2 wt%), and thus providing various transition intervals and crystallinities, melting were synthesized. Samples were denoted as cPEVAxxDyy, where xx represents the vinyl acetate content (VAC) and yy the DCP wt% in the starting mixture. Gel contents with G > 85% were observed for all cPEVAs, when the DCP content was 1 and 2 wt% in the starting reaction mixture G > 90% was reached. The VAC of the copolymer networks was determined via thermogravimetric analysis (TGA), revealing a VAC of 20 wt% and 31 wt% for the cPEVA20 and the cPEVA31 series respectively (Table 1). Data for cPEVA20 series were adopted from reference.<sup>15</sup> The theoretical average segment length of polyethylene (PE) sequences (n<sub>0</sub>) was determined from the <sup>1</sup>H-NMR spectra (Supplementary Information Figure S1), here  $n_0 = 24$  and 13 PE repeating units (-CH<sub>2</sub>-CH<sub>2</sub>-) for the cPEVA20 and the cPEVA31 series were calculated respectively.

The equilibrium degree of swelling (*Q*) was found to decrease from 1510% to 630% with increasing DCP content in the starting mixture. The crosslink density, as determined by Mooney-Rivlin analysis (**Table 1**), increased from  $v_c = 70$ mol·m<sup>-3</sup> to 260 mol·m<sup>-3</sup> for cPEVA20 and from  $v_c = 80$  mol·m<sup>-3</sup> to 325 mol·m<sup>-3</sup> for cPEVA31 series with increasing DCP content, which was in good correlation with the obtained *Q* values. The Mooney-Rivlin constant 2*C*<sub>1</sub>, which is mainly related to the number of covalent netpoints in the networks, was found to increase with increasing DCP content in the starting reaction mixture. Similarly 2*C*<sub>2</sub>, representing the contribution of physical crosslinks like entanglements, increased with increasing DCP content.

Differential scanning calorimetry (DSC) analysis was employed to investigate thermal properties of the cPEVAs. The melting and crystallization peak temperatures of the copolymer networks obtained in DSC experiments decreased with increasing VA-content from  $T_{\rm m} = 81$  °C to 84 °C ( $T_{\rm c} = 53$  °C to 57 °C) for cPEVA20s towards  $T_{\rm m} = 65$  °C to 68 °C ( $T_{\rm c} = 36$  °C to 39 °C) for the cPEVA31 series (Table 2). Data for cPEVA20 series were adapted from reference.<sup>15</sup> At the same time the melting temperature interval  $(\Delta T_m)$  was found to decrease from  $\Delta T_{\rm m} \approx 95$  °C for cPEVA20s to  $\Delta T_{\rm m} \approx 80$  °C for cPEVA31s (Supplementary Information Figure S2), while the same trend was observed for the melting enthalpy  $(\Delta H_m)$  decreasing from  $\Delta H_{\rm m}$  around 67 to 70 J·g<sup>-1</sup> (cPEVA20s) to significantly lower values of 41 to 44 J·g<sup>-1</sup> for the copolymer networks with lower VAC. This observation can be attributed to the shorter PE average segment length of 13 repeating units in cPEVA31 samples resulting in the formation of smaller or thinner crystals, which melt at lower temperatures. Besides the substantial impact of the VAC on the thermal properties, the variation of the crosslinking density resulted only in minor changes of the thermal characteristics, where  $T_c$  and  $T_m$  slightly decreased with increasing crosslink density, while  $\Delta T_{\rm m}$  and  $\Delta H_{\rm m}$  remained almost unchanged.

The results of the tensile tests are summarized in Table 2. At ambient temperature the elastic modulus (E) was higher for the cPEVA20 series (~27 MPa) than for the cPEVA31 series (~11 MPa), which was attributed to additional physical netpoints (i.e. PE crystals) in the cPEVA20 series, which had a higher degree of crystallinity. Elongation at break  $(\varepsilon_b)$  at ambient temperature decreased from 700% to 635% for the cPEVA20 series and from 755% to 615% for the cPEVA31 series when crosslinking density increased. As the decrease in  $\varepsilon_{\rm b}$  was low, we concluded that the PE crystals as physical net points dominated the elastic properties. The corresponding stress at break ( $\sigma_{\rm b}$ ) was almost constant within a series, being ~16 MPa for cPEVA20s and ~14 MPa for cPEVA31s. At  $T_{high} > T_m$ , i.e. in the viscoelastic state, the mechanical properties were only influenced by the chemical crosslinks and the entanglements of the polymer chains. E increased from 0.5 to 1.2 MPa for cPEVA20s and from 0.6 to 1.5 MPa for cPEVA31s with increasing crosslink density. Also  $\varepsilon_{\rm b}$  was reduced with increasing crosslink density, decreasing from 740% to 190% for cPEVA20s and from 1010% to 200% for cPEVA31s. Here a good correlation to the results from the Mooney-Rivlin analysis was observed.

