

Analytical Methods

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3 1 **Development of a gas chromatography-mass spectrometry method for the**
4 2 **determination of ultraviolet filters in beach sand samples**

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13 10
14 11 **Abstract**

15 12 An analytical method for the determination of eight fat-soluble ultraviolet (UV) filters in
16 13 beach sand samples is presented for the first time. The method is based on a leaching
17 14 process of the target compounds from sand samples using vortex mixer agitation and
18 15 further centrifugation, followed by dispersive liquid-liquid microextraction (DLLME) of
19 16 the supernatant and gas chromatography-mass spectrometry (GC-MS) analysis of the
20 17 DLLME extract. The variables involved in the leaching and in the DLLME processes
21 18 were studied to provide the best enrichment factors. In the first case, the leaching
22 19 solvent type and volume, and the vortex mixer agitation time were studied. In the case
23 20 of the DLLME, the type and volume of both disperser and extraction solvent and the
24 21 influence of the pH and the ionic strength of the supporting aqueous solution were
25 22 studied. Under the selected conditions, the method was successfully validated showing
26 23 good linearity ($R^2 > 0.995$), method limits of detection in the pg g^{-1} level, enrichment
27 24 factors in the range of 8 to 50 (depending on the analyte) and good intra- and inter-day
28 25 precision. No significant matrix effects were found, thus external calibration can be
29 26 used. However, internal calibration was recommended to improve repeatability in both
30 27 the DLLME and the GC-injection. Moreover, in order to correct losses during the
31 28 leaching process, the surrogate was added to the samples before the leaching step.
32 29 The validated method was successfully applied to the analysis of several beach sand
33 30 samples from different origin.

34 31 *Keywords:* Beach sand; Dispersive liquid-liquid microextraction; Gas chromatography-mass spectrometry;
35 32 ultraviolet filters; Vortex-assisted leaching

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1. Introduction

It is well-known that sun exposure provides many health benefits on the human health, such as an improvement in the endogenous production of vitamin D or prevention of some diseases as rickets or osteoporosis. However, sun overexposure causes adverse effects, such as skin cancer, cutaneous photoaging and damage to the skin's immunological system [1].

The concern about the health risks commented above has led to an increase in the use of cosmetics containing the so-called UV filters as active ingredients to prevent or minimize the harmful effects of the UV radiation. These active compounds have an organic or inorganic nature, and they act absorbing and/or reflecting, respectively, the UV radiation. The compounds that can be used as UV filters in cosmetic products, and their maximum allowed concentrations are regulated by the legislations in force in each country [1-3].

The excessive use of cosmetics containing these compounds (not only those cosmetics intended specifically for sun protection but also all type of daily products such as moisturizers, after shave products, shampoos, etc) had led to an appearance of the UV filters in the aquatic environment, through direct and indirect sources, where they are being accumulated [4,5]. The high lipophilic characteristics of some of them makes them susceptible to be accumulated in the suspended particles contained in water, sediments, sludge or even biota [4]. Furthermore, different *in vitro* and/or *in vivo* studies show that some UV filters, even at trace levels, present endocrine disrupting activity that might affect the reproduction of fish [5-8]. For this reason, UV filters are currently considered as emerging contaminants and it is interesting to develop analytical methods that allow their determination in the environment at trace levels.

Most publications about the development of analytical methods to determine UV filters in environmental samples are focused on the analysis of environmental water samples [4,5,9,10]. However, different analytical methods can be found in the literature dealing with the determination of UV filters in environmental soil samples, such as river and/or lake sediments [11-17], coastal sediments [16], bight sediments [18], ground soil [12], sewage sludge [10,15,19-23] or even indoor dust [24].

In order to improve the method sensitivity and/or to eliminate some potentially interfering compounds, preconcentration and/or clean-up techniques have been employed. Thus, the determination of UV filters in this type of samples was carried out by extracting (usually in consecutive steps) the analytes from the solid sample into various organic solvents, such as methanol or acetone, by solid-liquid partitioning

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3 71 [11,12,15,18,19]. This traditional extraction technique is time-consuming, poorly
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5 72 selective (i.e., many interferents may be co-extracted) and it often requires large
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7 73 amounts of organic solvents, which causes dilution of the target analytes in the extract.
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9 74 So, an additional clean-up and/or preconcentration step is needed in some cases
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11 75 [12,15]. Newer extraction techniques, such as microwave-assisted extraction (MAE)
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13 76 [16], pressurized liquid extraction (PLE) [13,14,17,20-23] or matrix solid-phase
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15 77 dispersion (MSPD) [24] were employed in subsequent works. In these techniques, both
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17 78 the organic solvent consumption and the time required to carry out the extraction are
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19 79 considerably decreased, but PLE often requires additional clean-up and/or
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21 80 preconcentration steps [13,14,20,22,23].

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22 81 A good alternative to the above mentioned extraction techniques is the so-called
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24 82 dispersive liquid-liquid microextraction (DLLME) [25]. Due to the several advantages
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26 83 that this extraction technique presents (i.e., fast, inexpensive, easy to operate and low
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28 84 consumption of organic solvent) it has become a very popular extraction technique that
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30 85 has been used for the determination of organic and inorganic compounds in different
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32 86 type of samples [26]. Specifically, this microextraction technique has already been
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34 87 used before for the determination of UV filters in water samples [27-35], but it has not
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36 88 ever been employed for the determination of UV filters in sediment samples, especially
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38 89 in case of beach sand samples, most probably due to the fact that these are solid
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40 90 samples. Nevertheless, in this type of samples, a leaching process of the target
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42 91 compounds from the matrix sample prior to the DLLME procedure could overcome this
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44 92 drawback.

