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# Enhanced removal of crystal violet from aqueous solutions using BaTiO<sub>3</sub>@ZnO: isotherm, kinetic, and thermodynamic evaluation

Ahmed Barakat,<sup>a</sup> Magdi E. Khalifa,<sup>a</sup> A. M. Abdelghany<sup>bc</sup> and Wael I. Mortada<sup>id</sup>\*<sup>d</sup>

Crystal violet (CV), commonly utilized in various industries, presents risks to both the environment and human health because of its durability and harmful nature. This research discusses the synthesis of a BaTiO<sub>3</sub>@ZnO composite for effectively eliminating CV from aqueous solutions. The composite was produced through a solid-state technique and characterized using XRD, FTIR, SEM-EDX, TEM, BET, and pH<sub>pzc</sub>. The study of CV adsorption involves optimizing various parameters that influence the process, including pH, initial dye concentration, dosage of the adsorbent, contact time, temperature, and ionic strength. The BaTiO<sub>3</sub>@ZnO composite displayed a mesoporous configuration with a surface area of 34.1 m<sup>2</sup> g<sup>-1</sup>, a total pore volume of 0.0354 cm<sup>3</sup> g<sup>-1</sup>, and an average pore radius of 2.53 nm, along with an average crystallite size of 64.58 nm. The experimental data align most closely with the Langmuir isotherm and pseudo-second-order kinetic model, indicating that monolayer adsorption and chemisorption are the main processes involved. The Langmuir isotherm demonstrated a maximum monolayer adsorption capacity of 97.84 mg g<sup>-1</sup> for the BaTiO<sub>3</sub>@ZnO composite. The thermodynamic studies suggest that the adsorption processes are spontaneous and endothermic. The BaTiO<sub>3</sub>@ZnO composite can be effectively recycled and reused for up to ten cycles, maintaining relatively high adsorption capacity despite a gradual decline over successive cycles. This study exhibited the success of doping ZnO into BaTiO<sub>3</sub> to form a composite that possesses enhanced surface area, porosity, and surface charge, thereby making the BaTiO<sub>3</sub>@ZnO composite a promising and efficient adsorbent for CV removal in industrial wastewater.

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## 1. Introduction

Water contaminated with organic dyes is a major environmental issue, especially given the extensive application of dyes across multiple industries.<sup>1</sup> Textiles, leather, paper, plastics, and other industrial fields extensively use organic dyes to add brilliant color to their products.<sup>2</sup> Organic dyes are one of the toxic pollutants that cause serious environmental and health hazards due to their recalcitrance to biodegradation and conventional approaches for wastewater treatment. When organic dyes discharge into water bodies, they cause a harmful effect on the aquatic systems.<sup>3</sup>

Crystal violet (CV), a synthetic cationic dye and a member of the triphenylmethane group, is widely employed in textile dyeing, printing, veterinary medicine, dermatology, forensic

science, and cosmetics.<sup>4</sup> Unfortunately, CV poses severe health risks; it has carcinogenic and mutagenic effects.<sup>5</sup> Prolonged exposure to CV may create problems with the liver and kidneys. In addition, CV is irritating to the skin, causes nausea and vomiting, may affect the respiratory system, and damages the cornea and conjunctiva.<sup>6</sup> If a CV is released into a natural water system, it must be removed from wastewater before discharge.

Various approaches are employed to remove organic dyes from wastewater. These procedures include coagulation, flocculation,<sup>7</sup> electrochemical methods,<sup>8,9</sup> advanced oxidation processes,<sup>10</sup> membrane filtration,<sup>11</sup> biodegradation,<sup>12</sup> and adsorption.<sup>13,14</sup> Among these techniques, adsorption is the best choice. It is easy to use, low-cost, and highly effective at removing dyes even in low concentrations. The adsorbent can be regenerated and reused several times, reflecting its eco-friendliness and economic impacts. The effectiveness of an adsorbent depends on its surface area, porosity, and surface chemistry.

Traditional adsorbent materials may suffer from drawbacks such as being expensive, difficult to regenerate, or effective only under certain conditions.<sup>15</sup> Metal oxides such as ZnO, TiO<sub>2</sub>, Fe<sub>3</sub>O<sub>4</sub>, and BaTiO<sub>3</sub> are extensively investigated as adsorbents and catalysts because of their stability, non-toxicity, availability, and ability to operate under varied pH and temperature conditions. These materials are expected to overcome the

<sup>a</sup>Chemistry Department, Faculty of Science, Mansoura University, Mansoura 35516, Egypt

<sup>b</sup>Spectroscopy Department, Physics Research Institute, National Research Centre, Giza, 12311, Egypt

<sup>c</sup>Basic and Applied Science Department, Horus University, International Coastal Rd, Kafr Saad, New Damietta, 34511, Egypt

<sup>d</sup>Urology and Nephrology Center, Mansoura University, Mansoura 35516, Egypt. E-mail: w.mortada@mans.edu.eg


limitations of traditional adsorbents by offering a high adsorption capacity, fast kinetics, and reusability, thereby contributing to sustainable wastewater treatment solutions.<sup>16</sup>

There are various plans to improve the adsorption capacity of BaTiO<sub>3</sub>, for example, modifying the size and morphology of BaTiO<sub>3</sub> particles through the temperature of synthesis and reaction periods, doping with noble metal nanoparticles (Ag and Au), and creating composites with other semiconductors (ZnO and TiO<sub>2</sub>) or carbon-based material (BaTiO<sub>3</sub>@graphene).<sup>17</sup> The BaTiO<sub>3</sub>@ZnO composite has an antimicrobial activity.<sup>18</sup> In addition to environmental applications, BaTiO<sub>3</sub>@ZnO composites have been investigated for electronic devices and energy storage applications.<sup>19</sup> These different applications point out the composite's potential as a multipurpose material for sustainable and innovative technologies.

The objective of this work is to investigate the efficiency of BaTiO<sub>3</sub>@ZnO composite as an adsorbent for CV removal from its aqueous solutions. BaTiO<sub>3</sub>@ZnO has stable physicochemical properties, low cost, reusability, and environmental friendliness. For this aim, BaTiO<sub>3</sub> was modified with zinc oxide (ZnO) to form a composite material (BaTiO<sub>3</sub>@ZnO). ZnO enhances the surface characteristics of the composite by increasing the specific surface area, improving porosity, and giving more active adsorption sites. Furthermore, ZnO offers a high isoelectric point and supports electrostatic interactions with aromatic dye molecules. The composite has a synergistic effect that improves the adsorption capacity. The BaTiO<sub>3</sub>@ZnO composite was easily synthesized by a solid-state technique, which is environmentally friendly and does not use hazardous solvents or toxic chemicals. X-ray diffraction (XRD), Fourier transform infrared (FTIR), scanning electron microscopy (SEM), transmission electron microscopy (TEM), and Brunauer–Emmett–Teller (BET) were employed to characterize the composite to establish a relationship between structural and surface characteristics of the composite and adsorption capacity. The effects of parameters (pH, initial dye concentration, adsorbent dosage, contact time, temperature, and ionic strength) on the adsorption process were investigated. Kinetics, thermodynamics, and adsorption isotherms were studied to understand the CV adsorption mechanism.

## 2. Experimental

### 2.1. Chemicals

In this study, analytical-grade chemicals and distilled water were employed. Anatase titanium dioxide (TiO<sub>2</sub>; purity of 99.8%), zinc oxide (ZnO; purity of 99.8%), and barium carbonate (BaCO<sub>3</sub>; purity of 99.9%) were purchased from Sigma-Aldrich (St. Louis, MO, USA). CV dye obtained from (Merck, Darmstadt, Germany). Analytical grade HCl (37%, El-Gomhouria, Egypt) and NaOH (≥98%, analytical grade, El-Gomhouria, Egypt) were used to adjust the pH of solutions.

### 2.2. Stock solution of CV

A 1000 mg L<sup>-1</sup> stock solution of CV dye was prepared by dissolving 1.0 g of CV in 1000 mL of distilled water. UV-Vis spectrophotometry analysis revealed the wavelength of

maximum absorption to be 590 nm. Working solutions were prepared daily by dilution of the stock solution.

### 2.3. Synthesis of BaTiO<sub>3</sub>@ZnO composite

The BaTiO<sub>3</sub>@ZnO composite was produced *via* a single-step solid-state reaction route.<sup>20,21</sup> In a typical preparation, 2.35 g of barium carbonate (BaCO<sub>3</sub>), 1.60 g of titanium dioxide (TiO<sub>2</sub>), and 0.81 g of zinc oxide (ZnO) were weighed according to the desired stoichiometric ratio. The powders were thoroughly mixed in an agate mortar and subjected to ball milling for 2 h. The homogenized mixture was placed in a platinum crucible and underwent a thermal treatment program that involved 2 hours at 350 °C to eliminate carbon dioxide from the decomposition of BaCO<sub>3</sub>, followed by 6 hours at 1000 °C. This technique introduces simplicity, scalability, and cost-effectiveness.

### 2.4. Instrumentation

The BaTiO<sub>3</sub>@ZnO composite was characterized using a range of analytical instruments. XRD was performed with a Bruker D8 advanced X-ray diffractometer (Germany) using a monochromatic Cu-K $\alpha$  radiation source,  $\lambda = 0.15406$  nm, running at 40 kV. FTIR spectra were recorded in the 4000–400 cm<sup>-1</sup> regions at a resolution of 2 cm<sup>-1</sup> on a Nicolet FTIR spectrophotometer (model 6700, USA) employing the KBr disk method. SEM images were obtained through Jeol JSM-6510LV equipment (Japan) equipped with energy dispersive X-ray (EDX), while TEM images were captured using a Jeol JEM-2100 instrument (Japan). The surface area was assessed *via* the BET method using the N<sub>2</sub> adsorption/desorption technique (NOVA Touch 4LX analyzer, USA). The CV concentrations were analyzed by a UV-Vis spectrophotometer (Unico Model 1200, USA) at a wavelength of 590 nm. The pH levels of the solutions were assessed by a pH meter (Adwa AD1030, China). A rotary orbital shaker (BIBBY Stuart Scientific-SO1, UK) was utilized for batch experiments. A centrifuge (80–2 electric, China) was also employed in the experiments to facilitate phase separation.

### 2.5. pH<sub>pzc</sub>

The point of zero charge (pH<sub>PZC</sub>) of the BaTiO<sub>3</sub>@ZnO composite was determined through the pH drift method. In this method, a series of 50 mL NaCl solutions (0.1 mol L<sup>-1</sup>) was adapted to a pH range (2–10) using NaOH (0.1 mol L<sup>-1</sup>) and HCl (0.1 mol L<sup>-1</sup>), followed by adding 20 mg of BaTiO<sub>3</sub>@ZnO composite in each tube and agitating at 200 rpm. After 24 h, the composite was extracted from the solution, and finally, the pH of the solutions was determined again. The difference between the initial and final pH ( $\Delta$ pH) was plotted *versus* initial pH to estimate pH<sub>pzc</sub>, which is the point when  $\Delta$ pH equals zero.

