# **RSC Advances**



This is an *Accepted Manuscript*, which has been through the Royal Society of Chemistry peer review process and has been accepted for publication.

Accepted Manuscripts are published online shortly after acceptance, before technical editing, formatting and proof reading. Using this free service, authors can make their results available to the community, in citable form, before we publish the edited article. This Accepted Manuscript will be replaced by the edited, formatted and paginated article as soon as this is available.

You can find more information about *Accepted Manuscripts* in the **Information for Authors**.

Please note that technical editing may introduce minor changes to the text and/or graphics, which may alter content. The journal's standard <u>Terms & Conditions</u> and the <u>Ethical guidelines</u> still apply. In no event shall the Royal Society of Chemistry be held responsible for any errors or omissions in this *Accepted Manuscript* or any consequences arising from the use of any information it contains.



www.rsc.org/advances

## **Graphical abstract**

Efficient catalytic transesterification of soybean oil with methanol to produce biodiesel over the  $CaO-ZrO_2$  solid base catalyst prepared by urea-nitrate combustion method



# **RSC** Advances

# ARTICLE

RSCPublishing

# Biodiesel synthesis over CaO-ZrO<sub>2</sub> solid base catalyst prepared by urea-nitrate combustion method

Shengfei Xia, Xiaoming Guo,<sup>\*</sup> Dongsen Mao, Zhangping Shi, Guisheng Wu and Guanzhong Lu

Received 00th 0000 2014, Accepted 00th 0000 2014

Cite this: DOI: 10.1039/x0xx00000x

DOI: 10.1039/x0xx00000x

www.rsc.org/catalysis

CaO-ZrO<sub>2</sub> solid base catalysts with Ca/Zr ratios varied from 4/6 to 9/1 were prepared via ureanitrate combustion method and used in the transesterification of soybean oil with methanol to produce biodiesel. The catalysts were characterized with N<sub>2</sub> adsorption, XRD, SEM and CO<sub>2</sub>-TPD techniques, and tested for biodiesel synthesis. The results show that a new phase of CaZrO<sub>3</sub> has been formed for the investigated CaO-ZrO<sub>2</sub> catalysts. With the increase in Ca/Zr molar ratio, the total basic sites over the catalyst increase and a maximum is obtained over CaO-ZrO<sub>2</sub> catalyst with a Ca/Zr ratio of 8/2. A similar variation trend of biodiesel yield is observed, suggesting that the catalytic activity correlates well with the total basic site on catalyst surface. Furthermore, the turnover frequency (TOF) had been calculated for various CaO-ZrO<sub>2</sub> catalysts and the result revealed that the catalytic activity also depends on the strength of basic site. The urea-nitrate combustion method was demonstrated to be a simple, fast and effective method for the preparation of CaO-ZrO<sub>2</sub> solid base catalysts, which could be effectively applied for biodiesel synthesis.

#### 1. Introduction

Due to the diminishing fossil fuel resources and the soaring global energy demands, the development of renewable energy sources has gained an increasing attention in recent years. Biodiesel, typically consisting of fatty acid methyl ester (FAME), can be produced by a transesterification of vegetable oil or animal fat with methanol in the presence of a suitable catalyst. Because of its renewable nature, environmentally friendly properties as well superior performance during the combustion process, biodiesel is a promising alternative to the traditional fossil diesel fuel <sup>1-5</sup>.

Two kinds of catalysts, homogeneous and heterogeneous catalysts, have been used for the transesterification reaction. Although homogenous catalysts allow transesterification to be performed in a shorter reaction time under moderate operating conditions, the catalyst separation and biodiesel purification steps will produce a large amount of waste water leading to an increase in production cost and environmental pollution <sup>6-9</sup>. Therefore, the research has been directed towards the development of heterogeneous catalysts. A serial of solid acid catalysts based on sulfated metal oxides had been prepared by Dimian et al. and used for the fatty acid esterification <sup>10,11</sup>. However, for the transesterification reaction, the performances of solid acid catalysts are still inferior compared with the solid base catalysts <sup>12</sup>. For this reason, a variety of heterogeneous solid base catalysts have been examined in transesterification reactions for biodiesel synthesis 12-16.

Among these solid base catalysts, CaO is the best-known and most intensively investigated system for its economy and reactivity <sup>17-19</sup>. However, some reports indicated that pure CaO catalyst was sensitive to atmospheric CO<sub>2</sub>, and it slightly dissolved in methanol during the transesterification process <sup>17,20,21</sup>. In addition to that, the mechanical strength of CaO particle is weak, which leads to the collapse of catalyst in a reactor and limits its industrial application <sup>21,22</sup>. In order to improve the stability of CaO catalyst, a strategy of combining CaO with other metal oxides is adopted <sup>23,24</sup>. Recently, the mixed oxide catalysts of Ca and Zr were popularly used for the transesterification reactions, and an excellent catalytic performance could be achieved <sup>25-29</sup>.

The traditional methods, such as co-precipitation <sup>25-27</sup>, impregnation <sup>26,28</sup>, physical mixing <sup>26</sup> and sol-gel <sup>29</sup>, have been employed to prepare CaO-ZrO mixed oxide catalysts. However, most of these methods suffer from either the procedures of complexity and time-consuming or the requirement of expensive starting materials. Especially, a calcination process with high temperature of 700-900 °C and long-time is indispensable, which will result in a phenomenon of catalyst agglomeration and further diminish the catalytic activity. Compared with these traditional methods, combustion synthesis, based on the principles of the propellant chemistry, has been extensively used to prepare mixed oxide catalysts for its advantages of applying inexpensive raw materials, maintaining a relatively simple and fast preparation process, and achieving

ARTICLE

fine powders with high homogeneity <sup>30-33</sup>. To our best knowledge, there is no article regarding the synthesis of CaO-ZrO solid base catalyst using the combustion method.