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46 93 In this sense, the aim of this paper is to draw on the high potential of the DLLME
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48 94 to develop a rapid, selective and sensitive method for the determination in beach sand
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50 95 samples of eight typical organic UV filters (Table 1). The developed method, which is
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52 96 expected to be used in environmental surveillance studies, is based on the leaching of
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54 97 the analytes from the sand sample prior to DLLME and followed by GC-MS analysis.
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57 99 <Table 1>
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101 2. Experimental

102 2.1. Reagents and samples

103 2-Ethylhexyl salicylate (ES) 99%, 2-hydroxy-4-methoxybenzophenone
104 (benzophenone-3 (BZ3)) 98%, 2-ethylhexyl 4-methoxycinnamate (EMC) 99.8% and 2-

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3 105 ethylhexyl 4-(dimethylamino)benzoate (ethylhexyl dimethyl PABA (EDP)) 98% from
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5 106 Sigma-Aldrich, 3,3,5-trimethylcyclohexyl salicylate (homosalate (HS)) >98% from Merck
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7 107 (Darmstadt, Germany), isoamyl 4-methoxycinnamate (IMC) 99.3% from Haarmann and
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9 108 Reimer (Parets del Vallés, Spain), 3-(4'-methylbenzylidene)camphor (MBC) 99.7%
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11 109 from Guinama S.L. (Valencia, Spain) and 2-ethylhexyl 2-cyano-3,3-diphenylacrylate
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13 110 (octocrylene (OCR)) >98% from F.Hoffman-La Roche Ltd. (Basel, Switzerland) were
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15 111 used as standards. Deuterated benzophenone (benzophenone-d₁₀ (BZ-d₁₀)) 99% from
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17 112 Isotec (Miamisburg, Ohio, USA) was used as surrogate to minimize possible deviations
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19 113 occurred during the DLLME and GC injection processes.

114 LC-grade absolute ethanol from Scharlau Chemie (Barcelona, Spain) was used
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116 as solvent to prepare the multicomponent and surrogate standard stock solutions.
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118 Analytical reagent-grade acetone also from Scharlau Chemie was used as solvent to
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120 prepare the working standard solutions and as leaching/disperser solvent. Analytical
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122 reagent-grade chloroform from Scharlau Chemie was used as extraction solvent. De-
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124 ionized water, obtained by means of a NANOpure II water purification system from
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126 Barnstead (Boston, USA), was used as supporting solvent in the DLLME process.

127 Analytical reagent-grade sodium chloride (NaCl) 99.5% from Scharlau Chemie
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129 was used to adjust the ionic strength of the DLLME aqueous supporting solutions.
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131 Sodium dihydrogen phosphate (NaH₂PO₄) and phosphoric acid (H₃PO₄), both also from
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133 Scharlau Chemie, were used to adjust the pH of these solutions.

134 High-purity helium (99.9999%) from Carburos Metálicos S.A. (Paterna, Spain)
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136 was used as carrier gas in the GC-MS system.

137 Sand samples were all collected from the beach shore of different Spanish
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139 beaches located in Valencia (Sample 1: *Malvarrosa beach* (June 2013); Sample 2:
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141 *Pinedo beach* (June 2013); Sample 3: *Patacona beach* (July 2013)) and Gran Canaria
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143 Island (Sample 4: *Los ingleses beach*, (August 2011)). An additional sand sample from
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145 *Malvarrosa beach* collected away from the shore and out of beach season (February
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147 2013) was used as blank. All they were stored in the dark and dried at 60 °C in
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149 porcelain capsules overnight before sample analysis.
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156 2.2. Apparatus

157 A Focus GC gas chromatograph, equipped with an AS 3000 autosampler and
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159 coupled to a DSQ II mass spectrometric detector (operated in positive electron
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161 ionization mode at ionization energy of 70 eV, with a multiplier voltage set at 1300 V),
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163 from Thermo Fisher Scientific (Austin, TX, USA) was employed.

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3 140 A Hettich (Tuttlingem, Germany) EBA 21 centrifuge and a Crison (Alella, Spain)
4 141 Basic 20 pH meter were used in sample treatment. An ultrasound bath (50 Hz, 360 W)
5 142 from J.P. Selecta S.A. (Barcelona, Spain) was also used in the leaching optimization.
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11 144 **2.3. Proposed method**

12 145 Multicomponent and surrogate standard stock solutions were prepared separately
13 146 in ethanol at 500 and 1000 $\mu\text{g mL}^{-1}$, respectively. From these solutions,
14 147 multicomponent and surrogate solutions were prepared daily in acetone at 2 and 10 μg
15 148 mL^{-1} , respectively. Calibration standard solutions (10-50 ng mL^{-1}) in acetone, containing
16 149 40 ng mL^{-1} of surrogate, were also prepared daily. An additional 40 ng mL^{-1} surrogate
17 150 solution in acetone was prepared as blank. These solutions were subjected to the
18 151 DLLME procedure.
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24 152 Besides, by triplicate, 10 g of dry sand sample were weighted and placed into 50
25 153 mL screw cap glass centrifuge tubes with conic bottom. Then, 20 μL of the surrogate
26 154 solution were added in all cases (i.e., at 20 ng g^{-1}). The mixture was homogenized and
27 155 left to solvent evaporation. A volume of 5 mL of acetone was added and the tube was
28 156 vigorously shaken with vortex mixer during 20 s and centrifuged at 5000 rpm for 10
29 157 min. The supernatant (ca. 2 mL) was separated, and this operation was repeated twice
30 158 with 1 mL of acetone. Then, the supernatants of each sample were merged in a 5 mL
31 159 volumetric flask and acetone was added up to the mark. After that, an aliquot was
32 160 filtered through 0.45 μm nylon membrane filters and subjected to the DLLME
33 161 procedure.
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43 163 **2.3.1. DLLME procedure**

44 164 Different aliquots of 5 mL of deionized water, used as supporting solvent, were
45 165 adjusted to pH 4 and placed into 7.5 mL screw cap glass centrifuge tubes. Then, 2 mL
46 166 of the acetone standard solutions (or sample extracts) containing 60 μL of chloroform,
47 167 were rapidly injected into the water. The formed cloudy solutions were vigorously
48 168 shaken with vortex mixer during 5 s. Finally, they were centrifuged at 3000 rpm for 3
49 169 min for phase separation. The sedimented phases were collected and transferred into
50 170 1.5 mL GC injection vials.
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60 172 **2.3.2. GC-MS analysis**

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3 173 Two μL of each one of the aforementioned sedimented phases were injected into
4 174 the GC injection port set at $280\text{ }^{\circ}\text{C}$ in splitless mode, and run at 1 mL min^{-1} helium
5 175 constant flow rate by using a HP-5MS Ultra Inert (95% dimethyl-5%
6 176 diphenylpolysiloxane, 30 m length, 0.25 mm i.d., $0.25\text{ }\mu\text{m}$ film thickness) column from
7 177 Agilent Technologies (Palo Alto, CA, USA). The oven temperature program was: from
8 178 $70\text{ }^{\circ}\text{C}$ (1 min) to $170\text{ }^{\circ}\text{C}$ at $10\text{ }^{\circ}\text{C min}^{-1}$, then to $200\text{ }^{\circ}\text{C}$ at $2\text{ }^{\circ}\text{C min}^{-1}$ and finally to $280\text{ }^{\circ}\text{C}$
9 179 (6 min) at $10\text{ }^{\circ}\text{C min}^{-1}$. The transfer line and ion source temperatures were set at 280
10 180 $^{\circ}\text{C}$ and $250\text{ }^{\circ}\text{C}$, respectively. The chromatograms were recorded in selected ion
11 181 monitoring (SIM) mode at the mass/charge (m/z) ratios shown in Table 2.
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25 183 <Table 2>
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35 185 Figure 1 shows, as an example, the obtained chromatogram for a sand blank spiked
36 186 with the target compounds at 20 ng g^{-1} and subjected to the described DLLME-GC-MS
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191 **3. Results and discussion**

