

Environmental Science Nano

Accepted Manuscript



This is an *Accepted Manuscript*, which has been through the Royal Society of Chemistry peer review process and has been accepted for publication.

Accepted Manuscripts are published online shortly after acceptance, before technical editing, formatting and proof reading. Using this free service, authors can make their results available to the community, in citable form, before we publish the edited article. We will replace this *Accepted Manuscript* with the edited and formatted *Advance Article* as soon as it is available.

You can find more information about *Accepted Manuscripts* in the [Information for Authors](#).

Please note that technical editing may introduce minor changes to the text and/or graphics, which may alter content. The journal's standard [Terms & Conditions](#) and the [Ethical guidelines](#) still apply. In no event shall the Royal Society of Chemistry be held responsible for any errors or omissions in this *Accepted Manuscript* or any consequences arising from the use of any information it contains.

1 Title: Potential Exposure and Treatment Efficiency of Nanoparticles in Water Supplies based on Wastewater

2 Reclamation

3 Peter Kirkegaard, Steffen Foss Hansen*, Martin Rygaard

4 Department of Environmental Engineering, Technical University of Denmark

5 *Corresponding author

6 Keywords: Wastewater reuse; potable reuse; nanoparticles; reclamation; drinking water

7

8

9 ***Highlights***

- 10 • We present current knowledge on nanoparticle fate in wastewater reclamation systems for potable
11 reuse

12 ***Nano impact (120 words)***

13 In this article we present the first ever evaluation of the removal of nanoparticles in waste water and water
14 treatment processes in order to estimate concentrations of NPs in reclaimed wastewater for potable reuse.
15 Based on mass flow analysis of two specific water reclamation cases (i.e. Orange County and Berlin) and a
16 literature review, we find that silver (Ag), titanium dioxide (TiO₂), and zinc oxide (ZnO) nanoparticles may
17 occur in concentrations up to 3 µg/L (Ag), 147 µg/L (TiO₂), and 0.3 µg/L (ZnO). Critical research needs
18 evolve around understanding the fate of nanoparticles treated by reverse osmosis, UV and disinfection
19 processes and understanding which kinds of nanoparticles in various types of products end up in our water
20 supply.

21 ***Abstract***

22 Water scarcity brings an increased focus on wastewater reclamation for drinking water supply. Meanwhile,
23 the production volume of nanoparticles (NPs) is rapidly increasing, but to date there has been little
24 attention to the fate of NPs in water systems based on wastewater reclamation. We have investigated the
25 possible concentrations of silver (Ag), titanium dioxide (TiO₂), and zinc oxide (ZnO) nanoparticles in tap
26 water for water supplies based on reclaimed wastewater. Tap water concentrations of the NPs were
27 assessed by mass flow analyses of two typical wastewater reclamation concepts: 1) advanced membrane
28 treatment and 2) bank infiltration, similar to systems established in Orange County, CA, USA and Berlin,
29 Germany. The mass flow analyses are based on a literature review of known wastewater concentrations of
30 NPs and removal efficiencies for the implemented treatment stages in two case systems. Few studies are
31 available on the removal efficiencies of NPs by advanced water treatment processes with a majority of

32 identified studies focusing on removal efficiencies in wastewater treatment plants and fate in surface
33 waters. The NP removal efficiency of several treatment processes is unknown at this stage. We found worst
34 case removal efficiencies for the two cases to be 97-99.97% for Ag-NPs, 91-99.2% for TiO₂-NPs, and 92-93%
35 for ZnO-NPs. Corresponding worst case concentrations in the tap water for the advanced membrane
36 treatment were 0.04 µg/L (Ag), 147 µg/L (TiO₂), and 0.28 µg/L (ZnO). Concentration for ZnO-NPs also
37 includes zinc ions and the concentration of ZnO-NPs is likely to be lower than indicated here. Worst case
38 removal by the wastewater reclamation bank infiltration system was predicted to lead to tap water
39 concentrations up to 3.3 µg/L (Ag), 13 µg/L (TiO₂), and 0.25 µg/L (ZnO). Overall, it is found that the primary
40 removal mechanisms of NPs are aggregation, sedimentation, coagulation, and biosorption and this
41 supports conventional biological treatment processes as likely effective barriers against NPs. Advanced
42 treatment methods such as microfiltration and ultrafiltration can exhibit very low removal of ZnO-NPs or
43 zinc ions caused by dissolution of ZnO-NPs. There are marked knowledge gaps, and further research in NP
44 fate in water treatment is encouraged.

45

46 **1 Introduction**

47 Engineered nanoparticles (NPs) are used to an ever increasing extend e.g. in consumer products, but we
48 know very little about how they are used and where they end up. According to The Nanodatabase
49 (www.nanodb.dk), which is a database maintained by the Danish Ecological Council, the Danish Consumer
50 Council and Department of Environmental Engineering at the Technical University of Denmark, more than
51 1200 products claimed to be based on nanotechnology or containing nanomaterials are now available to
52 the European consumers on-line. 52% of these products entail nanoparticles suspended in liquids e.g.
53 personal care products such as cosmetics and only about 16% and 7% have surface bound NPs or NPs
54 suspended in solids and hence it is reasonable to assume that most of these compounds will ultimately end
55 up in our wastewater treatment systems (Figure 1).

56 Treated wastewater ends up in recipients such as rivers, lakes, and oceans, where it may planned or
57 unplanned (de facto) become the indirect source for drinking water supplies^{1,2}. Although few large scale
58 reclamation plants for potable reuse are operational, it has been suggested that direct potable reuse can
59 play a much larger role in future solutions to water scarcity³. With occurrence of nanoparticles in
60 wastewater it is therefore relevant to investigate their potential presence and effective treatment in
61 drinking water.

62 In this paper, we estimate the concentrations of silver (Ag), titanium dioxide (TiO₂), and zinc oxide (ZnO)
63 NPs that can be expected to end up in the water supply as a consequence of wastewater reclamation.
64 NanoAg, nanoTiO₂ and nanoZnO was chosen as they are the most commonly used NPs in consumer
65 products (Figure 2)^{4,5}. These three NPs are often suspended in liquids when used in consumer products and
66 hence can be expected to end up in the wastewater. Other nanoparticles which are produced in large
67 quantities annually are carbon black and silicon dioxide⁶. However, carbon black nanoparticles are
68 predominantly used in products (e.g. tires) which are disposed at landfills^{7,8} while the silicon dioxide is
69 predominately used in food products and is not viewed as a health hazard even in concentrations of 1500
70 mg/L⁶. Therefore, these nanoparticles are not assessed in this study.

71 **2 Method**

72 The exposure and fate of nanoparticles in water treatment was investigated by mass flow analysis of two
73 typical wastewater reclamation concepts based on a review of the current knowledge on nanoparticle fate
74 in water treatment systems. A literature review was conducted to find the current knowledge on typical NP
75 concentrations in wastewater, and their fate and transformation in wastewater treatment processes,
76 advanced wastewater treatment, surface water, drinking water treatment, and natural filtration through
77 the soil column.

78 **2.1 Two typical concepts for wastewater reclamation**

79 We estimated the potential NP concentration in drinking water for two existing water reuse systems in
80 Orange County, California, USA³ and Berlin¹. Orange County is situated in a water scarce region and relies
81 partly on import of water from outside the area. The Municipal Water District of Orange County (MWDOC)
82 base its water supply on 62% groundwater, 34% imported water, and 4% surface water⁹. Since the 1970's
83 the groundwater has been replenished by reclaimed wastewater. The wastewater reclamation system of
84 Orange County (Figure 3) consists of a conventional wastewater treatment plant (Plant no. 1) which
85 discharges its effluent to the Advanced Water Treatment Facility that is part of the Groundwater
86 Replenishment System (GWRS) for the Orange County area. The Advanced Water Treatment Facility
87 includes treatment methods such as disinfection, UV, microfiltration, and reverse osmosis. The effluent
88 from the Advanced Water Treatment Facility is suitable for drinking and is subsequently delivered to the
89 Santa Ana Groundwater Basin. After abstraction, the groundwater is disinfected before distribution to the
90 public water supply¹⁰.

91 Berlin's water supply is less technology intensive than in Orange County. In Berlin, local groundwater is
92 abstracted from local aquifers and then treated by aeration and sand filtration before distribution to the
93 city (Figure 3B). The aquifers are recharged with water from the local rivers and lakes¹¹. It is a "de facto"
94 reclamation scheme because the same rivers and lakes also receives effluent from the local conventional

95 wastewater treatment plants ¹². Because of the recognized link between wastewater effluents and the
96 drinking water ^{13,14}, Berlin has had a high awareness on keeping the state of the lakes and rivers healthy.
97 The groundwater abstraction mainly occurs from soil layers dominated by sand and gravel in a depth of 30
98 to 50m below surface ¹². In the central area of Berlin, the sewage system is combined, e.g. rain water and
99 wastewater are collected by the same pipes. In the event of an overflow in this system, some of the sewage
100 water is discharged to the rivers untreated because of WWTP capacity overload. In the aftermath of such
101 event, increased concentrations of usually well removed contaminants have been detected in the rivers
102 while contaminants usually difficult to remove are found in lower concentrations in the rivers due to
103 dilution ¹⁵.

