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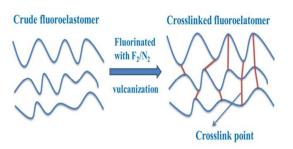
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A novel vulcanization of fluoroelastomer by fluorination is studied, simultaneously accompanied fluorine content increase, and tribological property is improved.

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The reaction kinetics and mechanism of crude fluoroelastomer vulcanized by direct fluorination with fluorine/nitrogen gas

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A novel vulcanization method for crude fluoroelastomer by direct fluorination with fluorine/nitrogen gas has been investigated. The results show that the vulcanization reaction of fluoroelastomer is closely related with fluorination temperature, fluorination time and fluorine gas partial pressure. The maximum

¹⁰ crosslink degree can be up to 97%, and the fluorine content of fluoroelastomer increased from 48.2% to 60% during the fluorination. The static friction coefficient of fluoroelastomer is decreased from 0.91 to 0.55, about 39.6% reduction after fluorination. The ATR-FTIR spectra indicate the crosslink reaction process of fluoroelastomer by direct fluorination arises three reaction stages and successively goes through four elementary reactions: substitution reaction; elimination reaction; addition reaction; crosslink

15 reaction. The increase of fluorine content mainly takes place in the first stage, and the crosslink reaction

mainly takes place in the second stage and third stage.

1. Introduction

Fluoroelastomers gain increasing concern in view of their excellent thermo stability, oil resistance, mechanical property,

²⁰ anti-radiation performance and abrasive resistance. Most of these properties are linked to the low polarizability and the strong electronegativity of the fluorine atom, to its small van der Waals radius (0.64 Å), and to the strong C-F bond (485 kJ·mol⁻¹).⁷ Therefore, fluoroelastomers have extensive application in ²⁵ industry, including engine oil seals, fuel system components like

hoses and O-rings, and drive train seals.¹⁻⁶

Fluoroelastomers, like all other thermosetting elastomers, need useful and practical chemical crosslink system. The traditional vulcanization methods of fluoroelastomer mainly include ionic ³⁰ vulcanization and free radical vulcanization.¹ During ionic vulcanization process, HF is eliminated from -CH₂-CF₂- structure to form -CH=CF- structure. Sequentially, the nucleophilic

- addition of a crosslinker to the -CH=CF- double bond proceeds, yielding crosslinks. However, the fluorine content of ³⁵ fluoroelastomer may decreases after ionic vulcanization. Free
- radical vulcanization (peroxide curing, such as a,a'-bis(t-butylperoxy)diisopropyl benzene and triallylisocyanurate) is a way to use free radicals to attack polymer chains to form polymeric free radicals. The polymeric radicals form crosslink networks directly
- ⁴⁰ or via the intermediary of radical traps. In addition, the fluorine content of fluoroelastomer still remains unchanged after free radical vulcanization.

Direct fluorination with fluorine gas has been rapidly developed in recent years.⁸⁻¹⁰ Direct fluorination reaction is

⁴⁵ usually heterogeneous, exothermic and spontaneous, owing to the high reactivity of fluorine and the formation of fluorine free radical ($F \cdot$) in the process. The $F \cdot$ can react with methylene (– CH_2-) of polymer chain to form alkyl free radical (-CH·-). The - CH·- is reportedly able to form crosslink networks, according to ⁵⁰ previous study of polyethylene fluorination.¹⁰

Therefore, it is expected that the F· can also be used as a new vulcanizing agent to vulcanize fluoroelastomer, and the fluorine content of fluoroelastomer increases simultaneously because the hydrogen atoms of $-CH_2$ - can be substituted by fluorine atom ⁵⁵ during the direct fluorination. Sequentially, the properties of fluoroelastomer, such as abrasive-resistance and solvent-resistance, can be improved effectively.¹¹ Due to the strong penetration ability of fluorine gas in rubber, not only the surface of fluoroelastomer with sufficient thickness can be vulcanized. The analysis above inspired us to explore the possibility of fluoroelastomer vulcanized by fluorine/nitrogen gas and simultaneously preparation fluoroelatomer with ultrahigh fluorine content.

In this study, the investigation on fluoroelastomer vulcanized by direct fluorination with fluorine/nitrogen gas was first reported. The fluorinated fluoroelastomer films have formed chemical crosslink networks. The fluoroelastomer shows different solubility and mechanical properties before and after 70 fluorination. Meanwhile, the direct fluorination can also increase the fluorine content and decrease the static friction coefficient with no damage to the elastic property of fluoroelastomer film. The reaction kinetics and mechanism of crosslink reaction by direct fluorination have been studied systematically.

