# Environmental Science Processes & Impacts

Accepted Manuscript



This is an *Accepted Manuscript*, which has been through the Royal Society of Chemistry peer review process and has been accepted for publication.

Accepted Manuscripts are published online shortly after acceptance, before technical editing, formatting and proof reading. Using this free service, authors can make their results available to the community, in citable form, before we publish the edited article. We will replace this Accepted Manuscript with the edited and formatted Advance Article as soon as it is available.

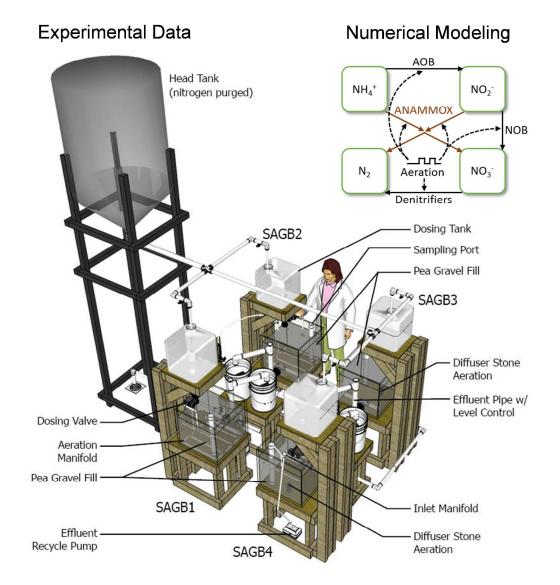
You can find more information about *Accepted Manuscripts* in the **Information for Authors**.

Please note that technical editing may introduce minor changes to the text and/or graphics, which may alter content. The journal's standard <u>Terms & Conditions</u> and the <u>Ethical guidelines</u> still apply. In no event shall the Royal Society of Chemistry be held responsible for any errors or omissions in this *Accepted Manuscript* or any consequences arising from the use of any information it contains.



rsc.li/process-impacts

Smart-aerated submerged attached growth bioreactors perform partial nitritation ANAMMOX at 20°C.



# 1 Environmental Impact

2 Limited infrastructure improvement budgets for small, rural communities have left countless 3 streams and rivers under threat by discharges of inadequately treated domestic wastewater. Acute 4 ammonia toxicity can kill organisms at the local scale and chronic nutrient releases contribute to 5 local, regional and coastal hypoxia attributable to undesirable, and often toxic, algal blooms. 6 Therefore, to protect the environment and to better ensure the long-term viability of rural 7 communities, relatively inexpensive, easy to maintain and increasingly energy efficient 8 wastewater treatment systems with nutrient removal capabilities are needed. This study 9 investigated how submerged attached growth bioreactors equipped with "smart", pH-controlled 10 aeration could remove nitrogen from domestic wastewater via the partial nitritation ANAMMOX

11 process at 20°C.

# Partial Nitritation ANAMMOX in Submerged Attached Growth Bioreactors with Smart Aeration at 20°C

James M. Shannon Lee W. Hauser Xikun Liu Gene F. Parkin Timothy E. Mattes Craig L. Just\*

Department of Civil and Environmental Engineering University of Iowa Iowa City, IA 52242 USA

\*corresponding author

# 1 Introduction

Effective and affordable treatment of municipal wastewater flows of less than  $3.8 \times 10^3 \text{ m}^3 \text{ d}^{-1}$  (1 2 3 million gallons per day, MGD) poses significant design challenges for small communities, 4 especially in cooler climates. Increasingly stringent standards and guidelines for discharges of ammonium  $(NH_4^+)$  and total nitrogen (TN) have driven the exploration of treatment systems that 5 6 maximize TN removal while minimizing aeration requirements. Submerged attached growth 7 bioreactors (SAGBs) have been successfully utilized for smaller wastewater flows (< 1 MGD) 8 due to relative ease of operation and robustness. Underground placement of SAGBs also facilitates cold–climate treatment and improves aesthetics.<sup>1</sup> SAGBs can be continuously aerated 9 10 to maximize treatment of carbonaceous biological oxygen demand (cBOD) and total Kjeldahl nitrogen (TKN) with greater than 95% cBOD and 90% and TKN removal.<sup>2</sup> A planted, vertical-11 flow SAGB with continuous aeration achieved a loading-rate dependent NH<sub>4</sub><sup>+</sup> removal of 65-12 87%.<sup>3</sup> A similar system with continuous aeration removed 97%, 99% and 29% chemical oxygen 13 demand (COD), NH4<sup>+</sup> and TN, respectively.<sup>4</sup> Additionally, planted horizontal-flow SAGBs 14 removed up to 96.3% TN in summer (Montreal, Canada) and nearly 60% in a 5°C winter, 15 greenhouse temperature.<sup>5</sup> A similar system removed 4–42% TKN in Montreal summer and 13– 16 29% TKN in winter.<sup>6</sup> 17 18 Other SAGBs utilize intermittent aeration to facilitate nitrification and denitrification which

19 reduces aeration costs as compared to constantly aerated systems. Our previous work

20 demonstrated that intermittently aerated, horizontal-flow SAGBs dosed with municipal primary

effluent removed 84–93% cBOD and 65–95% TN in planted and unplanted cells.<sup>7</sup> A planted,

intermittently aerated vertical flow SAGB removed 54–78% of  $NH_4^+$  and 29–57% of TN as a

function of hydraulic loading.<sup>3</sup> A similar system achieved 96% COD, 99% NH<sub>4</sub><sup>+</sup> and 90% TN 23 removal<sup>8</sup> and another achieved 96% COD, 97% NH<sub>4</sub><sup>+</sup>, and 74% TN removal.<sup>4</sup> 24 The Amphidrome<sup>®</sup> SAGB treats domestic wastewater flows of up to 0.5 MGD to less than 30 25 mg/L cBOD and less than 10 mg/L TN.<sup>9,10</sup> With methanol addition, a similar system removed 26 over 94% cBOD and 52–72% TN from municipal wastewater.<sup>11</sup> Another study, performing 27 28 sidestream treatment of dewatering centrate, achieved an average TN removal of 85% when methanol was added.<sup>12</sup> A similar SAGB with limited aeration favored nitrite (NO<sub>2</sub>) formation 29 from  $NH_4^+$  while minimizing nitrate (NO<sub>3</sub><sup>-</sup>) production and with the addition of methanol and 30 sodium bicarbonate. 25% of the TN was removed.<sup>13</sup> 31 Partial nitritation (i.e. the fractional conversion of available  $NH_4^+$  to  $NO_2^-$ ) coupled with 32 33 anaerobic ammonium oxidation (ANAMMOX) is a relatively new wastewater treatment approach that can treat TN while decreasing aeration needs.<sup>14, 15</sup> Partial nitritation requires 34 precision dissolved oxygen (DO) control (typically < 0.5 mg/L) to select for ammonium 35 oxidizing archaea/bacteria (AOB) activity while limiting nitrite oxidizing bacteria (NOB). Under 36 these conditions,  $NH_4^+$  is oxidized to  $NO_2^-$  as alkalinity is consumed and pH (typical range, 6.5– 37 8) is driven lower<sup>15</sup>: 38

$$39 \qquad \text{NH}_4^+ + 1.38 \text{ O}_2 + 1.98 \text{ HCO}_3^- \rightarrow 0.018 \text{ C}_5 \text{H}_7 \text{NO}_2 + 0.98 \text{ NO}_2^- + 1.04 \text{ H}_2 \text{O} + 1.89 \text{ H}_2 \text{CO}_3 \tag{1}$$

