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ARTICLE

Frontal vitrification of PDMS using air plasma and consequences for surface wrinkling

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We study the surface oxidation of polydimethylsiloxane (PDMS) by air plasma exposure and its implications for mechanically-induced surface wrinkling of the resulting glass-elastomer bilayers. The effect of plasma frequency (kHz and MHz), oxygen content (from O₂ to air), pressure ($0.5 \leq P \leq 1.5$ mbar), as well as exposure time and power, is quantified in terms of the resulting glassy skin thickness h , inferred from wrinkling experiments. The glassy skin thickness is found to increase logarithmically with exposure time t , for different induction powers p , and all data collapse in terms of plasma dose, $D \equiv p \times t$. The kinetics of film propagation are found to increase with oxygen molar fraction y_{O_2} and decrease with gas pressure P , allowing both wrinkling wavelength λ and amplitude A to be effectively controlled by gas pressure and composition. A generalised relationship for frontal vitrification is obtained by re-scaling all λ and h data by D/P . A coarse-grained wave propagation model effectively describes and quantifies the process stages (induction, skin formation and propagation) under all conditions studied. Equipped with this knowledge, we further expand the capabilities of plasma oxidation for PDMS wrinkling, and a wavelength of $\lambda \approx 100$ nm is readily attained with a modest strain $\epsilon_{\text{prestrain}} \approx 20\%$.

1 Introduction

Wrinkling of ‘sandwich bilayers’ is an attractive route for large area and low cost surface patterning, with feature sizes ranging from 100s nm to 100s μm and beyond.¹⁻³ Pattern formation occurs readily via a mechanical instability of bilayers under compression, typically consisting of a thin, rigid film supported by a softer substrate. Compression along the plane of the film can be imposed by various methods, either during film formation or by a subsequent reversible step. These include mechanical strain⁴⁻⁶, temperature cycling^{7, 8}, solvent induced swelling and evaporation,^{7, 9-11} and solution deposition and film drying^{7, 12-14}, amongst others. Film formation approaches include thin film floating or transfer¹⁵, vapour deposition,^{7, 16, 17} ion sputtering¹²⁻¹⁴, substrate oxidation and vitrification (e.g., via plasma exposure or UV ozonolysis).^{4-6, 8, 18} While a range of materials can be used as substrates, elastomers like polydimethylsiloxane (PDMS) are convenient due to their relatively low modulus (≈ 1.6 MPa¹⁹), near incompressibility (Poisson ratio $\nu \approx 0.5$ ¹⁹), large elongation at break ($\approx 200\%$ ²⁰), surface adhesion and transparency. Oxidation of PDMS, by ultraviolet ozonolysis (UVO) or plasma exposure, results in cleaving Si-CH₃ groups and the formation of a denser, SiO_x-

rich glass-like surface layer^{21, 22, 23, 24} effectively yielding a strongly bound ‘sandwich bilayer’ with a high skin/substrate modulus contrast as required for wrinkling. UVO oxidation occurs by exposure to 185 and 254 nm light, accompanied by ozone-formation,²² which in turn induces PDMS conversion with a non-uniform cross-sectional profile (over 50-100nm^{22, 25, 26}), whose effective thickness h yields wrinkling wavelengths λ in the 10 to 100 μm range under compression^{4, 22}. Plasma oxidation takes place by ionisation of a gas, typically oxygen, under vacuum by an oscillating electric field²⁷, and comparatively yields thinner skins ($h \sim 10$ nm) and thus smaller λ ($\approx 100\text{nm} - 10 \mu\text{m}$ ^{4, 5}). The efficiency of surface oxidation is expected to depend on gas (or mixture of gases) and pressure²³, which have not been explored in the context of wrinkling.

We have recently reported on the PDMS skin formation induced by O₂ plasma (40 kHz) exposure and found surface vitrification to be a frontal process, whose glassy thickness h increases with logarithmic kinetics with plasma dose D ⁵. Three stages of film formation could be identified: (i) induction, (ii) formation and (iii) propagation, describing the increase of skin modulus and thickness during glassy front propagation. We could then map the wrinkling λ accessible by this method,⁵ and found the coupling of skin growth and propagation to yield a

practical $\lambda_{\min} \approx 140$ nm at high strains ($\varepsilon \approx 200\%$)⁵, near the maximum elongation at break. While smaller λ have been demonstrated in wrinkling cascades²⁸, we are concerned here with single frequency sinusoidal surfaces.

In this paper, we assess whether air plasma exposure, more attractive from a manufacturing and safety standpoints, is effective as a frontal PDMS skin vitrification approach. We evaluate the influence of processing parameters – induction plasma frequency (kHz, MHz), gas pressure P and composition γ_{O_2} , power p and exposure time t – on the glassy skin thickness h and thus wrinkling wavelengths λ attainable. For generality, we select the most common plasma induction frequencies, namely 40 kHz and 13.6 MHz, and gas pressures within 0.5-1.5 mbar suitable for ignition.

