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ARTICLE

Simultaneous Preparation of Nano Silica and Iron Oxide from Palm Oil Fuel Ash and Thermokinetics of Template Removal

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Abstract Nanomaterials have potential applications in the fields of catalysis, drug delivery, nanocomposites, and nanofluids. This study suggests a method for simultaneous preparation of nano silica and iron oxide from palm oil fuel ash (POFA). First, POFA was leached out with H₂SO₄ followed by alkali (NaOH) leaching. Basification (pH=14) of the filtrate of the first leaching process produced iron oxide, while acidification of the alkali leachate produced nano silica. Addition of polymeric surfactant polyethylene glycol (PEG MW 20,000) resulted in deagglomeration of silica nanoparticles. Silica nanoparticles with sizes in the range of 20–80 nm, surface area of 326 m²/g, and pore diameter of 8.2 nm were obtained. Thermokinetic and thermodynamic studies of template (PEG) removal from the silica matrix were performed using the Kissinger and Ozawa methods based on model-free kinetics. The activation energy of PEG decreased from 330 KJ.mol⁻¹ to 140 KJ.mol⁻¹ when it was used as a template; this result demonstrates the lack of chemical bonding between the surfactant and silica. The findings are supported by the Fourier-transform infrared spectra of the PEG-silica composites.

Introduction:

Bioenergy, which is energy obtained from biomass, has been emphasized in modern research as a substitute for fossil fuel-based energy; biofuels offer the advantages of renewability and green combustion. Currently, the contributions of bio energy in terms of heat, fuels, and power are estimated to be as high as 15% of the total global power supply. Other projections estimate that 33%–50% of the world's energy demands will be fulfilled by biomass by the middle of the 21st century. Generation of 476 million tons of biomass ash (BA) has been forecasted as biomass combustion becomes one of the major methods used for energy production¹. Malaysia, as the second-largest producer of palm oil in the world, has focused on developing bioenergy from palm oil mill wastes. Other than biofuels derived from palm oil, one of the mostly utilized process include power plants, based on burning of palm tree residues². Solid ultrafine ash obtained from combustion of palm kernels and bunches in palm oil mills at temperatures of 800–1000 °C is called palm oil fuel ash (POFA)³. As palm oil production increases, a gradual increase in POFA production may be expected. POFA production in 2010 was reportedly as high as 4 million tons compared with the 3 million tons produced in 2007^{2, 4}. POFA, like other BAs, is composed mainly of inorganic oxides, along with unburnt and semi-burnt organic materials that depend on the palm residue and combustion conditions inside the boiler³. Ecologically benign disposal and valuable applications are two main considerations

for POFA and other BAs. Dumping in lowlands, as a common practice, has received criticism from local communities and ecologists because of the persistence and resistance to decomposition of POFA. Moreover, increasing prices of solid waste disposal have emphasized the importance of the need to transform POFA into valuable end-products and processes for application in various industries⁵.

POFA has recently been applied as an effective adsorbent for purification of polluted water and air; significant adsorption of different dyes, for example, has been achieved using modified POFA with adsorption capacities of as high as 400.01 and 423.5 mg/g^{6, 7}. Introduction of POFA as an auxiliary cementing material has resulted in reductions in water permeability and porosity of concrete, thereby leading to substantial corrosion resistance^{8, 9}. Novel POFA-based geopolymers were recently introduced as potential green cementing materials. POFA utilization as a primary raw material for geopolymerization is hindered by the high SiO₂ and very low Al₂O₃ contents of the material^{2, 4}.

The emergence of nano- and mesoporous silica materials and their manipulation for use in adsorption, catalysis, drug delivery, sensors, nano casting templates, and sustainable raw materials for the synthesis of nanostructured silicon for Li-ion battery anodes, among others, have led researchers to explore newer and cheaper resources of silica¹⁰. Alkyl silicates, e.g., tetraethyl orthosilicate (TEOS), are the most widely used precursors utilized for nano silica synthesis, but they are expensive and release organic alcohols as by-products¹¹. As

well, the environmentally hazardous process of sodium silicate synthesis limits its application as precursor for SiO₂ synthesis. Thus, researchers have sought to determine new sustainable materials for silica preparation¹². Rice husk ash was recently found to be a sustainable source of silica because it is composed of highly reactive amorphous silica^{13, 14}. With a chemistry similar to that of rice husk ash, POFA may potentially be utilized as a sustainable source of nano silica and subsequent silicon nanostructures. Besides nano silica, POFA can also be used for extracting oxides of calcium, iron, and aluminum because it contains considerable amounts of these oxides. Compared with rice husk ash, however, the potential application of POFA as a source material for synthesis of valuable nano oxides has not received adequate attention from the research community¹².

In this work, issues related to the environmental nuisance presented by POFA are addressed by synthesizing silica nanoparticles and iron oxide through the template-free and polyethylene glycol (PEG-20000)-templating methods. This study also discusses the thermokinetics and thermodynamics of the template removal from the silica-PEG complex. Although PEG has been reported in previous literature as a valuable templating agent for high-surface area silica synthesis, to the best of our knowledge, thermokinetic and thermodynamic studies of its removal have yet to be published¹⁵.

Thermally treated POFA was subjected to acid leaching followed by alkali leaching. The filtrate of the first leaching process was converted into iron oxide, while the second filtrate was utilized to produce silica nanoparticles. Products were confirmed by scanning electron microscopy (SEM) and transmission electron microscopy (TEM), X-rays diffraction (XRD) and infra-red spectroscopy. The thermal kinetics and thermodynamics of decomposition of PEG were investigated using model-free kinetics methods based on DTG technique.

Experimental

Materials

Grayish POFA was collected from a local Malaysian power plant, and its chemical composition was determined by X-ray fluorescence spectrophotometry (XRF), as shown in Table 1. NaOH (99%, Merck Millipore) pellets were used to prepare NaOH solutions using deionized water; these solutions were standardized against oxalic acid. Alkali solutions were stored in polyethylene containers to avoid glass contamination. The nitric acid (68%) and sulfuric acid (98%) used in this study were procured from Merck Millipore, Malaysia. PEG (MW 20,000, Merck Millipore) was utilized as structure-directing group (templating agent).

Methods

Pretreatment of POFA

POFA was screened through a 150 µm sieve using a vibrating sieve shaker (AS 200 basic, RETSCH, Germany) to separate larger particles from POFA. To remove unburnt and unspent

biomass residue, POFA was heated at 600°C for 6 h in a chamber furnace (Protherm, Turkey). The resultant POFA was used as a precursor for the extraction of iron and silicon oxide.

Table 1 XRF analysis of POFA

SiO ₂	CaO	Al ₂ O ₃	K ₂ O	Fe ₂ O ₃	MgO	P ₂ O ₅	Minor Components	Loss on ignition
55	5.5	5.4	5.4	4.7	3.5	3.4	1.1	16

Preparation of Iron oxide

To synthesize iron oxide, POFA was treated with H₂SO₄ to leach out acid-soluble components for a designated time at a certain temperature and the resulting filtrate was precipitated in alkali (NaOH). To find out the suitable acid treatment conditions, five acid concentrations, i.e., 1, 2, 3, 4, and 5 N, five reaction times, i.e., 1, 2, 3, 4, and 5 h, and four reaction temperatures, i.e., 30, 60, 90, and 100°C were investigated. In this experiment POFA (15 g) was magnetically mixed with H₂SO₄ (designated conc.) in a round bottom flask equipped with a reflux condenser at 500 rotations per minute (rpm) for the designated time and temperature. The POFA-acid mixture was filtered, and the filtrate was used for preparation of iron oxide. The residue, also called acid-leached POFA (APOFA), was used for nano silica synthesis discussed in next section (Fig. 1). Acidic filtrate was added to an excess of NaOH (2 N) and a dark brown suspension was obtained. The suspension was washed in the centrifuge (biofuge, Thermo Scientific, US) at 6000 rpm for 5 minutes with water (4×40 mL) to ensure complete removal of unreacted alkali and water soluble salts. The brown powder formed, after drying at 110°C in an oven, was sintered at 500 °C in the furnace for 3 h leading to formation of iron oxide, and the resultant material was characterized through various analytical techniques.

