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1 **Performance and emission analysis of a multi cylinder gasoline engine operating on**  
2 **different alcohol-gasoline blends**

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6 **Abstract**

7 Alcohols are potential renewable alternatives for gasoline because of their bio-based origin.  
8 Although ethanol has been successfully implemented in many parts of the world, other  
9 alcohols may also be utilized, such as methanol, propanol, and butanol. These alcohols  
10 contain much energy and a high octane number. Furthermore, they displace petroleum.  
11 Therefore, this study focuses on methanol, ethanol, propanol, and butanol as gasoline fuel  
12 alternatives. We conducted tests in a four-cylinder gasoline engine under the wide open  
13 throttle condition at varying speeds and results. This engine was fueled with 20%  
14 methanol/80% gasoline (M20), 20% ethanol/80% gasoline (E20), 20% propanol/80%  
15 gasoline (P20), and 20% butanol/80% gasoline (B20). M20, E20, P20, and B20 displayed  
16 brake specific fuel consumptions levels and brake thermal efficiencies that were higher than  
17 those of gasoline at 7.78%, 5.17%, 4.43%, and 1.95% and 3.6%, 2.15%, 0.7%, and 1.86%,  
18 respectively. P20 and B20 showed better torque than E20, but they consumed more fuel.  
19 Moreover, the alcohol—gasoline blends generated a higher peak in-cylinder pressure than  
20 pure gasoline. As gasoline fuel alternatives, propanol and butanol were more effective than  
21 gasoline in engines. In addition, the alcohol—gasoline blends also emitted less carbon  
22 monoxide and hydrocarbon than gasoline. However, E20 emitted more nitrogen oxide than

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23 the other alcohol–gasoline blends. Thus, propanol and butanol are more effective options than  
24 ethanol for a gasoline engine in terms of fuel properties, engine performance, and emissions.

25 **Key words:** Ethanol; Alcohol gasoline, Performance, Emission, Gasoline engine.

## 26 **Introduction**

27 For researchers and manufacturers in the field of energy, the replacement of petroleum  
28 gasoline with alternative fuels is an important issue given rising petroleum fuel prices,  
29 environmental threats from engine exhaust emissions, fossil fuel depletion, the effects of  
30 global warming, and energy concerns.<sup>1</sup> Global energy consumption has increased sharply  
31 recently, and it will increase by approximately 53% by 2030, according to the International  
32 Energy Agency.<sup>2</sup> The United States Energy Information Administration projects that the  
33 liquid fuel consumption in the world will increase from 86.1 million barrels/day to 110.6  
34 million barrels/day by 2035.<sup>3</sup> Furthermore, the burning of petroleum-derived fuel generates  
35 emissions that seriously affect both the environment and human health. In particular, the  
36 burning of fossil fuels is a main contributor to the increase in carbon dioxide (CO<sub>2</sub>)  
37 emissions, which in turn aggravates global warming. If fossil fuel emissions are not strictly  
38 regulated soon, greenhouse gas (GHG) emissions from fossil fuels will increase by 39% by  
39 2030. Hence, alternative fuel sources for clean combustion have received increased attention  
40 given several factors, such as worldwide environmental concerns, price hikes in petroleum  
41 products, and the expected depletion of fossil fuels.<sup>4</sup> Therefore, the development of clean  
42 alternative fuels that are locally available, environmentally acceptable, and technically  
43 feasible is a global concern. In the transport sector, biofuels can be a good substitute for fossil  
44 fuels because they can be adopted directly without altering the engine and fuelling processes.

45 The use of alcohols as substitutes for petrol in spark ignition (SI) engines has been  
46 investigated extensively. These alcohols enrich oxygen, enhance octane, and reduce carbon

47 monoxide (CO) emission. As an alternative fuel, ethanol is the most widely used alcohol  
48 type.<sup>5</sup> It can be combined with gasoline because of its simple chemical structure, high octane  
49 number and oxygen content, and accelerated flame propagation.<sup>6</sup> Many experimental studies  
50 have confirmed that ethanol increases engine efficiency, torque, and power. However, its  
51 brake specific fuel consumption (BSFC) is higher than that of gasoline.<sup>7</sup>

52 Balki et al.<sup>8</sup> studied the performance, combustion, and emission characteristics of a single-  
53 cylinder gasoline engine fuelled by gasoline, ethanol, and methanol. Pure ethanol and  
54 methanol enhanced torque by 3.7% and 4.7%, at the expense of a 58% and 84% increase in  
55 BSFC, respectively, compared with those of gasoline fuel. Nitrogen oxide (NO<sub>x</sub>), CO, and  
56 hydrocarbon (HC) emissions by engines containing methanol and ethanol decreased by 49%  
57 and 47.6%, 22.6% and 21.25%, and 21.6% and 19.13%, respectively, compared with those  
58 emitted by gasoline. However, CO<sub>2</sub> emissions increased by 4.4% and 2.51%. Costa and Sodr   
59 <sup>9</sup> investigated the performance and emission of hydrous ethanol (6.8% water content) and a  
60 blend of 78% gasoline–22% ethanol (E22) at varying speeds. Hydrous ethanol displayed a  
61 higher break thermal efficiency (BTE) and BSFC than E22 throughout the entire speed range.  
62 However, torque and break mean effective pressure increased with engine speed. Moreover,  
63 hydrous ethanol reduced CO and HC emissions but increased CO<sub>2</sub> emissions. Ko  et al. <sup>7</sup>  
64 experimentally investigated the performance and pollutant emissions of unleaded gasoline–  
65 ethanol blends. The torque and BSFC values of E50 and E85 were higher than those of  
66 gasoline by 2.3% and 2.8% and 16.1% and 36.4%, respectively. Moreover, the addition of  
67 ethanol to gasoline significantly reduced CO, HC, and NO<sub>x</sub> emissions. Ethanol–gasoline  
68 blends also accommodated high compression ratios without inducing knocking.

