

This is an *Accepted Manuscript*, which has been through the Royal Society of Chemistry peer review process and has been accepted for publication.

Accepted Manuscripts are published online shortly after acceptance, before technical editing, formatting and proof reading. Using this free service, authors can make their results available to the community, in citable form, before we publish the edited article. This Accepted Manuscript will be replaced by the edited, formatted and paginated article as soon as this is available.

You can find more information about *Accepted Manuscripts* in the **Information for Authors**.

Please note that technical editing may introduce minor changes to the text and/or graphics, which may alter content. The journal's standard <u>Terms & Conditions</u> and the <u>Ethical guidelines</u> still apply. In no event shall the Royal Society of Chemistry be held responsible for any errors or omissions in this *Accepted Manuscript* or any consequences arising from the use of any information it contains.



www.rsc.org/advances



42x21mm (300 x 300 DPI)

RSC Advances Accepted Manuscript

1	CDI Ragone Plot as a Functional Tool to Evaluate Desalination
2	Performance in Capacitive Deionization
3	
4	Taeyoung Kim and Jeyong Yoon*
5	
6	School of Chemical and Biological Engineering, Institute of Chemical Processes, Seoul
7	National University, Daehak-dong, Gwankak-gu, Seoul 151-742, Republic of Korea
8	
9	*The corresponding author
10	Jeyong Yoon
11	Daehak-dong, Gwankak-gu, Seoul 151-742, Republic of Korea
12	Tel: +82-2-880-8927
13	Fax: +82-2-876-8911
14	E-mail address: jeyong@snu.ac.kr
15	
16	Submitted to
17	RSC Advances Communication
18	

A novel concept to evaluate desalination performance in capacitive deionization (CDI) is proposed called the CDI Ragone plot. The plot can allows for intuitive acquisition of deionization capacity (mg/g), rate (mg/g/s), and time (s) and thus, will work as a functional tool to evaluate desalination performance in CDI.

23 Capacitive deionization (CDI) is a promising desalination process driven by 24 electrical potential and the consequent double layer formation on the surface of a porous electrode.^{1, 2} An excess of counter-ions in the double layer leads to a depletion of ions in the 25 region adjacent to the electrode surface; thus, desalinated water can be produced by 26 extracting the solution between the two electrodes. CDI has attracted much attention 27 compared to conventional desalination processes such as thermal distillation and reverse 28 osmosis (RO) because of its potential for an efficient energy use.^{3,4} Furthermore, the energy 29 consumed during desalination is simultaneously stored in electrodes because its configuration 30 31 and principle are similar to an energy storage device. Therefore, the stored energy can be conceptually recovered⁵⁻⁸, and a practical energy recovery system⁹⁻¹¹ facilitates low-energy 32 production of fresh water, although it still has a long way to go to realize such an ideal 33 desalination process at this moment. 34

So far, various attempts have been carried out to achieve an efficient desalination 35 performance. These approaches include synthesizing novel carbon materials¹²⁻¹⁷, modifying 36 carbon electrodes^{18, 19}, involving Faradaic reactions²⁰⁻²², incorporating ion-exchange 37 membranes or polymers²³⁻²⁵, altering operation methods²⁶, and developing new processes²⁷⁻²⁹. 38 No matter what strategy CDI implements, it is quite important to determine its desalination 39 40 performance based on an appropriate evaluation method. However, desalination performance has been reported in various ways; thus, CDI requires a standard method to evaluate the 41 42 desalination performance which could allow for further advancements in this area. Among

the various ways, two indicators have most frequently been reported as representing 43 44 performance, which are the capacity and rate of desalination. The desalination capacity shows the amount of removed ions per mass of electrodes, normally when the performance reaches 45 its equilibrium¹. On the other hand, the desalination rate indicates the kinetics of desalination 46 expressed as the rate constant¹⁷ or capacity divided by time^{25, 29}. However, these two 47 parameters have been separately provided at the specific condition, thus facile acquisition of 48 the overall desalination performance is difficult. Therefore, CDI requires a more advanced 49 evaluation method, determining the overall performance which includes the capacity and rate. 50

51 In this study, we propose a new concept to evaluate desalination performance in CDI called the CDI Ragone plot. Compared to the conventional Ragone plot for energy storage 52 53 devices, the CDI Ragone plot evaluates the desalination performance taking into 54 consideration both the capacity and rate, which allows for the intuitive acquisition of the 55 overall desalination performance based on a conventional operating method. Herein we show 56 an evaluation methodology and the implications of the CDI Ragone plot along with the effects of the various parameters, as a functional tool for examining desalination performance 57 58 in CDI.

