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When catalyst meets reactor: continuous biphasic processing of xylan to furfural over GaUSY/Amberlyst-36

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The multi-step conversion of xylan hemicellulose and xylose to furfural is investigated in a continuous-flow biphasic fixed-bed reactor over a catalytic bed constituted by a physical mixture of a Lewis-acid gallium-containing USY zeolite for xylose isomerisation and a Brønsted-acid ion-exchanged resin, Amberlyst-36, for hemicellulose hydrolysis and xylulose dehydration. The water-soluble substrates are converted in the aqueous phase into intermediates which promptly transform into the desired furan product thanks to the high degree of contact between the solid catalysts. The large interfacial area developed in the reactor through the Taylor flow of liquids enables an efficient extraction of furfural to the organic phase, minimising side reactions. The diminished contact of the GaUSY catalyst with water controls its instability against metal leaching, leading to stable operation for 24 h on stream. Optimisation of variables including the catalyst ratio, the nature of the extracting phase, the contact time, and the feed concentration, enables to attain furfural yields of 72% from xylose and 69% from xylan. The latter value is the highest reported in the literature for hemicellulose processing over a heterogeneous catalytic system. These results highlight the potential of concerted catalyst and reactor design strategies towards the realisation of more efficient and intensified processes for the sustainable production of bio-based chemicals and fuels.

1 Introduction

Over the last decade, the finiteness of fossil fuel reserves has promoted increasing research efforts aimed towards the development of effective strategies to valorise abundant saccharide feedstocks.¹ Along with a few other compounds, furfural and 5-(hydroxymethyl)furfural (HMF) have been identified as the most promising intermediates in future biobased value chains for chemicals and fuels production.² They can be derived from xylan hemicellulose and cellulose through hydrolysis followed by either Brønsted acid-catalysed dehydration or Lewis and Brønsted acid-catalysed isomerisation-dehydration of the xylose and glucose obtained. Upon the initial investigation of the conversion of the latter C_5 and C₆ sugars in an aqueous medium mainly over homogeneous catalysts,³ furfural and HMF yields have not exceeded 30% due to the occurrence of multiple side and consecutive reactions.⁴ The alternative use of organic solvents (e.g. DMSO, gammavalerolactone) with heterogeneous catalysts or of ionic liquids with homogeneous catalysts has proved to significantly boost the furans yields (up to 80 or 95%, respectively).⁵ Still, these media are impractical at a large scale. The high boiling point of the former implies a high-energy input for downstream purification procedures, while the latter are costly and relatively unstable against the water formed as a byproduct. As a more attractive option for enhancing the selectivity. Dumesic et al.⁶ proposed to process sugars in a biphasic medium comprising water and a low-boiling point organic solvent such as methyl isobutyl ketone. In this system, an extractive reaction takes place, *i.e.* the carbohydrates are transformed in the aqueous phase and the organic phase extracts and accumulates the desired furan product as soon as it is formed, limiting the occurrence of further unwanted reactions.^{6,7} The benefits of this approach have been demonstrated by the enhanced HMF yield (55%) attained upon HCl-catalysed fructose dehydration.⁶ Following this concept, Huber *et al.*⁸ have reported furfural yields > 90% from hemicellulose using HCl or H₂SO₄ as catalysts in a mixture of NaCl-containing water and THF.

In addition to a high process selectivity, the use of heterogeneous rather than homogenous catalysts, not imposing energy-intensive separation steps,⁹ and the application of continuous-flow instead of batch reactors, ensuring higher productivities, are most prominent and complementary aspects to enable a prospective efficient large-scale conversion of

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 $\mbox{Scheme 1.}$ Continuous-flow biphasic reactor used for the upgrading of C_{s} carbohydrates to furfural.

