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## ARTICLE

# Ferroelectric Domain Morphology and Temperature-Dependent Piezoelectricity of (K,Na,Li)(Nb,Ta,Sb)O<sub>3</sub> Lead-Free Piezoceramics

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Cite this: DOI: 10.1039/x0xx00000x

Received 00th January 2012,  
Accepted 00th January 2012

DOI: 10.1039/x0xx00000x

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Domain morphology and temperature-dependent piezoelectricity in terms of piezoelectric coefficient  $d_{33}$  and normalized strain  $d_{33}^*$  of (K,Na,Li)(Nb,Ta,Sb)O<sub>3</sub> lead-free piezoceramics at polymorphic phase boundary were investigated. Transmission electron microscopy (TEM) and piezoresponse force microscopy (PFM) studies revealed the characteristic domain morphology comprising strip-like domains and featureless domains. Moreover, a facile method based on the field-dependent piezoelectric coefficient  $d_{33}(E)$  measurement was verified to characterize *in situ* temperature dependence of piezoelectric coefficient  $d_{33}$ , as an alternative for the conventional *ex situ* route. It was demonstrated that the normalized strain  $d_{33}^*$  exhibits superior thermal resistance to piezoelectric coefficient  $d_{33}$ , though both parameters are susceptible to temperature variation.

## 1 Introduction

The functionality of direct conversion between electrical and mechanical energy endows piezoelectric materials with wide-ranging applications, e.g., actuators, transducers, and sensors, etc.<sup>1</sup> As environmental consciousness is heightened, the currently dominating Pb(Zr,Ti)O<sub>3</sub> (abbreviated as PZT) family is confronted with global restrictions such as the WEEE Directive (Waste of Electrical and Electronic Equipment) and the RoHS Directive (Restriction of certain Hazardous Substances) due to the large portion of hazardous lead substance it contains, albeit its superior piezoelectric performance. Therefore, last decade has witnessed considerable dedication devoted to developing high-end lead-free counterparts to substitute for PZT.<sup>2-8</sup>

The breakthrough achieved by Saito *et al.*<sup>8</sup> in textured (K,Na)NbO<sub>3</sub> (KNN)-based lead-free piezoceramics with remarkable piezoelectricity crowned this system with enormous opportunities to be one of the most promising candidates, and accordingly triggered worldwide interest.<sup>2, 3, 6</sup> Most of the researches emphasized on tailoring the piezoelectric performance via compositional modification<sup>9, 10</sup> or domain engineering,<sup>11, 12</sup> which are actually related to manipulating the polymorphic phase transition (PPT) around room temperature. It is generally agreed that the increased polarization directions in PPT region benefit the enhancement of piezoelectric performance at ambient temperature.<sup>13, 14</sup> Furthermore, contributions originating from domain hierarchy<sup>15</sup> resemble that in lead-based<sup>16</sup> and lead-free<sup>17</sup> counterparts with the distinct phase structures of morphotropic phase boundary (MPB). It is proved that transmission electron microscopy (TEM) is a

powerful tool to uncover the domain hierarchy,<sup>15</sup> while piezoresponse force microscopy (PFM) can deliver fruitful information about the domain orientation.<sup>14, 18</sup> A combination of TEM and PFM techniques may provide more perspicuous schema of domain morphology, which has been rarely reported for KNN. However, industrial implements demand not only the good piezoelectric performance at room temperature but also its stability in response to ambience changes. In contradiction to the temperature-independent MPB in PZT systems, the PPT in KNN-based ceramics is considered with the drawback of high sensitivity to temperature fluctuation, which is unfavorable for practical applications.<sup>19-21</sup> Therefore, it is necessary to carefully evaluate the temperature-dependent piezoelectricity of KNN-based ceramics. Nevertheless, only a few works reported the temperature-dependent piezoelectric coefficient  $d_{33}$  of KNN-based ceramics.<sup>22-24</sup> Wang *et al.*<sup>22</sup> showed the *in situ* measurement of temperature-dependent  $d_{33}$  on a custom-designed apparatus, while an *ex situ* annealing-measuring route was adopted in most studies.<sup>23, 24</sup> Then, it would be attractive to both scientific and technological domains if a simple method can be developed to characterize the *in situ* temperature dependence of  $d_{33}$ .

