

Analytical Methods

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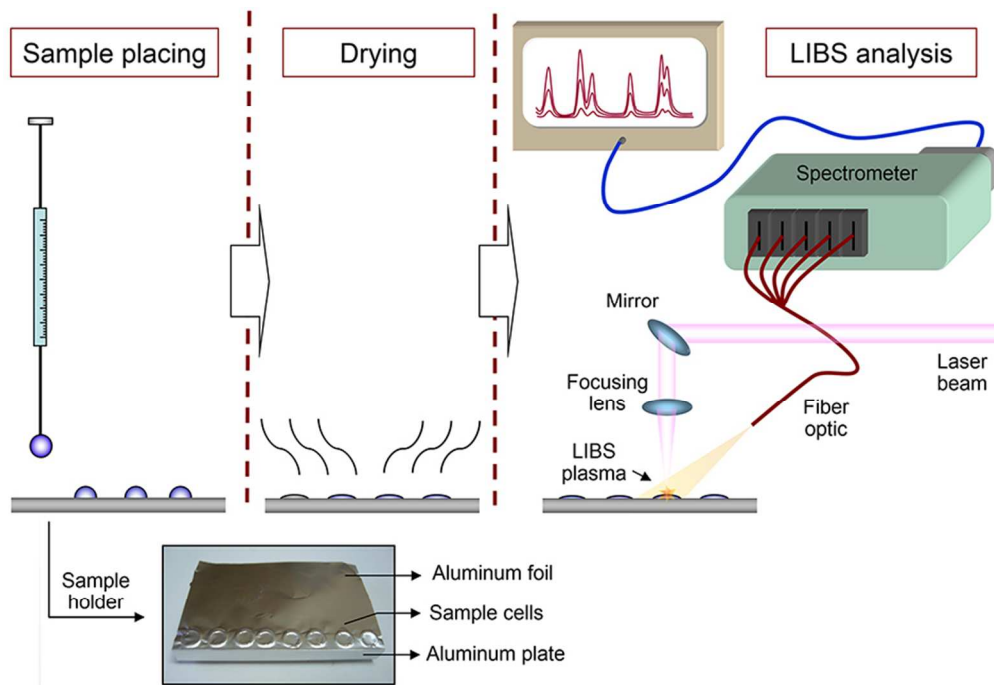
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SDME-LIBS as a synergistic association for overcoming LIBS drawback in liquid analysis.
80x55mm (300 x 300 DPI)

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1 **HYPHENATION OF SINGLE-DROP MICROEXTRACTION WITH**
2 **LASER-INDUCED BREAKDOWN SPECTROMETRY FOR TRACE**
3 **ANALYSIS IN LIQUID SAMPLES: A VIABILITY STUDY[†]**

4
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13 [†] Electronic supplementary information (ESI) available: Further experimental results.
14

15 **Abstract**

16 In this work, an analytical methodology based on Single Drop Microextraction (SDME)
17 followed by Laser-Induced Breakdown Spectrometry (LIBS) has been tested for trace metals
18 determination in liquid samples. By this method, analytes in the samples were extracted into a
19 small volume of toluene as ammonium pyrroldinedithiocarbamate (APDC) chelates. After
20 that, the analyte-enriched toluene was dried on a solid substrate and, finally, the resulting
21 solid residue was analyzed by LIBS. Analyte extraction by SDME procedure was firstly
22 optimized by using a multivariate optimization approach. Under optimum SDME conditions,
23 analytical figures of merit of the proposed SDME-LIBS methodology were compared to
24 those of the direct LIBS analysis method (i.e., without SDME procedure). An estuarine water
25 certified reference material was analyzed for method trueness evaluation. The results
26 obtained in this study indicate that SDME-LIBS methodology leads to a sensitivity increase

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3 1 of about 2.0-2.6 times the ones obtained with LIBS. Detection limits of SDME-LIBS
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6 2 decreases accordingly to the obtained sensitivity improvement, reaching values in the range
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8 3 21-301 $\mu\text{g kg}^{-1}$ for the analytes tested. Measurement repeatability was similar in both SDME-
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10 4 LIBS (13-20% RSD) and LIBS (16-20% RSD) methodologies, being mainly limited by the
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13 5 LIBS experimental setup used in this work for LIBS analysis of liquid samples. The SDME-
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15 6 LIBS analysis of the certified reference material led to recovery values in the range of 96% to
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17 7 112%.
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9 **1 Introduction**