192 **3.1. Study of the experimental variables involved in the DLLME procedure**

193 Different variables may affect the DLLME process, such as the type and volume
194 of both extraction and disperser solvents, and the pH and ionic strength of the aqueous
195 phase [25]. The influence of all these variables was evaluated in terms of the analytical
196 signal (i.e. chromatographic peak area of each target analyte).
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As the DLLME is carried out after the analytes leaching, the leaching solvent was also employed as disperser solvent in DLLME in order to make compatible both techniques. Thus, unlike conventional DLLME, in this case the disperser solvent, instead of the aqueous phase, contains the target compounds. The aqueous phase is not used as donor phase but as supporting solvent to make the DLLME possible (i.e., to form the cloudy solution and to transfer the analytes to the extraction solvent). Hence, a multicomponent solution of 100 ng mL^{-1} of the target analytes was employed as disperser solvent in the different DLLME studies. Later, the mixture of disperser and extraction solvent were injected into 5 mL of deionized water.

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3 206 The extraction time was not studied in this work because it is well known that in
4 207 this extraction technique the surface area between the extraction solvent and the
5 208 aqueous phase is infinitely large so the transfer of the analytes is fast. The equilibrium
6 209 state is achieved quickly and the extraction time is very short. This is the most
7 210 important advantage of DLLME technique [25].

11 211 The surrogate (BZ-d₁₀) was not used to perform the DLLME optimization since it
12 212 could be affected in the same or different way as analytes and could provide wrong
13 213 conclusions.
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19 215 *3.1.1. Study of the extraction solvent and disperser solvent*

21 216 The combination of the extraction solvent and the disperser solvent is an
22 217 important issue in the DLLME process that requires an exhaustive study prior to the
23 218 final selection. The extraction solvent should extract the target analytes efficiently and
24 219 have low solubility in the aqueous phase. Moreover, as only a few microliters of
25 220 extraction solvent are employed, a solvent with a higher density than water is
26 221 recommended in order to remain in the bottom of the extraction tube and ease its
27 222 collection. On the other hand, the disperser solvent should be miscible in both the
28 223 supporting aqueous solution and the organic extraction solvent, and has also to form
29 224 the so-called cloudy solution. Moreover, after centrifugation, a phase separation has to
30 225 be achieved. In this sense, dichloromethane and chloroform were studied as extraction
31 226 solvents, and acetone, acetonitrile and ethanol were studied as disperser solvents.

34 227 Therefore, a bivariate study considering all the possible combinations was
35 228 performed. For this purpose, mixtures of 1 mL of each disperser solvent (940 μ L) with
36 229 each extraction solvent (60 μ L) were injected into 5 mL of deionized water. When
37 230 dichloromethane was used as extraction solvent, no cloudy solution was formed.
38 231 Furthermore, when the combination ethanol-chloroform was tested, no phase
39 232 separation occurred after centrifugation. The best results were accomplished when the
40 233 mixture acetone-chloroform was used. Thus, acetone and chloroform were selected as
41 234 disperser and extraction solvents, respectively, for further studies.
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55 236 *3.1.2. Effect of the disperser solvent volume*

57 237 As the disperser solvent contains the target analytes, the higher the volume of
58 238 acetone injected the higher will be the amount of analyte extracted. Thus, mixtures of
59 239 different volumes of the acetone standard solution and 60 μ L of chloroform, with a total

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3 240 mixture volume ranging from 0.5 to 5 mL, were tested. Volumes above 2 mL
4 241 redounded in no phase separation. Therefore, a total volume mixture of 2 mL (1940 μ L
5 242 of disperser solvent in this case) was finally chosen.
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10 244 3.1.3. Effect of the extraction solvent volume

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12 245 When the extraction solvent volume is increased, the amount of extracted analyte
13 246 is expected to increase too, but it should be taken into account that the dilution effect is
14 247 also increased. Thus, a careful study is needed in order to achieve the best results.
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18 248 In this sense, mixtures of chloroform (ranging from 40 to 120 μ L) and the
19 249 disperser solvent, with a total volume of 2 mL were tested. 40 μ L of chloroform was
20 250 disregarded because there was no phase separation. The rest of the results are plotted
21 251 in Figure 2, which shows that the higher analytical signals were obtained when the
22 252 smaller extraction solvent volume was employed, probably due to the dilution effect.
23 253 Thus, 60 μ L of extraction solvent was employed in the subsequent experiments.
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<Figure 2>

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33 257 3.1.4. Effect of the pH of the supporting aqueous solution

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35 258 The influence of the pH of the supporting aqueous solution on the extraction
36 259 efficiency was studied. Different aqueous solutions were adjusted to pH values ranging
37 260 from 2 to 8. For non-ionisable compounds (i.e., IMC, 4-MBC, EMC and OCR) no
38 261 significant changes were observed. In case of phenolic compounds such as ES, HS
39 262 and BZ3 are better extracted at acidic pH rather than alkaline pH, since at acidic pH
40 263 their phenolic moieties are not ionized and the extraction is favoured. However, the
41 264 extraction of EDP is not favoured at very low pH since its amine moiety is protonated
42 265 (and thus charged). In summary, the best responses were obtained at mild acidic pHs
43 266 rather than high pHs. Hence, the aqueous solutions employed as supporting solvent
44 267 were adjusted to pH 4 before the injection of the disperser-extraction solvent mixture.
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51 269 3.1.5. Effect of the ionic strength of the supporting aqueous solution

52 270 In general terms, the addition of salt reduces the solubility of the organic
53 271 compounds in water and forces them to pass to the extraction solvent improving the
54 272 extraction efficiency (*salting-out* effect). Thus, in order to study this effect, NaCl was
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3 273 added to the supporting aqueous solution at concentration values up to 15 % (m/v). For
4 274 saline contents of 10 to 15 % the extraction solvent floated on the aqueous phase as
5 275 an extremely thin layer, with the subsequent difficulty to collect it. For this reason NaCl
6 276 contents higher than 7.5% were discarded. Figure 3 shows that the higher was the ionic
7 277 strength the lower were the responses. This could be explained by the fact that
8 278 increasing the saline content of the aqueous phase significantly increases the volume
9 279 of the sedimented phase obtained (from 20 to 70 μL). The obtained results indicate that
10 280 the dilution becomes more important than the *salting-out* effect for this case. Therefore,
11 281 the ionic strength of the supporting aqueous solution was not adjusted in further
12 282 experiments.