In the present study, domain morphology and temperature-dependent piezoelectric response of (K,Na,Li)(Nb,Ta,Sb)O<sub>3</sub> (KNNLTS) ceramics were investigated systematically. Featured domain morphology embodied by the coexistence of strip-like domains and featureless domains was observed by TEM and PFM. In addition, a novel and facile method based on the field-dependent piezoelectric coefficient  $d_{33}(E)$  measurement was successfully demonstrated to characterize the *in situ* change of piezoelectric coefficient  $d_{33}$  with temperature.

## 2 Experimental

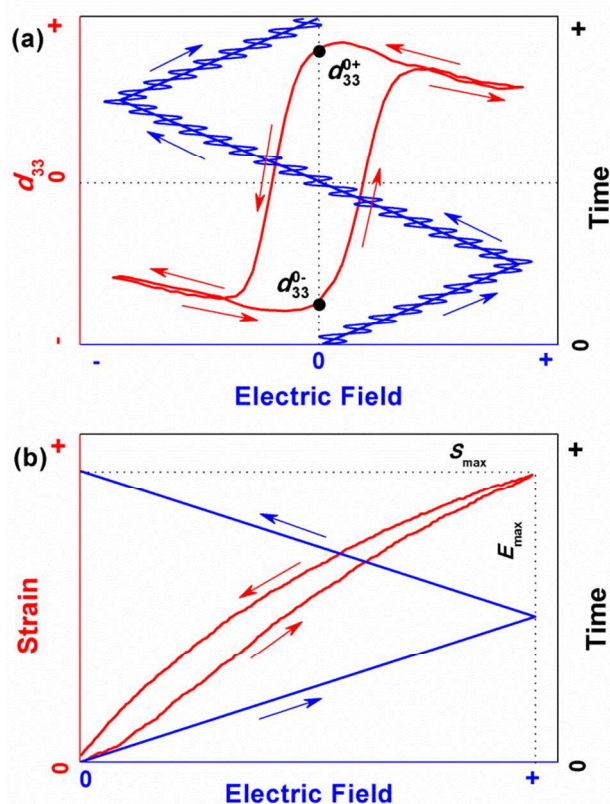
### Sample preparation

Piezoceramics with the nominal composition of  $\text{Li}_{0.02}(\text{K}_{0.45}\text{Na}_{0.55})_{0.98}(\text{Nb}_{0.77}\text{Ta}_{0.18}\text{Sb}_{0.05})\text{O}_3$  (KNNLTS) were fabricated via a conventional ceramic processing route with raw materials of  $\text{K}_2\text{CO}_3$  (99 %),  $\text{Na}_2\text{CO}_3$  (99.8 %),  $\text{Li}_2\text{CO}_3$  (97 %),  $\text{Nb}_2\text{O}_5$  (99.95 %),  $\text{Ta}_2\text{O}_5$  (99 %), and  $\text{Sb}_2\text{O}_3$  (99 %). The starting chemicals were weighted stoichiometrically and planetary ball milled for 24 h in an ethanol solution. The weight ratio between the milling balls and raw materials is about 10:1 and the rotational speed during ball milling is  $250 \text{ min}^{-1}$ . The slurry was dried and calcined at  $850 \text{ }^\circ\text{C}$  for 5 h. The synthesized powders were subjected to ball milling again for another 24 h in ethanol. After drying, the powders were pressed into disks of 10 mm in diameter and 1.5 mm in thickness, followed by cold isostatic pressing under 200 MPa for 2 min. Such pellets were sintered at  $1100\text{--}1120 \text{ }^\circ\text{C}$  in air for 2 h. For macroscopic electrical characterization, the as-sintered ceramics were polished down to 1 mm in thickness and painted with silver pastes fired at  $550 \text{ }^\circ\text{C}$  for 30 min to form electrodes. The samples were poled under an electric field of  $4 \text{ kV mm}^{-1}$  at  $120 \text{ }^\circ\text{C}$  in silicone oil for 30 min.