10 Laser-Induced Breakdown Spectrometry (LIBS) is perhaps one of the most versatile
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12 11 techniques for elemental analysis, since it can be applied to a great variety of real-world
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14 12 analytical problems.¹⁻⁶ However, in spite of its potential for the analysis of practically any
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16 13 kind of sample, most LIBS applications have been focused on solid samples analysis whereas
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18 14 its applicability to liquid samples has been, in comparison, poorly exploited. The minor
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20 15 interest in LIBS analysis of liquids can be mainly attributed to its inherent experimental
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22 16 drawbacks,^{2,7,8} which lead to low sensitivity and precision compared to LIBS analysis of
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24 17 solids or to the analysis of liquids with most conventional spectrometric techniques. Even if
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26 18 numerous LIBS experimental strategies have been developed to solve, or at least to reduce,
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28 19 the experimental drawbacks of LIBS analysis of liquid samples,⁹⁻¹⁸ these methodologies still
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30 20 provide analytical results that are, in general, worst than those provided by other well
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32 21 established spectrometric techniques such as ICP-OES.¹⁹
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34 22 In spite of its comparatively lower sensitivity, there is still an inherent advantage that could
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36 23 turn LIBS into a very attractive technique for liquid samples analysis compared to the use of
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38 24 conventional techniques; that is the possibility for *in situ* and on-line analysis offered by this
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40 25 technique due to its field-operable and easily automated instrumentation.
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4 1 A possible way to improve sensitivity and decrease limits of detection in LIBS analysis of
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6 2 liquid samples could be the use of a previous step for analyte enrichment. Liquid Phase
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8 3 Microextraction (LPME) procedures are nowadays extensively used for separation and
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10 4 concentration of both organic and inorganic analytes.²⁰⁻²² These novel microextraction
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12 5 methodologies are faster and more easily automatable than conventional extraction
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14 6 procedures and use negligible volume of extraction solvents, which are often hazardous and
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16 7 expensive. Among the different LPME modalities, Single Drop Microextraction (SDME),
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18 8 Dispersive Liquid Liquid Microextraction (DLLME) and Hollow Fibre Liquid Phase
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20 9 Microextraction (HF-LPME) methodologies have been applied to the concentration of
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22 10 inorganic analytes for trace elemental analysis with excellent results.²³⁻³⁰ The combination of
23
24 11 LPME with LIBS could be a promising alternative for trace elemental analysis due to the
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26 12 complementarity of both extraction and detection procedures; LPME usually results in a
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28 13 microvolume of analyte-enriched extraction solvent, which sometimes needs to be
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30 14 subsequently diluted to adequate it (i.e., quantity, chemical or physical properties) to the
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32 15 requirements of the instrumental system used for analysis (e.g., ICP-OES or FAAS). LIBS,
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34 16 however, has proved to be useful for the direct analysis of microvolumes of liquid samples,
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36 17 owing to its ability to interrogate extremely low quantities of material.³¹ Therefore,
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38 18 microvolumes of solvent resulting from microextraction procedures could be easily analyzed
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40 19 without the need of previous dilution. An added advantage of this combination could arise
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42 20 from the small dimensions and possibility of automation of both LPME and LIBS
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44 21 instrumentation, which could make LPME-LIBS hyphenation suitable for the future
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46 22 development of portable systems for *in situ* and on-line analysis of liquid samples.
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51 23 In this work, combination of LIBS with SDME modality has been tested as an analytical
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53 24 methodology aimed to extend the applicability of LIBS to trace elemental analysis of liquid
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55 25 samples, opening a new way of research on LPME-LIBS hyphenation. Here, Single Drop
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3 1 Microextraction was applied to water samples prior to analyte determination by LIBS, in
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5 2 order to improve the sensitivity of the method. Toluene was used in SDME as extracting
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7 3 solvent of several metals as ammonium pyrrolidinedithiocarbamate (APDC) complexes.
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9 4 SDME procedure was previously optimized by using multivariate analysis. The resulting
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11 5 microvolumes of analyte-enriched solvent were analyzed by LIBS after being dried on an
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13 6 aluminum substrate, as a method for overcoming the experimental difficulties of LIBS
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15 7 analysis of liquids. Analytical figures of merit obtained with both SDME-LIBS and direct
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17 8 LIBS methodologies (*i.e.*, analysis of the water samples by LIBS, after being dried on the
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19 9 aluminum substrate but without previous SDME procedure) are presented and discussed. The
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21 10 proposed methodology was finally tested for determination of several metals in a certified
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23 11 reference material (Estuarine Water, LGC6016).
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32 13 **2 Experimental**