69 In many countries, governments mandate the integration of ethanol with gasoline. The  
70 Environmental Protection Agency (EPA) issued a waiver that authorizes the incorporation of  
71 up to 15% ethanol into gasoline for cars and light pickup trucks made in 2001 onwards.<sup>10</sup> The

72 US Renewable Fuel Standard mandates the production of up to 36 billion gallons of ethanol  
73 and advanced bio-fuels by 2022.<sup>11</sup> To meet the high demand for ethanol, alcohols with  
74 increased carbon numbers can be utilized as enhanced alternatives because the use of ethanol  
75 as fuel in gasoline engines is mainly limited by its low heating value (LHV). Hence,  
76 additional low-LHV fuel must be generated to match a certain power level.<sup>12</sup> Alcohols with  
77 high carbon numbers, such as propanol and butanol, have a higher LHV than ethanol.  
78 Therefore, they can overcome this shortcoming. Furthermore, all of these alcohols can be  
79 derived from coal-derived syngas, which is a renewable energy source.<sup>13</sup> Ethanol can also be  
80 converted into alcohols with high carbon numbers and fermented to enhance alcohol  
81 production through biorefinery.<sup>14</sup>

82 Some studies have compared different alcohol—gasoline blends. Gravalos et al.<sup>15</sup> integrated  
83 approximately 1.9% methanol, 3.5% propanol, 1.5% butanol, 1.1% pentanol, and variable  
84 concentrations of ethanol with gasoline in a single-cylinder gasoline engine. A total of 30%  
85 alcohol was incorporated into the gasoline. The alcohol—gasoline blend emitted less CO and  
86 HC but more NO<sub>x</sub> and CO<sub>2</sub> than pure gasoline. In the present study, multiple alcohol—  
87 gasoline blends also emit more acceptable levels of CO and HC than the ethanol—gasoline  
88 blend. Yacoub et al.<sup>16</sup> integrated methanol, ethanol, propanol, butanol, and pentanol with  
89 gasoline in an engine and analyzed its performance and emissions. Each alcohol was blended  
90 with gasoline containing 2.5% and 5% oxygen. The alcohol—gasoline blend displayed better  
91 BTE, knock resistance, and emissions than gasoline, but its BSFC was higher. Alcohols with  
92 low carbon content (e.g. C1, C2, and C3) contain high levels of oxygen. Hence, relatively  
93 less of these alcohols is required to reach the targeted oxygen percentage than alcohols with  
94 high carbon content (e.g., C4 and C5). Alcohol percentage and properties varied across  
95 blends. Thus, different alcohol—gasoline blends cannot be compared properly under  
96 optimized oxygen concentrations. Gautam et al.<sup>17</sup> prepared six alcohol—gasoline blends

97 with various proportions of methanol, ethanol, propanol, butanol, and pentanol that total 10%  
98 alcohol. The alcohol–gasoline blends emitted lower brake specific CO, CO<sub>2</sub>, and NO<sub>x</sub> than  
99 pure gasoline. However, these researchers did not blend specific volume percentages of  
100 alcohol or consider fuel properties.

101 Thus, few studies compare specific percentages of alcohols, such as methanol, ethanol,  
102 propanol and butanol, with respect to performance and emission characteristics in the  
103 gasoline of an SI engine. Moreover, very few studies focus on the partial replacement of  
104 gasoline with propanol as an SI engine fuel. Nonetheless, the derivation of alcohols with high  
105 carbon numbers from renewable sources has increasingly been investigated.<sup>18-22</sup> In particular,  
106 the application of such alcohols as gasoline engine fuel must be examined extensively. Thus,  
107 this research aims to determine the effect of methanol–gasoline, ethanol–gasoline, propanol–  
108 gasoline, and butanol–gasoline blends on engine performance, combustion, and exhaust  
109 emissions. The results obtained with these blends are compared with those of gasoline and  
110 the commonly used ethanol–gasoline blend in gasoline engines.

## 111 **Materials and method**

### 112 **Fuel selection**

113 In this study, we utilized methanol, ethanol, and branched isomers of propanol and butanol  
114 (99.8% purity) given their high octane numbers. We procured the ethanol from Chemical  
115 Industries (Malaya) Sdn Bhd., Malaysia and the other alcohols from QREC Chemical  
116 Company, Thailand. We obtained Primax 95 gasoline with research octane number (RON) 95  
117 from PETRONAS, Malaysia as the base gasoline. We blended methanol, ethanol, propanol,  
118 and butanol with gasoline (M20, E20, P20, and B20, respectively) at volume concentrations  
119 of 20% alcohol and 80% gasoline. Table 1 lists the properties of the gasoline and the alcohol–  
120 gasoline blends.