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26 286 **3.2. Study of the experimental variables involved in the leaching procedure**

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28 287 For the determination of the UV filters in sand samples by DLLME, firstly, is
29 288 necessary to leach them from the solid matrix. The leaching solvent volume and vortex
30 289 mixer time were studied to achieve the higher analytical responses. A sand blank
31 290 sample spiked with 100 ng g^{-1} of the target analytes was employed to carry out this
32 291 study.

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37 292 As in the case of DLLME study, the surrogate was not employed in the leaching
38 293 study since it could be affected in the same or different way as analytes and could lead
39 294 to wrong conclusions.

40 41 42 43 44 296 **3.2.1. Effect of the leaching solvent type**

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46 297 The selection of the leaching solvent is a critical variable since the leaching and
47 298 the DLLME processes must be compatible. On one hand, it should effectively leach the
48 299 target analytes to the samples and, on the other hand, behave as a good disperser
49 300 solvent in the DLLME. For the last reason, acetone was selected as leaching solvent
50 301 because of the results obtained in 3.1.1.

51 52 53 54 55 56 57 303 **3.2.2. Effect of the leaching solvent volume**

58 304 The influence of the leaching solvent volume in the analytical signal was
59 305 studied. For this purpose, different volumes ranged from 5 to 20 mL of acetone were

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3 306 added to the spiked sand blanks placed into the 50 mL screw cap glass centrifuge
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5 307 tubes. After that, the tubes were vigorously shaken with vortex mixer during 5 s and
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7 308 centrifuged at 5000 rpm for 10 min. The supernatant acetone was collected with a
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9 309 syringe and filtered through 0.45 μm nylon membrane filters. Then, the acetone-
10 310 chloroform mixture was prepared and subjected to the DLLME process (see section
11 311 2.3.1). As can be seen in Figure 4 the analytical signal decreases when the volume of
12 312 acetone is increased. This is due to the dilution of the target analytes in the leached
13 313 phase. Volumes below 5 mL did not provide satisfactory results, since a high amount of
14 314 acetone remained soaking the sand sample. Then, the volume of acetone employed in
15 315 the leaching process in further experiments was 5 mL. Nevertheless, two additional
16 316 consecutive extractions with 1 mL of acetone each were carried out in order to increase
17 317 the extraction efficiency (see Section 3.4).

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319 <Figure 4>

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321 **3.2.3. Effect of the vortex mixer agitation time**

322 The vortex mixer agitation time was studied up to 60 s. The results are shown in
323 Figure 5. As can be seen, shaking times longer than 20 s did not provide better
324 responses. Therefore, 20 s were selected for further experiments.

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326 <Figure 5>

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328 Besides, it is worth remarking that direct evaporation of the leaching solvent
329 after the leaching of the analytes from the sand sample instead of carrying out the
330 DLLME process was tested. The residue obtained after the evaporation was
331 redissolved in a low volume of chloroform (50 μL) and injected into the GC-MS system.
332 Although this methodology is simpler, worse results were achieved since the analytical
333 signals observed for the analytes were considerably lower than those obtained when
334 the DLLME process was carried out. It could be attributed to losses during the
335 evaporation or to the adsorption into the walls of the evaporation tube. Moreover, it
336 should be emphasized that an additional clean-up is achieved by DLLME.

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338 **3.3. Use of surrogate**

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3 339 In order to reduce the variability of the measurements, especially caused by the
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5 340 GC injection and the handling of low volumes in the DLLME process, the use of
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7 341 deuterated benzophenone, i.e., benzophenone-d₁₀ (BZd₁₀), as surrogate was
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9 342 considered. Thus, A_i/A_{sur} (where A_i is the peak area of the target analyte and A_{sur} that of
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11 343 the surrogate) was used as response function for quantification purposes. BZ-d₁₀ was
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13 344 selected for various reasons: (1) it is extractable in chloroform by the DLLME proposed
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15 345 method; (2) its volatility is suitable to be measured by GC; (3) as it is a deuterated
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17 346 compound, its possible presence in the environmental samples is nil, on the contrary of
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19 347 its non-deuterated homologous; and (4) it does not present ionisable functional groups
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21 348 in its structure, and thus, its extraction is not influenced by pH. Thus internal calibration
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23 349 was used instead of external calibration.

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351 **3.4. Study of matrix effects and leaching efficiency**

352 In order to evaluate matrix effects, the following experiments were performed by
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354 triplicate: on one hand, a dried sand blank was subjected to the leaching process. After
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356 centrifugation, 2 mL of the supernatant were spiked with the target analytes at 200 ng
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358 mL⁻¹ and the surrogate at 100 ng mL⁻¹; on the other hand, 2 mL of an acetone standard
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360 solution containing the analytes and surrogate at the same concentration than the
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362 above-mentioned solution was also prepared. Both solutions were subjected to the
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364 DLLME and measured in the GC-MS system. The obtained recoveries were 80±12,
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366 94±7, 86±11, 92±6, 106±15, 82±9, 84±12 and 95±12 % for ES, HS, IMC, MBC, BZ3,
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368 EMC, EDP and OCR, respectively. These results show that matrix effects caused by
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370 the sand sample are negligible.

