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# Tailoring carbon shell thickness in graphene–Li<sub>2</sub>S–carbon nanocomposite cathodes for enhanced polysulfide control and electrochemical stability

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Lithium–sulfur (Li–S) batteries are promising next-generation energy storage systems due to their high theoretical energy density and the abundance of sulfur; however, their practical application is severely limited by the poor electrical and ionic conductivity of Li<sub>2</sub>S and the dissolution of intermediate polysulfides. In this work, a comprehensive multiphysics simulation study is conducted to investigate the influence of carbon shell thickness (0–20 nm) on the electrochemical, thermal, and ionic performance of graphene–Li<sub>2</sub>S–carbon nanocomposite cathodes under experimentally realizable conditions (1C discharge rate and 35 °C). The model, developed using COMSOL Multiphysics, couples heat transfer, ion transport, and electric current conservation to capture the complex interactions governing cathode behavior. To ensure experimental relevance and reliability, the simulation results are rigorously validated against reported experimental voltage–capacity data for graphene–Li<sub>2</sub>S–carbon cathodes, achieving a low root mean square error of 0.09 V. The results reveal that a carbon shell thickness of approximately 10 nm provides an optimal balance between polysulfide confinement and lithium-ion transport, leading to minimized temperature rise, reduced ionic resistance, and improved current-density uniformity. By establishing a quantitative agreement with experimental literature, this study offers a predictive and experimentally grounded framework for the rational design and optimization of high-performance Li–S battery cathodes.

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## 1. Introduction

Lithium–sulfur (Li–S) batteries are a promising energy storage technology due to their high theoretical energy density of 2600 Wh kg<sup>−1</sup>, far surpassing conventional lithium-ion batteries, and the use of sulfur, which is abundant, low-cost, and environmentally friendly.<sup>1,2</sup> These attributes make Li–S batteries attractive for applications like electric vehicles and grid storage. However, their practical deployment is challenged by several limitations stemming from the complex electrochemical and chemical interactions at the cathode–electrolyte interface. The primary issues include the low electrical and ionic conductivity of sulfur ( $\sim 10^{-5}$  S m<sup>−1</sup>) and its discharge product, lithium sulfide (Li<sub>2</sub>S,  $\sim 10^{-8}$  S m<sup>−1</sup>), which hinders efficient electron and ion transport. Additionally, the dissolution of intermediate polysulfides (e.g., Li<sub>2</sub>S<sub>8</sub>, Li<sub>2</sub>S<sub>6</sub>) into the electrolyte causes the “shuttle effect,” where these species migrate to the anode, leading to active material loss, parasitic reactions, and electrolyte decomposition. These factors collectively degrade capacity retention and cycle life, limiting the battery’s performance and longevity.<sup>3–8</sup> To overcome these challenges, innovative cathode designs are essential to enhance conductivity, suppress

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polysulfide shuttling, and stabilize the electrode–electrolyte interface.<sup>9–11</sup>

Recent research has focused on composite cathodes incorporating carbon-based materials like graphene, carbon nanotubes, and porous carbon shells to address these issues.<sup>12–14</sup> Graphene, with its high electrical conductivity ( $\sim 10^4 \text{ S m}^{-1}$ ) and tunable surface chemistry, is particularly effective, as it can physically or chemically trap polysulfides, reducing their dissolution into the electrolyte.<sup>15–17</sup> Encapsulating  $\text{Li}_2\text{S}$  particles with a carbon shell further improves electron and ion transport while acting as a protective barrier against electrolyte interactions, minimizing side reactions.<sup>18–20</sup> However, the thickness of the carbon shell is a critical parameter. Thicker shells may increase tortuosity and resistance, impeding ion diffusion, while thinner shells might not sufficiently confine polysulfides, allowing leakage and shuttle effects.<sup>21–23</sup> Optimizing this balance requires a deep understanding of the interplay between thermal, ionic, and electrical properties, which govern the cathode's electrochemical kinetics and chemical stability.<sup>24–26</sup> Advanced multiphysics modeling, such as that enabled by COMSOL Multiphysics, can elucidate these interactions by simulating coupled phenomena like heat dissipation, ion transport, and electrochemical reactions, providing a predictive framework for designing high-performance Li–S cathodes.<sup>27–29</sup> Such approaches are crucial for translating the theoretical potential of Li–S batteries into practical, high-efficiency energy storage systems.

Recent advances in lithium–sulfur battery research have highlighted that the electrochemical performance of composite sulfur cathodes is strongly governed by the structural characteristics of the carbon host and substrate. In particular, parameters such as carbon thickness, porosity, electrical conductivity, and host morphology critically influence lithium-ion transport, electronic percolation, and polysulfide confinement, especially under practical conditions such as high sulfur loading and lean electrolyte operation.<sup>3,30</sup> Recent experimental studies on low-dimensional carbon composites, including graphene, carbon nanotube, and foam-based architectures, demonstrate that insufficient carbon thickness or poorly interconnected frameworks lead to severe polysulfide shuttling, while excessively thick or densely packed carbon hosts increase ionic tortuosity and polarization, thereby limiting rate capability.<sup>31,32</sup> These findings underscore the necessity of quantitatively understanding the trade-offs associated with carbon-host structural design, motivating the present simulation-based investigation of carbon shell thickness in graphene– $\text{Li}_2\text{S}$ –carbon composite cathodes under experimentally realistic conditions.

Multiphysics modeling, particularly using COMSOL Multiphysics, has emerged as a powerful tool for elucidating complex interactions in Li–S batteries by simulating coupled thermal, ionic, and electrical phenomena, providing quantitative insights into how material properties and structural parameters, such as carbon shell thickness, influence performance.<sup>33,34</sup> By integrating governing equations like the Nernst–Planck equation for ion transport, heat transfer equations, and current conservation laws, COMSOL's flexible finite element framework

accurately captures nonlinear feedback loops between temperature, ion concentration, and electrochemical reactions, enabling precise discretization of complex geometries like spherical  $\text{Li}_2\text{S}$  particles encapsulated by carbon shells.<sup>35–37</sup> This approach outperforms simpler models and tools like ANSYS or MATLAB by offering a holistic view of cathode behavior, addressing temperature-dependent ionic conductivity, ohmic heating, and reaction-driven heat sources, which are critical for mitigating polysulfide dissolution and concentration polarization in Li–S systems.<sup>38,39</sup> Given the intricate chemical and electrochemical challenges in these batteries, where experimental trial-and-error approaches fall short, COMSOL's ability to validate simulations against experimental data, such as voltage–capacity profiles, ensures reliability and makes it indispensable for optimizing cathode designs and enhancing battery longevity.<sup>40,41</sup>

This study employs a COMSOL Multiphysics-based model to investigate the effect of carbon shell thickness (0, 5, 10, 15, and 20 nm) on the performance of graphene– $\text{Li}_2\text{S}$ –carbon nanocomposite cathodes in Li–S batteries under a 1C discharge rate at 35 °C. By coupling heat transfer, ion transport, and electric current modules, the model quantifies thermal, ionic, and electrical responses, with a focus on chemical stability and polysulfide control. Validated with an RMSE of 0.09 V against experimental data, the results identify a 10 nm shell as optimal, minimizing temperature rise, ionic resistance, and polysulfide dissolution while enhancing electrochemical kinetics. These findings provide a predictive framework for designing high-performance Li–S cathodes, addressing key chemical challenges for sustainable energy storage.