121 **Table 1: Properties of pure gasoline and different alcohol-gasoline blends.**

122 **Experimental setup**

123 We experimented on a four-cylinder gasoline engine at the Engine Laboratory of the  
124 Mechanical Engineering Department in the University of Malaya. Table 2 details the engine,  
125 and Fig. 1 depicts the schematic of the experimental setup. The test engine was coupled with  
126 an eddy current dynamometer (Froude Hofmann model AG150, United Kingdom) with a  
127 maximum power of 150 kW. The engine was first operated on gasoline for a few minutes to  
128 stabilize the operating condition. The fuel was then changed to the alcohol blend. After  
129 sufficient amounts of the blend were consumed, data were acquired to ensure the removal of  
130 residual gasoline from the fuel line. Each test engine was again operated under gasoline to  
131 drain all of the blends in the fuel line.

132 The engine was operated between 1000 rpm to 6000 rpm with a step of 1000 rpm at 100%  
133 load condition. We measured fuel flow using a KOBOLD ZOD positive-displacement type  
134 flow meter (KOBOLD, Germany). The data were automatically collected using the CADET  
135 10 data acquisition system. To analyze combustion, we applied a pressure sensor and crank  
136 angle encoder (RIE-360). Both sensors vary the in-cylinder pressure at a crank angle. The  
137 data were digitally recorded by a computer using the DEWESoft combustion analyzer  
138 software. Exhaust emissions were measured using the AVL DICOM 4000 exhaust gas  
139 analyzer (AVL DiTEST, Austria), where CO, NO, and HC are determined by non-dispersive  
140 infrared, heated chemiluminescence, and heated flame ionization detectors. Table 3 exhibits  
141 the accuracies of the measured parameters. In each test, performance and emission were  
142 measured in triplicate. These measurements were highly repeatable within the test series.

143 **Fig. 1: Schematic diagram of the engine test bed**

144 **Table 2: Specification of the tested engine**

145 **Table 3: Specifications of the exhaust gas analyzer**

146 **Results and Discussion**

147 **Engine performance analysis**

148 **Torque**

149 Torque is a turning force produced by the pressure from the crankshaft of the piston. Engine  
150 torque depends on engine stroke length, charge condition, and average effective cylinder  
151 pressure.<sup>23</sup> Under a constant engine condition, torque varies given different fuels as a result of  
152 the fuel properties and the effective pressure generated. Fig. 2 compares the engine torque  
153 given the test fuels. On average, M20, E20, P20, and B20 significantly increased the torque  
154 of gasoline by 5.02%, 3.39%, 10%, and 9.2%, respectively ( $0.0003 < p < 0.011$ ). As indicated  
155 in this figure, torque was maximized at 4000 rpm in all fuels. The increased torque may be  
156 attributed to the high latent heat of vaporization (HoV). Fuel vaporizes in the intake manifold  
157 and in the combustion chamber. When the Latent heat of vaporization (LoV) of alcohol  
158 increases, charge temperature is lowered as the alcohol evaporates. Furthermore, charge  
159 density increases. Engine torque is also enhanced by associated fuel mass at the same air–fuel  
160 ratio. This result is consistent with those obtained by other researchers.<sup>24, 25</sup> Moreover, the  
161 incorporation of oxygenated alcohol produces a lean mixture that burns more efficiently than  
162 gasoline.<sup>7</sup> The maximum brake torque timing increases combustion pressure and torque as a  
163 result of the enhanced anti-knock behavior.<sup>26</sup> P20 obtained the ideal engine torque (138.2  
164 Nm) at 4000 rpm. This improved torque may be attributed to the enhanced RON of propanol  
165 because high RON aggravates ignition delay, which decelerates energy release rate and limits  
166 heat loss from the engine because the heat from the cylinder is not transferred to the coolant  
167 in time.<sup>13</sup> Hence, engine torque decreases after it is maximized by engine acceleration.



168 **Fig. 2. Variation of torque with engine speed.**

169 **Brake specific fuel consumption**

170 Fig. 3 depicts the variation in the BSFC of the test fuels at different engine speeds. On  
171 average, the BSFC values of M20, E20, P20, and B20 were higher than that of unleaded  
172 gasoline by 7.58%, 5.17%, 4.43%, and 1.95%, respectively. This result is typically ascribed  
173 to the low energy content of the alcohols, which enhances engine BSFC when it is applied  
174 directly.<sup>8</sup> Therefore, increased amounts of fuel are required to produce the same level of  
175 engine power as that generated by low LHV fuel. The high BSFC of alcohol may also be  
176 induced by high alcohol density.<sup>7</sup> Nonetheless, the BSFC of B20 is closer to that of gasoline  
177 than the other alcohols. Furthermore, P20 and B20 displayed BSFC values that were 2% and  
178 4% lower, respectively, than that of E20. Alcohols with high carbon number consumed less  
179 fuel because LHV increases with carbon number (Table 1). In all test fuels, BSFC decreased  
180 with engine acceleration because the volumetric and combustion efficiencies increased.<sup>27</sup>

181 **Fig. 3. Variation of BSFC with engine speed.**

182 **Brake thermal efficiency**

183 Fig. 4 displays the BTE values of the different test fuels. On average, the thermal efficiencies  
184 of M20, E20, P20 and B20 were significantly higher than that of gasoline by 3.6%, 2.15%,  
185 0.7% and 1.86%, respectively ( $0.001 < p < 0.04$ ). Alcohol—gasoline blends with low carbon  
186 numbers have higher BTE values than those with high carbon numbers. This condition can be  
187 attributed to the fact that blends with low carbon numbers contain more oxygen than those  
188 with high carbon numbers. As a result, combustion is improved, thereby enhancing thermal  
189 efficiency.<sup>28</sup> Moreover, fuel is vaporized in the compression stroke when latent HoV is high.  
190 Given that fuel absorbs heat from the cylinder during vaporization, the air—fuel mixture is

191 compressed more easily, thus improving thermal efficiency. Balki et al.<sup>8</sup> noted that the HoV  
192 and oxygen content of alcohol enhances BTE in alcohol—gasoline blends.