Table 1: Chemica	al compositio	on, gel conten	it, equilibriu	im swelling and	d degrees of crys	tallinity of o	cPEVAs		
Sample ID <sup>a</sup>	DCP [wt%]	VAC <sup>b</sup> [wt%]	G ° [%]	Q° [%]	x <sub>c</sub> <sup>d</sup> [%]	w <sub>c</sub> <sup>e</sup> [%]	2 <i>C</i> <sup>1</sup> <sup>f</sup> [MPa]	2C <sub>2</sub> <sup>f</sup> [MPa]	$\nu_{\rm c}^{\rm f}$ [mol·m <sup>-3</sup> ]
cPEVA20D05	0.5	$20\pm 2$	$85 \pm 1$	$1300\pm10$	$27.4\pm0.7$	23.8	$0.21\pm0.03$	$0.47\pm0.03$	$69 \pm 9$
cPEVA20D10	1	$20\pm 2$	$92 \pm 1$	$840\pm10$	$26.8\pm0.7$	23.3	$0.47\pm0.03$	$0.89\pm0.1$	$150 \pm 10$
cPEVA20D20	2	$20\pm 2$	$96 \pm 1$	$630\pm10$	$25.1\pm0.9$	24.4	$0.81\pm0.05$	$1.10\pm0.04$	$260 \pm 15$
cPEVA31D05	0.5	$31 \pm 2$	$88 \pm 1$	$1510\pm10$	$15.7 \pm 1.3$	15.6	$0.24\pm0.01$	$0.94\pm0.09$	81 ± 4
cPEVA31D10	1	$31 \pm 2$	$94 \pm 1$	$960 \pm 10$	$14.3\pm0.7$	15.3	$0.44\pm0.02$	$1.16\pm0.1$	$149\pm 6$
cPEVA31D20	2	31 ± 2	$96 \pm 1$	$640 \pm 10$	$14.1 \pm 2.2$	14.4	$0.96\pm0.04$	$1.42 \pm 0.11$	$326 \pm 13$

a) The first two-digit number in sample ID was given according to the experimental value of VA-contents in cPEVAs determined by TGA measurements and the last two-digit number was given according to the content of DCP in wt% in crosslinking reaction; b) VA-contents in cPEVAs determined by TGA measurements; c) Gel content *G* and degree of swelling *Q* of cPEVAs was determined in toluene at 50 °C; d) Crystallinity index as calculated from WAXS; e) Weight crystallinity as calculated from DSC measurements, f) Mooney–Rivlin constants  $2C_1$  and  $2C_2$  and crosslink density ( $v_c$ ) were obtained based on the results of tensile tests at  $T_{high} > T_m$  according to Mooney–Rivlin equations. Data of cPEVA20 series were adopted from reference <sup>15</sup>.

<b>Fable 2</b> : Thermal and mechanical properties of	of cPEVAs
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Sample ID	T à	an d	$\Delta H_m^{a}$ [J·g <sup>-1</sup> ]	Am	bient temperat	ure <sup>b</sup>	T <sub>high</sub> <sup>b</sup>			
	[°C]	[°C]		E [MPa]	$\sigma_{ m b}$ [MPa]	&ь [%]	E [MPa]	$\sigma_{ m b}$ [MPa]	<i>Е</i> ь [%]	
cPEVA20D05	84	57	68.3	$27 \pm 3$	$17 \pm 2$	$700\pm80$	$0.5\pm0.1$	$0.8\pm0.1$	$740\pm100$	
cPEVA20D10	83	56	67.1	$26 \pm 4$	$17 \pm 5$	$660 \pm 50$	$0.7\pm0.1$	$0.7\pm0.1$	$380\pm90$	
cPEVA20D20	81	53	70.1	$28 \pm 1$	$15 \pm 1$	$635\pm10$	$1.2 \pm 0.1$	$0.9\pm0.1$	$190\pm50$	
cPEVA31D05	68	39	45.0	$12 \pm 1$	$14 \pm 2$	$755 \pm 50$	$0.6 \pm 0.1$	$1.6 \pm 0.1$	$1010\pm50$	
cPEVA31D10	66	38	44.0	$11 \pm 1$	$16 \pm 5$	$700\pm60$	$1.0 \pm 0.1$	$1.3 \pm 0.1$	$515 \pm 30$	
cPEVA31D20	65	36	41.2	$11 \pm 1$	$14 \pm 3$	$615 \pm 10$	$1.5 \pm 0.1$	$1.1 \pm 0.2$	$200 \pm 50$	

a) Data determined by DSC: melting transition temperature ( $T_m$ ); crystallization temperature ( $T_c$ ) and overall melting enthalpy ( $\Delta H_m$ ); b) Young's modulus (*E*), elongation at break ( $\varepsilon_b$ ), and its corresponding stress ( $\sigma_b$ ) were determined by tensile tests at ambient temperature and at  $T_{high} = 100$  °C for cPEVA20s and at  $T_{high} = 80$  °C for cPEVA31s. Data of cPEVA20 series were adopted from reference<sup>15</sup>.