40 With a desired level of  $NH_4^+$  oxidation reached, aeration is turned off and ANAMMOX activity 41 commences as DO tends toward zero. ANAMMOX bacteria recover alkalinity as  $NH_4^+$  and  $NO_2^-$ 42 are converted to nitrogen gas (N<sub>2</sub>) and  $NO_3^-$  as described by Strous<sup>14</sup>:

43 
$$NH_4^+ + 1.32 NO_2^- + 0.066 HCO_3^- + 0.13 H^+ \rightarrow 1.02 N_2 + 0.26 NO_3^- + 0.066 CH_2O_0 N_{0.15} + 2.03 H_2O$$
 (2)

47 coefficients for  $HCO_3^-$ ,  $H_2O$ , and biomass yields:

44

45

46

48 
$$NH_4^+ + 1.32 NO_2^- + 0.07 HCO_3^- + 0.13 H^+ \rightarrow 1.02 N_2 + 0.26 NO_3^- + 0.014 C_5 H_7 NO_2 + 2.05 H_2 O$$
 (3)

- 49 Combining Equations 1 and 3 reveals the net stoichiometry for the complete partial nitritation
- 50 ANAMMOX process that occurs over two, rate independent steps:
- $\begin{array}{ll} 51 & 2 \ \mathrm{NH_4^+} + 0.34 \ \mathrm{NO_2^-} + 1.38 \ \mathrm{O_2} + 2.05 \ \mathrm{HCO_3^-} + 0.13 \ \mathrm{H^+} \rightarrow \\ 52 & 1.02 \ \mathrm{N_2} + 0.26 \ \mathrm{NO_3^-} + 0.032 \ \mathrm{C_5H_7NO_2} + 3.09 \ \mathrm{H_2O} + 1.89 \ \mathrm{H_2CO_3} \end{array}$
- Converting N-containing species in Equation 4 to "as N" equivalents and normalizing to NH<sub>4</sub>N<sup>+</sup> yields the nitrogen balance for the partial nitritation ANAMMOX process:

55 
$$NH_4 - N^+ + 0.063 NO_2 - N^- \rightarrow 0.33 N_2 - N + 0.037 NO_3 - N^- + 0.0026 C_5 H_7 NO_2 - N$$
 (5)

56 Similar to the nitrification-denitrification process, the consumption and subsequent recovery of 57 alkalinity across the two stage partial nitritation ANAMMOX cycle results in a characteristic 58 "saw tooth" pH pattern over time. This pH signal can serve as an aeration control parameter 59 toward the creation of "smart-aerated" systems. The most common current application for 60 smart–aerated, partial nitritation ANAMMOX is for large treatment systems without attached growth media that are operated at 25–40°C.<sup>16-20</sup> One planted SAGB with controlled DO of 0.2– 61 0.6 mg/L achieved 87.2% cBOD removal and 68.7–85.1% TN removal.<sup>21</sup> A SAGB using 62 63 hydrophilic acryl fiber netting as the growth medium treated high  $NH_4^+$  wastewater via partial nitritation ANAMMOX at 35°C with an aerobic zone at 2–3 mg/L DO for AOB activity and an 64 anoxic zone for ANAMMOX achieved 60–80% NH<sub>4</sub><sup>+</sup> removal.<sup>22</sup> 65

66	Partial nitritation ANAMMOX theoretically requires 0.7 moles of $O_2$ to yield 0.5 mole of $N_2$
67	compared to 1.8 moles required for nitrification-denitrification and 1.3 moles required for
68	nitritation-denitritation (Figure 1). <sup>23</sup> Smart-aerated SAGBs operating in partial nitritation
69	ANAMMOX mode hold promise to remove nitrogen from wastewater using less aeration and
70	thus reducing treatment costs for small communities. But, many of these communities experience
71	wastewater temperatures below the generally accepted 25°C minimum for effective
72	ANAMMOX-based nitrogen removal. <sup>24</sup> Therefore, this study is what we understand to be the
73	first report of partial nitritation ANAMMOX below the 25°C threshold in pilot-scale, smart-
74	aerated SAGBs operated at 20°C.
75	Materials and Methods
76	ANAMMOX Seed Reactor Activity and DNA Analysis
77	ANAMMOX seed material (1.6 L) from the Hampton Roads Sanitation District, York River,
78	Virginia, treatment plant that was recently retrofitted to be the first $DEMON^{\mathbb{R}}$ sidestream
79	deammonification system in North America. <sup>25</sup> The seed was maintained in a 2 L, glass container
80	that was table shaken at 100 RPM at 38.5°C. A nitrogen purge line with diffuser stone was
81	inserted to maintain anaerobic conditions and the seed reactor was periodically fed $NH_4^+$ (~25
82	mg/L, variable), NO <sub>2</sub> <sup>-</sup> (~25 mg/L, variable), NaHCO <sub>3</sub> (100 mg/L), NaH <sub>2</sub> PO <sub>4</sub> (25 mg/L), K <sub>2</sub> HPO <sub>4</sub>
83	(30 mg/L), MgCl <sub>2</sub> (40 mg/L), and CaCl <sub>2</sub> (60 mg/L). ANAMMOX activity was measured during
84	a 72 hour $NH_4^+$ and $NO_2^-$ (initial concentrations of 25 mg/L) utilization experiment with analysis
85	by ion chromatographs (AS2000 and AS900, Thermo Scientific Dionex, Sunnyvale, CA)
86	equipped for cations (CS15 column) and anions (AS22 column) with software control and data
87	processing (Chromeleon, version 7). Dissolved oxygen was measured by luminescence with an
88	electronic probe and meter (IntelliCAL <sup>™</sup> LDO101 probe, HQ40d meter, Hach Company).