sugars. With respect to the use of solid catalysts, Davis et al.¹⁰ evaluated the batch biphasic isomerisation-dehydration of different C₆ sugars using the Lewis-acidic Sn-beta zeolite in combination with diluted HCl obtaining 60% HMF yield. Fully heterogeneous catalytic systems based on TiO₂, metal phosphates, supported Cs-containing heteropolyacids or zeolites, have also been assessed in biphasic media and led to limited HMF (40%) and furfural (54%) yields.¹¹ The highest furfural yield (74%) was achieved with a composite material consisting of zeolite beta nanocrystals embedded in a siliceous TUD-1 mesoporous matrix.¹² Concerning the employment of continuous reactors, continuous stirred biphasic tank reactors⁶ and tubular reactors operated with a segmented-flow of the aqueous and organic phases¹³ have been explored. The second configuration allows for superior mass transfer properties, since the organic phase forms a thin wall around the slugs of the aqueous phase, leading to a 4-fold higher interfacial area.¹⁴ Thus, Brasholz et al.¹⁵ could convert fructose to HMF in the presence of HCl with a yield of 74% at a contact time of 15 min. When using zirconia and titania as catalysts, McNeff et al.¹⁶ obtained HMF from glucose with a maximum yield of only 29% at a contact time of 2 min. The limited relevance of the catalytic results of the latter isolated effort to combine a continuous-flow reactor with a heterogeneous solid is likely due to the suboptimal acid characteristics of the materials applied.

Herein, we design a highly efficient process for the transformation of C₅ sugars to furfural under a Taylor flow of water and an organic phase over a bifunctional catalytic bed (Scheme 1). The Lewis-acid solid comprises a galliumcontaining USY zeolite prepared via the facile alkaline-assisted metallation method, which already demonstrated suitable to highly selective Lewis-acid introduce centres in (alumino)silicates.¹⁷ Its activity, selectivity, and stability was first evaluated in the aqueous-phase conversion of xylose to xylulose. Thereafter, it was complemented by Brønsted-acid Amberlyst-36 to attain furfural. Due to the consecutive nature of the reactions involved and, thus, the crucial role of an intimate mixing between the two catalysts to maximise the furfural yield, a well-homogenised physical mixture of the solids was used. The influence of key variables including the nature of the extracting phase, H_2O :organic solvent ratio, temperature, and catalyst proportion on the process were determined in order to enhance the furfural yield and the stability of the catalysts. Catalytic tests at variable particle size and temperature and calculations were performed to verify a kinetic controlling regime and gain insights into the characteristics of the Taylor flow in the packed bed. Finally, our optimised technology was extrapolated to the conversion of the more complex xylan substrate to furfural, attaining successful results.

2 Experimental

2.1 Catalysts

Two different commercially available USY zeolites have been used in this study. CBV720 (bulk Si/Al = 15, denoted as USY-1) was purchased from Zeolyst, whereas HSZ390-HUA (bulk Si/Al = 385, denoted as USY-2) was supplied by Tosoh. Gallium was introduced in the zeolites via post-synthetic alkaline-assisted metallation as previously reported.¹⁷ Thus, the as-received samples were treated in NaOH solutions (0.2 M, 30 cm³ per gram of dried zeolite) containing 0.04 or 0.05 M of Ga(NO₃)₃·H₂O (ABCR, 99.9%) in the case of USY-1 and USY-2, respectively, during 30 min at 338 K in an EasymaxTM 102 reactor (Mettler Toledo). The resulting materials were converted into their protonic forms by three consecutive ion exchanges in an aqueous solution of ammonium nitrate (0.1 M NH₄NO₃, 6 h, 298 K, 100 cm³ per gram of dried zeolite), followed by calcination in static air at 823 K (5 K min⁻¹) for 5 h. The Ga-containing catalysts are referred to as GaUSY-1 and GaUSY-2. Amberlyst-36 (acid sites concentration \geq 5.40 eq kg⁻¹, $S_{\text{BET}} = 33 \text{ m}^2 \text{ g}^{-1}$) was purchased from Dow-Chemicals.

2.2 Characterisation

The gallium content in the fresh and used materials was evaluated by inductively-coupled plasma optical emission spectroscopy (ICP-OES) using a Horiba Ultra-2 instrument. Prior to the ICP measurements, the materials were digested in an acidic mixture (HCl/HNO₃/HF) under heating (343 K, overnight). The amount of carbon deposited on the catalysts after reaction was determined by elemental analysis using a LECO CHN-9000 instrument. Powder X-ray diffraction (XRD) was measured using a PANalytical X'Pert Pro-MPD diffractometer with Ni-filtered Cu Kα radiation $(\lambda = 0.1541 \text{ nm})$. Data were recorded in the 5-70° 2 θ range with an angular step size 0.05° and a counting time of 7 s per step. Nitrogen isotherms at 77 K were collected using a Quadrasorb-SI analyser. Quantachrom Prior to the measurements, samples were degassed in vacuum (10^{-1} mbar) at 573 K for 3 h. Fourier transform infrared (FTIR) spectroscopy of adsorbed pyridine was carried out using a Bruker IFS66 spectrometer equipped with a liquid N2-cooled