193 **Fig. 4. Variation of BTE with engine speed.**

194 **Exhaust gas temperature**

195 Fig. 5 presents the effect of test fuels on the EGT of the test engine, which is a significant  
196 indicator of cylinder temperature. EGT can also be used to analyze exhaust emission,  
197 especially of NO<sub>x</sub> because NO<sub>x</sub> formation often depends on temperature.<sup>29</sup> In this figure, the  
198 addition of alcohol to gasoline reduces EGTs, with the exception of ethanol. The heating  
199 value of alcohol is lower than that of gasoline; thus, the combustion temperature and EGTs of  
200 alcohol—gasoline blends are lower than those of gasoline. However, the high latent HoV of  
201 ethanol induces ignition delay and increases its EGT relative to other fuels. In all fuels, EGTs  
202 increase with engine speed. Moreover, EGT and combustion temperature increase as  
203 increased amounts of fuel burn at high engine speeds.

204 **Fig. 5. Variation of Exhaust gas temperature with engine speed.**

205 **In-cylinder gas pressure**

206 We can compare the combustion characteristics of different fuels based on cylinder gas  
207 pressure and heat release rate. Fig. 6 compares the cylinder gas pressures of all of the test  
208 fuels at an engine in full throttle load at a speed of 4000 rpm. All of the fuels displayed  
209 similar inlet and exhaust pressure curves because throttle angle was almost constant.  
210 Furthermore, the maximum pressures for all test fuels were close to the top dead center  
211 (TDC). As observed in the figure, cylinder gas pressure increased earlier in alcohol—gasoline  
212 blends than in pure gasoline. Furthermore, this pressure was higher in the blends. According  
213 to Melo et al.<sup>30</sup> explained alcohol increase spark timing and avoid knocking as a result  
214 maximum pressure obtained for using alcohol. Balki et al.<sup>8</sup>, the increase in alcohol enhanced

215 timing and prevented knocking, thus maximizing the pressure obtained using alcohol. Balki  
216 et al.<sup>8</sup> added that high latent HoV and oxygen content in alcohols increases cylinder gas  
217 pressure. Moreover, Fig. 6 shows that the addition of alcohol shortens combustion duration  
218 compared with that of gasoline. This finding is attributed to high laminar flame speed and  
219 RON by Balki et al.<sup>8</sup> The peak in-cylinder was highest for P20. It because of, heat release  
220 started early for P20 than others fuel as P20 is having higher RON.

### 221 **Fig. 6. Comparison of in-cylinder pressure at 4000rpm**

### 222 **Engine emission analysis**

#### 223 **CO emission**

224 CO emission represents a loss in the chemical energy that is not fully utilized in the engine. It  
225 is a product of incomplete combustion given either an insufficient amount of air in the air-  
226 fuel mixture or the interruption of combustion cycle time.<sup>31</sup> Fig. 7 depicts the variation in CO  
227 exhaust emissions in relation to engine speed. In M20, E20, P20, and B20, CO emissions are  
228 significantly lower than those of gasoline by averages of 16.6%, 13.9%, 9.6%, and 5.6%,  
229 respectively ( $p < 0.01$ ). Alcohols are oxygenated fuels; therefore, they enhance oxygen  
230 content in fuel for combustion. This process generates the “leaning effect”, which sharply  
231 reduces CO emission.<sup>32</sup> Thus, alcohol—gasoline blended fuel emits less CO than gasoline  
232 fuel. Table 1 shows that the alcohols with low carbon numbers contain much oxygen and  
233 possess a simple molecular structure. Hence, CO emission from the alcohol—gasoline blend  
234 with low carbon number is lower than that from the blend with high carbon number.  
235 Nonetheless, all of the alcohol—gasoline blends emit less gas at overall engine speed than  
236 gasoline. At high engine speed, CO emission is lower in alcohol—gasoline blends than in  
237 pure gasoline fuel. Furthermore, the engine has limited time to complete the combustion  
238 cycle; thus, flame speed must be increased to complete combustion.<sup>25, 33</sup> As a result of this

239 increased flame speed in alcohol, alcohol—gasoline blends emit less CO at high engine  
240 speeds. This finding is consistent with that of previous studies, which utilized ethanol—  
241 gasoline blends.<sup>9</sup>

242 **Fig. 7. Variation of CO emission with engine speed.**

### 243 **HC emission**

244 Emissions of unburned HC are primarily caused by unburned mixtures induced by improper  
245 mixing and incomplete combustion. These emissions are a main contributor to photochemical  
246 smog and ozone pollution.<sup>34</sup> Fig. 8 exhibits the emissions of unburned HC by all test fuels at  
247 speeds ranging from 1000 rpm to 6000 rpm. These emissions were slightly lower in all  
248 alcohol—gasoline blends than in pure gasoline. On average, emissions of unburned HC by  
249 M20, E20, P20, and B20 significantly decreased by 10.7%, 14.9%, 5.4%, and 2.9%,  
250 respectively ( $0.03 < p < 0.05$ ). This result may be attributed to the leaning effect and the  
251 oxygen content in the alcohol.<sup>7</sup> Moreover, these emissions decrease as engine speed increases  
252 in all blends. At high speeds, the air—fuel mixture homogenizes to increase in-cylinder  
253 temperature. This condition in turn enhances combustion efficiency. Thus, HC emission  
254 decreases more at high engine speeds than at low speeds. This conclusion is consistent with  
255 that of Koc et al.<sup>7</sup>