89	Presence of ANAMMOX bacteria was determined by DNA extraction, polymerase chain
90	reaction (PCR) amplification of the 16S rRNA gene, cloning, sequencing and phylogenetic
91	analysis. Genomic DNA was extracted (PowerWater <sup>®</sup> Sterivex <sup>TM</sup> DNA Isolation Kit, MO BIO
92	Laboratories, Carlsbad, CA) from 200 mL of 20-fold diluted (RNase-free water, Qiagen,
93	Germantown, MA) ANAMMOX seed and PCR inhibiting substances were removed (QIAquick
94	PCR Purification Kit, Qiagen). A 25 µL PCR reaction mix containing 12.5 µL of Taq PCR
95	Master Mix (Qiagen), 600 nM each of the forward and reverse primers (A438f/A684r; specific
96	for the ANAMMOX 16S rRNA gene <sup>26</sup> ) and 450 ng of DNA template was used. Partial 16S
97	rRNA genes (246 base pair (bp) expected product size) were amplified (Eppendorf MasterCycler
98	EP S, Hamburg, Germany) and the products were purified (MinElute PCR Purification Kit,
99	Qiagen). The purified PCR products were ligated overnight at 4°C into the pCR <sup>®</sup> 2.1 vector using
100	the TA Cloning <sup>®</sup> Kit (Invitrogen, Carlsbad, CA) with a 1:1 molar insert to vector ratio. Ligations
101	were transformed into One Shot <sup>®</sup> TOP10 Chemically Competent E. coli (Invitrogen) and
102	transformants were analyzed according to the cloning kit instructions. Plasmids were extracted
103	using QIAprep Spin Miniprep Kit (Qiagen) and clones were PCR-screened with M13 primers
104	(both F and R). Appropriately sized inserts were Sanger-sequenced with the M13F primer (5'-
105	GTAAAACGACGGCCAG -3') at the Iowa Institute of Human Genetics, Genomics Division.
106	The 16S rRNA gene sequences were analyzed for nearest neighbor sequences via the SimRank
107	function in Greengenes (http://greengenes.lbl.gov), a chimera-checked 16S rRNA database. <sup>27</sup>
108	SimRank estimates the similarity between two sequences with respect to how many unique 7
109	nucleotide sequence runs (7-mers) they share. SimRank similarity scores do not necesarily
110	equate with % identities that are obtained by sequence alignment. Nucleotide sequences derived
111	from this study have been deposited in Genbank (Accession nos. KM401817-KM401837).

- 112 *Pilot–Scale SAGB Setup and Operation*
- 113 Four pilot-scale SAGBs (Figure 2) were constructed within a temperature controlled chamber 114 operated at 20°C. Synthetic wastewater was stored in a 950 L polypropylene head tank positioned 4 m above floor level. The head tank was connected via 3.8 cm diameter PVC pipe to 115 116 four 45 L polypropylene dosing tanks positioned above the inlet of each 61 cm x 61 cm x 46 cm 117 SAGB. The dosing tank outlets were connected to an electronic valve and that to an inlet 118 manifold. The inlet manifold was a 1.3 cm diameter PVC down pipe connected to a 1.3 cm 119 diameter, 55 cm long, horizontal pipe with eight 2.4 mm dosing holes. Treated wastewater exited 120 each SAGB via a horizontal, 3.8 cm diameter PVC pipe, 55 cm long with sixteen 3.6 mm 121 diameter holes. The effluent manifold piping penetrated the SAGB wall before connecting to a 122 water level control apparatus. The level control apparatus was a vertical 3.8 cm diameter, 30.5 123 cm tall PVC pipe open to atmosphere. The level control apparatus was contained in a 19 L 124 bucket that drained to the sanitary sewer via 3.8 cm diameter pipe. SAGB1 and SAGB2 125 contained aeration manifolds consisting of four, 1.3 cm diameter PVC pipes, 50 cm long, with 126 3.2 mm outlet holes connected via 61 cm long distribution piping including a 76 cm tall inlet 127 pipe. SAGB3 and SAGB4 were aerated via a 2 cm diameter diffuser stone placed 13 cm from the 128 inlet, 2.5 cm above bottom. Compressed air was provided by a pump (Pondmaster AP 100, 129 Danner Manufacturing, Islandia, NY) connected to a distribution manifold with adjustable 130 needle flow valves. Additionally, SAGB4 was equipped with a recirculation pump that delivered 131 effluent water to the sampling port at 0.1 LPM. 132 Washed pea gravel (~0.1 m<sup>3</sup>) was added to each SAGB before inoculation with 45 L of
- 133 municipal primary effluent (Iowa City, IA). A synthetic wastewater, comprised of yeast extract
- 134 (10 mg/L), casamino acids (10 mg/L), NaHCO<sub>3</sub> (100 mg/L), NaH<sub>2</sub>PO<sub>4</sub> (25 mg/L), K<sub>2</sub>HPO<sub>4</sub> (30

135	mg/L), MgCl <sub>2</sub> (40 mg/L), and CaCl <sub>2</sub> (60 mg/L), sodium acetate (110 mg/L), glucose (100 mg/L)
136	and glycine (67 mg/L) (modified from Klatt <sup>28</sup> ), was added gradually to each SAGB over 7 days
137	to minimize bacterial washout. The head tank was filled with synthetic wastewater that was
138	continuously sparged with nitrogen to slow microbial degradation prior to dosing. The dosing
139	valves were microcontroller (Arduino UNO R3, SmartProjects, Italy) programmed to deliver 3 L
140	of synthetic wastewater every 6 hours to achieve a mean hydraulic residence time of
141	approximately 4 days. All SAGBs were operated for 19 weeks with SAGB1 and SAGB2 aerated
142	at 1.2 LPM on a 6 hour on, 6 hour off cycle to mimic conditions from our previous work. <sup>7</sup>
143	SAGB3 and SAGB4 received no mechanical aeration during this period.
144	Synthetic wastewater dosing was then halted, and 0.25 L of the ANAMMOX seed was added to
145	each SAGB followed by a 7 day attachment period. At this point, SAGB3 and SAGB4 were each
146	equipped with pH-controlled (IntelliCAL <sup>TM</sup> PHC101 probe and SC200 universal controller,
147	Hach Company, Loveland, CO) air flow meters (FMA5518, Omega Engineering, Stamford,
148	Connecticut) that delivered 2.0 LPM when on. Given the established pH range of 6.5–8.0 for
149	partial nitritation ANAMMOX processes, two pH ranges between 7.0 and 7.5 were chosen for
150	this study. The pH-control for SAGB3 was programmed to begin aeration at pH 7.25 and to
151	cease aeration at pH 7.05 and the pH–control for SAGB4 had set points of 7.45 and 7.25,
152	respectively. The SAGBs were inoculated again with primary effluent 3 weeks and 7 weeks into
153	the 10 week partial nitritation ANAMMOX operational period that culminated in a 48 hour
154	intensive sampling event.
155	SAGR Nitrogen Removal Assessment and ANAMMOY Analysis