Carbon composite electrodes were prepared with MSP-20 (Kansai Coke and 59 Chemicals, Japan), carbon black (Super P, Timcal), and polytetrafluoroethylene (PTFE, 60 61 Aldrich) binder (86:7:7 in weight ratio). A mixture containing these components was kneaded 62 with a few milliliters of ethanol until it solidified, and sheet-type electrodes were made by pressing with a roll-pressing machine. The desirable thickness was obtained by adjusting the 63 64 gap of the two rollers; the thickness was $\sim 300 \ \mu m$ unless otherwise specified. After the fabrication, the electrodes were dried in a vacuum oven at 120°C for 12 h. Other carbon 65 electrodes (S-51HF (Norit), YS-2 (Japan EnviroChemicals), CEP21 (Power Carbon 66

Technology, Korea), and MDC¹² (MOF-derived carbon)) were fabricated with the same
procedure.

A custom-built CDI cell was used to evaluate desalination performance, in which 69 70 built-in graphite current collectors were installed. A pair of round-shape carbon electrodes (20 71 mm in diameter) having a center hole (4 mm in diameter) was placed onto current collectors, 72 and each electrode was covered by anion- and cation-exchange membranes (selemion, AGC 73 ENGINEERING CO., LTD, Japan) with the same geometry as the electrode (membrane-74 assisted CDI, MCDI). Between the two ion-exchange membranes, a polymer spacer 75 (thickness=185 µm) was located to allow a feed solution to pass from the outside to the center 76 hole. After the assembly, the CDI cell was pressed and sealed off. A feed solution (2, 10, 50, 77 and 100 mM NaCl) was supplied to the CDI cell with a peristaltic pump (flow rate=1, 2, and 4 ml/min) and the effluent conductivity was collected with a flow-type conductivity meter 78 79 (3574-10C, HORIBA, Japan) which was connected to the outlet. After passing through the 80 conductivity meter, the effluent was disposed (single-pass mode). All experiments were conducted in a temperature chamber at 25°C. 81

Desalination performance was evaluated under constant current operation.^{1, 30} The 82 CDI cell was controlled with a cycler (WBCS3000, WonaTech, Korea); it was charged under 83 various constant currents (1-25 mA) with a cut-off voltage of 1.2 V followed by short-84 85 circuiting for many seconds until the outlet conductivity showed a plateau which was close to 86 the initial conductivity. These steps were repeated 3 times to secure the dynamic equilibrium, and the 3^{rd} cycle was used as a representative profile. The deionization capacity (mg/g, the 87 mass of NaCl (mg) divided by the mass of both electrodes (g)) was derived from the area 88 below the influent conductivity during the charging step.³¹ The mean deionization rate 89 90 (mg/g/s) was obtained by dividing the deionization capacity by the duration of charging (s). It

91 should be noted that operating method (i.e., constant current charging–constant current 92 discharging, constant voltage charging–zero voltage discharging, etc.) or CDI without 93 membranes could result in different desalination performances²⁵, but our focus was to 94 observe the performance obtained only from constant current charging in MCDI. Detailed 95 operating parameters for each experimental condition are provided in Table S1⁺.

96 Fig. 1(a) shows a conceptual diagram of the CDI Ragone plot, in which x and y 97 axes represent the deionization capacity and mean deionization rate, respectively. This plot 98 combines two important parameters that represent the desalination performance, which are relevant to the energy and power of energy storage devices in a conventional Ragone plot.³² 99 100 The most outstanding aspect of the CDI Ragone plot is that it can provide three essential 101 parameters at once: the deionization capacity (x-axis), mean deionization rate (y-axis), and 102 deionization time (dashed lines). More importantly, the overall desalination performance can 103 be evaluated minimizing bias caused by selecting a specific condition. The desalination 104 performance must be evaluated under various current loads to achieve this goal; the lowest and highest current loads could provide the full capacity and maximum rate, respectively. Fig. 105 1(b) shows representative experimental data, which were converted to draw the CDI Ragone 106 107 plot. As can be seen, steady conductivity profiles were observed below the initial conductivity (dashed line), showing the typical behavior of constant current operation.³⁰ 108 109 When operating the CDI cell in this mode, a steady and controlled effluent can be produced 110 depending on the current load; the lower current produces an effluent with a slightly 111 decreased conductivity for a longer time while the higher current produces an effluent with a 112 largely decreased conductivity in a relatively short time. Therefore, a higher mean 113 deionization rate is expected when increasing the current load. On the other hand, the 114 deionization capacity decreases as the current load increases, which could be ascribed to