256 **Fig. 8. Variation of HC emission with engine speed.**

### 257 **CO<sub>2</sub> emission**

258 CO<sub>2</sub> is a GHG produced by the complete combustion of hydrocarbon fuel. Its formation is  
259 affected by the carbon—hydrogen ratio in fuel. Stoichiometrically, hydrocarbon fuel  
260 combustion should generate only CO<sub>2</sub> and water (H<sub>2</sub>O). Fig. 9 presents the variation in CO<sub>2</sub>  
261 emission across different fuels. As per the study results, CO<sub>2</sub> emission is higher in alcohol—  
262 gasoline blends than in pure gasoline; on average, CO<sub>2</sub> emissions by M20, E20, P20, and B20

263 are 15%, 12%, 6.5%, and 5.8% significantly higher ( $0.01 < p < 0.03$ ). This finding can be  
264 attributed to carbon flow rate. To attain a certain level of engine power given a constant  
265 throttle position, the amount of alcohol–gasoline blended fuel consumed must be higher than  
266 that of gasoline. Therefore, the carbon flow rates of the alcohol–gasoline blends are higher  
267 than those of gasoline.<sup>30</sup> The oxygen ratio in alcohols also enhances the combustion  
268 efficiency of alcohol–gasoline blends, which enhances CO<sub>2</sub> emission in alcohol–gasoline  
269 blends.

270 **Fig. 9. Variation of CO<sub>2</sub> emission with engine speed.**

### 271 **NO<sub>x</sub> emission**

272 During combustion at high temperature, nitrogen in the air oxidizes to form NO<sub>x</sub>. Thus, the  
273 generation of NO<sub>x</sub> in an engine is closely related to combustion temperature, oxygen  
274 concentration, and residence time inside the combustion chamber.<sup>35</sup> Fig. 10 exhibits the  
275 variation in NO<sub>x</sub> emission at WOT and at different engine speeds. On average, NO<sub>x</sub>  
276 emissions by M20, E20, P20, and B20 are significantly higher than that by pure gasoline at  
277 20%, 32%, 14.5% and 11% ( $0.001 < p < 0.05$ ). This results may be ascribed to the high  
278 oxygen concentration in the alcohol–gasoline blend. Among all of the fuels, E20 displayed  
279 the highest EGT, which indicated that it emitted the most NO<sub>x</sub>. Moreover, NO<sub>x</sub> emission  
280 increased with the acceleration of engine speed in all of the tested fuels. At high speeds,  
281 increased amounts of fuel are burned. Furthermore, torque and BSFC increase, and as a  
282 result, in-cylinder temperature increases. This increase may also enhance NO<sub>x</sub> emission  
283 instead of lowering heating value.<sup>35</sup>

284 **Fig. 10. Variation of NO<sub>x</sub> emission with engine speed**

285 **Conclusion**

286 This study mainly compares the performance, combustion, and emission characteristics of  
287 M20, E20, P20, and B20 as engine fuels. Based on experimental observation, we can draw  
288 the following conclusions:

- 289 • Alcohol–gasoline blends displayed better engine torque and BTE than gasoline.  
290 Torque was also enhanced in alcohol blends with high carbon numbers compared with  
291 those with low carbon numbers given their improved fuel properties such as RON,  
292 LHV etc. In particular, P20 exhibits the best torque and BTE among all of the fuels.  
293 Moreover, the BSFC levels of P20 and B20 are more acceptable than that of E20 at  
294 1.21% and 3.06% because of their high LHV.
- 295 • In-cylinder gas pressure increases earlier in all alcohol–gasoline blends than in  
296 gasoline fuel because of the high flame speed of alcohol. Furthermore, the combustion  
297 duration of alcohol–gasoline blends was shorter than that of gasoline. Peak in-cylinder  
298 pressure was also higher for alcohol–gasoline blends (particularly the P20 blend) than  
299 for pure gasoline.
- 300 • All alcohol–gasoline blends emitted less CO and HC than gasoline. Specifically, E20  
301 emitted the lowest amount. However, these blends emitted more NO<sub>x</sub> and CO<sub>2</sub> than  
302 gasoline. Moreover, P20 and B20 emitted 5-6% less NO<sub>x</sub> and 11-14% less CO<sub>2</sub> than  
303 E20. Thus, alcohol–gasoline blends are more environment-friendly than gasoline.
- 304 • In general, the fuel properties of P20 and B20 were superior to the other alcohol–  
305 gasoline blends. Furthermore, these blends enhanced engine performance and lowered  
306 emissions more effectively than the ethanol–gasoline blend in an unmodified gasoline  
307 engine.

308

309 **Acknowledgment**

310 The authors would like to appreciate University of Malaya for financial support through  
311 Research Grant no. CG 060-2013.