# 155 SAGB Nitrogen Removal Assessment and ANAMMOX Analysis

156 The transient nitrogen-species behavior and overall nitrogen removal of each SAGB was

assessed during an intensively–sampled 48 hour period in the 30<sup>th</sup> week of operation. During this

	-
	0
	Manuscri
	0
	S
	5
	σ
	5
	D
	Ð
	6
	δ
	6
	Ö
	<b>Ipacts Accepted</b>
	S
	5
	ď
	Ö
	Ξ
	õ
d	()
	esses
).	5
	()
ar	Ŭ
	0
	5
	0
	Ð
	g
	Science
	0
	S
3	
3	
	ronmental S
	vironmental S

158	time, the influent $NH_4^+$ (n = 1), TN (n = 4), COD (n = 4), total organic carbon (TOC, n = 4),
159	$NO_2^-$ (n = 1) and $NO_3^-$ (n = 1) concentrations and effluent $NH_4^+$ (n = 21), TN (n = 4), COD (n =
160	4), TOC (n = 4), $NO_2^-$ (n = 21) and $NO_3^-$ (n = 21) concentrations were determined. Dissolved
161	oxygen was directly measured and SAGB samples were collected for $NH_4^+$ , $NO_2^-$ and $NO_3^-$
162	analyses every 2 hours from a 3.8 cm diameter sample port (Figure 2) installed 13 cm from the
163	inlet. The port spanned the depth of the pea gravel and contained several 1 cm diameter holes
164	along its length and was wrapped with porous fabric. Samples for $NH_4^+$ , $NO_2^-$ and $NO_3^-$ were
165	filtered, stored at 4°C and analyzed by ion chromatography within 48 hours. Total nitrogen was
166	measured by persulfate digestion method 4500–N $C^{29}$ and COD was determined using the
167	dichromate method 5220D. <sup>29</sup> Dissolved oxygen was measured as described previously and the
168	pH was measured either by the continuously operating probes already described or by a glass
169	electrode and meter (AR15, Fisher Scientific, Pittsburg, PA). Total organic carbon was measured
170	by direct method 415.3 <sup>30</sup> and alkalinity was measured via Hach Method 10239 (Hach Company).
171	At the conclusion of the experiment, pea gravel (700 grams) from each SAGB was collected near
172	the inlet at approximately 20 cm below surface for ANAMMOX DNA analysis. The samples
173	were collected in sterile, glass containers and 100 mL of autoclaved deionized water was added.
174	The samples were shaken vigorously to dislodge biomass which was analyzed using the DNA
175	protocol previously described.

# 176 Dynamic Kinetic Modeling of Partial Nitritation ANAMMOX Associated TN Removal

A numerical stock and flow model, with dynamic coupling to aeration events, was built and
utilized to explore the linked N-transformations performed by AOBs, NOBs, denitrifiers, and
ANAMMOX bacteria in SAGB3 and SAGB4 over time (Figure 3). When aeration was on, AOB
and NOB activity was allowed. When aeration was off, denitrification and ANAMMOX activity

181 was allowed. The ANAMMOX rates for  $NO_2^-$  utilization,  $NO_3^-$  formation and  $N_2$  formation were 182 stoichiometrically-coupled to the ANAMMOX rate for  $NH_4^+$  utilization according to Equation 3. 183 Production of ANAMMOX biomass is relatively small in comparison to transformations of other 184 N stocks and was, therefore, lumped with  $N_2$  production (N removal). The differential equations

185 that comprise the model were solved numerically using Euler's method with 1 hour time steps

186 (STELLA version 8.0, ISEE Systems, Inc., Lebanon, New Hampshire).

#### 187 **Results and Discussion**

188 ANAMMOX Seed Reactor Activity and Bacterial Identification

189 At the onset of the ANAMMOX activity experiment,  $NH_4^+$  and  $NO_2^-$  concentrations in the seed

190 reactor were 25.5 and 23.9 mg–N/L, respectively. After 72 hours, the  $NH_4^+$  concentration was 5

191 mg–N/L and NO<sub>2</sub><sup>-</sup> was 8.7 mg–N/L with first–order decay coefficients 0.54 d<sup>-1</sup> and 0.34 d<sup>-1</sup>,

- 192 respectively. Dissolved oxygen was < 0.1 mg/L. The removal of NH<sub>4</sub><sup>+</sup> under anaerobic
- 193 conditions was viewed as one line of evidence that ANAMMOX bacteria were active in the seed
- 194 reactor. Furthermore, SimRank analysis of the partial 16S rRNA gene (246 bp) showed top hits

as a *Candidatus* Brocadia sp. (of the Planctomycetales order) with a 75–97% SimRank identity.

- 196 Candidatus Brocadia and Candidatus Kuenenia were found in biomass samples from the
- 197 wastewater treatment plant in Strauss, Austria<sup>31</sup>, which provided the ANAMMOX seed for the
- 198 York River plant that supplied our seed material. Other bacteria identified as possibly present for
- 199 the seed reactor and for the SAGBs included *Candidatus* Anammoxoglobus, *Candidatus*
- 200 Jettenia, and *Candidatus* Scalindua which are all known ANAMMOX bacteria.
- 201 SAGBs with Timer–Controlled Aeration (SAGB1 and SAGB2)
- 202 The sample port results for SAGB1 (Figure 4) showed that DO concentrations varied between
- 203 zero and approximately 8 mg/L with DO being utilized with each dosing of synthetic

204	
204	wastewater. SAGB2 (Figure 4) showed slightly higher overall DO concentrations within the
205	sample port, but less synchronicity between wastewater dosing time and DO consumption than
206	for SAGB1. Nitrate was the dominant nitrogen form measured in the sample ports for SAGB1
207	and SAGB2 which, considered with the DO data, indicates that nitrification occurred during the
208	aerated phases of the operational cycle. Periods of anaerobic conditions, suggested by DO data
209	for SAGB1, and periods of low DO measured in SAGB2 indicated that denitrification (to $N_{\rm 2}$
210	and/or $N_2O$ ) was possible in these bioreactors when aeration was off. A total of 1,728 L of air
211	was delivered to SAGB1 and SAGB2 during the four, 6-hour aeration cycles that occurred
212	during the 48 hour intensive measurement period.
213	The 45% reduction of TN concentration from average influent values to average effluent values
214	in SAGB1 and SAGB2 (Table 1) suggests that nitrification-denitrification was indeed occurring.
215	The nitrification phase suggested activity by AOBs and by NOBs as effluent nitrate
216	concentrations reached 36±4 mg–N/L. But, the denitrification potential would have been limited
217	by organic carbon availability (1.4±0.3 mg/L in the effluent, Table 1) in SAGB1 and SAGB2
218	remaining from a dosed amount of 16 mg/L. Compared to our previous work <sup>7</sup> , these SAGBs
219	underperformed on TN removal (65–95% previously) and performed similarly with respect to
220	oxygen demand reduction (84-93% cBOD removal previously). These results were expected
221	given that mean DO concentrations were quite high (4.6±2.6 mg/L) and that these SAGBs were
222	operated as controls for the partial nitritation ANAMMOX SAGBs. DNA results from pea gravel
223	samples collected at the conclusion of the 30 week experiment confirmed the presence of
224	<i>Candidatus</i> Brocadia with a SimRank of >91% for the four samples analyzed. But, ANAMMOX
225	activity was assumed to be negligible given the periods of high DO and given that conditions
226	clearly favored NOB growth and activity.