Our paper is organised as follows: Section 1.1 introduces the fundamental wrinkling equations, in both the low and high deformation sinusoidal regimes, followed by a coarse-grained model of the frontal oxidation process in Section 1.2. Section 2 describes the experiments and wrinkling analysis to directly measure patterned λ and A , and thereby infer skin thickness h . In Section 3, the experimental results for the range of processing parameters are presented and interpreted in terms of the frontal model. Section 4 summarizes the findings and provides recommendations for PDMS wrinkling by surface oxidation and mechanical compression.

1.1 Wrinkling bilayer mechanics

Mechanically-induced wrinkling occurs as a consequence of the application of strain to a bilayer consisting of a stiff thin film bonded to a compliant substrate. Sinusoidal surface undulations result from the energy minimisation of bulk deformation and skin bending²⁹⁻³¹, with wavelength

$$\lambda = 2\pi h \left(\frac{E_f (1-\nu_s^2)}{E_s (1-\nu_f^2)} \right)^{1/3} \quad (1)$$

where h is the film thickness, E_f and E_s are the elastic moduli of both film and substrate, and $\nu_{f,s}$ is the Poisson ratio of each layer. Eq. (1) is often simplified by introducing the plane strain modulus $\bar{E} = E(1-\nu^2)$. The wrinkling amplitude

$$A = h \left(\frac{\varepsilon}{\varepsilon_c} - 1 \right)^{1/2} \quad (2)$$

depends on strain ε , and a critical strain value^{30,31}

$$\varepsilon_c = \frac{1}{4} \left(\frac{3\bar{E}_s}{\bar{E}_f} \right)^{2/3} \quad (3)$$

must be exceeded for wrinkling to occur²⁹⁻³¹.

The wrinkling profile, defined by λ and A , can thus be separately tuned by judiciously changing the film thickness h and strain ε (since only A depends on ε , in this limit). The wrinkling *morphology* is effectively tuned by the strain field (see for example^{4, 18, 32}),

although only uniaxial strain is considered here. Beyond the limit of low deformation³³⁻³⁸, when $\varepsilon \gg \varepsilon_c$, both the wavelength and amplitude³⁵ now depend on ε and

$$\lambda = \frac{\lambda_{LD}}{(1+\varepsilon)(1+\xi)^{1/3}} \quad (4)$$

$$A = \frac{A_{LD}}{(1+\varepsilon)^{1/2}(1+\xi)^{1/3}} \quad (5)$$

where $\xi = 5\varepsilon(1+\varepsilon)/32$. The low deformation eqs. (1,2) provide a reasonable approximation for a range of low ε values, and are thus commonly employed. At even higher deformations, wrinkling is no longer sinusoidal, as higher modes and folding eventually dominate^{39, 40} and the linear relationship between λ with film thickness h no longer holds.

1.2 Modelling the plasma-induced frontal glass formation

Previous studies on wrinkling of bilayers obtained through plasma oxidation of PDMS^{5, 8} have shown the existence of a logarithmic dependence between the oxidised film thickness and the exposure time. This planar frontal glass-formation process has been successfully described by a minimal spatio-temporal model, borrowing concepts from well-established directional solidification via frontal photopolymerisation⁴¹⁻⁴³. In short, we describe the extent of PDMS conversion into glass an equation of motion for conversion order parameter $\phi(z,t)$

$$\frac{\partial \phi(z,t)}{\partial t} = K[1 - \phi(z,t)]I(z,t) \quad (6)$$

where K is a constant related to the oxidation reaction kinetics, I is the plasma intensity, and z is the position coordinate orthogonal to the specimen and with origin at the top surface. The boundary conditions $\phi(z=0,t=0)=0$ and $\phi(z=0,t=\infty)=I$ stipulate that the material starts as neat PDMS ($\phi=0$) and fully converts ($\phi=I$) at long times. The non-monotonic variation of $I(z,t)$ is modelled by a relation analogous to a Beer-Lambert law

$$\frac{\partial I(z,t)}{\partial z} = -\mu(z,t)I(z,t) \quad (7)$$

describing the effective penetration of the plasma in the material, where μ is generally an averaged attenuation coefficient (weighted by composition). If the material properties do not change significantly upon conversion, i.e. $\mu(z,t) \approx \mu$ (invariant case),^{41, 42} we obtain an analytical expression for the glassy film thickness h

$$h = \frac{\ln(t)}{\mu} - \frac{1}{\mu} \ln \left(\frac{1}{K I_0} \ln \left(\frac{1}{1-\phi_c} \right) \right)$$

where ϕ_c is a critical conversion value required for glass formation (analogous to a *percolation* threshold), and $I_0 = I(z=0,t)$. Our minimal frontal model describes the glassy film formation with only three parameters: $1/\mu$, readily determined by the *slope* of a h vs $\ln(t)$ graph, $\overline{K I_0}$ and ϕ_c determined by the *intercept* of the graph (and decoupled by a series of self-consistent experiments at various P). Further, we found that plasma dose ($D = p \times t$) captured the combined effects of changing plasma power p and exposure time t , and d thus

collapses all experimental results for h or λ at different P and t . We therefore re-write the expression as

$$h = \frac{\ln(D)}{\mu} - \frac{1}{\mu} \ln\left(\frac{1}{Kl_0} \ln\left(\frac{1}{1-\phi_c}\right)\right) \quad (8)$$

and will seek to obtain quantitative relationships for the model parameters as a function of plasma processing conditions (detailed further in Supporting Information and Figs. S1 and S2).