In this work, CaO-ZrO solid base catalysts with the molar ratio ranged from 4/6 to 9/1 for the transesterification of soybean oil were prepared by urea-nitrate combustion method without a further high temperature and longtime calcinations step. The combustion reactions are analyzed in terms of propellant chemistry and the combustion behaviors are detected. The prepared CaO-ZrO catalysts have been examined by various characterization techniques. The effects of Ca/Zr molar ratio on the physicochemical property and catalytic activity were emphasized. Furthermore, the relationship between the basicity and catalytic activity of the catalysts for transesterification were discussed in detail.

#### 2. Experimental

#### 2.1. Catalyst preparation

A serial of CaO-ZrO<sub>2</sub> catalysts with different Ca/Zr molar ratios were prepared using urea-nitrate combustion method. Firstly, Ca(NO<sub>3</sub>)<sub>2</sub>·4H<sub>2</sub>O and Zr(NO<sub>3</sub>)<sub>4</sub>·5H<sub>2</sub>O (AR grade, Shanghai Chemical Reagent Corporation, Shanghai, China) were mixed with a small quantity of deionized water in a basin. The resulting mixture was stirred and heated at 80 °C until a transparent aqueous solution was obtained. Then the required amount of urea was slowly added to the metal nitrate solution under constant stirring. Afterward, the basin was introduced in an open muffle furnace preheated at 500 °C. The solution started boiling and frothing, and in a short time ignited spontaneously with rapid evolution of a large quantity of gases, yielding a foamy, voluminous powder. The maximum temperature reached during the combustion process was measured with a Chrome-Alumel (K type) thermocouple whose hot junction was placed right over the mouth of the basin. The synthesized catalysts are denoted as C<sub>x</sub>Z<sub>y</sub>, where x and y represent the atomic concentration of Ca and Zr, respectively. In addition, in order to make a comparison, a typical CaO-ZrO<sub>2</sub> catalyst with Ca/Zr molar ratio of 8/2 was prepared by the conventional carbonate co-precipitation method described previously <sup>25</sup>.

#### 2.2. Catalyst characterization

The dried semi-solid gel obtained by heating the precursor at 80  $^{\circ}$ C for 8 hours was collected prior to combustion reaction for a thermal analysis measurement. The thermal gravimetric and differential scanning calorimetry (TG-DSC) profiles were recorded on a thermal analyzer (STA 449-F3, NETZSCH) at a heating rate of 5  $^{\circ}$ C/min under a continuous flow of air.

X-ray diffraction (XRD) patterns were recorded with a PANalytical X'Pert diffractometer operating with Ni  $\beta$ -filtered Cu K $\alpha$  radiation at 40 kV and 40 mA. Two theta angles ranged from 10 to 70° with a speed of 6° per minute.

Full nitrogen adsorption/desorption isotherms at -196 °C were obtained after outgassing the sample under vacuum at 200 °C for 4 h, using a Micromeritics ASAP2020 M+C adsorption

apparatus. Specific surface area ( $S_{BET}$ ) was calculated using a value of 0.162 nm<sup>2</sup> for the cross-sectional area of the nitrogen molecule.

The surface morphology was observed by the scanning electronic microscopy (SEM, S-3400N, Hitachi). The samples were coated with gold using a sputter coater.

The basicity of the catalysts was measured by  $CO_2$  temperature-programmed desorption ( $CO_2$ -TPD). Prior to the adsorption of  $CO_2$ , the catalysts were heated at 600 °C for 60 min to clean the surface from moisture and other adsorbed gases. After cooling to room temperature, the catalyst was saturated with  $CO_2$  at 50 °C for 60 min, and then flushed with He flow to remove any physisorbed molecules. Afterward, the TPD experiment was started with a heating rate of 5 °C/min under He flow, and the desorbed  $CO_2$  was detected by a thermal conductivity detector (TCD). The amount of the desorbed  $CO_2$  was quantified by comparing the integrated area of the TPD curves to the peak area of the injected  $CO_2$  calibration pulse.

<sup>1</sup>H nuclear magnetic resonance (<sup>1</sup>H NMR) spectra were recorded on a Bruker AVANCE-III 500 spectrometer with tetramethylsilane as the internal reference using  $CDCl_3$  as a solvent in all cases.

#### 2.3. Transesterification reaction

The transesterification reactions (Scheme 1) were carried out in a 250 ml three-neck round bottom flask, equipped with a watercooled reflux condenser and a magnetic stirrer. The reaction procedure was as follows: First, the catalyst was dispersed in methanol under a stirring rate of 500 rpm. Then, the soybean oil (purchased from Shanghai Jiali Oil Plant, acid value < 0.2 mg KOH/g) was added into the mixture and heated to a controlled temperature of 65 °C by an oil bath. To monitor the progress of reaction, a sample (0.5 ml) was withdrawn by drip tube each time from the reaction mixture at an interval of 0.5 h, and then centrifuged to get phase separation. Before the analysis of FAME yield, the upper layer was washed three times with brine to ensure complete removal of glycerol and alkali, and finally dried over anhydrous MgSO<sub>4</sub>.