104 ***2.2 Mass flow analysis***

105 The removal efficiency by the two systems in Berlin and Orange County was assessed using mass flow
106 analysis following the basic principles presented by Brunner ¹⁶. The considered mass flow analysis is a
107 simple model which is based on removal efficiencies identified for each of the treatment processes used in
108 the investigated waste water reclamation systems. The setup of the model is that escaping nanoparticles
109 from a previous treatment step is removed by the identified removal efficiency for a proceeding treatment
110 process. Therefore, the model does not take concentration dependency of the identified removal processes
111 into account e.g. It is well-known that removal by aggregation is concentration dependent.
112 In order to properly evaluate the NP fate in the reclamation concepts, the removal efficiencies of the three
113 NPs by the treatment stages are assessed in two scenarios representing the worst and best case
114 evaluations of the assumed removal efficiencies. The lowest removal efficiency in each range is assumed to
115 represent the worst case removal scenario while the corresponding highest removal efficiency is used for
116 the best case removal scenario. Where only a single value for the NP removal efficiency in a given
117 treatment stage has been identified, this single value is assumed to be the removal efficiency in both the
118 minimum and maximum removal scenarios. Where there is no documentation for the removal efficiency of

119 a given NP by a given treatment stage, minimum removal is assumed to be 0% and maximum removal to be
120 100%.

121 **3 Results**

122 **3.1 NP concentrations in wastewater**

123 The estimation of potential end concentration of NPs in drinking water starts with the estimation of
124 concentrations in the wastewater influent. Gottschalk et al.¹⁷ modelled concentrations of Ag-NPs, TiO₂-
125 NPs, and ZnO in WWTP effluent for US, EU, and Switzerland. Tiede et al.⁸ used different forms of modeling
126 to calculate concentrations for TiO₂-NPs and Ag-NPs in the WWTP effluent which again are based on the
127 use, product concentration, and fate estimations reported by Boxall et al.¹⁸, Mueller & Nowack¹⁹, and
128 Gottschalk et al.¹⁷. From their results we assumed WWTP influent concentrations of 107.2 µg/L for Ag-NPs,
129 1,636.4 µg/L for TiO₂-NPs, and 3.6 µg/L for ZnO-NPs.

130 **3.2 Fate of NPs in treatment processes**

131 When it comes to understanding and mapping what happens with the NPs in treatment processes, the
132 specific fate and transformation process in the sewer, the WWTP, microfiltration, etc. is of vital importance.
133 Out of 71 studies identified for the period 2008-2013 (Figure 4) wastewater treatment plants (27) and
134 surface water (17) has received most attention. Then come microfiltration (7), drinking water treatment
135 plants (7), ultrafiltration (6), and soil and groundwater (6). Sewers, reverse osmosis, UV and disinfection
136 have been covered by 0-1 study each.

137 The estimated removal efficiencies of Ag-NPs, TiO₂-NPs, and ZnO-NPs by each treatment stage identified in
138 the literature are presented in table 1 and will be discussed in the following in the light of Orange County
139 and Berlin.

140 **3.2.1 Sewer**

141 Kaegi et al.²⁰ observed that due to the much larger surface areas, the Ag-NPs will tend to attach to the
142 larger surface of suspended solids rather than the biofilms in the sewage pipes. Therefore, it is likely that
143 about 0% of Ag-NPs will be retained in the sewers although a portion of the Ag-NPs might have become
144 sulfidized upon arrival at the WWTPs. No identified studies have investigated the fate of TiO₂-NPs and ZnO-
145 NPs in the sewers.

146 **3.2.2 WWTP**

147 The removal efficiency of Ag-NPs by WWTPs has been found to be in the range 39-99.9% for varying
148 conditions related to NP surface coating and concentration of TSS^{17,19-24}. However, peak loadings of Ag-NPs
149 to the WWTP, may cause a large fraction of the Ag-NPs to end up in the effluent due to constraints in
150 sorption kinetics and capacity of the biosolids to which the Ag-NPs could be attached/absorbed²². Musee
151 et al.²⁵ found that Ag-NPs have a high attraction to the sludge and low solubility regardless of the pH-level
152 of the wastewater. In general, activated sludge (e.g. heteroaggregation) is likely to be the main driver for
153 retention of Ag-NPs^{20-23,26,27}.

154 Similar to the removal efficiency of Ag-NPs, increasing concentration of TSS is likely to result in increasing
155 removal of the influent TiO₂-NPs^{24,27}. Removal efficiencies of TiO₂-NPs at 23-97% depending on the type of
156 surface coating and concentration of TSS have been observed^{24,27}. Due to the very low solubility of TiO₂-
157 NPs, the presence of ionic Ti is not expected²⁴. The results presented by Johnson et al.²⁶ indicate that the
158 primary treatment can remove about 13% and the secondary treatment (activated sludge) removes further
159 88%. Overall, Johnson et al. found the removal efficiency of TiO₂-NPs by WWTPs to be 90%²⁶.

160 Most of the ZnO-NPs are estimated to agglomerate and aggregate in WWTPs^{28,29}. Overall, the removal
161 efficiency of ZnO-NPs in WWTPs is likely to be 88-100%^{17,28}.

162 It should be noted that all three NPs are found to have a potential inhibitive effect on the microbial
163 community in the WWTPs, at least in the short term until the microbes have adapted to the new
164 compounds^{21,24,25,28,30-34}.

165 **3.2.3 Microfiltration and Ultrafiltration**

166 Micro- and ultrafiltration are key treatment stages in many wastewater reclamation schemes². Although
167 microfiltration and ultrafiltration membranes are likely to retain a significant large portion of NPs, a small
168 fraction is still expected to break through. Abbott Chalew et al. found that 55-99% of Ag-NPs and 56-100%
169 of TiO₂-NPs are likely to be retained by microfiltration membranes and that 98-100% of Ag-NPs and 96-
170 100% of the TiO₂-NPs will be retained by ultrafiltration membranes³⁵. However, the expected dissolution of
171 ZnO-NPs to zinc ions at neutral pH-values are expected to cause a much lower removal efficiency of ZnO-
172 NPs of 17-64% by microfiltration and 4-98% by ultrafiltration membranes although it is unclear how large a
173 fraction is transformed to zinc ions³⁵ (Table 1). Ladner et al. found that the removal efficiency towards NPs
174 of a membrane largely depends on the properties of the NP as well as membrane surface functionality³⁶.
175 Especially, the surface charge of the nanoparticles is essential as electrostatic repulsion/attraction with the
176 typically negatively charged membranes is an important aspect in the overall removal efficiency. Moreover,
177 the molecular weight cut-off (MWCO) of the membrane is an important parameter with higher MWCO
178 providing an increasing risk for breakthrough of especially negatively charged nanoparticles. Overall, 0-10%
179 of negatively charged Ag-NPs and TiO₂-NPs and about 100% of positively charged TiO₂-NPs were observed
180 to be removed by microfiltration membranes (pore size 0.1-10 μm³⁷). For ultrafiltration membranes (pore
181 size 1-100 nm³⁷), 60-90% of negatively charged Ag-NPs (including the 14% of Ag-NPs(-) which was
182 dissolved), 95-100% of TiO₂-NPs(-) and about 100% of TiO₂-NPs(+) was observed to be removed³⁶. The
183 removal efficiencies found by Abbott Chalew et al.³⁵ are valid for pH=7-8 of the solution while the results
184 by Ladner et al.³⁶ is for pH = 8.2-9.6. This indicates that the pH of the solution also has an effect on the
185 removal efficiency of NPs by a given membrane.

186 In Orange County, the water is treated by microfiltration after the disinfection stage in the Advanced Water
187 Treatment Facility. The pH-value of the microfiltration influent and effluent is 7.3 and 7.5, respectively ¹⁰.
188 Therefore, we assume that the removal efficiencies by Abbott Chalew et al. ³⁵ should be applicable to the
189 microfiltration units in the ATWF. It is noted that the removal efficiency in microfiltration/ultrafiltration
190 membranes possibly can increase for ZnO-NPs by adjusting for higher pH as some results indicate ³⁵.

191 **3.2.4 Disinfection**

192 When the effluent from the WWTP arrives at the Advanced Water Treatment Facility (AWTF) in Orange
193 County, the first stage of treatment is disinfection by sodium hypochlorite. Yuan et al. found that by adding
194 sodium hypochlorite to the water about 95% of Ag-NPs was removed irrespective of pH-level in the water
195 ³⁸. Hydrogen peroxide and other disinfectants are also used in the AWTF, which might contribute further to
196 the overall removal of NPs. Additionally, no studies, which investigated the corresponding removal
197 efficiency of TiO₂-NPs and ZnO-NPs, were found.

198 In Orange County, the groundwater is typically disinfected prior distribution to the consumer. 14% of the
199 extracted groundwater is treated by ultrafiltration and reverse osmosis among others before distribution ³⁹.
200 However, for this mass flow analysis, these water treatment processes are disregarded at this stage due to
201 their small share. In Anaheim, Orange County, sodium hypochlorite (12.5%) is used as the only treatment of
202 groundwater prior to distribution (Personal communication) while the water utility in Irvine Ranch adds
203 chloramines at about 3 ppm in order to keep a ratio of 4.5:1 chloramine to ammonia (Personal
204 communication). The pH-level of the groundwater in Anaheim and Irvine Ranch is 7.9 and 8.2, respectively
205 (Personal communication). However, Yuan et al. found that changes in pH-level would have little effect on
206 the removal efficiency of Ag-NPs ³⁸. Therefore, the removal efficiency of the remaining Ag-NPs in the
207 treatment of groundwater is estimated to be approximately 95%. The literature does not provide
208 corresponding values for TiO₂-NPs and ZnO-NPs and therefore, their removal efficiencies are assumed to be
209 0% and 100%, respectively in the mass flow analysis.

210 **3.2.5 Reverse Osmosis**

211 To the best of our knowledge, no studies have been published on the effectiveness of RO when it comes to
212 NPs. Due to its smaller membrane pore sizes, the removal efficiency by reverse osmosis can be expected to
213 be better than the removal efficiencies for ultrafiltration. Studies of micropollutants have shown that
214 molecules larger than the membrane pore size can pass a reverse osmosis membranes. It was found that
215 the rejection rates of micropollutants by reverse osmosis could be influenced by other parameters than size
216 exclusion, including feed water quality, fouling and membrane materials^{40,41}. Therefore, the potential of
217 reverse osmosis in retaining NPs might be less than one can expect from size exclusion alone. To account
218 for this knowledge gap, the reverse osmosis removal rates for all three NPs were assumed between 0% and
219 100% in the mass flow analysis.