2 Experimental

2.1 Sample preparation

PDMS elastomer samples were obtained by mixing the pre-polymer and crosslinker (Sylgard 184, Dow Corning) at a 10:1 ratio by mass. The mixture was vigorously stirred with a spatula, placed under vacuum for 15 min to degas, and deposited on a flat glass surface for 3 h, before curing at 75°C in a convection oven for 1 h to crosslink into an elastomer. The PDMS slab obtained, with a thickness of ≈ 2 mm, was cut into pieces of 2 cm² (1 cm \times 2 cm).

For each experiment, distinct specimens were placed in a uniaxial strain stage and then stretched with a micrometer screw to the desired extent. The value of $\varepsilon_{\text{prestrain}}$ was calculated as

$$\varepsilon_{\text{prestrain}} \% = \left(\frac{L_1}{L_0} - 1\right) \times 100 \quad (9)$$

where L_0 and L_1 are the length of the PDMS between the two clamps of the stage before and after stretching. The length was measured with a precision of ± 0.01 mm. The stretched PDMS specimen was then placed in the plasma chamber for oxidation, removed and released from strain, resulting in permanently wrinkled samples in the relaxed state for profile analysis.

2.2 Plasma oxidation

Two different plasma chambers were utilized: (1) a Harrick Plasma PDC-002, connected to a gas mixer and pressure gauge (PDC-FMG-2, Harrick Plasma), and a vacuum pump (IDP3A01, Agilent Technologies) with nominal frequency of 13.6 MHz (RF) and three power settings (30, 10 and 7 W); and (2) a Diener Plasma FEMTO, with a frequency of 40 kHz and power settings from 10 to 90 W, fitted with a pressure sensor (TM 101, Thermovac). Air, oxygen and nitrogen gas cylinders (BOC, O₂ purity of 99.5%) supplied the gas

mixer or the chamber inlets directly. The chambers were evacuated to a pressure of ≈ 0.2 mbar over approximately 5 min, before admitting the gas (or mixture) for 5 min until the desired pressure was reached and stabilized. The plasma was then ignited, at the required power, and exposure controlled with a timer (± 1 s). Pressures higher than 1 mbar were found not to allow for plasma ignition, and the plasma was thus ignited at a lower pressure and the gas flow rate immediately increased to reach the desired pressure (this behaviour is expected from Pashen's law,⁴⁴ and measured for air plasma,⁴⁵ which in this pressure range requires higher breakdown voltages for ionisation). The temperature variation during plasma exposure was directly monitored and found to sufficiently small, such that thermally-induced wrinkling upon cooling is not observed in this range (Supporting Information, Figs. S3 and S4).

Figure 1 illustrates the experimental procedure followed to produce wrinkled PDMS specimens by plasma oxidation.

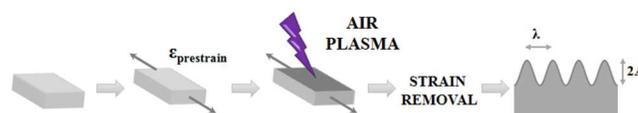


Figure 1: Formation of wrinkles on SiO_x-PDMS bilayers by plasma oxidation: a neat PDMS specimen is pre-strained uniaxially by $\varepsilon_{\text{prestrain}}$, then exposed to plasma (for various gas mixtures, frequency, power, pressure and time), and then allowed to relax forming sinusoidal wrinkling patterns with prescribed λ and A from which glassy skin thickness h is inferred.

2.3 Profile analysis

Pattern wavelengths larger than 1 μm were measured by optical microscopy (Olympus BX41M, 100 \times objective) in brightfield reflection mode, and analyzed using ImageJ. Smaller pattern dimensions were measured via atomic force microscopy (AFM) with Bruker Innova microscope in tapping mode at 0.2 Hz with Si tips (MPP-11100-W, Bruker), and analysed with NanoScope software. Figure 2 depicts a representative wrinkled specimen characterized with both microscopes, as well as the corresponding height profile and sinusoidal line fit.

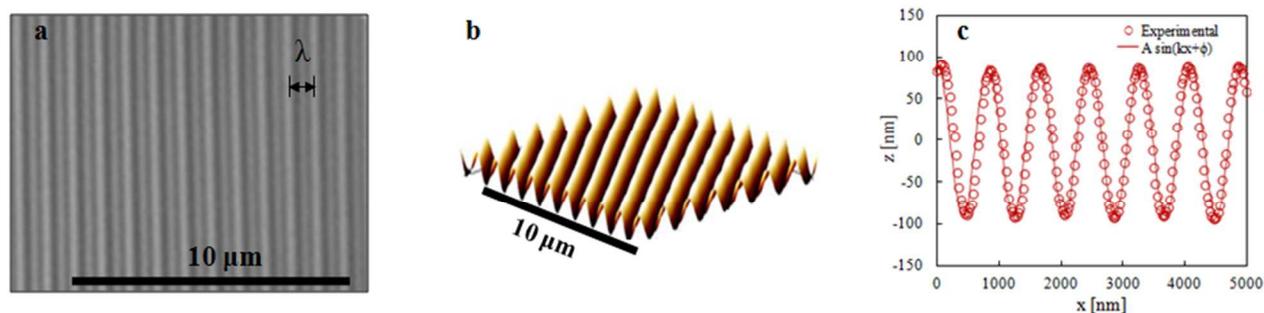


Figure 2: Representative wrinkling pattern obtained by plasma exposure of a PDMS specimen upon relaxation of uniaxial strain (Air, MHz plasma, $t=50$ min, $P=7$ W, $\epsilon_{\text{prestrain}}=20\%$). (a) Optical microscopy image, (b) AFM tapping mode topography and (c) corresponding 1D section profile and fitted sinusoidal curve.