33 14 **2.1 LIBS experimental setup**

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35 15 Fig. 1 shows the LIBS experimental setup used throughout this work for liquid samples
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37 16 analysis. The laser-induced plasmas were generated by focusing a 10 Hz pulsed Nd-YAG
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39 17 laser (model HYL Handy-YAG, Q-switched, Quanta System S.P.A., Varese, Italy), emitting
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41 18 a pulse of energy 180 mJ (pulse width 10 ns FWHM) at 1064 nm, on the sample to analyze.
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43 19 The laser was focused on the sample by a N-BK7 plano-convex lens with 100 mm focal
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45 20 length (model KPX094AR.33, Newport Corporation, Irvine, United States). Plasma emission
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47 21 was collected directly with a five-furcated fiber optic (5x400 μm fiber optic cable, model
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49 22 FC5-UV400-2, Avantes, Apeldoorn, The Netherlands) and was imaged on the entrance slits
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51 23 of a five channel spectrometer with full spectral coverage from 200 nm to 844 nm (model
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53 24 AVS-Rackmount-USB2 housing equipped with five preconfigured AvaSpec-ULS2048-
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55 25 USB2-RM channels, Avantes, Apeldoorn, The Netherlands). A delay system consisting in
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4 1 two pulse generators (Digital delay/pulse generator, model DG 535, Stanford Research
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6 2 Systems Inc., Sunnyvale, USA and 1 Hz-50 MHz pulse generator, model PM-5715, Philips
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8 3 Export B.V., Eindhoven, The Netherlands) was used for synchronization of laser firing and
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10 4 data acquisition. Spectra were collected 1.3 μ s after the plasma generation (optimum
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12 5 condition), with 1 ms acquisition time (minimum time setting available on the spectrometer).
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17 2.2 Sample preparation

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20 8 Water samples containing Cr, Mn, Ni, Cu and Zn as target analytes were analyzed by LIBS in
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22 9 two different ways: (i) without applying any previous sample treatment for analyte
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24 10 concentration (*i.e.*, direct LIBS) and (ii) after a microextraction procedure with SDME
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26 11 methodology to separate and concentrate analytes present in the samples (*i.e.*, SDME-LIBS).
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28 12 In both cases, and in order to avoid liquid splashing during LIBS analysis and to enhance
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30 13 LIBS sensitivity and reproducibility, the corresponding liquids (*i.e.*, water sample or analyte-
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32 14 enriched toluene) were converted into solid by drying on an aluminum surface prior to LIBS
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34 15 measurement (*i.e.*, SENLIBS), as already described elsewhere.³¹ In direct LIBS, few μ L of
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36 16 the water samples were confined into a small cell shaped in an aluminum foil (see Fig. 1).
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38 17 The aluminum foil, placed on an 8 mm thick aluminum plate, was heated by a hot plate to
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40 18 completely evaporate the water. The solid residue was then irradiated with the laser for LIBS
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42 19 analysis.
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44 20 In SDME-LIBS, metal ions were extracted from the water samples as ammonium
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46 21 pyrrolidinedithiocarbamate (APDC) complexes, using toluene as extraction solvent for
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48 22 SDME. After extraction, few μ L of the analyte-enriched toluene were placed on the
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50 23 aluminum foil, were heated by the hot plate to completely evaporate the toluene and, as
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52 24 described above for direct LIBS analysis, were irradiated by the laser for LIBS measurement.
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3 1 In both methodologies, the result of the LIBS analysis was the mean of three replicate
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5 2 measurements (*i.e.*, three single laser shots) made on different positions of the same solid
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8 3 residue.
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10 4 11 12 5 *2.2.1 Single Drop Microextraction procedure*

13 6 For metals extraction by SDME, approximately 9 g of sample was placed in a 20 mL glass
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15 7 vial containing a magnetic stir bar. Solid APDC reagent was added to the vial up to a
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17 8 concentration well in excess of that required to chelate all metals in the solution. Then, the
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19 9 solution pH was adjusted with diluted NH₃ and HCl solutions and, finally, the sample weight
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21 10 was brought to 10 g with deionized water. A microsyringe, containing a known volume of
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23 11 toluene, was clamped above the vial and its needle was immersed into the sample. The
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25 12 plunger was depressed and a microdrop of toluene was exposed to the sample at room
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27 13 temperature for a certain period of time, to allow partition of the analytes between the
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29 14 aqueous phase and the organic droplet. During this time, the solution was continuously stirred
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31 15 with a magnetic stirrer to accelerate the mass transfer process. After extraction, the toluene
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33 16 drop was retracted into the microsyringe and a microvolume of this analyte-enriched solvent
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35 17 was placed on the aluminum foil for LIBS analysis (Figure 1).
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46 19 **2.3 Reagents and solutions**

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48 20 Aqueous calibration standards were prepared by appropriate dilution of a 1000 mg L⁻¹ mono-
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50 21 element standard solutions of Cr, Mn, Ni, Cu and Zn (High-purity mono-element standard
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52 22 solutions, Charleston, United Kingdom) in distilled deionized water (18 MΩ cm resistivity).
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54 23 Ammonium pyrrolidinedithiocarbamate (APDC) (Fluka, Buchs, Switzerland) was used as
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56 24 chelating agent. Diluted hydrochloric acid solution, prepared from a Suprapur 30% (w w⁻¹)
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58 25 HCl solution (Merck, Darmstadt, Germany) and diluted ammonia solution, prepared from a
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3 1 Reagent Grade 32% (w w⁻¹) (in NH₃) solution (Scharlau, Barcelona, Spain) were used for pH
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5 2 adjustment. HPLC grade toluene (Scharlau, Barcelona, Spain) was used as extraction solvent
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7 3 in the microextraction procedure. Estuarine water certified reference material (LGC6016,
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9 4 LGC Deselaeres S.L., Middlesex, United Kingdom) was used for evaluation of method
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11 5 trueness.
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18 2.4 Apparatus