## 2. Model and simulation methodology

### 2.1. Model structure

To investigate the effect of carbon shell thickness on the thermal–ionic–electrical performance of the graphene– $\text{Li}_2\text{S}$ –carbon cathode in lithium–sulfur batteries, a two-dimensional (2D) axisymmetric model was developed. The model consists of a spherical  $\text{Li}_2\text{S}$  particle with a fixed radius, encapsulated by an annular carbon shell with variable thicknesses (0, 5, 10, 15, and 20 nm). The surrounding medium is a liquid electrolyte with properties consistent with those reported in ref. 42. A constant current boundary condition corresponding to a 1C discharge rate was applied to simulate the operational conditions of the battery at an optimal operating temperature of 35 °C.

### 2.2. Governing equations and modules

To comprehensively investigate the thermal, ionic, and electrical behavior of the graphene– $\text{Li}_2\text{S}$ –carbon cathode in lithium–sulfur batteries, a multiphysics modeling approach was adopted. The simulations were conducted using COMSOL Multiphysics, a finite element analysis software capable of coupling multiple physical phenomena. The model integrates three primary modules: Heat Transfer in Solids, Transport of



Diluted Species, and Electric Currents. These modules are interconnected to account for the complex interplay between thermal, ionic, and electrical processes within the cathode system. Below, each module is described in detail, including the governing equations, assumptions, and their coupling mechanisms, ensuring a robust framework for analyzing the effect of carbon shell thickness on the cathode's performance.

**2.2.1. Heat transfer in solids.** The thermal behavior of the cathode system, comprising the  $\text{Li}_2\text{S}$  particle, carbon shell, and surrounding liquid electrolyte, is governed by the transient heat transfer equation. This equation accounts for heat conduction and the heat generated by electrochemical reactions and resistive losses. The governing equation is expressed as:<sup>43</sup>

$$\rho C_p \frac{\partial T}{\partial t} = \nabla \cdot (k \nabla T) + Q \quad (1)$$

where  $\rho$  ( $\text{kg m}^{-3}$ ) is the density,  $C_p$  ( $\text{J (kg K)}^{-1}$ ) is the specific heat capacity,  $T$  (K) is the temperature,  $k$  ( $\text{W (m K)}^{-1}$ ) is the thermal conductivity, and  $Q$  ( $\text{W m}^{-3}$ ) is the volumetric heat source. The heat source  $Q$  encapsulates contributions from electrochemical reaction heat (exothermic/endothermic processes) and ohmic heating due to ionic and electronic resistances. The thermal conductivity of the  $\text{Li}_2\text{S}$  particle is relatively low, necessitating the carbon shell to enhance heat dissipation. The electrolyte's thermal properties were assumed isotropic, with values derived from the reference study.<sup>42</sup> Boundary conditions included an initial uniform temperature of 35 °C (308.15 K) across the system and an adiabatic condition (zero heat flux) at the outer boundaries to simulate an insulated environment. This module captures the temperature distribution, which is critical for assessing the thermal stability of the cathode under operational conditions, as elevated temperatures can degrade performance and accelerate side reactions.

**2.2.2. Transport of diluted species.** The transport of  $\text{Li}^+$  ions within the electrolyte and through the carbon shell is modeled using the Nernst–Planck equation, which accounts for diffusion, migration, and convection (though convection is neglected due to the static nature of the system). The governing equation is:<sup>44</sup>

$$\frac{\partial c}{\partial t} = \nabla \cdot (D \nabla c + z \mu F c \nabla \phi) \quad (2)$$

where  $c$  ( $\text{mol m}^{-3}$ ) is the  $\text{Li}^+$  ion concentration,  $D$  ( $\text{m}^2 \text{s}^{-1}$ ) is the diffusion coefficient,  $z$  is the charge number ( $z = 1$  for  $\text{Li}^+$ ),  $\mu$  ( $\text{m}^2 \text{V s}^{-1}$ ) is the ionic mobility,  $F$  ( $96\,485 \text{ C mol}^{-1}$ ) is the Faraday constant, and  $\phi$  (V) is the electric potential. The ionic mobility is related to the diffusion coefficient *via* the Einstein relation:<sup>45</sup>

$$\mu = \frac{DzF}{RT} \quad (3)$$

where  $R$  is the universal gas constant ( $8.314 \text{ J (mol K)}^{-1}$ ) and  $T$  is the temperature in kelvin. The diffusion coefficient for  $\text{Li}^+$  ions in the electrolyte was sourced from,<sup>42</sup> while the carbon shell's porous structure was modeled with an effective diffusion coefficient adjusted for porosity and tortuosity. Boundary conditions included a zero flux for  $\text{Li}^+$  ions at the solid boundaries of the  $\text{Li}_2\text{S}$  particle and carbon shell, and a uniform initial

concentration in the electrolyte, set to  $1.0 \text{ mol m}^{-3}$  based on typical lithium–sulfur battery electrolyte compositions. This module is essential for understanding ion transport limitations, which directly influence the electrochemical performance and capacity retention of the cathode.

The carbon shell's porous structure is modeled with an effective diffusion coefficient adjusted for porosity ( $\epsilon$ ) and tortuosity ( $\tau$ ) using the Bruggeman relation:<sup>44</sup>

$$D_{\text{eff}} = \frac{D \cdot \epsilon^{1.5}}{\tau} \quad (4)$$

where  $D$  is the bulk diffusion coefficient. Baseline values (porosity  $\epsilon \approx 0.4$ – $0.6$ , tortuosity  $\tau \approx 2$ – $3$ ) were derived from experimental data in ref. 42. Higher porosity enhances electrolyte infiltration and reduces ionic resistance, while increased tortuosity (*e.g.*, in thicker shells) impedes ion diffusion paths, leading to higher concentration gradients and polarization. These parameters were sensitivity-tested ( $\pm 20\%$  variation) in Section 3.5, confirming their strong influence on ion transport and overall electrochemical stability.

**2.2.3. Electric currents.** The distribution of electric potential and current density in the electrode and electrolyte phases is modeled using the current conservation equation, assuming steady-state conditions for electrical conduction:<sup>46</sup>

$$\nabla \cdot (\sigma \nabla \phi) = 0 \quad (5)$$

where  $\sigma$  ( $\text{S m}^{-1}$ ) is the electrical conductivity and  $\phi$  (V) is the electric potential. The electrical conductivity of the  $\text{Li}_2\text{S}$  particle is low, necessitating the carbon shell to enhance electron transport to the reaction sites. The carbon shell's conductivity was modeled as a function of its thickness, with values derived from.<sup>42</sup>

In the electrolyte, ionic conductivity dominates, and its temperature dependence was incorporated using an Arrhenius-type relationship:

$$\sigma = \sigma_0 \exp\left(-\frac{E_a}{RT}\right) \quad (6)$$

where  $\sigma_0$  is a pre-exponential factor and  $E_a$  is the activation energy. Boundary conditions included a fixed potential at the cathode boundary (set to the open-circuit potential of  $\text{Li}_2\text{S}$ , approximately 2.1 V *vs.*  $\text{Li/Li}^+$ ) and a constant current density at the electrolyte boundary corresponding to a 1C discharge rate (based on the theoretical capacity of  $\text{Li}_2\text{S}$ ,  $1166 \text{ mAh g}^{-1}$ ). This module enables the analysis of current density uniformity, which is critical for minimizing polarization losses and ensuring efficient electrochemical reactions.