75 2. Experimental

2.1 Film fabrication

The crude fluoroelastomer (F26, terpolymer of vinylidene fluoride and hexafluoropropylene copolymer) is supplied by Zhonghao Chenguang Research of Chemical Industry. 5 g crude fluoroelastomer was dissolved in 25 mL acetone, and the solution was cast on glass. Then the films were dried at 140 °C for 6 h to remove acetone completely. The thickness of film was controlled s at about 40-50 μm.

2.2 Direct fluorination

Direct fluorination was carried out in closed stainless steel vessel. The air in the closed vessel was removed and replaced by nitrogen gas ($N_2 > 99.99\%$) for three cycles to remove residual

- ¹⁰ oxygen and moisture in the chamber and on the polymer films. Then the crude fluoroelastomer films were preheated in the closed vessel for 10min at specific temperature (e.g. 15 °C, 30 °C, 40 °C). After preheating, the vessel was replenished with a specific pressure of the F_2/N_2 (10 vol% for F_2) mixed gas (e.g. 6
- ¹⁵ kPa, 10 kPa, 20 kPa) to fluorinating. The direct fluorination of fluoroelastomer films was performed at different fluorination temperatures, fluorination times and fluorine gas partial pressures to investigate the influence of these factors on the crosslink reaction of fluoroelastomer.

20 2.3 Crosslink degree test

The fluorinated fluoroelastomer film (mass M₁) was dissolved in acetone for 10 min. The insoluble part was separated from acetone, dried at 100 °C for 10 min and weighted (mass M₂). Crosslink degree was calculated according to the following ²⁵ equation:

Crosslink degree =
$$\frac{M_2}{M_1} \times 100\%$$
 (1)

2.4 Fluorine content tests

The bulk fluorine content of the crude and fluorinated fluoroelastomer films were tested by oxygen flask combustion

³⁰ (OFC) method, which is referred to the previous literatures.¹²⁻¹³ Additionally, the fluorine content of crude and fluorinated fluororlastomer film's surface were measured by energy dispersive X-Ray spectroscopy (EDX, FEI company, USA).

2.5 Characterization

- ³⁵ The surface morphology of the crude and fluorinated fluoroelastomer film was measured by scanning electron microscope (SEM). SEM was operated with FEI Inspect F (FEI company, EU/USA) at 20 kV and the magnification was set at 10,000×.
- ⁴⁰ The tensile mechanical properties of the fluoroelastomer were measured by an Instron Model 5567 twin column table mounted testing system at ambient conditions with a gauge length of 40 mm and a crosshead speed of 50 mm/min.
- Glass transition temperature (Tg) was characterized by ⁴⁵ differential scanning calorimetry (DSC), performed on Netzsch 204 DSC with a heating rate of 5 °C/min in flowing nitrogen.

The static friction coefficient of crude and fluorinated fluoroelastomer was obtained through the ratio of the maximum static friction force to the vertical gravity force.

⁵⁰ The chemical composition and structure of fluorinated fluoroelastomer film were characterized by attenuated total reflectance Fourier transform infrared (ATR-FTIR). ATR-FTIR spectra of fluoroelastomer films were recorded on a Nicolet Magna 650 spectroscope in the range from 4000 to 400 cm^{-1} .

55 3. Results and discussion

3.1 Crosslink degree of fluorinated fluoroelastomer film

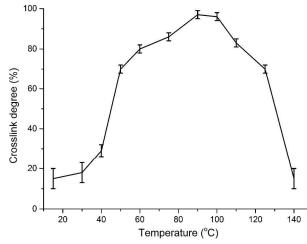


Fig.1 The crosslink degree as a function of fluorination temperature (°C), the fluorine gas (F₂/N₂ mixed gas, 10 vol% for F₂) partial pressure was 30 kPa and the fluorination time was 60 min.

