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High-performance \( \text{SrNb}_{0.1}\text{Co}_{0.9-x}\text{Fe}_x\text{O}_{3-\delta} \) perovskite cathodes for low temperature solid oxide fuel cells

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Received (in XXX, XXX) Xth XXXXXXXXX 20XX, Accepted Xth XXXXXXXXX 20XX
DOI: 10.1039/b000000x

Chemical to electrical energy conversion using solid oxide fuel cell (SOFC) becomes more practical as the operating temperature is lowered to 600 °C and below. Given the thermally activated nature of the oxygen reduction reaction (ORR) at the cathode side, development of cathode catalyst with very low polarisation resistance is essential. Here, we showed that partial substitution of Co within \( \text{SrNb}_{0.1}\text{Co}_{0.9}\text{O}_{3-\delta} \) by Fe (up to 0.5) triggers the formation of oxygen non-stoichiometry while preserving the primitive cubic lattice, thus substantially enhancing the ORR performance below 600 °C (relative to the parent compound). Close correlation between the oxygen non-stoichiometry and ORR activity trends was implied to some extent. \( \text{SrNb}_{0.1}\text{Co}_{0.9-x}\text{Fe}_x\text{O}_{3-\delta} \) (SNFC0.2) cathode exhibits a very low area specific resistance value of 0.052 \( \Omega \text{ cm}^2 \) at 600 °C which translates to superior fuel cell performance e.g. peak power density of 1587 mW cm\(^{-2} \) at 600 °C. Moreover, the synergistic relationship between ORR activity, thermal expansion coefficient and enhanced CO\(_2\) resistance warrants SNFC cathode significance. The last attribute is envisioned as a dominant factor for applications using alternative fuels (e.g. CO which normally contains CO\(_2\)) and in a portable single chamber SOFC.

1. Introduction

Of all available technologies to convert chemical-based energy resources to electricity, fuel cell is the most attractive one in terms of conversion efficiency (it can overcome the combustion limitation e.g. Carnot cycle) and fuel flexibility. This is particularly true for solid oxide fuel cells (SOFCs). In this device, \( \text{O}_2 \) reacts with electron (in the cathode), to produce oxygen ions which are then transported (through the electrolyte), and react with fuel (in the anode) to produce electrons at a distinct potential (from the electron at the cathode side).\(^{1,2} \) The use of oxygen ionic conductors as an electrolyte allows other than \( \text{H}_2 \) fuels such as hydrocarbon and \( \text{CO} \). Low temperature SOFC (LT-SOFC) concept (with operating temperature of 400-600 °C) has currently been brought forward to surpass (SOFC’s) current economic and technical barriers such as high system costs and degradation pace in conjunction with slow start-up and shut-down cycle.\(^{4,5} \) At these temperatures nonetheless, cathode kinetics becomes a major limiting step to obtain good performance.\(^{6,9} \)

The effective oxygen reduction reaction (ORR) area in the cathode can be enlarged by adopting mixed ionic-electronic conducting (MIEC) perovskites instead of conventional electronic conductor perovskites (e.g. \( \text{La}_{1-x}\text{Sr}_{x}\text{MnO}_3 \)); therefore bringing down the operating temperature (for conventional SOFC) of 800-1000 °C to 650-800 °C, the latter of which is known as intermediate temperature SOFCs.\(^{7,12} \) \( \text{SrCoO}_3 \) (SC)-based perovskites exemplifies a MIEC cathode benchmark, made well-known, when in 2004, Shao and Haile demonstrated working SOFC device utilising \( \text{Ba}_{0.6}\text{Sr}_{0.4}\text{Co}_0.5\text{Fe}_{0.5}\text{O}_{2.5} \) (BSCF) cathode with peak power density of ~1000 mW cm\(^{-2} \) at 600 °C.\(^{12} \) Later on, a comparable performance was also reported using \( \text{SrSc}_0.2\text{Co}_0.8\text{O}_{3-\delta} \) (SSC) and \( \text{SrNb}_{0.1}\text{Co}_{0.9}\text{O}_{3-\delta} \) (SNC) cathodes.\(^{14,15} \)

If their susceptibility to CO\(_2\) and high thermal expansion coefficients (TEC) can be addressed, it would be practical to incorporate these SC-based cathodes to realise LT-SOFC.\(^{16-18} \) CO\(_2\) resistance would specially be crucial for application in single-chamber SOFC.\(^{7,19,20} \)