### 2.6. Batch adsorption experiments of BaTiO<sub>3</sub> and BaTiO<sub>3</sub>@ZnO

Batch adsorption tests were executed to assess the influences of experimental factors on CV removal using BaTiO<sub>3</sub> and BaTiO<sub>3</sub>@ZnO composite. The goal of studying BaTiO<sub>3</sub>, besides the BaTiO<sub>3</sub>@ZnO composite, was to compare the performance and adsorption behavior of both adsorbents. The investigated



factors included pH (2–10), adsorbent dose (5–70 mg), initial dye concentration (30–200 mg L<sup>-1</sup>), contact time (30–390 min), temperature (25–50 °C), and ionic strength (0.05–0.25 mol L<sup>-1</sup> of NaCl). In a standard experiment, a known quantity of adsorbent was added to 10 mL of CV solution at the desired pH. The mixture was stirred at 200 rpm at room temperature using a rotary shaker until equilibrium was reached, which occurred after 300 min for BaTiO<sub>3</sub> and 360 min for the BaTiO<sub>3</sub>@ZnO composite. After reaching equilibrium, the samples were centrifuged for 15 min at 4000 rpm to extract the adsorbent from the solution. The CV concentration in the supernatant was then measured by a spectrophotometer at 590 nm.

Eqn (1) and (2) were used to estimate the amount of CV adsorbed at equilibrium ( $q_e$ ) (mg g<sup>-1</sup>) and the percentage of CV removal (% $E$ ), respectively:

$$q_e = \frac{(C_0 - C_e)V}{m} \quad (1)$$

$$\% E = \frac{C_0 - C_e}{C_0} \times 100 \quad (2)$$

where  $C_0$  (mg L<sup>-1</sup>) is the initial CV concentration,  $C_e$  (mg L<sup>-1</sup>) is the equilibrium concentration of CV,  $V$  (L) is the volume of CV solution, and  $m$  (g) is the mass of the adsorbent.

Table 1 Characteristic of environmental water samples

Nile river water		Sewage wastewater	
TDS	315 mg L <sup>-1</sup>	TDS	1005 mg L <sup>-1</sup>
Turbidity (NTU)	15.24 NTU	TSS	19 mg L <sup>-1</sup>
BOD	10.0 mg L <sup>-1</sup>	BOD	52 mg L <sup>-1</sup>
COD	6.0 mg L <sup>-1</sup>	COD	66 mg L <sup>-1</sup>
DO	6.27 mg L <sup>-1</sup>	DO	6.4 mg L <sup>-1</sup>
NO <sub>2</sub>	0.53 mg L <sup>-1</sup>	NO <sub>2</sub>	25 mg L <sup>-1</sup>
NO <sub>3</sub>	3.2 mg L <sup>-1</sup>	NO <sub>3</sub>	0.3 mg L <sup>-1</sup>
PO <sub>4</sub>	0.96 mg L <sup>-1</sup>	PO <sub>4</sub>	3.2 mg L <sup>-1</sup>
NH <sub>3</sub> -N	0.03 mg L <sup>-1</sup>	NH <sub>3</sub> -N	3 mg L <sup>-1</sup>

## 2.7. Desorption and reusability

Desorption and reusability were studied to evaluate the economic benefit and practical application of BaTiO<sub>3</sub> and BaTiO<sub>3</sub>@ZnO composite adsorbents for the removal of CV. Ten successive adsorption–desorption cycles were carried out under fixed conditions (initial dye concentration: 50 mg L<sup>-1</sup>, adsorbent dose: 10 mg, volume: 10 mL, temperature: 35 °C, equilibrium time: 360 min, pH: 8). After each cycle, dye molecules were desorbed from the adsorbents using absolute ethanol, followed by rinsing with deionized water and drying at 70 °C for 1 h before reuse again.

## 2.8. Application

Two real water samples (Table 1) and one synthetic effluent sample were used to test the applicability of the procedure for the recovery of CV. Samples from the Nile River (Mansoura) and Sewage wastewater were collected and centrifuged at 4000 rpm for 10 min to remove any suspended particles. The supernatants were separated and subjected to the recovery procedure. A synthetic effluent sample was prepared according to Li *et al.*<sup>22</sup> 10 mg each of NaCl, Na<sub>2</sub>SO<sub>4</sub>, CH<sub>3</sub>COONa, Na<sub>2</sub>CO<sub>3</sub>, Na<sub>2</sub>HPO<sub>4</sub>, MgSO<sub>4</sub>, CaCl<sub>2</sub>, and KCl were dissolved separately and mixed to form 1.0 L of the synthetic sample. 10 mL of each sample was spiked with different concentrations of CV and subjected to the optimized procedure. A simple diagram illustrating the workflow and apparatus for the real-sample adsorption tests is shown in Fig. (1). The recovery was calculated from the following relation:

$$R = \frac{\text{Concentration spiked} - \text{Concentration unspiked}}{\text{Concentration added}} \times 100 \quad (3)$$

# 3. Results and discussion

## 3.1. Characterization of BaTiO<sub>3</sub>@ZnO composite

**3.1.1. XRD.** X-ray diffraction (XRD) analysis is an essential technique for examining the crystalline structure, phase

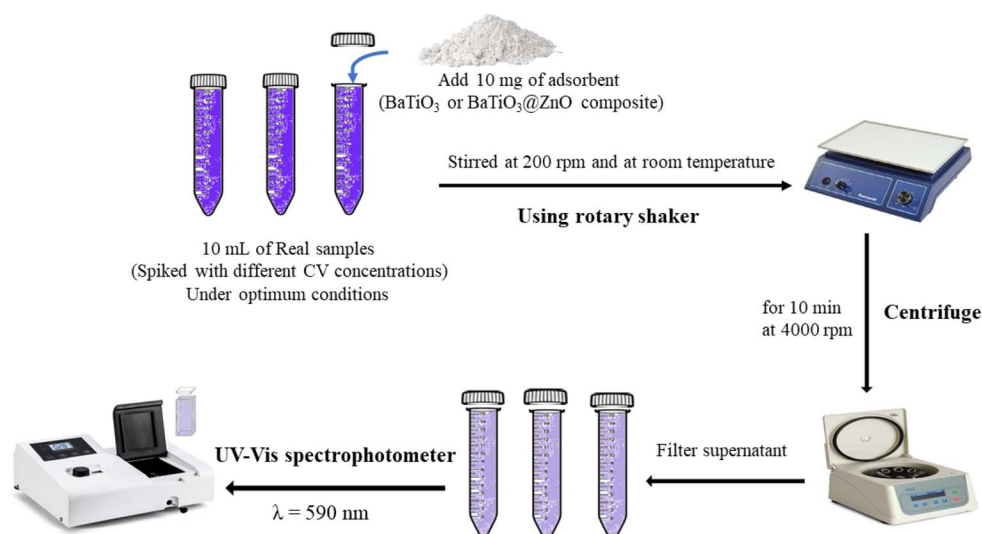


Fig. 1 Workflow diagram for the real-sample adsorption tests.



composition, and average particle size of the BaTiO<sub>3</sub>@ZnO composite. The XRD pattern of the BaTiO<sub>3</sub>@ZnO composite before and after CV adsorption is displayed in Fig. 2a.

As shown in pattern (2a i), before CV adsorption, it illustrates the crystalline phases corresponding to the two components: BaTiO<sub>3</sub> and ZnO. The major diffraction peaks observed at  $2\theta = 31.7^\circ, 34.4^\circ, 36.2^\circ, 47.5^\circ, 56.5^\circ, 62.8^\circ, 66.3^\circ, 67.9^\circ, 69.02^\circ, 72.5^\circ$ , and  $76.9^\circ$  with corresponding planes (100), (002), (101), (102), (110), (103), (200), (112), (201), (004), and (202), respectively, are characteristic of the hexagonal wurtzite structure of ZnO, which matched with standard reference patterns (JCPDS No. 36-1451).<sup>23</sup> This confirms the presence of ZnO with a hexagonal structure, lattice parameters  $a = b = 3.24950 \text{ \AA}$  and  $c = 5.20690 \text{ \AA}$ , and space group P 63 mc. While the diffraction peaks located at  $2\theta = 25.3^\circ, 37.8^\circ, 38.6^\circ, 48.1^\circ, 53.9^\circ, 55.1^\circ, 62.1^\circ, 62.7^\circ, 70.3^\circ$ , and  $75^\circ$  are assigned to planes (101), (004), (112), (200), (105), (211), (213), (204), (220), and (215), respectively, they are related to anatase phases of TiO<sub>2</sub> (JCPDS No. 21-1272).<sup>24</sup> This confirms the presence of a tetragonal BaTiO<sub>3</sub> structure with lattice

parameters  $a = b = 3.785 \text{ \AA}$  and  $c = 9.514 \text{ \AA}$  and the  $I4_1/amd$  space group. The XRD spectra indicate the successful formation of the BaTiO<sub>3</sub>@ZnO composite. The average crystallite size of the particles can be determined using the Debye-Scherrer formula (3).

$$D = \frac{k\lambda}{\beta \cos \theta} \quad (4)$$

where  $D$  is the average crystallite size (nm),  $k$  is a constant (shape factor around 0.9),  $\lambda$  corresponds to the wavelength of the X-ray applied (0.15406 nm),  $\beta$  is the FWHM (full width at half maximum) of the diffraction lines, and  $\theta$  is the Bragg diffraction angle. The average crystallite size of the particles was determined to be 64.58 nm, which is a nanoparticle size and is suitable for the adsorption process.

In pattern (2a ii), after CV adsorption, there are changes in some diffraction peaks, marked with asterisks (additional peaks at  $2\theta = 27.8^\circ$  and  $59.1^\circ$  – peak intensity at  $2\theta = 23.9^\circ, 42.0^\circ, 43.0^\circ, 44.9^\circ$ , and  $46.7^\circ$ ). These peaks may be ascribed to the interaction of CV with the composite surface. The crystalline peaks of the BaTiO<sub>3</sub>@ZnO composite remain the same with no change, indicating the integrity of the BaTiO<sub>3</sub>@ZnO composite and the ability to reuse it in dye removal.

**3.1.2. FTIR.** Fourier-transform infrared (FTIR) spectroscopy was employed to identify the functional groups present on the surface of the BaTiO<sub>3</sub>@ZnO composite and to investigate the nature of interactions with CV dye. The spectra recorded before and after CV adsorption are displayed in Fig. 2b. Before adsorption (spectrum I), the composite exhibits characteristic bands at  $432 \text{ cm}^{-1}$ , attributable to stretching vibrations of Ba–O, Ti–O, and/or Zn–O bonds.<sup>25–27</sup> Additional peaks at 692, 788, and  $854 \text{ cm}^{-1}$  are associated with Ti–O and Ti–O–Ti stretching modes,<sup>28</sup> confirming the formation of the BaTiO<sub>3</sub> phase. A sharp band near  $1418 \text{ cm}^{-1}$  corresponds to residual carbonate ( $\text{CO}_3^{2-}$ ) vibrations,<sup>29</sup> likely originating from the BaCO<sub>3</sub> precursor.