The overall crystallinity determined from wide-angle X-ray scattering  $(x_c)$  or DSC  $(w_c)$  experiments was similar, being around 25% for the cPEVA20s and about 15% for the cPEVA31 series (**Table 1**). This observation indicates that the amount of crystals was not affected by the introduced crosslinks.

The nanostructure of cPEVAs was analyzed by small- and wide-angle X-ray scattering (SAXS and WAXS) measurements at ambient temperature. Crystallinity index  $(x_c)$  and average lateral crystal extension  $(l_c)$  were determined from the (110) reflection of PE in the WAXS pattern, while the average long period (L) and the average lamella crystal thickness ( $d_c$ ) were obtained from SAXS data. The calculated results are listed in Table 3. All non-programmed samples exhibited isotropic Debye-Scherrer rings in WAXS and circular correlation rings in SAXS experiments, indicating that the crystalline domains are randomly arranged. The L and  $d_c$  were almost similar for both cPEVA20 series with values about  $L \approx 12$  nm and  $d_c \approx 6$  nm (c.f. **Table 3**). As L was found to be approximately two times  $d_c$ in cPEVAs, the crystallinity within a stack can be anticipated as  $\approx$  50%. Their structure might consist of stacks of alternating crystalline-amorphous PE lamellae, which are surrounded by a mixed amorphous PE-VA matrix comprising short PEsegments, unable to form crystals.

Based on the obtained average PE crystal thickness of 6 nm it can be assumed that the ordered PE nanostructure is related to PE segments with an average segment length of about 20 to 25 repeating units, which was in good correlation with the theoretical calculations from the NMR spectroscopy data for cPEVA20s. For the cPEVA31 series, with a calculated average segment length of 13 repeating units, one would expect an average crystal thickness around 3 nm, but in WAXS experiments we observed also a  $d_c \approx 6$  nm. This difference might be attributed to a non-statistical distribution of the VA moieties within the copolymer matrix and thus larger PE segment lengths than predicted by the theory.

As the deformation temperature  $T_{deform}$  was assumed to be the key parameter for creation of a TME in polymers, we further investigated the crystalline thickness as function of temperature exemplarily for cPEVA31D20 and cPEVA20D20. The non-deformed samples were heated in 10 K steps from 25 °C to 75 °C and SAXS patterns were recorded. In **Figure 1a** and **Table** 

**3** the resulting  $d_c$  vs temperature data are presented, showing a continuous increase of the crystal thickness with increasing temperature. The maximum  $d_c$ s were 8.5 nm for cPEVA20D20 at 75 °C and 7.5 nm for cPEVA31D20 at 63 °C, whereby the lower maximum  $d_c$  of cPEVA31D20 can be attributed to a lower PE-segment length.



**Figure 1: a)** Average lamellae thickness  $d_c$  determined by SAXS of non-deformed cPEVA20D05 (black squares) and cPEVA31D05 (half filled circles) during heating and theoretical prediction of the lamellae thickness (grey stars) from the peak maximum (P0 to P5) of graph b; b) Relative heat flow curves obtained in DSC experiments conducted after subsequent annealing at 90, 80, 70, 60, 50, 40, 30, and 20 °C for cPEVA20D05 (black) and cPEVA31D05 (gray); c) DSC curves of annealed cPEVA20 with different crosslinking density, cPEVA20D05 (black), cPEVA20D10 (grey) and cPEVA20D20 (light grey) and d) DSC thermogramms of cPEVA31D05 (black), cPEVA31D10 (grey) and cPEVA31D05 (black), cPEVA31D10 (grey) and cPEVA31D20 (light grey).

#### 3.2. Temperature-memory capability

The applied  $T_{deform}$ s for the TME experiments were chosen to span the whole melting temperature interval  $\Delta T_{\rm m}$  obtained in DSC experiments. Thus  $T_{deform}$ s for cPEVA20s ranged from 10 to 90 °C and for cPEVA31s deformation temperatures from 10 to 70 °C were utilized (for details see experimental section). The temperature-memory capability of cPEVAs was investigated by cyclic thermomechanical tensile tests (see scheme in Supplementary Information Figure S3a) and the obtained results are summarized in Supplementary Information Tables S1 and S2. The temporary shape in semicrystalline shape-memory polymers is fixed by crystallizable switching segments, which act as temporary physical netpoints. In a classical thermally-induced SME cycle the sample is deformed at  $T_{\text{high}} > T_{\text{m}}$ , where the switching segment is amorphous, and cooled to  $T_{low} < T_m$  allowing crystallization of the switching segment and thus the formation of temporary netpoints which retain the temporary shape. By reheating to  $T_{\text{high}}$  the temporary netpoints are disassembled by melting of the switching segment and the permanent shape is recovered.