Here we report new cathodes within a perovskite framework of \( \text{SrNb}_{0.1}\text{Co}_{0.9-x}\text{Fe}_x\text{O}_{3-\delta} \) (SNC, 0.1 ≤\( x \) ≤0.5). These cathodes show excellent ORR activity at low temperatures and more importantly, low TEC values and CO\(_2\) resistance. SNC0.2, for example, shows the lowest area specific resistance value (which is inversely proportional to the ORR activity) of only 0.301 and 0.111 \( \Omega \text{ cm}^2 \) at 500 and 550 °C, respectively. Of significant interest is the moderate thermal activation energy (\( E_a \)) value for ASRs of SNC0.2 (i.e. 94 kJ mol\(^{-1} \)), since high activation energy value implies rapid performance deterioration with decreasing temperature. Accordingly, high peak power densities of 610 and 1587 mW cm\(^{-2} \) were achieved on an anode-supported 20 μm \( \text{Sm}_{0.2}\text{Co}_0.8\text{O}_{1.9} \) (SDC) single fuel cell at 500 and 600 °C.

2. Experimental Section

Synthesis of powders: \( \text{SrNb}_{0.1}\text{Co}_{0.9}\text{Fe}_x\text{O}_{3-\delta} \) (\( x=0, 0.1, 0.2, 0.3 \) and 0.5) powders were synthesised using a solid-state reaction route. Stoichiometric amounts of \( \text{SrCO}_3 \), \( \text{Nb}_2\text{O}_5 \), \( \text{Co}_3\text{O}_4 \) and \( \text{Fe}_2\text{O}_3 \) (all analytical grade, Sinopharm Chemical Reagent Co. Ltd.) were weighed, mixed and milled in a planetary mill (Fritsch, Pulverisette 6) using acetone as a solvent media at 400 rpm for 1 h. After drying, the powders mixture was calcined at 1200 °C in air for 10 h. The milling and calcination were repeated again to obtain single phase \( \text{SrNb}_{0.1}\text{Co}_{0.9-x}\text{Fe}_x\text{O}_{3-\delta} \).

Fabrication of the symmetrical cells and the single fuel cell:

Symmetrical cells with electrode|SDC|electrode configuration were fabricated for electrochemical impedance spectroscopy (EIS) measurements. Dense SDC pellets (0.5 g) of 12 mm in diameter and 0.8 mm thickness were prepared by dry pressing followed by sintering at 1400 °C for 5 h. The cathode powders were first dispersed in a pre-mixed solution of glycerol, ethylene glycol, and isopropyl alcohol. A colloidal suspension was obtained by a planetary milling (Fritsch, Pulverisette 6) at 400 rpm for 0.5 h. The suspension was then deposited symmetrically onto opposing sides of the dense SDC disks using spray deposition. The disk and deposited layers were then calcined at 1000 °C for 2 h in an air atmosphere. The silver paste was then deposited as the current collector.

Anode-supported thin-film electrolyte dual-layer cells were prepared via dual dry-pressing and high-temperature sintering. Anode powders consisting of 60 wt% \( \text{NiO} \) and 40 wt% SDC were prepared by mixing and milling NiO and SDC powders using an agate mortar and pestle. The green bi-layer electrolyte disks were densified by firing at 1400 °C for 5 h in an air atmosphere. The cathode slurry was then painted onto the whole circular area of the dense electrolyte surface and fired at 1000 °C for 2 h in an air atmosphere. The resultant coin-shaped cathode had an effective area of 0.48 cm\(^2\).
Basic characterization: The crystal structures were determined by powder X-ray diffraction (D8 Advance, Bruker, Germany) with filtered Cu-Kα radiation (40 kV and 40 mA) using a receiving slit of approximately 0.2–0.4 mm. The diffraction patterns were collected by step scanning between 20 = 10–90° with a step size of 0.05°. Rietveld refinements of the powder XR D patterns were performed using DIFFRACplus Topas 4.2 software. During the refinements, general parameters, such as the scale factor, background parameters, and the zero point of the counter, were optimised. To simplify the complexity associated with refining large amount of parameters simultaneously, Le Bail refinement was initially used to determine the space group and lattice parameters of the SrNb0.9Co0.9xFe0.3-y phases. Rietveld refinement was then used to determine the position of each atom in the lattice.