3 Results and Discussion

3.1 Wavelength Measurements

3.1.1 Low deformation and bilayer approximations

At sufficiently low deformations, eqs. (1,2) hold and the wrinkling wavelength λ is practically independent of ϵ , which allows the glass film thickness h to be readily estimated assuming a bilayer model. This procedure has been validated, at least in part, with simultaneous X-ray reflectivity measurements⁵. However, ϵ must exceed the critical ϵ_c which in turn depends on the skin glassy modulus E_f subject to variations during the early stages of film formation. In order to compare different plasma exposure conditions, we opt to select a constant value of $\epsilon_{\text{prestrain}} \approx 20\%$ that exceeds ϵ_c at all conditions studied, while remaining relatively low to ensure relatively low strains, for which the patterns are sinusoidal (Fig 2c) and eqs. (1-5) remain valid. This is illustrated in Fig. 3 by plotting $\lambda(\epsilon)$ for a representative specimen. The experimental data were fitted to eq. (4) where λ_{LD} – the single fitting parameter – was obtained through data regression. At $\epsilon_{\text{prestrain}} \approx 20\%$, one obtains $\lambda_{LD}/\lambda_{HD} \approx 1.215$ from eq. (4), which is verified experimentally within measurement uncertainty. Assuming the experimental $\lambda \approx \lambda_{LD}$ and using eqs. (1-3) to compute h would underestimate the skin thickness by approximately 20%, and we thus employ eq. (4) to compute h . The largest source of uncertainty remains therefore the assumption of a *bilayer* film structure, discussed previously⁵, but which appears acceptable in a comparative evaluation of plasma processing parameters. We focus on the experimentally measured $\lambda(20\%)$ in the presentation of results and then parameterize both $\lambda(20\%)$ and h in conclusion.

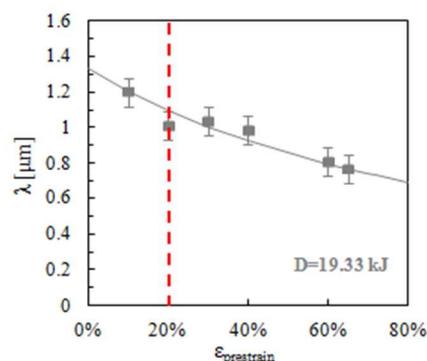


Figure 3: Dependence of the experimental wrinkle wavelength (λ) on pre-strain $\epsilon_{\text{prestrain}}$ applied prior to MHz air plasma exposure at constant pressure $P=0.93$ mbar and dose $D=19.33$ kJ. The line is a fit to eq. (8) yielding λ_{LD} for $\epsilon \rightarrow 0$.

3.1.1 Effect of time, power and frequency

We first report on the effect of air plasma frequency on the wavelength of oxidised PDMS at $\epsilon_{\text{prestrain}} \approx 20\%$, and measure distinct specimens at different power p and exposure time t . The results are summarised in Fig. 4 and confirm the logarithmic dependence⁵ of wrinkling periodicity λ (and thus skin thickness h) in all cases investigated.

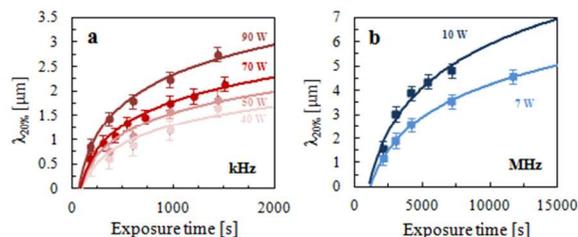


Figure 4: Wavelength of sinusoidal wrinkles for samples prestrained by $\epsilon_{\text{prestrain}}=20\%$ and treated with (a) kHz and (b) MHz air plasma, as a function of exposure time for different power settings, where air pressure was kept constant at $P=0.93$ mbar. The lines are logarithmic fits.

Following our earlier work on O_2 plasma oxidation of PDMS,⁴⁻⁶ we find that rescaling the dependence of λ as a function of dose D ($\equiv p \times t$) results in the collapse of all data (pairs of t, p) onto a single master curve for each plasma frequency, as shown in Fig. 5. Given the direct proportionality between wrinkling λ and

glassy film thickness h in this sinusoidal regime, it is possible to interpret the data in terms of skin growth kinetics. Both the slope and intercept of the logarithmic relationship vary with plasma frequency and inspection of eq. (8) thus indicates that μ and K , the effective attenuation parameter and rate constant, depend on frequency at constant pressure. Frontal vitrification is faster with a MHz plasma (yielding a lower μ) but has a slightly longer induction time/dose (corresponding to a lower K), with respect to a kHz plasma under the same conditions (of gas composition, pressure and dose).