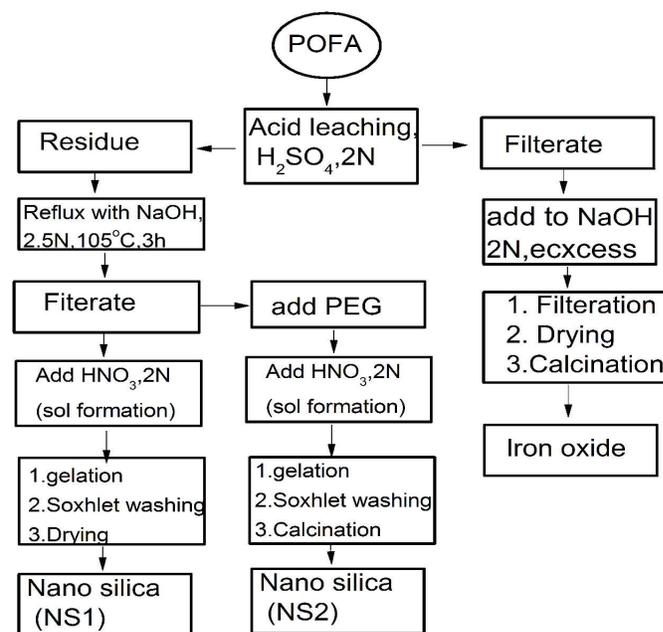


Figure 1 Protocol for the synthesis of iron oxide and silica nanoparticles from POFA.

Synthesis of nano silica

Alkali leaching of amorphous silica from POFA and followed by acid precipitation was used for silica extraction^{12, 16}. To investigate the reaction parameters giving maximum yield, three variables, namely, alkali concentration (1, 2, 3, 4, and 5 N), reaction time (30, 60, 120, 180, and 240 min), and reaction temperature (25, 50, 70, 105, 110 °C), were used in this study, using modified factorial design where one variable was varied whereas the other two variables were kept constant.

In this experiment, APOFA (10 g) was treated with NaOH (80 mL) of known normality for a certain time and temperature in a round bottom flask with constant stirring at 200 rpm. After reaction, the sample was hot-filtered by suction filtration and rinsed with deionized water (3 × 40 mL). HNO₃ (2 M) was added dropwise to the filtrate with continuous stirring at 200 rpm until formation of a white silica sol. This sol was aged for 24 h at room temperature and then washed with HNO₃ (0.05 N) in a Soxhlet apparatus for 60 min. The silica formed was designated as NS1 and was characterized using analytical techniques.

In another experiment, PEG (2 g) was dissolved in the hot alkaline filtrate with vigorous stirring and then cooled to room temperature (25 °C). HNO₃ (2 M) was added dropwise to the filtrate, resulting in the formation of a nano silica sol. Salt-free silica sol was dried overnight at 60°C and designated as PEG-SiO₂. The dried, white, amorphous powder formed was sintered at 600 °C for 6 h in a furnace (Protherm, Turkey) to remove PEG leading to the formation of nano silica. The nano silica formed through this procedure was designated as NS2 and analysed through various instrumental techniques

Characterization

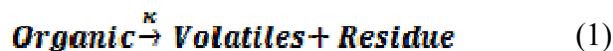
Infrared analyses of the raw materials and end-products were performed on a Spectrum One instrument (Perkin Elmer, USA) at a scanning rate of 32scans/sample, using the KBr pellet method. To investigate the crystallinity of the powdered material, X-ray diffraction (XRD) was carried out on an X-ray diffractometer (D8 Advance, Bruker, Germany) at a scanning rate of 2°/min over the 2θ range of 2°–80° using a Cu anode. To determine the surface area pore diameter and pore volume of NS1, NS2, Iron oxide and POFA, N₂ adsorption/desorption isotherms were measured by a surface area and porosity analyzer (ASAP, 2020, Micromeritics).

The morphology and microstructure of the iron oxide and nano silica were investigated using a field emission scanning electron microscope (Zeiss Supra 55VP, Germany). Dry powder was fixed onto aluminum stub using carbon tape and was observed under electron microscope at different magnifications. To determine the exact size of grains and their boundaries, a transmission electron microscope (Zeiss Libra 200FE, Germany) was used at a reduced pressure of 7 mbar. Prior to TEM analysis, samples were sonicated in isobutanol for 30 min. Thermal analysis of the pure polymer (PEG-20000) and PEG-SiO₂ were carried out on a simultaneous thermogravimetric analyser (STA 6000, Perkin Elmer, USA) in

the temperature range of 50–800 °C. Analyses were conducted at heating rates of 15, 20, 30 and 40 °C.min⁻¹ under an inert atmosphere (N₂). Thermograms (TGs) and corresponding derivative (DTG) curves were plotted using built-in software. The variations of the thermal profile with heating rates were used to investigate the kinetics and thermodynamics of the template removal from PEG-SiO₂.

Kinetic and thermodynamic studies

Model-free kinetic methods were used to calculate the activation energy (E_a) and pre-exponential factor (A) of the pyrolysis of PEG and PEG-SiO₂. Several researchers have reported kinetics studies of thermal decomposition using TGA and DTG data¹⁷⁻¹⁹. A simple equation that can describe the thermal decomposition of an organic material is:



Here, volatiles represent tar and gaseous products while k represents the rate of reaction, which may be calculated using the Arrhenius equation:

$$k = Ae^{\left(\frac{-E_a}{RT}\right)} \quad (2)$$

Whereas E_a is the activation energy (kJ.mol⁻¹), T is the absolute temperature, R is the ideal gas constant (8.314 J.K⁻¹.mol⁻¹) and A represents the pre-exponential factor (min⁻¹). The rate of transformation from solid state to volatile product is described by the following expression:

$$\frac{d\alpha}{dt} = k(T)f(\alpha) \quad (3)$$

whereas α , t , $k(T)$, and $f(\alpha)$ represent the degree of reactant conversion, reaction time, rate constant, and reaction model, respectively. Conversion, α , reflects the normalized form of weight loss data of the decomposed sample and is defined as follows:

$$\alpha = \frac{m_i - m_a}{m_i - m_f} \quad (4)$$

Whereas m_i is the initial mass of the sample, m_a is the actual mass, and m_f is the mass after pyrolysis. Combination of the Eq. (3) and (4) give a fundamental equation (5) that can be used to calculate kinetic parameters on the basis of TGA results.

$$\frac{d\alpha}{dt} = A \cdot f(\alpha) \cdot e^{-\frac{E_a}{RT}} \quad (5)$$

The conversion function $f(\alpha)$ for a solid-state material depends on the reaction mechanism and can generally be written as follows:

$$f(\alpha) = \alpha^m(1-\alpha)^n[-\ln(1-\alpha)]^p \quad (6)$$

Whereas m , n , and p are empirically obtained exponential factors, one of which must always be zero. Combination of different values of these exponential factors is helpful in describing most probable mechanisms²⁰.

When the temperature increases at a constant rate, β can be defined as the heating rate:

$$\beta = \frac{dT}{dt} \quad (7)$$

Eq. (5) can be written as;

$$\frac{d\alpha}{dT} = \frac{A}{\beta} \cdot f(\alpha) \cdot e^{(-E_a/RT)} \quad (8)$$

Eq. 8 shows the rate of degradation of a substance as a function of temperature. This equation is a fundamental equation and used for calculation of kinetics parameters. In this work, kinetic parameters were obtained from the non-isothermal DTG technique by using the Kissinger (ASTM E-698) and Ozawa methods. These methods require multiple TGA runs with varying β to calculate the kinetic parameters of a reaction without prior knowledge of the reaction mechanism.