The oxygen non-stoichiometry and the average of valence states of B-site cation (Co and Fe) at room temperature were determined by iodometric titration. Briefly, approximately 0.1 g of powder was dissolved in a 6 mol\(^{-1}\) HCl solution under the protection of a nitrogen atmosphere to prevent the oxidation of I\(^{-}\) ions (from KI) by air, followed by titration with a standard thiosulfate (S\(_2\)O\(_3\)\(^2-\)) solution. The oxygen non-stoichiometry and the average of valence states of Co and Fe at high temperatures were measured by thermogravimetric analysis (TGA, Model STA 449 F3, NETZSCH) under synthetic air from room temperature to 1000 °C. The heating and cooling rates were 10 °C min\(^{-1}\). Moreover, the oxygen non-stoichiometry (\(\delta\)) at different temperatures was calculated based on the thermogravimetric data.

The oxygen non-stoichiometry at different temperatures in the sample was obtained with the following equation:

\[
\delta = \frac{M \times m_0 - (M - 15.9994 \times \delta) \times m}{15.9994 \times m} 
\]

Where \(m_0\) and \(m\) are the original weight and the actual weight after heating of the sample, respectively; \(M\) is the molar mass of the stoichiometric form of \(\text{SrNb}_0.9\text{Co}_{0.9x}\text{Fe}_{0.3-y}\) (0 ≤\(x\) ≤0.5); \(\delta\) is the oxygen non-stoichiometry of the sample at the room temperature.

The oxygen desorption properties of the composite powders were probed using oxygen temperature programmed desorption (O\(_2\)-TPD). For a typical O\(_2\)-TPD measurement, approximately 0.15 g oxide powders (in the size of 40–60 meshes) were loaded in a U-type quartz tube. Pure argon at a flow rate of 15 ml min\(^{-1}\) [STP] (standard temperature and pressure) was fed to the reactor as the carrier gas and the temperature was increased from room temperature to 930 °C at a rate of 10 °C min\(^{-1}\). The effluent gases were analysed by a mass spectrometer (MS, Hiden, QIC-20) to monitor the oxygen concentration.

A bar with the dimensions of 2 mm × 5 mm × 20 mm was sintered at 1100 °C in air to determine the TECs. TECs were measured using a Netsch DIL 402C/3/G dilatometer from 25 °C to 1000 °C with an air-purge flow rate of 50 ml min\(^{-1}\).

The morphologies of the cathode and cathode/electrolyte interface were obtained using an environmental scanning electron microscope (ESEM, QUANTA-2000).

Electrochemical measurements: Electrochemical impedance spectra (EIS) of the cathode was obtained by AC impedance measurements using an electrochemical workstation composed of a Solartron 1260A frequency response analyser and a Solartron 1287 potentiostat. The symmetrical cells were tested between 450–750 °C in an ambient air atmosphere. The applied frequency range was from 0.01 Hz to 100 kHz, and the signal amplitude was 10 mV. The measurement was performed under an open circuit voltage (OCV) condition. Electrode polarisation resistance data were analysed with Z-plot 3.0c software.

The I–V and I–P polarisation curves were collected using a Keithley 2420 source meter based on the four-probe configuration. The single cell test was conducted over an in-lab constructed fuel cell test station within the temperature range of 400–600 °C. During the test, H\(_2\) was fed into the anode side as a fuel at a flow rate of 80 ml min\(^{-1}\) [STP], while the cathode side was exposed to ambient air.

3. Results and discussion

Fig. 1a depicts room-temperature powder X-ray diffraction (XRD) patterns of SrNb\(_0.9\text{Co}_{0.9x}\text{Fe}_{0.3-y}\) (0 ≤\(x\) ≤0.5) perovskites. All compositions exhibit primitive cubic structure with Pm-3m symmetry (space group #221) as confirmed by Rietveld refinement; the lattice parameters of which are listed in Table 1. Fig. 1b shows magnified section around the most intense peak (e.g. ~32.7°) which shifts gradually to the lower angle for higher Fe content; indicating lattice expansion. This can be rationalised in terms of smaller Co ions (ionic radius of 0.61 Å (Co\(^{3+}\)) or 0.53 Å (Co\(^{2+}\)) substitution by larger Fe ions (ionic radius of 0.645 Å (Fe\(^{3+}\)) or 0.585 Å (Fe\(^{4+}\)) ions) (Note: all in high spin at 6-fold coordination).