All investigated cPEVAs exhibited excellent temperaturememory properties demonstrated by an almost linear correlation between the  $T_{deform}$  and the response temperature  $T_{sw}$ (Figure 2). The recorded stress-temperature-strain plots obtained under stress-free conditions are exemplarily displayed for cPEVA20D10 in Supplementary Figure 3b. The stress at  $\varepsilon_{\rm m}$  was increasing when  $T_{\rm deform}$  was decreased, which was attributed to the higher crystallinity of the sample. For equal  $T_{\text{deform}}$  the stress increased with increasing crosslink density, which was related to the additional covalent netpoints. High shape recovery ratios of  $R_r \ge 87\%$  were achieved for all copolymers independent from the applied  $T_{deform}$ %, indicating the high entropic elasticity of the polymer networks at  $T_{high}$ , reflecting the excellent stabilization of the permanent shape by the chemical crosslinks. In contrast, the shape fixity ratios were found to decrease with decreasing  $T_{deform}$  from  $R_f$  around 100% to  $R_f$  values of 50 to 60% for  $T_{deform} = 10$  °C (c.f. Figure 2).  $R_f$ values above 100% were attributed to crystallization induced elongation upon cooling at constant stress as previously reported.25

#### 3.3. Annealing experiments

Annealing experiments were conducted on cPEVAs to investigate the contribution of the isothermal crystallization to the crystal structure. For doing so, non-deformed specimens were annealed stepwise in the thermo-chamber of the tensile tester and were analyzed by a first DSC heating run. The resulting thermograms are shown in **Figure 1**.

As mentioned before the broad  $\Delta T_{\rm m}$  of cPEVAs can be treated as an infinite number of sharp single melting temperatures, whereby each individual transition would be controlled by a crystal population of a distinct thickness. Therefore, the broad  $\Delta T_{\rm m}$  in cPEVAs can be assumed as broad distribution of crystal lamellae thicknesses, which are related to the PE-segment length distribution. Here, the Thomson-Gibbs equation (**Equation 10**) describes the relation between crystal thickness  $d_{\rm c}$  and its melting temperature  $T_{\rm m}$ .<sup>26, 27</sup> Where  $T_{\rm m}^0$  is the melting temperature of an infinitely large PE-crystal (414.4 K)<sup>28</sup> and  $\gamma_{\rm e}$ is the top and bottom surface energy of the crystalline lamellae (33 erg·cm<sup>-2</sup>).

$$T_m = T_m^0 - \frac{2\gamma_e T_m^0}{d_c \Delta H_m} \qquad (10)$$

A stepwise annealing protocol, where the samples were first heated to 90 °C and then cooled to 20 °C in subsequent steps of 10 K, while allowing isothermal crystallization at each temperature, was applied to separate different crystal populations within  $\Delta T_{\rm m}$  from each other (see **Experimental** section). The annealed samples were analyzed by DSC heating experiments. In Figure 1b the DSC curves obtained in the first heating run of cPEVA20d05 and cPEVA31D05 are shown. Both cPEVA series exhibited multiple distinct melting peaks (P0 to P4/P5) corresponding to the applied individual annealing temperatures, which was similar to the behavior reported for annealed non-crosslinked PEVA<sup>29, 30</sup> comprising multiple  $T_{\rm m}$ s. The  $T_{\rm m}$ s could be related to the corresponding theoretical lamellae thickness (Figure 1a) representing the contribution of the isothermal crystallization step during temperature-memory creation procedure (TMCP). Theoretical thickness increased from 3.9 nm for  $T_{\rm m} = 15$  °C to 8.3 nm for  $T_{\rm m} = 80$  °C, indicating the formation of thick and thermally stable crystals when increased isothermal crystallization temperature was applied. The theoretical  $d_c$  values were smaller than the  $d_c$ determined from SAXS, especially at low temperatures, because SAXS showed the average lamellae thickness with contributions from the entire crystal population. The influence of the annealing treatment on cPEVAs could be interpreted as follows: The peak P5 at 80 °C could only be observed for cPEVA20s comprising a higher PE segment length. A pronounced influence of the crosslink density on the peak area of the P4 and P5 became only apparent for cPEVA20 samples, while for cPEVA31 networks were not affected by the variation of the crosslink density (Figure 1c-d). Here the peak area of P5 was found to decrease with rising crosslink density, which can be attributed to a reduction of PE-segment length leading to the formation of thinner crystal lamellae resulting in an increase in the peak area of P4. In contrast the peaks P0, P1, P2 and P4 were not affected by increasing the crosslink density (Figure 1c). Summarizing, higher  $T_{deform}$ , which correspond to isothermal crystallization at higher temperatures, would favor the creation of thick crystalline lamellae. In contrast lower  $T_{\text{deform}}$  would promote thin crystals. By cooling to  $T_{\text{low}}$ additional crystallization occurs in both cases but the resulting average crystal thickness would be increased when a higher  $T_{deform}$  was applied. In this way higher or lower  $T_{deform}$  will contribute to the TME.