371 In order to evaluate the leaching efficiency, the following experiments were
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373 performed in triplicate: on one hand, a dried sand blank was spiked with the target
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375 analytes at 100 ng g⁻¹, and subjected to the leaching process. After centrifugation, 2 mL
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377 of the supernatant were collected and spiked with the surrogate at 100 ng mL⁻¹. On the
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379 other hand, the same dried sand blank was subjected to the leaching process, and
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381 after centrifugation, 2 mL of the supernatant were spiked with the target analytes at 200
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383 ng mL⁻¹, in order to simulate 100% leaching efficiency, and then with the surrogate at
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385 100 ng mL⁻¹. All these solutions were subjected to the DLLME and measured in the
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387 GC-MS system. The leaching efficiencies obtained were below 70%. The experiments
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389 were repeated by performing two additional consecutive extractions with 1 mL of
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391 acetone each. The results showed that the extraction efficiency increased, but not
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393 quantitatively, since the target analytes partially remained in the acetone soaking the

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3 374 sand sample. Then, an additional experiment was carried out in the same way to a
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5 375 dried sand blank spiked with the target analytes at 100 ng g^{-1} but also with the
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7 376 surrogate at 50 ng g^{-1} , and then subjected to the leaching process. After centrifugation,
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9 377 2 mL of the supernatant were collected and subjected to the DLLME process. The
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11 378 results revealed quantitative apparent extraction efficiencies for all the target
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13 379 compounds (i.e., 105 ± 14 , 96 ± 9 , 104 ± 10 , 84 ± 9 , 87 ± 4 , 96 ± 14 , 100 ± 14 and 104 ± 14 % for
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15 380 ES, HS, IMC, MBC, BZ3, EMC, EDP and OCR, respectively) if the surrogate was
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17 381 added before the leaching process. These results show that the losses during the
18
19 382 leaching process, presumably due to the volume of acetone cannot be totally
20
21 383 recovered, are corrected with the use of the surrogate.

22
23 384 Based on these both experiments, it can be concluded that internal calibration,
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25 385 using standard solutions of the target compounds and surrogate in acetone can be
26
27 386 used. In the case of samples, they need to be spiked with the surrogate before the
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29 387 leaching and DLLME processes.

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32 33 389 **3.5. Study of the drying temperature**

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35 390 In order to remove the water in the beach sand samples, which could affect the
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37 391 leaching and/or the DLLME processes, they must be dried. However, this could
38
39 392 redound in analyte losses due to their volatilization and/or degradation. In this sense,
40
41 393 the drying temperature was studied. Preliminary studies showed that several hours at
42
43 394 around $100 \text{ }^\circ\text{C}$ were needed to dry the samples. Therefore, in duplicate, a dried sand
44
45 395 blank sample was spiked with 100 ng g^{-1} of the target analytes using an acetone
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47 396 standard solution. It was homogenized and left to evaporate at room temperature.
48
49 397 Then, it was divided into three portions; one of them was left overnight at room
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51 398 temperature whereas the other two were left at $60 \text{ }^\circ\text{C}$ and $100 \text{ }^\circ\text{C}$, respectively. Later,
52
53 399 they were subjected to the proposed method. Results (Figure 6) show that losses were
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55 400 significant at $100 \text{ }^\circ\text{C}$, whereas they were negligible at $60 \text{ }^\circ\text{C}$. Thus, samples were dried
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57 401 at this temperature.

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59 402

60 1 403 **3.6. Analytical figures of merit of the proposed DLLME-GC-MS method**

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3 404 The quality parameters of the proposed method, such as enrichment factor,
4
5 405 linearity, method limits of detection (MLOD) and quantification (MLOQ), and intra- and
6
7 406 inter-day precision, were evaluated under the final optimized conditions. The results
8
9 407 are summarized in Table 3.

1
2
3 408 The enrichment factors (EF) obtained for the DLLME process (defined as $EF =$
4 409 C_{sed}/C_0 , where C_{sed} is the concentration of the target compound in the organic
5 410 sedimented phase and C_0 is the initial concentration of this compound, in this case, in
6 411 the disperser solvent) ranged from 8.2 ± 0.7 (OCR) to 50 ± 4 (BZ3) (Table 3). The
7 412 maximum EF value that could be obtained, corresponding to a total transfer of the
8 413 target analytes from the disperser solvent to the extraction solvent, is calculated as
9 414 V_0/V_{sed} , where V_0 is the disperser solvent volume and V_{sed} the sedimented phase
10 415 volume. In the present work, V_0 corresponds to 2 mL and the V_{sed} obtained was around
11 416 25 μL . Thus, the maximum EF value that could be obtained in the present method
12 417 corresponds to values around 80. Although the values obtained for some of the target
13 418 compounds are relatively low, especially for OCR, it should not be forgotten that also
14 419 an additional clean-up is achieved when the DLLME is performed.

15 420 The linearity was studied by measuring standard solutions in acetone containing
16 421 the surrogate at 40 ng mL^{-1} , which were subjected to the DLLME process. A solution of
17 422 the surrogate in acetone at 40 ng mL^{-1} was also analyzed as blank. Calibration curves
18 423 were plotted using the ratio of the peak area of each target analyte to the surrogate
19 424 (A_i/A_s) versus the analyte concentration. Results indicated that linearity reached at
20 425 least 1000 ng mL^{-1} for all the target compounds. However, due to the low concentration
21 426 levels expected for the target analytes, the calibration range was set from 10 to 50 ng
22 427 mL^{-1} . The calibrations parameters are shown in Table 3 and reveal a high level of
23 428 linearity in all cases.

24 429 The method limit of detection (MLOD) and quantification (MLOQ) of the target
25 430 analytes are also shown in Table 3. As can be seen, the MLODs and MLOQs values
26 431 were found to be in the pg g^{-1} level ranging from 18 ± 1 to $53 \pm 6 \text{ pg g}^{-1}$ and from 61 ± 5 to
27 432 $180 \pm 20 \text{ pg g}^{-1}$, respectively, which shows that the proposed method is suitable to
28 433 determine these compounds at trace levels.

29 434 The precision of the method was evaluated applying the proposed method to a
30 435 sand blank spiked at three concentration levels of the target analytes (5, 20 and 50 ng
31 436 g^{-1}) and the surrogate at 20 ng g^{-1} , during the same working session (intra-day
32 437 precision) or in different working sessions (inter-day precision). Results, expressed as
33 438 relative standard deviation (RSD) of five measurements, are shown in Table 3 and
34 439 reveal that good precision was achieved for all the target analytes.

35 440

36 441 **3.7. Application of the proposed method to the analysis of real samples**

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2
3 442 Four beach sand samples collected in the summer season were analyzed using
4 443 the proposed DLLME-GC-MS method. Results are shown in Table 4. As can be seen,
5 444 all the samples analyzed contained appreciable amounts of several of the UV filters
6 445 under study. Specifically, the samples with higher content of UV filters (concentration
7 446 and type) were Samples 1 (*Malvarrosa beach*) and Sample 4 (*Los ingleses beach*) in
8 447 accordance with the fact that these beaches are more crowded than the other two.
9 448 Moreover, ES and OCR are the most abundant UV filters in beach sediments samples
10 449 since these compounds are widely employed in sunscreen creams formulations
11 450 nowadays.