Table 1 Lattice parameters of SNCF from Rietveld refinements using Pm-3m space group.

<table>
<thead>
<tr>
<th></th>
<th>SNC</th>
<th>SNCF0.1</th>
<th>SNCF0.2</th>
<th>SNCF0.3</th>
<th>SNCF0.5</th>
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of the oxygen non-stoichiometry and average valence state of B-site cation was probed using thermal gravimetric analysis in air; the results of which are shown as Fig. 2. All compositions show analogous trend of increase of $\delta$ and decrease of $n$. As such, the initial values at room temperature become the determining factor. It is worthwhile to note that the average valence states of Co and Fe approaches 3+ between 500 and 600 °C. In the absence of interaction between oxygen vacancies and ordering phenomena and when electronic conductivity is not a limiting factor, ORR activity normally correlates with the oxygen non-stoichiometry.\textsuperscript{14,15,24-27} This can be understood considering the oxygen vacancies role as the oxygen ions diffusion pathway within the bulk material, effectively extending the ORR from the cathodeelectrolyteloxygen three phase boundaries (TPB) to the whole cathode surface. Higher oxygen diffusion rate therefore translates to larger cathode surface for ORR. In short, the oxygen vacancies supply the active sites for oxygen adsorption (e.g. oxygen dissociation) at cathode surface.\textsuperscript{5}

Table 2 Oxygen non-stoichiometry ($\delta$) and average valence states of B-site ($n$) of SNCF at room temperature.

<table>
<thead>
<tr>
<th>Sample</th>
<th>$\delta$</th>
<th>$n$</th>
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<tr>
<td>SNCF0.1</td>
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</tr>
<tr>
<td>SNCF0.2</td>
<td>0.34</td>
<td>3.1</td>
</tr>
<tr>
<td>SNCF0.3</td>
<td>0.31</td>
<td>3.2</td>
</tr>
<tr>
<td>SNCF0.5</td>
<td>0.25</td>
<td>3.3</td>
</tr>
</tbody>
</table>

Fig. 2 The oxygen nonstoichiometry ($\delta$) and average valence states of B-site cation ($n$) between 450-750 °C.

The ORR activity of the SNCF (0≤$x$≤0.5) cathodes was quantified by electrochemical impedance spectroscopy using symmetric cells with Sm$_0.2$Ce$_0.8$O$_{1.9}$ (SDC) as an electrolyte. Fig. 3a shows the resultant Nyquist plots between 500 and 600 °C. The area specific resistance (ASR) of the cathode is obtained from the difference between the low frequency and the high-frequency intercepts on the real axis and represents the resistance of the cathode. Except for SNCF0.5, all doped compositions provide lower ASR values (relative to SNC). Quite significant here is the fact that the resistances of the three doped compositions, SNCF0.1, SNCF0.2 and SNCF0.3 at 550 °C were below a target ASR value of 0.15 $\Omega$ cm$^2$ (below 550 °C) specified by Steele et al.\textsuperscript{28} We note that the best composition, SNCF0.2 delivered the lowest ASR values of 0.301, 0.111 and 0.052 $\Omega$ cm$^2$ at 500, 550 and 600 °C, respectively. As a comparison, SNC cathode prepared at identical condition showed ASR values of 0.600, 0.195 and 0.068 $\Omega$ cm$^2$ at 500, 550 and 600 °C, respectively; approximately 30-100% higher. Notably, at 450 °C (the lowest measured temperature), a relatively low ASR 0.937 $\Omega$ cm$^2$ was attained for SNFC0.2; much favorable compared to 1.74 $\Omega$ cm$^2$ for SNC. These observations together with the thermal activation energy ($E_a$) for ASRs of SNCF (0.1≤$x$≤0.5) cathodes are evident in Fig. 3b. While SNC cathode exhibited $E_a$ value of 108 kJ mol$^{-1}$, SNCF0.2 provided a lower value of 94 kJ mol$^{-1}$ which is deemed more favorable to retain high performance at lower temperatures. The mapping of performance of SNFC0.2 against other high performance
perovskite cathodes in the form of Arrhenius plots is shown in Fig. S1. This figure include Co-based cathodes represented by \( \text{La}_0.6\text{Sr}_{0.4}\text{CoO}_3 \)\(^{29}\), \( \text{SrSc}_{0.2}\text{CoO}_3 \)\(^{30}\), \( \text{SrNb}_{0.1}\text{CoO}_3 \)\(^{14}\), \( \text{SrCo}_{0.7}\text{Nb}_{0.3}\text{O}_3 \)\(^{15}\), \( \text{SrNb}_{0.1}\text{CoO}_3 \)\(^{14}\) and \( \text{SrSc}_{0.2}\text{CoO}_3 \)\(^{30}\) layered structure materials such as \( \text{PrBaCo}_2\text{O}_4 \)\(^{31}\), \( \text{SrBa}_{0.5}\text{CoO}_3 \)\(^{32}\) and double perovskite, \( \text{Bi}_{2}\text{Sr}_{0.6}\text{Co}_{0.4}\text{O}_3 \)\(^{23}\). Several Fe doped Co-based cathodes are also incorporated, for example \( \text{Ba}_{0.8}\text{Sr}_{0.1}\text{Co}_{0.1}\text{FeO}_3 \)\(^{33}\), \( \text{BaCo}_{0.7}\text{Fe}_{0.3}\text{O}_3 \)\(^{34}\), \( \text{BaCo}_{0.5}\text{Fe}_{0.5}\text{O}_3 \)\(^{35}\) and layered structure materials such as \( \text{SrCo}_{0.7}\text{Fe}_{0.3}\text{O}_3 \)\(^{36}\), \( \text{SrCo}_{0.7}\text{Fe}_{0.3}\text{O}_3 \)\(^{37}\), \( \text{NdBaCo}_{0.9}\text{Fe}_{0.2}\text{O}_3 \)\(^{38}\) and \( \text{NdBaCo}_{0.9}\text{Fe}_{0.2}\text{O}_3 \)\(^{39}\). SNCF0.2 cathode shows the lowest ASR and \( E_a \) values among all the listed cathodes which highlights its potential towards enabling low temperature SOFCs.