### Characterization of phase structure and electrical properties

High-resolution X-ray diffraction (XRD) measurement was conducted to determine the crystal structure by using  $\text{Cu K}\alpha$  radiation (Rigaku, D/Max250, Tokyo, Japan). The temperature dependence of dielectric permittivity and loss were determined using an impedance analyzer (HP 4192A, Palo Alto, CA). The piezoelectric coefficient  $d_{33}$  was measured using a quasi-static  $d_{33}$  meter (ZJ-3A, Institute of Acoustics, Chinese Academy of Science, Beijing, China), by which a small oscillating force is applied to the samples and the charge output is measured and divided by the applied force amplitude. The ferroelectric properties, field-dependent piezoelectric coefficient  $d_{33}(E)$  hysteresis loops, and unipolar piezoelectric strain  $S(E)$  curves were recorded on a ferroelectric tester (aixACCT TF Analyzer 1000, Germany). For the polarization  $P(E)$  hysteresis loops measurement, an electric field of  $3 \text{ kV mm}^{-1}$  at 1 Hz was applied. The input and output signals for the field-dependent piezoelectric coefficient  $d_{33}(E)$  measurement and the unipolar piezoelectric strain  $S(E)$  measurement are illustrated in Fig. 1. The excitation signal for the field-dependent piezoelectric coefficient  $d_{33}(E)$  measurement is a continuously changing triangular-shaped base waveform of low frequency with a superimposed high frequency small signal voltage. It is an electric field with a frequency of 1 Hz and amplitude of  $3 \text{ kV mm}^{-1}$ , on which an AC voltage of 25 V and 250 Hz was superimposed, in this case. The displacement data  $d_0$  is simultaneously captured with an additional external displacement sensor, e.g., laser interferometer according to the equation:<sup>25</sup>

$$d_0 = (\lambda/1.414\pi)(V_{\text{out}}/V_{\text{p-p}}) \quad (1)$$



**Fig. 1** Illustration of input and output signals for (a) the field-dependent piezoelectric coefficient  $d_{33}(E)$  measurement and (b) the piezoelectric strain  $S(E)$  measurement, respectively.

where  $\lambda$ ,  $V_{\text{out}}$ , and  $V_{\text{p-p}}$  are the wavelength of monochromatic laser, the detected signal, and the peak to peak value of the interference signal, respectively. And then the field-dependent piezoelectric coefficient  $d_{ij}(E)$  can be derived from the displacement data using the following equation:<sup>25</sup>

$$d_{ij}(E) = (d_0/U)(t/x) \quad (2)$$

where  $U$  is the driving voltage amplitude,  $x$  is the corresponding length in the direction of sample deformation,  $t$  thickness of the sample in the direction of the applied electric field.  $x$  equals to  $t$  in the case of  $d_{33}(E)$  measurement. Thus the positive value at zero field in the  $d_{33}(E)$  hysteresis loops denoted by  $d_{33}^{0+}$  (see Fig. 1(a)) can be taken as piezoelectric coefficient  $d_{33}$ . For the piezoelectric strain  $S(E)$  measurement, a unipolar triangular-shaped electric field is applied to the specimen, and the displacement is documented at the same time. The normalized strain  $d_{33}^*$  can be deduced from the below equation:<sup>4</sup>

$$d_{33}^* = S_{\text{max}}/E_{\text{max}} \quad (3)$$

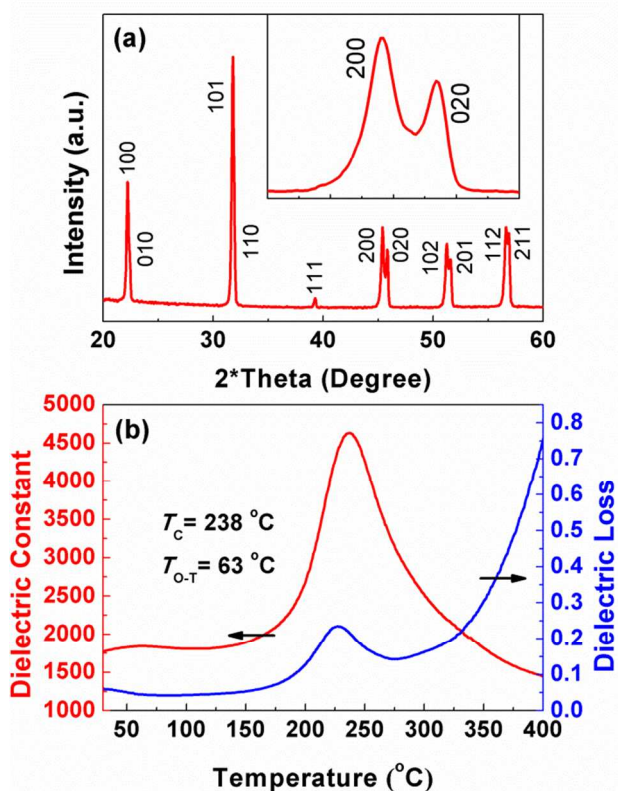
where the  $E_{\text{max}}$  and  $S_{\text{max}}$  are the maximum applied electric field and corresponding unipolar strain output, respectively, as depicted in Fig. 1(b).