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**Figure 2:** Temperature-memory effect of cPEVAs. Response temperatures  $T_{sw}$  (open symbols) and shape fixity ratio  $R_f$  (solid symbols) depending on  $T_{deform}$  determined by cyclic thermomechanical tensile tests of cPEVA20D05 (triangle up), cPEVA20D10 (circle), cPEVA20D20 (square), cPEVA31D05 (triangle down), cPEVA31D10 (star), and cPEVA31D20 (diamond) as function of the deformation temperature  $T_{deform}$ . The dotted line denotes the linear correlation  $T_{sw} = T_{deform}$  representing an ideal temperature-memory effect.

# 3.4 Nanostructural investigations by SAXS/WAXS – Mechanistic aspects of TME $\,$

In addition to the contribution of the isothermal crystallization at  $T_{deform}$ , the deformation step was expected to have significant influence on the crystal structure responsible for memorizing  $T_{\text{deform}}$ . Thus the crystalline PE nanostructures were analyzed before and after deformation at  $T_{deform}$  as well as after completion of the TMCP at  $T_{\text{low}}$ . In this way the contributions of the deformation step and the cooling step on the crystallizable controlling units responsible for the TME should by elucidated. The obtained WAXS patterns as well as the azimuthal profiles are shown in Figure 3 for cPEVA20D20 and in Supplementary Information Figure 4 for cPEVA31D20, while the respective SAXS patterns are displayed in Figure 4. The analyzed structural parameters such as the degree of crystallinity  $(x_c)$ , the average lateral crystal size  $(l_c)$ , the average crystal thickness  $(d_c)$  and the longitudinal long period (L)calculated from SAXS and WAXS diffraction patterns are listed in Table 3. It has to be pointed out that at the highest  $T_{\text{deforms}}$  (i.e. 90 °C for cPEVA20D20 and 70 °C for cPEVA31D20) the specimens are amorphous as all crystals are in the molten state and in this way the TMCP and the recovery could be considered as a classical shape-memory experiment. WAXS patterns (Figure 3a-h and The illustrated Supplementary Information Figure 4a-h) represent the

structures at ambient temperature before deformation, when deformed to  $\varepsilon_{\rm m} = 150\%$  at different  $T_{\rm deforms}$  (cPEVA20D20: 90, 65, 40 and 25 °C; cPEVA31D20: 70, 55, 40 and 25 °C) and at  $T_{\rm low} = 10$  °C after completion of TMCP. For all samples the main (hk0) reflections, i.e. (110) and (200) were found on the equatorial part, reflecting that the orientation of the polymer chains is parallel to the strain direction. The meridional part of the pattern did not exhibit any reflections. The overall degree of crystallinity of both programmed copolymer samples was found to be similar to the original non-programmed sample with  $x_c$  in the range of 27 to 30 % for cPEVA20D20 and  $x_c$  values from 13 to 16% for cPEVA31D20. With increasing  $T_{deform} x_c$  was found to systematically decrease to  $x_c = 9 \%$  (cPEVA20D20 at 65 °C) or 7% (cPEVA31D20 at 55 °C) while almost no difference between elongated and non-elongated test specimen could be observed, which suggested that strain-induced crystallization processes are not involved during TMCP.

Different azimuthal profiles related to the (110) peak were obtained for copolymers with different VAC equivalent to a different PE segment length. Here cPEVA20D20 (**Figure 3**) showed a lower degree of orientation compared to cPEVA31D20 (**Supplementary Figure 4**), which exhibited sharper peak profiles ( $\chi$  direction), which were attributed to a higher mobility of smaller crystals and therefore a higher orientation after application of the deformation. A broadening of the azimuthal profiles in  $\chi$  direction was observed with increasing  $T_{deform}$ . Interestingly at  $T_{deform} = 90$  °C a somehow bimodal azimuthal profile was observed, which might be attributed to a structure of tilted lamellae.<sup>31</sup>

The average lateral crystal size  $(l_c)$  determined from the (110) reflection of the programmed cPEVA20D20 samples at ambient temperature was found to increase from  $l_c = 5.3$  nm to  $l_c = 10.4$  nm with increasing  $T_{deform}$  from 25 °C to 90 °C. The samples programmed at higher T<sub>deform</sub>s of 90 °C and 65 °C exhibited a similar lc around 10 nm like the original nonprogrammed sample. This leads to the conclusion that at high  $T_{\text{deform}}$ , where only a few or almost no PE crystals are present after deformation, the crystal growth during cooling to  $T_{\rm low}$  is not hindered and larger crystals can be formed. Significantly lower  $l_c$  values in the range of 5 to 7 nm were found at lower deformation temperatures. This might be explained by the disruption of existing PE crystals into smaller microfibril-like structures during the deformation at lower  $T_{deform}$ . The new crystalline structures formed during further cooling to  $T_{low}$  are hindered in extension by the small structures generated during deformation, which resulted in an overall reduction of the lateral extension of the crystalline domains. Similar findings have been reported for a cold drawn polyethylene-octene copolymer.<sup>32</sup>

In contrast for cPEVA31D20 having a lower PE segment length the  $l_c$ -values remained almost constant around 6 to 7 nm independent from the applied  $T_{deform}$ , which corresponds to the  $l_c$  of the non-programmed sample.