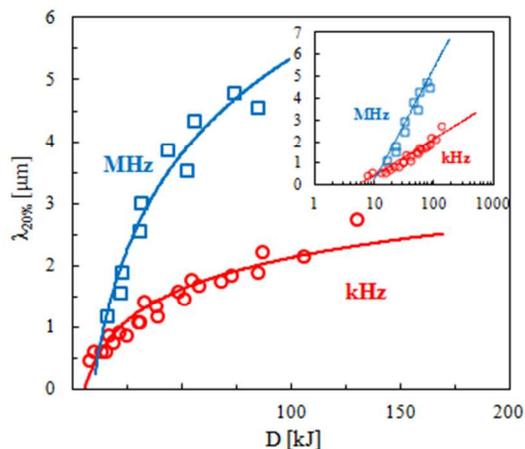
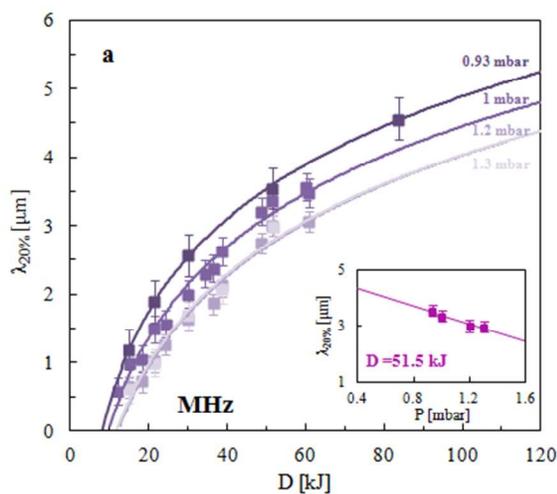


Figure 5: Wrinkling wavelength (λ) of PDMS samples strained by $\epsilon_{\text{prestrain}}=20\%$ and exposed to kHz and MHz air plasmas, at constant pressure $P=0.93$ mbar, as a function of plasma dose (D). All data in Fig. 4 collapse into single master curves for the two frequencies, well described by a logarithmic dependence. The inset shows the results in a lin-log scale.



3.1.2 Effect of pressure

We next consider the effect of gas pressure, within 0.66-1.5 mbar, on the frontal vitrification kinetics induced by air plasma. The experimental results are shown in Fig. 6 and demonstrate that increasing pressure P decreases λ at constant plasma dose (illustrated in inset, for both MHz and kHz frequencies). In order to rationalise the results, we recall again the proportionality of λ and h (eqs. 1,4) in this regime to conclude that an increase in plasma pressure slows down the kinetics of the oxidation reaction. The result is not unexpected: as the collision rate in the plasma increases with pressure the molecular mean free path decreases, which in turn compromises the ionisation process.⁴⁴ Since the oxidation reaction (leading to the formation of the glassy layer) proceeds with a radical mechanism, a decrease in ionization rate at higher pressures should thus slow down conversion and thus yield thinner glassy films (and lower wrinkling λ).

Inspired by the successful rescaling of wrinkling data at differing powers p and exposure times t in terms of a plasma dose D , we evaluated various rescaling variables involving pressure P . For this purpose, we fit all data according to our eq. (8) at the various gas P , yielding the results shown in Fig. 7. Evidently μ (which sets the log slope) remains unchanged with P . However, K (or KI_0), which sets the intercept, is found to decrease with P , as expected for the discussion above. Since ϕc is constant (≈ 0.06) and $KI_0 \sim 1/P$ within this (narrow) P range (cf. Fig. 7), one might expect from eq. (8) that approximately $h \propto \ln(D/P)$. Indeed, we find that, within this P range, all data collapses when plotted as a function of D/P , as shown in Fig. 8. This correlation provides useful guidance in designing PDMS surface A and λ via plasma oxidation.

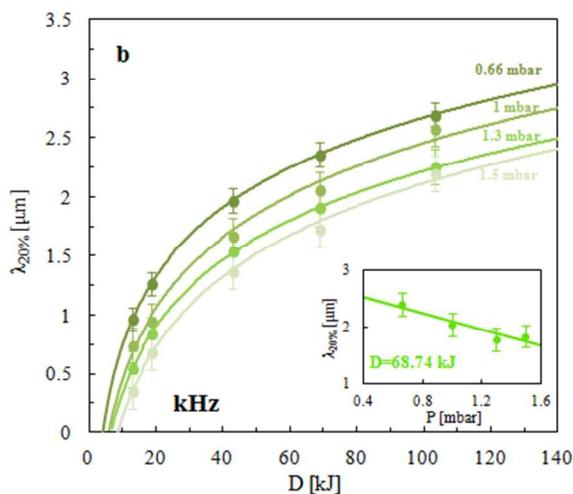


Figure 6: Sinusoidal wrinkle periodicity (λ) at 20% prestrain as a function of plasma dose (D) for different values of air pressure (P) for a (a) kHz and a (b) MHz plasma. The lines are logarithmic fits. The inset shows dependence of λ with P at a fixed dose, which is found to be linear within this range.