### Details of TEM and PFM studies

The TEM specimens were prepared by mechanically polishing to a thickness of approximately 20  $\mu\text{m}$ . The central parts of the

disks were further reduced by precision argon-ion milling (RES101, Leica EM, Wetzlar, Germany) at an acceleration voltage of 4 kV. These specimens were investigated using a high-resolution TEM (HRTEM JEOL 2011, Tokyo, Japan) operated at 200 kV with a point resolution of 0.19 nm. For the PFM observations, the as-sintered samples were mechanically polished to about 20  $\mu\text{m}$  in thickness. The PFM experiments were carried out using a commercial atomic force microscopy (MFP-3D, Asylum Research, USA). The PFM signal was recorded at room temperature under ac voltage  $U_{ac}=5\text{--}10\text{ V}$ ,  $f_{ac}=50\text{ kHz}$  applied to a conductive Pt-Ir coated cantilever PPP-NCHPt (Nanosensors, Switzerland). Both vertical and lateral PFM images were taken, which provide information about the distribution of out-of-plane and in-plane components of ferroelectric domains, respectively.

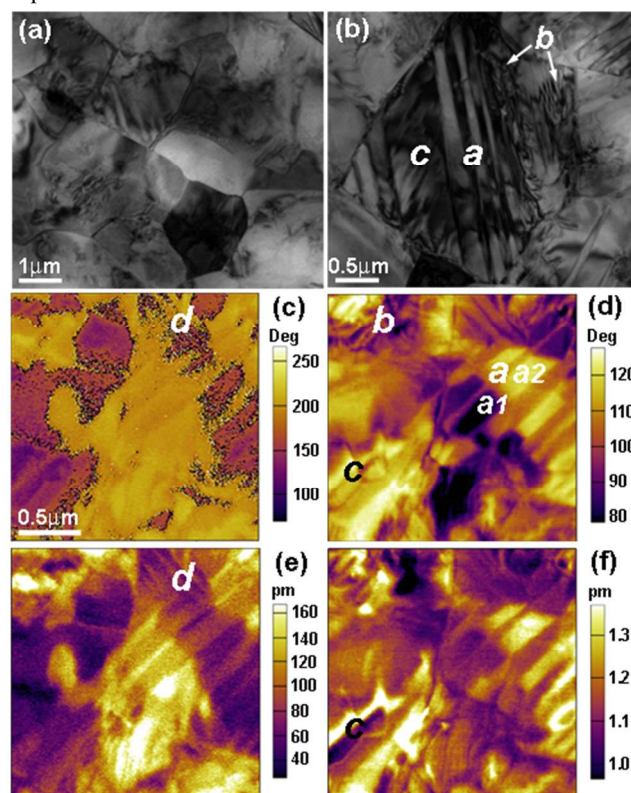
### 3 Results and Discussion



**Fig. 2** (a) The XRD pattern of as-sintered KNNLTS ceramics; (b) temperature dependence of dielectric permittivity and dielectric loss of poled KNNLTS ceramics.

The XRD pattern of KNNLTS ceramics is presented in Fig. 2(a), for which the index for an orthorhombic phase was adopted, exhibiting a typical perovskite structure. It is well-accepted that the piezoelectricity of KNN-based ceramics is magnificently dependent on the phase structures, which can be roughly quantified by analyzing the relative intensities of (200) and (020) peaks ( $I_{200}/I_{020}$ ) around  $2\theta=45^\circ$ . For randomly-oriented piezoceramics with an orthorhombic symmetry, the ideal ratio  $I_{200}/I_{020}$  equals to 2:1, while it evolves to 1:2 for a

tetragonal phase.<sup>26</sup> However, more detailed information about high-angle X-ray diffraction, such as (222) and (004) peaks, is indispensable for precise analysis of crystallographic or domain evolution.<sup>11, 26</sup> For the present material, the  $I_{200}/I_{020}$  ratio is slightly higher than 1 (see the enlarged peaks in the inset figure of Fig. 2(a)), indicating the coexistence of orthorhombic and tetragonal phases with orthorhombic being the dominating symmetry. The XRD results are supported by the temperature-dependent dielectric constant and loss measurement, as shown in Fig. 2(b). Two anomalies are observed around 63  $^\circ\text{C}$  and 238  $^\circ\text{C}$  in the dielectric constant curve, corresponding to the polymorphic phase transition point  $T_{O-T}$  and Curie temperature  $T_C$ , respectively. It should be mentioned that the dielectric measurement was conducted in a heating cycle, and the inherent thermal hysteresis usually results in higher output of  $T_{O-T}$  and  $T_C$  than the real values on a scale of tens of degree Celsius. In other words, the polymorphic phase transition point  $T_{O-T}$  should be located near the room temperature. Benefiting from the PPT effect, superior piezoelectric performance can be expected.<sup>13</sup>



**Fig. 3** TEM analysis of typical (a) grain distribution and (b) domain configuration; (c) vertical piezoreponse force microscopy (VPFM) image and (d) lateral piezoreponse force microscopy (LPFM) image of domain morphology, and the corresponding piezoreponse amplitude of (e) VPFM and (f) LPFM modes of KNNLTS ceramics.