12 451 However, it should be noted that the concentration of UV filters found in this
13 452 environmental samples could be highly variable as it depends on the people
14 453 concourse, the number of users of sunscreens products, the water tide and the
15 454 sampling date, among other factors.

16 455 Nevertheless, the data obtained by this method, jointly to those obtained by those
17 456 methods focused in the analysis of water samples, could aid to evaluate the impact of
18 457 the UV filters in the marine ecosystem [36], thus obtaining important conclusions from
19 458 an environmental standpoint.

20 459

21 460 **4. Conclusions**

22 461 A sensitive analytical method based on vortex-assisted leaching followed by
23 462 DLLME and GC-MS determination is proposed to determine eight fat-soluble UV filters
24 463 at trace levels in beach sand samples.

25 464 The study of the matrix effects and the leaching efficiency reveal that internal
26 465 calibration using standard solutions of the target compounds and surrogate in acetone
27 466 can be used. The beach sediment samples were spiked with the surrogate and
28 467 subjected to both the leaching and DLLME processes.

29 468 Good analytical features, including limits of detection, sensitivity and intra- and
30 469 inter-day precision are obtained.

31 470 The proposed method can be considered both user and environmentally-friendly
32 471 since although organic solvents are necessary to carry out the extraction process, their
33 472 amounts have been minimized by the use of the DLLME procedure.

34 473 The proposed method was successfully applied to the analysis of four samples
35 474 from different origin. In all cases, ES and OCR are the UV filters found at higher

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3 475 concentration. This is a reasonable fact taking into account that these are two of the
4
5 476 most commonly used UV filters in cosmetic formulations today.
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7 477 Finally, it should be said that the proposed method can be used from an
8
9 478 environmental surveillance standpoint to evaluate the fate of these emerging pollutants
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11 479

12 13 480 **Acknowledgements**

14
15 481 Authors acknowledge the financial support of the Spanish Government (Project
16
17 482 CTQ2009-12709) and of the University of Valencia (Project UV-INV-AE13-137567). I.T.
18
19 483 also likes to thank the Generalitat Valenciana for her predoctoral grant.
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3 **Figure captions.**
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8 **Fig. 1** A chromatogram obtained applying the proposed DLLME-GC/MS method to a
9 sand blank spiked with 20 ng g⁻¹ of the target analytes and the surrogate (BZ-d₁₀) (see
10 text for experimental details)
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13
14 **Fig. 2** Effect of the extraction solvent volume on the DLLME process (extraction
15 conditions: 5 mL of deionized water solution, mixtures of 2 mL of acetone containing
16 100 µg L⁻¹ of the target analytes as disperser solvent and chloroform as extraction
17 solvent, with different volumes of chloroform)
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22 **Fig. 3** Effect of the ionic strength of the aqueous phase on the DLLME process
23 (extraction conditions: 5 mL of deionized water adjusted at pH 2-4 and at different ionic
24 strength values, 1940 µL of acetone containing 100 µg L⁻¹ of the target analytes as
25 disperser solvent mixed with 60 µL of chloroform as extraction solvent)
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30 **Fig. 4** Effect of the leaching solvent volume on the analytical signal (leaching
31 conditions: 10 g of sand blank spiked with the target analytes at 100 µg L⁻¹, different
32 acetone volumes and 5 s of vortex mixer agitation)
33
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37 **Fig. 5** Effect of the vortex mixer agitation time on the analytical signal (leaching
38 conditions: 10 g of sand blank spiked with the target analytes at 100 µg L⁻¹, 5 mL of
39 acetone and different times of vortex mixer agitation)
40
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43
44 **Fig. 6** Effect of the drying temperature on the analytical signal (see text for
45 experimental conditions. A_i/A_S corresponds to the ratio of the peak area of each target
46 analyte to the surrogate (BZ-d₁₀))
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Fig. 1