Table 3 Fitted impedance spectra values for SNCF (0 ≤ x ≤ 0.5) cathodes between 550 and 650°C.

<table>
<thead>
<tr>
<th>Sample</th>
<th>550 °C</th>
<th>600 °C</th>
<th>650 °C</th>
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<tr>
<td>R(_{E1})</td>
<td>R(_{E2})</td>
<td>R(_{E1})</td>
<td>R(_{E2})</td>
</tr>
<tr>
<td>SNC</td>
<td>0.060</td>
<td>0.135</td>
<td>0.025</td>
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<tr>
<td>SNCF0.1</td>
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<td>0.071</td>
<td>0.035</td>
</tr>
<tr>
<td>SNCF0.2</td>
<td>0.072</td>
<td>0.039</td>
<td>0.036</td>
</tr>
<tr>
<td>SNCF0.3</td>
<td>0.092</td>
<td>0.036</td>
<td>0.045</td>
</tr>
<tr>
<td>SNCF0.5</td>
<td>0.120</td>
<td>0.091</td>
<td>0.053</td>
</tr>
</tbody>
</table>

More information can be obtained from the impedance spectra (Fig. 3a) to evaluate the ORR kinetics of SNCF cathodes. Therefore, equivalent circuit model containing the series resistor and parallel resistor/constant phase element components with a configuration of \( R_o - (R\(_{E1}\)-CPE\(_1\)) - (R\(_{E2}\)-CPE\(_2\)) \) were used to fit the spectra. Our previous studies demonstrate the suitability of this model for mixed ionic-electronic conducting cathodes having high oxygen vacancy concentration such as \( \text{Ba}_{0.5}\text{Sr}_{0.5}\text{Co}_{0.3}\text{FeO}_{2.5} \)\(^{32}\), \( \text{SrCo}_{0.7}\text{CoO}_3 \)\(^{30}\), \( \text{SrNb}_{0.1}\text{CoO}_3 \)\(^{30}\) and \( \text{SrNb}_{0.1}\text{FeO}_3 \)\(^{36}\) cathodes. In this model, \( R_o \) is the ohmic resistance from the electrolyte, electrode and lead; CPE\(_1\) and CPE\(_2\) are constant phase elements. Resistance at high frequency represents the resistance of the charge transfer processes (R\(_{E1}\)) which include the electron-transfer and ion transfer processes, occurring at the current collector/electrode and the electrode/electrolyte interfaces, respectively. Resistance at low frequency, on the other hand, represents the resistance of non-charge-transfer processes (R\(_{E2}\)) which include adsorption of oxygen, oxygen diffusion at the gas-cathode surface interface and surface diffusion of intermediate oxygen species.\(^{31,43}\) The deconvoluted results are listed in Table 3. For SNC, R\(_{E2}\) values are larger than R\(_{E1}\) values, indicating relatively slow non-charge transfer processes on SNC cathode surface (compared to charge transfer processes). Partial substitution of Co with Fe creates additional oxygen vacancies which enhances non-charge transfer processes as evidenced by lowering R\(_{E2}\) values. The oxygen vacancies trend somewhat correlates with R\(_{E2}\) values in the order of SNFC0.1-0.3 followed by SNFC0.5. Recently, Kulkja et al.\(^{34}\) employed combined theoretical and experimental analysis to evaluate the relationship between surface oxygen vacancy and ORR and analyse the rate-determining step on ORR mechanism of \( (\text{La},\text{Sr})\text{MnO}_3 \), \( (\text{La},\text{Sr})(\text{Co},\text{Fe})\text{O}_3 \) and \( (\text{Ba},\text{Sr})(\text{Co},\text{Fe})\text{O}_3 \) cathodes. Such study is beyond the scope of this work however the trend observed here is quite consistent with the work of Kulkja et al. which highlights the role of enhanced oxygen vacancy concentration to promote oxygen surface exchange processes.