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22 features make this material abundantly available for industrial applications. C/C
23 composites can be manufactured by different techniques, such as pyrolysis of
24 thermosetting resins, pyrolysis of pitch, and chemical vapor infiltration (CVI) route
25 using hydrocarbon gases [1, 2]. The carbon sources used for the fabrication of C/C
26 composites are fossil fuels and their derivatives. The pyrolysis of these fossil fuels and
27 their derivatives need a high temperature around 1000 °C. However, fossil fuels are
28 subject to depletion, pollution, and environmental hazards as they are consumed.

29 Recently, synthesis of carbonaceous materials by hydrothermal carbonization (HTC)
30 has become an emerging method from the viewpoint of economic, environmental, and
31 societal issues [3]. Biomass is commonly used as carbon source for synthesis of
32 carbonaceous materials by HTC. Biomass is a qualified carbon raw material for the
33 synthesis of valuable carbon materials because it is available in high quality and huge
34 amount, and is an environmental friendly renewable resource. To date, most of the
35 carbon materials prepared by HTC using biomass limit to functional carbonaceous
36 materials, such as carbon sphere [4, 5], nanofiber [6], core-shell structure [7], and so on.
37 As far as we are aware, fabrication of C/C composites by HTC using biomass has never
38 been reported earlier. In this study, we report the C/C composites synthesized by HTC
39 using starch as the carbon source. The microstructure and mechanical properties of the
40 obtained composites were studied.

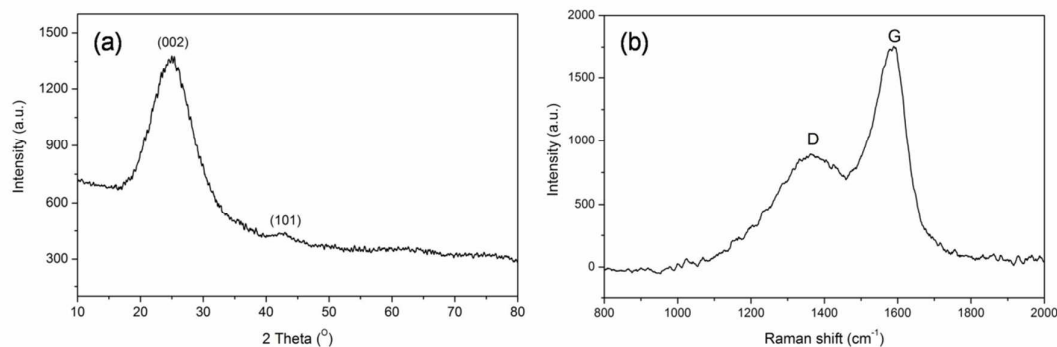
41 **2. Experiments**

42 A needle punched carbon felt with a bulk density of 0.4 g/cm³ was used as preform,
43 which were purchased from the YiXing Tianniao Hight Technology Co ., Ltd. The felts
44 were made up of layers of non-woven carbon fiber cloth and short-cut web after needle-
45 punching step by step. The carbon fiber type of the felts was T300 PAN-based carbon

46 fiber. The received carbon felt was cut into rectangular cuboids with dimension of
47 10×20×40 mm. Starch soluble (Chemically Pure) was employed as the carbon source,
48 which was purchased from the Aladdin industrial corporation. The starch soluble was
49 dissolved in water with a concentration of 54 g/L. A typical cycle of the hydrothermal
50 carbonization process is as follows. Firstly, the cut carbon felt was put into a 100 ml
51 Teflon autoclave and immersed with 50 ml starch solution. Subsequently, the Teflon
52 autoclave was sealed and heated by a microwave accelerated reaction system (MARS-
53 10, SINEO) with a frequency of 2450 MHz and output of 400 W. The heating of the
54 autoclave was performed as follow: (i) heating to 200 °C with a heating rate of 10
55 °C/min; (ii) holding at 200 °C for 120 min; (iii) free-cooling to room temperature. In the
56 temperature holding process, the pressure maintains at 2.0 MPa in the hydrothermal
57 system. Then, the carbon felt was takeout from the cooled autoclave and washed in
58 water to remove the attached materials. Finally, the carbon felt was dried at 80 °C for 6
59 hours. The weight of the treated carbon felt was recorded. The similar process was
60 carried out for 10 cycles to get the densified C/C composites.