$H_{2}C-OCOR_{1}$ $I$ $HC-OCOR_{2} + 3 CH_{3}OH \xrightarrow{\text{catalyst}}$ $I$ $H_{2}C-OCOR_{2}$	H <sub>2</sub> C-OH   HC-OH +   H <sub>2</sub> C-OH	R1COO-CH3 R2COO-CH3 R3COO-CH3
<i>Triglyceride</i> icheme 1 Transesterification of triglycerides	<i>Glycerol</i> with methanol.	FAME

#### 2.4. Product analysis

<sup>1</sup>H NMR technique was employed to estimate the yield of FAME using the following formula <sup>34</sup>

$$Y\% = \frac{2A_1}{3A_2} \times 100$$

where  $A_1$  and  $A_2$  are the areas of <sup>1</sup>H NMR peaks corresponding to the methoxy protons (CH<sub>3</sub>O-) in the methyl ester at chemical shifts of 3.68 ppm (singlet peak) and

#### 3. Results and discussion

methylene carbons.

#### 3.1. Combustion reaction analysis and combustion behavior

For urea-nitrate combustion, primarily N2, CO2, and H2O are evolved as the gaseous products <sup>35,36</sup>. Thus, the combustion reactions in the present paper can be represented as follows:

### $x Ca(NO_3)_2 \cdot 4H_2O + y Zr(NO_3)_4 \cdot 5H_2O + m CO(NH_2)_2 + (3m - 1)_2 \cdot 5H_2O + m CO(NH_2)_2 + m C$ $5x-10y)/2 O_2 \rightarrow (CaO)_x(ZrO_2)_y + (x+2y+m) N_2 + m CO_2 +$ $(4x+5y+2m) H_2O$

According to the principle of propellant chemistry <sup>37</sup>, for stoichiometric redox reaction between a fuel and an oxidizer, the ratio of the net oxidizing valence of the metal nitrate to the net reducing valence of the fuel should be unity. In this case, 1 mol  $C_x Z_y$  stoichiometrically requires (5x+10y)/3 mol urea (i.e. m = (5x+10y)/3) without the necessity of getting oxygen from atmosphere. When the urea amount is smaller than that of stoichiometry, the combustion reaction is called a fuel-deficient reaction. For this case, the value of (3m-5x-10y) would be negative, suggesting that O<sub>2</sub> would be evolved in the products. However, when the urea amount is larger than that of stoichiometry, corresponding to a fuel-rich reaction, atmospheric O<sub>2</sub> had been involved ensuring the complete combustion of urea.

It is well known that the fuel content is one of the most important parameters in combustion synthesis. To investigate the influence of fuel amount on the combustion reaction, the urea amount of 50% (fuel-deficient), 100% (stoichiometric) and 150% (fuel-rich) of stoichiometric amount were employed for the synthesis of the C<sub>x</sub>Z<sub>y</sub> sample. It was experimentally observed that the combustion appears in a smoldering manner for the fuel-deficient precursor. On the other hand, the stoichiometric and fuel-rich precursor exhibited incandescent flame growing after auto-ignition, and the autoignition of the latter was found to be more violent compared to that of the former. This means that the combustion intensity enhances with the increase in urea amount, and similar result had been reported in the literature <sup>32,38</sup>. Hereinafter, 150% of stoichiometric amount urea was adopted to achieve a full decomposition of nitrate, urea and possible carbon residues produced in the combustion process.

The highest flame temperatures measured with the thermocouple appear at 1000-1100 °C for the samples with different Ca/Zr ratio, and the duration of combustion is about one minute. Certainly, the highest flame temperature also can be thermaldynamically estimated under the assumption that the combustion is an adiabatic process. Because of heat losses. incomplete combustion, and heating of air, it can be conceived that the measured flame temperatures were lower than the theoretical adiabatic flame temperatures <sup>39</sup>.

The combustion behavior of the dried gel collected prior to decomposition was also monitored by TG-DSC. A typical TG-DSC plot for the  $C_8Z_2$  sample is shown in Fig. 1. It can be seen that a weight loss of about 4% with a concurrent endothermic peak locates at 30-160 °C, which is attributed to the vaporization of physically absorbed water and the dehydration reaction of gels. Another weight loss stage occurs at 160-240 °C. It is associated with an endothermic peak centered at 210 °C and can be assigned to the decomposition of a small amount zirconium nitrate. In the temperature range of 240-550 °C, a huge weight loss accompanied by a marked exothermic effect clearly indicates the combustion reaction between urea and NO3-. At temperature above 600 °C, the weight loss is negligible, and this indicates that the decomposition of precursor completed before 600 °C. The total weight loss determined for the production of  $C_8Z_2$  was 77.3%, and it was approximate to the theoretical value of 81.5%. These results of thermoanalysis confirm that Ca-Zr complex oxide can be synthesized effectively during the combustion reaction although the duration of combustion is rather short, requiring no further calcinations at such a high temperature of 800 °C, which is employed necessarily in the preparation of Ca-based solid base with traditional methods 40.



Fig. 1. TG and DSC profiles for the dried gel of C<sub>8</sub>Z<sub>2</sub> sample.