227 Partial Nitritation ANAMMOX SAGB without Recirculation (SAGB3)

228 Sample port results for SAGB3 (Figure 5, A & B) indicated that DO concentrations were at or 229 near zero throughout the 48 hour sampling period. The pH-controlled aeration cycle was 230 triggered five times (Figure 5) and the presence of  $NO_2^-$  (~1 mg–N/L) and  $NO_3^-$  (~10 mg–N/L) 231 in the sample port was an indication that available oxygen was consumed, at least partially, by 232 AOB and NOB activity. With additional oxygen, the NOBs would have converted all NO<sub>2</sub><sup>-</sup> to NO<sub>3</sub><sup>-</sup> as demonstrated in the more fully aerated SAGB1 and SAGB2. Therefore, SAGB3 was 233 234 shown capable of performing partial nitritation – the first step in the partial nitritation 235 ANAMMOX process. A total of 1,344 L of air was delivered to SAGB3 from the 5 aeration 236 cycles during the 48 hour intensive measurement period. 237 In the effluent, total nitrogen was reduced 48% and the  $NH_4^+$  concentration was reduced 67% as compared to the influent (Table 1) in SAGB3. The removal of NH<sub>4</sub><sup>+</sup> in an anaerobic bioreactor 238 239 that contains NO<sub>2</sub><sup>-</sup> is strong evidence for ANAMMOX activity. Assuming the entire 55 mg–N/L 240 influent TN in SAGB3 was available as  $NH_4^+$  for partial nitritation ANAMMOX, Equation 5 241 predicts 3.5 mg–N/L NO<sub>2</sub><sup>-</sup> would be produced and consumed, 2.1 mg–N/L NO<sub>3</sub><sup>-</sup> and 18.2 mg/L 242 N<sub>2</sub> would be formed and 0.14 mg-N/L would accumulate into ANAMMOX biomass. Total 243 nitrogen removal predicted by partial nitritation ANAMMOX would therefore be 18.3 mg-N/L 244 (N<sub>2</sub> plus biomass–N) and would account for 68% of the 27 mg–N/L TN removed from SAGB3 245 (Table 1).

The kinetic modeling results (Figure 5C) showed dynamic coupling to aeration events through stepwise utilization of  $NH_4^+$ ,  $NO_2^-$  and dissolved oxygen. The production of partial nitritation ANAMMOX associated  $NO_3^-$  (as opposed to NOB-associated production) was modeled as a steady increase over the 48 hour period since  $NO_2^-$  was constantly present (Figure 5B) and,

250	therefore, did not limit the ANAMMOX reaction. The rate coefficients for AOBs, NOBs,
251	denitrification, ANAMMOX $NH_4^+$ utilization and ANAMMOX $NO_2^-$ utilization were used in the
252	model to generate partial nitritation ANAMMOX associated conversion rates for $NH_4^+$ , $NO_2^-$ ,
253	$NO_3^-$ , and $O_2$ (Table 2). Again, assuming the entire 55 mg-N/L influent TN in SAGB3 was
254	available as $NH_4^+$ for partial nitritation ANAMMOX, the modeled $NH_4^+$ conversation rate of 3
255	mg/L/d over a 4 day retention time would indicate a loss of 12 mg/L, or 44.4%, of the 27 mg-
256	N/L removed. This result, coupled with the analysis above, suggests that partial nitritation
257	ANAMMOX associated TN removal was between 44 and 68% in SAGB3.
258	Nitrogen removal may have alternatively occurred via denitrification and/or denitritation.
259	Theoretical removals were estimated assuming 100% of the COD removal (51 mg/L) occurred as
260	a result of these processes. Given that 2.86 mg COD is required to convert 1 mg–N $NO_3^-$ and
261	1.71 mg COD is required to convert 1 mg–N $NO_2^-$ (calculated using methods described in
262	Rittmann and McCarty <sup>32</sup> ) to N <sub>2</sub> , up to 17.8 mg–N/L NO <sub>3</sub> <sup>-</sup> and up to 29.8 mg–N/L NO <sub>2</sub> <sup>-</sup> could
263	have been removed via denitrification or denitritation, respectively. Additionally, using a net
264	biomass yield of 0.4 and assuming that biomass was 12.4% nitrogen <sup>32</sup> , an estimated 2.5 mg–N/L
265	was incorporated into biomass. Collectively, these quantities represent 75% and over 100% of
266	the TN removal measured in SAGB3, respectively. However, it is highly unlikely that 100% of
267	the COD removal occurred via anaerobic processes since faster growing aerobic heterotrophs
268	would have consumed some of the DO during times of aeration. For example, if 50% of the DO
269	was consumed by heterotrophs, the denitrification/denitritation potential would have been
270	reduced to a level where significant partial nitritation ANAMMOX would be required to close
271	the nitrogen mass balance. Furthermore, effluent $NO_3^-$ concentrations of $17\pm1.5$ mg–N/L suggest
272	additional oxygen was consumed by autotrophic NOBs. The elevated NO3 <sup>-</sup> concentrations also

273 indicate that denitrification potential was limited by carbon scarcity, providing further indirect

collected in SAGB3 at the conclusion of the 10 week nitritation ANAMMOX operational phase

evidence for significant partial nitritation ANAMMOX. DNA results from pea gravel samples

had top hits for *Candidatus* Brocadia with a SimRank of 75–79% for three samples.