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20 8 A 25 µL syringe (model 1702, Hamilton, Bonaduz, Switzerland) was used to suspend the
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22 9 toluene microdrop inside the standard/sample solutions in the SDME procedure and to place
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24 10 a microvolume of water sample/extraction solvent on the metallic substrate (*i.e.*, aluminum
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26 11 foil) for LIBS analysis. pH measurements were performed with a pH meter (model micropH
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28 12 2000, Crison, Alella, Spain). The solutions were stirred with a magnetic stirrer (model 501,
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30 13 Darlab Egara S.L., Barcelona, Spain). A hot plate (model 500 Darlab Egara S.L., Barcelona,
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32 14 Spain) was used to dry the droplets before LIBS analysis.
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39 3 Results and discussion.

40 41 3.1 Optimization of SDME experimental parameters

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44 18 A multivariate approach was employed to optimize the main experimental factors affecting
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46 19 metals extraction. Several factors including pH, APDC concentration, drop volume,
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48 20 extraction time and stirring speed were studied in order to maximize the extraction yield of
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50 21 the SDME procedure. In order to identify the most important experimental factors affecting
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52 22 SDME, among the ones initially considered, a previous screening study (Plackett-Burman
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54 23 design) was carried out. After that, significant factors were optimized by means of a
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56 24 Circumscribed Central Composite Design (CCCD). In the screening and optimization studies,
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58 25 the experiments were randomly carried out in order to nullify the effect of extraneous or
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3 1 nuisance variables. In both cases, emission signal obtained from LIBS analysis of the
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6 2 resulting extractions was used as the output variable (response) of interest. Statistical
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8 3 software (NemrodW[®] version 2007, LPRAI, Marseille, France) was used for generation of
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10 4 the experimental design matrices and for data processing.
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15 6 *3.1.1 Screening study*

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18 7 A Plackett-Burman design was used for identification of the significant factors affecting
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20 8 SDME (screening). In this particular type of experimental design, interactions between the
21
22 9 different factors are considered to be negligible and, therefore, significant factors can be
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25 10 identified using a limited number of experiments. In this study, a five-factor 12-experiments
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27 11 Plackett–Burman screening design was used. Each factor was represented at two levels,
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29 12 defining the upper and lower limits of the range covered by each factor (see Table 1). Levels
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31 13 chosen for the different factors were based on literature data and preliminary experiments.
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34 14 Synthetic aqueous solutions containing 1 $\mu\text{g g}^{-1}$ of the analytes were used as samples in all
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36 15 the screening experiments. After the extractions, the resulting analyte-enriched solvents were
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38 16 analyzed by LIBS, evaluating the emission signal obtained for the different analytes.
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41 17 Fig. S1 in ESI[†] shows the main effects Pareto charts obtained from the screening
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43 18 experiments. Since microextraction conditions are usually analyte-dependent, a separate
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45 19 screening evaluation was performed for each analyte in order to identify the common
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47 20 significant factors affecting the overall extraction process. Pareto charts in Fig. S1 in ESI[†]
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49 21 illustrate the order of significance of the variables affecting SDME for the different emission
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51 22 lines evaluated. As can be seen, these charts contain a bar for each factor, with the length of
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53 23 the bar being proportional to the relative influence of that factor on the metal extraction.
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55 24 Those bars that extend over the dashed vertical line indicate factors that are statistically
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57 25 significant at 95% probability. The direction of the bar is related to the “sign” of the effect
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1 produced by that factor. That is, those bars to the right of the origin indicate positive effect in
2 the response when increasing the value of the factor and, on the contrary, those bars to the
3 left indicate negative effect.

4 As observed from Fig. S1 in ESI,[†] the screening study provides similar results for all the
5 emission lines evaluated. Drop volume, extraction time and pH can be considered significant
6 factors affecting the extraction with a positive effect, with pH being the most critical
7 parameter. On the other hand, APDC concentration and stirring speed, even if having a
8 slightly positive effect on the response, do not produce any significant impact on extraction.
9 These two factors were, therefore, fixed at their higher level for subsequent extractions (*i.e.*,
10 1% (w v⁻¹) APDC concentration; 1700 rpm stirring speed), and only drop volume, extraction
11 time and pH were considered for optimization in the following study.