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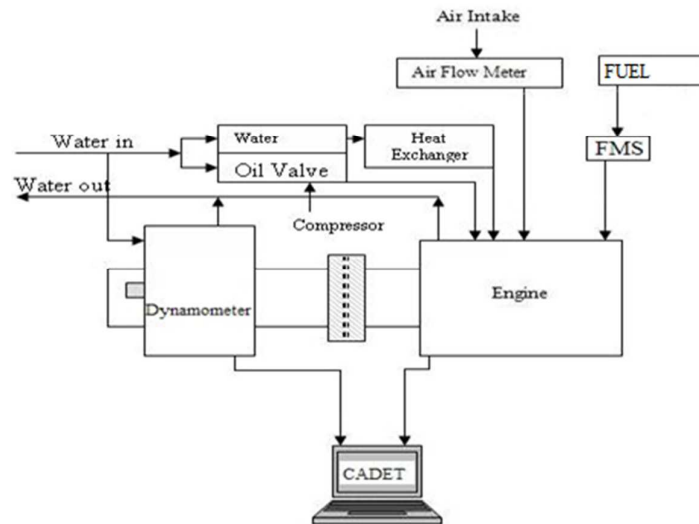


Fig. 1: Schematic diagram of the engine test bed

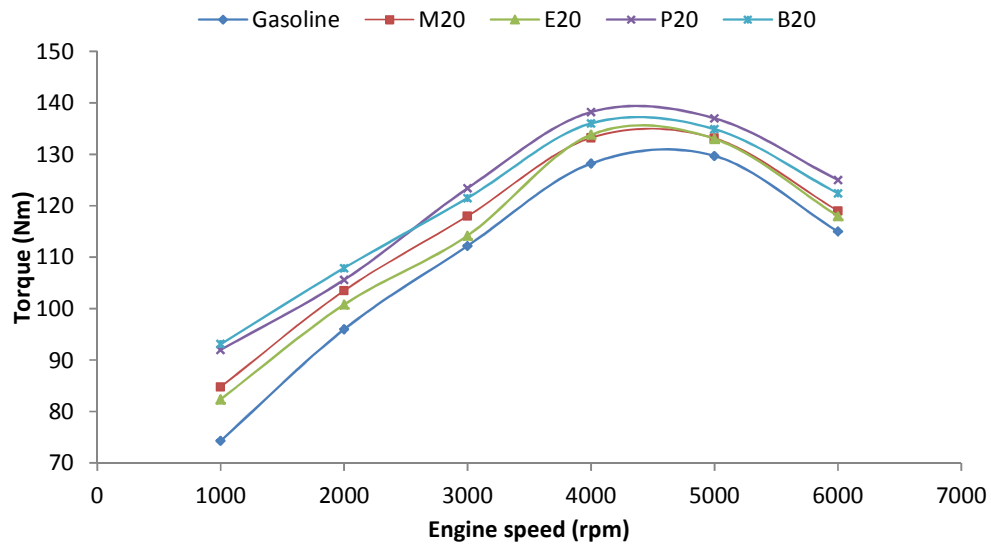
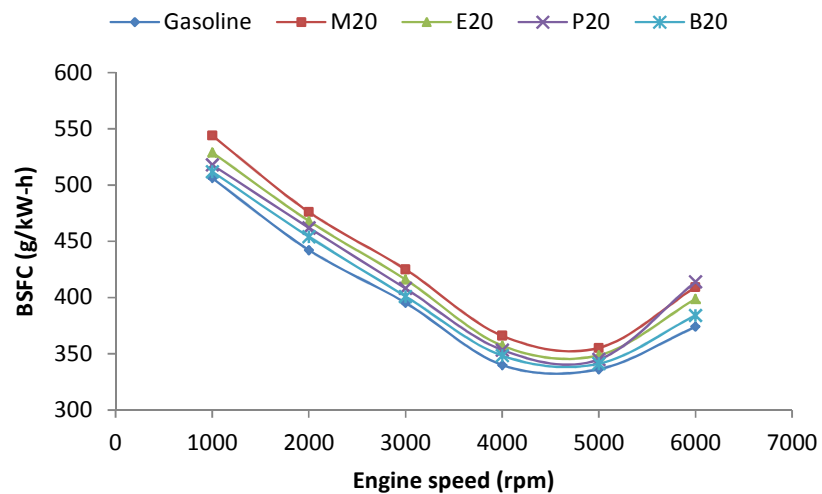
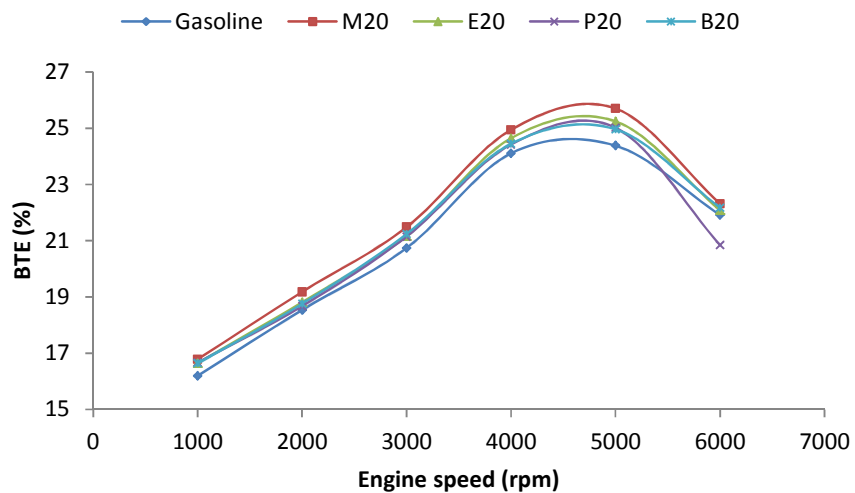


Fig. 2. Variation of torque with engine speed.