115

116

117

118

119

120

121

122

123

RSC Advances

impeded ion transport from the bulk phase to the inside of an electrode and voltage loss because of IR drop. When all of the data points obtained at each current load are plotted, it becomes an arc-shaped line pointing from upper-left to bottom-right in the colored regions in Fig. 1(a). There can be two extreme cases; the one with a high rate but a low capacity (denoted by the blue color) and the one with a high capacity but a low rate (denoted by the red color). The goal of developing a CDI electrode or system will be to shift the plot toward the upper, right region of the plot, which represents the ideal desalination performance (denoted by the green color).



Fig. 1. A conceptual diagram of a CDI Ragone plot (a) and the representative conductivity profiles (b). A CDI Ragone plot consists of the deionization capacity and mean deionization rate, indicating total removed ions during charging and deionization capacity divided by duration of charging, respectively. These two parameters were obtained under constant current charging followed by zero-voltage discharging shown in (b); the area below the influent conductivity (dashed line) refers to the removed ions by the CDI cell. Data points

obtained at each current load are located in the CDI Ragone plot, thus becoming a curve representing its experimental condition. The location and shape of a curve represent the desalination performance; two imaginary cases would be a high rate & low capacity (blue color) and a high capacity & low rate (red color). An ideal CDI system would shift a curve toward the upper, right region of the plot (green color).

136

137 To confirm the implications of the CDI Ragone plot, prevalent parameters 138 affecting the desalination performance were examined including salt concentration, flow rate, 139 electrode thickness, and types of carbon materials. First, we investigated the effect of salt 140 concentration (2–100 mM NaCl) on the CDI Ragone plot. As shown in Fig. 2(a), a higher salt 141 concentration shifted the plot toward the upper, right region of the plot, indicating increases 142 in both the deionization capacity and mean deionization rate. The capacity increase (a shift to 143 the right region) is mainly because of the compaction of the double layer and the subsequent rise in capacitance.^{31, 33} In addition, the enhanced rate (a shift to the upper region) can be 144 145 simply explained by the conductivity increase of the influent solution and the subsequent 146 swift transport of ions from the spacer channel to the electrodes. When comparing the 147 capacity and rate dependent on the salt concentration, more change was observed in the rate 148 than in the capacity; the maximum rate at each highest current load ranged from 0.019 to 0.101 mg/g/s (a five-fold difference), while a relatively minor difference was observed in the 149 150 full capacity (17.9 to 23.6 mg/g) at each lowest current load. In this regard, a higher salt 151 concentration is advantageous because rapid desalination can be achieved compared to a 152 lower salt concentration. However, it should be noted that the charge efficiency¹ (the ratio of 153 removed ions to transferred charge) has been reported to decrease with an increase in salt concentration (see Table S2[†]).^{30, 34} From an energetic point of view, a lower charge efficiency 154

155	is disadvantageous because it implies that more energy is consumed for desalination. Next,
156	the effect of flow rate (1-4 ml/min) on desalination performance was examined as plotted in
157	Fig. 2(b). The result shows that each plot converges to one point at the lowest current load,
158	indicating a similar deionization capacity and mean deionization rate, while the difference
159	becomes significant as the current load increases. A lower current load allows enough time
160	for ion transport from a bulk phase to an electrode regardless of the flow rate. At a higher
161	current load, however, a higher flow rate could provide more ions in response to an increase
162	in the current load compared to a lower flow rate (see Fig. S2 [†]), thus exhibiting a higher
163	capacity and rate. This is in good agreement with a previous study on flow rate ²⁵ , and also
164	extended the previous result by evaluating the performance over various current loads, which
165	is the major advantage of the CDI Ragone plot.

RSC Advances Accepted Manuscript



Fig. 2. Effect of various parameters on the CDI Ragone plot. Each plot shows the effect of the (a) salt concentration, (b) flow rate, (c) electrode thickness, and (d) type of carbon materials. Each parameter was examined based on the standard operating condition (10 mM NaCl, 2 ml/min, 300 μ m, and MSP-20), and the range of the current load was from 1 to 25 mA but properly adjusted to show the overall performance. Detailed operating parameters for each experimental condition are provided in Table S1[†].