**2.2.4. Coupled physics.** The thermal, ionic, and electrical modules are intricately coupled to reflect the multiphysics nature of the battery system. The heat source  $Q$  in the heat transfer equation is a function of both ohmic heating and reaction heat, which depends on the local current density and overpotential derived from the Electric Currents module. The temperature distribution from the Heat Transfer module influences the material properties in the other modules, such as the ionic conductivity of the electrolyte and the diffusion



coefficient of  $\text{Li}^+$  ions, both of which follow Arrhenius-type temperature dependencies. Additionally, the electric potential gradient from the Electric Currents module drives the migration term in the Nernst–Planck equation, linking ion transport to the electrical field. This coupling ensures that the model captures the feedback loops between thermal effects, ion transport, and electrochemical performance. For instance, a rise in temperature due to heat generation can enhance ionic conductivity but may also exacerbate side reactions, affecting long-term stability.

**2.2.5. Numerical implementation.** The governing equations were discretized using the finite element method in COMSOL Multiphysics. A 2D axisymmetric geometry was employed to reduce computational complexity while maintaining accuracy for the spherical  $\text{Li}_2\text{S}$  particle and carbon shell. The mesh was refined near the particle–electrolyte interface to capture steep gradients in temperature, ion concentration, and potential. A time-dependent solver was used for the Heat Transfer and Transport of Diluted Species modules, with a time step of 0.1 s to ensure numerical stability. The Electric Currents module was solved in a stationary state, as electrical transients are typically faster than thermal and ionic processes. Convergence was ensured by monitoring residuals and using adaptive mesh refinement. The computational domain extended sufficiently into the electrolyte to minimize boundary effects, with a domain size 10 times the particle radius.

### 2.3. Parameters and boundary conditions

Material parameters (electrical conductivity, ionic conductivity, diffusion coefficient, and specific heat capacity) were extracted from.<sup>42</sup> The initial and boundary conditions were defined as follows:

- (1) Initial temperature: uniform temperature of 35 °C across the system.
- (2) Current rate: constant current equivalent to a 1C discharge rate (based on the theoretical capacity of  $\text{Li}_2\text{S}$ , 1166 mAh g<sup>-1</sup>).
- (3) Thermal boundary conditions: zero heat flux at the outer boundaries (adiabatic conditions).
- (4) Electrical boundary conditions: fixed potential at the cathode boundary and constant current at the electrolyte boundary.
- (5) Mass transport boundary conditions: zero flux for  $\text{Li}^+$  ions at solid boundaries and uniform initial concentration in the electrolyte.

In addition to the baseline parameters, this study incorporates critical cell-fabrication variables to address their impact on electrochemical performance. The proportion of insulating active material is modeled by varying the  $\text{Li}_2\text{S}$  volume fraction (baseline: 50%, varied  $\pm 20\%$  to 40–60%) within the nanocomposite, affecting overall conductivity and tortuosity. The amount of electrolyte is represented by the electrolyte-to-sulfur (E/S) ratio (baseline: 10  $\mu\text{L}$  per mg S, varied  $\pm 20\%$  to 8–12  $\mu\text{L}$  per mg S) through adjustments to the electrolyte domain size in the 2D axisymmetric model. The amount of lithium (lithium excess) is approximated in a full-cell context by varying the

lithium concentration at the anode boundary (baseline: 100% excess, varied  $\pm 20\%$  to 80–120%), influencing polysulfide shuttling and reversibility. These parameters were integrated into the coupled modules to simulate their effects on thermal, ionic, and electrical outputs.

### 2.4. Model validation

To ensure that the proposed lithium–sulfur battery conditions are experimentally realizable and that the numerical predictions are reliable, the developed multiphysics model was validated against experimental data reported in the literature. Specifically, voltage–capacity profiles from Wu *et al.*,<sup>39</sup> who experimentally investigated graphene– $\text{Li}_2\text{S}$ –carbon nanocomposite cathodes under comparable conditions, were used as a benchmark. The experimental system in ref. 42 closely matches the present model in terms of cathode chemistry, carbon-coated  $\text{Li}_2\text{S}$  architecture, electrolyte composition, and operating conditions. Simulated discharge curves at C/2, 1C, and 2C rates were directly compared with the experimental results. The root mean square error (RMSE) between simulated and experimental voltages was calculated to be 0.09 V, indicating excellent quantitative agreement. The RMSE is defined as:

$$\text{RMSE} = \sqrt{\frac{1}{N} \sum_{i=1}^N (V_{\text{sim},i} - V_{\text{exp},i})^2} \quad (7)$$

where  $V_{\text{sim},i}$  and  $V_{\text{exp},i}$  are the simulated and experimental voltages, respectively, at the  $i$ -th data point, and ( $N$ ) is the total number of data points compared. The calculated RMSE for the voltage–capacity profiles was 0.09 V, indicating a high degree of agreement between the simulated and experimental results (Fig. 1). This RMSE value is considered acceptable within the

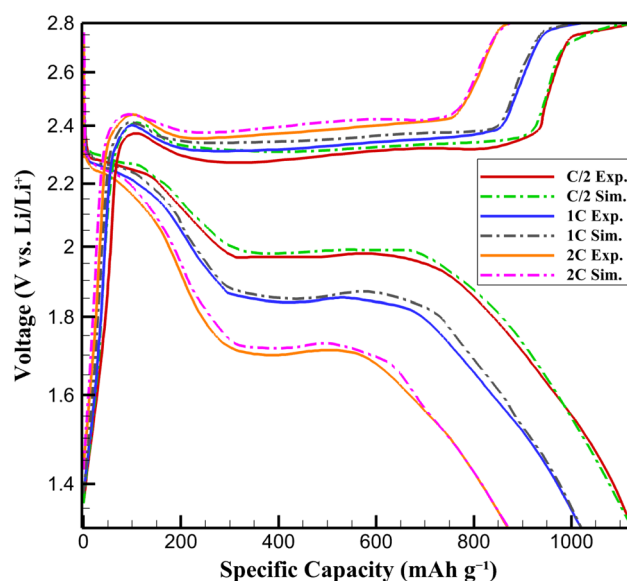


Fig. 1 Comparison of experimental<sup>42</sup> and simulated voltage–capacity profiles of graphene– $\text{Li}_2\text{S}$ –carbon nanocomposite cathode at C/2, 1C, and 2C rates.