220 **3.2.6 UV**

221 After the reverse osmosis treatment process, the permeate water is treated by UV irradiation. At this stage,
222 the pH of the water is at 5.7¹⁰. Yuan et al. observed that at pH=5.2, UV radiation removes about 60% of the
223 Ag-NPs in the water, but found no effect of the UV treatment on NPs at pH=7.5³⁸. We assume that the
224 removal efficiency of Ag-NPs by the Advanced Treatment Water Facility's UV treatment is likely to be up to
225 60%. Corresponding removal efficiencies were not found for TiO₂-NPs and ZnO-NPs.

226 **3.2.7 Surface Water**

227 The effluent from the WWTPs in Berlin is discharged to the surrounding rivers and lakes. Here, the NPs are
228 either transported away from the city or transported through the soil down to the groundwater at the sites
229 where bank filtration and artificial recharge is situated.

230 The effluent from the Advanced Water Treatment Facility in Orange County is pumped to the Kraemer,
231 Miller, and Miraloma Basins or to the Talbert Seawater Intrusion Barrier at the coast. At the Kraemer,
232 Miller, and Miraloma Basins, the treated water percolates to the groundwater while the treated water

233 directed to the intrusion barrier is pumped into the groundwater reservoir. In both cases, the water is
234 mixed with the existing groundwater. Due to the assumed short residence time in the basins, no
235 interactions or transformation of NPs are expected.

236 Several studies have been made on the fate and transformation of Ag-NPs in surface waters. The potential
237 retention of Ag-NPs in surface water has been predicted by Monte Carlo simulations to be around 50%^{17,19}.
238 The possible retention of TiO₂-NPs and ZnO-NPs in surface water has been assessed by experimental results
239 and Monte Carlo simulations which estimate that 53-100% of TiO₂-NPs are likely to be retained while ZnO-
240 NPs will be removed 24-75%^{17,19,42,43}. The retention of Ag-NPs, TiO₂-NPs, and ZnO-NPs in surface water are
241 likely to be determined by several factors such as the surface coating of the NPs, flow rate, and pH
242^{17,19,42,43}. The found percentage ranges for retention are estimated to be the best guess for Berlin while no
243 retention is assumed in the basins in Orange County.

244 **3.2.8 Soil and Groundwater**

245 The unsaturated layers in Berlin and Orange County are predominantly sand and gravel, especially in the
246 top layers^{10,12,44}. However, silts and clays are also present in large quantities in certain areas of Orange
247 County. The proportion mechanisms of sand, silt, and clay and particle route in the Santa Ana groundwater
248 basin in Orange County is unknown. The removal efficiency by the unsaturated zone in both cases are
249 estimated to be 26-71% for Ag-NPs and 5-99% for TiO₂-NPs⁴⁵⁻⁴⁷. Based on laboratory tests, the retention in
250 the natural aquifers are expected to be governed by ionic strength, NOM, residual chloride, low grain sizes,
251 and pH^{43,45-48}. Based on the results produced by Keller et al., it is estimated that 72.7% of TiO₂-NPs and
252 21.5% of ZnO-NPs will sediment in groundwater media⁴³. However, no studies were found on the potential
253 effect by the interaction between groundwater and soil which could provide a different removal efficiency
254 altogether. Nonetheless, it is assumed that sedimentation and sorption in soil is likely to act as another
255 barrier for the transport of NPs through the soil layers.

256 Due to the sandy soil in the two areas^{12,49}, the removal efficiency for both Berlin and Orange County is
257 estimated to be 50-71% for Ag-NPs in the unsaturated zone, 5-99% for TiO₂-NPs in unsaturated soil and
258 72% in saturated soil layers, and about 21.5% for ZnO-NPs in saturated soil layers^{43,45-47}.

259 **3.2.9 Water Treatment Plants**

260 A handful of studies have investigated the possible removal of NPs by conventional drinking water
261 treatment. Z. Li et al. observed that a sand filter retained about 40% of Ag-Citrate-NPs, about 25% of ZnO-
262 PVA-NPs, and 0% of Ag-PVPNPs⁵⁰. However, all the uncoated NPs examined, namely TiO₂-NPs, ZnO-NPs,
263 and CeO₂-NPs, were almost 100% retained by the sand filter. Moreover, the removal efficiency of each
264 investigated type of NP will most likely be constant once a given pore volume has been reached but at
265 various C/C₀-values (C = effluent concentration, C₀ = influent concentration)⁵⁰. In addition, Z. Li et al.
266 developed a model based on the experimental results for filter sand and ran simulations for two cases of
267 NP-influent: single spiked input and continuous flow input⁵⁰. The sand filter was observed to retain a large
268 amount of the NPs in the event of a single spiked input (influent concentration of NPs of 50-500 ppm) but if
269 a continuous flow (influent concentration of NPs of 5-50 ppm) was simulated, almost a 100% breakthrough
270 rate was observed. Z. Li et al. explains this phenomenon as being caused by steric repulsion of the coated
271 NPs⁵⁰.

272 Abbott Chalew et al. found the average removal efficiency of Ag-NPs by traditional water treatment plants
273 to be around 80-98%³⁵. For TiO₂-NPs, the average removal efficiency was found to be in the region of 92-
274 97% for the simulated traditional water treatment, while for ZnO-NPs it was found to be 1-52%. The
275 removal efficiencies for ZnO-NPs includes zinc ions, which indicate that the removal of ZnO-NPs is likely to
276 be greater than presented. By comparing the observed removal efficiencies by Z. Li et al.⁵⁰ and Abbott
277 Chalew et al.³⁵, aeration should remove 50% or more of the NPs in the influent to the water treatment
278 plant.

279 The six drinking water treatment plants in Berlin treat the extracted groundwater by conventional
280 processes such as sand filter, primary treatment, and secondary treatment. Li et al. found that less than
281 50% of surface coated NPs will be retained by sand filters⁵⁰. As many engineered NPs are surface coated,
282 this is likely to be the removal efficiency of sand filters in most cases. Abbott Chalew et al. found removal
283 efficiencies for conventional drinking water treatment processes of Ag-NPs, TiO₂-NPs, and ZnO-NPs to be
284 80-98%, 92-97%, and 1-52%, respectively³⁵. In Orange County, the extracted groundwater is treated by
285 disinfection which is covered in section 3.2.6.

286 ***3.3 Mass Flow Analysis***

287 ***3.3.1 Orange County***

288 Our results show that Ag-NPs are almost completely removed (99.97%) by the wastewater reclamation
289 system in Orange County primarily due to the effectiveness of the processes in the conventional
290 wastewater treatment plant and the disinfection stage in the Advanced Water Treatment Facility (figure 5).
291 The worst case removal scenario predicts that about 9% of TiO₂-NPs and 8% of ZnO-NPs will pass through
292 the treatment processes and may end up in the tap water.

293 Figure 6 depicts the concentrations after treatment by each treatment stage in Orange County. The
294 estimated worst case concentration of TiO₂-NPs in the influent to the WWTP is predicted to be 147 µg/L
295 while ZnO-NPs and Ag-NPs were predicted in concentrations of 280 ng/L and 37 ng/L, respectively.

296 ***3.3.2 Berlin***

297 The overall removal of NPs in Berlin was estimated based on the assumed removal efficiencies for the
298 treatment stages in Table 1. The results show that the Berlin reclamation sequence is most efficient in
299 retaining TiO₂-NPs. The system is also estimated to retain almost all of the Ag-NPs arriving at the WWTPs.

300 ZnO-NPs seem to be the most difficult NP of the three to remove (figure 7). Especially, the usage of
301 conventional wastewater treatment seems to be crucial in order to ensure high removal efficiency.

302 The estimated concentrations of the three NPs in the tap water to the consumers in Berlin indicate that
303 TiO₂-NPs can be found in the largest concentrations followed by Ag-NPs. The worst case scenario predicts
304 that all three NPs may end up in the tap water in concentrations between 0.25-13 µg/L (figure 7). In
305 addition, the system in Berlin utilizes surface water treatment plants (SWTPs) which treats the river water
306 in order to minimize the concentration of phosphorous among others in the local surface water. In these
307 plants flocculation, sedimentation, and filtration occurs¹². These processes are likely to contribute to the
308 overall NP removal efficiency of the system in Berlin. However, no information regarding the treated
309 volume could be found. The SWTPs are therefore not included in the mass flow analyses.

310 **4 Discussion**

311 **4.1 Evaluation of the Wastewater Reclamation Systems in Orange County** 312 **and Berlin**

313 The mass flow analyses in the previous sections of the wastewater reclamation systems in Orange County
314 and Berlin indicate that considering a worst case scenario, the advanced treatment currently in operation in
315 Orange County is likely to be more efficient towards Ag-NPs than the corresponding system in Berlin while
316 the opposite is the case for TiO₂-NPs and ZnO-NPs (Table 2)

317 The concentration of TiO₂-NPs in the tap water in the worst case scenario for Berlin is less than 10% of the
318 corresponding concentration in Orange County. On the other hand, the system in Orange County has a
319 worst case overall treatment efficiency of 99.97% for Ag-NPs, whereas Berlin is predicted to remove just
320 97% of the Ag-NPs. For ZnO-NPs, the found concentrations in the worst case scenario are almost equivalent
321 for both systems.

322 The two disinfection stages (sodium hypochlorite) in the wastewater reclamation system in Orange County
323 are the main cause for the higher worst case removal efficiency of Ag-NPs compared to the system in
324 Berlin. For Ag-NPs, the difference in worst case removal efficiencies for the two systems are mainly a 95%
325 removal efficiency of the two disinfection stages and 55% removal efficiency of the microfiltration
326 treatment in Orange County versus a 50% and 80% removal by the surface water and WTP respectively, in
327 the Berlin system. Therefore, size exclusion by microfiltration³⁵ and especially oxidative dissolution and
328 aggregation of Ag-NPs by disinfectants³⁸ seem to be a more effective barrier than ones provided by the
329 surface water (aggregation) and drinking water treatment plants (coagulation and bioadsorption) in Berlin
330 ^{35,42,43,50,51}.