After CV adsorption (spectrum II), several changes are observed. A new band emerges at  $1433 \text{ cm}^{-1}$ , which can be assigned to aromatic C=C stretching or C–H bending vibrations of the methyl groups in the CV molecule.<sup>30,31</sup> Additionally, shifts and intensity alterations occur in the low-frequency region: a new band appears at  $502 \text{ cm}^{-1}$ , possibly due to Ti–O or Zn–O bending vibrations,<sup>32,33</sup> while a band at  $581 \text{ cm}^{-1}$  emerges, corresponding to metal–oxygen stretching modes.<sup>32</sup> Moreover, the intensities of the peaks at 1084 and  $854 \text{ cm}^{-1}$  decrease noticeably, suggesting surface interactions that modify vibrational modes of the composite. The absence of distinct ZnO-specific bands in the spectrum may be due to the low IR activity of Zn–O vibrations and their overlap with Ba–O and Ti–O modes. Nevertheless, the observed spectral changes before and after adsorption provide strong evidence of interfacial interactions, indicating that CV adsorption involves both electrostatic attraction and chemisorption onto the composite surface.

**3.1.3. SEM/EDX analysis.** SEM provides important details about the surface morphology of the BaTiO<sub>3</sub>@ZnO composite as depicted in Fig. 3a. The SEM image exhibits particles agglomerated with irregular shapes and varying sizes. The particles possess a smooth surface with a uniform distribution. The

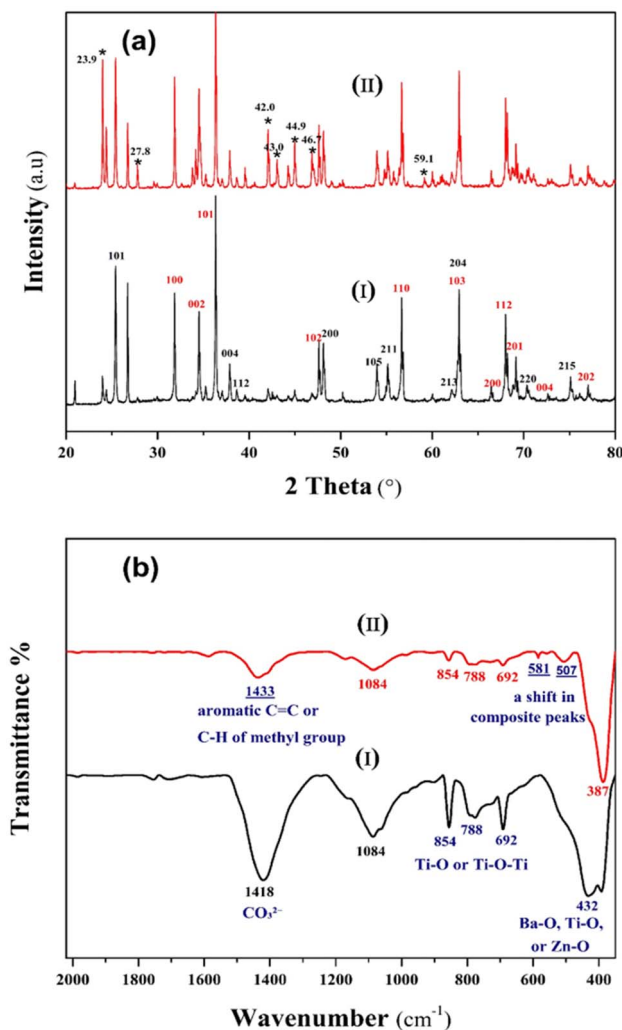


Fig. 2 (a) XRD pattern of BaTiO<sub>3</sub>@ZnO composite: (i) before and (ii) after adsorption of CV; (b) FTIR spectra of BaTiO<sub>3</sub>@ZnO composite: (i) before and (ii) after adsorption of CV.



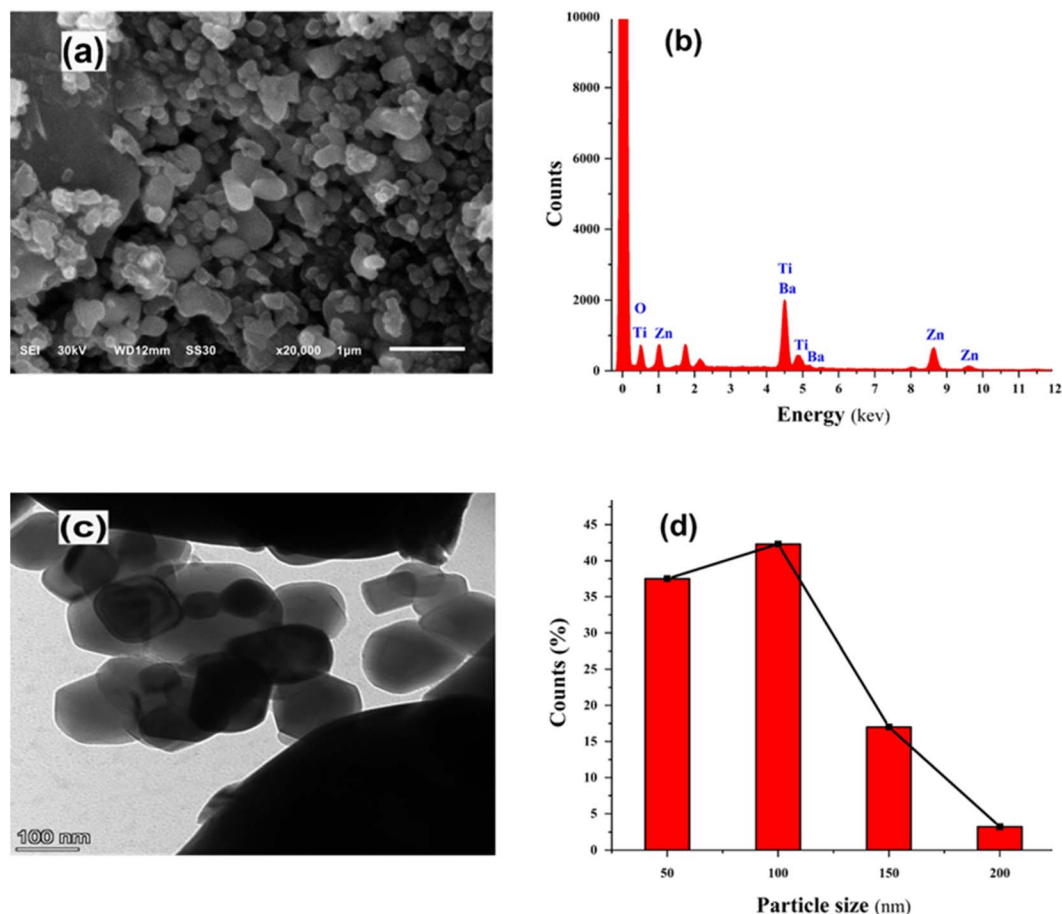


Fig. 3 (a) SEM image; (b) EDX image; (c) TEM image; (d) histogram of particle size distribution: for BaTiO<sub>3</sub>@ZnO composite.

image shows that the composite is present in a crystalline structure.

Energy dispersive X-ray (EDX) is an analytical technique that determines the elemental components of a sample. The EDX spectrum confirmed the elemental composition of the BaTiO<sub>3</sub>@ZnO composite, illustrating Ba, Ti, O, and Zn as the major constituents (Fig. 3b). The percentage mass of elements—barium (2.70%), titanium (9.28%), oxygen (80.28%), and zinc (7.74%)—is displayed in Table 2. This result confirms the successful incorporation of ZnO with BaTiO<sub>3</sub> to form a composite.

**3.1.4. TEM.** The crystalline particle size and distribution of the BaTiO<sub>3</sub>@ZnO composite are shown in the TEM image (Fig. 3c). The TEM image reveals that the composite consists of nanoparticles mainly spherical to slightly polyhedral in shape with different sizes. The image illustrates an agglomeration of

particles with a moderate uniform distribution, which is a common feature in metal oxide nanomaterials synthesized by wet chemical techniques. The corresponding particle size distribution histogram (Fig. 3d), derived from the TEM image, indicates the average particle diameter is 67.95 nm, with the most particles located in the range 50–100 nm. This value matches XRD calculations.

**3.1.5. BET studies.** The N<sub>2</sub> adsorption–desorption isotherm was carried out to get the surface area and pore characteristics of both the BaTiO<sub>3</sub>@ZnO composite and BaTiO<sub>3</sub>.

The BaTiO<sub>3</sub>@ZnO composite exhibits type IV isotherms according to the IUPAC classification with a hysteresis ring, which indicates a mesoporous structure of the composite, as depicted in Fig. 4a. As illustrated in Table 3, the BET surface area of the BaTiO<sub>3</sub>@ZnO composite and BaTiO<sub>3</sub> were found to be 34.1 m<sup>2</sup> g<sup>−1</sup> and 28.1 m<sup>2</sup> g<sup>−1</sup>, respectively. Average pore radius and pore volume were determined by the Barret-Joyner-Halenda (BJH) method. The average pore radius of the BaTiO<sub>3</sub>@ZnO composite was 2.53 nm, and for BaTiO<sub>3</sub>, it was 3.59 nm. Pore volume for the BaTiO<sub>3</sub>@ZnO composite and BaTiO<sub>3</sub> were noticed to be 0.0354 cm<sup>3</sup> g<sup>−1</sup> and 0.0437 cm<sup>3</sup> g<sup>−1</sup>, respectively. Pore size distribution curve using the BJH method (Fig. 4b) indicates that most pores of the composite are centered around 2.5 nm with a uniform mesoporous structure, which is favorable for diffusion and interaction of dye molecules with the active surface.

Table 2 EDX analysis of BaTiO<sub>3</sub>@ZnO composite

Element	Weight %	Atomic %
O	49.29	80.28
Ti	17.05	9.28
Zn	19.41	7.74
Ba	14.24	2.70
Total	100	100



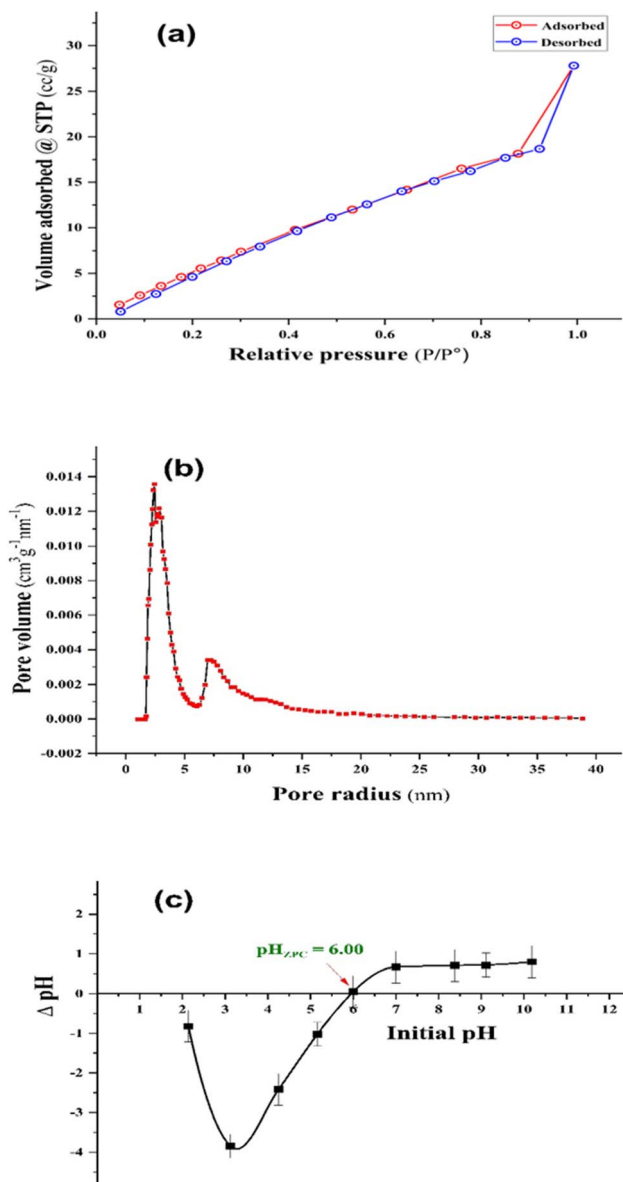


Fig. 4 (a)  $N_2$  adsorption-desorption isotherm; (b) BJH plot and pore size distribution; (c) point zero charge (PZC): for  $BaTiO_3@ZnO$  composite.