Kissinger method (ASTM E-698)

Kissinger developed a model-free, non-isothermal method to calculate the E_a and $\ln A$ for a thermal conversion using DTG peaks' temperatures. This method allows calculation of E_a and $\ln A$ from a plot of $\ln(\beta/T_m^2)$ against $1000/T_m$ by using Eq. 9 for a series of experiments with different β , where T_m is the peak temperature of the DTG curve representing maximum conversion rate²¹;

$$\ln\left(\frac{\beta}{T_m^2}\right) = \ln\left(\frac{AR}{E}\right) - \frac{E}{RT_m} \quad (9)$$

E_a can be calculated from the slope of the plot, which is equal to $-E_a/R$, and A can be calculated from the intercept using Eq. 10.

$$A = \frac{E}{R} \cdot \exp(i) \quad (10)$$

Here, "i" represents the intercept of the graph.

Ozawa method

Similar to the Kissinger method, Ozawa proposed another method to calculate thermokinetics parameters of thermal conversion²². Although this method is an integral one, but it can be applied to DTG curves²³. In this method, E_a and A are calculated from the slope and intercept of the plot of $\ln \beta$ versus $1000/T$ using Eq. (11), respectively.

$$\ln(\beta) = \ln\left(\frac{0.0484AE_a}{R \cdot g(\alpha)}\right) - 1.0516 \frac{E_a}{RT_m} \quad (11)$$

Whereas $g(\alpha)$ is constant at a given value of conversion (α) and represents the reaction mechanism. The value of $g(\alpha)$ is unity for uni molecular reactions and can be calculated using the Coats-Redfern model²⁴.

Thermodynamic study

The correlation between kinetic and thermodynamic parameters results from the combination of the Arrhenius equation with Eyring or Wertera and Zenera laws related to the temperature dependence of the rate constant $k(T)$ as given in Eq.(12).

$$k(T) = \frac{k_B}{h} T e^{[-\frac{\Delta G}{RT}]} \quad (12)$$

Eq. (12) can be modified as

$$k(T) = B T e^{\frac{\Delta S}{R}} e^{-\frac{\Delta H}{RT}} \quad (13)$$

And

$$B = \frac{k_B}{h} = 0.20836 \cdot 10^{11} \text{ K}^{-1} \text{ s}^{-1} \quad (14)$$

Whereas k_B , h , and B are the Boltzmann constant, Plank constant, and vibration frequency, respectively. The thermodynamic parameters of the activated complex, including its free energy (ΔG), enthalpy (ΔH), and entropy (ΔS) of the process, may be calculated using the Eyring equations;

$$\Delta H = E_a - RT_p \quad (15)$$

$$\Delta S = R[\ln\left(\frac{hA\alpha}{k_B T_m}\right) - 1] \quad (16)$$

$$\Delta G = \Delta H - T_m \Delta S \quad (17)$$

Using Eq. 15–17, the thermodynamic parameters of the activated complex may be calculated using T_m in the DTG curve so that the values of ΔG , ΔH and ΔS are related to the highest rate process.

Results and Discussion

Iron oxide synthesis

POFA consists of considerable amount of crystalline silicon oxide along with amorphous oxides of silicon, iron, aluminum, and calcium. As such, preparation steps for extracting nano silica from POFA are not identical to those for extracting silica from rice husk and rice husk ash.

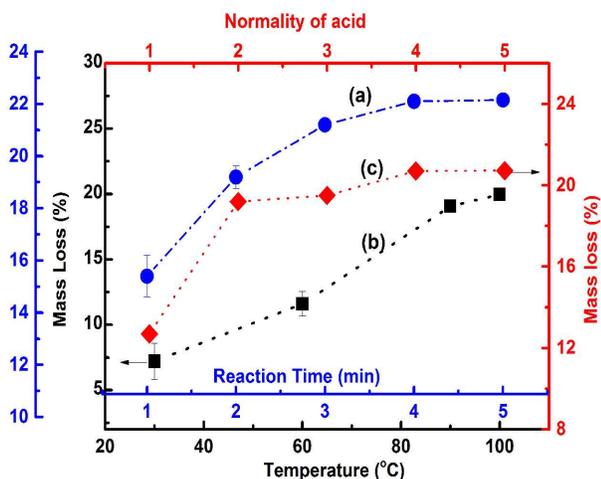


Figure 2 The mass loss profile of POFA during acid treatment. Curves a, b, and c show the extent of mass loss (%) of POFA with respect to time, temperature and acid concentration, respectively.

Acid treatment of sintered POFA leads to successive leaching of these metallic oxides leaving behind silicon oxide. Fig. 2 shows the acid leaching process of POFA at varying temperatures, reaction times, and acid concentrations.

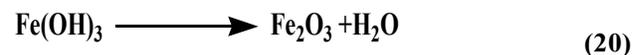
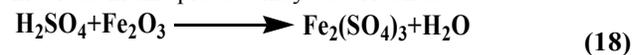
Curve "a" in Fig.2 represents the extent of mass loss of POFA with respect to time at 100°C with H₂SO₄(2N). The dissolution of POFA increases gradually with increase in reaction time until 3 hours and afterwards minor change were occurred in the dissolution profile of POFA. Therefore 3 hours reaction time was found most adequate for this process. Moreover, as shown in Fig. 2 (black line), the maximum amount of material was leached out of POFA at 100 °C when POFA was treated for 3 hours with 2N H₂SO₄. There was a gradual increase in POFA leaching with temperature and 100°C was considered as adequate as reflux started at that temperature.

Approximately, 19.5 of the POFA was extracted using 2 N H₂SO₄ at 100 °C for 3 h. An increase in mass loss of 1.5% was observed when acid strength was increased from 2 N to 5 N and other conditions were held constant i.e. reaction time of 3h and temperature of 100°C. A maximum mass loss of 21% was achieved within 3 h of refluxing at 100 °C with 5 N H₂SO₄. The acid solubility of POFA appeared to be a function of temperature, time and acid concentration. Thus, a temperature of 100 °C, acid concentration of 2 N, and reaction time of 3 h were determined as optimal reaction conditions.

Acid leachate was precipitated with NaOH (2 N) to obtain iron oxide. This method is pH-selective, and products of various compositions may be formed at different pH. At pH=14, the major products obtained from the leachate included iron oxides with impurities of aluminum and calcium oxide; by contrast, at pH below 10, the predominant product is aluminium oxide with some silica²⁵. As determined by EDX, there was 6.7 weight % Al which was removed by washing the product with alkaline waster.

In this method, acid dissolves the iron oxide along with aluminium and calcium oxides of POFA²⁵. Sodium hydroxide

reacts with iron salts leading to formation of iron hydroxide that is dehydrated at calcination forming iron oxide²⁶. The reactions involved in this process may be written as:



Synthesis of nano silica

Alkali dissolution of amorphous silica and subsequent precipitation with acid were performed for nano silica preparation²⁷. The effects of reaction time, temperature, and concentration of alkali solution on APOFA dissolution are shown in Fig. 3. Silica dissolution was observed to occur as a function of time, temperature, and alkali concentration. A gradual increase in silica dissolution was observed with increasing reaction time (curve a). A reaction time of 180 min was found to be the most productive, as no further increases in dissolution were observed even when the reaction time was extended to 240 min in 2.5 N NaOH at 105 °C as evident from Fig.3 (curve a).

The most suitable temperature for dissolution of APOFA was found to be 105 °C, and no further increase in the dissolution was observed even when temperature was increased to 110 °C in a 2.5N NaOH for 180 min reaction (curve b).