173 Fig. 2(c) shows the desalination performance depending on the variation in electrode thicknesses (200–400 um), which is extended result of our previous work.³⁵ As can 174 175 be seen, the plot shifts upward when increasing the electrode thickness, indicating faster 176 desalination, while the full capacity obtained at the lowest current load for each thickness 177 shows a similar value. The result confirms the strong influence of the electrode thickness on the rate of desalination¹⁴, which is one of the important parameters when designing and 178 179 optimizing a CDI process. Compared to previous two parameters, however, the variation in 180 the thickness led to different carbon loading on the electrode; a different CDI Ragone plot would come out when it is normalized by another basis (e.g., foot print area, see Fig. 3(a)), so 181 182 that a careful attention is required to interpret the plot. Lastly, we show a comparison of 183 various carbon materials on the CDI Ragone plot, which is the most frequently used approach by developing novel electrodes.^{12-18, 29, 36, 37} As shown in Fig. 2(d), the CDI Ragone plot 184 185 enables a comprehensive comparison of electrodes made of various carbon materials at a glance in terms of desalination performance. First, a comparison of microporous activated 186 carbons (S-51HF (\blacktriangle), YS-2 (\blacksquare), and MSP-20 (\bullet))³¹ shows the effect of surface area on the 187 deionization capacity and rate. A higher surface area and subsequent capacitance³¹ shifted the 188 189 plot toward the upper, right side of the CDI Ragone plot, indicating a higher capacity and rate. 190 When comparing MSP-20 (\bullet) and CEP21 ($\mathbf{\nabla}$), for which CEP21 is relatively hydrophobic (see Fig. S3[†]), CEP21 exhibited a higher capacity at the lowest current load but its capacity 191 192 and rate decreased with increasing current load. It can be inferred that hydrophobicity 193 inhibited the transport of ions inside the electrode³⁸, and this interruption became significant 194 when faster charging was implemented. Therefore, we could deduce from the CDI Ragone plot that carbon which is more hydrophilic (MSP-20) is a better option for rapid desalination. 195 196 The CDI Ragone plot also could be used to find the role of pore structures on desalination performance. As reported in our previous study¹², a large pore size could facilitate the rapid 197

198 transport of ions, thus resulting in rapid desalination. We observed that MDC (\blacklozenge) is located 199 more in the upper region of the plot than that of the other materials, especially at the higher 200 current load, indicating faster desalination. On the other hand, its capacity is relatively low, 201 indicating a trade-off behavior between capacity and rate as in the case of the 'high rate & 202 low capacity' shown in Fig. 1(a). However, similar to the case of the variation in the 203 thickness, a careful attention is required because the activated carbons had different pore 204 structure, especially the MDC. Though the large pore size of MDC could facilitate the 205 performance when it is shown in the mass basis, but its low density led to poor performance 206 based on electrode area (see Fig. 3(b)). Therefore, the CDI Ragone plot with various basis 207 including the mass, area, and volume would make more reliable evaluation. In other words, 208 the conventional mass-based normalization for desalination performance needs improvement 209 to be applicable for entire parameters that were discussed above. Among various normalization units (e.g., mg/g, mg/cm², mg/cm³), the performance based on electrode 210 volume (mg/cm³) could provide more beneficial information for commercialization because 211 212 overall performance can be determined under restricted volume of the CDI system in practice. 213 However, normalization by electrode volume still makes bias for the electrode thickness; the 214 mass- (Fig. 2(c)) and volume-based (data not shown) CDI Ragone plots are the same in terms 215 of their relative locations (the thinner electrode was located upward), leading to conflicting 216 result compared to the overall performance assessed from the area-based normalization (Fig. 217 3(a)). Therefore, it is recommended to fix the electrode thickness in order to use volume-218 based performance, suggesting a standard experimental condition should be made together 219 with a normalization basis in future studies. From the result that was obtained in various 220 parameters, the CDI Ragone plot was found to be a functional tool to investigate and 221 optimize the desalination performance of a system; it could provide overall desalination 222 performance in terms of capacity and rate. Furthermore, the CDI Ragone plot could be used

to determine an optimal current load depending on its applications: maximum capacity, rate, and balanced performance between capacity and rate. Comparison between studies would be possible after a standard experimental setup is defined in the future study. More importantly, this study could produce many sequel studies based on various standards (e.g., volume-based capacity or full cycle-based rate), operation methods (e.g., constant voltage), and configurations (e.g., CDI without membranes or flow-electrode CDI).