**Fig. 3. Variation of BSFC with engine speed.**



**Fig. 4. Variation of BTE with engine speed.**

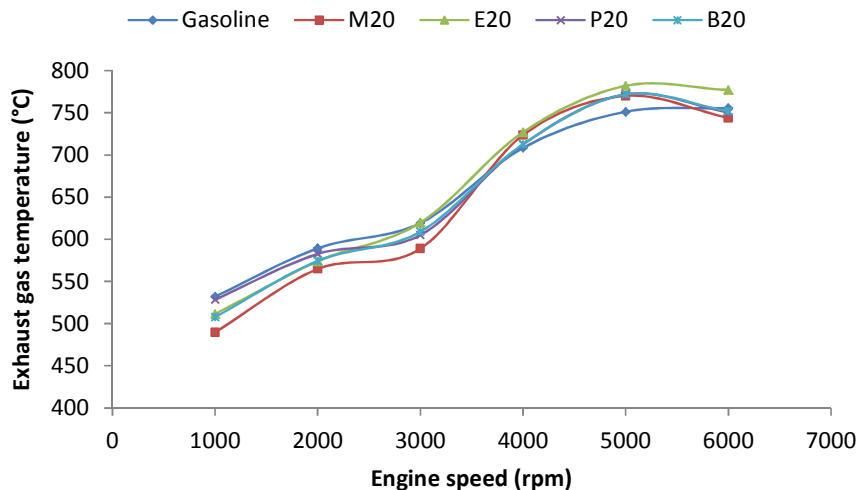


Fig. 5. Variation of Exhaust gas temperature with engine speed.

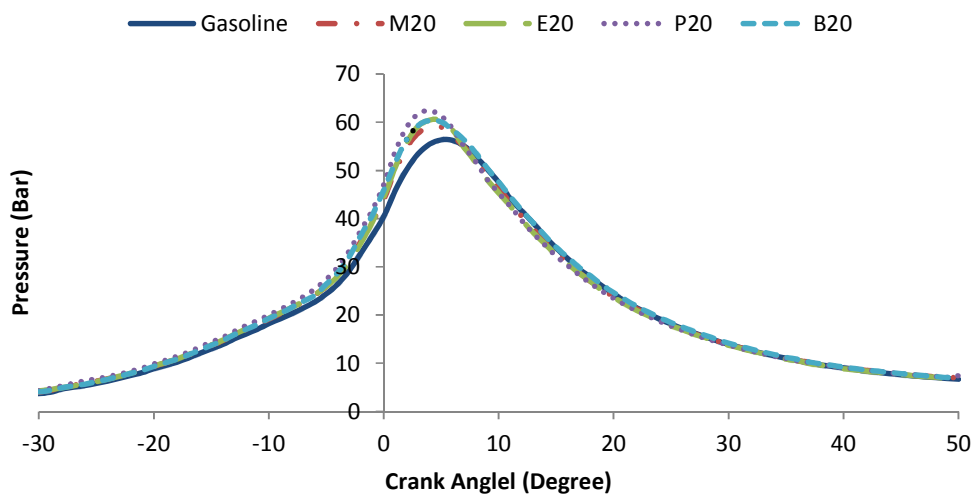


Fig. 6. Comparison of in-cylinder pressure at 4000rpm

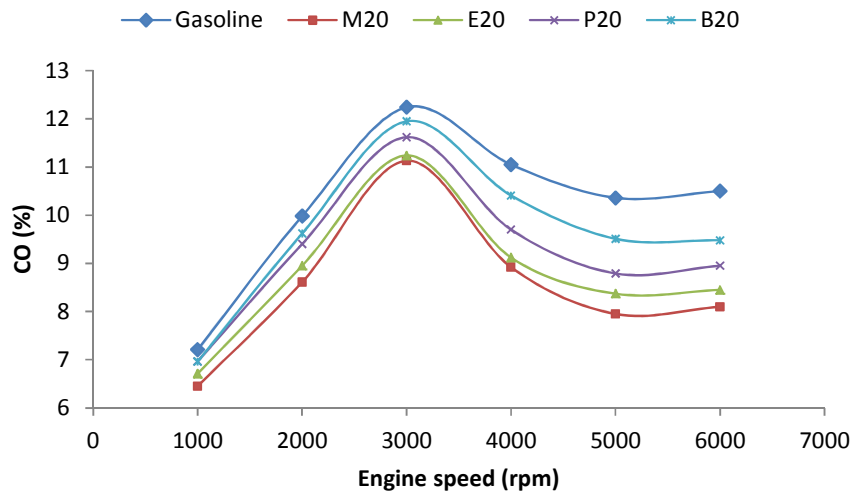


Fig. 7. Variation of CO emission with engine speed.

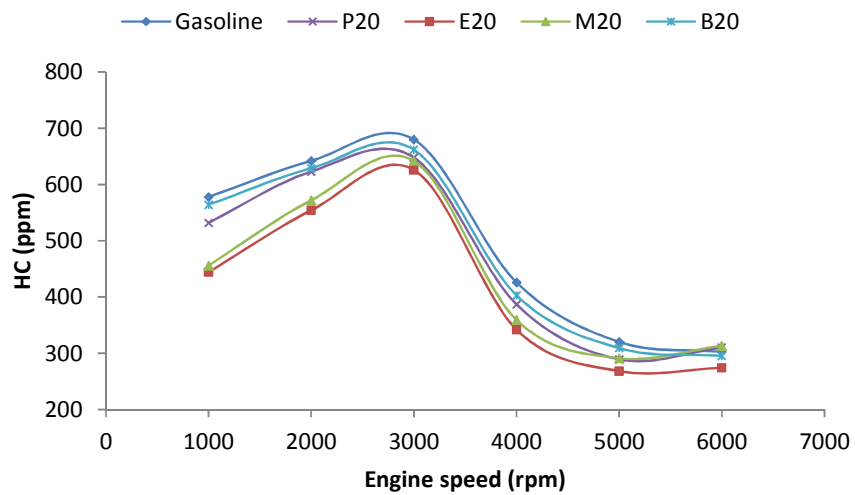


Fig. 8. Variation of HC emission with engine speed.