277 Partial Nitritation ANAMMOX SAGB with Recirculation (SAGB4)

274

278 Sample port results for SAGB4 (Figure 5 D & E) showed that a single, pH-controlled aeration 279 cycle was triggered during the sampling period which caused a momentary DO increase from <0.1 mg/L to  $\sim 0.7$  mg/L. The NH<sub>4</sub><sup>+</sup> concentrations were slightly greater than those measured in 280 281 the SAGB3 sampling port, but the NO<sub>3</sub><sup>-</sup> and NO<sub>2</sub><sup>-</sup> concentrations were substantially lower than 282 SAGB3. Collectively, these results indicate that the DO concentrations were lower overall in 283 SAGB4 compared to SAGB3 and that NOB activity was consequently much lower in SAGB4 as well. The lack of measureable NO<sub>2</sub><sup>-</sup> in the SAGB4 sample port indicates low AOB activity 284 285 and/or rapid NO<sub>2</sub><sup>-</sup> utilization by ANAMMOX bacteria. A total of 660 L of air was provided to

286 SAGB4 during the 48 hour intensive measurement period.

287 In the effluent, the total nitrogen was reduced by 53% in SAGB4 (Table 1). If the entire 61 mg-288 N/L of influent TN were transformed through partial nitritation ANAMMOX, 3.8 mg–N/L NO<sub>2</sub> 289 would have been formed and utilized, 20.1 mg–N/L N<sub>2</sub> would have been emitted, 2.3 mg–N/L 290  $NO_3^-$  would have been produced and 0.16 mg-N/L of biomass would have grown (based on 291 Equation 5). If this were the case, 63% of the 32 mg-N/L TN removed (Table 1) by SAGB4 292 would be attributable to partial nitritation ANAMMOX. Effluent COD was reduced by 83% and 293 NO<sub>3</sub> and NO<sub>2</sub> were not detected (Table 1). The kinetic modeling results (Figure 5F) revealed 294 the oxygen dependence of  $NO_2^-$  formation by AOBs and the lack of partial nitritation ANAMMOX associated  $NH_4^+$  utilization when  $NO_2^-$  is absent (Figure 5E). Again, various rate 295

coefficients were used in the model to generate associated conversion rates (Table 2) and the TN
removal attributed to partial nitritation ANAMMOX was 16% using this approach. Therefore, a
range of 16 to 63% of partial nitritation ANAMMOX associated TN removal was achieved for
SAGB4.

300 Using the same approach as described for SAGB3, up to 25.2 mg-N/L NO<sub>3</sub><sup>-</sup> or up to 42.2 mg-301 N/L NO<sub>2</sub><sup>-</sup> could have been removed via denitrification or denitritation if 100% of the COD was 302 removed during those processes. Incorporation of N into biomass would have removed 303 approximately 3.6 mg-N/L. These values represent 90% and over 100% of the 32 mg-N/L TN 304 removed. However, the low DO conditions and lack of  $NO_3^-$  production measured in the sample 305 port suggests that denitrification was not a significant removal mechanism. Nitritation-306 denitritation could have been a significant nitrogen loss mechanism in SAGB4, but partial 307 nitritation ANAMMOX would have been a viable removal mechanism as well. And, the unlikely 308 scenario that 100% of the COD removal was a consequence of denitritation increases the 309 likelihood of significant partial nitritation ANAMMOX removal being required to close the 310 nitrogen mass balance. DNA analysis of the attached growth at the end of the experiment again 311 suggested the presence of Candidatus Brocadia with a SimRank of 78-97% for the four samples 312 analyzed.

This study provides compelling evidence that SAGBs with pH–controlled aeration can remove similar amounts of TN via the partial nitritation ANAMMOX process at 20°C while utilizing substantially less aeration than timer–controlled SAGBs that perform nitrification– denitrification. This result is significant since only recently has a stable nitritation ANAMMOX culture been reported to operate below 25°C at the lab–scale.<sup>24, 33</sup> De Clippeleir's work utilized a

318 lab-scale, rotating biological contactor at 15°C. Hu's experiment was done in a lab-scale

319	sequencing batch reactor initially at 30°C followed by a gradual temperature reduction to as low
320	as 12°C. Both studies showed partial nitritation ANAMMOX to be feasible at these lower
321	temperatures while treating relatively low-ammonia wastewater. Our data also supports the
322	feasibility of utilizing one-stage bioreactors <sup>34</sup> for partial nitritation ANAMMOX at a larger,
323	pilot-scale and with autonomous, pH-controlled aeration. Our partial nitritation ANAMMOX
324	associated $NO_2^-$ utilization rates of 1.7-3.2 mg-N/L/d were much lower than reported rates for
325	suspended cell cultures (400-1100 mg/L/d). <sup><math>34</math></sup> But, this was expected since the cell cultures were
326	studied at ideal temperatures and at a much higher cell densities than can be expected in SAGBs.
327	The relatively high $NH_4^+$ concentrations in the effluent of the smart–aerated SAGBs is an
328	indication that more research is needed to optimize AOB and ANAMMOX activity while
329	minimizing NOB activity. Nonetheless, this study expands our understanding of the promise and
330	current limitations of smart-aerated, partial nitritation ANAMMOX SAGBs for biological
331	nitrogen removal.
332	Conclusions
333	The SAGBs with smart-aeration, operating in partial nitritation ANAMMOX mode, required
334	less aeration (1344 L and 660 L) than the timer-controlled SAGBs (1728 L) during the 48 hour
335	intensive sampling period while achieving a similar level of TN removal at 20°C. This represents

- an aeration-associated energy efficiency benefit of over 50%. But, high effluent  $NH_4^+$
- 337 concentrations (11–21 mg/L) in the smart–aerated SAGBs indicated that research is needed to
- optimize the operational parameters to maximize TN removal, meet  $NH_4^+$  discharge limits and
- 339 gain the reduced aeration benefit from partial nitritation ANAMMOX SAGBs.

# 340 Acknowledgements

- 341 The authors acknowledge the financial support of Donald Bently and Dick Konzen and thank Dr.
- 342 Charles Bott for graciously providing ANAMMOX bacteria.

#### References

- 1. S. Schlegel and H. Koeser, *Water Sci Technol*, 2007, 55, 83-89.
- 2. DWA/ATV, Plants with Submerged Fixed Beds ATV Manual for Biological and Advanced Wastewater Treatment (in German), Berlin, 1997.
- 3. H. Dong, Z. Qiang, T. Li, H. Jin and W. Chen, *J Environ Sci (China)*, 2012, **24**, 596-601.
- 4. J. Fan, S. Liang, B. Zhang and J. Zhang, *Environ Sci Pollut Res Int*, 2013, 20, 2448-2455.
- 5. G. Maltais-Landry, R. Maranger, J. Brisson and F. Chazarenc, *Water Res*, 2009, **43**, 535-545.
- 6. C. Ouellet-Plamondon, F. Chazarenc, Y. Comeau and J. Brisson, *Ecol Eng*, 2006, **27**, 258-264.
- 7. E. D. Redmond, C. L. Just and G. F. Parkin, *Water Environ Res*, 2014, 86, 305-313.
- 8. J. Fan, W. Wang, B. Zhang, Y. Guo, H. H. Ngo, W. Guo, J. Zhang and H. Wu, *Bioresour Technol*, 2013, **143**, 461-466.
- 9. P. B. Pedros and W. K. Dobie, WEFTEC, 2006.
- 10. F. R. Mahony Associates, *Amphidrome*, http://www.amphidrome.com. Accessed Web Page.
- 11. P. B. Pedros, J. Y. Wang and H. Metghalchi, *J Environ Eng*, 2007, **133**, 191-197.
- 12. P. B. Pedros, A. Onnis-Hayden and C. Tyler, *Water Environ Res*, 2008, **80**, 222-228.
- 13. P. B. Pedros, C. Cherchi, A. Onnis-Hayden and E. Wenger, WEFTEC, 2007.
- 14. M. Strous, J. J. Heijnen, J. G. Kuenen and M. S. M. Jetten, *Appl Microbiol Biotechnol*, 1998, **50**, 589-596.
- 15. Water Environment Federation, *Biofilm Reactors, WEF Manual of Practice No. 35*, WEF Press, Alexandria, Virginia, 2010.
- 16. M. O'Shaughnessy, J. Sizemore, M. Musabyimana, P. Sanjines, S. Murthy, B. Wett, I. Takacs, D. Houweling, N. G. Love and K. Pallansch, WEFTEC, 2008.
- K. A. Third, A. O. Sliekers, J. G. Kuenen and M. S. Jetten, *Syst Appl Microbiol*, 2001, 24, 588-596.
- W. Zeng, Y. Zhang, L. Li, Y.-z. Peng and S.-y. Wang, *Enzyme Microb Technol*, 2009, 45, 226-232.