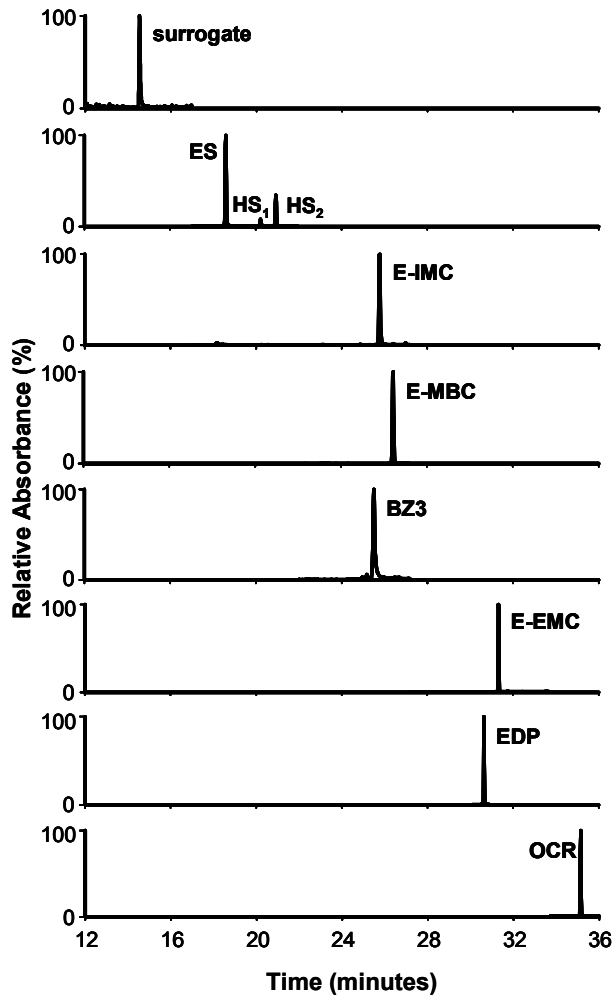


Fig. 2

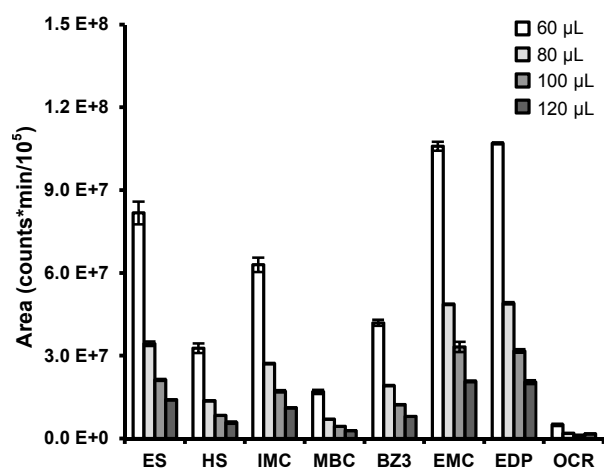


Fig. 3

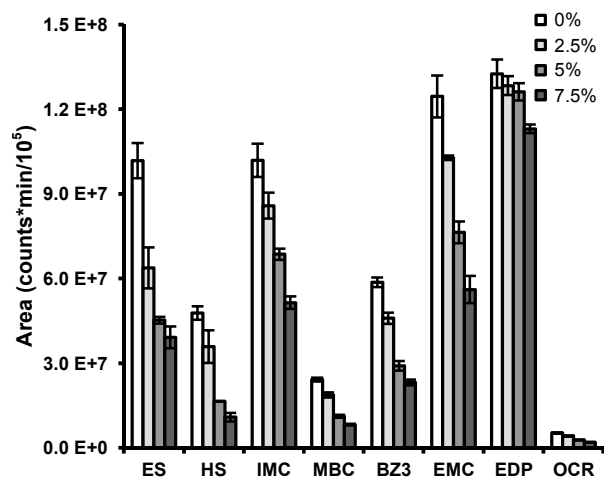


Fig. 4

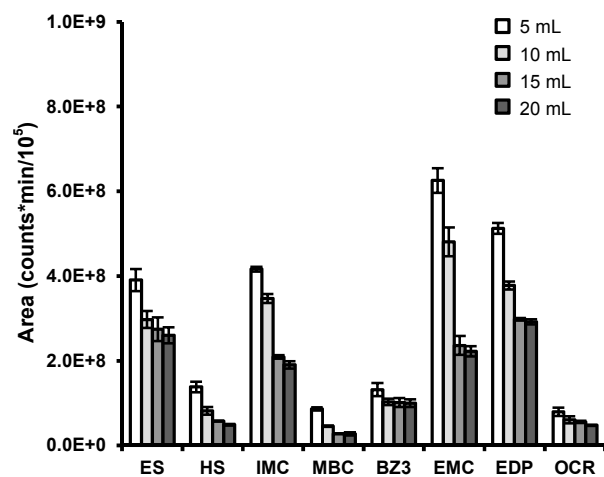


Fig. 5

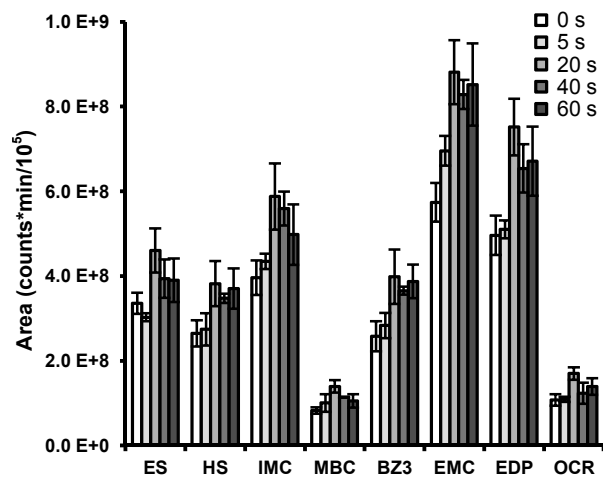


Fig. 6

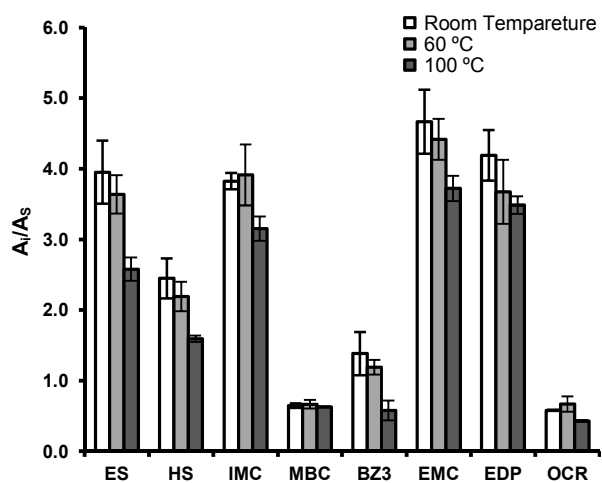
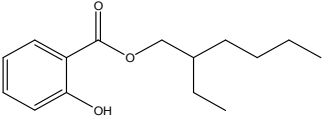
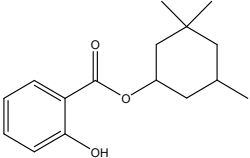
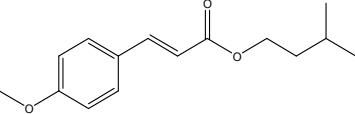
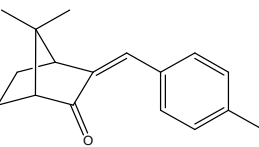
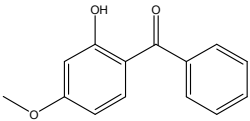
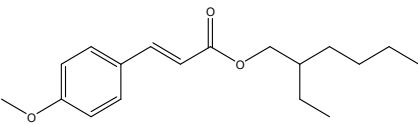
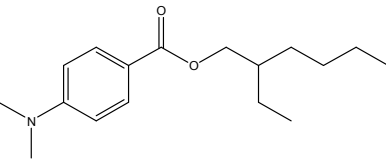
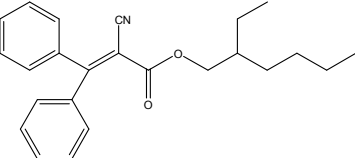


Table 1. Chemical structure and some data of the target compounds.

| UV filter | Chemical structure | Molecular formula | CAS number |
|--|--|---|------------|
| 2-ethylhexyl salicylate (ES) |  | C ₁₅ H ₂₂ O ₃ | 118-60-5 |
| Homosalate (HS) ^a |  | C ₁₆ H ₂₂ O ₃ | 118-56-9 |
| Isoamyl 4-methoxycinnamate (IMC) ^b |  | C ₁₅ H ₂₀ O ₃ | 71617-10-2 |
| 3-(4-methylbenzylidene) camphor (4-MBC) ^b |  | C ₁₈ H ₂₂ O | 36861-47-9 |
| Benzophenone-3 (BZ3) |  | C ₁₄ H ₁₂ O ₃ | 131-57-7 |
| 2-ethylhexyl 4-methoxycinnamate (EMC) ^b |  | C ₁₈ H ₂₆ O ₃ | 5466-77-3 |
| Ethylhexyl dimethyl PABA (EDP) |  | C ₁₇ H ₂₇ NO ₂ | 21245-02-3 |
| Octocrylene (OCR) |  | C ₂₄ H ₂₇ NO ₂ | 6197-30-4 |

^a There are two isomers (HS₁ and HS₂).