61 XRD measurements were performed on a Panalytical X-Pert Pro diffractometer
62 with CuK α monochromatic radiation ($k=1.5406\text{\AA}$). Raman spectra were recorded on a
63 Renishaw RM2000 microspectrometer with 514.5 nm laser excitation. Fourier
64 transform infrared spectroscopy (FTIR) spectra were recorded on a Bruker EQUINOX
65 55 spectrometer. Scanning electron microscopy (SEM) images were taken on a JEOL
66 6390 instrument in vacuum. The sample was coated with platinum before SEM
67 analytical. Flexural strength and flexural elastic modulus of the composites were
68 measured using the three-point bending test with a span of 30 mm.

69 3. Results and discussion



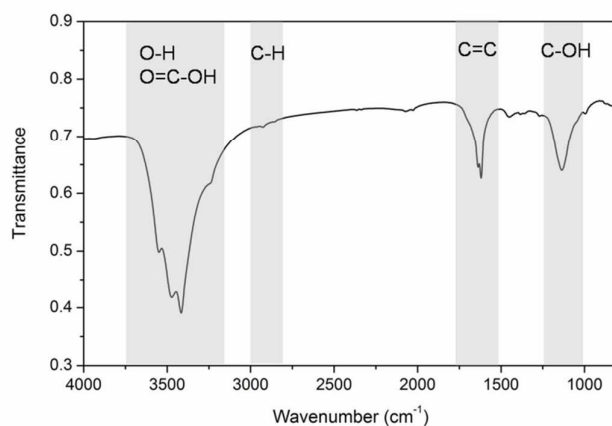
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71 Fig. 1 XRD pattern (a) and Raman spectra (b) of the prepared C/C composites.

72 Fig. 1(a) shows the XRD patterns of the prepared samples. The peaks at
73 approximately 25.3° and 42° correspond to (002) and (101) plane of carbon. The
74 broadening and left-shift of these peaks suggests the presence of an amorphous carbon
75 phase in the prepared C/C composites. Raman spectrum was used to further analyze the
76 structure of the carbon matrix, as shown in Fig. 1(b). The Raman spectrum shows two
77 bands at 1580 and 1353 cm^{-1} , corresponding to the E_{2g} vibration mode of the graphite
78 layers (G-band) and the A_{1g} mode for the disordered graphite structures (D-band),
79 respectively. It is well known that the graphitic degree of carbons is confirmed by the
80 width of I_G peak and the value of I_D/I_G . The I_D/I_G value of carbon matrix is 0.61 which
81 indicates that the carbon matrix is mostly composed of amorphous structure. The XRD
82 and Raman results show that the obtained carbonaceous matrix is an amorphous carbon,
83 which is similar to the carbon sphere obtained by HTC of glucose [8].

84 Fig. 2 shows the FT-IR spectra of the prepared samples. The wide band between
85 3000 and 3700 cm^{-1} is assigned to the stretching vibrations of O-H (hydroxyl or
86 carboxyl), and the bands around 2800 - 3000 cm^{-1} are the characteristic stretching
87 vibrations of aliphatic C-H [9]. The absorption bands at 1698 and 1622 cm^{-1} are
88 attributed to C-O and C=C vibrations, suggesting the aromatization of the samples

89 during the hydrothermal treatment. The bands at 1138 cm^{-1} correspond to C-O
90 (hydroxyl, ester or ether) stretching. These results suggest that functional groups mainly
91 containing -OH and C=O were produced on C/C composites, which are common for the
92 carbonaceous materials prepared by HTC [10].