12 13 3.1.2 Optimization study

14 The three main factors identified in the previous screening study were optimized by using a
15 Circumscribed Central Composite Design (CCCD). This experimental design requires 5
16 levels for each factor: a central level (0), a low level (-1), a high level (+1) and two star points
17 located at $\pm\alpha$ ($\alpha = 1.682$) from the centre of the experimental domain (0). The levels chosen
18 for the three factors considered (*i.e.*, drop volume, extraction time and pH), as well as the
19 location of their start points, are given in Table 2. The design matrix for this CCCD design
20 involved a total of 18 runs. As in the previous screening study, all the experiments were
21 carried out using synthetic solutions containing 1 $\mu\text{g g}^{-1}$ of the target analytes. LIBS signals
22 of the different emission lines were evaluated in order to compare the optimum conditions for
23 extraction of the different analytes and to decide, accordingly, a common optimum conditions
24 for extraction of all of them.

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3 1 The results obtained in this study are given in Figs. S2 to S6 in ESI[†] as response surfaces and
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5 2 contour plots. Each figure shows the results obtained for a different analyte. Graphics (a), (b)
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7 3 and (c) in these figures show the variation of LIBS emission signal as a function of each pair
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9 4 of factors, while keeping fixed the third one at its optimum value. As can be observed from
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11 5 the plots, all response surfaces show maximum points which are, in general, similar for all the
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13 6 analytes evaluated.

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17 7 Emission signal increases with drop volume to reach a maximum at approximately 7.5 μL . In
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19 8 any case, the use of larger volumes was difficult to handle since the droplet became unstable
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21 9 and easily fell off from the tip of the syringe needle.

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25 10 Similar behavior was observed for pH, with signal increasing up to pH of approximately 10
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27 11 and decreasing thereafter. For metal cations extraction, pH plays a crucial role in the
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29 12 formation of the neutral chelates which can be efficiently transferred to the organic phase.
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31 13 Low pH values favor the protonated form of the complexing reagent, therefore limiting
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33 14 chelates formation and, consequently, metals extraction. On the other hand, insoluble
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35 15 hydroxides or soluble ammonia complexes are preferentially formed at high pH values,
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37 16 avoiding the neutral chelates to form and leading also to a decrease in metals extraction.

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41 17 As expected, increasing the extraction time results in an increase in the total amount of
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43 18 analyte extracted, reaching a maximum at around 10 minutes. Mass transfer is, indeed, a
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45 19 time-dependent process in which transfer rate decreases as the system approach equilibrium.

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48 20 Due to the similarity between the optima obtained for the different analytes, average values
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50 21 were chosen as the common optimum condition for SDME of all of them. Thus, experimental
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52 22 conditions for extraction were set at pH, 10; drop volume, 7.5 μL ; extraction time, 10 min.;
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54 23 APDC concentration, 1% (w v^{-1}) and stirring speed, 1700 rpm.

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3.2 LIBS and SDME-LIBS: analytical figures of merit

In order to assess the analytical capability of SDME-LIBS procedure versus LIBS for the analysis of trace metals in liquid samples, analytical figures of merit (*i.e.*, sensitivity, repeatability and LOD) of both analytical procedures were evaluated and compared. To this end, calibration standards were analyzed by both methods in order to obtain the corresponding calibration graphs: (i) without a previous extraction procedure (direct LIBS analysis of the standards) and (ii) after extraction of the analytes by SDME at optimum conditions. In the former method, calibration was performed by directly analyzing five calibration standards with concentrations of Zn, Mn, Cu and Cr increasing up to 2500 $\mu\text{g kg}^{-1}$ and Ni increasing up to 8000 $\mu\text{g kg}^{-1}$. In the latter, analytes were extracted from the same number of calibration standard solutions, but with concentrations of Ni, Mn, Cu and Cr increasing up to 1000 $\mu\text{g kg}^{-1}$ and Zn increasing up to 800 $\mu\text{g kg}^{-1}$. Afterward, the resulting analyte-enriched toluene microdroplets were analyzed by LIBS. In both cases, the experimental procedure for LIBS analysis of the liquids was that described in the experimental section (section 2.2.). That is, 7.5 μL of the calibration standard (direct LIBS analysis) or 7.5 μL of the resulting analyte-enriched toluene (SDME-LIBS analysis) were placed on the aluminum foil, heated to dryness and analyzed by LIBS. In all cases, LIBS analysis was carried out by averaging the LIBS signal obtained from three single laser shots in different positions on the same dried residue. Even if more laser firings could have been possibly performed on the dried residue, this number was chosen in order to completely avoid a possible overlapping of the ablated zones created in the residue by previous laser shots. Table 3 summarizes the analytical figures of merit obtained by both methods. Here, sensitivity was derived from the slope of the calibration graphs. Repeatability, expressed as RSD, was estimated from the analysis of eight aliquots taken from the same vial of 1 $\mu\text{g g}^{-1}$ calibration standard. For SDME-LIBS procedure, this means from eight extractions, one per

1 aliquot. LOD calculation was based on 3 times the standard deviation of 10 blank
2 determinations (*i.e.*, deionized water for LIBS and toluene for SDME-LIBS). LIBS signal
3 was found to be linear in the concentration range evaluated for each method.