**Table 1** Effect of  $\pm 20\%$  variation in key parameters on cathode performance (10 nm carbon shell, 1C discharge, 35 °C)

Parameter	Variation	$T_{\max}$ (°C)	$\Delta T_{\max}$ (%)	$R_{\text{ion}}$ ( $\Omega \text{ cm}^2$ )	$\Delta R_{\text{ion}}$ (%)	$\sigma_j$ ( $\text{mA cm}^{-2}$ )	$\Delta \sigma_j$ (%)
$\text{Li}^+$ diffusivity	20%	36.3	−0.55	7.2	−15.3	0.21	−16
( $D_0 = 1.0 \times 10^{-10} \text{ m}^2 \text{ s}^{-1}$ )	−20%	36.8	0.82	10.2	20	0.33	32
Ionic conductivity	20%	36.4	−0.27	7.3	−14.1	0.22	−12
( $\sigma_0 = 1.2 \times 10^{-2} \text{ S m}^{-1}$ )	−20%	36.7	0.55	9.9	16.5	0.29	16
Thermal conductivity	20%	36.2	−0.82	8.4	−1.2	0.24	−4
( $k_0 = 100 \text{ W m}^{-1} \text{ K}^{-1}$ )	−20%	36.8	0.82	8.6	1.2	0.26	4
$\text{Li}_2\text{S}$ volume fraction	+20% (60%)	36.9	1.1	10.5	23.5	0.35	40
(baseline: 50%)	−20% (40%)	36.2	−0.82	7	−17.6	0.2	−20
E/S ratio	+20% (12 $\mu\text{L}$ per mg S)	36.4	−0.27	8	−5.9	0.23	−8
(baseline: 10 $\mu\text{L}$ per mg S)	−20% (8 $\mu\text{L}$ per mg S)	36.7	0.55	9.5	11.8	0.28	12
Lithium excess	+20% (120%)	36.3	−0.55	8.1	−4.7	0.22	−12
(baseline: 100%)	−20% (80%)	36.8	0.82	9.2	8.2	0.3	20

context of lithium–sulfur battery modeling, where complex electrochemical phenomena, such as polysulfide dissolution and side reactions, introduce variability in experimental data. The low RMSE confirms that the model effectively captures the dominant electrochemical and transport processes governing the cathode's performance.

Furthermore, all operating parameters employed in this study (namely a 1C discharge rate, an operating temperature of 35 °C, electrolyte-to-sulfur ratios of 8–12  $\mu\text{L mg}^{-1}$ , and  $\text{Li}_2\text{S}$ -based composite cathodes) fall within ranges commonly used in laboratory-scale lithium–sulfur battery experiments. This confirms that the simulated battery conditions are fully realizable in practical experimental setups. The close agreement between simulation and experimental data, together with the use of experimentally relevant parameters, validates the model's capability to capture the dominant electrochemical, thermal, and transport processes governing Li–S battery behavior. Consequently, the trends and optimization insights derived from this simulation study are expected to be directly transferable to experimental cathode design.

## 2.5. Sensitivity analysis

To evaluate the robustness of the developed multiphysics model and to determine the relative influence of material parameters on the cathode performance, a sensitivity analysis was conducted. Three key parameters were selected:

- (1)  $\text{Li}^+$  diffusivity in the electrolyte ( $D_0 = 1.0 \times 10^{-10} \text{ m}^2 \text{ s}^{-1}$ )
- (2) Ionic conductivity of the electrolyte ( $\sigma_0 = 1.2 \times 10^{-2} \text{ S m}^{-1}$  at 35 °C)
- (3) Thermal conductivity of the carbon shell ( $k_0 = 100 \text{ W m}^{-1} \text{ K}^{-1}$ )

Each parameter was varied by  $\pm 20\%$  relative to its baseline value, while keeping other parameters constant. The influence of these variations was analyzed on three primary outputs: maximum cathode temperature ( $T_{\max}$ ), total ionic resistance ( $R_{\text{ion}}$ ), and current density non-uniformity ( $\sigma_j$ ). The sensitivity analysis was extended to include three additional cell-fabrication parameters:  $\text{Li}_2\text{S}$  volume fraction (baseline: 50%), E/S ratio (baseline: 10  $\mu\text{L}$  per mg S), and lithium excess (baseline: 100%). Each was varied by  $\pm 20\%$ , and their impacts on maximum cathode temperature ( $T_{\max}$ ), total ionic resistance

( $R_{\text{ion}}$ ), and current density non-uniformity ( $\sigma_j$ ) were evaluated for the optimal 10 nm carbon shell under 1C discharge at 35 °C. The extended results are summarized in Table 1.

Additionally, porosity ( $\epsilon$ ) and tortuosity ( $\tau$ ) of the carbon shell were varied by  $\pm 20\%$  (baseline:  $\epsilon = 0.5$ ,  $\tau = 2.5$ ) to assess their impact on ion transport. A 20% decrease in porosity or increase in tortuosity elevates ionic resistance by  $\sim 15$ –20% and worsens current density uniformity (e.g.,  $\sigma_j$  increases to  $0.33 \text{ mA cm}^{-2}$ ), highlighting their role in mitigating polysulfide shuttling and polarization.

## 3. Results and discussion

This section presents the simulation results for the graphene– $\text{Li}_2\text{S}$ -carbon cathode in lithium–sulfur batteries, focusing on the impact of carbon shell thickness (0, 5, 10, 15, and 20 nm) on thermal, ionic, and electrical performance under a 1C discharge rate at 35 °C. The results are analyzed through temperature profiles, current density uniformity, ionic resistance, and  $\text{Li}^+$  ion concentration distributions. The findings are validated against experimental data from Wu *et al.*,<sup>42</sup> as discussed in Section 3.4.

### 3.1. Maximum temperature comparison

The maximum temperature within the cathode was evaluated to assess thermal management as a function of carbon shell thickness. Fig. 2 shows maximum temperatures for different carbon shell thicknesses. For the uncoated  $\text{Li}_2\text{S}$  particle (0 nm), the maximum temperature reached 38.2 °C due to significant heat generation from electrochemical reactions and poor thermal conductivity of  $\text{Li}_2\text{S}$ . With a 5 nm carbon shell, the maximum temperature decreased to 37.1 °C, reflecting the enhanced thermal conductivity of the carbon layer. The 10 nm shell yielded the lowest maximum temperature of 36.5 °C, indicating optimal heat dissipation due to a balance between thermal conductivity and shell thickness. For 15 nm and 20 nm shells, the maximum temperatures increased slightly to 36.7 °C and 36.9 °C, respectively, suggesting that thicker shells introduce thermal resistance, limiting further heat dissipation. These results highlight that a 10 nm carbon shell is optimal for minimizing temperature rise, which is critical for preventing



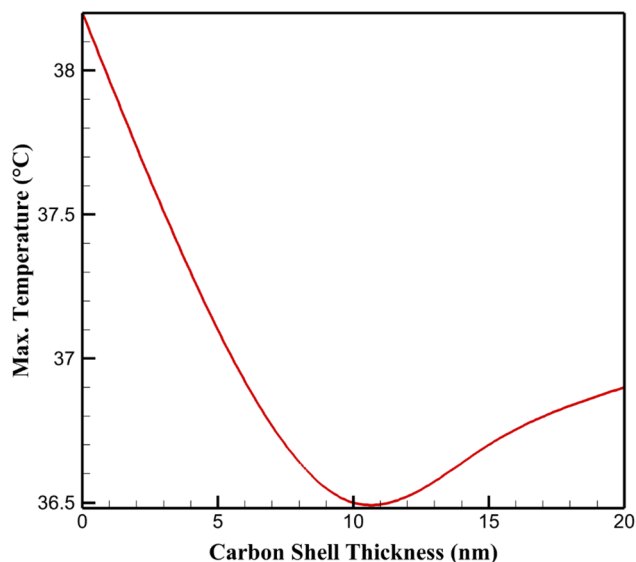


Fig. 2 Maximum temperature for different carbon shell thicknesses.

thermal runaway and material degradation in lithium–sulfur batteries.