^b There are two geometrical isomers (Z and E) when exposed to light.

Table 2. GC-MS features of the target compounds.

| UV filter | Retention time (min) | m/z ^a | Acquisition time window (min) |
|-----------------------------------|--|-----------------------|-------------------------------|
| BZ-d ₁₀ (surrogate) | 14.44 | 82, 110 , 192 | 10.0-17.0 |
| ES | 18.45 | 120 , 138, 250 | 17.0-22.0 |
| HS | 20.04 (<i>HS</i> ₁), 20.75 (<i>HS</i> ₂) | 120, 138 , 262 | 17.0-22.0 |
| IMC | 21.20 (<i>Z</i>), 25.54 (<i>E</i>) | 161, 178 , 248 | 20.0-27.2 |
| MBC | 24.50 (<i>Z</i>), 26.23 (<i>E</i>) | 128, 211, 254 | 22.0-27.2 |
| BZ3 | 25.33 | 151, 227 , 228 | 22.0-27.2 |
| EMC | 29.78 (<i>Z</i>), 31.22 (<i>E</i>) | 161, 178 , 290 | 27.2-30.0 31.0-33.7 |
| EDP | 30.62 | 148, 165 , 277 | 30.0-31.0 |
| OCR | 35.04 | 204 , 232, 360 | 33.7-40.0 |

^a The m/z values used as quantifiers are shown in bold.

Table 3. Main analytical parameters of the proposed DLLME-GC-MS method.

| UV filter | EF ^a | Slope ^b ± deviation (ng ⁻¹ mL)/ 10 ⁵ | Regression coefficient (r ²) ^b | MLOD ^c (pg g ⁻¹) | MLOQ ^d (pg g ⁻¹) | Precision, RSD ^e (%) | | | | | |
|-----------|-----------------|--|---|--|--|---------------------------------|-----------------------|-----------------------|----------------------|-----------------------|-----------------------|
| | | | | | | Intra-day | | | Inter-day | | |
| | | | | | | 5 ng g ⁻¹ | 20 ng g ⁻¹ | 50 ng g ⁻¹ | 5 ng g ⁻¹ | 20 ng g ⁻¹ | 50 ng g ⁻¹ |
| ES | 25 ± 2 | 4900 ± 200 | 0.995 | 38 ± 5 | 130 ± 20 | 14 | 8 | 6 | 16 | 8 | 7 |
| HS | 19 ± 1 | 4000 ± 100 | 0.997 | 53 ± 6 | 180 ± 20 | 13 | 9 | 5 | 15 | 9 | 8 |
| IMC | 38 ± 3 | 6100 ± 200 | 0.998 | 41 ± 5 | 140 ± 20 | 11 | 6 | 4 | 14 | 7 | 6 |
| MBC | 42 ± 2 | 1140 ± 70 | 0.997 | 29 ± 2 | 96 ± 8 | 10 | 8 | 5 | 13 | 8 | 7 |
| BZ3 | 50 ± 4 | 2000 ± 100 | 0.997 | 41 ± 5 | 140 ± 20 | 11 | 5 | 4 | 11 | 10 | 7 |
| EMC | 21 ± 2 | 9200 ± 500 | 0.9991 | 18 ± 1 | 61 ± 5 | 9 | 7 | 8 | 12 | 9 | 9 |
| EDP | 31 ± 3 | 8100 ± 500 | 0.998 | 46 ± 9 | 150 ± 30 | 7 | 7 | 5 | 15 | 12 | 8 |
| OCR | 8.2 ± 0.7 | 1700 ± 100 | 0.997 | 35 ± 3 | 117 ± 9 | 7 | 7 | 7 | 13 | 11 | 10 |

^a EF: Enrichment factor, as the mean of three replicates.

^b Working range: 10-50 ng mL⁻¹. Number of calibration points: 6.

^c MLOD: method limit of detection, calculated as 3 times the signal-to-noise ratio.

^d MLOQ: method limit of quantification, calculated as 10 times the signal-to-noise ratio.

^e Relative standard deviation (RSD); five replicate analysis of spiked sand blank at different concentrations of the target analytes during the same working session (intra-day precision) or in different working sessions (inter-day precision)

Table 4. UV filters content found in beach sand samples after applying the proposed DLLME-GC-MS method.

| UV filter | Concentration (ng g ⁻¹) | | | |
|-----------|-------------------------------------|-----------------------|-----------------------|-----------------------|
| | Sample 1 ^a | Sample 2 ^b | Sample 3 ^c | Sample 4 ^d |
| ES | 5.3 ± 0.2 | 2.6 ± 0.2 | 1.8 ± 0.5 | 12 ± 1 |
| HS | 1.8 ± 0.2 | 1.06 ± 0.04 | < LOQ | 4.9 ± 0.7 |
| IMC | 1.3 ± 0.3 | < LOQ | < LOQ | 1.2 ± 0.3 |
| MBC | 0.9 ± 0.1 | < LOQ | < LOQ | 2.0 ± 0.4 |
| BZ3 | 1.0 ± 0.1 | < LOQ | < LOQ | < LOQ |
| EMC | 2.1 ± 0.3 | 0.9 ± 0.2 | < LOQ | 10 ± 1 |
| EDP | < LOQ | < LOQ | < LOQ | < LOQ |
| OCR | 8 ± 1 | 1.7 ± 0.4 | 5.2 ± 0.9 | 25 ± 3 |

^a Sample 1: *Malvarrosa beach* (Valencia, Spain).

^b Sample 2: *Pinedo beach* (Valencia, Spain).

^c Sample 3: *Patacona beach* (Valencia, Spain).

^d Sample 4: *Los ingleses beach* (Gran Canaria Island, Spain).