- 19. H. Zhao, R. Lemaire, M. Christensson, G. Thesing, F. Veuillet, J. Ochoa, D. Lamarre and A. Gadbois, *Single-Stage Deammonification Process Performance MBBR Versus IFAS Configurations*, WEF Nutrient Removal and Recovery, 2013.
- 20. B. Wett, *Water Sci Technol*, 2006, **53**, 121-128.
- 21. L. Y. Zhang, L. Zhang, Y. D. Liu, Y. W. Shen, H. Liu and Y. Xiong, *Desalination*, 2010, **250**, 915-920.
- 22. K. Furukawa, P. K. Lieu, H. Tokitoh and T. Fujii, *Water Sci Technol*, 2006, 53, 83.
- 23. H. Gao, Y. D. Scherson, G. F. Wells, Environ Sci Process Impacts, 2014, 16, 1223-1246.
- 24. Z. Hu, T. Lotti, M. de Kreuk, R. Kleerebezem, M. van Loosdrecht, J. Kruit, M. S. Jetten and B. Kartal, *Appl Environ Microbiol*, 2013, **79**, 2807-2812.
- 25. Worldwide Water, *North America's first full-scale DEMON® deammonification system recognized*, http://www.worldwaterworks.com/resources/press-releases/aaees-honor-award, Accessed Web Page.
- 26. S. Humbert, J. Zopfi and S.-E. Tarnawski, *Environ Microbiol Rep*, 2012, 4, 484-490.
- 27. T. Z. DeSantis, P. Hugenholtz, N. Larsen, M. Rojas, E. L. Brodie, K. Keller, T. Huber, D. Dalevi, P. Hu and G. L. Andersen, *Appl Environ Microbiol*, 2006, **72**, 5069-5072.
- 28. C. G. Klatt and T. M. LaPara, *Biotechnol Bioeng*, 2003, **82**, 313-320.
- 29. APHA, AWWA and WPCF, *Standard methods for the examination of water and wastewater*, 22nd edn., Washington, DC., 2012.
- 30. Code Federal Regulations, *Title 40—Protection of Environment, parts 136–149*, US Government Printing Office, Washington, DC., 2012.
- B. Wett, G. Nyhuis, S. Podmirseg, M. Gómez Brandón, T. Puempel, M. Hell, W. Kirchler, M. Cesconi and S. Murthy, *Population dynamics at the limits of DEMON plant operations*, http://www.essdemon.com/libraries.files/Wett\_DEMON\_plant\_operations.pdf. Accessed Web Page.
- 32. B. Rittmann and P. McCarty, *Environmental Biotechnology: Principles and Applications*, McGraw-Hill, New York, NY, 2001.
- 33. H. De Clippeleir, S. E. Vlaeminck, F. De Wilde, K. Daeninck, M. Mosquera, P. Boeckx, W. Verstraete and N. Boon, *Appl Microbiol Biotechnol*, 2013, **97**, 10199-10210.
- 34. T. Lotti, R. Kleerebezem, C. Lubello and M. C. M. van Loosdrecht, *Water Res*, 2014, **60**, 1-14.

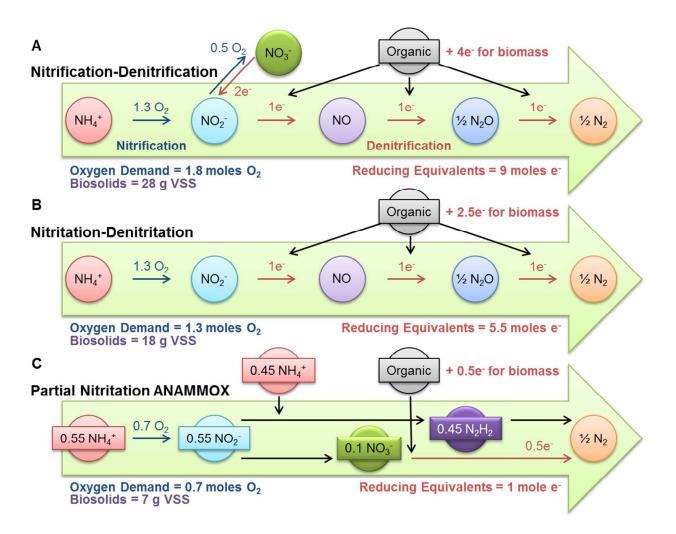


Figure 1: Comparison of oxygen demand, reducing equivalents and biosolids production for (A) nitrification-denitrification, (B) nitritation-denitritation, and (C) partial nitritation ANAMMOX. Adapted from Gao et al.<sup>23</sup>



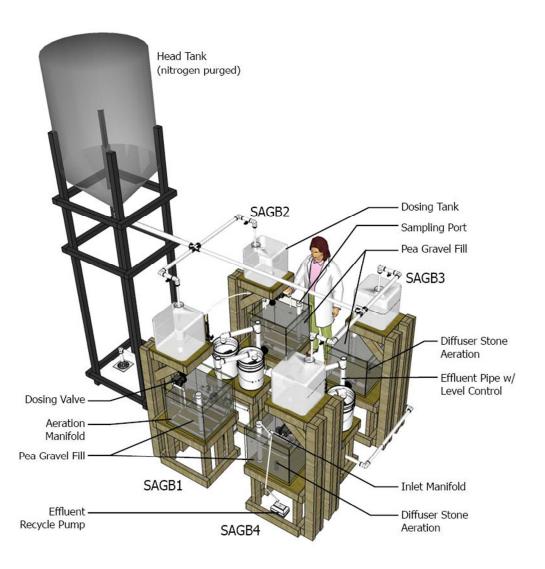


Figure 2: The pilot-scale submerged attached growth bioreactors with timer-controlled aeration (SAGB1 and SAGB2), pH-controlled aeration with no effluent recycle (SAGB3), and pH-control with effluent recycle (SAGB4).