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mercury cadmium telluride (MTC) detector. Self-supporting zeolite wafers (20 mg, 5 ton cm⁻², 1 cm²) were pretreated at 10^{-3} mbar and 693 K for 4 h. After cooling down to room temperature, the samples were saturated with pyridine vapour and then evacuated at room temperature for 15 min and subsequently at 473 K for 30 min. Spectra were recorded in the 650-4000 cm⁻¹ range (4 cm⁻¹ resolution) by co-addition of 32 scans. High-resolution magic angle spinning ⁷¹Ga nuclear magnetic resonance (MAS NMR) spectroscopy was conducted using a Bruker AVANCE 700 NMR spectrometer equipped with a 4-mm probe head and 4-mm ZrO₂ rotors at 213.5 MHz. Spectra were acquired using a spinning speed of 10 kHz, 20,000 accumulations, 1 µs pulses, a recycle delay of 0.02 s and Ga(NO₃)₃·H₂O as reference.

Catalytic tests

Catalytic tests were performed using a homemade continuousflow reactor setup (Scheme 1) composed of a (i) dual-pump system (Gilson-305 and Gilson-306) equipped with a mixing chamber (Gilson-811D) and a manometric module (Gilson-806), (ii) a stainless-steel tubular reactor with a precolumn (Swagelok SS-T4-S-035, o.d. = $\frac{1}{4}$ inch, i.d. = 4.6 mm) both heated by a tubular oven, and (iii) a backpressure regulator (Swagelok, LH2981001). The reactor was loaded with GaUSY-1, GaUSY-2 (0.18-0.54 g in both cases) or Amberlyst-36 (0.72 g, sieve fraction = 0.18-0.25, 0.25-0.36 and 0.6-0.7 mm),or a physical mixture of the zeolite- and resin-based catalysts (1.08 g in total), diluted 1:3 with quartz (sieve fraction = 0.25-0.36 mm) and inserted in a tubular oven heated at 393-413 K. Thereafter, the liquid feed was admitted. The latter was composed of a Taylor flow of an aqueous phase containing 5 wt.% xylose (Sigma-Aldrich, 99%), or 2.5 wt.% of xylan (from beech wood, Sigma-Aldrich, 90%), and an extracting organic phase consisting of either methyl isobutyl ketone (MIBK, ABCR, 99%), toluene (Fluka, \geq 99.7%), or dichloroethane (DCE, Fluka, $\geq 99.5\%$) in a 10:90 or 20:80 H₂O:organic solvent volume ratio. To prevent solvent loss by evaporation, the system was pressurised to 25 bar prior to heating. Samples were periodically collected at the outlet. The aqueous and organic phases were separated after decantation. Xylose, xylulose and lyxose were isolated by high-performance liquid chromatography (HPLC) in a Agilent 1260 Infinity system equipped with a a Biorad Aminex HPX-87C column heated at 353 K and a refractive index detector (Agilent G1362 A) set a 303 K using Millipore water $(0.50 \text{ cm}^3 \text{ min}^{-1})$ as the eluent. Quantification was obtained by integration of their respective peaks. Xylose and lyxose (Sigma-Aldrich, 99%) were employed as references. In case of xylulose, the yield was calculated using the response factor of xylose. Furan derivatives present in the organic phase were analysed using a gas chromatograph (GC, HP 6890) equipped with an HP-5 capillary column and a flame ionisation detector. Furfural (Sigma-Aldrich, 99%) was employed as reference. He was used as the carrier gas (flow rate = $1 \text{ cm}^3 \text{ min}^{-1}$, pressure = 0.4 bar, split ratio = 35) and an injection volume of $2 \mu L$ was applied. The initial temperature of 353 K was held for 1 min before heating to 523 K (10 K min^{-1}). The yield of furfural was determined using biphenyl (ABCR, 99%) as internal standard.

Results and Discussion

GaUSY catalysts for sugar isomerisation

In order to select the most suited GaUSY isomerisation catalyst, alkaline-assisted galliation was performed on two different parent zeolites, the Al-rich USY-1 and the Al-lean USY-2.