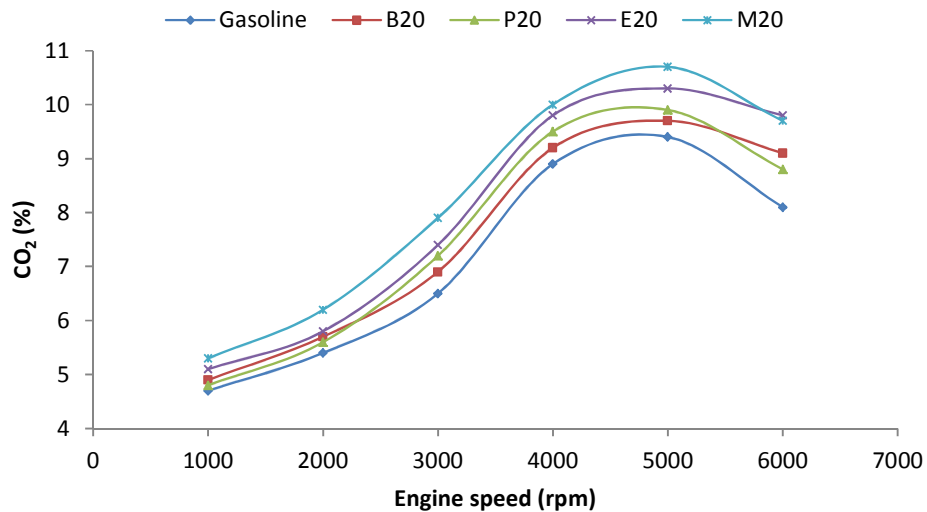


Fig. 9. Variation of CO<sub>2</sub> emission with engine speed.

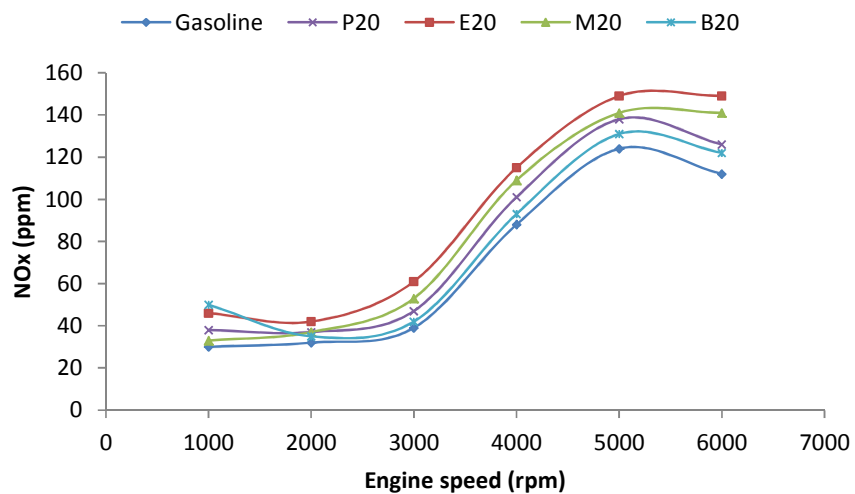


Fig. 10. Variation of NO<sub>x</sub> emission with engine speed

**Table 1: Properties of pure gasoline and different alcohol-gasoline blends.**

Property	Unit	Gasoline	M20	E20	P20	B20
Oxygen	wt. %	0	9.99	6.94	5.32	4.32
Density (at 15°C)	Kg/m <sup>3</sup>	736.8	743.82	748.3	747.32	750.64
LHV	MJ/kg	43.919	39.434	40.799	41.725	42.273
RON	--	95	98.7	99.735	100.81	97.95
RVP (at 37.8°C)	kPa	63.9	55.2	67.7	58.9	55.5
LoV	kJ/kg	349	1178	923	761	683
Specific gravity (at 15°C)	--	0.7375	0.7967	0.795	0.7899	0.8067
Dynamic viscosity (at 20°C)	mPa.s	0.516	0.521	0.629	0.802	0.925

\* Here, LHV= Lower heating value, ROM, Research octane number, RVP= Reid vapor pressure, LoV= Latent heat of Vaporization

**Table 2: Specification of the tested engine**

Engine parameter	Value
Number of cylinder	4
Displacement volume	1596 cm <sup>3</sup>
Bore	78mm
Stroke	84mm
Connecting rod length	131mm
Compression ratio	10:1
Fuel system	Multi-point electric port fuel system
Max output (at rpm)	78kW at 6000rpm
Max torque ( at rpm)	135N-m at 4000rpm

**Table 3: Specifications of the exhaust gas analyzer**

	Measurement range	Detection limit
CO	0-10% vol.	0.01 % Vol.
CO <sub>2</sub>	0-20% vol.	0.1 % Vol.
HC	0-20.000 ppm vol.	1 ppm
NO <sub>x</sub>	0-5.000 ppm vol.	1 ppm
O <sub>2</sub>	0-25 % vol.	0.01 % Vol.