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Table 3:	Crystalline dom	ain sizes and dis	stances during T	MCP as dete	ermined by	/ SAXS/WAXS	experiments							
							cPEVA20D2	20						
		$\varepsilon = 0\%$					$\varepsilon_{\rm m} = 150\%$	,				$\varepsilon_{\rm u}$ at $T_{\rm low}^{\rm e}$		
T <sub>deform</sub> [°C]	L <sup>a</sup> [nm]	<i>l</i> <sup>c</sup> <sup>b</sup> [nm]	$d_c^{c}$ [nm]	$x_c^d$ [%]	T <sub>deform</sub> [°C]	L <sup>a</sup> [nm]	l <sub>c</sub> <sup>b</sup> [nm]	$d_c^{c}$ [nm]	$x_{c}^{d}$ [%]	T <sub>deform</sub> [°C]	L <sup>a</sup> [nm]	<i>l</i> <sup>c</sup> <sup>b</sup> [nm]	$d_c^{\ c}$ [nm]	x <sub>c</sub> <sup>d</sup> [%]
25	$11.4\pm0.5$	$10.4\pm0.5$	$6.0\pm0.5$	$27 \pm 2$	25	$12.2\pm0.5$	$4.9\pm0.5$	$5.9\pm0.5$	$28 \pm 2$	25 <sup>f</sup>	$12.6\pm0.5$	$5.3\pm0.5$	$5.9\pm0.5$	30 ± 2
40	$12.6\pm0.5$	$9.8\pm0.5$	$6.5 \pm 0.5$	$20 \pm 2$	40	$13.2 \pm 0.5$	$9.9\pm0.5$	$5.5 \pm 0.5$	$20 \pm 2$	$40^{ m f}$	$11.4\pm0.5$	$6.6 \pm 0.5$	$4.3\pm0.5$	$28 \pm 2$
65	$14.9\pm0.5$	$9.0\pm0.5$	$7.7 \pm 0.5$	$11 \pm 2$	65	$18.9\pm0.5$	$9.6\pm0.5$	$9.0 \pm 0.5$	$9 \pm 2$	$65^{\rm f}$	$14.3\pm0.5$	$10.2 \pm 0.5$	$6.1 \pm 0.5$	$28 \pm 2$
										$90^{\rm f}$	$12.5\pm0.5$	$10.4\pm0.5$	$5.4\pm0.5$	$29 \pm 2$
							cPEVA31D2	20						
		$\varepsilon = 0\%$					$\mathcal{E}_{\rm m} = 150\%$	1				$\mathcal{E}_{u}$ at $T_{low}^{e}$		
$T_{\rm deform}$	La	$l_c^{b}$	$d_c$ °	$x_{c}^{d}$	$T_{\rm deform}$	La	l <sub>c</sub> <sup>b</sup>	$d_c$ °	$x_{c}^{d}$	$T_{\rm deform}$	La	$l_c^{b}$	$d_c^{\ c}$	$x_{c}^{d}$
[°C]	[nm]	[nm]	[nm]	[%]	[°C]	[nm]	[nm]	[nm]	[%]	[°C]	[nm]	[nm]	[nm]	[%]
25	$11.5\pm0.5$	$6.1 \pm 0.5$	$5.9 \pm 0.5$	$14 \pm 2$	25	$11.5\pm0.5$	$5.2\pm0.5$	$4.5\pm0.5$	$15 \pm 2$	25 <sup>f</sup>	$11.0\pm0.5$	$6.5\pm0.5$	$4.4 \pm 0.5$	$16 \pm 2$
40	$12.4\pm0.5$	$5.2 \pm 0.5$	$6.4\pm0.5$	$12 \pm 2$	40	$14.9\pm0.5$	$5.4\pm0.5$	$7.2\pm0.5$	$11 \pm 2$	$40^{\rm f}$	$13.1\pm0.5$	$6.0 \pm 0.5$	$5.4\pm0.5$	$14 \pm 2$
55	$14.1\pm0.5$	$4.4\pm0.5$	$7.0\pm0.5$	$9 \pm 2$	55	$18.4\pm0.5$	$5.4\pm0.5$	$8.2\pm0.5$	$7 \pm 2$	$55^{\rm f}$	$13.1\pm0.5$	$6.6\pm0.5$	$6.0\pm0.5$	$14 \pm 2$
										$70^{ m f}$	$12.5\pm0.5$	$7.2 \pm 0.5$	$4.8\pm0.5$	$13 \pm 2$

a) Long period determined from CDF; b) Average lateral crystal extension determined from (110) reflection; c) Average crystal thickness determined from CDF; d) Crystallinity determined from WAXS; e) Measurements performed at  $T_{low} = 10$  °C on samples which were deformed at  $T_{deform}$  indicated in f) and cooled to  $T_{low} = 10$  °C to fix the temporary shape ( $\varepsilon_u$ ).