#### 3.2. Structure and texture of the catalysts

The XRD patterns of CaO-ZrO<sub>2</sub> catalysts with varied Ca/Zr molar ratios were shown in Fig. 2 (A). The diffraction peaks at  $2\theta$  of  $32.2^{\circ}$ ,  $37.3^{\circ}$ , and  $53.9^{\circ}$  are ascribed to CaO phase (JCPDS 070-4068). In the case of  $C_4Z_6$  and  $C_5Z_5$ , no diffraction lines of CaO are detected, suggesting that CaO is incorporated into ZrO<sub>2</sub> lattice to form homogenous CaO-ZrO<sub>2</sub> solid solution <sup>25,26,41</sup>. As the Ca/Zr ratio increase to 6/4, the diffraction peaks of CaO appear, and the relative intensity of the peaks increase with a further increase in the amount of Ca. This indicates that excessive Ca2+ cannot enter the solid solution and exist in the free CaO. The characteristic diffraction peaks of CaZrO<sub>3</sub> (JCPDS 076-2401) corresponding to the crystallized solid

Exo.

ARTICLE

solution of CaO-ZrO<sub>2</sub>, were observed at  $2\theta$  of  $22.1^{\circ}$ ,  $31.5^{\circ}$ , and 45.1° for all investigated samples. With the increase in the Ca/Zr ratio, the intensity of CaZrO<sub>3</sub> diffraction peaks enhances firstly and then decrease, and a maximum is obtained for the  $C_6Z_4$  sample. This phenomenon can be explained as follows: When Ca/Zr ratio is below 6/4, a portion of ZrO<sub>2</sub> exist in tetragonal zirconia (t-ZrO<sub>2</sub>,  $2\theta = 30.3^{\circ}$ , 50.2°, JCPDS 88-1007), and it hinders the formation and crystallization of CaZrO<sub>3</sub>. An analogous depression effect of the free CaO phase on the formation and crystallization of CaZrO3 occurs as the Ca/Zr ratio higher than 6/4. A careful examination of the XRD pattern exhibited in Fig. 2 (B) reveals that the diffraction peaks of CaZrO<sub>3</sub> shift to lower degree from C<sub>4</sub>Z<sub>6</sub> to C<sub>9</sub>Z<sub>1</sub>. This is because that Zr<sup>4+</sup> (radius 0.86 Å) in CaZrO<sub>3</sub> was substituted by Ca<sup>2+</sup> cations (radius 0.99 Å) resulting an increase in the crystal lattice parameter <sup>26</sup>. Moreover, as shown in Fig. 2 (A), a diffraction peak at  $2\theta$  of  $29.4^{\circ}$  identical to the incompletely decomposed CaCO<sub>3</sub>, which may be produced during the combustion reaction and/or the air-exposure, is detected for the samples of C<sub>7</sub>Z<sub>3</sub>, C<sub>8</sub>Z<sub>2</sub> and C<sub>9</sub>Z<sub>1</sub>, and its intensity increase with the increase in Ca/Zr molar ratio.



**Fig. 2.** (A) XRD patterns of the as-prepared CaO-ZrO<sub>2</sub> catalysts with different Ca/Zr molar ratio, (B) magnification XRD patterns of the CaZrO<sub>3</sub> phase in CaO-ZrO<sub>2</sub> catalysts. ( $\blacktriangle$ ) CaO; ( $\bigstar$ ) ZrO<sub>2</sub> (tetragonal); ( $\blacksquare$ ) CaZrO<sub>3</sub> (monoclinic); ( $\bullet$ ) CaCO<sub>3</sub>.

To estimate the effect of high temperature and longtime calcination procedure on the CaO-ZrO<sub>2</sub> structure, the  $C_8Z_2$  sample prepared by combustion method was further calcined at 800 °C for 6 h and examined by XRD. As shown in Fig. 2(A),

the diffraction patterns of the as-prepared samples with/without a calcination procedure show no significant differences except the disappearance of a tiny diffraction peak of  $CaCO_3$  after calcining. These results indicate that the temperature during the combustion reaction is high enough to promote the synthesis of  $CaO-ZrO_2$  in spite of a short reaction time. This is in agreement with the result of TG-DSC. Again, calcining step at a higher temperature only promote the degree of crystallinity and the grain growth.

Table 1. BET surface area, pore volume of CaO-ZrO2	2
catalysts with different Ca/Źr molar ratios and the TO	F for
FAME formation.	

Catalyst	$S_{BET}$ (m <sup>2</sup> /g)	Pore volume (cm <sup>3</sup> /g)	TOF×10 <sup>3</sup> (s <sup>-1</sup> ) <sup>a</sup>
$C_4Z_6$	6.87	0.0145	b
$C_5Z_5$	3.86	0.0101	36.3
$C_6Z_4$	2.77	0.0075	49.1
$C_7Z_3$	2.54	0.0063	49.9
$C_8Z_2$	2.50	0.0062	55.6
$C_9Z_1$	1.84	0.0015	42.8

<sup>a</sup> Reaction conditions: catalyst loading=1.25 wt.%, methanol to oil molar ratio=25:1, reaction temperature =65 °C, reaction time=1 h. <sup>b</sup> The FAME Yield is too low to be detected under the reaction conditions.



Fig. 3. SEM micrograph of the  $C_8Z_2$  sample

The BET surface area and the pore volume measured by nitrogen physisorption for CaO-ZrO<sub>2</sub> catalysts are presented in Table 1. An increase in the Ca amount leads to a gradual decrease in the BET surface area and the minimum is  $1.84 \text{ m}^2/\text{g}$  for the C<sub>9</sub>Z<sub>1</sub> sample. The similar variation was observed for the pore volume of catalysts. This is because that the specific surface area of CaO is much lower than that of ZrO<sub>2</sub><sup>42</sup>; as the Ca/Zr range from 4/6 to 9/1, the independent phase of ZrO<sub>2</sub> vanishes accompanying the appearance of separated CaO phase. Moreover, the decrease in the surface area and pore volume is also related to the partial blocking of the pores in catalysts by CaO <sup>19,22,43</sup>.