Moreover, improved dissolution was observed when the alkali concentration was increased from 1 N to 2.5 N. No further increase in dissolution was observed when the alkali concentration was further increased to 5 N at 105 °C and 180 min (curve c). The results thus far show that most of the amorphous silica is leached out by 2.5 N NaOH at 105°C and 180 min reaction time. Highly alkaline solutions were avoided being promoting corrosion of the glass reaction assemblies.

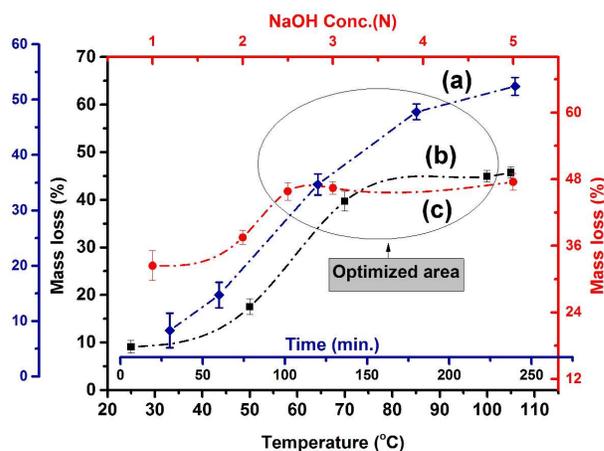


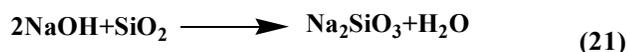
Figure 3 Graph of the extraction of silica from POFA using NaOH (aq). Curves a, b and c represent the variation in mass loss of APOFA with respect to time, temperature and NaOH concentration, respectively.

In this study, 2.5N NaOH, 180 minutes reaction time and 105°C reaction temperature were found the optimal conditions for the extraction of nano silica from POFA.

Alkali reacts with amorphous silica in POFA at a 2:1 molar ratio producing sodium silicate. Thus, the optimized values are in accordance with the stoichiometric composition of POFA.

Silica leaching is controlled by the diffusion of hydroxide in reactive grains and its absorption on solid surface. The diffusion of hydroxide enhances with the alkalinity and the solution's ionic strength²⁸.

Reactions taking place during this procedure may be written as follows:



FTIR analyses

FTIR analyses of the starting material and resulting products are shown in Fig. 4. Two peaks can be confirmed in all samples, i.e., absorption bands at ~3400 and ~1640 cm⁻¹, which correspond to asymmetric stretching and bending vibrations of O–H bonds attributed to either water or silanol groups²⁹. POFA showed peaks at 1432, 1106, 806, and 465 cm⁻¹. Similarly, most of these peaks were also produced by nano silicas, such as PEG-SiO₂, NS1, and NS2; these results show that POFA is mainly composed of silica consistent with XRF analysis (Table 1). The vibration band at 1432 cm⁻¹ represents the C–O bonds of calcite in the POFA²⁹.

Pure silica exhibited three typical peaks at around 1100, 800, and 450 cm⁻¹ because of asymmetric and symmetric stretching and rocking vibrations of siloxane (Si–O–Si) bonds³⁰. In PEG-SiO₂, small peaks at 2919 and 1432 cm⁻¹ attributed to C–H and C–O asymmetric stretching vibrations, respectively, were observed. These peaks confirm the presence of PEG within the silica matrix. The presence of O–H bands in PEG-SiO₂ reveals no chemical reaction between PEG and silanol groups. FTIR analyses confirmed the extraction of iron oxide and silica from POFA.

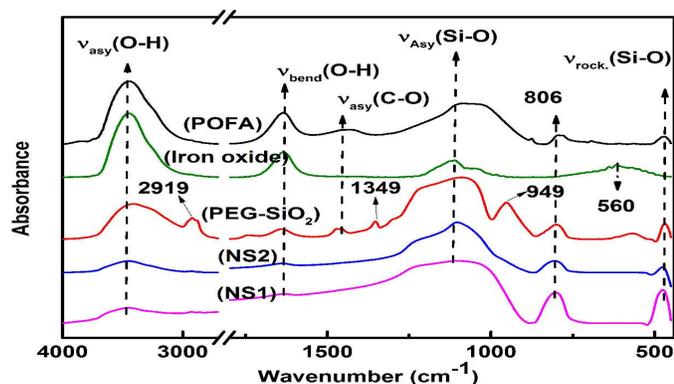


Figure 4 FTIR spectra of POFA, iron oxide, PEG-SiO₂, NS1, and NS2.

A peak at 560 nm in the iron oxide spectrum was attributed to Fe–O bending vibrations, which confirm the presence of hematite³⁰. Although FTIR analysis confirmed the extraction of silica and iron oxide from POFA, XRD is necessary to verify the amorphous nature of these products, as discussed in next section.

XRD analysis

To confirm the amorphous nature and phases of nano silica and iron oxide particles, XRD was employed. Fig. 5 presents diffractograms of POFA, iron oxide, NS1, and NS2. POFA showed a complex pattern that reflects its various components. The presence of quartzite was confirmed by peaks at 20.8°, 26.5°, 39.5°, 50.1°, and 59.9°, which are consistent with ICOD-00-046-1045. The presence of Fe₂O₃ (hematite) and calcite were confirmed by small peaks at 35.6° and 43.14°, consistent with ICOD-00-033-0664 and ICOD-00-005-0586, respectively. The presence of less intense peaks reveals trace amounts of these mineral phases. Quartz formation resulted from high-temperature (>700°C) burning of palm biomass wastes. XRD patterns of the nano silica (NS1 and NS2) showed broad peaks in the range of 20°–25° and centered at 23°; these peaks confirm the amorphous nature of the silica. Similar XRD patterns have been reported by several researchers as evidence of the amorphous nature of the nano silica^{31, 32}. Silica's amorphousity is controlled by the calcination temperature and time. Calcination at temperature higher than 700°C resulted in the conversion of amorphous silica to quartzite. Quartz is considered as a very stable and inactive phase of silica without clear applicability in composites, cements, concretes, geopolymers, or silicon synthesis^{10, 33}. The XRD pattern of iron oxide shows a broad hump in the region of 2θ=30°–40°, which represents the semi crystalline behavior of the material. The presence of peaks at 35.6°, 54.0°, and 63.1° confirms the presence of hematite in accordance with ICOD-00-033-0664.

The results thus far demonstrate that POFA has a multi components composition with a considerable amount of inactive quartzite. Nano silica formed with application of a templating agent showed XRD patterns similar to the silica obtained without the template; such results confirm that the

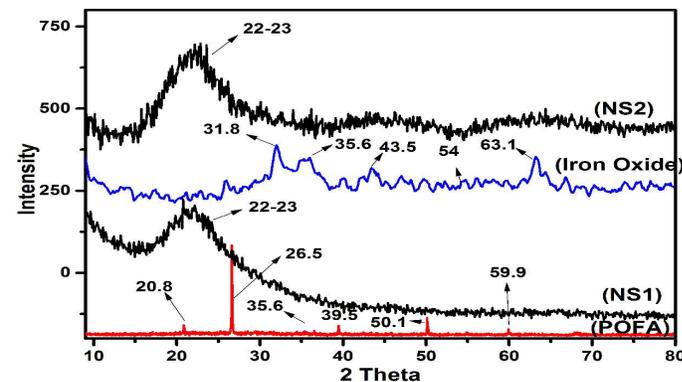


Figure 5 XRD patterns of Palm oil fuel ash, iron oxide, NS1 and NS2.