Catalyst	Ga loading ^a (wt.%)	Crystallinity ^b (%)	$\frac{V_{pore}^{c}}{(cm^{3} g^{-1})}$	V_{micro}^{d} (cm ³ g ⁻¹)	$\frac{S_{\text{meso}}^{d}}{(\text{m}^2 \text{ g}^{-1})}$
USY-1	-	100	0.56	0.29	128
USY-2	-	100	0.58	0.30	105
GaUSY-1	5.8	78	0.49	0.25	119
GaUSY-2	5.9	77	0.57	0.29	116

^{*a*}Determined by ICP-OES. ^{*b*}Derived from XRD. ^{*c*}Volume adsorbed at $p/p_0 = 0.99$. ^{*d*}Determined by the *t*-plot method.



Figure 1. (a) Xylose isomerisation over the Lewis-acid USY zeolites in water. Conditions: xylose content in H₂O = 5 wt.%, $W_{zeolite}$ = 0.36 g, T = 403 K, τ_r = 6.8 min. (b) Xylose isomerisation over USY-ATGa4 in water and H₂O:MIBK (20:80) and isomerisation-dehydration over USY-ATGa4/Amberlyst-36 in H₂O:MIBK (20:80). Conditions: xylose content in H₂O = 5 wt.%, $W_{zeolite}$ = 0.36 g, W_{resin} = 0.72 g, T = 403 K, τ_r = 6.8 min.



Figure 2. (a) ⁷¹Ga MAS NMR spectra of galliated USY zeolites prior to and after 24-h use in isomerisation-dehydration and (b) XRD patterns of USY-1 and its galliated counterpart prior to and after use in isomerisation or isomerisation-dehydration. The reflections marked by the asterisk are due to the quartz that was unavoidably mixed with the catalyst upon unloading of the reactor. Conditions: xylose content in H₂O = 5 wt.%, $W_{zeolite} = 0.36$ g, $W_{resin} = 0.72$ g, H₂O:MIBK = 20:80, T = 403 K, $\tau_r = 6.8$ min.

While galliated USY-1 has been reported to be highly active and stable for the conversion of dihydroxyacetone to ethyl lactate,¹⁷ post-synthetic gallium introduction in USY-2 was never attempted so far. For sake of comparison, the quantity of Ga(NO₃)₃ used in the metallation procedure was adapted for each sample in order to generate catalysts containing similar gallium content (ca. 6 wt.%). The compositional, structural and porous properties of parent and modified samples are reported in Table 1. The crystallinity only decreased by ca. 20% upon metallation of both USY-1 and USY-2, confirming the retention of the zeolitic structure in the treatment. This was further supported by the negligible changes in micropore volume (V_{micro}), which remained at the levels expected for the large pore USY zeolites (0.25 and 0.29 cm³ g⁻¹ for GaUSY-1 and GaUSY-2, respectively). The external surface area was hardly altered by the treatment, in agreement with our previous observation that the alkaline-assisted metallation process heals vacancies.17

The modified materials were evaluated in the continuousflow isomerisation of xylose to xylulose at 403 K (Fig. 1a). While USY-1 did not show any activity, thus excluding a possible contribution of Lewis-acidic extra-framework aluminium (EFAl), GaUSY-1 and GaUSY-2 exhibited a xylose conversion of 14% and 21%, respectively. Xylulose was the dominant product (61 and 69% selectivity, in the order), while only traces of lyxose were detected (3% selectivity in both cases). As no additional signal was visualised in the chromatogram, it was assumed that the remaining portion of xylose converted was transformed into insoluble humins. In view of elucidating this difference in performance, the zeolites were studied by IR of adsorbed pyridine as well as ⁷¹Ga MAS NMR spectroscopy. The concentration of Lewis-acid sites was slightly higher for GaUSY-2 than for GaUSY-1 (134 μ mol g⁻¹ *versus* 101 μ mol g⁻¹). Additionally, differences were observed in the structure of the metal sites introduced (Fig. 2a). While both the spectra of GaUSY-1 and of GaUSY-2 featured a peak at 174 ppm, usually associated to tetrahedral (T_d) gallium species, and a signal at 0 ppm, likely associated to octahedral (O_h) or distorted tetrahedral (dT_h) gallium species, the latter contribution was much stronger and sharper for GaUSY-2, indicating the presence of gallium species with more uniform structure. These results suggest that the higher activity of the GaUSY-2 material descends from a slightly higher acidity and the presence of sites with more suitable characteristics. The role of hydrophobicity, which is well known to relate to the Al content in the zeolite, should also not be excluded, as the USY-1 and USY-2 matrices have substantially different Si/Al ratios (15 versus 385). Indeed, hydrophobicity plays a pivotal role on catalyst stability and activity in the upgrading of biomass in aqueous and biphasic mixtures, as recently demonstrated by Resasco et al.¹⁸