4 As expected, the use of a microextraction procedure leads to sensitivity improvement for all
5 the emission lines evaluated. The extent of this improvement can be easily assessed by
6 looking at the enhancement factor in Table 3, which was calculated as the ratio of
7 sensitivities obtained with and without SDME. As can be seen, all enhancement factors were
8 in the range 2.0-2.6, without any appreciable analyte-dependence. Since sensitivity
9 improvement for a given analyte can be directly associated with its extraction efficiency into
10 the organic phase, this result probably indicates that all metal-APDC chelates were similarly
11 extracted by the applied SDME procedure. As a matter of example, Figs. 2a and 2b show the
12 signal increase observed for ZnII (202.548 nm) and NiI (352.454 nm) emission lines,
13 respectively, when a 1 $\mu\text{g g}^{-1}$ calibration standard is analyzed by SDME-LIBS. In general
14 terms, it seems that SDME-LIBS procedure results in analytical sensitivities that are
15 approximately 2.3 times the ones obtained with LIBS (mean value over the five emission
16 lines evaluated).

17 Repeatability was found to be in the range 13% - 20% RSD, without any clear trend with
18 respect to analyte or analytical procedure. Repeatability of both analytical procedures was
19 observed to be mainly limited by the current LIBS experimental setup for liquid samples
20 analysis. It could be seen, by visual inspection, that the solid residue resulting from the liquid
21 sample drying was not homogeneously distributed over the aluminum foil, thus leading to
22 low repeatability even from replicate measurements performed on different positions on the
23 same sample residue.

24 Detection limits were all below 0.5 mg kg^{-1} for both LIBS and SDME-LIBS methodologies.
25 Without the use of SDME, LOD values ranged from 463 $\mu\text{g kg}^{-1}$ for NiI (352.454nm) to 49

1 $\mu\text{g kg}^{-1}$ for ZnII (202.548 nm). These values were reduced to $189 \mu\text{g kg}^{-1}$ and $21 \mu\text{g kg}^{-1}$,
2 respectively, with the use of SDME. As can be observed from Table 3, relative LODs
3 obtained for the different emission lines were in good agreement with the corresponding
4 enhancement factor, with the exception of Mn. This fact, as well as the comparatively high
5 limit of detection obtained for this element, can be probably due to the presence of Mn as an
6 impurity in the aluminum foil used as solid substrate, which leads to poor reproducibility of
7 the blank measurements. Without considering this element, it can be seen from Table 3 that
8 the use of SDME-LIBS results in LOD values that are approximately 2.5 times lower than
9 those obtained with direct LIBS.

11 **3.3 Analysis of a certified reference material**

12 Method trueness was evaluated from the analysis of a certified reference material (estuarine
13 water). Trueness test was only carried out with the proposed SDME-LIBS procedure, since
14 certified concentrations were all below the quantification limits obtained for direct LIBS
15 analysis. Table 4 shows the results of the estuarine water analysis. Here, percent recovery
16 was used as estimation of method trueness. As observed, the results obtained with SDME-
17 LIBS methodology were in good agreement with the certified values, with recovery values
18 ranging from 96% to 112%.

20 **4 Conclusions**

21 The results obtained in this preliminary study demonstrate that LIBS detection preceded by a
22 single drop microextraction procedure for analyte enrichment allows performing liquid
23 samples analysis with higher sensitivity than direct LIBS. Therefore, SDME-LIBS could be
24 considered a synergistic association for improving LIBS sensitivity drawback in liquid
25 analysis. With the proposed SDME-LIBS analytical methodology, approximately 2.3 fold

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3 1 sensitivity enhancement and 2.5 fold LOD improvement were obtained, compared to the
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5 2 direct LIBS analysis of the liquid samples (i.e., without SDME procedure). Under optimum
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7 3 SDME conditions, SDME-LIBS methodology lead to LOD values in the range of 21-301 μg
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9 4 kg^{-1} for the analytes tested, being LIBS analysis performed in almost single pulse mode.
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11 5 However, even if the use of SDME, as LPME modality chosen in this work, has been proved
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13 6 to improve sensitivity of direct LIBS analysis, the obtained results can not be considered
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15 7 completely satisfactory for the proposed goal and should be only considered as a starting
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17 8 point for exploring the potentialities of this hyphenated techniques for trace elemental
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19 9 analysis of liquid samples. Therefore, much more research work in this field should be done
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21 10 in the future, aimed to improve the capability of the method.