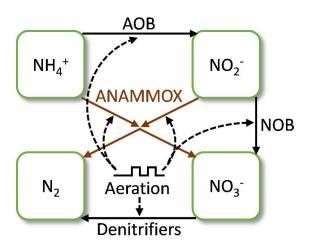


Figure 3: Graphical representation of the aeration-coupled, numerical stock and flow model used to describe the partial nitritation ANAMMOX kinetics in SAGB3 and SAGB4.





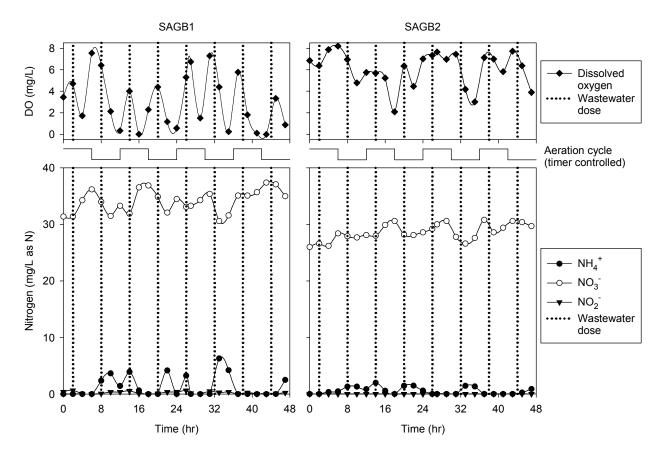


Figure 4: Sample port data from SAGB1 and SAGB2 showing concentrations of DO,  $NH_4^+$ ,  $NO_3^-$  and  $NO_2^-$  measured every two hours during the 48 hour intensive sampling period. Wastewater dosing times are indicated by dotted, vertical lines and timed-aeration cycles are shown by the saw tooth, horizontal lines.

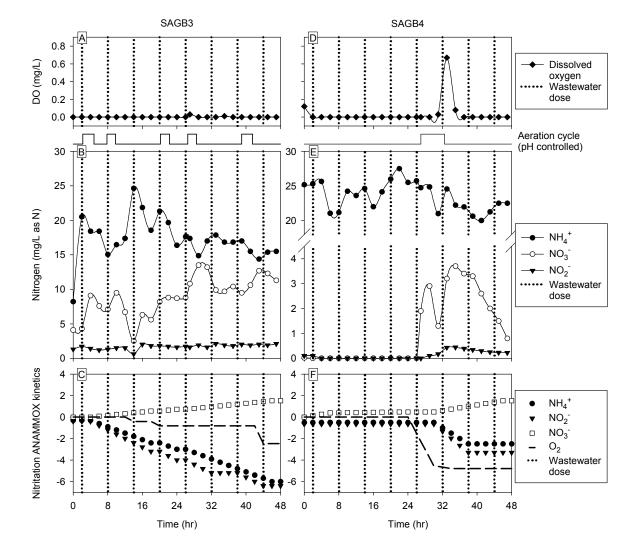


Figure 5: Sample port data from SAGB3 (A & B) and SAGB4 (D & E) showing concentrations of DO,  $NH_4^+$ ,  $NO_3^-$  and  $NO_2^-$  measured every two hours during the 48 hour intensive sampling period. Kinetic modeling results for SAGB3 (C) and SAGB4 (F) for a simulated 48 period that dynamically mimicked aeration events under experimental conditions. Wastewater dosing times are indicated by dotted, vertical lines and pH-controlled aeration cycles are shown by the saw tooth, horizontal lines.

0
<b>S</b>
S
2
Т
Đ
5
5
ö
4
<b>t</b> S
0
Q
d
E
õ
S
Ð
U)
S
<b>U</b>
ŏ
Ľ
Ce
Ž
Ð
5
S
ta
Ξ
D
B
0
5
Ū.

	Influent Concentration (mg/L)							Effluent Concentration (mg/L)						
	Average ± S.D. Average ± S.D.													
SAGB	Total	$NH_4^+$	COD	TOC	Alk	NO <sub>3</sub> -	$NO_2^-$	Total N     NH4 <sup>+</sup> COD     TOC     Alk     NO3 <sup>-</sup>				NO <sub>3</sub> <sup>-</sup>	$NO_2^-$	
	Ν							(removal)	(removal)	(removal)	(removal)	(removal)		
1&2	58*	30	77*	16*	143*	< 0.1	< 0.1	32±3	< 0.1	2±4	1.4±0.3	N.A.	36±4	< 0.1
$1 \alpha 2$	38.	50	//.	10.	145	<0.1	1 <0.1	(45%)	(100%)	(97%)	(91%)	IN.A.	30±4	<b>\U.1</b>
n	5512	34	67±6	15±4	141	<0.1	<0.1	28±0.7	11±1.5	16±10	2.0±2.4	64	17+1.5	0.010.2
3	55±3	54	0/±0	15±4	141	<0.1	<0.1	(48%)	(67%)	(76%)	(87%)	(55%)	17±1.5	0.8±0.3
4	61+0	22	96124	1710	145	<0.1	<0.1	29±2	21±2	14±5	1.4±0.9	105	<0.1	<0.1
4	61±9	33	86±34	17±2	145	<0.1	<0.1	(53%)	(36%)	(83%)	(92%)	(28%)	<0.1	<0.1

Table 1: Influent and effluent concentrations and removal percentages for TN, NH<sub>4</sub><sup>+</sup>, COD, TOC, alkalinity, NO<sub>3</sub><sup>-</sup>, and NO<sub>2</sub><sup>-</sup>.

\*estimated from values obtained from the SAGB3 and SAGB4 dosing tanks.

## **Environmental Science: Processes & Impacts**

Table 2: Kinetic modeling rate coefficients and resulting partial nitritation ANAMMOX conversion rates and associated total N removal.

			Rate Coeffic	cients (hr <sup>-1</sup> )	Partial Nitritation ANAMMOX As Conversion Rates (mg L <sup>-1</sup> d <sup>-1</sup>					
SAGB	AOB	NOB	Denitrification	ANAMMOX NH4 <sup>+</sup>	ANAMMOX NO2 <sup>-</sup>	NH4 <sup>+</sup>	NO <sub>2</sub> <sup>-</sup>	NO <sub>3</sub> -	<b>O</b> <sub>2</sub>	Total N % Removal
3	1.2	0.1	0.01	0.3	0.4	-3.0	-3.2	0.76	-0.82	44
4	1.0	0.1	0.01	0.5	0.66	-1.3	-1.7	0.34	-2.4	16