229



Fig. 3. CDI Ragone plots normalized by foot print area of electrode (3.02 cm^2) for (a) electrode thickness and (b) type of carbon materials. Results of Figs. 2(c) and 2(d) were converted from mass-based performance (mg/g and mg/g/s) to area-based performance (mg/cm² and mg/cm²/s). All experiments were carried out under the standard operating condition (10 mM NaCl, 2 ml/min, 300 µm, and MSP-20), unless otherwise indicated. Detailed operating parameters for each experimental condition are provided in Table S1⁺.

237 A novel concept to evaluate desalination performance was proposed, called the 238 CDI Ragone plot. This plot can facilitate the design and optimization of the CDI process 239 depending on its application. From the comparative study on various parameters using the 240 CDI Ragone plot, optimal conditions can be suggested for the best desalination performance in terms of the deionization capacity and rate. In the CDI Ragone plot, a upper, right side 241 242 shift in the plot is favorable because it indicates a higher deionization capacity and rate. This 243 kind of shift was achieved by increasing the salt concentration and flow rate, and decreasing 244 the electrode thickness. In addition, three carbon electrodes exhibited outstanding desalination performance (mg/g and mg/g/s) in different aspects. CEP21 had the highest 245 246 capacity with a poor rate performance and MDC had the highest rate with a low capacity 247 while MSP-20 was in between the two. However, MDC exhibited the poor desalination performance in the different normalization units (mg/cm² and mg/cm²/s), suggesting the 248 249 necessity of improving the conventional mass-based normalization method. Therefore, a 250 standard experimental condition and normalization basis are required for more reliable 251 evaluation of various parameters and for comparison between studies. Such accomplishment 252 can make the CDI Ragone plot to facilitate designing and optimizing the CDI process, 253 working as a comprehensive guide to evaluate desalination performance.

254

255 Acknowledgements

This project is supported by Korea Ministry of Environment as "Converging Technology Project (2014001640002)". The authors thank Dr. Seung Jae Yang and Prof. Chong Rae Park for providing MDC.

259

295

10.1039/c4ee02378a.

RSC Advances

† Electronic Supplementary Information (ESI) available: See DOI: 10.1039/c000000x/ 260 261 262 **Notes and References** 263 1. S. Porada, R. Zhao, A. Van Der Wal, V. Presser and P. M. Biesheuvel, Prog. Mater Sci., 2013. 2. 264 M. Noked, A. Soffer and D. Aurbach, J. Solid State Electrochem., 2011, 15, 1563-1578. 265 R. Zhao, S. Porada, P. M. Biesheuvel and A. van der Wal, Desalination, 2013, 330, 35-41. 3. 266 4. Y. Oren, *Desalination*, 2008, 228, 10-29. 267 5. P. Długołe, cki and A. van der Wal, Environ. Sci. Technol., 2013, 47, 4904-4910. 268 S.-i. Jeon, J.-g. Yeo, S. Yang, J. Choi and D. K. Kim, Journal of Materials Chemistry A, 2014, 2, 6. 269 6378-6383. 270 7. M. A. Anderson, A. L. Cudero and J. Palma, *Electrochim. Acta*, 2010, 55, 3845-3856. 271 8. E. García-Quismondo, R. Gómez, F. Vaguero, A. L. Cudero, J. Palma and M. Anderson, PCCP, 272 2013, 15, 7648-7656. 273 9. A. M. Pernía, J. G. Norniella, J. A. Martín-Ramos, J. Díaz and J. A. Martinez, Power 274 Electronics, IEEE Transactions on, 2012, 27, 3257-3265. 275 10. A. Pernia, F. J. Alvarez-Gonzalez, M. Prieto, P. Villegas and F. Nuno, Power Electronics, IEEE 276 Transactions on, 2014, 27, 3257-3265. 277 11. M. Alkuran, M. Orabi and N. Scheinberg, 2008. 278 12. S. J. Yang, T. Kim, K. Lee, Y. S. Kim, J. Yoon and C. R. Park, *Carbon*, 2014, 71, 294-302. 279 13. Z.-Y. Yang, L.-J. Jin, G.-Q. Lu, Q.-Q. Xiao, Y.-X. Zhang, L. Jing, X.-X. Zhang, Y.-M. Yan and K.-280 N. Sun, Adv. Funct. Mater., 2014, 24, 3917-3925. 281 14. S. Porada, L. Borchardt, M. Oschatz, M. Bryjak, J. Atchison, K. Keesman, S. Kaskel, P. M. 282 Biesheuvel and V. Presser, Energy & Environmental Science, 2013, 6, 3700-3712. 283 15. X. Wen, D. Zhang, L. Shi, T. Yan, H. Wang and J. Zhang, J. Mater. Chem., 2012, 22, 23835-284 23844. 285 16. C. Tsouris, R. Mayes, J. Kiggans, K. Sharma, S. Yiacoumi, D. DePaoli and S. Dai, Environ. Sci. 286 Technol., 2011, 45, 10243-10249. 287 17. H. Li, L. Zou, L. Pan and Z. Sun, Environ. Sci. Technol., 2010, 44, 8692-8697. 288 18. H. Yin, S. Zhao, J. Wan, H. Tang, L. Chang, L. He, H. Zhao, Y. Gao and Z. Tang, Adv. Mater., 289 2013, 25, 6270-6276. 290 19. L. Han, K. G. Karthikeyan, M. A. Anderson, J. J. Wouters and K. B. Gregory, *Electrochim.* 291 Acta, 2013, 90, 573-581. 292 20. M. Pasta, C. D. Wessells, Y. Cui and F. La Mantia, Nano Lett., 2012, 12, 839-843. 293 21. J. Yang, L. Zou, H. Song and Z. Hao, *Desalination*, 2011, 276, 199-206. 294 22. J. Lee, S. Kim, C. Kim and J. Yoon, *Energy & Environmental Science*, 2014, DOI:

296 23. J.-B. Lee, K.-K. Park, H.-M. Eum and C.-W. Lee, *Desalination*, 2006, 196, 125-134.

- 297 24. Y.-J. Kim and J.-H. Choi, *Water Res.*, 2010, 44, 990-996.
- 298 25. R. Zhao, O. Satpradit, H. Rijnaarts, P. M. Biesheuvel and A. van der Wal, *Water Res.*, 2013,
 299 47, 1941-1952.
- 30026.T. Kim, J. E. Dykstra, S. Porada, A. van der Wal, J. Yoon and P. M. Biesheuvel, J. Colloid301Interface Sci., DOI: 10.1016/j.jcis.2014.08.041.
- 302 27. S.-i. Jeon, H.-r. Park, J.-g. Yeo, S. Yang, C. H. Cho, M. H. Han and D.-K. Kim, *Energy & Environmental Science*, 2013.
- 304 28. S. Porada, D. Weingarth, H. V. M. Hamelers, M. Bryjak, V. Presser and P. M. Biesheuvel,
 305 *Journal of Materials Chemistry A*, 2014, 2, 9313-9321.
- 306 29. M. E. Suss, T. F. Baumann, W. L. Bourcier, C. M. Spadaccini, K. A. Rose, J. G. Santiago and M.
 307 Stadermann, *Energy & Environmental Science*, 2012, 5, 9511-9519.
- 308 30. R. Zhao, P. M. Biesheuvel and A. Van der Wal, *Energy & Environmental Science*, 2012, 5, 9520-9527.
- 310 31. T. Kim and J. Yoon, *J. Electroanal. Chem.*, 2013, 704, 169-174.
- 311 32. P. Simon and Y. Gogotsi, *Nature materials*, 2008, 7, 845-854.
- 312 33. A. J. Bard and L. R. Faulkner, *Electrochemical methods: fundamentals and applications*,
 313 Wiley New York, 1980.
- 314 34. P. M. Biesheuvel, S. Porada, M. Levi and M. Bazant, *J. Solid State Electrochem.*, 2014, 18, 1365-1376.
- 316 35. T. Kim, H. D. Yoo, S. M. Oh and J. Yoon, *Electrochim. Acta*, 2014, 139, 374-380.
- 317 36. S. Porada, L. Weinstein, R. Dash, A. Van Der Wal, M. Bryjak, Y. Gogotsi and P. M. Biesheuvel,
 318 ACS Applied Materials & Interfaces, 2012, 4, 1194-1199.
- 319 37. G. Wang, Q. Dong, Z. Ling, C. Pan, C. Yu and J. Qiu, J. Mater. Chem., 2012, 22, 21819-21823.
- 320 38. J. Zhou, W. Xing, S. Zhuo and Y. Zhao, *Solid State Sciences*, 2011, 13, 2000-2006.

321

322

323