331 The primary reason for the difference in the worst case removal efficiency of TiO₂-NPs by the two
332 wastewater reclamation systems are due to the processes in surface waters and water treatment plants in
333 Berlin. The found worst case removal efficiencies of TiO₂-NPs by the advanced treatment in Orange County
334 are down to the lower minimum removal efficiency by microfiltration. The different removal mechanisms
335 provide the system in Berlin with the advantage as no removal efficiency of TiO₂-NPs by disinfection,
336 reverse osmosis, or UV could be identified. The differences between microfiltration treatment used in
337 Orange County and the processes occurring in water treatment plants and rivers are predominantly due to
338 the removal mechanism in microfiltration being reliable on size exclusion³⁵ while the natural attraction of
339 TiO₂-NPs to the particles and matter in surface water (including mutual attraction between the TiO₂-NPs)
340 ^{42,43,51} as well as the coagulation³⁵ and bioadsorption⁵⁰ in conventional water treatment are observed to
341 more effective.

342 The difference between the found worst case removal efficiencies of ZnO-NPs for Berlin and Orange County
343 is the smallest compared to the corresponding for Ag-NPs and TiO₂-NPs. However, the WWRS in Berlin is
344 still estimated to be slightly more effective than the corresponding in Orange County due to slightly higher

345 overall estimated worst case removal efficiency of ZnO-NPs by surface waters and WTPs than the
346 corresponding by microfiltration.

347 **4.2 The known barriers against NPs**

348 The literature search results indicate that ultrafiltration provides the best removal efficiency of Ag-NPs (98-
349 100% removed) due to size exclusion³⁵. Moreover, the heteroaggregation occurring in treatment processes
350 in WWTPs and drinking water treatment plants are likely to provide a significant retention of Ag-NPs. The
351 dominant removal mechanism in WWTPs suggested by the identified studies is the natural attraction of Ag-
352 NPs to the total suspended solids in the medium and the bacteria in the activated sludge^{20,30}. Disinfection
353 and microfiltration are also likely to retain a large ratio of Ag-NPs. UV disinfection was effective
354 predominantly due to dissolution and aggregation of the Ag-NPs³⁸.

355 By similar comparison, ultrafiltration is likely to be the most efficient barrier towards TiO₂-NPs (96-100%
356 removed) due to size exclusion³⁵. However, the coagulation, sedimentation, and flocculation in the water
357 treatment result in a high removal efficiency of TiO₂-NPs (92-97%). Furthermore, high single removal
358 efficiency of TiO₂-NPs were documented for WWTPs, surface waters, soil, and microfiltration which highest
359 estimated removal efficiency of TiO₂-NPs were found to be 97%, 99.9%, 99%, and 100%, respectively. The
360 aggregation and biosorption of TiO₂-NPs in WWTPs were observed to be the primary removal mechanism
361^{24,27}. The removal efficiency of TiO₂-NPs in (sandy) soil was very much dependent on the pH-value of the soil
362 which could lead to almost negligible removal efficiency (5%). Moreover, if the soil has a high dissolved
363 organic carbon content a high removal efficiency (>95%) can be expected due to the composition of the
364 clay. Size exclusion of aggregated TiO₂-NPs due to the pore size of the microfiltration membrane was the
365 main reason for its high removal efficiency³⁵. In surface waters with acidic conditions and low flow rate (3.2
366 L/s), the sedimentation of TiO₂-NPs is found to be almost 100% regardless of surface coating. However, by
367 increasing the pH and flow rate, the TiO₂-NPs are more difficult to settle⁴².

368 The processes in the WWTP is likely to be the most efficient barrier against the breakthrough of ZnO-NPs.
369 Hou et al. found that about 70% of ZnO-NPs (no surface coating) are likely to rapidly settle in the primary
370 clarification tank and the remaining ZnO-NPs are suggested to be completely removed by processes in the
371 aeration and activated sludge treatment stage²⁸. The primary removal mechanism was found to be
372 biosorption. The rapid settling is also observed in surface water media where 8 hours of flocculation and 1
373 hour of sedimentation of ZnO-NPs is likely to result in 75% removal of ZnO-NPs⁵¹. However, a removal
374 efficiency of ZnO-NPs of 24% in river water media indicates that the flow rate are the primary parameter
375 for the removal of ZnO-NPs in surface water⁴³. Ultrafiltration and microfiltration can also exhibit a high
376 removal efficiency of ZnO-NPs (64% and 98%, respectively) but due to the dissolution of ZnO-NPs into zinc
377 ions, these barriers are also observed to exhibit very low removal efficiencies (17% and 4%, respectively)³⁵.
378 In general, the identified studies highlights aggregation – and especially heteroaggregation – and size
379 exclusion as essential removal mechanisms in waste water and water treatment^{20,52}.

380 **4.3 Knowledge gaps**

381 In our attempt to complete a mass flow analysis for potable water reclamation in Orange County and
382 Berlin, a marked lack of observations from several treatment stages and compartments is evident. This
383 prevents an accurate estimation of the fate of the investigated NPs. Of the three NPs in question, ZnO-NPs
384 have received least attention. Only single observations were found for several combinations of NP type and
385 treatment stage, for example ZnO-NPs in WWTP, and groundwater (Table 1). Ranges of removal efficiency
386 of Ag-NPs and TiO₂-NPs were found for wastewater treatment, microfiltration, and soil layers whereas only
387 single observations for the removal efficiency of Ag-NPs and TiO₂-NPs could be found for disinfection and
388 groundwater, respectively.

389 No studies which examined the removal efficiency of NPs by reverse osmosis were identified. The pore size
390 of the reverse osmosis membranes is below 0.1 nm and it is justified to assume that the reverse osmosis
391 membranes will have a removal efficiency at least equal to ultrafiltration membranes or better. But as

392 Bellona et al.⁴⁰ found, rejection at the membrane might not be as straightforward, because size exclusion
393 of compounds may not be the only parameter controlling rejection. In addition, primarily due to their
394 tendency to dissolve into zinc ions, ZnO-NPs have been observed to be difficult to remove by size
395 exclusion³⁵ and further studies are needed in order to determine the exact concentrations of ZnO-NPs
396 which are able to breakthrough the barriers in a given system. In the review of the identified studies, the
397 WWTPs were found to exhibit the highest removal efficiency of ZnO-NPs. Moreover, WWTPs are also likely
398 to exhibit a relative high removal efficiency of Ag-NPs and TiO₂-NPs which indicate that the biological
399 processes in the WWTPs at the current knowledge level appears as the most efficient NP barrier in
400 wastewater reclamation systems.

401 In general, further studies are needed in order to attain more knowledge of the fate of NPs in the various
402 treatment stages. Only the studies of the removal efficiency of the three NPs by WWTPs and surface waters
403 can be regarded as providing a minimum level of nuanced understanding of the fate and behavior of NPs.
404 This indicates that the primary focus from the research community has been on the release to and fate in
405 the environment and to lesser extent the risk of exposure to humans through drinking water. Therefore,
406 knowledge is lacking on the removal efficiency of more advanced treatment processes, with no
407 observations reported for reverse osmosis. Furthermore, the studies evaluated in this study have primarily
408 been conducted in laboratory settings or by modelling and simulation, which might provide a distorted
409 perception of the transformation of NPs in real environments which is also highlighted in the work by
410 Garner and Keller⁵².

411 Finally, an important knowledge gap lies in the estimation of the influent concentration. The influent
412 concentration of each NP in the mass flow analyses are based on results found by Tiede et al.⁸ and
413 Gottschalk et al.¹⁷ and are based primarily on the observed behavior of NPs in the various treatment
414 processes and previous results from similar studies as well as assumptions on the production volume and
415 WWTP influent concentration of NPs. Although, we do believe that these concentrations represent the best

416 known emission concentrations of NPs, it should be acknowledge that different estimations are available
417 and that influent and effluent estimations will of course depend on fundamental assumptions about, for
418 instance, production volumes⁵³.

419 **5 Conclusions**

420 Based on a mass flow analysis of possible nanoparticle fate and treatment in two typical potable reuse
421 systems, we have found that:

- 422 • Considering a worst case scenario, nanoparticles may reach the drinking water supply in
423 ng/L to µg/L concentrations after both advanced membrane based reclamation and simpler
424 conventional water treatment.
- 425 • There are marked knowledge gaps and actual removal efficiencies for several combinations
426 of nanoparticle and treatment stages are largely unknown.
- 427 • Observations reported so far support biological treatment processes as the most efficient
428 engineered barriers against nanoparticle in wastewater reclamation systems for potable
429 reuse.