The results showed that the  $BaTiO_3@ZnO$  composite has a higher surface area and has a slight decrease in pore volume and average pore radius to become a finer mesoporous material, making it more efficient for removing CV from wastewater. This matches previous studies that have shown ZnO addition to

Table 3 Surface area and pore characteristics of  $BaTiO_3@ZnO$  composite and  $BaTiO_3$

Sample	BET surface area ( $m^2 g^{-1}$ )	Pore volume ( $cm^3 g^{-1}$ )	Average pore radius (nm)
$BaTiO_3$	28.1	0.0437	3.59
$BaTiO_3@ZnO$	34.1	0.0354	2.53

$BaTiO_3$  increases the specific surface area, decreases particle size, and improves surface morphology and reactivity; all of these contribute to better adsorption of dye molecules.<sup>34</sup>

**3.1.6. Point of zero charge.** pH<sub>pzc</sub> is the point at which the adsorbent surface exhibits a neutral net charge. The pH<sub>pzc</sub> of  $BaTiO_3@ZnO$  composite was found to be pH 6.0, as displayed in Fig. 4c. This indicates that the composite surface acquires a negative charge above this value and has a positive charge at values below.<sup>35</sup> It is an essential parameter in the electrostatic interaction between cationic CV and  $BaTiO_3@ZnO$  composite. Subsequently, the composite was extracted from the solution, and the final pH of the solution was assessed.

## 3.2. Batch adsorption process

**3.2.1. Effect of pH.** The pH of the solution plays an essential role in the adsorption process because it affects the surface charge of the adsorbent, the ionization of the adsorbate molecules, and the interaction of the adsorbent with dye molecules.<sup>36</sup> The effect of pH on the removal efficiency of CV using either  $BaTiO_3$  or  $BaTiO_3@ZnO$  composite was investigated by varying the pH range from 2 to 10 using 0.1 mol  $L^{-1}$  NaOH or 0.1 mol  $L^{-1}$  HCl and under consistent experimental conditions (initial dye concentration: 50 mg  $L^{-1}$ , adsorbent dose: 10 mg, dye volume: 10 mL, temperature: 35 °C, contact time: 360 min). As illustrated in Fig. 5a, the  $BaTiO_3$  powder showed a gradual increase in the removal efficiency from 20.28% at pH 2 to 43.91% at pH 8–10. In comparison, the  $BaTiO_3@ZnO$  composite exhibited considerably higher performance; the removal efficiency increased from 32.07% at pH 2 to 86.91% at pH 6, after which it plateaued up to pH 10. The removal efficiency increases with increasing pH; this may be due to the reduction of the competition effect between  $H^+$  ions and dye molecules for surface sites. Furthermore, the deprotonation of adsorbent surfaces supports the electrostatic attraction between the negatively charged surface and the cationic CV.<sup>37</sup> The removal efficiency reached a plateau at pH from neutral to alkaline; this suggests the saturation of the active site on the surface or the adsorption capacity became limited beyond a specific pH. The better efficiency of the composite is ascribed to the synergistic interaction between  $BaTiO_3$  and ZnO, which improves surface charge distribution and enhances active sites for CV adsorption.

**3.2.2. Influence of initial concentration of dye.** The concentration of CV affects the adsorption efficiency of  $BaTiO_3$  and  $BaTiO_3@ZnO$  composite. The experiment was performed in the range of initial concentration (30–200 mg  $L^{-1}$ ); other parameters were kept constant (adsorbent dosage: 10 mg, solution volume: 10 mL, contact time: 360 min, temperature: 35 °C, pH: 8). The adsorption capacity ( $q_e$ ) of both adsorbents rises with increasing dye concentration, as displayed in Fig. 5b. The  $BaTiO_3@ZnO$  composite showed higher adsorption capacity than  $BaTiO_3$ . The composite displayed a maximum  $q_e$  of  $\sim 91.6$  mg  $g^{-1}$  at (150–200) mg  $L^{-1}$ . The  $BaTiO_3$  showed a maximum  $q_e$  of  $\sim 22$  mg  $g^{-1}$  at 50 mg  $L^{-1}$ . The superior efficiency of the composite is attributed to the synergistic effect between ZnO and  $BaTiO_3$ , which increases surface area, improves porosity, and boosts electrostatic attraction and



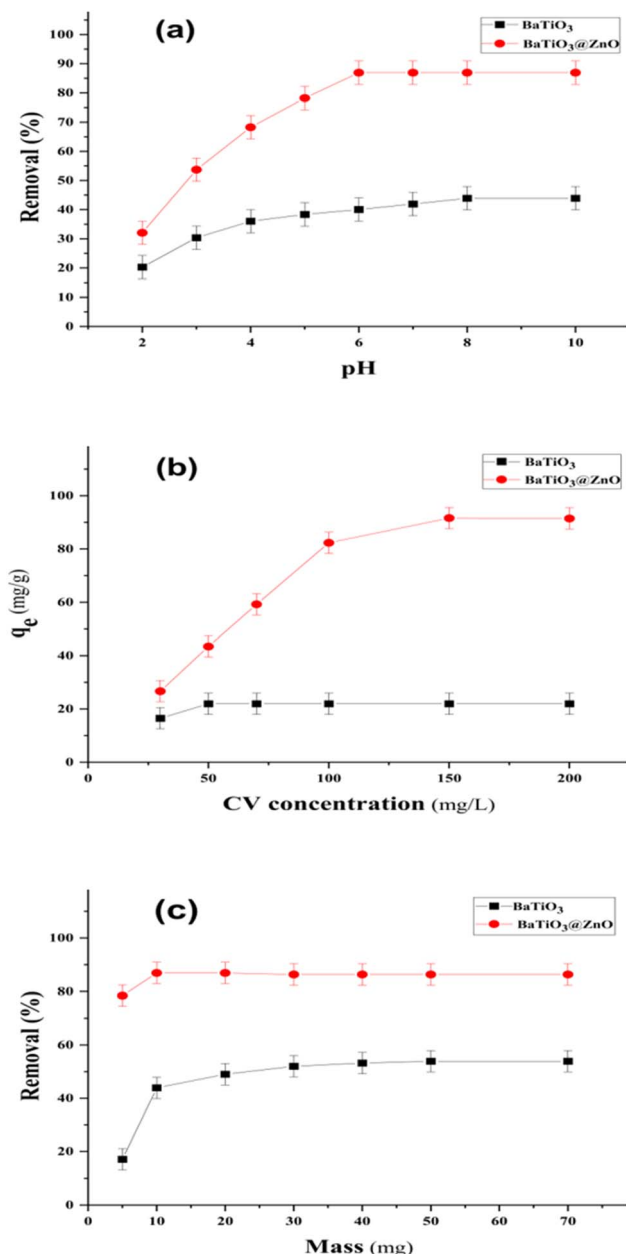


Fig. 5 (a) Effect of pH; (b) influence of initial dye concentration; (c) influence of adsorbent dosage: on the removal and adsorption of CV using  $\text{BaTiO}_3@\text{ZnO}$  composite and  $\text{BaTiO}_3$  (conditions: initial dye concentration =  $50 \text{ mg L}^{-1}$ , adsorbent dose =  $10 \text{ mg}$ , volume =  $10 \text{ mL}$ , temperature =  $35^\circ\text{C}$ , equilibrium time =  $360 \text{ min}$ , pH =  $8$ ).

surface charge interaction with dye molecules. The results matched with other previous studies, which mentioned the advantages of composite oxide materials in improving adsorption capacity.<sup>16</sup>

**3.2.3. Influence of adsorbent dosage.** The adsorbent dose is an essential factor that influences dye removal performance by controlling the availability of active surface sites for adsorption. Under controlled conditions (an initial dye concentration of  $50 \text{ mg L}^{-1}$ , a solution volume of  $10 \text{ mL}$ , a temperature of  $35^\circ\text{C}$ , a contact time of  $360 \text{ min}$ , and a pH of  $8$ ), the influence of the dosage of  $\text{BaTiO}_3$  and  $\text{BaTiO}_3@\text{ZnO}$

composite on CV uptake was evaluated. The behavior of adsorption of the two adsorbents is different, as shown in Fig. 5c.

For  $\text{BaTiO}_3$ , a continual increase in dye removal was observed as the dose of the adsorbent was increased, showing better availability of binding sites.<sup>38</sup> At a specific dosage (approximately  $50 \text{ mg}$ ), additional increments in dosage did not lead to a proportional enhancement in efficiency. The plateau behavior suggests that either too much adsorbent caused particle aggregation, which reduces the effective surface area