The activity of GaUSY-2 was monitored for 24 h on stream in the presence of (i) pure water, (ii) a mixture of water and MIBK and (iii) a mixture of water and MIBK and the dehydration catalyst Amberlyst-36 (Fig. 1b). In order to more easily identify differences, the catalyst amount was doubled to reach higher conversion levels. A strong decrease in xylose conversion (from 46% to 6%) was observed in pure water after 24 h on stream (Fig. 1b). XRD, ICP-OES and elemental composition analyses of the spent catalysts were performed to shed light on the origin of this activity loss. The lack of diffraction lines in the pattern of the used catalyst evidenced the full collapse of the zeolite structure upon reaction in pure water (Fig. 2b), which was accompanied by significant gallium leaching (from 5.9 to 0.27 wt.%) and deposition of C-based species on the catalyst surface (4.1 wt.%). Xylose isomerisation was then conducted in the presence of a mixture of water and MIBK in 20:80 vol.% ratio, mimicking the liquid environment later applied to the full process (Fig. 1b). Under those conditions, gallium leaching was better controlled (from 5.9 to 2.1 wt.%) and the crystallinity of the zeolite preserved to a much greater extent (Fig. 2b). Remarkably, in a biphasic medium and in the co-presence of Amberlyst-36, the xylose conversion remained constant along the duration of the run (Fig. 1b). Analysis of the gallium content after 6 and 24 h of reaction still evidenced metal depletion in the first few hours of the test (from 5.9 to 2.3 wt.%), but the catalyst composition remained substantially unaltered upon further time on stream

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Figure 3. Screening of different parameters in the biphasic isomerisation-dehydration of xylose to furfural. Conditions: a) xylose content in $H_2O = 5$ wt.%, $W_{zeolite} = 0.36$ g, $W_{resin} = 0.72$ g, T = 403 K, H_2O :organic solvent = 20:80; b) xylose content in $H_2O = 5$ wt.%, $W_{zeolite} = 0.18$, 0.36, or 0.54 g, $W_{resin} = 0.72$ g (corresponding to $W_{zeolite}$: W_{resin} ratios of 0.25:1, 0.50:1, or 0.75:1), T = 403 K, H_2O :MIBK = 20:80; c) xylose content in $H_2O = 5$ wt.%, $W_{zeolite} = 0.36$ g, $W_{resin} = 0.72$ g, T = 403 or 413 K, H_2O :organic solvent = 20:80; d) xylose content in $H_2O = 5$ wt.%, $W_{zeolite} = 0.36$ g, $W_{resin} = 0.72$ g, T = 403 or 413 K, H_2O :organic solvent = 20:80; d) xylose content in $H_2O = 5$ wt.%, H_2O :MIBK = 10:90 or 20:80.

(1.9 wt.%). Since the gallium loss was analogous in the presence or absence of Amberlyst-36 and the ⁷¹Ga MAS NMR spectra did not show any considerable changes in the structure of the gallium sites upon reaction (Fig. 2a), the unstable behaviour of GaUSY-2 in the biphasic isomerisation was likely due to the accumulation of xylulose and the consequent generation of byproducts easily adsorbing on the catalyst surface. Unfortunately, it was impossible to completely separate GaUSY-2 from Amberlyst-36 after the reaction for CHN analysis to support this interpretation.

In order to prove the truly heterogeneous nature of our catalytic system, the pH of the outlet stream was analysed, as leaching of sulfonic groups from the resin would render the mixture acidic. No deviation from pH 7 was found either during the first or the last 5 h of the continuous test. Additionally, it was demonstrated that the reactor effluent was not active in converting freshly added xylose (5 wt.%) to either xylulose or furfural during a 5-h batch experiment at 403 K.