430 Whether the estimated concentrations pose a risk for humans is yet to be determined.

431

432 **References**

433

- 434 1 M. Rygaard, P. J. Binning and H.-J. Albrechtsen, *J. Environ. Manage.*, 2011, **92**, 185–194.
- 435 2 D. Gerrity, B. Pecson, R. S. Trussell and R. R. Trussell, *J. Water Supply Res. Technol.*, 2013, **62**, 321.
- 436 3 H. L. Leverenz, G. Tchobanoglous and T. Asano, *J. Water Reuse Desalin.*, 2011, **1**, 2.
- 437 4 Nanodb.dk, 2014.
- 438 5 Nanotechproject.org, 2014.
- 439 6 European Commission, *Types and Uses of Nanomaterials, including Safety Aspects*, 2012.
- 440 7 F. Gottschalk, R. W. Scholz and B. Nowack, *Environ. Model. Softw.*, 2010, **25**, 320–332.
- 441 8 K. Tiede, P. K. Westerhoff, S. Foss Hansen, G. . Fern, R. J. Aitken, Q. Chaudhry and A. B. A. Boxall,
442 *Review of the risks posed to drinking water by man-made nanoparticles*, 2011.
- 443 9 MWDQC, 2010.
- 444 10 GWRS, *Technical Brochure*, 2013.
- 445 11 Veolia Water, *Information Sheets Regarding Water Recycling*, 2005.
- 446 12 Berliner Wasserbetriebe, *Water for Berlin*, 2013.
- 447 13 G. Massmann, J. Sultenfuss, U. Dunnbier, A. Knappe, T. Taute and A. Pekdeger, *Hydrol. Process.*,
448 2008, **22**, 788–801.
- 449 14 T. Heberer, *J. Hydrol.*, 2002, 266, 175–189.
- 450 15 P. Weyrauch, A. Matzinger, E. Pawlowsky-Reusing, S. Plume, D. von Seggern, B. Heinzmann, K.
451 Schroeder and P. Rouault, *Water Res.*, 2010, **44**, 4451–62.
- 452 16 P. H. Brunner and H. Rechberger, *Practical handbook of material flow analysis : Advanced methods*
453 *in resource and waste management*, Lewis Publishers, 2004.
- 454 17 F. Gottschalk, T. Sonderer, R. W. Scholz and B. Nowack, 2009, **43**, 9216–9222.
- 455 18 A. B. A. Boxall, Q. Chaudhry, C. Sinclair, A. Jones, R. J. Aitken, B. Jefferson and C. Watts, *Current and*
456 *Future Predicted Environmental Exposure to Engineered Nanoparticles*, 2007.
- 457 19 N. C. Mueller and B. Nowack, *Environ. Sci. Technol.*, 2008, **42**, 4447–53.

- 458 20 R. Kaegi, A. Voegelin, C. Ort, B. Sinnet, B. Thalmann, J. Krismer, H. Hagendorfer, M. Elumelu and E.
459 Mueller, *Water Res.*, 2013, **47**, 3866–77.
- 460 21 E. Jeong, S. R. Chae, S. T. Kang and H. S. Shin, *Water Sci. Technol.*, 2012, **65**, 1298–303.
- 461 22 R. Kaegi, A. Voegelin, B. Sinnet, S. Zuleeg, H. Hagendorfer, M. Burkhardt and H. Siegrist, *Environ. Sci.*
462 *Technol.*, 2011, **45**, 3902–8.
- 463 23 L. Li, G. Hartmann, M. Döblinger and M. Schuster, 2013.
- 464 24 Y. Wang, P. Westerhoff and K. D. Hristovski, *J. Hazard. Mater.*, 2012, **201-202**, 16–22.
- 465 25 N. Musee, J. N. Zvimba, L. M. Schaefer, N. Nota, L. M. Sikhwivhilu and M. Thwala, *J. Environ. Sci.*
466 *Health. A. Tox. Hazard. Subst. Environ. Eng.*, 2014, **49**, 59–66.
- 467 26 A. C. Johnson, M. J. Bowes, A. Crossley, H. P. Jarvie, K. Jurkschat, M. D. Jürgens, A. J. Lawlor, B. Park,
468 P. Rowland, D. Spurgeon, C. Svendsen, I. P. Thompson, R. J. Barnes, R. J. Williams and N. Xu, *Sci.*
469 *Total Environ.*, 2011, **409**, 2503–10.
- 470 27 M. a Kiser, H. Ryu, H. Jang, K. Hristovski and P. Westerhoff, *Water Res.*, 2010, **44**, 4105–14.
- 471 28 L. Hou, J. Xia, K. Li, J. Chen, X. Wu and X. Li, *Water Sci. Technol.*, 2013, **67**, 254–60.
- 472 29 L. K. Limbach, R. Bereiter, E. Müller, R. Krebs, R. Galli and W. J. Stark, *Environ. Sci. Technol.*, 2008, **42**,
473 5828–33.
- 474 30 S. P. Dhas, P. J. Shiny, S. Khan, A. Mukherjee and N. Chandrasekaran, *J. Basic Microbiol.*, 2013, 1–12.
- 475 31 S. Eduok, B. Martin, R. Villa, a Nocker, B. Jefferson and F. Coulon, *Ecotoxicol. Environ. Saf.*, 2013, **95**,
476 1–9.
- 477 32 G. Liu, D. Wang, J. Wang and C. Mendoza, *Sci. Total Environ.*, 2011, **409**, 2852–7.
- 478 33 X. Sun, Z. Sheng and Y. Liu, *Sci. Total Environ.*, 2013, **443**, 828–35.
- 479 34 X. Zheng, R. Wu and Y. Chen, *Environ. Sci. Technol.*, 2011, **45**, 2826–32.
- 480 35 T. E. Abbott Chalew, G. S. Ajmani, H. Huang and K. J. Schwab, *Environ. Health Perspect.*, 2013, **121**,
481 1161–6.
- 482 36 D. a Ladner, M. Steele, a Weir, K. Hristovski and P. Westerhoff, *J. Hazard. Mater.*, 2012, **211-212**,
483 288–95.
- 484 37 R. W. Baker, *Membrane Technology and Applications*, John Wiley & Sons, Ltd, Chichester, UK, 2012.
- 485 38 Z. Yuan, Y. Chen, T. Li and C.-P. Yu, *Chemosphere*, 2013, **93**, 619–25.
- 486 39 City of Huntington Beach, *2010 Urban Water Management Plan*, 2011.

- 487 40 C. Bellona, J. E. Drewes, P. Xu and G. Amy, *Water Res.*, 2004, **38**, 2795–809.
- 488 41 P. Xu, J. E. Drewes, T.-U. Kim, C. Bellona and G. Amy, *J. Memb. Sci.*, 2006, **279**, 165–175.
- 489 42 N. Ticiana Boncagni, J. M. Otaegui, E. Warner, T. Curran, J. Ren and M. Marta Fidalgo de Cortalezzi,
490 2009, 7699–7705.
- 491 43 A. A. Keller, H. Wang, D. Zhou, H. S. Lenihan, G. Cherr, B. J. Cardinale, R. Miller and Z. Ji, *Environ. Sci.*
492 *Technol.*, 2010, **44**, 1962–1967.
- 493 44 MWDSC, *Final Groundwater Assessment Study*, 2007.
- 494 45 O. Sagee, I. Dror and B. Berkowitz, *Chemosphere*, 2012, **88**, 670–5.
- 495 46 N. Solovitch, J. Labille, J. Rose, P. Chaurand, D. Borschneck, M. R. Wiesner and J.-Y. Bottero, *Environ.*
496 *Sci. Technol.*, 2010, **44**, 4897–902.
- 497 47 J. Fang, X. Shan, B. Wen, J. Lin and G. Owens, *Environ. Pollut.*, 2009, **157**, 1101–9.
- 498 48 S. Bae, Y. S. Hwang, Y.-J. Lee and S.-K. Lee, *Environ. Health Toxicol.*, 2013, **28**, e2013006.
- 499 49 OCWD, 2010.
- 500 50 Z. Li, A. Aly Hassan, E. Sahle-Demessie and G. a Sorial, *Water Res.*, 2013, **47**, 6457–66.
- 501 51 Y. Zhang, Y. Chen, P. Westerhoff, K. Hristovski and J. C. Crittenden, *Water Res.*, 2008, **42**, 2204–12.
- 502 52 K. L. Garner and A. a. Keller, *J. Nanoparticle Res.*, 2014, **16**, 2503.
- 503 53 A. a. Keller, S. McFerran, A. Lazareva and S. Suh, *J. Nanoparticle Res.*, 2013, **15**, 1692.
- 504 54 G. Tchobanoglous, H. Leverenz, M. H. Nellor and J. Crook, *Direct potable reuse. A path forward*,
505 2011.
- 506
- 507

508 **Figure text**

509 Figure 1. Number of products with registered location of nanoparticles (nanodb.dk).

510 Figure 2. Number of registered nanoparticles grouped by product category (nanodb.dk).

511 Figure 3. Conceptual diagram of the wastewater reclamation systems in A Orange County and B) Berlin

512 ^{1,2,54}.

513 Figure 4. Number of published studies dealing with NP fate in water treatment processes grouped by year.

514 Retrieved from the International Council on Nano Technology ICON database and Web of Science. 'Other'

515 refers to publications dealing with NPs different from Ag-, TiO₂-, and Zn-NPs.

516 Figure 5. Estimated accumulated percentage of removed NPs after each treatment stage in the Orange

517 County wastewater reclamation system for the removal scenarios: Minimum and maximum. Where no

518 removal efficiency has been found in the literature it is assumed that 0% was removed for the minimum

519 scenario and 100% removed for the maximum scenario. It is assumed that no NPs are removed in the

520 sewers.

521 Figure 6. Concentration of NPs (µg/L) after each treatment stage in the Orange County wastewater

522 reclamation system for the removal scenarios: Minimum, and maximum. The estimated concentrations of

523 Ag-NP and TiO₂ in the influent to the WWTP are based on the study by Tiede et al. ⁸ while the

524 corresponding concentration of ZnO-NPs is based on the study by Gottschalk et al. ¹⁷.

525 Figure 7. Estimated accumulated percentage of removed NPs after each treatment stage in the Berlin

526 wastewater reclamation system for the minimum and maximum removal scenarios. Where no removal

527 efficiency has been found in the literature it is assumed that 0% was removed for the minimum scenario

528 and 100% removed for the maximum scenario. It is assumed that no NPs are removed in the sewers. WTP:

529 Conventional drinking water treatment.

530 Figure 8. Concentration of NPs ($\mu\text{g/L}$) after each treatment stage in the Berlin wastewater reclamation
531 system for the removal scenarios: Minimum, and maximum. The estimated concentrations of Ag-NP and
532 TiO_2 in the influent to the WWTP are based on the study by Tiede et al.⁸ while the corresponding
533 concentration of ZnO-NPs is based on the study by Gottschalk et al.¹⁷. WTP: Conventional drinking water
534 treatment.