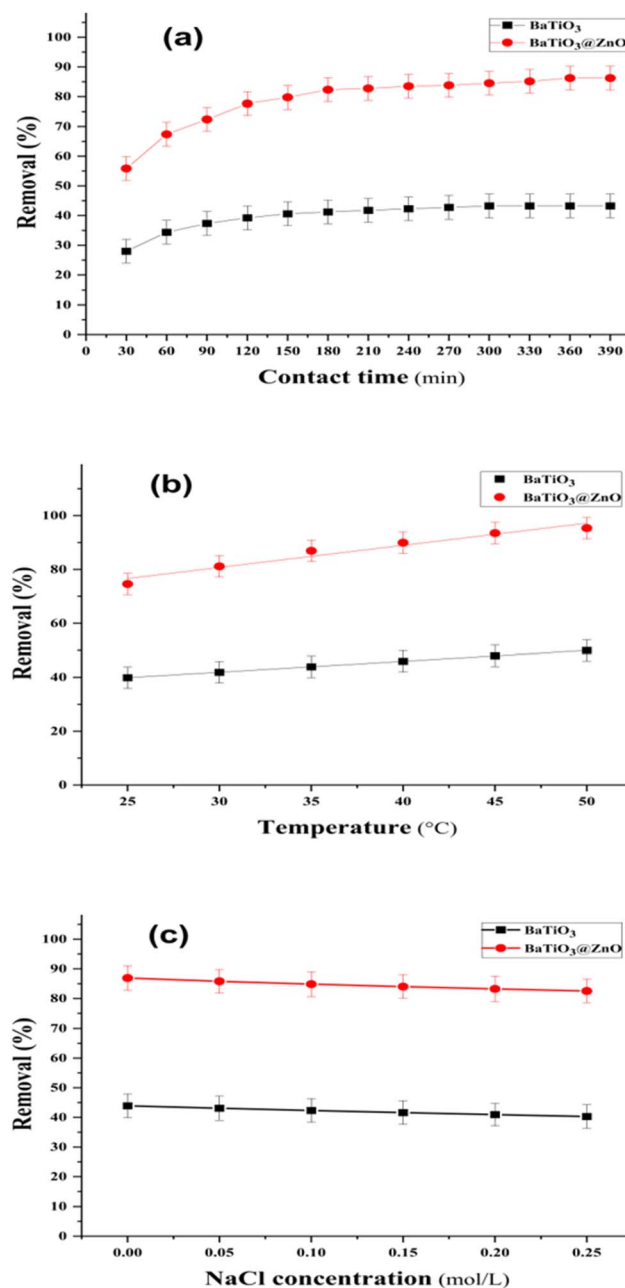


Fig. 6 (a) Influence of contact time; (b) influence of temperature; (c) influence of ionic strength: on the removal % of CV using  $\text{BaTiO}_3@\text{ZnO}$  composite and  $\text{BaTiO}_3$  (conditions: initial dye concentration =  $50 \text{ mg L}^{-1}$ , adsorbent dose =  $10 \text{ mg}$ , volume =  $10 \text{ mL}$ , temperature =  $35^\circ\text{C}$ , pH =  $8$ , equilibrium time =  $360 \text{ min}$ ).



and prevents more adsorption, or that the dye molecules were practically exhausted from the solution.<sup>39</sup>

The BaTiO<sub>3</sub>@ZnO composite eliminated a substantial amount of the dye even at very low doses, with efficiency reaching its peak at about 10 mg. After that, as the dosage was increased, the performance was almost constant, suggesting that the adsorption sites were quickly saturated.<sup>40</sup> This enhancement can be explained by a synergistic effect between ZnO and BaTiO<sub>3</sub>, which leads to an increment in the number of active sites, improves surface charge, and accelerates dye-adsorbent interactions. The removal capacity of the composite is high at low doses, which leads to savings in material and cost in water treatment processes.

**3.2.4. Influence of contact time.** Contact time is an essential parameter in the adsorption process and tells us how long the adsorption process takes to reach equilibrium. The effect of contact time on the removal of CV using BaTiO<sub>3</sub> and BaTiO<sub>3</sub>@ZnO composite was investigated with different time intervals (30–390 min) at fixed experimental conditions: initial CV concentration of 50 mg L<sup>-1</sup>, adsorbent dose of 10 mg, solution volume of 10 mL, temperature of 35 °C, and pH 8.

As shown in Fig. 6a, the BaTiO<sub>3</sub> exhibited a gradual increase of CV removal with time until reaching equilibrium at 300 min with a removal percent near 43%. The BaTiO<sub>3</sub>@ZnO composite showed a more efficient adsorption process through a rapid CV uptake in the initial stage of contact time and a higher dye removal exceeding 86% at equilibrium time (360 min). The initial uptake of dye is rapid due to the presence of abundant active sites; with time, the saturation takes place, and the adsorption kinetics become slower.<sup>41</sup> The better performance of the composite is due to the synergistic effect between ZnO and BaTiO<sub>3</sub>.

**3.2.5. Influence of temperature.** The temperature is a vital parameter in the adsorption process due to its effect on the surface characteristics of the adsorbent and the mobility of dye molecules in aqueous solutions. The influence of temperature on the removal efficiency of CV using BaTiO<sub>3</sub> and BaTiO<sub>3</sub>@ZnO composite was examined at various temperatures of 25, 30, 35, 40, 45, and 50 °C under optimal conditions (10 mg of adsorbent to 10 mL of dye solution at an initial dye concentration of 50 mg L<sup>-1</sup> and pH = 8 during an equilibrium time of 360 min). Fig. 6b illustrates that there is a steady increase in the removal efficiency as the temperature increases for both adsorbents, which suggests the adsorption of CV is temperature dependent. BaTiO<sub>3</sub> showed a gradual rise in the removal efficiency from 39.89% to 49.94% at 25 °C and 50 °C, respectively. The BaTiO<sub>3</sub>@ZnO composite illustrated greater removal efficiency, which increased from 74.60% to 95.37% across the same temperature range. The enhancement of removal efficiency as a result of increasing temperature may be due to increased mobility, kinetic energy, and diffusion rate of dye molecules that become more accessible to the surface of the adsorbent.<sup>42</sup>

**3.2.6. Influence of ionic strength.** The effect of ionic strength on the adsorption of CV by BaTiO<sub>3</sub> and BaTiO<sub>3</sub>@ZnO composite was analyzed using different concentrations of NaCl (0.05–0.25 mol L<sup>-1</sup>) at fixed experimental conditions (*C*<sub>0</sub> = 50 mg L<sup>-1</sup>, adsorbent dose = 10 mg, a solution volume = 10 mL,

pH = 8, temperature = 35 °C, equilibrium time = 360 min). As exhibited in Fig. 6c, both adsorbents showed a gradual decrease in the removal efficiency of dye with increasing ionic strength. The reason may be related to the presence of excess Na<sup>+</sup> and Cl<sup>-</sup> ions in the solution, which may compete with dye molecules for adsorption sites and compress the electrical double layer, leading to a decrease in the electrostatic attraction between the positively charged dye and the negatively charged surfaces of the adsorbent.

The BaTiO<sub>3</sub> displayed a small decrease in removal efficiency throughout the ionic strength range from 43.09% to 40.30%, which indicates restricted surface area and electrostatic interactions. While the BaTiO<sub>3</sub>@ZnO composite showed improved and consistent removal efficiency, even at high salt concentrations, from 85.81% to 82.53%. This indicates increased surface reactivity and adsorption capacity. The results agree with earlier research, which suggests that the higher ionic strength might reduce dye adsorption. This happens due to charge screening and ion competition.<sup>43</sup>

**3.2.7. Adsorption kinetics.** Adsorption kinetics provides a critical understanding of the mechanism and rate of dye adsorption onto solid surfaces. Kinetics data are used in designing water treatment facilities. The kinetic behavior of CV adsorption onto BaTiO<sub>3</sub> and BaTiO<sub>3</sub>@ZnO composite was examined in this research using three common models: pseudo-first-order, pseudo-second-order, and intra-particle diffusion models.

**3.2.7.1. Pseudo-first-order kinetics.** The pseudo-first-order model, as proposed by Lagergren, is that the rate of dye adsorption is directly proportional to the quantity of unoccupied adsorption sites.<sup>44</sup> The linearized model is expressed as

$$\log(q_e - q_t) = \log q_e - \left(\frac{k_1}{2.303}\right)t \quad (5)$$

where *q<sub>e</sub>* and *q<sub>t</sub>* (both in mg g<sup>-1</sup>) are, respectively, the adsorbed amounts at equilibrium and at time *t*, and *k<sub>1</sub>* (min<sup>-1</sup>) is the equilibrium rate constant for the pseudo-first-order adsorption. The magnitudes of *k<sub>1</sub>* and *q<sub>e</sub>* were measured from the slope and intercept of the linear plot of log(*q<sub>e</sub>* - *q<sub>t</sub>*) against *t* (Fig. 7a). Although the correlation coefficients are high in this model (*R*<sup>2</sup> = 0.9861 for BaTiO<sub>3</sub> and 0.9582 for BaTiO<sub>3</sub>@ZnO), the calculated *q<sub>e</sub>* values were far from the experimental values, suggesting that the pseudo-first-order model is incapable of describing the adsorption mechanism. This reveals that physical adsorption is not the rate-controlling force in adsorption.

**3.2.7.2. Pseudo-second-order kinetics.** The pseudo-second-order model suggests that the rate of adsorption is governed by chemisorption, which is referred to as the sharing or exchange of electrons between adsorbate and adsorbent.<sup>45</sup> Its linear form is

$$\frac{t}{q_t} = \frac{1}{k_2 q_e^2} + \frac{t}{q_e} \quad (6)$$

where *k<sub>2</sub>* (g mg<sup>-1</sup> min) is the equilibrium rate constant of the pseudo-second-order adsorption, and *q<sub>e</sub>* was calculated from the plot of  $\frac{t}{q_t}$  versus *t* (Fig. 7b).





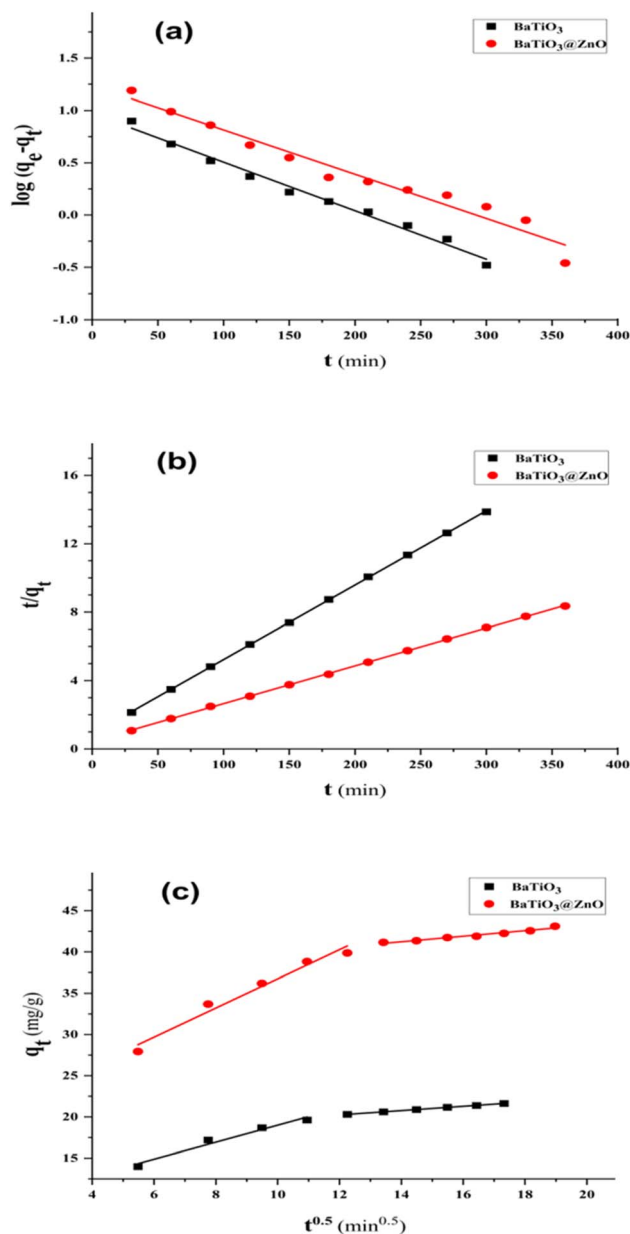


Fig. 7 (a) Pseudo-first-order kinetic model; (b) pseudo-second-order kinetic model; (c) intra-particle diffusion model: for adsorption of CV onto BaTiO<sub>3</sub>@ZnO composite and BaTiO<sub>3</sub>.