It is known that fluorination is a free radical reaction. During the polyethylene fluorination process, $-CH_2$ - structure can react with fluorine atom to develop the -CHF- structure or generate -CH- and F \cdot . The polymeric radicals of different polymer chains can be coupled to develop chemical crosslink networks.¹⁰ The crude F26 fluoroelastomer contains -CH₂- structure in its macromolecular backbone that provides the possibility of crosslink reaction. The crude fluoroelastomer can be well dissolved in acetone solvent. However, the solubility of fluoroelastomer film becomes poor in

⁷⁰ acetone after fluorination, indicating that fluoroelastomer film has developed crosslink networks during the process of direct fluorination. The crosslink degree was characterized by the solubility of fluoroelastomer in acetone after fluorination. The influences of three significant fluorination factors (fluorination ⁷⁵ temperature, fluorination time, fluorine gas partial pressure) on

the crosslink degree of fluoroelastomer film were investigated. The crosslink degree of fluoroelastomer films fluorinated at different temperature was measured in Fig.1. The fluorine gas $(F_2/N_2 \text{ mixed gas, 10vol\% for } F_2)$ partial pressure in the ⁸⁰ fluorination ambience was 30 kPa, and the fluorination time was 60min. Fluoroelastomer films fluorinated at relative low fluorination temperature (15 °C, 30 °C) have a low crosslink degree. The crosslink degree increased along with fluorination temperature increases. When the reaction took place at 30-60 °C, 85 the crosslink degree of fluorinated films increased rapidly. The maximum value of crosslink degree can reach 97%, when the fluoroelastomer film is fluorinated at 90 °C. At 100-140 °C fluorination, the crosslink degree declines gradually due to the degradation of fluoroelastomer film possibly. Chain degradation 90 reaction caused by fluorine radicals rather than crosslink reaction is possibly the dominant reaction at 100-140 °C fluorination.

The influence of fluorination time and fluorine gas partial pressure on the crosslink degree of fluorinated films were investigated as well. As shown in Fig.2 (a), at low fluorination temperature (15 °C), the fluoroelastomer film had the relatively low crosslink degree. At high fluorination temperature (50 °C, 100 °C), there is a linear relationship between crosslink degree and fluorination time after 10 min fluorination. When the ⁵ fluoroelastomer film was fluorinated at 100 °C for 10 min with different fluorine gas partial pressure, there is also a linear relationship between crosslink degree and fluorine gas partial pressure as shown in the Fig.2 (b). Fluorinated with 50 kPa F_2/N_2 mixed gas (10 vol% for F_2) for only 10 min, the fluoroelastomer

¹⁰ film got the highest crosslink degree (96%). However, when fluorinated with 30 kPa F_2/N_2 mixed gas (10 vol% for F_2) for a

long time (60 min), the fluoroelastomer film can get the same crosslink degree (97%). The increase of F_2 partial pressure can substantially shorten the fluorination time, when the fluorinated ¹⁵ films achieve the identical crosslink degree.

It can be concluded that the fluorination temperature is the most important influence factor of the crosslink reaction, which not only affects the crosslink degree but also possibly causes the chain degradation reaction. The fluorine gas partial pressure can ²⁰ be regarded as the second important influence factor which shortens the fluorination time.

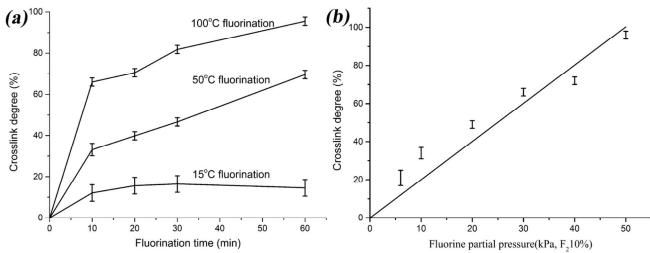


Fig.2 The crosslink degree as a function of (a) fluorination time (min), the fluorine gas (F₂/N₂ mixed gas, 10 vol% for F₂) partial pressure was 30kPa and the fluorination temperature was 15 °C, 50 °C, 100 °C; and (b) F₂ partial pressure (kPa), the fluorination temperature was 100 °C and the fluorination time was 10min

3.2 Fluorine content analysis

25

Table.1 the fluorine content tested by EDX and OFC method

increase	in	its	fluorine content.	