For ferroelectric polycrystals, domain morphology is closely related with piezoelectric performance.<sup>16, 27, 28</sup> In the present work, TEM and PFM were employed to explore the

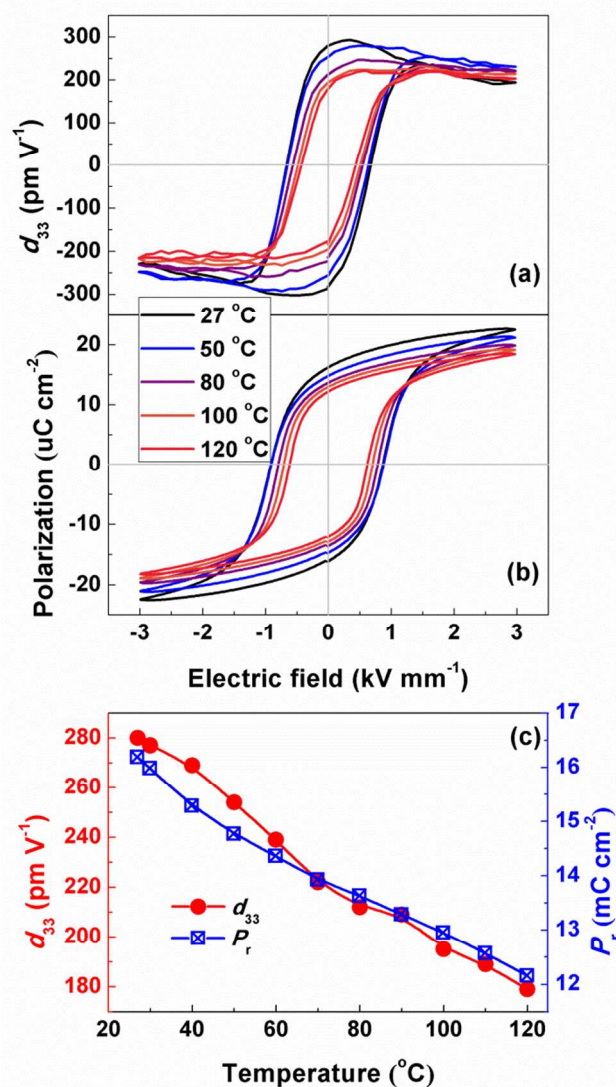
microstructure of KNNLTS ceramics, respectively. The TEM image displayed in Fig. 3(a) shows that the KNNLTS ceramics have typical square-shaped grains with grain sizes ranging from 1 to 3  $\mu\text{m}$ . It was reported that the coexistence of orthorhombic and tetragonal phase structures at room temperature will result in complex domain patterns.<sup>15</sup> Representative domain structures of KNNLTS piezoceramics were observed, as shown in Figs. 3(b-d). It should be noted that typical domain patterns composed of submicro- and nano-sized domains could be found in one single grain. Fig. 3(b) shows that strip-like domains with width of several hundred nanometers marked as area *a* and irregular-shaped (featureless) domains in nano-scale in area *b* coexist, agreeing well with the results reported previously.<sup>15, 29</sup> Most intriguingly, the nano-domains with an average size of 100 nm developed in submicro-domains forming a domain hierarchy (see area *c*); and the angle between nano- and submicro-domain walls in the projection plane is approximately  $45^\circ$ , resembling to that of PZT<sup>16</sup> and BCZT<sup>30</sup> compositions with phase coexistence. It was disclosed that domain size is proportional to the square root of domain wall energy.<sup>31</sup> In general, piezoelectric effect comprises intrinsic and extrinsic contributions. The former refers to the linear piezoelectric effect of lattice displacement, while the latter relates to the movement of domain walls.<sup>32</sup> The reduced domain wall energy renders nano-domains readily respond to external excitations, e.g., mechanical force or electric field, contributing as extrinsic portions.