This model perfectly correlated with experimental data for both adsorbents, presenting correlation coefficients of  $R^2 = 0.9998$  for the BaTiO<sub>3</sub>@ZnO composite and  $R^2 = 0.9999$  for BaTiO<sub>3</sub>. Additionally, the calculated equilibrium capacities were very similar to the experimental values, showing that chemical interactions control the adsorption process.

**3.2.7.3. Intraparticle diffusion model.** Weber and Morris introduced the intra-particle diffusion model to examine the influence of pore diffusion on adsorption kinetics.<sup>46</sup> The equation can be expressed as

$$q_t = k_{id}t^{1/2} + C_i \quad (7)$$

where  $q_t$  (mg g<sup>-1</sup>) is the adsorption capacity at time  $t$  (min),  $k_{id}$  (mg g<sup>-1</sup> min<sup>-0.5</sup>) is the intra-particle diffusion constant, and  $C_i$  is the intercept at stage  $i$  and represents boundary layer thickness.  $k_{id}$  and  $C_i$  were computed from the ( $q_t$  against  $t^{1/2}$ ) plot (Fig. 7c). The plots showed multi-stage linearity, indicating that the adsorption process was divided into two stages: an initial external surface adsorption and intra-particle diffusion. The plots did not pass through the origin, suggesting that intra-particle diffusion was not the only rate-controlling mechanism. Compared to BaTiO<sub>3</sub> alone, the BaTiO<sub>3</sub>@ZnO composite showed superior surface accessibility and diffusion properties, as evidenced by its higher  $k_{id}$  values.

In summary, among the three kinetic models studied, the pseudo-second-order model most accurately supplied the adsorption kinetics of CV on both BaTiO<sub>3</sub> and BaTiO<sub>3</sub>@ZnO composite, pointing to chemisorption as the predominant mechanism. The enhanced performance of the composite is mainly due to the synergistic interaction between BaTiO<sub>3</sub> and ZnO, which resulted in increased surface activity and faster dye uptake. Table 4 summarizes the adsorption parameters for the kinetic models.

**3.2.8. Adsorption isotherms.** Adsorption isotherms are mathematical models that define the relation between the amount of adsorbate adsorbed on the surface of the adsorbent and the concentration of adsorbate in solution at equilibrium. Adsorption isotherms are necessary to understand the adsorption mechanism. Three classical isotherms for the equilibrium modeling of data, including the Langmuir, Freundlich, and Temkin isotherms, were employed in this work.

**3.2.8.1. Langmuir isotherm.** According to the Langmuir theory, monolayer adsorption takes place on a surface with a finite number of identical sites.<sup>47</sup> Its linear approximation is given by eqn (8)

$$\frac{C_e}{q_e} = \frac{1}{bq_m} + \frac{1}{q_m}C_e \quad (8)$$

where  $C_e$  (mg L<sup>-1</sup>) is the equilibrium concentration of dye,  $q_e$  (mg g<sup>-1</sup>) is the amount of dye adsorbed at the equilibrium,  $b$  (L mg<sup>-1</sup>) is the Langmuir isotherm constant representing the affinity of binding sites, and  $q_m$  (mg g<sup>-1</sup>) is the monolayer adsorption capacity. The slope and interception of the linear curve of  $C_e/q_e$  against  $C_e$  (Fig. 8a) are used to determine the values of  $q_m$  and  $b$ , respectively, and are reported in Table 5. Also, the coefficient of correlation ( $R^2$ ) is determined. Moreover, this model yields a dimensionless separation factor,  $R_L$ , to indicate the favorability of adsorption. It can be stated as

$$R_L = \frac{1}{1 + bC_0} \quad (9)$$

where  $b$  (L mg<sup>-1</sup>) is the Langmuir isotherm constant and  $C_0$  (mg L<sup>-1</sup>) is the maximum initial dye concentration. When the value of  $R_L$  is between 0 and 1, it would indicate favorable adsorption conditions.<sup>48</sup>

**3.2.8.2. Freundlich isotherm.** The Freundlich isotherm is an empirical model that incorporates multilayer adsorption and heterogeneous surface energies.<sup>49</sup> It can be expressed with the linearized formula



Table 4 Adsorption parameters for kinetic studies

Kinetic model	BaTiO <sub>3</sub>		BaTiO <sub>3</sub> @ZnO composite	
	Parameters	Values	Parameters	Values
Pseudo first order	$q_e$ exp (mg g <sup>-1</sup> )	21.96	$q_e$ exp (mg g <sup>-1</sup> )	43.46
	$R^2$	0.9861	$R^2$	0.9582
	$q_e$ calc (mg g <sup>-1</sup> )	9.34	$q_e$ calc (mg g <sup>-1</sup> )	17.28
Pseudo second order	$k_1$ (min <sup>-1</sup> )	$10.7 \times 10^{-3}$	$k_1$ (min <sup>-1</sup> )	$9.76 \times 10^{-3}$
	$R^2$	0.9999	$R^2$	0.9998
	$q_e$ calc (mg g <sup>-1</sup> )	22.98	$q_e$ calc (mg g <sup>-1</sup> )	45.26
Intra particle diffusion	$k_2$ (g mg <sup>-1</sup> min <sup>-1</sup> )	$21.43 \times 10^{-4}$	$k_2$ (g mg <sup>-1</sup> min <sup>-1</sup> )	$10.95 \times 10^{-4}$
	$R^2$	0.9537	$R^2$	0.9629
	$K_{1D}$ (mg g <sup>-1</sup> min <sup>-0.5</sup> )	1.03	$K_{1D}$ (mg g <sup>-1</sup> min <sup>-0.5</sup> )	1.77
	$C_1$ (mg g <sup>-1</sup> )	8.70	$C_1$ (mg g <sup>-1</sup> )	19.08
	$R^2$	0.9995	$R^2$	0.9585
	$K_{2D}$ (mg g <sup>-1</sup> min <sup>-0.5</sup> )	0.261	$K_{2D}$ (mg g <sup>-1</sup> min <sup>-0.5</sup> )	0.336
	$C_2$ (mg g <sup>-1</sup> )	17.10	$C_2$ (mg g <sup>-1</sup> )	36.52

$$\ln q_e = \ln K_f + \frac{1}{n} \ln C_e \quad (10)$$

where  $K_f$  is the Freundlich constant for the adsorption capacity, and  $1/n$  is a heterogeneity factor. The magnitudes of the  $K_f$  and  $n$  were estimated from the intercept and slope of the linear plot of  $\ln q_e$  against  $\ln C_e$  (Fig. 8b), respectively, and are shown in Table 5. The correlation coefficient ( $R^2$ ) is also presented. A  $1/n < 1$  suggests favorable adsorption and higher interactions at lower concentrations.

**3.2.8.3. Temkin isotherm.** The Temkin isotherm considers the effect of indirect adsorbate–adsorbate interactions on adsorption heat. It assumes that the adsorption energy decreases linearly with increasing surface coverage.<sup>50</sup> The linear equation is

$$q_e = \frac{RT}{b_T} \ln K_T + \frac{RT}{b_T} \ln C_e \quad (11)$$

Here,  $R$  is the universal gas constant,  $T$  is the temperature,  $b_T$  (J mol<sup>-1</sup>) is the Temkin constant associated with the heat of adsorption, and  $K_T$  (L g<sup>-1</sup>) is the Temkin binding energy constant.  $b_T$  and  $K_T$  can be estimated from the slope and intercept of the plot of  $q_e$  against  $\ln C_e$  (Fig. 8c), respectively, and are displayed in Table 5. Also, the correlation coefficient ( $R^2$ ) is depicted.

According to the experimental data, the adsorption of CV on BaTiO<sub>3</sub> and BaTiO<sub>3</sub>@ZnO composite was found to be most appropriately fitted by the Langmuir model, with the highest correlation coefficients ( $R^2 > 0.996$ ), and the maximum adsorption capacities for both adsorbents are in close agreement with the experimental values. This indicates monolayer adsorption on uniform surfaces. Supported by these results, the  $R_L$  values of BaTiO<sub>3</sub> and BaTiO<sub>3</sub>@ZnO composite are both in the range from 0 to 1, suggesting that the adsorption of CV by BaTiO<sub>3</sub> and BaTiO<sub>3</sub>@ZnO composite is favorable. The adsorption capacity increases to 97.84 mg g<sup>-1</sup> in the case of the BaTiO<sub>3</sub>@ZnO composite, compared with 23.49 mg g<sup>-1</sup> of BaTiO<sub>3</sub>. Despite the Freundlich and Temkin models providing good fits, the lower  $R^2$  values indicate that the adsorption

process is consistent with Langmuir assumptions. The results validate the improved efficacy of the composite in dye removal applications, which is attributed to increased active sites and better interaction energies.

**3.2.9. Thermodynamic studies.** The dsorption process of CV onto BaTiO<sub>3</sub> and BaTiO<sub>3</sub>@ZnO composites was explained by a thermodynamic investigation based on van't Hoff analysis. Gibbs free energy change ( $\Delta G^\circ$ ), enthalpy change ( $\Delta H^\circ$ ), and entropy change ( $\Delta S^\circ$ ) were calculated to establish the feasibility and nature of adsorption.<sup>51</sup> The equilibrium constant ( $K_c$ ) can be written as

$$K_C = q_e/C_e \quad (12)$$

where ( $q_e$ ) is the amount of dye adsorbed per unit mass of adsorbent at equilibrium (mg g<sup>-1</sup>) and ( $C_e$ ) is the equilibrium concentration of dye in the solution (mg L<sup>-1</sup>).

$$\Delta G = -RT \ln K_C \quad (13)$$

The eqn (12) was employed to obtain  $\Delta G^\circ$ , where  $T$  is the temperature in Kelvin and  $R$  is the universal gas constant.

$$\ln K_C = -\frac{\Delta H^\circ}{RT} + \frac{\Delta S^\circ}{R} \quad (14)$$

From the slope and intercept of the  $\ln K_c$  against  $1/T$  plot (Fig. 9a) and based on the van't Hoff equation eqn (13),  $\Delta H^\circ$  and  $\Delta S^\circ$  were obtained, respectively.

The adsorption of BaTiO<sub>3</sub> and BaTiO<sub>3</sub>@ZnO composite is spontaneous, with values of  $\Delta G^\circ$  being negative at all temperatures studied. The positive  $\Delta H^\circ$  values confirm the endothermic adsorption, and the BaTiO<sub>3</sub>@ZnO composite showed a higher enthalpy, which indicates a stronger interaction with dyes. The positive values of ( $\Delta S^\circ$ ) indicate the increased disorder at the solid–liquid interface during the adsorption. The results confirm the thermodynamic and effectiveness benefits of the BaTiO<sub>3</sub>@ZnO composite for dye elimination (Table 6).