535 ***Table text***

536 Table 1. Overview of removal efficiencies for Ag-NPs, TiO_2 -NPs, and ZnO-NPs in water treatment reported
537 from field studies (field), laboratory experiments (lab), and computer simulations (sim).

538 Table 2. Summary of estimated removal efficiencies and worst case concentrations of each NP by the
539 wastewater reclamation system in Orange County and Berlin.

540

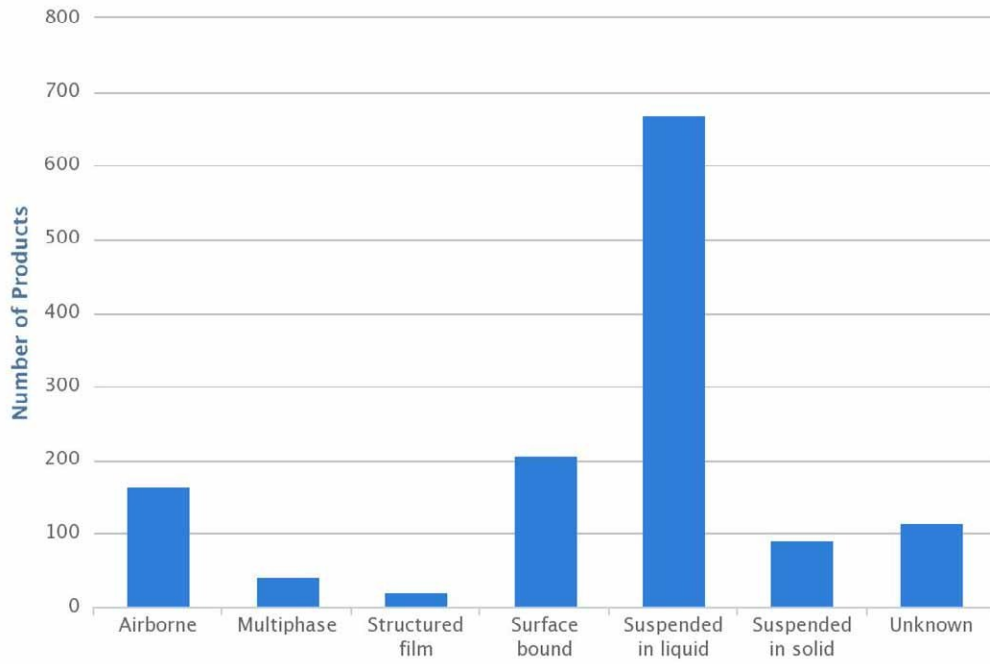


Figure 1. Number of products with registered location of nanoparticles (nanodb.dk).

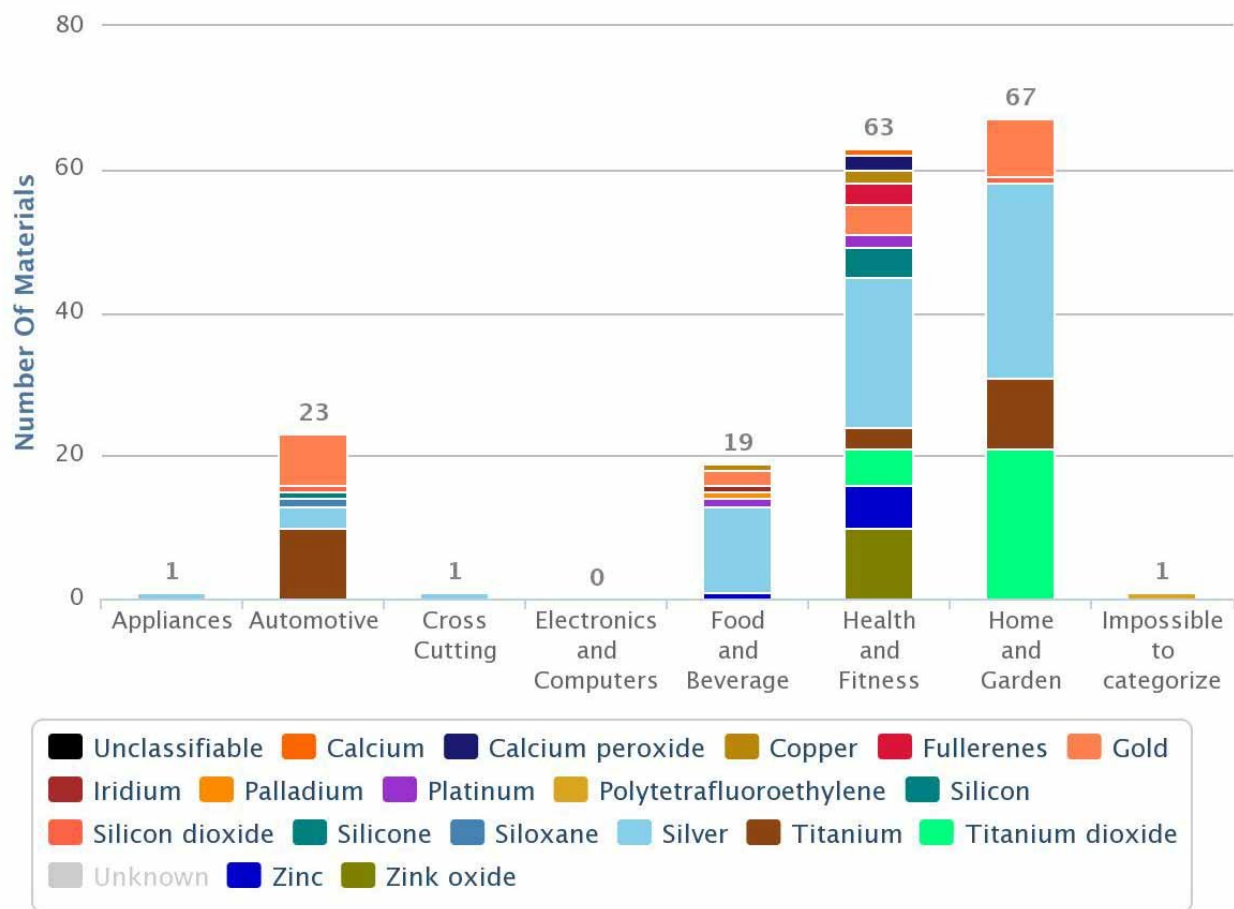


Figure 2. Number of registered nanoparticles grouped by product category (nanodb.dk).

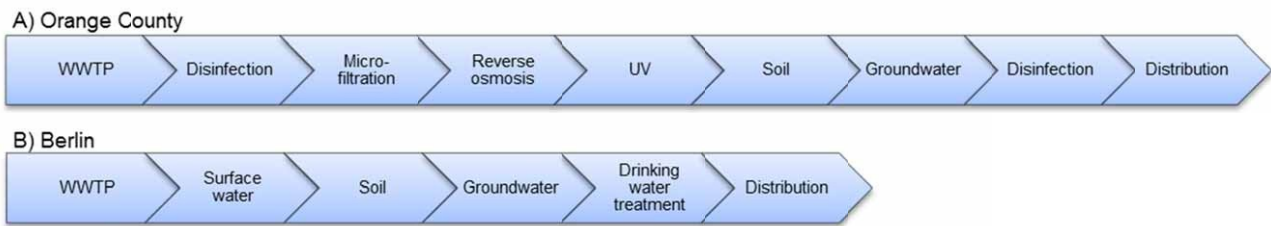


Figure 3. Conceptual diagram of the wastewater reclamation systems in A Orange County and B) Berlin (Gerrity et al., 2013; Rygaard et al., 2011; Tchobanoglous et al., 2011).