PFM observations are consistent with TEM outcomes, as demonstrated in Figs. 3(c-f). The vertical and lateral PFM phase images shown in Figs. 3(c) and (d) evidence that the domain morphology of KNNLTS ceramics indeed comprises strip-like ferroelastic domains (area *a*) and featureless nano-sized domains (area *b*). Figs. 3(e) and (f) present the vertical and lateral piezoresponses, respectively, which are mainly from the intrinsic components. Generally, an orthorhombic system provides twelve possible spontaneous polarizations  $P_s$  in all  $\langle 110 \rangle$  directions, while there are six  $P_s$  in directions of  $\langle 100 \rangle$  for a tetragonal symmetry. The angles between two polarization vectors for KNN can be  $90^\circ$  and  $180^\circ$  as in a tetragonal system or  $60^\circ$  and  $120^\circ$  for orthorhombic crystals. Combined analysis of phase and piezoresponse images can provide detailed information about domain orientations. Take the domains denoted by *a1* and *a2* in area *a* for example. The phase difference between *a1* and *a2* is about  $50^\circ$  with a larger piezoresponse observed in *a1*. Considering the possible domain orientations in orthorhombic-tetragonal phases coexisting KNN-based piezoceramics, the reasonable explanation is that they are  $60^\circ/120^\circ$  domains for *a1* and *a2* with *a1* lying in-plane. For domains in area *c*, no obvious contrast was observed in the phase image, whereas difference in piezoresponse exists in this area, implying the presence of  $90^\circ$  domains. A trace of  $180^\circ$  domains, which shows distinct contrast in phase while have the same piezoresponse in the vertical imaging mode, was also recorded in area marked as *d*. However, it can be inferred from the PFM study as discussed above, orthorhombic phase prevails in this system, though it is proved to be coexistence of

orthorhombic and tetragonal symmetries. These findings match well with the above XRD and TEM investigations.

**Table 1** Comparison of  $d_{33}$  or  $d_{33}^*$  values measured by three distinctive methods at room temperature.

Method	Quasi-Static $d_{33}$ Meter	Field-Dependent Piezoelectric Coefficient $d_{33}(E)$ Measurement	Piezoelectric Strain $S(E)$ Measurement
$d_{33}$ or $d_{33}^*$ ( $\text{pC N}^{-1}$ )	$267 \pm 7$	$280 \pm 5$	$361 \pm 11$



**Fig. 4** Temperature-dependent (a) piezoelectric coefficient  $d_{33}(E)$  hysteresis curves, (b) polarization  $P(E)$  hysteresis loops, and (c) piezoelectric coefficient  $d_{33}$  and remnant polarization  $P_r$ .

High piezoelectricity can be expected in the KNNLTS ceramics at ambient temperature due to the combined effects of PPT and nano-domain contributions as aforementioned. The piezoelectric coefficient  $d_{33}$  characterized using a quasi-static  $d_{33}$  meter reached  $267 \text{ pC N}^{-1}$  (see Table I), which is a relatively

high value for KNN-based piezoceramics. Moreover,  $d_{33}$  was evaluated by other two distinctive techniques: the field-dependent piezoelectric coefficient  $d_{33}(E)$  measurement and the piezoelectric strain  $S(E)$  measurement, as shown in the following.