Method	F (wt%)	
EDX	Crude film	58.7
	Fluorinated film	70.5
OFC	Crude film	57.9
	Fluorinated film	67.7

The fluorine content of the fluoroelastomer was tested before and after direction fluorination by energy dispersive X-Ray ³⁰ spectroscopy (EDX) and oxygen flask combustion (OFC) method. The fluorine contents of crude film and fluorinated film are listed in Table.1 as weight percent (wt%). It is known that the fluorine content of rubber film's surface is tested by EDX and that of the bulk film is tested by OFC method. As shown in ³⁵ table.1, after the fluorination, the fluorine contents of the film surface and the bulk film increase to 70.5 wt% and 67.7 wt% respectively, which have no significant difference between each other. Therefore, it can be concluded that the bulk of fluoroelastomer film was fluorinated rather than the surface, ⁴⁰ when it was reacted at 90 °C with 30 kPa F₂/N₂ mixed gas (10

- ⁴⁰ when it was reacted at 90° C with 50 kPa F_2/N_2 inited gas (10 vol% for F_2) for 60 min. Therefore, fluorination with fluorine gas has strong penetration ability in rubber, unlike in plastic (PE, PP) ^{10, 14-15} and fiber (aramid fiber) ⁸. The whole fluoroelastomer film (40-50µm) can be fluorinated with fluorine gas, and fluorinated ⁴⁵ layer in rubber is much thicker than it is in PE (0.5µm).¹⁴ In this
- 45 layer in rubber is much thicker than it is in PE (0.5μm). In this respect, the fluorination with fluorine gas is an effective vulcanization method for fluoroelastomer with significant

 Table.2 EDX of crude fluoroelastomer film and different temperature

 50
 fluorinated fluoroelatomer film

	untreated	30°C	40°C	60°C	90°C
C (wt%)	35.6	29.3	27.9	29.9	29.5
F (wt%)	58.7	70.7	72.1	70.1	70.5
				1 1 01	

Meanwhile, the fluorine content of the fluorinated film's surface at different temperature fluorination was tested by EDX shown in Table.2 as weight percent (wt%). The fluorine content of the fluorinated film's surface increased from 58.7 wt% to 70.7 wt% ⁵⁵ after 30 °C fluorination. And the fluorine contents kept about 70wt% with the fluorination temperature increased from 40 °C to 90 °C. However, the crosslink degree was elevated obviously with increase of the fluorination temperature as shown in Fig.1. In general, the crosslink degree and the fluorine content are both ⁶⁰ increased in 30 °C fluorination. The crosslink degree increased, but the fluorine content remained unchanged in 40 °C-90 °C fluorination. Therefore, further research is required to investigate the mechanism of the observed phenomenon.

3.3 The kinetics and mechanism of crosslink reaction by 65 direct fluorination

As we know, direct fluorination with fluorine gas is a solid-gas reaction actually, which is described as a multi-stage, multi-reaction untreated shrinking core model.¹⁶⁻¹⁸ The untreated shrinking core model is accepted as the best simple model for the ⁷⁰ majority of reacting solid-gas systems presented by Ishida at 1971.¹⁶⁻¹⁷ The model successfully represents the fluorination of

uranium dioxide where uranium hexafluoride gas is produced through uranyl fluoride as a solid intermediate.¹⁷ The solid-gas reaction is controlled by two main parameters: the non-dimensional diffusion rates of reactant gas and the reaction rates.

- ⁵ When reacting for 60 min, the bulk of fluoroelastomer film was fluorinated completely, which were testified by the results of EDX and OFC method shown in **3.2**. Therefore, we can ignore the influence of the reactant gas diffusion in fluoroelastomer film. Only considering the reaction rates, we calculated the kinetics
- ¹⁰ parameters of the fluorination with fluorine gas through the curve of crosslink degree and fluorination temperature.

So the equation of fluorination reaction rate can be displayed by the Arrhenius equation¹⁶⁻¹⁷:

$$F(\alpha) = Ae^{-\frac{\mu_{\alpha}}{RT}t} = kt$$
⁽²⁾

- ¹⁵ Where α is solid conversion percent(we can regard crosslink degree as α), *t* is fluorination time, *A* is pre-exponential factor, E_a is apparent activation energy, *R* is gas constant, *k* is reaction speed constant, $F(\alpha)$ is integral equation of solid conversion percent. When solid-gas reaction is controlled by chemical ²⁰ reaction as far as flaky material, $F(\alpha)$ is equal to α in the
- untreated shrinking core model.¹⁹⁻²⁰ Then the Arrhenius equation can be written as:

$$\ln F(\alpha) = \ln \alpha = \ln At - \frac{E_a}{R} \cdot \frac{1}{T}$$
(3)

Thus, there is a linear relationship with $\ln \alpha$ and 1/T. The slope ²⁵ indicates apparent activation energy (E_{α}) and the intercept represents pre-exponential factor (A). The α , $\ln \alpha$ and 1/T of different fluorination temperatures were listed in Table.3 and Fig.3.