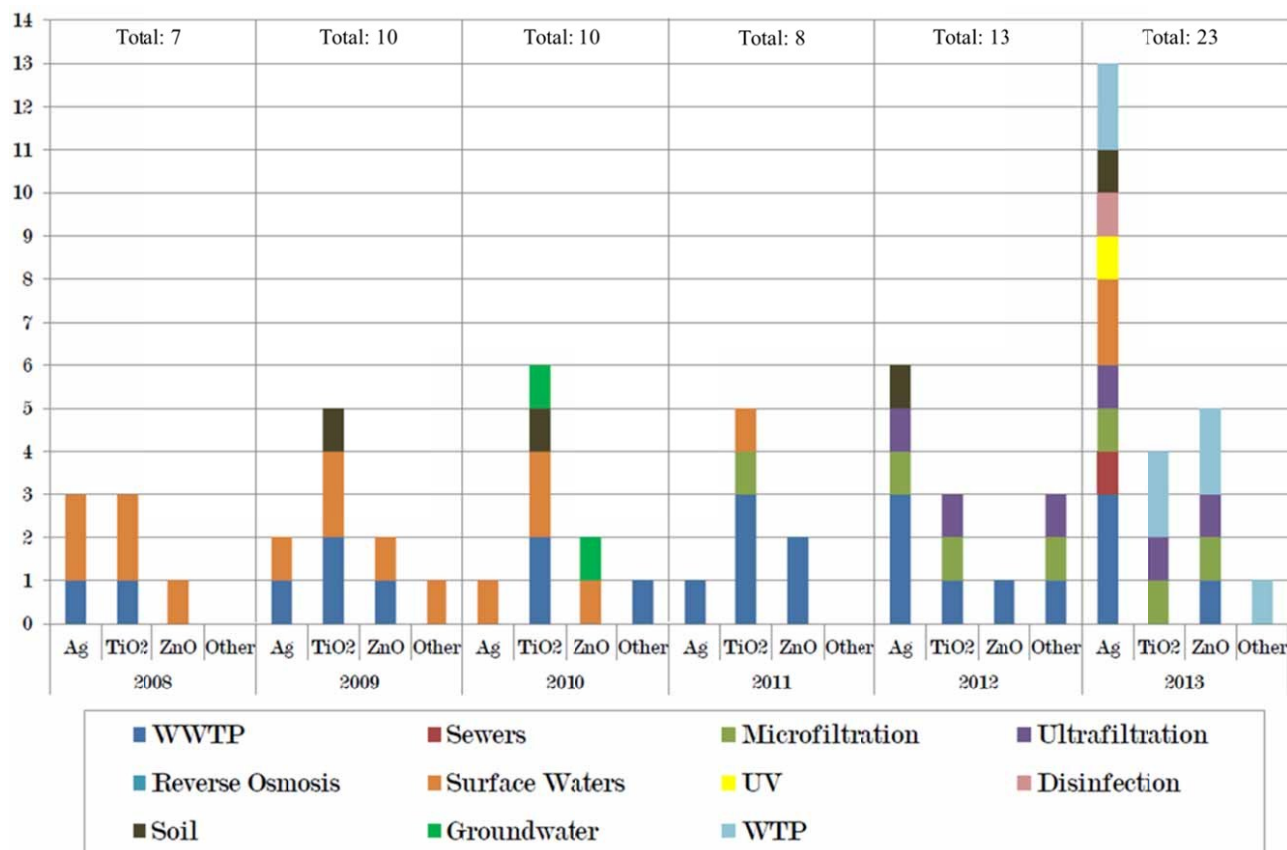


Figure 4. Number of published studies dealing with NP fate in water treatment processes grouped by year. Retrieved from the International Council on Nano Technology ICON database and Web of Science. 'Other' refers to publications dealing with NPs different from Ag-, TiO₂-, and Zn-NPs.

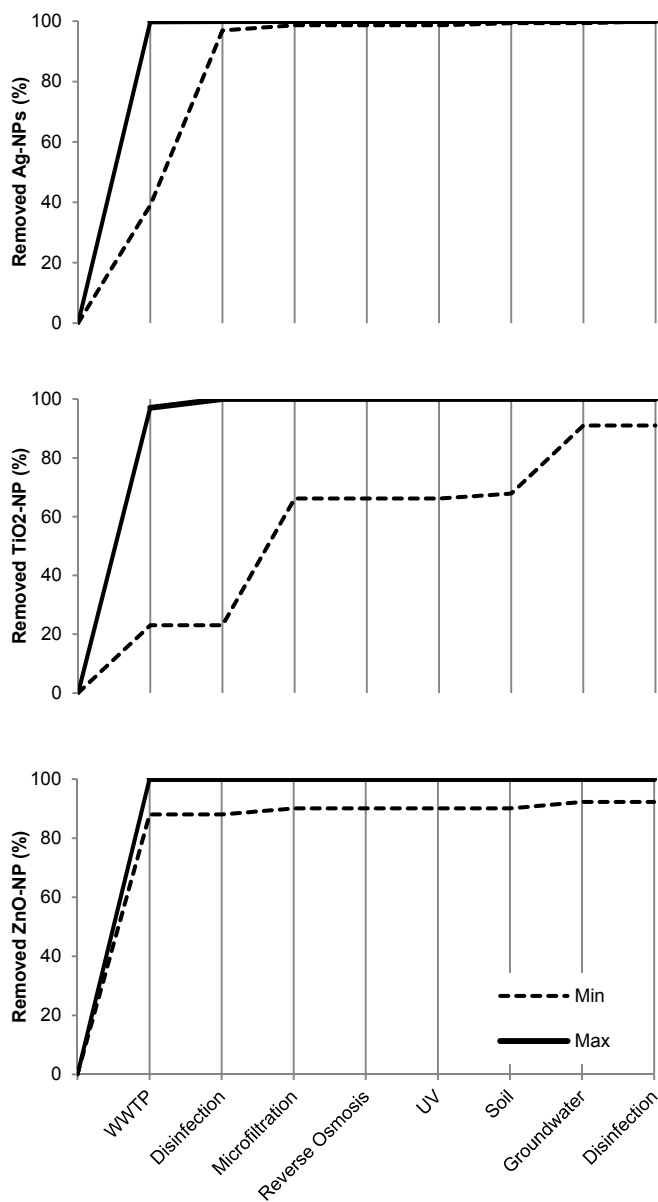


Figure 5. Estimated accumulated percentage of removed NPs after each treatment stage in the Orange County wastewater reclamation system for the removal scenarios: Minimum and maximum. Where no removal efficiency has been found in the literature it is assumed that 0% was removed for the minimum scenario and 100% removed for the maximum scenario. It is assumed that no NPs are removed in the sewers.

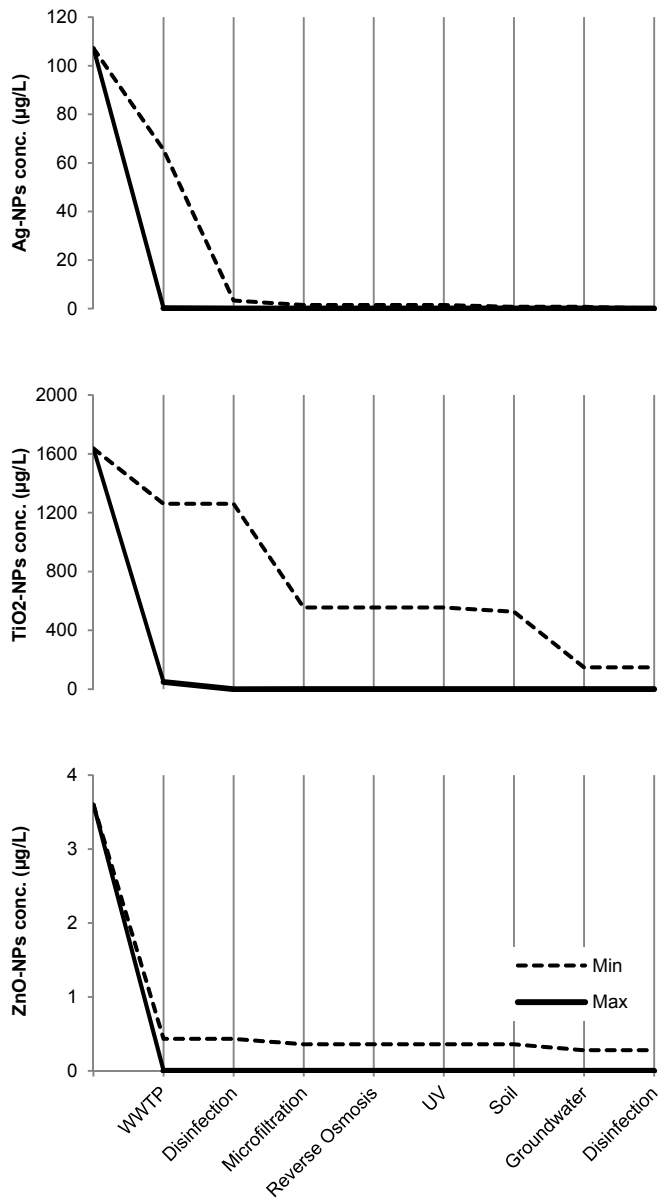


Figure 6. Concentration of NPs ($\mu\text{g/L}$) after each treatment stage in the Orange County wastewater reclamation system for the removal scenarios: Minimum, and maximum. The estimated concentrations of Ag-NP and TiO₂ in the influent to the WWTP are based on the study by Tiede et al. (2011) while the corresponding concentration of ZnO-NPs is based on the study by Gottschalk et al. (2009).

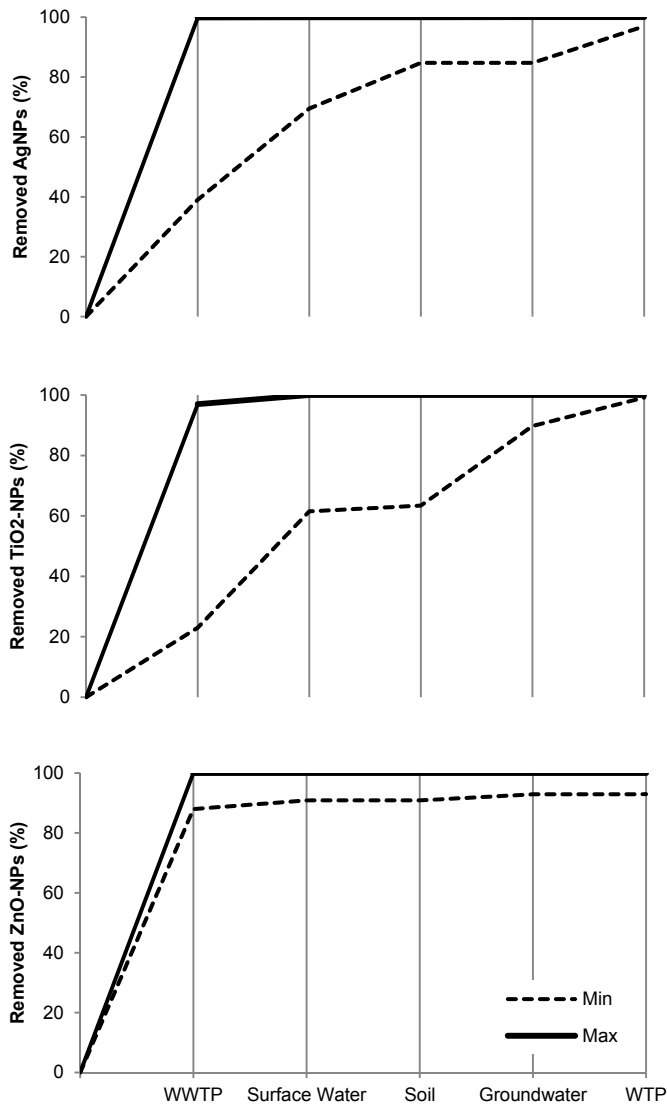


Figure 7. Estimated accumulated percentage of removed NPs after each treatment stage in the Berlin wastewater reclamation system for the minimum and maximum removal scenarios. Where no removal efficiency has been found in the literature it is assumed that 0% was removed for the minimum scenario and 100% removed for the maximum scenario. It is assumed that no NPs are removed in the sewers. WTP: Conventional drinking water treatment.