For the uncoated  $\text{Li}_2\text{S}$  particle (0 nm), the maximum temperature reached 38.2 °C, reflecting significant heat accumulation. This is primarily due to the low thermal conductivity of  $\text{Li}_2\text{S}$  (approximately  $1.5 \text{ W (m K)}^{-1}$ ), which limits heat dissipation from exothermic electrochemical reactions, such as the reduction of  $\text{Li}_2\text{S}$  to form lithium polysulfides. These reactions release heat due to the entropy change associated with phase transformations and electron transfer processes. Additionally, the high internal resistance of uncoated  $\text{Li}_2\text{S}$  contributes to ohmic heating, further elevating the temperature. From a chemical standpoint, such temperature increases can promote undesirable side reactions, including polysulfide dissolution into the electrolyte, which forms soluble intermediates (e.g.,  $\text{Li}_2\text{S}_8$ ,  $\text{Li}_2\text{S}_6$ ) that reduce capacity retention.

Introducing a 5 nm carbon shell reduced the maximum temperature to 37.1 °C, a 1.1 °C improvement. The carbon shell, with a thermal conductivity of approximately  $100 \text{ W (m K)}^{-1}$ , enhances heat dissipation by providing a high-conductivity pathway for heat transfer from the  $\text{Li}_2\text{S}$  core to the surrounding electrolyte. Chemically, the carbon shell also stabilizes the electrode–electrolyte interface, reducing the rate of side reactions that generate additional heat. The optimal performance was observed with a 10 nm carbon shell, where the maximum temperature dropped to 36.5 °C. This thickness strikes a balance between sufficient thermal conductivity and minimal thermal resistance across the shell, optimizing heat dissipation while maintaining structural integrity. The carbon shell's porous structure facilitates electrolyte infiltration, ensuring that reaction sites remain accessible, which indirectly minimizes localized heat generation by promoting uniform electrochemical activity.

For thicker shells (15 nm and 20 nm), the maximum temperatures increased slightly to 36.7 °C and 36.9 °C, respectively. This trend is attributed to increased thermal resistance

due to the greater thickness of the carbon layer, which impedes heat transfer from the  $\text{Li}_2\text{S}$  core to the electrolyte. From a chemical perspective, thicker carbon shells may also restrict  $\text{Li}^+$  ion diffusion, leading to higher local current densities at the particle surface. This increases ohmic heating and localized reaction rates, contributing to elevated temperatures. Furthermore, the carbon shell's interaction with the electrolyte may alter the solvation dynamics of  $\text{Li}^+$  ions, potentially increasing the activation energy for ion transport and exacerbating heat generation.

### 3.2. Current density uniformity analysis

The uniformity of current density on the  $\text{Li}_2\text{S}$  particle surface in the graphene– $\text{Li}_2\text{S}$ –carbon cathode was evaluated to assess the electrochemical performance under a 1C discharge rate at 35 °C, with carbon shell thicknesses of 0, 5, 10, 15, and 20 nm. Table 2 presents the standard deviation of current density, and Fig. 2 illustrates the distribution trends. From a chemical perspective, uniform current density is critical for minimizing localized overpotentials and side reactions, which can degrade the cathode's performance in lithium–sulfur batteries. Table 2 shows standard deviation of current density for different carbon shell thicknesses.

The uncoated  $\text{Li}_2\text{S}$  particle exhibited a high standard deviation of  $0.45 \text{ mA cm}^{-2}$ , indicating significant non-uniformity. This is attributed to the low electrical conductivity of  $\text{Li}_2\text{S}$  ( $\sim 10^{-5} \text{ S m}^{-1}$ ), which causes uneven electron distribution and localized reaction hotspots. Chemically, such non-uniformity promotes polysulfide formation and dissolution, reducing capacity retention. A 5 nm carbon shell reduced the standard deviation to  $0.32 \text{ mA cm}^{-2}$ , as the carbon's high electrical conductivity ( $\sim 10^4 \text{ S m}^{-1}$ ) facilitates electron transport to reaction sites, enhancing uniformity. The 10 nm shell achieved the lowest standard deviation of  $0.25 \text{ mA cm}^{-2}$ , reflecting optimal electron distribution due to a balanced thickness that ensures conductivity without excessive ion diffusion barriers. This minimizes side reactions, such as polysulfide shuttling, by promoting uniform  $\text{Li}_2\text{S}$  reduction.

For 15 nm and 20 nm shells, the standard deviations increased to  $0.28$  and  $0.31 \text{ mA cm}^{-2}$ , respectively. Thicker shells introduce higher resistance to  $\text{Li}^+$  ion diffusion, as the porous carbon structure restricts ion mobility, leading to localized current accumulation. Chemically, this can exacerbate electrolyte decomposition and surface passivation, hindering electrochemical efficiency. The 10 nm shell thus represents an optimal design, balancing electron and ion transport to achieve uniform

Table 2 Standard deviation of current density for different carbon shell thicknesses

Carbon shell thickness (nm)	Standard deviation of current density ( $\text{mA cm}^{-2}$ )
0	0.45
5	0.32
10	0.25
15	0.28
20	0.31



current density and stable chemical performance. Balanced porosity and tortuosity at  $\sim 10$  nm yield the lowest standard deviation ( $0.25 \text{ mA cm}^{-2}$ ) by enabling even electron/ion access, reducing localized overpotentials and side reactions such as polysulfide formation.

### 3.3. Total ionic resistance

The total ionic resistance across the cathode–electrolyte interface of the graphene– $\text{Li}_2\text{S}$ –carbon cathode was analyzed under a 1C discharge rate at  $35^\circ\text{C}$  for carbon shell thicknesses of 0, 5, 10, 15, and 20 nm. Fig. 3 illustrates the resistance as a function of carbon shell thickness. From a chemical perspective, ionic resistance is a critical parameter influencing the electrochemical performance of lithium–sulfur batteries, as it affects  $\text{Li}^+$  ion transport, reaction kinetics, and the stability of the electrode–electrolyte interface. Table 3 displays ionic resistance for different carbon shell thicknesses.