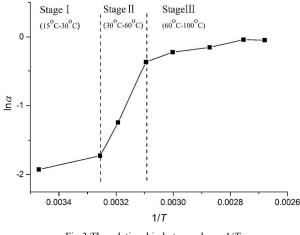


Fig.3 The relationship between $\ln \alpha - 1/T$

There are three linear relationships with $\ln \alpha$ and 1/T in Fig.3. Thus, the whole fluorination crosslink reaction can be divided into three stages. The apparent activation energy (E_a) and preexponential factor (A) of three stages are shown in Table.4.

Table.4 E_a and A of different fluorination reaction stage

 Reaction stage	E_a (kJ/mol)	$A (\min^{-1})$
 stage I	7.4±1.5	0.054±0.003
stage II	70.1±3.4	2.5±0.06×10 ⁹
stage III	6.4±0.9	0.13±0.02

The fluorination crosslink reaction can be divided into three stages through the study of reaction kinetics. The structure changes in three reaction stages were studied by ATR-FTIR spectroscopy. Referring to Fig.3, 30 °C fluorination was regarded ⁴⁰ as the end of stage I; 40 °C fluorination was regarded as the center of stage II; 60 °C fluorination was regarded as the start of Stage III; 90 °C fluorination was regarded as the end of stage III. Then ATR-FTIR spectroscopy of fluoroelastomer film fluorinated at 30 °C, 40 °C, 60 °C, 90 °C for 60 min is shown in ⁴⁵ Fig.4.

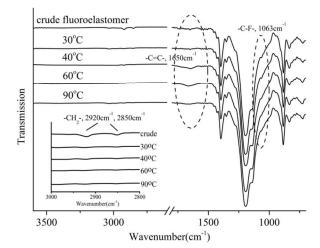


Fig.4 ATR-FTIR spectra of the crude and fluorinated fluoroelastomer at different temperature

As shown in Fig.4, in the crude fluoroelastomer film's ATR-⁵⁰ FTIR spectroscopy, 2920 cm⁻¹, 2850 cm⁻¹ peaks are attributed to -CH₂- moieties.^{14, 21} The -CH₂- structure vanished completely in 30 °C fluorination. Additionally, the fluorine content increased substantially in 30 °C fluorination as shown in Table.2, which reveals that the hydrogen atom of -CH₂- structure was substituted ⁵⁵ by fluorine atom. In the direct fluorination of polyethylene, the hydrogen atom of -CH₂- is substituted by fluorine atom at about 28 °C initially¹⁰ and the substitution reaction of fluorine atom occurs.

In 30 °C-60 °C fluorination, -C=C-(1650 cm⁻¹)²² structure is ⁶⁰ present as shown in Fig.4. There is no 1650cm⁻¹ peak in the spectroscopy of 30 °C fluorination. However, the -C=C-(1650cm⁻¹) structure is formed at 40 °C, 60 °C fluorination. The HF is eliminated from -CHF-CF₂- structure to form -CF=CF- structure. 1283 cm⁻¹, 1197 cm⁻¹, 1137 cm⁻¹, 1063 cm⁻¹ peaks are attributed ⁶⁵ to C-F moieties.^{10, 15, 18} The area of 1063 cm⁻¹ peak obviously decrease in 40 °C fluorination. It also indicates that there is a

Table.3 The relationship between α , $\ln \alpha$, 1/T of different fluorination temperature

<i>T</i> (°C)	15	30	40	50	60	75	90	100
α	0.15	0.18	0.29	0.70	0.80	0.86	0.97	0.96
lnα	-1.90	-1.71	-1.24	-0.36	-0.22	-0.15	-0.04	-0.04
$1/T (\times 10^{-3} K^{-1})$	3.47	3.26	3.19	3.10	3.00	2.87	2.75	2.68

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reaction eliminating HF.

In 60 °C-90 °C fluorination, the -C=C-(1650 cm⁻¹) structure still exists at 60 °C as shown in Fig.7. But at 90 °C fluorination (the crosslink degree peak at 97%), the -C=C-(1650 cm⁻¹) $^{\circ}$ structure disappeared completely. The -C=C- structure reacted with fluorine (F·) to form fluoric alkyl free radical (·CF-CF₂). And the fluoric alkyl free radical (-·CF-CF₂-) were coupled to develop highly crosslink network.