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27 11 On one hand, sensitivity could be further improved with the use of different reagents for
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29 12 metal chelation and extraction, with the use of different microextraction methodologies such
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31 13 as DLLME or HF-LPME, which could lead to enrichment factors higher than those obtained
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33 14 with SDME, or even with the application of double pulse LIBS configuration for LIBS
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35 15 analysis instead of single pulse LIBS, which has been demonstrated to be an efficient strategy
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37 16 for LIBS signal enhancement.¹⁸ On the other hand, the precision of the method, currently
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39 17 limited by the low repeatability of LIBS measurements, could be also improved by using
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41 18 alternative strategies for deposition of the microdroplets on the aluminum substrate, leading
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43 19 to predictable and homogeneous deposits morphology, or by optimizing the LIBS system
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45 20 optical setup, allowing the integration of a higher number of laser shots on the solid residue
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47 21 without the risk of overlapping between the several ablated zones. Last but not least, future
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49 22 studies should also be focused on the possibility to convert the three currently separated, but
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51 23 independently automatable processes (i.e., microextraction, sample deposition/drying and
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53 24 LIBS analysis) in a fully automated SDME-LIBS analytical procedure for stand-alone
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55 25 operation, useful for in-situ trace metals analysis of liquid samples.

5 Acknowledgements

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Figures

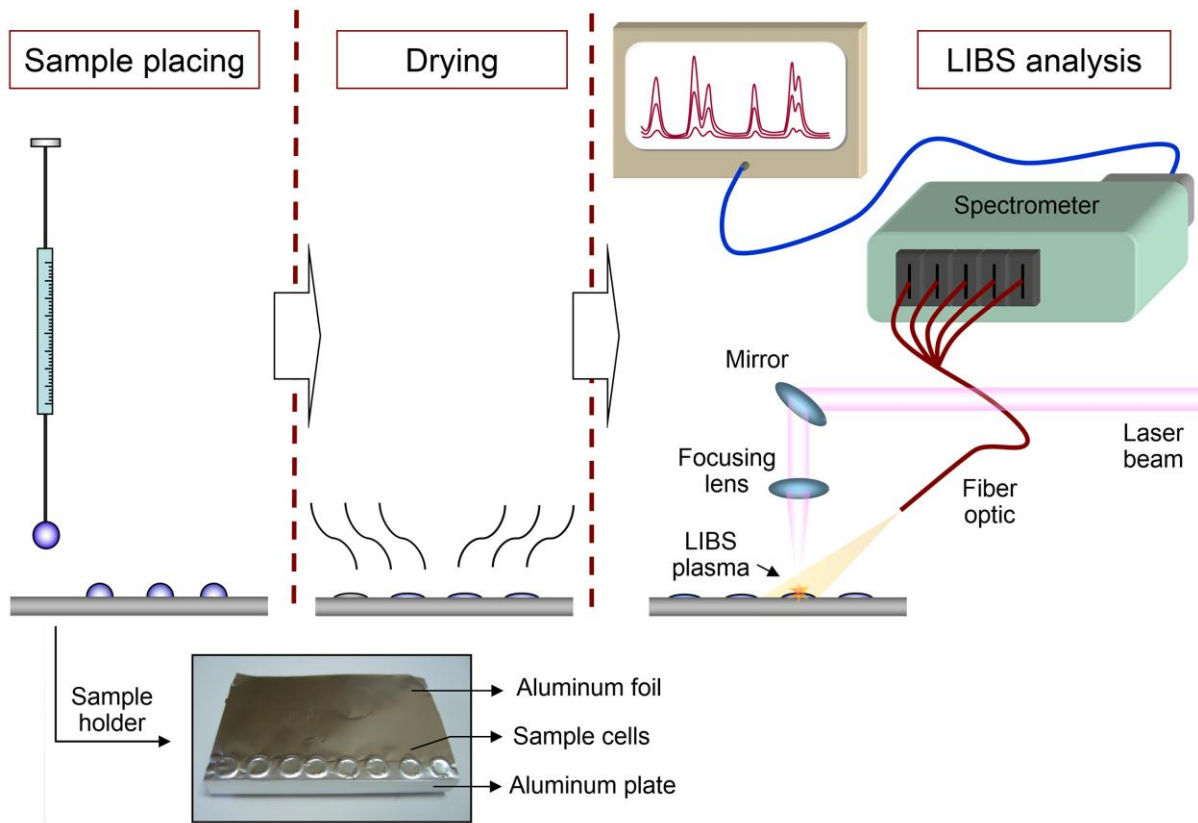


Fig. 1 LIBS experimental setup used in the analysis of liquid samples.