The uncoated  $\text{Li}_2\text{S}$  particle exhibited a high ionic resistance of  $12.3 \Omega \text{ cm}^2$ , primarily due to its low ionic conductivity ( $\sim 10^{-8} \text{ S m}^{-1}$ ). This impedes  $\text{Li}^+$  ion transport, leading to significant concentration polarization and promoting side reactions, such as polysulfide formation, which dissolve into the electrolyte and degrade performance. A 5 nm carbon shell reduced the resistance to  $9.8 \Omega \text{ cm}^2$  by enhancing the electrode–electrolyte interface stability. The porous carbon structure facilitates  $\text{Li}^+$  ion diffusion, reducing the activation energy for ion transport. The 10 nm shell achieved the lowest resistance of  $8.5 \Omega \text{ cm}^2$ , optimizing ion transport pathways while maintaining sufficient porosity for electrolyte infiltration. This minimizes chemical barriers to  $\text{Li}^+$  solvation and desolvation, enhancing reaction kinetics.

For 15 nm and 20 nm shells, ionic resistances increased to 9.1 and  $10.2 \Omega \text{ cm}^2$ , respectively, due to longer diffusion paths through the thicker carbon layers, which increase tortuosity and hinder  $\text{Li}^+$  mobility. This can lead to localized ion depletion, increasing the likelihood of electrolyte decomposition and

Table 3 Impact of  $\text{Li}_2\text{S}$  volume fraction and E/S ratio on key performance metrics (10 nm shell, 1C,  $35^\circ\text{C}$ )

Parameter variation	$T_{\text{max}} (^\circ\text{C})$	$R_{\text{ion}} (\Omega \text{ cm}^2)$	$\sigma_j (\text{mA cm}^{-2})$
$\text{Li}_2\text{S}$ fraction: 40%	36.2	7	0.2
$\text{Li}_2\text{S}$ fraction: 50% (baseline)	36.5	8.5	0.25
$\text{Li}_2\text{S}$ fraction: 60%	36.9	10.5	0.35
E/S: 8 $\mu\text{L}$ per mg S	36.7	9.5	0.28
E/S: 10 $\mu\text{L}$ per mg S (baseline)	36.5	8.5	0.25
E/S: 12 $\mu\text{L}$ per mg S	36.4	8	0.23

surface passivation. The 10 nm shell thus provides an optimal balance, minimizing ionic resistance and supporting efficient electrochemical reactions. Thicker shells (15–20 nm) increase tortuosity, elevating resistance (from  $8.5 \Omega \text{ cm}^2$  at 10 nm to  $10.2 \Omega \text{ cm}^2$  at 20 nm) and promoting ion depletion, which exacerbates shuttle effects and electrolyte decomposition.

### 3.4. $\text{Li}^+$ ion concentration analysis

The distribution of  $\text{Li}^+$  ions in the graphene– $\text{Li}_2\text{S}$ –carbon cathode and surrounding electrolyte was analyzed at the end of a 1C discharge at  $35^\circ\text{C}$  for carbon shell thicknesses of 0, 5, 10, 15, and 20 nm (Fig. 4). From a chemical perspective, uniform  $\text{Li}^+$  ion distribution is crucial for minimizing concentration polarization, reducing side reactions, and enhancing the electrochemical performance of lithium–sulfur batteries. Table 4 presents  $\text{Li}^+$  ion concentrations for different carbon shell thicknesses.

The uncoated  $\text{Li}_2\text{S}$  particle exhibited a significant concentration gradient, with a surface concentration of  $0.80 \text{ mol m}^{-3}$  and an electrolyte concentration of  $1.20 \text{ mol m}^{-3}$ . This is due to the low ionic conductivity of  $\text{Li}_2\text{S}$ , which restricts  $\text{Li}^+$  diffusion, leading to ion depletion at the cathode surface. Chemically, this gradient promotes polysulfide formation and dissolution, as insufficient  $\text{Li}^+$  availability hinders uniform electrochemical reduction, exacerbating capacity fade. A 5 nm carbon shell reduced the gradient, with concentrations of  $0.90 \text{ mol m}^{-3}$  at the surface and  $1.10 \text{ mol m}^{-3}$  in the electrolyte, as the porous carbon facilitates ion transport by lowering the activation energy for  $\text{Li}^+$  solvation. The 10 nm shell achieved the most uniform profile, optimizing ion diffusion through a balanced porosity and thickness, minimizing chemical barriers to reaction kinetics. For 15 nm and 20 nm shells, gradients increased slightly, as thicker shells increase tortuosity, impeding  $\text{Li}^+$  mobility. This can enhance localized side reactions, such as electrolyte decomposition. The 10 nm shell thus optimizes  $\text{Li}^+$  distribution, supporting stable electrochemical performance. For thinner shells (e.g., 5 nm), higher effective porosity facilitates uniform  $\text{Li}^+$  distribution (reducing gradients from  $0.80 \text{ mol m}^{-3}$  at the surface for 0 nm to  $0.90 \text{ mol m}^{-3}$ ), minimizing side reactions like polysulfide dissolution.

### 3.5. Chemical modulation of polysulfide dynamics by carbon shell thickness

The chemical role of carbon shell thickness (0, 5, 10, 15, and 20 nm) in modulating the performance of the graphene– $\text{Li}_2\text{S}$ –

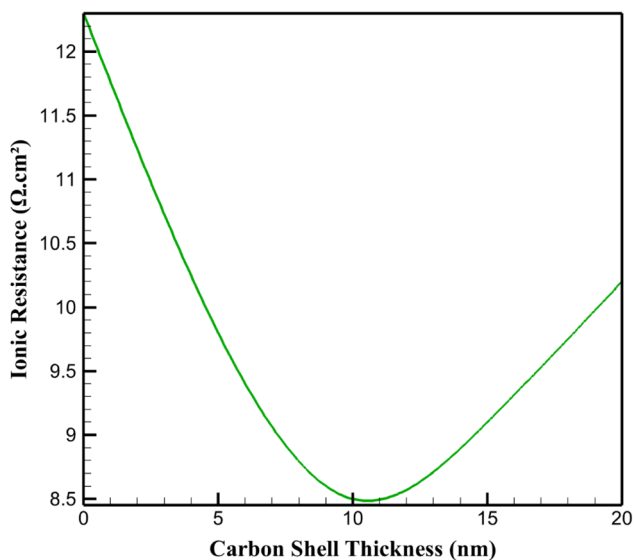


Fig. 3 Ionic resistance for different carbon shell thicknesses.