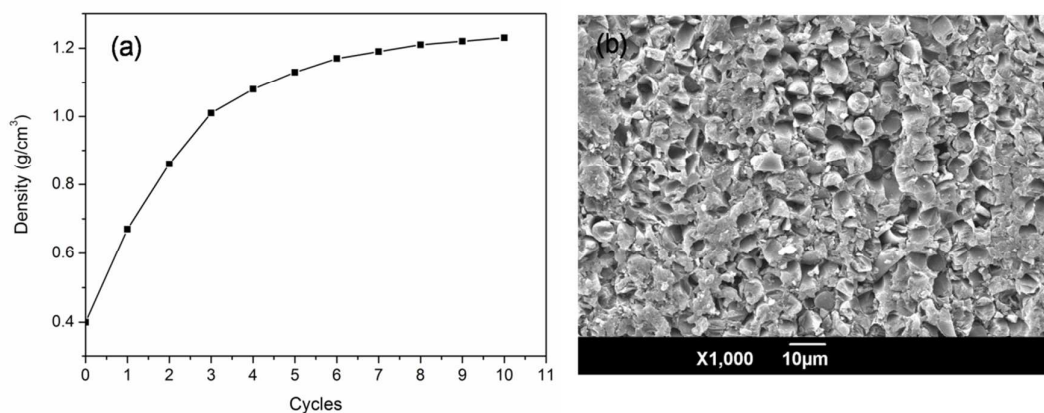


93

94 Fig. 2 FT-IR spectra of the matrix carbon in the prepared C/C composites

95 Fig.3 (a) shows the variation of the composites density with the HTC time. In the
96 initial cycles of the HTC treatment, the density of the composites increases rapidly.
97 With 4 cycles (8 hours) of HTC treatment, the density of the composites reaches about
98 1.0 g/cm^3 . After 10 cycles (20 hours) HTC treatment, the density of composites reaches
99 1.23 g/cm^3 . The open porosity of the C/C composites is 10.9%. These results suggest
100 that HTC is an efficient way for the densification of the C/C composites. The C/C
101 composites prepared by HTC are lighter than the one prepared by CVI, suggesting the
102 density of the HTC carbon is smaller than that of the pyrolytic carbon. Measured by the
103 Archimedes principle, the density of the HTC carbon is about 1.25 g/cm^3 . Fig.3 (b)
104 shows the morphology of the composites after 20 h HTC treatment. Carbonaceous
105 materials fill up the narrow interspaces among the fibers and make the composites dense.

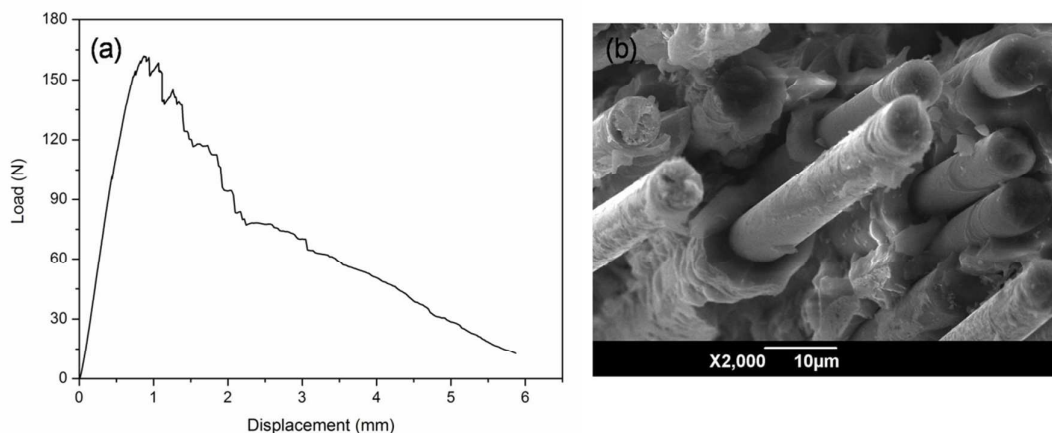
106 The carbon matrix in intimate contact with the carbon fiber suggests the carbon
107 precursor is able to wet the surfaces of the carbon fiber during the HTC process.