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**Figure 3:** Equatorial section of the wide-angle X-ray scattering patterns of cPEVA20D20 (**a-h**) during TMCP. Left:  $T_{low} = 10$  °C and  $\varepsilon = 0\%$ ; **a-d**) at  $T_{deform}$  (as indicated) and  $\varepsilon_m = 150\%$ ; **e-h**) at  $T_{low} = 10$  °C and  $\varepsilon_u$  (temporary shape); **i** and **j**: Azimuthal profiles of the (110) diffraction of cPEVA20D20 at the different situations **a-h**. **i**) non-deformed (black), **a** (red), **b** (orange), **c** (dark cyan) and **d** (blue); **j**) non-deformed (black), **e** (red), **f** (orange), **g** (dark cyan) and **h** (blue).

In addition to the crystallinity and the lateral crystal size data, the in situ SAXS experiments provide information about the longitudinal long period L, including one amorphous and one crystalline layer, and the average thickness of the crystalline lamella  $d_c$ . In Figure 4 various SAXS patterns obtained for the original non-deformed cPEVA20D20 and cPEVA31D20 sample at ambient temperature (Figure 4I and II), at different  $T_{\text{deform}}$  with  $\varepsilon_{\text{m}} = 150\%$  (Figure 4a-d and 4i-l) and after completion of TMCP at  $T_{\text{low}}$  (Figure 4e-h and 4m-p) are shown. Both non-programmed samples cPEVA20D20 and cPEVA31D20 exhibited an isotropic structure with a long period around L = 11.5 nm and a crystalline thickness of  $d_c \approx$ 6.0 nm. At the desired deformation temperatures without elongating the sample the isotropic structure remained and the values for L and  $d_c$  increased with raising temperature, while at  $T_{\text{deform}} = 90 \,^{\circ}\text{C}$  (cPEVA20D20) and at  $T_{\text{deform}} = 70 \,^{\circ}\text{C}$ (cPEVA31D20) no discrete scattering pattern could be observed.

In the following first the further SAXS data obtained for cPEVA20D20 will be discussed. Also after deformation to  $\varepsilon_m = 150\%$  at  $T_{deform} = 90$  °C no discrete scattering pattern could be observed, while after cooling to  $T_{low}$  and releasing the stress in the temporary shape a four point pattern was obtained (**Figure 4e**). This pattern exhibits a typical correlation in the  $s_3$  direction of elongation, which can be attributed to a structure of tilted lamellae. When lower  $T_{deform}$ s of 65, 40 and 25 °C were applied the SAXS patterns achieved during deformation at  $T_{deform}$  and after completion of TMCP differed strongly from those obtained at 90 °C. Here a relatively broad lateral distribution of the maxima was generated with patterns having a distinct streak parallel to the equator ( $s_{1,2}$ ), which indicate a microfibrillar or cylinder-like structure.<sup>33</sup> Such a transformation from the point

reflections in the non-deformed state to a microfibrillar or cylinder-like structure can be attributed to inter- and intralamellar slipping processes and crystallite fragmentation during deformation at low  $T_{deform}s$ .<sup>34</sup>

The SAXS pattern obtained for cPEVA31D20, with exception of  $T_{deform} = 70$  °C, where the sample was completely amorphous, had a four-point character similar to cPEVA20D20 (**Figure 4i-p**), whereby these pattern appear more layer-like, which can be attributed to a pronounced cylinder-like structure of the crystalline PE domains.

Programming at  $T_{deform} = 90$  °C, where the copolymer network is completely amorphous, resulted in similar values for the long period (L = 12.5 nm) and the crystalline thickness ( $d_c = 5.4$  nm) as in the original state. Here, the cooling to  $T_{low} = 10$  °C generated a subsequent increasing population of crystalline domains, starting with the formation of thicker crystals at higher temperatures and ending with thinner crystals at lower temperatures, which are placed in between the previously formed ones. A similar trend was observed when the sample was deformed at  $T_{deform} = 65$  °C, where a crystalline fraction of  $x_c = 9\%$  remained and a L of 18.9 nm and a  $d_c$  of 9.0 nm represented the existing PE crystals. After cooling to  $T_{low}$  the long period as well as the average crystal thickness decreased to L = 14.3 nm and  $d_c$  of 6.1 nm, respectively.