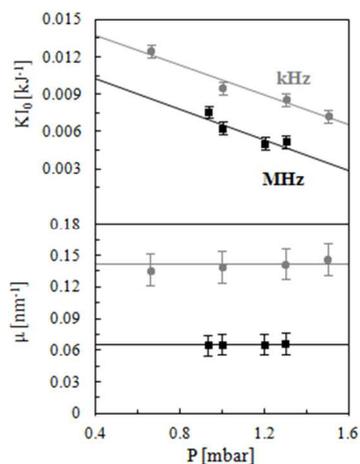


Figure 7: Pressure dependence of model parameters KI_0 and μ for all air plasma exposure doses and different frequencies. The parameters were computed from eq. (8) taking $\phi_c=0.06$. The pressure dependence of KI_0 is equally well described by $\sim 1/P$ or linearly with $-P$, within this (relatively narrow) range.

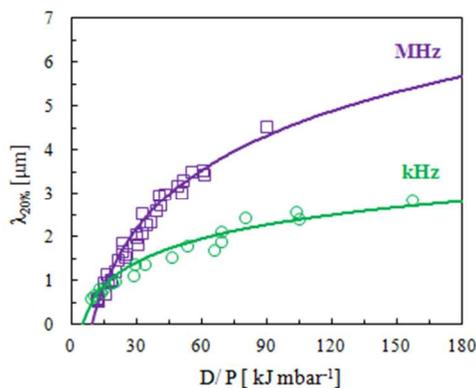


Figure 8: Wrinkling wavelength (λ) of PDMS samples strained by $\epsilon_{prestrain}=20\%$ and oxidized by kHz and MHz air plasmas, as a function of the ratio of plasma dose/air pressure (D/P). The curves in Fig. 6 collapse further into single master curves for each frequency. Lines are fits to eq. (9).

3.1.3 Film formation and propagation

During the early stages of plasma oxidation and accompanying glassy film formation, we have found^{4,5} that both the skin modulus \bar{E}_f and thickness h increase during O_2 plasma exposure, which we term the *skin formation* stage. This stage is particularly important as the modulus mismatch between skin and substrate continuously increases, which in turn sets ϵ_c required for wrinkling to take place, which decreases following eq. (3). Limited by the material elongation at break (ϵ_{max}), the combination of the two effects results in a minimum λ achievable⁵ at constant ϵ . At the end of the film formation stage, as the surface glassy layer densifies^{22, 46}, it eventually reaches full conversion or *saturation*, corresponding to $\phi(z=0, t>t_s)=1$, in the context of our model where t_s is a saturation time (or corresponding dose D_s). Beyond t_s the film large propagates with constant modulus and a sharp interfacial profile into the unconverted PDMS bulk layer, and we refer to this stage as the *film*

propagation stage. The transition between film formation and propagation is manifested in two ways: (i) a discontinuity (i.e. a ‘kink’) appears in the logarithmic dependence of $\lambda(D)$ and (ii) the aspect ratio of wrinkling profiles A/λ becomes insensitive to D , as the modulus \bar{E}_f ceases to change and only h increases (which is cancelled by taking A/λ).

In order to examine whether this physical picture applies for air plasma oxidation and to evaluate the effect of pressure in the skin formation stage, we investigate very low air plasma doses, $D < D_s$. Previously,⁵ with an O_2 kHz plasma we found an effective $\lambda_{min} \approx 140$ nm with a high ϵ of 200% (near PDMS failure at ϵ_{max} , and thus compromising reproducibility). Our skin thickness estimates of $h \approx 5$ –50 nm agree broadly with various previous measurements^{22–26, 46} of plasma, UV, UVO and corona discharge, which we have discussed earlier.⁵ Our hypothesis is that by increasing air pressure, one might be able to access even lower wrinkling wavelengths, desirable for a range of nanoscale applications. The experimental results for λ obtained at low D for two different pressures in a MHz air plasma are shown in Fig. 9. In line with our observations in the propagation regime (Figs. 6 and 7), increasing pressure P also decreases λ in the film formation stage. Employing even a modest strain of $\epsilon_{prestrain}=20\%$ and $P=1.2$ mbar, we readily obtain a wrinkle periodicity of $\lambda \approx 100$ nm (Supporting Information, Fig. S5), below what was achieved previously⁵ and indicating that tuning plasma pressure (as well as further increasing ϵ , while decreasing D) are effective routes to obtaining sub-100 nm wrinkling wavelengths. This is one of the main results of our paper.

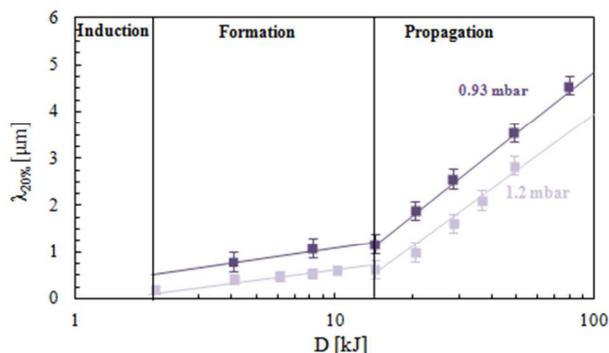


Figure 9: Wavelength (λ) of wrinkled PDMS samples prestrained by $\epsilon_{prestrain}=20\%$ and treated with MHz plasma, as a function of dose (D) for two values of air pressure $P=1.2$ mbar and $P=0.93$ mbar. The transition from film formation to propagation stages, defined by the saturation time/dose when the glassy skin reaches full conversion at the surface, is visible by a kink on the logarithmic propagation kinetics.