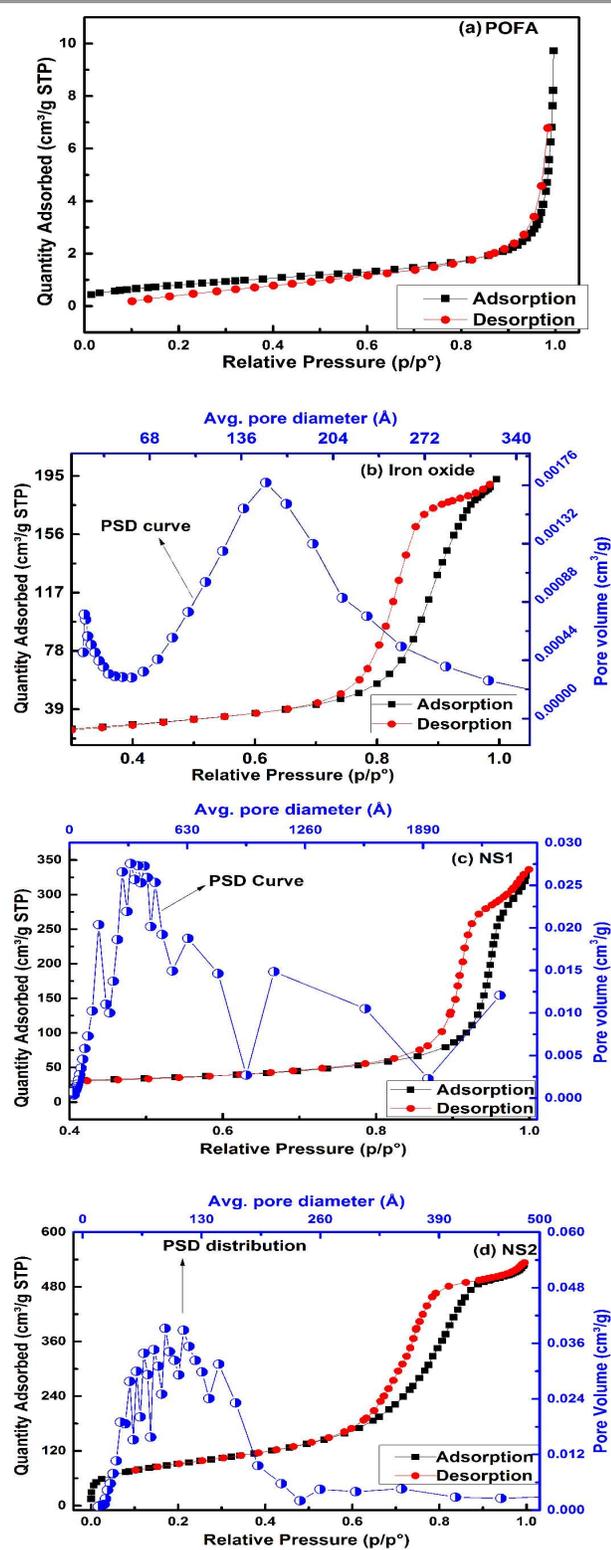


Figure 6 Nitrogen adsorption and desorption isotherms and pore size distribution analyses of (a) POFA, (b) iron oxide, (c) NS1, and (d) NS2.

PEG template does not affect the crystallinity of the resultant nano silica¹². Although XRD provided detailed information of

the phases present in the materials of interest, the patterns obtained do not explain the effects of PEG on the morphology and surface profile of nano silica. Surface profile and porosity analyses are discussed in next section.

Surface area and BET analysis

Figs. 6a–6c shows the N₂ adsorption/desorption isotherms of POFA, iron oxide, NS1, and NS2, respectively. The adsorption and desorption lines of POFA overlap to show a type I isotherm. Such behavior is produced by microporous materials³⁴. Iron oxide, NS1, and NS2 demonstrate hysteresis loops in their adsorption-desorption isotherms. These loops represent a type IV isotherm, which is a fingerprint of mesoporous materials. Therefore, the silica and iron oxide produced in this work are mesoporous in nature. The pore size distribution shifted to 8.2 nm when PEG-20000 was used as a templating agent as given in PSD curve in Fig 6c. It is reported that the amount of PEG used inversely influenced the mesopore size of the silica sample¹².

Table 2 presents the textural properties of the POFA and the nanoparticles. Surface area of NS2 reached to 326 m²/g when the PEG template was used compared to 87.6 m²/g for NS1, which is comparable with the reported surface areas (330–955 m²/g) of RH-based silicas^{1, 3–9}. The surface areas of iron oxide and NS1 are 81.2 and 87.6 m²/g respectively. The surface area of the mesoporous material depends on the pore size and pore volume. NS2 has a smaller pore size of 8.2 nm compared with NS1 (23.7 nm); this result reveals that PEG not only deagglomerates silica particles but also affects the pore size and volume of the resultant product. Thus, we can conclude that mesoporous silica and iron oxide with moderate surface areas can be prepared from POFA. PEG has previously been used as a mesopore-directing agent during synthesis of mesoporous silica, SBA 15 and other similar structures^{12, 32}.

Table 2. Textural properties of POFA, iron oxide, and nano silicas

	BET Surface area (m ² /g)	Pore volume (cm ³)	Pore diameter (nm)
POFA	2.86	0.014	16.8
NS1	87.6	0.48	23
NS-2	326	0.75	8.2
Iron Oxide	81.3	0.30	13.9

Microstructural analysis

FESEM micrographs of POFA, NS1, NS2, and iron oxide are presented in Figs. 7a–7d, respectively. POFA particles exhibit a porous surface comparable with those observed in the micrographs of fly ash and other industrial ashes⁵. The presence of small particles on POFA surface reflects the heterogeneous morphology and non-uniform particle size distribution observed when particle size exceed 100 μm; crushed shapes are formed at particle sizes below 20 μm⁵. The semi porous structure observed also suggests that POFA mostly consists of amorphous materials. Silica formed without addition of PEG (NS1) shows the formation of highly agglomerated

nanoparticles (Fig. 7b). In the area marked by a circle in this figure, the presence of small particles may be observed.

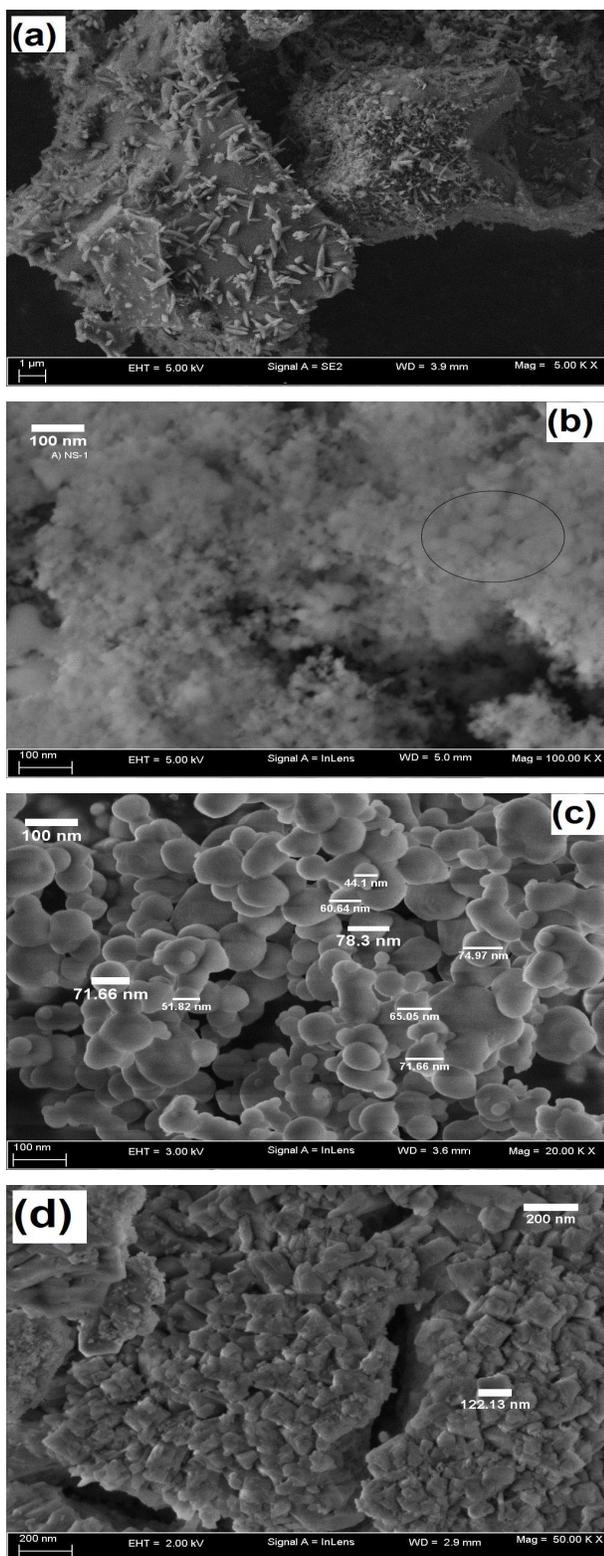


Figure 7 FESEM images of (a) POFA, (b) NS1, (d) NS2, and (c) iron oxide.