After deformation at lower  $T_{deform}$ s of 40 °C and 25 °C long periods of L = 13.2 nm and L = 12.2 were obtained, which are slightly higher compared to the values observed for the nondeformed samples at the same  $T_{deform}$ s, whereas the crystal thickness was reduced to values of 5.5 to 5.9 nm. After cooling from  $T_{deform} = 40$  °C to  $T_{low}$  both the longitudinal long period and the crystal thickness were found to be slightly reduced to L= 11.4 nm and  $d_c = 4.3$  nm. Together with the increase in  $x_c$  and the decrease in  $l_c$  obtained from WAXS experiments this indicated that less laterally extended crystals are intersected between the existing crystalline domains. When programmed at 25 °C L and  $d_c$  were not affected during cooling to  $T_{low} = 10$  °C, while  $x_c$  increased substantially, which indicated that a small fraction of identical crystalline structures were inserted in between existing crystals upon cooling.

During programming at lower  $T_{deforms}$  the predominant process was the structural rearrangement of existing PE crystallites, which was dictated by the deformation.

A similar trend for the changes in the crystalline nanostructure was observed for cPEVA31D20 when programmed at higher  $T_{\text{deforms}}$  of 70, 55 or lower  $T_{\text{deforms}}$  of 40 and 25 °C, but less pronounced (see **Table 3**).

Based on the observations from WAXS/SAXS and annealing experiments two different contributions to the nanostructural changes in cPEVA responsible for the memorization of the deformation temperature depending on the choice of  $T_{deform}$ were proposed, which are schematically displayed in Figure 5. Starting from the non-deformed sample with a broad distribution of crystal thickness as reflected by its broad melting transition (DSC results), heating to higher T<sub>deform</sub> (Figure 5a-e) results in a few remaining thicker crystals, which are thermally stable at these temperatures, as confirmed by SAXS measurements. Annealing at this  $T_{deform}$  increased the thermally stable crystal fraction. When the deformation is applied these crystals are tilted and oriented, whereby some crystal thickening might occur. By cooling to  $T_{low}$ , oriented PE chains crystallize and finally relatively thick crystals are generated. The now established nanostructure of the temporary shape has a broader crystal thickness distribution compared to

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**Figure 4:** SAXS patterns of cPEVA20D20 (I and a-h) and cPEVA31D20 (II and i-p) during TMCP. I and II:  $T_{low} = 10$  °C and  $\varepsilon = 0\%$ ; a-d and i-I:  $T_{deform}$  (indicated) and  $\varepsilon_m = 150\%$ ; e-h and m-p:  $T_{low} = 10$  °C and  $\varepsilon_u$  (temporary shape).

At lower  $T_{deform}$ s (**Figure 5a-e'**) the overall starting nanostructure is almost maintained during the initial heating step as only a few thinner crystals are melting. Annealing at low temperatures would increase the thermally less stable crystal fraction. When the deformation is applied, rearrangement of the nanostructure takes place in such way that thicker and larger crystals were disrupted into smaller and thinner (and less lateral extended) ones, which are oriented. By cooling to  $T_{low} = 10$  °C only a few thinner crystals can grow as the space for crystallization is already occupied. Finally, the temporary shape comprises a nanostructure with thin and small oriented crystals, which melt at low temperatures during reheating and in this way the sample remembers the lower  $T_{deform}$  applied during programming.



**Figure 5:** Schematic illustration of the TME mechanism. Black structures represent crystalline domains of different size. The upper pathway (**b** to **e**) shows the mechanism for higher  $T_{deform,high}$  and the lower pathway (**b'** to **e'**) for lower  $T_{deform,low}$ . Furthermore a sketch of the average crystal thickness ( $d_c$ ), the average lateral extension ( $I_c$ ), and the long period (L) is presented (**f**).

#### 4. Conclusions

Series of cPEVAs with two different VACs comprising a broad melting temperature range and three different crosslink densities were prepared, which exhibited a pronounced temperature-memory effect. The contribution of the temperature applied during TMCP was explored by annealing experiments, which revealed preferential formation of thick crystals when higher temperatures were applied. In situ X-ray investigations were employed to investigate the nanostructural changes of the crystallizable PE controlling units during functionalization and activation of the temperature-memory effect, especially regarding the contribution of the deformation step. It could be shown that two different mechanisms are responsible for memorizing higher or lower  $T_{deform}$ . At higher  $T_{deform}$ s predominantly newly formed large crystal structures were established during cooling to  $T_{low}$ , which are controlling the TME. In contrast, at lower  $T_{deform}$ s, which is comparable to a cold drawing scenario, the TME was determined by the rearrangement of existing crystalline structures during deformation, whereby large crystalline structures are disrupted into smaller ones related to low response temperatures. The observed nanostructural changes during TMCP were found to be almost independent from the composition of the investigated cPEVAs. The mechanism of the TME in semi-crystalline cPEVAs, with contributions from thermal treatment and mechanical deformation, might be extended to other TMPs comprising crystallizable controlling units and in this way enable a knowledge based design.

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