\(^{10,44,45}\) It is worth noting that a lower ORR activity was obtained for SNFC0.5 relative to SNC although the oxygen vacancy concentration is higher for SNFC0.5. Increasing Fe doping consistently leads to increased R\(_{E1}\) values which reach their maximum values at 50% Fe, the highest doping amount tested in this work. Upon comparing R\(_{E1}\) and R\(_{E2}\) values for SNFC0.5 (Table 3), the contribution from R\(_{E1}\) (charge transfer processes) clearly outweighs that from R\(_{E2}\) (non-charge transfer processes) and becomes the limiting factor. This can simply be understood from the higher content of less redox active Fe (relative to Co)\(^{29,31,46,47}\) which is likely to impede the charge transfer processes. Another piece of supporting evidence can be found in our previous work\(^{46}\) which reports an analogous perovskite compound where Co is completely replaced with Fe e.g. \( \text{SrNb}_{0.1}\text{FeO}_3 \)\(^{36}\) (SNF). R\(_{E1}\) values for SNF are 0.6, 0.3 and 0.15 \( \Omega \) cm\(^2\) at 550, 600 and 650 °C which are substantially higher than those for SNCF0.5.
To evaluate the impact of electrode microstructure (e.g. grain size, pore structure and connection with electrolyte) on electrochemical performance, scanning electron microscopy (SEM) images of the surface and cross-section of SNCF cathode after firing at 1000 °C for 2 h are obtained and displayed in Fig. 4. Sturdy cathode to electrolyte connection is apparent (more clear on Fig. S2 – lower magnification); denoting the thermal compatibility of SNCF perovskite against the SDC electrolyte. Smaller grain size for higher Fe content (e.g. Fe content of 0.3 and more) is likely attributable to the reduced sinterability; consistent with the decreased oxygen non-stoichiometry and diffusion trend delineated above. \(^{48}\) Given that smaller grain size results in increased surface area (at constant volume), reduced sinterability for SNCF may actually be favorable in achieving enhanced ORR activity. Fe doping can therefore be adjusted to manipulate the sinterability of Co-based perovskite cathodes as also reported elsewhere.  \(^{38,49}\) The contribution of the grain size however is not substantial on these SNCF cathodes. It is evident that the ORR activity is closely related to the oxygen non-stoichiometry, as the highest ORR activity of SNCF0.1 and SNCF0.2 (e.g. lowest ASRs) correlates with the largest oxygen non-stoichiometry values of these cathodes. To a minor extent, smaller grain size of SNCF0.2 may contribute to the slightly higher ORR activity for SNCF0.2 at 500 and 550 °C. However, larger grain size of SNFC0.2 (relative to the grain size of SNCF0.3 and SNFC0.5) does not translate to higher ORR activity for SNFC0.3 and SNFC0.5, which rules out dominant grain size influence.