Fig. 3 shows the SEM micrograph of the as-prepared  $C_8Z_2$  sample. A cluster of uniform flakes with the thickness less than 0.2  $\mu$ m was observed. The agglomeration is not significant

although the sample suffer from a combustion process with a high temperature of 1000 °C. This can be ascribed to the short duration of combustion and the evolution of a large quantity of gases, which hinder the agglomeration of the CaO-ZrO<sub>2</sub> mixed oxide.

#### 3.3. Basicity of the catalysts

The surface base properties of catalysts were investigated by CO<sub>2</sub>-TPD technique, and the CO<sub>2</sub> desorption profiles obtained for CaO-ZrO2 with different Ca/Zr molar ratios are presented in Fig. 4. It can be seen that a desorption peak (denoted as  $\alpha$ ) appears at 450-550 °C for all samples. The intensity of  $\alpha$  peak increases first and then decreases with increasing the Ca/Zr ratio, and a maximum is obtained over the  $C_6Z_4$  sample. The  $\alpha$ peak is attributed to the interaction of CO<sub>2</sub> with the strong basic sites on the surface of CaZrO<sub>3</sub><sup>26,42</sup>. In the temperature range of 520-650 °C, the catalysts with Ca/Zr ratio of  $\geq 6/4$  exhibit another desorption peak (denoted as  $\beta$ ), and it is related to the stronger basic site of the free CaO aggregated on the surface of the catalysts <sup>26</sup>. Moreover, a negligible desorption peak located at 125  $^{o}\mathrm{C}$  can be detected only for the samples of  $\mathrm{C}_{4}\mathrm{Z}_{6}$  and  $C_5Z_5$ , which corresponds to the surface weak basic site of  $ZrO_2$  $^{26,44}$ . The results of the CO<sub>2</sub> desorption profiles with various Ca/Zr molar ratio coincide with that of XRD pattern aforementioned. It is noteworthy that with the increase in Ca/Zr molar ratios,  $\alpha$  and  $\beta$  peaks shift toward higher temperature, suggesting a continuous increase in the strength of basic sites, and the maximum of peaks are listed in Table 2. As well documented, the strong basicity over the surface of oxide is mainly originated from the isolated (or low coordination) oxygen anions <sup>34,41,45,46</sup>; the greater an oxygen anion's electrodonating is, the stronger its Lewis basicity will be. The results of the XRD had shown that more Zr<sup>4+</sup> neighboring O<sup>2-</sup> anion were substituted by Ca<sup>2+</sup> with increasing the Ca/Zr ratio. Because the electronegativity of Ca<sup>2+</sup> is smaller than that of Zr<sup>4+ 26</sup>, the electrodonating property of oxygen anions over the surface of CaZrO<sub>3</sub> enhance with the increase in Ca/Zr ratio, resulting in the increase in the strength of basic sites and the shift of  $\alpha$  peak toward higher temperature. As  $\beta$  peak is concerned, the shift of peak may relate to the interaction between CaO and ZrO2, which will weaken the basicity of CaO. With the increase in CaO content, more CaO was separated from the mixed oxide and aggregated on the surface, as shown in XRD pattern, accompanying with a decrease in the interaction between CaO and ZrO<sub>2</sub>.

The number of different base site was evaluated by calculating the integral of each peak, and the data were summarized in Table 2. As shown in Table 2, the number of  $\alpha$  basic site takes on a volcanic variation trend with the elevation of Ca/Zr ratio, and a maximum of 0.299 mmol/g is observed for C<sub>6</sub>Z<sub>4</sub>. In the case of  $\beta$  basic site, the number increases continuously from C<sub>6</sub>Z<sub>4</sub> to C<sub>9</sub>Z<sub>1</sub>. It should be noted that the amount of CO<sub>2</sub> derived from  $\beta$  peak include the contribution of the decomposition of residual CaCO<sub>3</sub>, which exists in the catalysts with Ca/Zr ratio above 7/3 (see Fig. 2 (A)). Similar results were reported by some authors <sup>44,47</sup>, and they treat the

Page 6 of 9

incompletely decomposed CaCO<sub>3</sub> as structural carbonate. Furthermore, it can be seen that the total basicity is low for  $C_4Z_6$  and  $C_5Z_5$ , and an abrupt increase is observed when the Ca/Zr ratio increase to 6/4, and then the fluctuation of the total basicity slows down. The sequence of total basic sites number is reverse to that of BET surface shown in Table 1. Similar result was reported by Kouzu et al. for CaO solid base catalysts <sup>48</sup>.



Fig. 4. CO<sub>2</sub>-TPD curves of CaO-ZrO<sub>2</sub> catalysts with different Ca/Zr molar ratio.

**Table 2.** The maximum temperature of  $CO_2$  desorption and the amount of basic site over Ca-ZrO<sub>2</sub> catalysts with different Ca/Zr molar ratio.