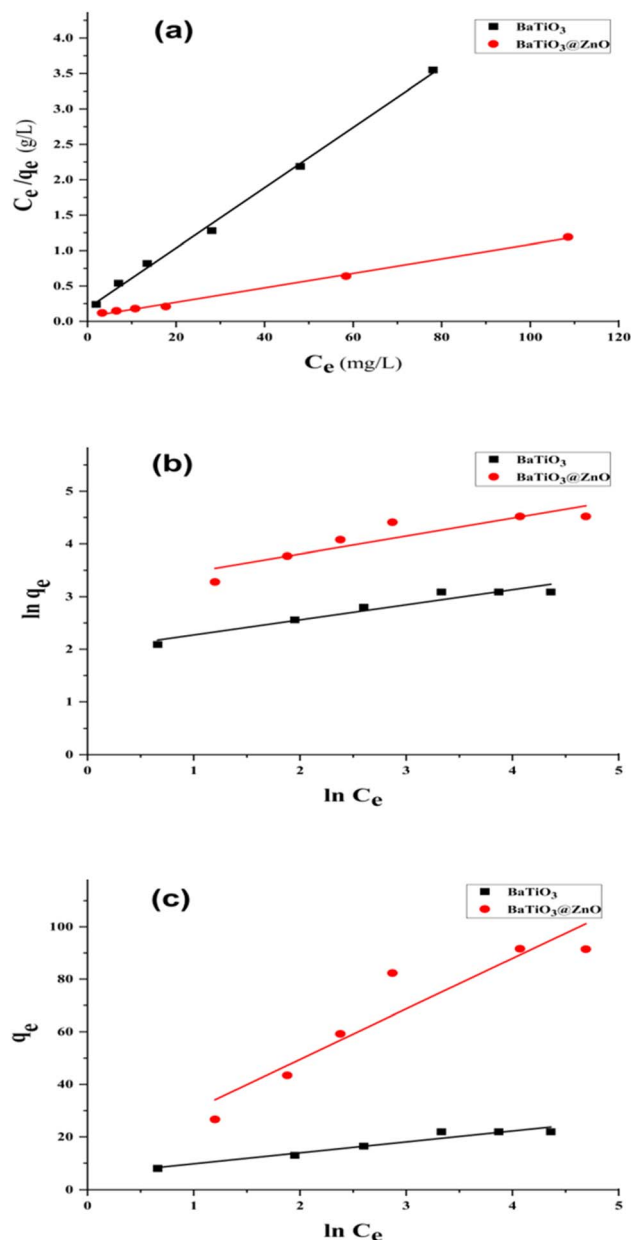


Fig. 8 (a) Langmuir plot; (b) Freundlich plot; (c) Temkin plot: for adsorption of CV onto BaTiO<sub>3</sub>@ZnO composite and BaTiO<sub>3</sub>.

Table 5 Isotherm parameters obtained for different models

Isotherm	BaTiO <sub>3</sub>		BaTiO <sub>3</sub> @ZnO composite	
	Parameters	Values	Parameters	Values
Experimental	$q_{\max}$ (mg g <sup>-1</sup> )	21.96	$q_{\max}$ (mg g <sup>-1</sup> )	91.60
	$R^2$	0.9966	$R^2$	0.9961
Langmuir	$q_{\max}$ (mg g <sup>-1</sup> )	23.49	$q_{\max}$ (mg g <sup>-1</sup> )	97.84
	$b$ (L mg <sup>-1</sup> )	0.2309	$b$ (L mg <sup>-1</sup> )	0.1559
	$R_L$	$7.9 \times 10^{-2}$	$R_L$	$4.1 \times 10^{-2}$
	$R^2$	0.9141	$R^2$	0.7757
Freundlich	$K_f$	7.27	$K_f$	22.86
	$n$	3.49	$n$	2.95
Temkin	$R^2$	0.9253	$R^2$	0.8520
	$K_T$ (L g <sup>-1</sup> )	3.85	$K_T$ (L g <sup>-1</sup> )	1.77
	$b_T$ (J mol <sup>-1</sup> )	$6.15 \times 10^2$	$b_T$ (J mol <sup>-1</sup> )	$1.33 \times 10^2$

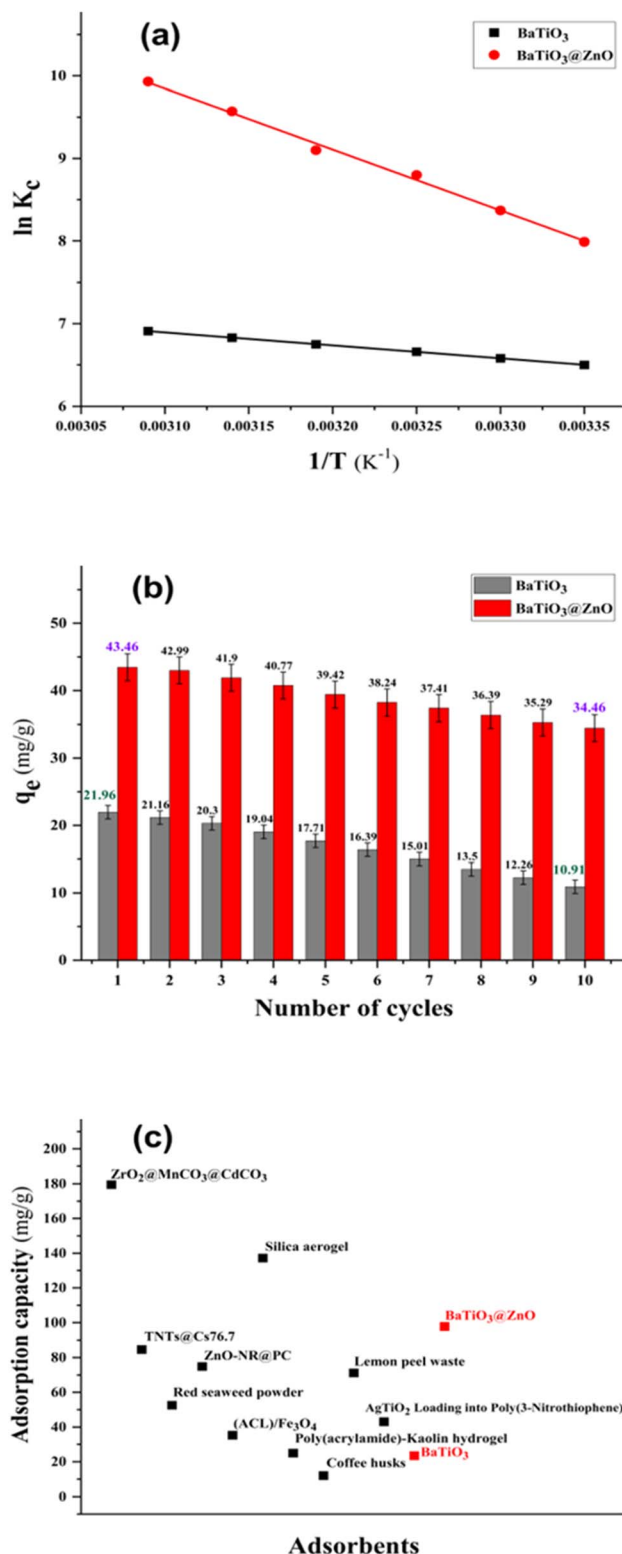


Fig. 9 (a) Van't Hoff plot for CV adsorption on BaTiO<sub>3</sub>@ZnO composite and BaTiO<sub>3</sub>; (b) adsorption of CV using the recycled adsorbents (BaTiO<sub>3</sub>@ZnO composite and BaTiO<sub>3</sub>) compared with a fresh one (conditions: initial dye concentration = 50 mg L<sup>-1</sup>, adsorbent dose = 10 mg, volume = 10 mL, temperature = 35 °C, equilibrium time = 360 min, pH = 8); (c) Scatter plot comparing the maximum adsorption capacity of BaTiO<sub>3</sub>@ZnO composite and BaTiO<sub>3</sub> with previously reported adsorbents for CV removal under various experimental conditions.



Table 6 Variables of thermodynamics at different temperatures

<i>T</i> (K)	BaTiO <sub>3</sub>			BaTiO <sub>3</sub> @ZnO composite		
	$\Delta G^\circ$ (kJ mol <sup>-1</sup> )	$\Delta H^\circ$ (kJ mol <sup>-1</sup> )	$\Delta S^\circ$ (kJ mol <sup>-1</sup> K <sup>-1</sup> )	$\Delta G^\circ$ (kJ mol <sup>-1</sup> )	$\Delta H^\circ$ (kJ mol <sup>-1</sup> )	$\Delta S^\circ$ (kJ mol <sup>-1</sup> K <sup>-1</sup> )
298	-16.106	13.06	0.0977	-19.793	61.36	0.272
303	-16.583			-21.090		
308	-17.070			-22.548		
313	-17.561			-23.689		
318	-18.055			-25.323		
323	-18.552			-26.687		

Table 7 Comparing adsorption capacity of BaTiO<sub>3</sub>@ZnO composite and BaTiO<sub>3</sub> with other adsorbents

Adsorbent	<i>q<sub>m</sub></i> (mg g <sup>-1</sup> )	References
ZnO <sub>2</sub> @MnCO <sub>3</sub> @CdCO <sub>3</sub> nanocomposite	179.52	53
Chemically activated carbon spheres TNTs@Cs76.7	84.7	54
Red seaweed powder	52.6	55
ZnO-NR@PC-derived from orange peel	74.89	56
Activated carbon prepared from lemon wood (ACL)/Fe <sub>3</sub> O <sub>4</sub> magnetic nanocomposite	35.3	57
Silica aerogel	137.17	58
Poly(acrylamide)-kaolin hydrogel	25.00	59
Coffee husks	12.04	60
Lemon peel waste	71.2	61
AgTiO <sub>2</sub> loading into poly(3-nitrothiophene)	43.10	62
ZnO	0.77	This work
BaTiO <sub>3</sub>	23.49	This work
BaTiO <sub>3</sub> @ZnO	97.84	This work

**3.2.10. Desorption and reusability.** As shown in Fig. 9b, the BaTiO<sub>3</sub>@ZnO composite kept a good ability to remove dye, with the adsorption capacity going down from 43.46 mg g<sup>-1</sup> in the first cycle to 34.46 mg g<sup>-1</sup> in the tenth cycle, and the BaTiO<sub>3</sub> showed an obvious decrease from 21.96 to 10.91 mg g<sup>-1</sup> for the same sequence. This indicates the potential of the BaTiO<sub>3</sub>@ZnO composite as a more stable and recyclable adsorbent and the suitability of BaTiO<sub>3</sub>@ZnO in the dye removal process. The retention of adsorption performance suggests good structural and chemical stability of the composite. In addition, the absence of significant performance degradation implies that Zn leaching is likely limited, which may be attributed to the strong interfacial interaction between BaTiO<sub>3</sub> and ZnO, as supported by the preserved crystalline features observed in XRD and FTIR analyses after reuse. These observations indicate that the composite exhibits considerable stability under repeated adsorption-desorption cycles.