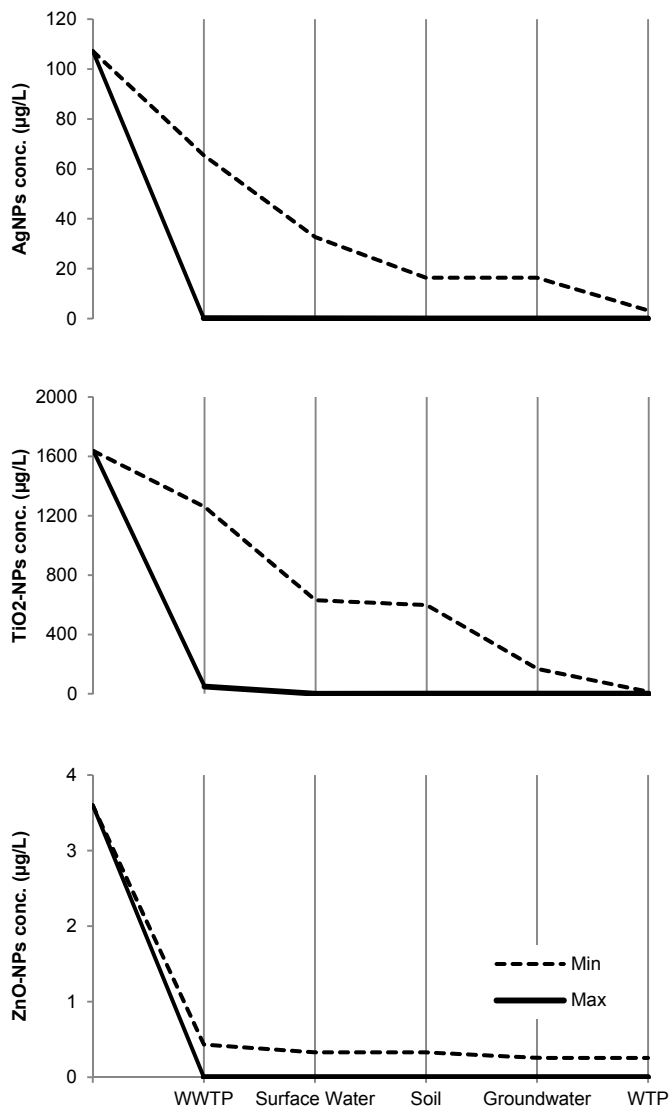


Figure 8. Concentration of NPs ($\mu\text{g/L}$) after each treatment stage in the Berlin wastewater reclamation system for the removal scenarios: Minimum, and maximum. The estimated concentrations of Ag-NP and TiO_2 in the influent to the WWTP are based on the study by Tiede et al. (2011) while the corresponding concentration of ZnO-NPs is based on the study by Gottschalk et al. (2009). WTP: Conventional drinking water treatment.

Table 1. Overview of removal efficiencies for Ag-NPs, TiO₂-NPs, and ZnO-NPs in water treatment reported from field studies (field), laboratory experiments (lab), and computer simulations (sim).

| Stage | Reference | Comments | Ag | TiO ₂ | ZnO | Type of study | Considered in the mass flow analysis | |
|-----------------------------|------------------------------|---|-----------|------------------|-------|----------------|--------------------------------------|-----|
| Sewers | (Kaegi et al., 2013) | The Ag-NPs are observed to be stabilized by adsorptions to sulfides and suspended solids. | 0 | - | - | Lab.+ field | Yes | |
| Wastewater Treatment Plants | (Kaegi et al., 2013) | Overall, sedimentation, aggregation and adsorption are identified as the primary mechanisms for the removal of NPs. Increasing concentration of Total Suspended Solids (TSS) is observed to increase the removal of NPs (M. a Kiser et al., 2010; Wang et al., 2012). In addition, Li et al (L. Li et al., 2013) found the removal efficiency of mechanical treatment and biological treatment to be 35% and 72%, respectively. | 98.9-99.9 | - | - | Lab.+ field | Yes | |
| | (Jeong et al., 2012) | | 70-90 | - | - | Lab. | Yes | |
| | (L. Li et al., 2013) | | 95 | - | - | Lab. | Yes | |
| | (Wang et al., 2012) | | 39-59 | 65-98 | - | Lab. | Yes | |
| | (M. a Kiser et al., 2010) | | 84-92 | - | 23-88 | - | Lab. | Yes |
| | (Mueller and Nowack, 2008) | | 81-92* | 81-92* | - | Sim. | Yes | |
| | (Gottschalk et al., 2009) | | ~76* | ~76* | ~88* | Sim. | Yes | |
| | (Gottschalk et al., 2010) | | - | ~86.6* | - | Sim. | Yes | |
| (Johnson et al., 2011) | - | ~89.5 | - | Field | Yes | | | |
| (Hou et al., 2013) | - | - | ~100 | Lab. | Yes | | | |
| Microfiltration | (Abbott Chalew et al., 2013) | Abbott Chalew et al. reports for pH 7-8 and Ladner et al. reports for pH 8.2-9.6. | 55-99 | 56-100 | 17-64 | Lab. | Yes | |
| | (Ladner et al., 2012) | | 0-10 | 0-10 | - | Lab. | No ⁽¹⁾ | |
| Ultrafiltration | (Abbott Chalew et al., 2013) | Abbott Chalew et al. reports for pH 7-8 and Ladner et al. reports for pH 8.2-9.6. | 98-100 | 96-100 | 4-98 | Lab. | Yes | |
| | (Ladner et al., 2012) | | 60-90 | 95-100 | - | Lab. | No ⁽¹⁾ | |
| Reverse Osmosis | N/A | It is expected that that reverse osmosis should have removal efficiency better than ultrafiltration (Abbott Chalew et al., 2013; Ganzleben et al., 2011) actual removal efficiency has not been investigated. | N/A | N/A | N/A | N/A | | |
| UV | (Yuan et al., 2013) | Oxidative dissolution was found to be the dominant reaction when exposing Ag-NPs to disinfectants. In addition, the level of pH, sodium nitrate, humic acid and the type of disinfectant is important for predicting the removal of NPs by disinfection. | 17-67* | - | - | Lab. | Yes | |

| Stage | Reference | Comments | Ag | TiO ₂ | ZnO | Type of study | Considered in the mass flow analysis |
|-------------------------------|---------------------------------|---|--------|------------------|-------|---------------|--------------------------------------|
| <i>Disinfection</i> | (Yuan et al., 2013) | | 95* | - | - | Lab. | Yes |
| <i>Surface Waters</i> | (Gottschalk et al., 2009) | The dominant removal mechanisms in surface waters seem to be low pH and flow rate as well as increased flocculation, sedimentation, aggregation, and electrostatic attraction. | ~50 | ~99 | ~70 | Sim. | Yes |
| | (Gottschalk et al., 2010) | | - | ~50 | - | Sim. | Yes |
| | (Ticiana Boncagni et al., 2009) | | - | ~100 | - | Lab. | Yes |
| | (Zhang et al., 2008) | | - | 53-75* | ~75* | Lab. | Yes |
| <i>Soil</i> | (Keller et al., 2010) | In general, the studies observed that low grain sizes, low concentration of humic acid, low flow conditions, low pH-value, and high ionic strength of the soil promotes electrostatic attraction and mechanical straining of NPs. | - | ~77* | ~24* | Lab. | Yes |
| | (Sagee et al., 2012) | | 22-80* | - | - | Lab. | Yes |
| | (Fang et al., 2009) | | - | 17-99.8 | - | Lab. | Yes |
| <i>Groundwater</i> | (Solovitch et al., 2010) | Increasing ionic strength and concentration of Total Organic Carbon (TOC) promote retention of NPs. | - | 5-99 | - | Lab. | Yes |
| | (Keller et al., 2010) | | - | 72* | 21,5* | Lab. | Yes |
| <i>Water Treatment Plants</i> | (Abbott Chalew et al., 2013) | Sand filtration is observed to remove 100% of uncoated NPs while below 40% of coated NP (depending on type and surface coating) can be removed by sand filters. Moreover, sand filtration seems to be susceptible towards a continuous influent seems resulting in a larger breakthrough of NPs than in a peak flow (Z. Li et al., 2013). | 80-98 | 92-97 | 1-52 | Lab. | Yes ⁽²⁾ |

*The removal efficiencies are read from graphs, tables or data. ⁽¹⁾ Not considered since the microfiltration influent and effluent in the ATWF of Orange County has pH 7.3 and 7.5 (GWRS, 2013). ⁽²⁾ The conventional water treatment simulated by Abbott Chalew et al. (Abbott Chalew et al., 2013) is based upon coagulation and the removal efficiencies is therefore not necessarily the correct removal efficiencies for the drinking water treatment plants in Berlin.

Table 2. Summary of estimated removal efficiencies and worst case concentrations of each NP by the wastewater reclamation system in Orange County and Berlin.

| | | Ag | TiO₂ | ZnO |
|--|---------------|-----------|------------------------|------------|
| Removal Efficiency Range (%) | Orange County | 99.97-100 | 91-100 | 92-100 |
| | Berlin | 97-100 | 99.2-100 | 93-100 |
| Worst Case Concentrations in Tap Water (µg/L) | Orange County | 0.04 | 147 | 0.28 |
| | Berlin | 3.3 | 13 | 0.25 |