Catalyst	Tα ( °C)	$T\alpha (T_{\beta})$	Number of basic sites (mmol/g)		Number of total basic sites (mmol/g)
	0)	( 0)	Site á	Site â	sites (minor g)
$C_4Z_6$	481	-	0.046	-	0.046
$C_5Z_5$	490	-	0.083	-	0.083
$C_6Z_4$	507	531	0.299	0.094	0.393
$C_7Z_3$	518	553	0.277	0.174	0.451
$C_8Z_2$	530	577	0.233	0.419	0.652
$C_9Z_1$	542	613	0.156	0.426	0.582

#### 3.4. Catalytic activity of the catalysts

The FAME yield over CaO-ZrO<sub>2</sub> catalysts with different Ca/Zr ratios as a function of reaction time were presented in Fig. 5. Since the transesterification is a reversible reaction, a high methanol/oil ratio is favorable to shift the equilibriumin towards the direction of FAME formation. Moreover, the excess methanol accelerates the remove of product molecules from the catalyst surface and further the regeneration of the active sites <sup>28</sup>. Therefore, a high methanol/oil molar ratio of 25:1 was employed in this study, and similar value of methanol/oil ratio could be found in the literature <sup>21,44,49</sup>. It is reported that the mass transfer would be the rate determining step when the catalyst amount is high <sup>19,49</sup>. In order to diminish the influence of mass transfer limitation, a low content of catalyst dosage (1.25 wt.% of oil) was used. The reaction was run at 65 °C corresponding to the boiling point of methanol under atmosphere pressure. It can be seen from Fig.5 that the FAME yield increases rapidly first with the increase in reaction time, and then reaches a steady region. The  $C_8Z_2$  sample exhibits the highest catalytic activity, and the FAME yield of 93.9% and 98% were obtained after 2 and 3 h reaction time, respectively. However, the FAME yields over the  $C_4Z_6$  and  $C_5Z_5$  samples are less than 15% even in a reaction time of 3 h. In general, the profile of the FAME yield against the reaction time takes on a shape of sigmoid, and the whole period can be divided into three stages <sup>13,17,19</sup>. At the initial stage, the reaction rate, which depends on the rate of mass transfer of the reactants, is quite low. Then, an abrupt increase in reaction rate appears, and this stage corresponds to the chemical reaction controlled regime. Finally, the reaction becomes slow again at the third stage for the reason of thermodynamic equilibrium. In this study, the absence of the stage of mass transfer limitation may be ascribed to the selection of reaction condition aforementioned.

The catalytic activity over the  $C_8Z_2$  sample prepared by carbonate co-precipitation method was also presented in Fig. 5, for the purpose of comparison. It is obvious that the catalyst prepared by carbonate co-precipitation method is less active for the biodiesel synthesis. For example, after 2 h reaction time, the FAME yield over the  $C_8Z_2$  sample prepared by carbonate coprecipitation is 58.2%, which is far below the value of 93.9% over the counterpart prepared by combustion method. The hightemperature and long-time calcination step was involved during the preparation, which might be responsible for the low FAME yield over the CaO-ZrO<sub>2</sub> catalyst prepared by the coprecipitation method.

To check the possibility of leaching, an experiment was carried out according to the literature <sup>22</sup>. The  $C_8Z_2$  sample prepared by combustion method was placed in contact with methanol under the same conditions as used in the transesterification process, except for the presence of soybean oil. After 3 h of contact, the catalyst was removed by filtration and the recovered methanol was used for transesterification reaction of soybean oil. The reaction was maintained at 65 °C for 3 h, and a FAME yield of about 2% was obtained. This result indicates that the leached active species contributed slightly to the transesterification of soybean oil with methanol.

The studies of mechanism of transesterification reaction illustrate that the role of the basic sites is to abstract proton from organic matter and then develop a series of nucleophile such as methoxide anions, mono-glyceroxide and diglyceroxide anions, which initiates the transesterification reaction 3,22,50. Therefore, it is significant to explore the relationship between the catalytic activity and the basicity of the catalysts. The variation of the FAME yield and the total amount of basic sites with the Ca/Zr molar ratio were presented in Fig. 6 together. The value of FAME yield are collected at reaction time of 1.0 h, to ensure that the transesterification reaction are in the chemical reaction controlled regime. Apparently, except for the  $C_9Z_1$  sample, the variation of the FAME yield with the change of Ca/Zr ratio correlates well with that of total amount of basic sites. The deviation of  $C_9Z_1$  can be ascribed to that the evaluations of basic sites for C<sub>9</sub>Z<sub>1</sub> by integrating the peak area of CO2-TPD profile include partial  $CO_2$  originated from the decomposition of structural CaCO<sub>3</sub>, as mentioned above in CO<sub>2</sub>-TPD.



Fig. 5. Effect of reaction time on the FAME yield. Reaction conditions: catalyst loading=1.25 wt.%, methanol to oil molar ratio=25:1, reaction temperature =65 °C.



**Fig. 6.** Effect of Ca/Zr molar ratio on the FAME yield and the total basic sites. Reaction conditions: catalyst loading=1.25 wt.%, methanol to oil molar ratio=25:1, reaction temperature =65 °C, and reaction time=1.0 h.

TOF (turnover frequency) of FAME formation (at reaction time of 1.0 h), which represents the molecular number of FAME formed per second per basic site, have been calculated for CaO-ZrO<sub>2</sub> catalysts and the results are listed in Table 1. It can be seen that the values of TOF increase from 36.3 to  $55.6 \times 10^{-3}$  s<sup>-1</sup> with the Ca/Zr ratio varied from 5/5 to 8/2, which approximate to the values  $(32.8-85.0\times10^{-3} \text{ s}^{-1})$  reported by Song et al. <sup>51</sup>. Conditioning on that the active sites involved in the rate-determining step are all equally active, the value of TOF should be a constant 52. As mentioned above, for the transesterication of soybean oil with methanol over CaO-ZrO<sub>2</sub> catalysts, there are two type basic sites (i.e. active sites), which results from the isolated (or low coordination) oxygen anion over the surface of CaZrO<sub>3</sub> and CaO, respectively. Simultaneously, the results of CO<sub>2</sub>-TPD revealed that the strength of the two type basic sites increased continuously with increasing the Ca/Zr ratio. Ding et al. <sup>14</sup> reported that the stronger basicity a catalyst had, the higher transesterication activity could be achieved, and the same viewpoint was suggested by Kouzu et al.<sup>17</sup>. Thereby, the values of TOF