PEG resulted in deagglomeration, and well-defined spherical silica nanoparticles can be observed in Fig. 7c. These nanoparticles present a size distribution in the range of 50–80 nm. PEG decreased interparticle interactions between silica particles by networking with silanol functionalities, which promotes deagglomeration. Highly agglomerated and irregular-shaped iron oxide particles are shown in Fig. 7d. The size of the particles varied from 100–200 nm. As no surfactant was used during iron oxide synthesis and the reaction was carried out in aqueous and alkaline media, more extensive interparticle hydrogen bonding through surface hydroxyl groups may be expected.

Agglomeration in nanoparticles is caused by hydrogen-bonding interactions between the surface hydroxyl (silanol in the case of silica) groups of the neighboring particles³². Surfactants interact with these particles through their polar region by forming hydrogen bonds. Polymeric PEG consists of a long chain of hydrocarbons (non-polar region) attached to a hydroxyl group synonymous with alcohol (polar region).

The probable mechanism through which PEG interacts with silica particles is depicted in Fig. 8. Strong hydrogen bonding between neighbouring silica nanoparticles initially occurs. This phenomenon is further increased when water-based silicates are used as starting materials. PEG molecules have polar (O–H) and non-polar (alkyl) regions. The O–H groups of PEG are more polar than silanol groups and can initiate non-bonding interactions with silanol. Being larger in size, the PEG molecules prevent silica particles from approaching one another, thereby resulting in deagglomeration²⁷. Interactions between silica and PEG begin when PEG is dissolved in the sodium silicate solution; thus, the role of PEG is not limited to deagglomeration. Besides non-bonding interactions, it is reported that glycols react chemically with silica to yield a glycosilicate complex³⁵. These reactions usually take place when lower-molecular weight PEG is used. Increases in surface area and variations in porosity suggest the existence of molecular interactions in the solution.

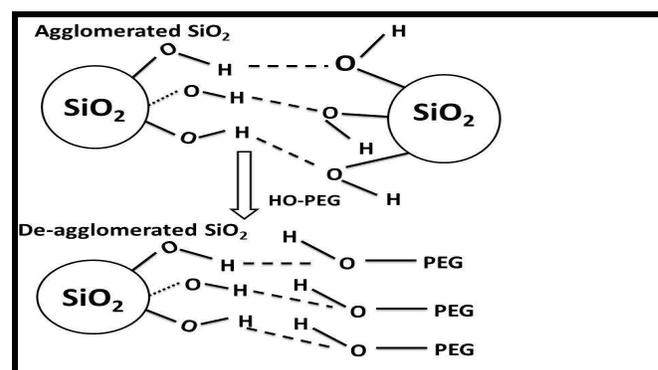


Figure 8 Mechanism of the deagglomeration of nano SiO_2 with the aid of PEG.

Transmission electron microscopy

TEM micrographs of NS-1, NS-2, and iron oxide are shown in Figs. 9a–9c. Both silica samples (NS1 and NS2) showed a spherical morphology, which indicates that particle morphology is not altered by addition of PEG and only agglomeration is restrained. The spherical shape of NS1 reveals that agglomerated silica has dimensions in the nanometer scale and a morphology identical to that of amorphous silica, as reported

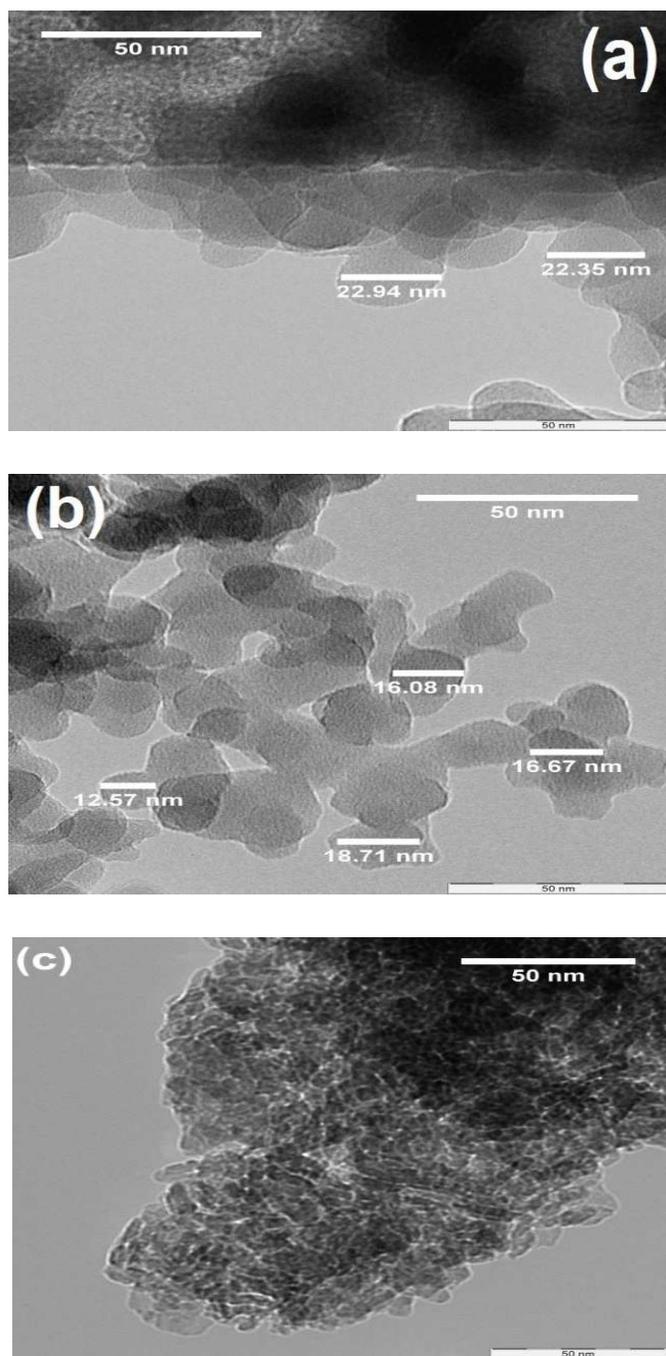


Figure 9 TEM analyses of (a) NS1, (b) NS2, and (c) iron oxide.

earlier¹⁶. Moreover the lesser agglomeration in the TEM images compared to FESEM images (Fig. 7b vs Fig.9a) are observed in NS1. This lesser agglomeration and formation of spherical silica particles may be caused by the sonication for thirty minutes in isobutanol. The particle size of NS1 was larger than that of NS2, which indicates that PEG effectively reduces particle sizes by decreasing interparticle interaction. Compared with the FESEM micrographs in Fig. 7c, the TEM images of NS2 show a finer particle size in the range of 12–20 nm. This phenomenon may be explained by considering the effects of dispersion and sonication of samples for 30 min. in isobutanol, which were performed prior to TEM analysis. Gao et. al reported that the particle size of silica nanoparticles extracted from oil shale ash and reported that agglomeration in silica was considerably reduced by sonication and azeotropic distillation with isobutanol³². Fig. 9(c) presents the TEM micrograph of iron oxide, which shows an angular morphology consistent with its FESEM micrograph (Fig. 9d). A similar degree of agglomeration and no considerable effect of sonication and dispersion in isobutanol were observed in the iron oxide sample. These results suggest that further decreases in size can be achieved by ultrasonication and application of different solvents as dispersant.