3.2 Wrinkling amplitude during film propagation

We next consider the effect of plasma pressure P on the wrinkling amplitude A . Our results so far indicate that the plasma processing parameters effectively tune the kinetics of glassy film formation and, in the propagation regime, this corresponds to changing $h(t)$ as modulus \bar{E}_f is expected to remain largely constant. Since we find that increasing P decreases λ (and thus h), as shown in Figs. 6 and 7, we expect the same linear dependence of wrinkling amplitude A with P , in accordance to eqs. (2,5). The experimental data for A achieved in for PDMS exposed to a MHz air plasma at constant $\epsilon_{prestrain}=20\%$ are shown in Fig. 10, confirming our expectation.

Inspection of eqs. (1,2) and (4,5) indicates that, at *constant* strain ε , aspect ratio A/λ should only depend on the plane strain moduli of the film and PDMS substrate. If \bar{E}_f remains constant and only the glassy skin thickness h changes with time t , characteristic of the *propagation* regime, then the aspect ratio A/λ should be constant with pressure. The inset of Fig. 10 reveals that, within measurement uncertainty, A/λ does remain constant, consolidating the conclusion that, in the propagation regime, the plasma processing parameters – and in particular P – provide an effective way to tune $h(t)$ frontal kinetics, as described in Fig. 7 (for λ).

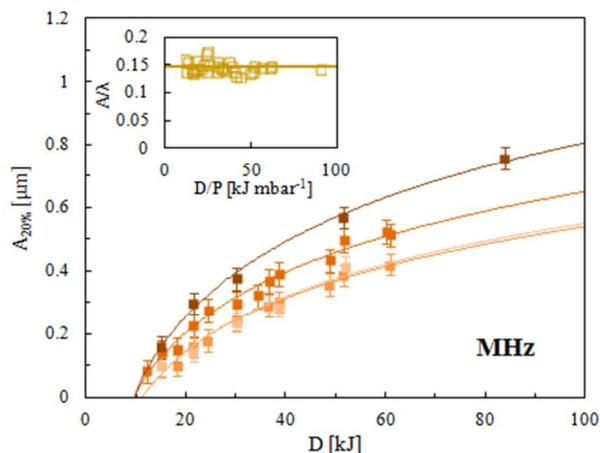


Figure 10: Sinusoidal wrinkling amplitude (A) as a function of plasma dose (D) for different values of air pressure (P) within a MHz plasma, during the film propagation stage. A constant value of $\varepsilon_{\text{prestrain}}=20\%$ was utilized to stretch the PDMS samples prior to plasma exposure. As in previous figures, the lines are logarithmic fits to eqs. (5,8). The inset shows the aspect ratio A/λ as a function of D/P which is found to remain constant within measurement uncertainty.

3.3 Effect of gas composition on frontal glass formation kinetics

We finally quantify the effect of the ionizing gas composition on wrinkling profile λ and glassy film thickness h . The MHz plasma was operated with pure oxygen, air and an equimolar mixture of oxygen and nitrogen, at constant pressure $P=0.93$ mbar, and as a function of exposure dose D . Experimental results in the propagation regime are plotted in Fig. 11. We find that decreasing the concentration of oxygen results in slower log kinetics of glassy film formation $h(t)$. This behaviour is expected, since the oxidation reaction slows down, as concentration of active species decreases. Interestingly, as shown in inset, the model parameter μ appears insensitive to gas composition, while KI_0 increases linearly with O_2 content y_{O_2} . We have found above (section 3.1.2) that gas pressure P affected reaction kinetics KI_0 but not μ , which can be understood as an *attenuation* parameter and thus a material property. Only plasma frequency, MHz or kHz, was found to affect μ . We now find that the variation of KI_0 with both pressure P and y_{O_2} is linear within the range investigated and measurement uncertainty.

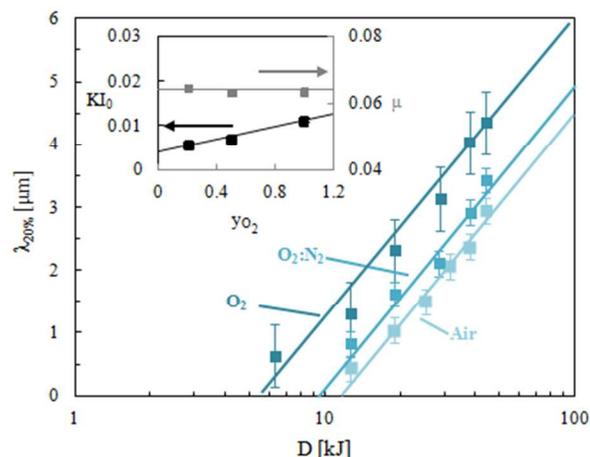


Figure 11: Wrinkling wavelength (λ) of PDMS samples prestrained by $\varepsilon_{\text{prestrain}}=20\%$ and exposed to a MHz plasma, as a function of dose (D) for different ionizing gases at constant pressure $P=0.93$ mbar. The inset shows the behaviour of the parameters of eq. (8) with the oxygen molar fraction in the gas. These were obtained through a regression using the values of h computed through (1) and taking $\phi_c=0.06$.