increase from  $C_5Z_5$  to  $C_8Z_2$ . As for the  $C_9Z_1$  sample, though it possesses the stronger basic site, the value of TOF is lower than that of  $C_8Z_2$ , and the reason may also attribute to the error of the evaluation of basic sites. Based on these results, it can be summarized that the catalytic activity are related to both the amount and strength of basic sites.

#### 4. Conclusions

CaO-ZrO<sub>2</sub> catalysts with Ca/Zr ratios ranged from 4/6 to 9/1 were prepared via urea-nitrate combustion method, and used to catalyze transesterification of soybean oil with methanol for the biodiesel synthesis. The influences of Ca/Zr ratio on the physicochemical and catalytic properties of catalysts were investigated. Based on the results of this work, the following conclusions can be made:

- 1. The urea-nitrate combustion method was demonstrated to be a simple, fast and effective method for the preparation of  $CaO-ZrO_2$  solid base catalysts without a further high temperature and longtime calcination step.
- 2. The substitution occurs between Zr<sup>4+</sup>and Ca<sup>2+</sup>, and a new phase of CaZrO<sub>3</sub> has been formed for the investigated CaO-ZrO<sub>2</sub> catalysts.
- 3. With the increase in Ca/Zr molar ratio, the BET surface decrease, whereas the total basic sites increase and a maximum is obtained over the  $C_8Z_2$  sample.
- 4. With the increase in Ca/Zr molar ratio, the strength of the basic site becomes stronger, resulting in a higher turnover frequency (TOF) for transesterification reaction.
- 5. The sequence of catalytic activity for the synthesis of biodiesel is in agreement with the total basic sites and the catalyst with Ca/Zr ratios of 8/2 exhibits the highest catalytic activity.

#### Acknowledgements

The authors thank Shanghai Municipal Education Commission (No. 13YZ117), Shanghai Municipal Science and Technology Commission (No. 13ZR1441200) and the National Natural Science Foundation of China (No. 21273150) for financial support.

#### Notes and references

Research Institute of Applied Catalysis, School of Chemical and Environmental Engineering, Shanghai Institute of Technology, Shanghai 200235, P. R. China.

\* Corresponding author. Tel/Fax: (+86)-21-60873301, E-mail: <u>guoxiaoming@sit.edu.cn</u> (X. Guo)

- 1 F. Ma, M.A. Hanna, Bioresour. Technol., 1999, 70, 1.
- 2 S.A. Basha, K.R. Gopal, S. Jebaraj, *Renew. Sust. Energ. Rev.*, 2009, 13, 1628.
- 3 E. Santacesaria, G.M. Vicente, M. Di Serio, R. Tesser, *Catal. Today*, 2012, **195**, 2.
- 4 Y. Kuwahara, K. Tsuji, T. Ohmichi, T. Kamegawa, K. Mori, H. Yamashita, *Catal. Sci. Technol.*, 2012, **2**, 1842.