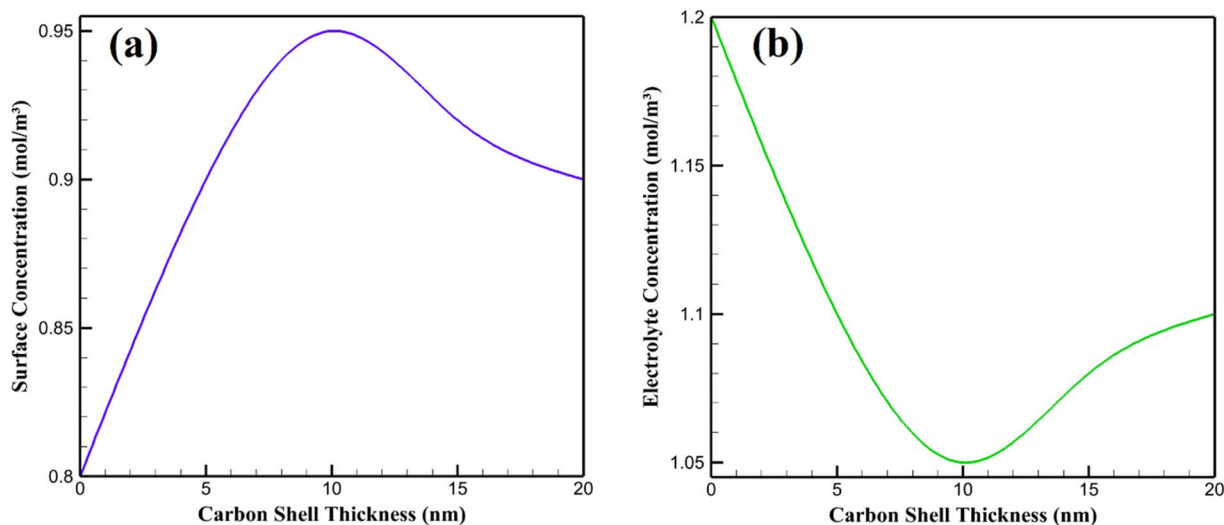


Fig. 4  $\text{Li}^+$  ion concentration profiles of graphene- $\text{Li}_2\text{S}$ -Carbon nanocomposite cathode at different carbon shell thicknesses: (a) surface concentration and (b) electrolyte concentration.

Table 4 Impact of lithium excess on key performance metrics (10 nm shell, 1C, 35 °C)

Lithium excess (%)	$T_{\text{max}}$ (°C)	$R_{\text{ion}}$ ( $\Omega \text{ cm}^2$ )	$\sigma_{\text{J}}$ ( $\text{mA cm}^{-2}$ )
80	36.8	9.2	0.3
100 (baseline)	36.5	8.5	0.25
120	36.3	8.1	0.22

carbon cathode in lithium-sulfur batteries is critical for addressing electrochemical stability and reaction kinetics. The carbon shell governs surface chemistry, particularly polysulfide formation, electrolyte interactions, and  $\text{Li}_2\text{S}$  redox processes. For the uncoated  $\text{Li}_2\text{S}$  particle, elevated temperatures (38.2 °C) and low ionic conductivity ( $\sim 10^{-8} \text{ S m}^{-1}$ ) exacerbate polysulfide dissolution (e.g.,  $\text{Li}_2\text{S}_8$ ,  $\text{Li}_2\text{S}_6$ ). Without a protective layer, these soluble intermediates diffuse into the electrolyte, promoting the shuttle effect and reducing capacity retention. This is driven by high activation energy for  $\text{Li}^+$  solvation at the bare  $\text{Li}_2\text{S}$  surface, which also triggers side reactions like electrolyte decomposition into insulating species such as  $\text{Li}_2\text{SO}_4$ . This electrolyte decomposition typically occurs *via* oxidation of dissolved long-chain polysulfides (e.g.,  $\text{Li}_2\text{S}_8$  or  $\text{Li}_2\text{S}_6$ ) by trace oxygen or moisture contaminants, or through nucleophilic attack by polysulfides on ether-based solvents (such as 1,3-dioxolane or dimethoxyethane), leading to ring-opening reactions and subsequent formation of insoluble  $\text{Li}_2\text{SO}_4$  and other sulfate-containing passivation layers on the cathode surface. A 5 nm carbon shell mitigates these issues by stabilizing the electrode-electrolyte interface, reducing polysulfide shuttling through physical confinement within its porous structure. This lowers the activation energy for  $\text{Li}^+$  transport, as evidenced by reduced ionic resistance ( $9.8 \Omega \text{ cm}^2$ ).

The 10 nm shell optimizes this effect, achieving minimal ionic resistance ( $8.5 \Omega \text{ cm}^2$ ) and near-uniform  $\text{Li}^+$  distribution ( $0.95 \text{ mol m}^{-3}$  at the surface,  $1.05 \text{ mol m}^{-3}$  in the electrolyte). Its balanced

porosity traps polysulfides *via* weak van der Waals interactions, curbing their dissolution while facilitating electrolyte infiltration for uniform  $\text{Li}_2\text{S}$  reduction. This minimizes overpotentials and suppresses side reactions, such as electrolyte oxidation forming passivating layers. Thicker shells (15 nm and 20 nm) increase ionic resistance ( $9.1$  and  $10.2 \Omega \text{ cm}^2$ ) due to higher tortuosity, impeding  $\text{Li}^+$  diffusion and causing localized ion depletion. This elevates polysulfide formation and electrolyte breakdown, compromising stability. The 10 nm shell thus excels in modulating polysulfide dynamics, enhancing electrochemical kinetics by balancing ion transport, thermal management, and chemical stability, offering a pathway to mitigate key challenges in lithium-sulfur battery performance. Porosity aids in trapping polysulfides *via* physical confinement and van der Waals interactions, while excessive tortuosity in thicker shells hinders this, increasing dissolution risks and compromising chemical stability.

### 3.6. Impact of insulating active material proportion and electrolyte amount

The proportion of insulating active material ( $\text{Li}_2\text{S}$  volume fraction) and the amount of electrolyte (E/S ratio) were varied to evaluate their effects on cathode performance. As shown in Table 3, a higher  $\text{Li}_2\text{S}$  fraction (60%) increases ionic resistance to  $10.5 \Omega \text{ cm}^2$  and temperature to 36.9 °C, due to reduced effective conductivity and increased heat from polarization. Chemically, this promotes polysulfide dissolution by limiting uniform  $\text{Li}^+$  access. Lower E/S ratios (8  $\mu\text{L}$  per mg S) exacerbate these issues, raising resistance by promoting ion depletion. The optimal baseline values minimize these effects, highlighting the need for  $\sim 50\%$   $\text{Li}_2\text{S}$  fraction and  $\text{E/S} > 10 \mu\text{L}$  per mg S for stability.

### 3.7. Impact of lithium amount on electrochemical reversibility

The amount of lithium (excess) affects reversibility by influencing polysulfide interactions. Table 4 shows that reducing





lithium excess to 80% increases non-uniformity to  $0.30 \text{ mA cm}^{-2}$ , as limited lithium promotes irreversible shuttling and anode passivation. Higher excess (120%) improves uniformity but may increase dendrite risks. Chemically, adequate lithium ( $\geq 100\%$ ) ensures stable  $\text{Li}_2\text{S}$  redox, reducing side reactions like  $\text{Li}_2\text{SO}_4$  formation.

### 3.8. Discussion

The sensitivity analysis demonstrates that  $\text{Li}^+$  diffusivity has the strongest influence on cathode performance. A 20% decrease in diffusivity increases ionic resistance by  $\sim 20\%$  (from  $8.5$  to  $10.2 \text{ } \Omega \text{ cm}^2$ ) and significantly worsens current density uniformity ( $\sigma_j = 0.33 \text{ mA cm}^{-2}$ ). Ionic conductivity variations show a moderate effect, with resistance changes of  $\sim 15\%$  and corresponding shifts in current uniformity. In contrast, variations in the thermal conductivity of the carbon shell had only a minor impact on  $T_{\text{max}}$  ( $\pm 0.3 \text{ } ^\circ\text{C}$ ) and negligible effects on electrochemical parameters, indicating that the system is thermally robust but more sensitive to ionic transport properties.