In Fig.4, the changes of fluoroelastomer structure respect to the ¹⁰ fluorination temperature were observed. To explain the mechanism of crosslink reaction by fluorination, four elementary reactions (substitution reaction, elimination reaction, addition reaction, crosslink reaction) are presented in Scheme.1.

Elementary reaction I (substitution reaction):

$$-CH_2-CF_2 - + F_2 \longrightarrow -CH-CF_2 - + F_{\bullet} + HF$$
$$-CH-CF_2 - + F_{\bullet} \longrightarrow -CHF-CF_2 - + F_{\bullet}$$

Elementary reaction II (elimination reaction):

$$-CHF-CF_2 -CF=CF-$$

$$-F_2C- \stackrel{CF_3}{\underset{F}{\overset{} =}} -CHF- \longrightarrow -F_2C- \stackrel{CF_3}{\underset{F}{\overset{} =}} cF-$$

Elementary reaction III (addition reaction):

Elementary reaction IV(crosslink reaction):

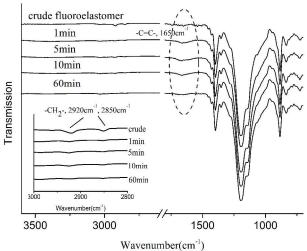
$$-CF - CF_{2} - + -CF - CF_{2} - \longrightarrow \qquad CF - CF_{2} - CF_{2$$

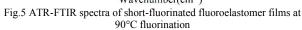
15 Scheme.1 the four elementary reactions of crosslink reaction by direct fluorination

The short time fluorinations (fluorinated for 1 min, 5 min, 10 min at 90 °C) were processed, in order to observe the elementary reaction. The ATR-FTIR spectra of short time fluorinated films 20 are presented in Fig.5. At 90 °C fluorination, the -CH2- structure was substituted by fluorine atom entirely and -C=C- structure was generated after only one minute reaction. In view of the fact that the crosslink degree increased with the fluorination time (Fig.2(a)), elementary reaction II (elimination reaction), 25 elementary reaction III (addition reaction) and elementary reaction IV (crosslink reaction) are regarded as occurring concurrently at 90 °C. Meanwhile, one fluorine atom is eliminated in elementary reaction II and one fluorine atom would be added in elementary reaction III. So the fluorine content of 30 fluorinated film is considered to increase after substitution reaction (elementary reaction I) and to remain unchanged after elimination reaction, addition reaction, crosslink reaction.

Referring to the above analysis of the elementary reactions, the

fluorine content of fluorinated film is predicted to increase in stage I (only substitution reaction occurs) and remain unchanged in stage II and stage III (substitution reaction, elimination reaction, addition reaction, crosslink reaction entirely occur). The prediction is in accordance with the fluorine content result shown in Table.2. The changes of fluorine atom content also can prove the accuracy of elementary reaction theory.





3.4 Mechanical properties

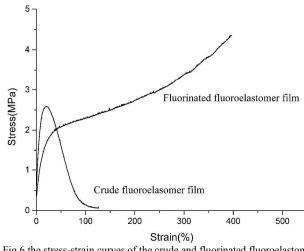


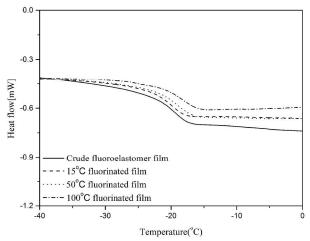
Fig.6 the stress-strain curves of the crude and fluorinated fluoroelastomer film

Additionally, the increase of fluorine content can alter the solubility of polymers in solvent so that fluorinated film couldn't ⁵⁰ be dissolved anymore. Therefore, the solubility changes of fluoroelastomer in acetone may be due to the increase of fluorine content rather than crosslinking. In this regard, the stress-strain curves of fluoroelastomer film before and after fluorinated at 90 °C ⁵⁵ with 30 kPa F₂/N₂ mixed gas (10 vol% for F₂) for 60 min, the crosslink degree can be up to the maximum. The mechanical property of the fluorinated film prepared under the above described condition was tested. The stress-strain curves of crude and fluorinated fluoroelastomer film are shown in Fig.6. The ⁶⁰ stress-strain curve of crude fluoroelasomer film implies that there

is no crosslink network. The yield stress of crude fluoroelasomer film is only about 2.58 MPa at 120% strain. However, the stressstrain curve of fluorinated fluoroelastomer film behaves like a thermosetting elastic rubber. After the film was fluorinated at