Reaction optimisation

Relevant reaction parameters were systematically varied in order to maximise the furfural yield and minimise the reaction temperature, which are beneficial to reduce the amount of waste produced and the energy input for the reaction and the downstream processing. Firstly, the extraction efficiency of furfural in the organic phase was considered as this plays a critical role in the suppression of side and consecutive reactions. Different organic solvents were tested, i.e. MIBK, toluene, and DCE (Fig. 3a). A comparable furfural yield (ca. 40%) was observed at the same contact time (13.6 min) when performing the reaction in H₂O:MIBK (20:80) and H₂O:DCE (20:80). However, as the conversion was lower using MIBK as an extraction solvent compared to DCE (55 versus 77% in the order), the former solvent allowed for a better selectivity. The use of toluene led to the worst selectivity. The superiority of MIBK is in line with the preference for this extrinsic phase in biphasic sugar processing in slurry reactors.^{6b} Furthermore, the selectivity trend MIBK > DCE > toluene appears to correlate to the solubility of the three solvents in H₂O, decreasing from 17 to 8.7 and to 0.5 g L^{-1} in the order. Catalyst deactivation was observed using DCE as well as toluene, whereas the activity could be fully retained using MIBK over 24 h (Fig. 3a). The efficient removal of furfural and humins deposited on the catalyst surface by MIBK has already been reported by Ordomsky et al.4c Further screening was thus conducted using this solvent.

As isomerisation and dehydration occur consecutively, the ratio of GaUSY-2:Amberlyst-36 also has crucial implications on the process selectivity. Three catalyst ratios (on a mass basis) were thus tested (Fig. 3b). Similar results were obtained with the 0.25:1 and 0.5:1 ratios in terms of furfural selectivity, but the reaction proceeded more rapidly in the second case, leading to a process with improved overall productivity. For the ratio 0.75:1, the furfural selectivity was lower, as confirmed by

the dark brown colour of the outlet solution. Xylulose accumulation due to the insufficient dehydration ability of this catalyst composition clearly enhanced humins formation.

The reaction was also tested at different temperatures (Fig. 3c). Only traces of furfural were observed at 293 K. The highest furfural yield, 72%, was obtained at 98% conversion at 413 K and a contact time of only 3.4 min, but the catalyst deactivated with time-on-stream. Remarkably, a similar yield (70%) was reached at the same conversion at 403 K after an only moderately longer contact time (13.6 min) and the catalyst remained stable. At both temperatures, only traces of xylulose and lyxose (2% selectivity) could be detected. These furfural yields are only slightly inferior to those obtained with the best heterogeneous catalysts in batch experiments, *i.e.* a composite material in a water-toluene mixture (74%) and H-mordenite in gamma-valerolactone (80%).^{5b,12}

Apart from the nature of the organic solvent, the ratio of the aqueous and organic phases strongly impacts the extraction efficiency and thus the furfural selectivity (Fig. 3d). The best performance was obtained at a H₂O:MIBK ratio of 10:90 with a furfural yield of 70% at a xylose conversion of 92%. The maximum yield obtained at H₂O:MIBK = 20:80 was 40% at 55% xylose conversion.



Figure 4. a) Furfural yield from xylose *versus* particle size. Conditions: xylose content in H₂O = 5 wt.%, $W_{zeolite} = 0.36$ g, $W_{resin} = 0.72$ g, H₂O:MIBK = 10:90, T = 403 K, $\tau_r = 6.8$ min. b) Arrhenius plot for xylose conversion to furfural. Conditions: xylose content in H₂O = 5 wt.%, $W_{zeolite} = 0.36$ g, $W_{resin} = 0.72$ g, H₂O:MIBK = 10:90, T = 293-413 K, $\tau_r = 2.26$ min.

Kinetic and flow analysis

The profiles of the xylulose and furfural yields versus contact time presented in Figs. 3b,c respectively display the typical volcano and S shapes observed for the intermediate and end products of a consecutive reaction. This evidence represents the first indication that the reaction is kinetically controlled and points to xylulose dehydration as the rate-determining step. In order to support the kinetic regime, catalytic tests were conducted in which the particle size of the resin was varied, while keeping all other parameters (including the volume of the catalytic bed and the mass of the resin) constant (Fig. 4a). Based on the virtually unchanged furfural yield, the presence of both intra- and extraparticle diffusion limitations was excluded. Additionally, the dependence of the reaction rate on the temperature was evaluated complementing the catalytic tests previously conducted at 403 and 413 K with a measurement at 393 K. As shown in Fig. 5, the Arrhenius plot obtained could be fitted very well by a linear regression line and the activation energy estimated (54 kJ mol⁻¹) was found to be in the range of values already reported in the literature for this reaction. Indeed, while figures of 111-125 kJ mol⁻¹ have been associated with the purely Brønsted-acid catalysed dehydration of xylose to furfural in water,¹⁹ the addition of a Lewis-acid catalyst (*i.e.* the isomerisation-dehydration pathway herein studied) has been shown to lower those values by up to 60%.²⁰ This further corroborates a kinetically-controlled reaction.