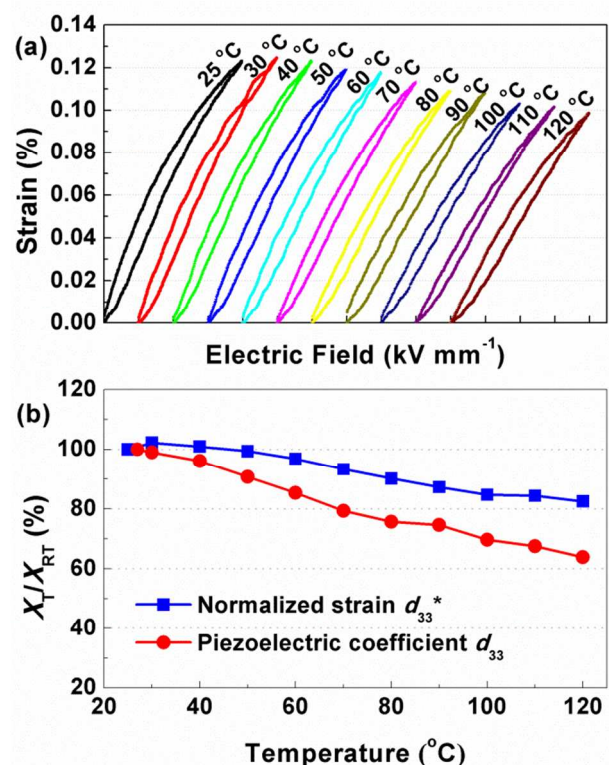
The field-dependent piezoelectric coefficient  $d_{33}(E)$  measurement yielded a  $d_{33}$  value of  $280 \text{ pC N}^{-1}$  at room temperature (as listed in Table I), slightly higher but comparable to the value obtained by a quasi-static  $d_{33}$  meter. Recently, the equivalence between the field-dependent piezoelectric coefficient  $d_{33}(E)$  measurement and quasi-static  $d_{33}$  meter has also been verified by Fialka *et al.*<sup>33</sup> Therefore, it may offer a facile method to evaluate the *in situ* temperature-dependent piezoelectric coefficient  $d_{33}$ ; concerning the feasibility to measure the  $d_{33}(E)$  hysteresis loops at varied temperatures. Figs. 4(a) and (b) provide the  $d_{33}(E)$  curves and polarization hysteresis  $P(E)$  loops at different temperatures, respectively, from which the temperature dependence of piezoelectric coefficient  $d_{33}$  and remnant polarization  $P_r$  can be obtained, as summarized in Fig. 4(c).  $d_{33}$  decreases monotonically with increasing the temperature, and 40 % reduction of  $d_{33}$  occurs when the temperature reaches  $120 \text{ }^\circ\text{C}$ . For piezoelectric crystals, the intrinsic piezoelectric coefficient  $d_{33}$  can be determined by the following equation:<sup>22, 32</sup>

$$d_{33} = 2Q\epsilon_0\epsilon_{33}P_3 \quad (4)$$

where  $Q$  is the electrostrictive constant and barely varies with temperature;<sup>34</sup>  $\epsilon_0$  is the vacuum permittivity;  $\epsilon_{33}$  is the permittivity and in this case it does not change much in the temperature range from room temperature to  $120 \text{ }^\circ\text{C}$ , as shown in Fig. 2(b). However,  $P_3$  is the polarization along the polar axis and approximately equals to remnant polarization  $P_r$  for ferroelectric polycrystals, which in the case shares a similar trend with  $d_{33}$  within the same temperature range. Thus the loss of polarizations at elevated temperatures possibly due to the PPT effect may be responsible for the reduction of  $d_{33}$ . Additionally, the characteristic domain morphology at polymorphic phase boundary gradually diminishes and the related extrinsic contribution to piezoelectric response also becomes weaker with increasing temperature.

A high piezoelectric coefficient  $d_{33}$  is recognized as the figure of merit for electromechanical applications, e.g., sensors or ultrasonic devices; while the normalized strain  $d_{33}^*$  is the key feature that matters in actuator systems.<sup>4</sup> The piezoelectric strain  $S(E)$  measurement gives a  $d_{33}^*$  value of  $361 \text{ pm V}^{-1}$  at an electric field of  $4 \text{ kV mm}^{-1}$  (see Table I). It is interesting to note that the normalized strain  $d_{33}^*$  is much larger than piezoelectric coefficient  $d_{33}$ , which may originate from the constitution of piezoelectric effect. As elucidated in the foregoing part, both intrinsic and extrinsic contributions constitute the piezoelectricity. The intrinsic contribution should be on the same level regardless of measuring approaches, while the extrinsic component is sensitive to external excitation, especially in the case of ceramics with nano-domains. For quasi-static  $d_{33}$  meter and the field-dependent piezoelectric coefficient  $d_{33}(E)$  measurement, low external fields (mechanical or electrical) of  $0.25 \text{ N}$  and  $25 \text{ V}$  were applied, respectively.

However, the piezoelectric strain  $S(E)$  measurement was done under an electric field well-above coercive field  $E_C$ . The higher extrinsic contribution from domain wall movement to the response of piezoelectric strain  $S(E)$  measurement may be the origin of much larger normalized strain  $d_{33}^*$  over the piezoelectric coefficient  $d_{33}$ . Furthermore, the electric-field-induced domain switching in piezoelectric strain  $S(E)$  measurement could be the additional income of strain.



**Fig. 5** (a) Unipolar piezoelectric strain  $S(E)$  curves at varied temperatures and (b) temperature stability of normalized strain  $d_{33}^*$ . The data of piezoelectric coefficient  $d_{33}$  was provided for comparison.