**3.2.11. Comparison with other adsorbents.** Different adsorbents for CV and their adsorption capacities are exhibited in Table 7 and Fig. 9c. For comparison, the adsorption performance of unmodified ZnO toward CV was evaluated under identical experimental conditions. The results showed that unmodified ZnO exhibits a very low adsorption capacity (0.77 mg g<sup>-1</sup>), which is mainly attributed to its restricted surface area and insufficient functional groups for effective interactions. Consequently, adsorption is negligible and

predominantly confined to weak surface contacts rather than chemical bonding or pore entrapment.<sup>52</sup>

It is clear that the BaTiO<sub>3</sub>@ZnO composite has a good maximum adsorption capacity (97.84 mg g<sup>-1</sup>) compared to the others. This clearly demonstrates that the enhanced adsorption performance of the BaTiO<sub>3</sub>@ZnO composite originates from the synergistic interaction between BaTiO<sub>3</sub> and ZnO rather than from ZnO alone. This comparison highlights the relevance of the present study and demonstrates the competitive performance of the BaTiO<sub>3</sub>@ZnO composite for CV removal.

**3.2.12. Application to real samples and economic considerations.** To evaluate the method's efficiency and practicality for real samples, it was applied to remove and measure CV in different water samples, for example, Nile River water, sewage wastewater, and synthetic dye.<sup>22</sup> The samples were spiked with various concentrations of CV dye (5, 10, and 20 mg L<sup>-1</sup> of dye) under optimum conditions (adsorbent dose: 10 mg, solution volume: 10 mL, pH: 8, contact time: 360 min, and temperature: 35 °C). As demonstrated in Table 8, the BaTiO<sub>3</sub>@ZnO composite achieved a recovery percentage between 86.7% and 94.8% with a relative standard deviation (RSD%) of 1.27–2.70. While BaTiO<sub>3</sub> exhibited a recovery percentage ranging from 59.8% to 89.8% and RSD% from 1.53 to 2.88. The improved performance of BaTiO<sub>3</sub>@ZnO is linked to its increased surface activity, whereas the slight reduction in complex water samples could be a result of competing ions and organic substances. The results confirm that the BaTiO<sub>3</sub>@ZnO composite is suitable for treating real wastewater.





Table 8 Determination of CV in different real samples

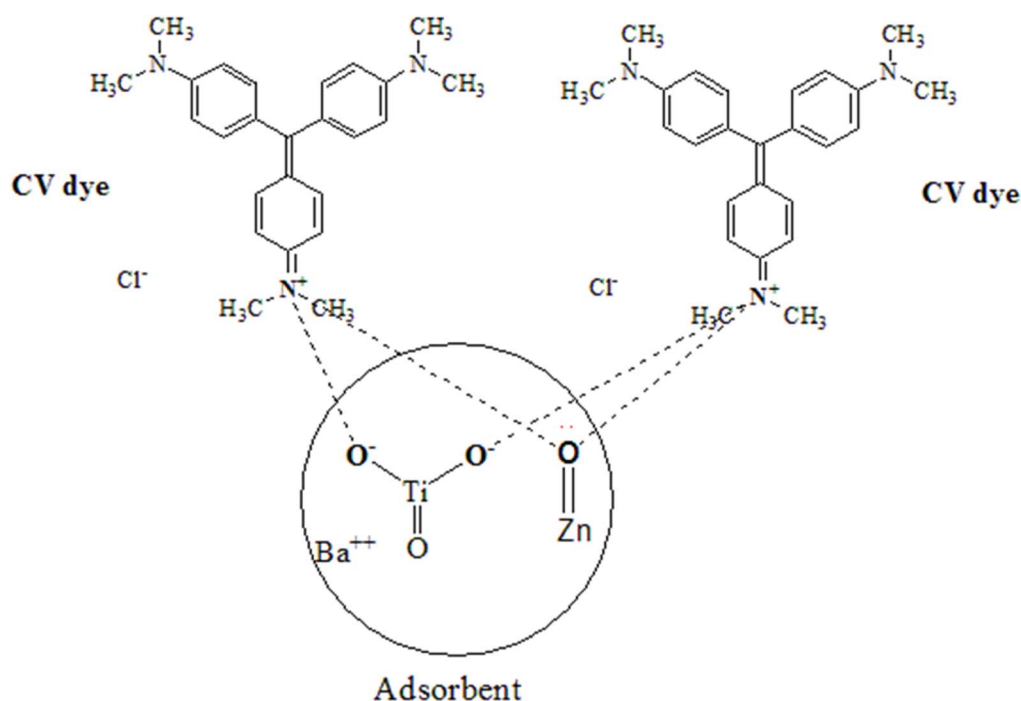
Sample	CV added (mg L <sup>-1</sup> )	BaTiO <sub>3</sub>			BaTiO <sub>3</sub> @ZnO		
		CV found (mg L <sup>-1</sup> )	Recovery (%)	RSD <sup>a</sup> (%)	CV found (mg L <sup>-1</sup> )	Recovery (%)	RSD <sup>a</sup> (%)
Distilled water	—	—	—	—	—	—	—
	5	4.49	89.81	1.53	4.74	94.77	2.33
	10	8.07	80.72	2.22	9.30	92.98	1.93
	20	12.99	64.94	2.44	18.15	90.77	2.28
Synthetic dye	—	—	—	—	—	—	—
	5	4.45	88.98	2.17	4.70	93.94	2.35
	10	7.91	79.06	2.09	9.16	91.60	1.95
	20	12.75	63.73	2.27	17.91	89.53	2.46
Nile river water	—	—	—	—	—	—	—
	5	4.38	87.60	2.52	4.64	92.84	2.08
	10	7.78	77.78	2.36	9.06	90.63	2.58
	20	12.26	61.29	2.25	17.59	87.95	1.72
Sewage wastewater	—	—	—	—	—	—	—
	5	4.31	86.23	2.56	4.59	91.74	2.70
	10	7.59	75.90	2.54	9.01	90.08	1.38
	20	11.96	59.78	2.88	17.34	86.71	1.27

<sup>a</sup> For RSD, ( $n = 3$ ).

Although BaTiO<sub>3</sub> and ZnO are not traditionally low-cost adsorbents, the synthesis procedure presented in this study is a solvent-free solid-state route that eliminates organic solvents, surfactants, or complex post-treatment steps. This significantly reduces material and operational costs. The synthesis also employs commercially available precursors, enabling large-scale production. The energy consumption in synthesis can also be minimized by controlling calcination temperature or using other low-energy techniques such as microwave-assisted,

mechanochemical, and hydrothermal methods, which are claimed to reduce the synthesis temperatures while maintaining material performance. The higher adsorption efficiency, chemical stability, and reusability of the BaTiO<sub>3</sub>@ZnO composite make it a good candidate for wastewater treatment applications, where regeneration and durability are critical.

**3.2.13. Probable adsorption mechanism.** The interaction mechanism between CV and the BaTiO<sub>3</sub>@ZnO composite may be a mix of chemisorption and electrostatic interactions

Fig. 10 adsorption mechanism of CV onto BaTiO<sub>3</sub>@ZnO composite.

(Fig. 10). FTIR analysis and kinetic data suggest that chemisorption takes place. The Langmuir isotherm shows that monolayer adsorption occurs on a uniform surface. The thermodynamic study points out that the process is spontaneous and endothermic, which indicates a strong interaction between the dye and the adsorbent. ZnO improves the surface properties of BaTiO<sub>3</sub> by increasing the number of active sites and boosting the interaction with the positively charged dye molecules. The adsorption of CV onto BaTiO<sub>3</sub>@ZnO is done through chemical bonding, surface attraction, and better surface activity. The BaTiO<sub>3</sub>@ZnO composite is an efficient adsorbent for eliminating CV from wastewater.

From a mechanistic perspective, the adsorption of crystal violet onto the BaTiO<sub>3</sub>@ZnO composite can be further described as a multistep process involving initial surface interactions followed by diffusion-controlled transport. Surface charge plays a critical role during the early stage of adsorption, where electrostatic attraction between the positively charged CV molecules and negatively charged surface sites of the composite facilitates rapid dye uptake. This electrostatic contribution is inherently dependent on solution pH and enhances the accessibility of available active sites. In addition to electrostatic interactions, possible chemical interactions between surface functional groups and dye molecules contribute to the overall adsorption mechanism, as inferred from FTIR spectral features and kinetic behavior. The incorporation of ZnO influences the interfacial properties of the composite by increasing surface heterogeneity and modifying charge distribution, thereby strengthening adsorbent–adsorbate interactions relative to pure BaTiO<sub>3</sub>. Furthermore, diffusion pathways also play a role in governing the adsorption kinetics. The contact-time-dependent adsorption behavior suggests the involvement of both surface adsorption and intraparticle diffusion in controlling the overall uptake rate of CV molecules. It should be emphasized that the proposed adsorption mechanism is inferred from correlative experimental observations rather than directly validated by advanced surface-sensitive techniques such as XPS, zeta potential measurements as a function of pH, or SEM-EDX elemental mapping.

## 4. Conclusion

In this study, the BaTiO<sub>3</sub>@ZnO composite was easily prepared and adopted as an adsorbent to remove CV from an aqueous solution. The characterization of the BaTiO<sub>3</sub>@ZnO composite was executed using XRD, FTIR, SEM-EDX, TEM, BET, and pH<sub>ZPC</sub>. The experimental factors, such as pH, initial dye concentration, adsorbent dosage, contact time, temperature, and ionic strength, influence the adsorption of CV onto BaTiO<sub>3</sub> and BaTiO<sub>3</sub>@ZnO composite. The maximum adsorption capacity of BaTiO<sub>3</sub> and BaTiO<sub>3</sub>@ZnO composite can attain 23.49 and 97.84 mg g<sup>−1</sup>, respectively. Both adsorbents obeyed the Langmuir isotherm and the pseudo-second-order kinetic model, which demonstrated monolayer coverage on the surface and chemisorption as the main mechanism. Thermodynamic results suggest that the adsorption of CV onto BaTiO<sub>3</sub> and the BaTiO<sub>3</sub>@ZnO composite was endothermic, spontaneous, and

feasible. Both adsorbents can be recycled and reused for up to ten consecutive cycles, showing a gradual decrease in adsorption performance. The results confirmed that the BaTiO<sub>3</sub>@ZnO composite is better and more effective than BaTiO<sub>3</sub> due to the addition of ZnO to BaTiO<sub>3</sub>, which enhances surface area and porosity and facilitates the electrostatic attraction with CV molecules. The BaTiO<sub>3</sub>@ZnO composite is an eco-friendly and inexpensive adsorbent and has potential for the remediation of wastewater contaminated with dyes. Further investigations using advanced surface characterization techniques are required to provide direct evidence of interfacial bonding and electrostatic contributions in the BaTiO<sub>3</sub>@ZnO composite, and future work needs to study another metal oxide with BaTiO<sub>3</sub> or add a third ingredient to the composite for the elimination of cationic dyes from aqueous solution.

## Author contribution

Ahmed Barakat: data curation, investigation, methodology, writing – original draft. Magdi E. Khalifa: conceptualization, data curation, investigation, methodology, supervision, writing – review & editing. A. M. Abdelghany: data curation, investigation, methodology and reviewing. Wael I. Mortada: conceptualization, data curation, investigation, methodology, supervision, writing – review & editing.

## Conflicts of interest

The authors declare no competing interests.

## Data availability

Data supporting this study are included within the article.

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