- ⁵ 90 °C for 60 min, the stress at 400% strain is about 4.37 MPa, indicating that there is crosslink network in fluorinated film. ²³⁻²⁴ Furthermore, as shown in Fig.1 and table.2, with the fluorination temperature increased from 40 °C to 90 °C, the crosslink degree increases sharply and the fluorine content keeps unchanged, also
- ¹⁰ indicating that the solubility changes of fluoroelastomer in acetone are caused by the crosslink networks rather than the increase of fluorine content in fluorinated fluoroelastomer film.

3.5 Glass-transition temperature (Tg)



15 Fig.7 The DSC curves of the crude and different temperature (°C) fluorinated fluoroelastomer film

 $\label{eq:table_state} \begin{array}{l} \textbf{Table.5} \ \text{Tg of the crude and different temperature (}^{\circ}\text{C}\text{) fluorinated} \\ \text{fluoroelastomer film obtained through DSC method} \end{array}$

Samples	Tg (°C)	Crosslinking degree (%)
Crude film	-25.5	0
15 °C fluorinated film	-24.2	14.56
50 °C fluorinated film	-23.5	69.63
100 °C fluorinated film	-22.5	95.49

Generally, polymer would transform from elastomer into plastic, ²⁰ when its fluorine content increase substantially. The DSC curves of crude and different temperature fluorinated fluoroelastomer films are shown in Fig.7. Moreover, Table.5 shows that the Tg of fluorinated fluoroelastomer films is slightly elevated with the increase of crosslink degree. However, the Tg of fluorinated

²⁵ fluoroelastomer films keeps about -23 °C, and the fluorinated films maintain properties of the elastomer. It can be concluded that fluorination can generate the crosslink networks in fluoroelastomer preserving elastic properties simultaneously.

3.6 The friction coefficient

- ³⁰ For elastomers, the direct fluorination with fluorine gas can decrease the friction coefficient and improve the wear life of elastomeric, such as ethylene-propylene, acrylonitrile-butadiene elastomers.²⁵ The static friction coefficient of fluorinated fluoroelastomer film prepared at different temperature were
- ³⁵ tested, and shown in Table.6. The static friction coefficient of fluorinated film decreases from 0.91 to 0.55 at low temperature fluorination (30 °C). The static friction coefficient of crosslinking

fluoroelatomer by fluorination is much lower than that of crosslinking fluoroelatomer by other methods (generally the static 40 friction coefficient >1.0). With the increase of fluorination

temperature from 30 °C to 100 °C, the static friction coefficient of fluorinated fluoroelastomer film keeps about 0.55.

Table.6 the static friction coefficients of the crude and fluorinated
fluoroelastomer film at different temperature

Fluorination temperature	Crude film	30 °C	50 °C	70 °C	100 °C
Friction coefficient	0.91±0.1	0.55±0.1	0.59±0.1	0.55±0.1	0.52±0.1

45 4. Conclusions

The present study demonstrates that direct fluorination with F_2/N_2 mixed gas comprises a new and successful way to vulcanize fluoroelastomer. The fluoroelastomer vulcanized by direct fluorination achieves a great increase in the crosslink degree with

- ⁵⁰ no damage on its elastic properties while the fluorine content is significantly increased. Moreover, the static friction coefficient of fluoroelastomer film was greatly decreased. The crosslink reaction of fluoroelastomer was controlled by fluorination temperature, fluorination time and fluorine gas partial pressure.
- 55 The mechanism of crosslink reaction by fluorination has been elaborated. The mechanism of crosslink reaction by fluorination mainly successively goes through four elementary reactions. First, a hydrogen atom of -CH₂- is substituted by fluorine atom. Sequentially, HF is eliminated from polymer main chain and
- ⁶⁰ develop the -C=C- structure. In the next step, $F \cdot$ and -C=Cstructure take place addition reaction developing the fluoric alkyl free radicals. Finally, the fluoric alkyl free radicals couple completing crosslink. The increase of fluorine content mainly takes place in first stage, and the crosslink reaction mainly takes splace in second stage and third stage.

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Notes and references

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[‡] Footnotes should appear here. These might include comments relevant to but not central to the matter under discussion, limited experimental and spectral data, and crystallographic data.

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