In practical terms, both increasing P and reducing O_2 content is found to result in slower glass formation kinetics and thus smaller λ and thinner glassy films h , under otherwise identical conditions. During the film propagation stage, a rather simple physical picture emerges in that eq. (8) holds and $h(t)$ is finely tuned by P , t and p (via D), O_2 composition and plasma frequency. The model parameters for λ and h are summarised in Table 1. (Graphical results for $h(t)$ are computed in Supporting Information, Figs. S1 and S2).

$$h[\text{nm}] = \frac{\ln(D)}{\mu} - \ln\left(\frac{1}{KI_0} \ln\left(\frac{1}{1-\phi_c}\right)\right)$$

f	μ	KI_0
13.6 MHz	0.065 ± 0.002	$0.0072y_{O_2} - 0.0061P + 0.01053$

40 kHz	0.136 ± 0.006	$0.0072y_{O_2} - 0.0061P + 0.0147$
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$$\lambda_{20\%} [\mu\text{m}] = \frac{\ln(D)}{a} + b$$

f	a	b
13.6 MHz	0.51 ± 0.02	$1.68y_{O_2} - 2.02P - 2.81$
40 kHz	1.07 ± 0.4	$1.04y_{O_2} - 1.255P - 2.42$

Table 1: Plasma-induced frontal vitrification kinetics of h and $\lambda_{20\%}$ with dose D , following eq. (8) and eqs. (1,2). Our minimal model provides a self-consistent description of all data in terms of plasma frequency (kHz, MHz), pressure P , oxygen content y_{O_2} of the ionizing gas, and exposure time t and power p , via the dose D [kJ].

4 Conclusions

We have investigated the mechanism and kinetics of glassy film formation on PDMS by plasma oxidation, focusing on the resulting wrinkling profiles, wavelength λ and amplitude A , attainable by uniaxial strain. An unprecedented range of experimental processing variables was considered: exposure time t , power p , gas pressure P , O₂ composition y_{O_2} , and plasma induction frequency (kHz, MHz). Under all conditions, the surface oxidation, densification and glass formation of PDMS induced by plasma is well described by a planar frontal process, in which the glassy skin thickness h grows logarithmically with time (or dose), and more generally with D/P . Our minimal frontal model captures the key aspects of the process and three stages, namely induction, film formation and propagation, can be identified.

Our model allows us to extract kinetic parameters μ and KI_0 that are useful in describing the frontal process and provide us with two main conclusions. During the film propagation stage, the skin modulus \bar{E}_f remains unchanged and only the film thickness h evolves (logarithmically) during exposure, as seen by the constant aspect ratio A/λ and continuous log kinetics. The propagation kinetics are straightforwardly tuned by the plasma processing parameters. We find that increasing O₂ content or decreasing P , accelerate kinetics KI_0 , while the plasma frequency alone (MHz or KHz) defines μ , an effective attenuation parameter. Equipped with this knowledge, designing a wrinkled sinusoidal topography with prescribed A and λ becomes trivial in the propagation stage.

In the early stages of plasma exposure, the PDMS surface simultaneously increases in modulus \bar{E}_f and thickness h ⁵. This means within a range of low plasma exposure dose, the bilayer modulus contrast is too small, and no wrinkling is observed up to large strains ε (until the material fails at ε_{max}). We refer to this as the induction stage. Beyond this point, wrinkling can be practically attained but the coupling of increase in modulus \bar{E}_f and thickness h with exposure defines an effective minimum wrinkling wavelength λ_{min} possible. With an O₂ kHz plasma, we found that value to be $\lambda_{min} \approx 140$ nm with a large prestrain of $\varepsilon_{prestrain} \approx 200\%$ which bring PDMS close to failure and compromises the reproducibility of the approach. In this work, we find that the film formation stage is also non-trivially affected by plasma processing parameters, such that a lower $\lambda_{min} \approx 100$ nm is readily attained, at much lower strains ($\varepsilon_{prestrain} \approx 20\%$ demonstrated) using air, at a higher $P=1.2$ mbar with a MHz plasma. These findings open an attractive and facile route for sub-100 nm PDMS wrinkling with plasma exposure by further optimisation of plasma exposure and strain parameters, by decreasing O₂ content, increasing P , decreasing D (via p and t) and increasing $\varepsilon_{prestrain}$ to ensure that ε_c is exceeded.

While only uniaxial strain fields are investigated in the present work, we and others have demonstrated multiaxial mechanical strain fields, and multi-step wrinkling processes^{4, 18, 32} to controllably extend the morphologies attainable in 2D. Inexpensive, uniform, large-area, non-lithographic wrinkling at the nanoscale is attractive for a range

of patterning applications, ranging from wetting and spreading of fluids and nanofluidics, to the directed assembly of complex fluids and colloids, as well as contact printing.

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