Thermal analysis produced reliable results of the amount of template in the nano silica matrix and is discussed in the next section¹².

Thermogravimetric analysis of PEG and PEG-SiO₂

TGA was utilized to understand the mechanism of interaction between PEG and silica as well as their thermal decomposition profile. Figs. 10a and 10b illustrate the TGA curves of pure PEG and PEG-SiO₂.

To determine the model-free kinetics, both samples were run at a minimum of three β . Pure PEG decomposed completely at 450 °C, and a single DTG peak (Fig. 10c) reflected uniform decomposition in a single step without intermediate stages. The decomposition pattern of PEG-SiO₂ is complex, and approximately 40% mass loss occurred at 600 °C; no further decomposition was observed when heating was increased to 800 °C. In the TGA and DTG curves of PEG-SiO₂ (Figs. 10b and 10d), four regions/peaks were observed. Peak “A” is located in the region of 100–150 °C and represents dehydration of surface water^{12, 36}. Peak “B” (240–260 °C) contributed 10% weight loss attributable to the release of silanol-bonded water; silanol-bonded water is generally stable and released at relatively higher temperatures. The third stage (Peak C) represents decomposition of PEG, as confirmed by comparison of Fig. 10b with Fig. 10a, accounting for 22% of the material loss. The amount of PEG incorporated into PEG-SiO₂ was calculated to be about 22%. A small peak at around 540 °C reflected decomposition of carbonaceous materials or char formed during earlier steps^{10, 18}. The shift in T_m from 344 °C at 15 °C.min⁻¹ to 366 °C at 40 °C.min⁻¹ shows that thermal decomposition is affected by the heating rate³⁷. A similar trend is also observed for pure PEG where a shift in T_m is observed

from 417°C at 15°C/min to 428.7°C at 40°C/min, as given in Fig 10c.

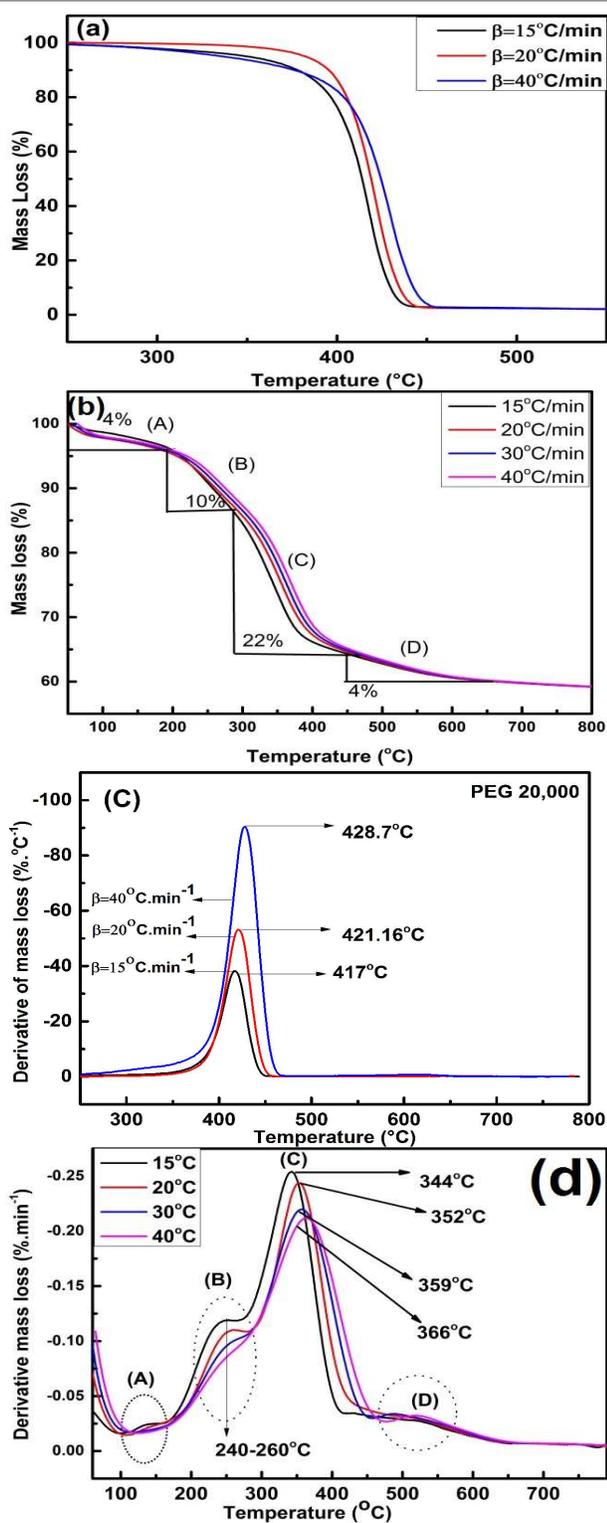


Figure 10 TGA plots of (a) PEG-20000 and (b) PEG-SiO₂. DTG plots of (c) PEG-20000 and (d) PEG-SiO₂.

This trend of DTG peak temperature variation was subsequently utilized for model-free kinetic analysis.

Similar TGA results of PEG-silica composites were reported by Li et.al without the presence of peak “D”. The existence of peak “D” may be attributed to the formation of pyrolysis products formation at higher heating rates¹².

The kinetics of the thermal decomposition are determined by TGA or DTG techniques by employing model-free and model-based kinetic equations. DTG technique was used in this study and is discussed in next section.

Thermokinetics studies of PEG removal

The DTG technique was used for thermokinetic and thermodynamic studies of PEG-SiO₂, and data obtained were compared with those of pure PEG. Ozawa and Kissinger plots of PEG and PEG-SiO₂ (peaks B and C) are described in Figs. 11a–11c. The apparent E_a and A were calculated from the slope and intercept of the plots using Eqs. 9–11, and results are tabulated in Table 3. Both samples demonstrated effective linear fitting, yielding fairly high values of R^2 (Table 3). Pure PEG exhibited an E_a of 330.1 KJ.mol⁻¹ (Kissinger) and 324.81 KJ.mol⁻¹ (Ozawa); these values are higher than that obtained by Feng-Yih et al. (283KJ.mol⁻¹)³⁸. Increases in E_a and $\ln A$ may be correlated with the amount and morphology of the sample, differences in β , and the kinetics method used. In PEG-SiO₂, peak “B” exhibited an E_a of 105.9 KJ.mol⁻¹ (Kissinger) and 109 KJ.mol⁻¹ (Ozawa), while peak “C” produced an E_a of 139.7 KJ.mol⁻¹ (Kissinger) and 142 KJ.mol⁻¹ (Ozawa). Differences in E_a support the hypothesis that peak “B” corresponds to dehydration of bonded water and peak “C” represents decomposition of PEG; these suppositions are consistent with the TGA and DTG results (Fig. 10b).

The values of $\ln A$ are also higher for pure PEG [57.7 min⁻¹ (Kissinger) and 51.6 min⁻¹ (Ozawa)] compared with those for PEG-templated silica [20 min⁻¹ (Kissinger) and 18.7 min⁻¹ (Ozawa)]. These decreases in E_a and $\ln A$ may be correlated with chemical interactions between PEG and silica. Renata et al. postulated that increases in E_a during CTMA⁺ removal from an MCM 41 matrix are due to strong interactions between the silica surface and the polymer³⁹.