Although it is not likely, the phase transition at high temperature may occur and significantly influence the ORR activity.  \(^{40,50-52}\) The possibility of such transition on the SNCF perovskite was checked by annealing them at high temperature followed by quenching to room temperature (to preserve their high temperature crystalline structure). Powder x-ray diffraction (XRD) patterns of the SNCF0.1-0.5 may contribute to the slightly higher ORR activity for SNCF0.2 at 500 and 550 °C. However, larger grain size of SNFC0.2 (relative to the grain size of SNCF0.3 and SNFC0.5) does not translate to higher ORR activity for SNFC0.3 and SNFC0.5, which rules out dominant grain size influence.

We take a highly active cathode, BSCF as a baseline to illustrate factors affecting phase stability of the perovskites. BSCF, particularly at high Ba and Co content e.g. 50% Ba and 80% Co is characterised by a pronounced size mismatch between A- and B-site cations. This attribute facilitates the reduction of B-site cations which leads to an increased effective ionic radius, a higher oxygen deficiency as well as reduction in oxygen vacancy migration barriers. Despite its beneficial effects to ionic conductivity and oxygen exchange kinetics, this A- and B-site cation size mismatch also destabilises the cubic perovskite structure, driving the formation of hexagonal phase exhibiting lower ionic conductivity and slower kinetics. \(^{34,53,54}\) To solve this structure issue, for example the hexagonal phase formation can be suppressed by adding low amount of high-valence cations such as Nb \(^{56}\) in B-site. \(^{55}\) The exclusion of large size Ba cation from the A-site minimise the mismatch further. In addition, partial substitution of Co in SNC with Fe is expected to provide improved phase stability considering higher covalency of Fe-O bond compared to Co-O bond. \(^{56}\)

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**Fig. 4** SEM images of the surface and cross-section of SrNb\(_{0.1}\)Co\(_{0.9-x}\)Fe\(_{x}\)O\(_{3-\delta}\) (0\(\leq\)x\(\leq\)0.5) cathodes fired at 1000 °C for 2 h in air: (a, f) x=0, (b, g) x=0.1, (c, h) x=0.2, (d, i) x=0.3, (e, j) x=0.5.

**Fig. 5** Powder x-ray diffraction patterns of SNCF (x=0.1-0.5) powders quenched from 500 and 700 °C including as-synthesised ones for comparison. (a) SNCF0.1; (b) SNCF0.2; (c) SNCF0.3; (d) SNCF0.5.
The electrochemical performance of SNFC0.2 was further tested using an SDC-Ni (50:50 vol. %) anode-supported SDC (20 µm) electrolyte single cell. The voltage and power density polarisation curves of a single fuel cell were obtained with hydrogen as a fuel and ambient air as the oxidation agent between 400-600 °C (Fig. 6a). The peak power densities were 610, 1089 and 1587 mW cm\(^{-2}\) at 500, 550 and 600 °C, respectively; the highest reported to date. Fig. 6b, in turn, compares the peak power densities of SNCF0.2 to those of BSCF\(^{10}\) and the parent compound, SNC\(^{14}\), highlighting its superior cell performance. Further performance improvement is an open possibility; offered via an engineering approach such as thickness reduction and microstructure optimisation.

Another piece of supporting data obtained by impedance spectroscopy is summarised in Fig. 7 which plots the resistance of fuel cell components e.g. electrode (cathode plus anode) and electrolyte between 500-600 °C. The polarisation resistances of the electrode are as low as 0.025 and 0.113 Ω cm\(^2\) at 600 and 500 °C, respectively. Notably, the resistances of the electrode in the single fuel cell are different from that of the symmetric cell due to the different testing condition imposed e.g. symmetric cell were tested under open circuit voltage while full cell were tested under cathodic polarisation condition.

Fig. 7 Electrodes and electrolyte polarisation resistances of single fuel cell between 500-600 °C.

Fig. 8 Thermal expansion curves of SNCF between 25-900 °C in air.

Fig. 9 \(\text{O}_2\)-temperature programmed desorption profiles of SNCF.

Fig. 8 shows the thermal expansion curve of SNCF (0 ≤ x ≤ 0.5) between 25-900 °C in air. An inflection in the curve is observed at ~450 °C which correlates with the reduction of Co\(^{4+}\) or Fe\(^{4+}\) to Co\(^{3+}\) or Fe\(^{3+}\) indicated by oxygen-temperature programmed desorption (O\(_2\)-TPD) results (Fig. 9). The average TEC values of SNCF and SDC\(^{57}\) are listed in Table 4; the values of which decreases with increasing Fe content. This
may be due to the stronger Fe-O bond (with respect to the Co-O bond).\textsuperscript{58} Low TEC normally leads to better structural stability in long term operation and during thermal cycling.