- 5 M. Kim, C. DiMaggio, S.O. Salley, K.Y. Simon Ng, *Bioresour*. *Technol.*, 2012. 118, 37.
- 6 D.E. Lopez, J.G. Goodwin Jr., D.A. Bruce, E. Lotero, *Appl. Catal. A: Gen.*, 2005, **295**, 97.
- 7 Y.H. Li, B. Ye, J.W. Shen, Z. Tian, L.J. Wang, L.P. Zhu, T. Ma, D.Y. Yang, F.X. Qiu, *Bioresour. Technol.*, 2013, **137**, 220.
- 8 J. Tantirungrotechai, S. Thepwatee, B. Yoosuk, Fuel, 2013, 106, 279.
- 9 A. C. Dimian, Z. W. Srokol, M. C. Mittelmeijer-Hazeleger, G. Rothenberg, *Top. Catal.*, 2010, 53, 1197.
- 10 M. L. Grecea, A. C. Dimian, S. Tanase, V. Subbiah, G. Rothenberg, *Catal. Sci. Technol.*, 2012, 2, 1500.
- 11 A. A. Kiss, A. C. Dimian, G. Rothenberg, *Energy Fuels*, 2008, 22, 598.
- 12 Z.Z. Wen, X.H. Yu, S.T. Tu, J.Y. Yan, E. Dahlquist, *Appl. Energ.*, 2010, 87, 743.
- 13 V.G. Deshmane, Y.G. Adewuyi, Fuel, 2013, 107, 474.
- 14 Y.Q. Ding, H. Sun, J.Z. Duan, P. Chen, H. Lou, X.M. Zheng, *Catal. Commun.*, 2011, **12**, 606.
- 15 M. Kouzu, M. Tsunomori, S. Yamanaka, J. Hidaka, Adv. Powder Technol., 2010, 21, 488.
- 16 W. Roschat, M. Kacha, B. Yoosuk, T. Sudyoadsuk, V. Promarak, *Fuel*, 2012, 98, 194.
- 17 M. Kouzu, J.S. Hidaka, Fuel, 2012, 93, 1.
- 18 X.J. Liu, H.Y. He, Y.J. Wang, S.L. Zhu, X.L. Piao, Fuel, 2008, 87, 216.
- 19 H.T. Wu, J.H. Zhang, Q. Wei, J.L. Zheng, J.A. Zhang, *Fuel Process. Technol.*, 2013, **109**, 13.
- 20 S. Gryglewicz, Bioresour. Technol., 1999, 70, 249.
- 21 L.S. Hsieh, U. Kumar, J.C.S. Wu, Chem. Eng. J., 2010, 158, 250.
- 22 N. Pasupulety, K. Gunda, Y.Q. Liu, G.L. Rempel, F.T.T. Ng, Appl. Catal. A: Gen., 2013, 452, 189.
- 23 Y.L. Meng, B.Y. Wang, S.F. Li, S.J. Tian, M.H. Zhang, *Bioresour*. *Technol.*, 2013, **128**, 305.
- 24 H. Sun, J.Z. Duan, P. Chen, H. Lou, X.M. Zheng, *Catal. Commun.*, 2011, **12**, 1005.
- 25 A.M. Dehkordi, M. Ghasemi, Fuel Process. Technol., 2012, 97, 45.
- 26 H. Wang, M.H. Wang, S.G. Liu, N. Zhao, W. Wei, Y.H. Sun, J. Mol. Catal. A: Chem., 2006, 258, 308.
- 27 H. Wang, S.G. Liu, W.Y. Zhang, N. Zhao, W. Wei, Y.H. Sun, Acta. Chim. Sin., 2006, 64, 2409.
- 28 N. Kaur, A. Ali, Fuel Process. Technol., 2014, 119, 173.
- 29 J.B. Chen, J.W. Su, J.M. Qi, X.X. Chen, L. Chen, Chin. J. Appl. Chem., 2011, 28, 267.
- 30 K.C. Patil, S.T. Aruna, T. Mimani, Curr. Opin. Solid. State. Mater. Sci., 2002, 6, 507.
- 31 J. Papavasiliou, G. Avgouropoulos, T. Ioannides, Appl. Catal. B: Enviro., 2006, 66, 168.
- 32 X.M. Guo, D.S. Mao, S. Wang, G.S. Wu, G.Z. Lu, *Catal. Commun.*, 2009, **10**, 1661.
- 33 X.M. Guo, D.S. Mao, G.Z. Lu, S. Wang, G.S. Wu, J. Catal., 2010, 271, 178.
- 34 G. Gelbard, O. Bres, R.M. Vargas, F. Vielfaure, U.F. Schuchardt, J. Am. Oil Chem. Soc., 1995, 72, 1239.
- 35 R.D. Purohit, B.P. Sharma, K.T. Pillai, A.K. Tyagi, *Mater. Res. Bull.*, 2001, **36**, 2711.

#### Page 9 of 9

ARTICLE

#### **RSC** Advances

- 36 M.J. de Andrade, M.D. Lima, R. Bonadiman, C.P. Bergmann, *Mater. Res. Bull.*, 2006, **41**, 2070.
- 37 S.R. Jain, K.C. Adiga, V.R. Pai Verneker, *Combust. Flame*, 1981, 40, 71.
- 38 D.A. Fumo, M.R. Morelli, A.M. Segadães, *Mater. Res. Bull.*, 1996, 31, 1243.
- 39 J.C. Toniolo, M.D. Lima, A.S. Takimi, C.P. Bergmann, *Mater. Res. Bull.*, 2005, 40, 561.
- 40 C. Liu, P.M. Lv, Z.H.Yuan, F. Yan, W.Luo, *Renew. Energ.*, 2010, **35**, 1531.
- 41 W.N.N.W. Omar, N.A.S. Amin, Fuel Process. Technol., 2011, 92, 2397.
- 42 H. Wang, M.H. Wang, W.Y. Zhang, N. Zhao, W. Wei, Y.H. Sun, *Catal. Today*, 2006, **115**, 107.
- 43 Y.H.T. Yap, H.V. Lee, R. Yunus, J.C. Juan, *Chem. Eng. J.*, 2011, **178**, 342.

- 46 V.K. Díez, C.R. Apesteguía, J.I. Dí Cosimo, *Catal. Today*, 2000, 63, 53.
- 47 S. Sato, R. Takahashi, M. Kobune, H. Gotoh, *Appl. Catal. A: Gen.*, 2009, **356**, 57.
- 48 M. Kouzu, T. Kasuno, M. Tajika, Y. Sugimoto, S. Yamanaka, J. Hidaka, *Fuel*, 2008, 87, 2798.
- 49 X.J. Liu, X.L. Piao, Y.J. Wang, S.L. Zhu, H.Y. He, Fuel, 2008, 87, 1076.
- 50 M. Kouzu, T. Kasuno, M. Tajika, S. Yamanaka, J. Hidaka, *Appl. Catal. A: Gen.*, 2008, **334**, 357.
- 51 R.L. Song, D.M. Tong, J.Q. Tang, C.W. Hu, *Energ. Fuel*, 2011, **25**, 2679.
- 52 M. Boudart, Chem. Rev., 1995, 95, 661.

- 44 H. Sun, Y.Q. Ding, J.Z. Duan, Q.J. Zhang, Z.Y. Wang, H. Lou, X.M. Zheng, *Bioresour. Technol.*, 2010, **101**, 953.
- 45 M. Verziu, B. Cojocaru, J. Hu, R. Richards, C. Ciuculescu, P. Filip, V.I. Parvulescu, *Green Chem.*, 2008, **10**, 373.