In our study, the decrease in E_a may be related to non-bonding attractions between the silica surface and PEG, which supports the notion of no chemical reaction occurring between silica and PEG. Observations by Saladino et al. may also explain the phenomena observed: nanoparticles catalyze the thermal decomposition of polymers by initiating earlier thermal degradation⁴⁰. These postulations are in good agreement with the TGA data of PEG-SiO₂ (Fig. 10b), which showed earlier degradation at 200 °C compared with PEG (approx. 400 °C). The E_a of PEG-SiO₂ in this work is slightly higher than those reported in the literature for lower-molecular weight PEG-4000, the E_a of which lies in the range of 112–116 kJ.mol⁻¹⁴¹.

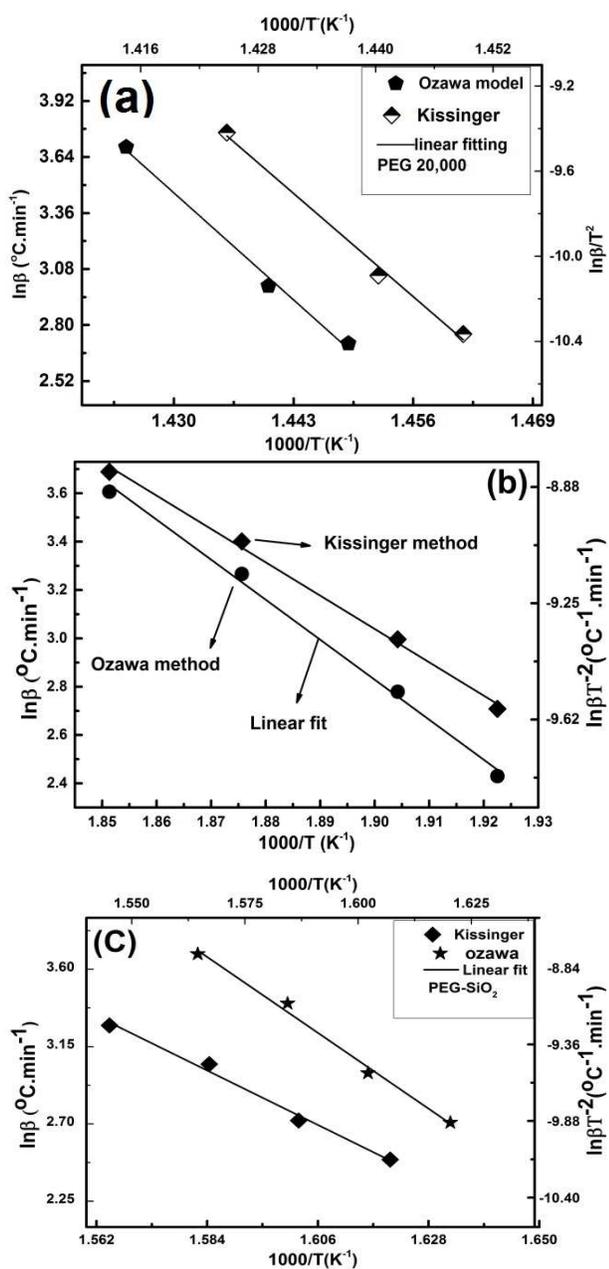


Figure 11 Ozawa and Kissinger model-based kinetics of (a) PEG-20000, (b) Peak "B" of PEG-SiO₂, and (c) Peak "C" of PEG-SiO₂.

Table 3. Thermokinetic and thermodynamic properties of PEG and PEG-SiO₂

Material	Method	E _a kJ.mol ⁻¹	ln A min ⁻¹	R ²	ΔH kJ.mol ⁻¹	ΔG Kj.mol ⁻¹	ΔS J.mol ⁻¹
PEG	Kissinger	330.1	57.7	0.993	324.3	173	220
	Ozawa	324.8	51.6	0.998	319.0	203	169
PEG-SiO ₂ (Peak B)	Kissinger	105.9	20.0	0.994	101.5	149	-91.1
	Ozawa	109.0	18.7	0.995	104.6	152	-102
PEG-SiO ₂ (Peak C)	Kissinger	139.7	22.7	0.987	134.6	178	-70.4
	Ozawa	142.7	21.2	0.988	137.6	190	-83.4

The closeness of the E_a values reveals a possible breakdown of cross-linking and conversion of high-molecular weight PEG into lower-molecular weight PEG.

Thermodynamic functions (i.e., ΔH[#], ΔG[#], and ΔS[#]) of the transition state were determined using Eqs. 15–17 through the Kissinger and Ozawa methods using DTG data, and the values obtained are tabulated in Table 3. The thermodynamic functions calculated by the Kissinger and Ozawa methods are fairly similar, which means both methods produce reliable thermodynamics results.

Changes in entropy (ΔS) for the thermal degradation of pure PEG are 220 j.mol⁻¹ (Kissinger) and 169 j.mol⁻¹ (Ozawa); these values demonstrate that the activated species has higher entropy (lower degree of arrangement) than the starting material. As explained using transition state theory of activated complexes, a positive value of ΔS represents an activated complex resulted in a "fast" stage reaction. By contrast, a negative ΔS demonstrates that the activated complex is structurally more complex compared with the starting material and can be considered a "slow" stage reaction product. This explanation is consistent with the TGA analyses of PEG and PEG-SiO₂ (Figs. 10a and 10b), as PEG shows a faster reaction⁴². Pure PEG exhibited an enthalpy change (ΔH) of 324 and 319 kJ.mol⁻¹ according to the Kissinger and Ozawa plots, respectively; these values are higher than the corresponding values of peak "C" of PEG-SiO₂, i.e., 134.6 and 136.6 kJ.mol⁻¹, respectively. Such results confirm that the thermal degradation processes of PEG and PEG-SiO₂ are endothermic in nature and that a large amount of energy is required for their decomposition⁴². Moreover, we can conclude that PEG loses its structural arrangement when added to silica as a template. Changes in Gibbs free energy (ΔG[#]) similarly demonstrate that thermal degradation of PEG and PEG-SiO₂ is a non-spontaneous process⁴³. Thermodynamic data confirmed that PEG decomposition is a non-spontaneous process and that a large amount of energy is required for decomposition. Abrupt changes in the thermodynamic properties of PEG-SiO₂ observed during decomposition agree with the assumption that the PEG structure is broken into lower-molecular weight PEG, as confirmed by the E_a and ln A values obtained.

Conclusion

The use of POFA for extracting nano silica and iron oxide was evaluated. Nano silica and iron oxide were obtained simultaneously from POFA. Nano silica of moderate surface area (326m²/g) and pore diameter (8.2 nm) was obtained when PEG was used as a templating agent. PEG promoted deagglomeration of silica by reducing hydrogen bonding between silica particles. FTIR and TGA analysis revealed that interactions between PEG and silica are physical in nature, and no chemical bonds were observed. TGA thermokinetics suggested that PEG is converted into lower-molecular weight PEG when used for templating. Iron oxide extraction was pH-selective and, if not carefully controlled, could be easily contaminated.

Acknowledgment

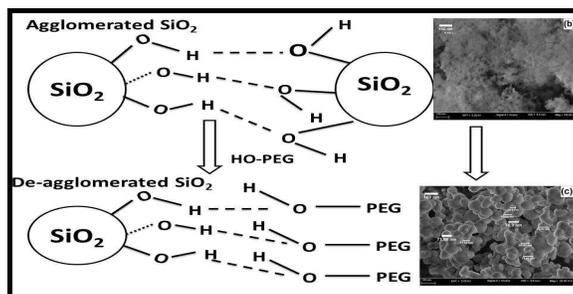
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Table of content

(a)



(b)

This work reports synthesis of nano silica and iron oxide from POFA.