While it would certainly be interesting to relate the good mass transfer properties of the system to the characteristics of the Taylor flow in the packed bed, the latter is a very challenging task. A visual inspection of the contacting patterns of fluids and solids is impossible since, due to the temperature and pressure requirements of the reaction, the steel reactor cannot be replaced by an identical unit made of quartz or Teflon. However, we gathered two strong hints that the aqueous and organic slugs would only marginally intermix in the packed bed, thus preserving the high interface and avoiding channelling effects. Firstly, a Taylor flow was still observed right at the outlet of the packed bed and the slugs exhibited similar size and frequency to those of the inlet Taylor flow. Secondly, the Reynolds number calculated at the highest flow rate is extremely low (0.1), pointing to laminar flow.

Extrapolation to xylan conversion

The hydrolysis-isomerisation-dehydration reaction of xylan was performed in the continuous-flow biphasic reactor under the optimised conditions determined for the conversion of xylose to furfural. Remarkably, at a contact time of 13.6 min, a furfural yield of 69% and a xylose yield of 8% were obtained (Fig. 5). Only a few other heterogeneous materials have been shown to enable hemicellulose conversion into furfural, the best system exhibiting a furfural yield of 63%.^{5b,21} Compared to this latter case, our reaction proceeds *ca*. 30 times faster, implying an enhanced space-time-yield for the overall process. As xylulose was still detected in the reaction mixture and its yield features the characteristic volcano dependence on the contact time



Figure 5. Furfural and xylose yields upon continuous-flow biphasic processing of xylan *versus* contact time. Conditions: xylan content in $H_2O = 2.5$ wt.%, $W_{zeolite} = 0.36$ g, $W_{resin} = 0.72$ g, T = 403 K, H_2O :MIBK = 10:90.



Figure 6. Furfural and xylose yields *versus* time-on-stream upon xylan conversion in H₂O/MIBK (10:90). Conditions: xylan content in H₂O = 2.5 wt.%, $W_{zeolite}$ = 0.36 g, W_{resin} = 0.72 g, T = 403 K, τ_r = 6.8 min.

(Fig. 5), xylulose dehydration appears as the rate determining step also in xylan processing. Relevantly, our catalyst displayed stable performance over 24 h on stream (Fig. 6) despite the higher complexity of the reaction in terms of number of steps and substrate bulkiness. Probably due to the lower saccharide concentration, the Ga loss during this test (5.9 to 2.7 wt.%) was even moderately less pronounced compared to the case of xylose conversion.

Conclusions

An efficient continuous conversion of C_5 carbohydrates was attained over a physical mixture of a galliated USY zeolite for the isomerisation of xylose to xylulose and of Amberlyst-36 for the hydrolysis of xylan and dehydration of the xylulose generated to furfural, respectively, under a Taylor flow of an aqueous and organic phase. Galliated Al-lean zeolites proved to be more active than analogous Al-rich materials. The stability of this catalyst in terms of metal leaching and amorphisation appeared to strongly depend on the solvent composition and the products formed, being poor in water upon the single isomerisation, and promising under biphasic operation upon isomerisation-dehydration. Operating parameters like extraction solvent, catalyst ratio, temperature, and H₂O:organic solvent ratio were optimised to maximise the furfural yield from xylose. The best value was 72%. Remarkably, xylan hemicellulose could be converted with very similar efficacy too. These results indicate that the simultaneous exploitation of suitable catalyst formulation and adequate reactor engineering concepts possess great potential to lead to processes with enhanced value. Performing reaction and separation in a single unit operation is not only beneficial in terms of the selectivity of the transformation but also towards process intensification. This approach should be explored more broadly in future biomass-based applications.

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Notes and references

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