108

109 Fig. 3 Variation of the density of the composites with the HTC time (a), and
110 microstructure of the prepared C/C composites (b).

111 Fig.4 (a) shows the load-displacement curves of the composite during flexural test.
112 The fracture of the composites presents a typical pseudo-plastic fracture characterization.
113 An elastic deformation at first occurs under flexural load, and the curve on this stage
114 shows a linear relationship between the strain and the load. Then the deformation
115 transfers to a plastic deformation stage. Meanwhile, the flexural load reaches its
116 maximum and then a stepwise failure occurs. Fiber pull-out can be seen in the fracture
117 surface of the C/C composites, as shown in Fig.4 (b). The surface of the pull-out fiber is
118 rough, suggesting a good bonding between fiber and matrix. The flexural strength and
119 modulus of the composites can reach 146 MPa and 9.6 GPa, respectively. The flexural
120 strength of the C/C composites prepared by HTC is similar to that of the C/C
121 composites prepared by CVI [11, 12]. However, the flexural modulus is lower than that
122 of the of the C/C composites prepared by CVI [11, 12]. These results suggest that the
123 C/C composites fabricated by HTC using biomass can applied in the engineering field.



124

125 Fig. 4 Load-displacement curves (a) and fracture surface (b) of the prepared composites.

126 **4. Conclusion**

127 We fabricate the C/C composites by HTC technique using starch as carbon source
128 successfully. The C/C composites can be densified by 20 hours HTC treatment and get
129 to 1.23 g/cm³ with a porosity of 10.9%. The matrix of the C/C composites is an
130 amorphous carbon functionalized with the hydroxyl and carboxyl groups. The flexural
131 strength and modulus of the composites can reach 146 MPa and 9.6 GPa. This
132 confirmed that the novel C/C composites have potential applications prospect, such as
133 bone substitute materials. HTC, as an economic and environmental-friendly technique,
134 is potential for the fabrication of C/C composites.

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139 **References**

140 [1] Fitzer E, Manocha LM. Carbon Reinforcements and Carbon/Carbon Composites.
141 New York: Springer-Verlag; 1998.

- 142 [2] Delhaès P. Carbon 2002; 40: 641–657.
- 143 [3] Hu B, Wang K, Wu L, Yu SH, Antonietti M, Titirici MM. Adv Mater 2010; 22:
144 813–828.
- 145 [4] Li T, Shen JF, Li N, Ye MX. Mater Lett 2012; 89: 202–205.
- 146 [5] Mi YZ, Hu WB, Dan YM, Liu YL. Mater Lett 2008; 62: 1194–1196
- 147 [6] Qian HS, Yu SH, Luo LB, Gong JY, Fei LF, Liu XM. Chem Mater 2006; 18: 2102–
148 2108.
- 149 [7] Sun X, Li Y. Angew Chem Int Edit 2004; 43: 597–601.
- 150 [8] Zheng M, Liu Y, Jiang K, Xiao Y, Yuan D. Carbon 2010; 48:1224–1233.
- 151 [9] Sevilla M, Fuertes AB. Chem Eur J 2009; 15: 4195–4203.
- 152 [10] Hu B, Yu SH, Wang K, Liu L, Xu XW. Dalton Trans 2008; 40: 5414–5423.
- 153 [11] Hu Y, Luo R, Zhang Y, Zhang J, Li J. Mater Sci Eng A 2010; 527: 797–801
- 154 [12] Chen T, Liao J, Liu G, Zhang F, Gong Q. Carbon 2003; 41: 993–999