\textbf{Table 4 TECs for SNCF samples between RT and 900 °C in air.}

<table>
<thead>
<tr>
<th>Samples</th>
<th>RT-450 °C</th>
<th>450-900 °C</th>
<th>RT-900 °C</th>
</tr>
</thead>
<tbody>
<tr>
<td>SNC</td>
<td>19.2</td>
<td>31.5</td>
<td>27.9</td>
</tr>
<tr>
<td>SNCF0.1</td>
<td>19.0</td>
<td>28.5</td>
<td>26.4</td>
</tr>
<tr>
<td>SNCF0.2</td>
<td>18.7</td>
<td>26.9</td>
<td>26.0</td>
</tr>
<tr>
<td>SNCF0.3</td>
<td>18.1</td>
<td>26.7</td>
<td>25.1</td>
</tr>
<tr>
<td>SNCF0.5</td>
<td>16.1</td>
<td>24.4</td>
<td>22.3</td>
</tr>
<tr>
<td>SDC\textsuperscript{59}</td>
<td>12.3 (30-800 °C)</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

Resistance to carbon dioxide adds to the practical value of a cathode due the presence of this gas in ambient atmosphere and fuel (as a product of synthesis gas), particularly when the application in single chamber SOFC is envisioned. Alkaline earth containing perovskites are normally prone to CO\textsubscript{2} poisoning.\textsuperscript{59-61} To determine its resistance to CO\textsubscript{2}, the ASR of SNCF cathodes at 600 °C is monitored before and after introducing CO\textsubscript{2} (in varying concentration between 1-10 vol.% CO\textsubscript{2}) into the cathode side (Fig. 10). Relative to BSCF and the parent compound, SNC, SNCF cathodes show marginal increase in their ASR values. We attributed the observed stability to the higher acidity of the metal oxide in SNCF perovskites.\textsuperscript{62} Furthermore, although all compounds shows the regeneration ability when air was introduced back into the atmosphere, SNFC cathodes can rapidly recover their original ASR values. CO\textsubscript{2} effect on the SNCF0.2 and BSCF was examined by powder x-ray diffraction (Fig. S3) and Fourier-Transform Infra-Red spectra (Fig. S4). Both results reveal the remarkably improved CO\textsubscript{2}-tolerance on the SNCF0.2. While carbonate phases is observed in the powder XRD of CO\textsubscript{2} treated BSCF, they don’t exist in SNCF0.2. Accordingly, there is a negligible indication of vibration in the wavelength characteristic of carbonaceous functional groups for SNCF0.2 which on the other hand is quite substantial in BSCF case.

\textbf{4. Conclusions}

In sum, a new family of Sr\textsubscript{1-x}Nb\textsubscript{x}Co\textsubscript{0.9-x}Fe\textsubscript{x}O\textsubscript{3-δ} (SNCF, 0.1≤x≤0.5) perovskite have been developed which exhibits improved cathode attributes with respect to their parent compound, Sr\textsubscript{0.1}Co\textsubscript{0.9}O\textsubscript{3-δ} (SNC). Partial Co substitution with Fe enhanced the ORR activity, reduced the TECs and increased CO\textsubscript{2} resistance. These properties closely correlated with the oxygen non-stoichiometry trend and sinterability behavior. Of all doped compounds, SNFC0.2 demonstrates the highest ORR activity.

\textbf{Acknowledgements}

This work was supported by the China National Funds to Distinguished Young Scientists under contract No. 51025209, the Outstanding Young Scholar Grant at Jiangsu Province under contract No. 2008023, the Fok Ying Tung Education Grant under contract No. 111073, the Program for New Century Excellent Talents in Chinese Ministry of Education and the National Basic Research Program of China under contract No. 2007CB209704. W.Z. appreciates the support of an Australian Research Council (ARC) Discovery Project.

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† Electronic Supplementary Information (ESI) available: [details of any information available should be included here]. See DOI:10.1039/b000000x/s

A novel family perovskite SrNb$_{0.1}$Co$_{0.9-x}$Fe$_x$O$_{3.5}$ (SNCF, 0.1≤x≤0.5) shows not only high oxygen-reduction-reaction activity at operating temperatures below 600 °C (e.g. peak power density of 1587 mW cm$^{-2}$ at 600°C) but also low TECs and improved CO$_2$ resistivity.