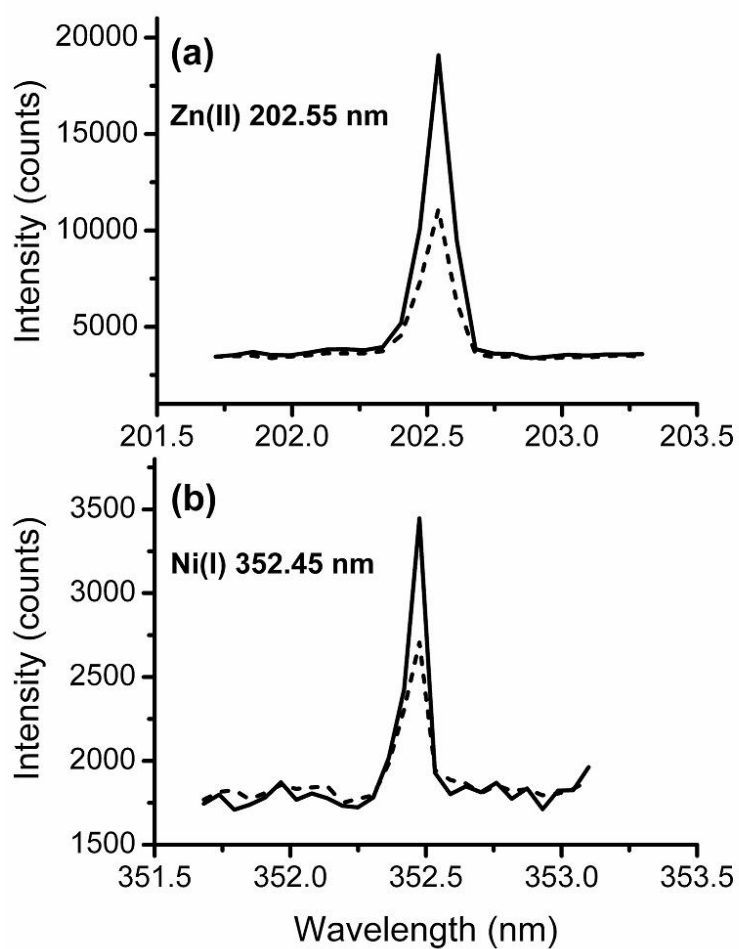


Fig. 2 LIBS signals obtained for (a) ZnII (202.548 nm) and (b) NiI (352.454 nm) emission lines when a $1 \mu\text{g g}^{-1}$ standard solution is analyzed by LIBS (dash line) and SDME-LIBS (solid line) methodologies.

Tables

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Table 1 Experimental factors and levels of the Plackett-Burman design.

Experimental factor	Level	
	Low (-1)	High (+1)
[APDC] (% w v ⁻¹)	0.5	1
Drop volume (μL)	5	7.5
pH	5	10
Stirring speed (r.p.m.)	850	1700
Extraction time (min)	5	10

Table 2 Experimental factors and levels of the Circumscribed Central Composite design (CCCD).

Experimental factor	Level			Star points ($\alpha=1.682$)	
	Low (-1)	Central (0)	High (+1)	$-\alpha$	$+\alpha$
Drop volume (μL)	2.5	5	7.5	0.8	9.2
pH	6	8	10	4.6	11.4
Extraction time (min)	4	7	10	1.9	12.1

Table 3 Analytical figures of merit obtained with LIBS and SDME-LIBS analytical methodologies.

Emission line (nm)	LIBS			SDME-LIBS			Enhancement Factor ^c	LOD Ratio ^d
	Sensitivity ^a (cts kg μg^{-1})	RSD ^b (%)	LOD ($\mu\text{g kg}^{-1}$)	Sensitivity ^a (cts kg μg^{-1})	RSD ^b (%)	LOD ($\mu\text{g kg}^{-1}$)		
ZnII (202.548)	19.5±1.1	17	49	51±2	13	21	2.6	2.3
MnII (259.373)	29±4	16	427	59±4	15	301	2.1	1.4
CuI (324.754)	26±5	20	141	55±5	18	54	2.2	2.6
NiI (352.454)	1.64±0.10	16	463	3.3±0.3	20	189	2.0	2.4
CrI (357.869)	7.0±1.0	19	143	17.6±1.2	16	50	2.5	2.9

^a Uncertainty expressed as standard deviation.

^b Evaluated from the analysis of eight aliquots taken from the same vial of 1 $\mu\text{g g}^{-1}$ calibration standard.

^c Calculated as the ratio of sensitivities obtained with SDME-LIBS and LIBS.

^d Calculated as the ratio of LODs obtained with LIBS and SDME-LIBS.

Table 4 Analysis of LGC6016 certified reference material (estuarine water) by SDME-LIBS.

Emission line (nm)	Certified value ^a	SDME-LIBS	
		Found value ^a	Recovery value (%)
ZnII (202.548)	75±2	84±21	112±25
MnII (259.373)	976±31	1026±215	105±21
CuI (324.754)	190±4	183±35	96±19
NiI (352.454)	186±3	n.q. ^b	n.q. ^b

^aIn $\mu\text{g L}^{-1}$ ± confidence interval at 95%. ^b not quantified.