Though the KNNLTS ceramics exhibit high piezoelectricity including both piezoelectric coefficient  $d_{33}$  and normalized strain  $d_{33}^*$  at room temperature, a temperature-insensitive strain behavior is indispensable to secure successful implements of the material in actuator systems.<sup>19, 22</sup> In this work, temperature-dependent  $d_{33}^*$  of KNNLTS ceramics was also reported. The temperature dependence of unipolar  $S-E$  curves and corresponding  $d_{33}^*$  values are presented in Fig. 5. The  $d_{33}^*$  peaks around the temperature of  $30 \text{ }^\circ\text{C}$ , and the variation is within 18 % in the whole temperature range. An intriguing phenomenon was observed that the normalized strain  $d_{33}^*$  possesses better temperature stability in comparison with that of small signal piezoelectric coefficient  $d_{33}$ . These phenomena are in accordance with our previous investigations on  $\text{CaZrO}_3$ -modified  $(\text{K,Na,Li})(\text{Nb,Ta})\text{O}_3$  ceramics,<sup>35</sup> thus they are possibly independent of the nature of compositions. Although it is well known that an electric field can induce a phase transition from paraelectric to ferroelectric phases,<sup>36, 37</sup> less attention has

been paid to the analogous phenomenon between two ferroelectric phases. It is speculated that the electric field induced phase transition could be one of the possible causes for the superior temperature stability of normalized strain  $d_{33}^*$  over piezoelectric coefficient  $d_{33}$ . Moreover, the outcomes can also be interpreted from the perspective of electric-field-engineered domain configuration. For BaTiO<sub>3</sub> single crystals, the stimulation of electric field facilitates the formation of fine domain structures even at the temperature above  $T_C$ .<sup>27</sup> The engineered domain morphology remains stable below  $T_C$ , and it was believed to be the main cause of significantly enhanced piezoelectric properties. In contrast to the fading domain morphology at high temperatures during the measurement of  $d_{33}$ , the piezoelectric strain  $S(E)$  measurement is accompanied by maintaining the featured domain configuration with the aid of electric field when approaching to high temperature. Determined by the additional extrinsic contribution from domain configuration, normalized strain  $d_{33}^*$  commits better thermal resistance than piezoelectric coefficient  $d_{33}$ . In addition, it should be mentioned that the current system exhibits inferior temperature stability of strain behavior to the CaZrO<sub>3</sub>-modified (K,Na,Li)(Nb,Ta)O<sub>3</sub> (especially the one with 5 mol% CaZrO<sub>3</sub>, abbreviated as CZ5).<sup>22</sup> It was suggested that the phase structure plays a primary role in CZ5 ceramics, which is endowed with diminished difference between orthorhombic and tetragonal phases as manifested by the reduced  $c/a$  ratio.<sup>22</sup> In contrast, a distinct phase evolution process still exists in KNNLTS ceramics, which may account for the inferior temperature stability of strain behavior.

Besides, the effect of stress on the piezoelectric performance, including the piezoelectric coefficient  $d_{33}$  and normalized strain  $d_{33}^*$ , is important for the applications of piezoceramics. It was reported that piezoelectric coefficient  $d_{33}$  is barely affected by the hydrostatic pressure in niobate single crystals,<sup>38</sup> while the  $d_{33}$  of PZT ceramics was shown to be sensitive to external stress.<sup>39</sup> In the case of normalized strain  $d_{33}^*$ , it is better to use the terminology of blocking stress, which means the maximum stress an actuator can generate against an infinitely stiff external clamping.<sup>4</sup> Literatures indicate that the lead-free systems could generate comparable blocking force with PZT ceramics.<sup>4</sup>

## Conclusions

In summary, domain morphology and temperature-dependent piezoelectricity of (K,Na,Li)(Nb,Ta,Sb)O<sub>3</sub> (KNNLTS) lead-free piezoceramics at polymorphic phase boundary were investigated. The joint effects of polymorphic phase transition and nano-domain contribution were identified to be the origin of the superior piezoelectric performance in the system. Besides, a novel and facile method based on the field-dependent piezoelectric coefficient  $d_{33}(E)$  measurement was demonstrated the capability of evaluating the *in situ* temperature-dependent piezoelectric coefficient  $d_{33}$ , which may facilitate the development of lead-free piezoceramics.

## Acknowledgements

This work was supported by National Nature Science Foundation of China (Grants no. 51332002, 51302144, 51221291, 51211140345) and the Ministry of Science and Technology of China under the Grant 2009CB623304.

## Notes and references

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