Overall, the analysis confirms that the identified optimal shell thickness of  $10 \text{ nm}$  remains valid under realistic variations of material properties. The model is most sensitive to  $\text{Li}^+$  transport parameters, suggesting that precise control of electrolyte composition and shell porosity is critical for achieving stable electrochemical performance.

The investigation into the graphene- $\text{Li}_2\text{S}$ -carbon cathode's performance under a  $1\text{C}$  discharge rate at  $35 \text{ } ^\circ\text{C}$  reveals that carbon shell thickness significantly influences thermal, ionic, and electrical behavior, critical for lithium-sulfur battery design. The interplay between material properties and electrochemical processes, particularly the chemical role of the carbon shell, mitigates limitations inherent to  $\text{Li}_2\text{S}$ , such as polysulfide dissolution and electrolyte instability. The  $10 \text{ nm}$  carbon shell consistently delivered optimal performance. Thermally, it minimized the maximum temperature ( $36.5 \text{ } ^\circ\text{C}$ ) by leveraging high thermal conductivity ( $\sim 100 \text{ W (m K)}^{-1}$ ), reducing heat-driven side reactions like polysulfide formation (e.g.,  $\text{Li}_2\text{S}_8$ ,  $\text{Li}_2\text{S}_6$ ), which degrade electrolyte stability and capacity retention. The uncoated  $\text{Li}_2\text{S}$  particle, with poor thermal conductivity ( $\sim 1.5 \text{ W (m.K)}^{-1}$ ), reached  $38.2 \text{ } ^\circ\text{C}$ , exacerbating heat accumulation from exothermic  $\text{Li}_2\text{S}$  reduction, promoting soluble polysulfide diffusion and electrolyte decomposition into insulating  $\text{Li}_2\text{SO}_4$ . Thicker shells ( $15 \text{ nm}$  and  $20 \text{ nm}$ ) increased thermal resistance, slightly elevating temperatures to  $36.7 \text{ } ^\circ\text{C}$  and  $36.9 \text{ } ^\circ\text{C}$ , indicating a trade-off between conductivity and thickness that impacts chemical stability.

Electrically, the  $10 \text{ nm}$  shell achieved the lowest current density standard deviation ( $0.25 \text{ mA cm}^{-2}$ ), ensuring uniform electron distribution. This minimizes localized overpotentials, reducing polysulfide formation driven by uneven electrochemical activity in the uncoated particle ( $0.45 \text{ mA cm}^{-2}$ ). Chemically, this uniformity curbs side reactions like electrolyte oxidation, which forms passivating layers. Thicker shells increased non-uniformity due to restricted  $\text{Li}^+$  diffusion, elevating risks of surface passivation. Ionically, the  $10 \text{ nm}$  shell reduced ionic resistance to  $8.5 \text{ } \Omega \text{ cm}^2$  and achieved near-

uniform  $\text{Li}^+$  distribution ( $0.95 \text{ mol m}^{-3}$  at the surface,  $1.05 \text{ mol m}^{-3}$  in the electrolyte), optimizing reaction kinetics. In contrast, the uncoated particle's ion depletion ( $0.80 \text{ mol m}^{-3}$ ) promotes polysulfide shuttling. Thicker shells increased resistance ( $9.1\text{--}10.2 \text{ } \Omega \text{ cm}^2$ ), hindering  $\text{Li}^+$  mobility and risking electrolyte breakdown. The  $10 \text{ nm}$  shell's porous structure traps polysulfides *via* van der Waals interactions, enhancing chemical stability and offering a pathway to mitigate lithium-sulfur battery challenges.

Furthermore, the extended sensitivity analysis highlights the dominant role of cell-fabrication parameters in battery performance. Increasing the  $\text{Li}_2\text{S}$  volume fraction by  $20\%$  (to  $60\%$ ) significantly elevates ionic resistance (to  $10.5 \text{ } \Omega \text{ cm}^2$ ) due to the insulating nature of  $\text{Li}_2\text{S}$ , which amplifies tortuosity and hinders ion transport, potentially exacerbating polysulfide shuttling. Conversely, a lower fraction ( $40\%$ ) improves uniformity but may reduce overall capacity. The E/S ratio critically affects electrochemical reversibility; a  $20\%$  reduction (to  $8 \text{ } \mu\text{L per mg S}$ ) increases resistance by  $11.8\%$ , promoting concentration polarization and side reactions like electrolyte decomposition. Lithium excess influences stability, with an  $80\%$  level raising non-uniformity by  $20\%$ , as insufficient lithium accelerates anode degradation and polysulfide migration. These factors, often overlooked in isolated cathode models, underscore the need for holistic cell design, where optimizing the carbon shell must be integrated with controlled active material loading, electrolyte volume, and lithium stoichiometry to achieve practical reversibility and longevity.

The trends identified in this work are fully consistent with recent experimental insights on carbon-hosted sulfur cathodes, which emphasize the importance of balancing carbon thickness, porosity, conductivity, and morphology to achieve stable electrochemical performance. Recent studies on graphene and CNT-based composite frameworks report that overly thin carbon coatings provide limited polysulfide confinement, whereas excessively thick or compact carbon hosts increase ionic tortuosity and polarization, reducing sulfur utilization.<sup>30,31</sup> Similarly, hierarchically porous and highly conductive carbon substrates have been shown to promote uniform current distribution, enhance lithium-ion accessibility, and suppress localized reaction hotspots under lean-electrolyte conditions. These experimentally observed structure-performance relationships directly support the present simulation results, which identify an optimal intermediate carbon shell thickness ( $\sim 10 \text{ nm}$ ) that minimizes ionic resistance and current-density non-uniformity while maintaining effective polysulfide control. The agreement between recent experimental observations and the multiphysics predictions reinforces the physical relevance and general applicability of the proposed cathode design principles.

The optimal carbon shell thickness of  $\sim 10 \text{ nm}$  identified in this work compares favorably with recent experimental and modeling studies. Liu *et al.* demonstrated that ultra-thin hollow carbon shells ( $< 8 \text{ nm}$ ) enhanced initial capacity due to reduced  $\text{Li}^+$  transport barriers, but suffered from rapid capacity fading caused by inadequate polysulfide confinement.<sup>47</sup> In contrast, Li *et al.* reported that thicker mesoporous carbon layers ( $> 15 \text{ nm}$ ) provided stronger polysulfide adsorption but introduced higher



ionic resistance, limiting rate performance.<sup>48</sup> Our results, showing a minimum ionic resistance of  $8.5 \Omega \text{ cm}^2$  and improved current-density uniformity at 10 nm, position this thickness as an intermediate compromise that avoids the severe drawbacks reported for both thinner and thicker shells. Similar trends were also predicted by Imediegwu *et al.* through electrochemical modeling, where diffusivity and electrode thickness emerged as critical parameters governing polarization.<sup>49</sup> Furthermore, the design strategy outlined by Dent *et al.* supports this balance, emphasizing that cathode architectures with controlled coating thicknesses are essential to simultaneously achieve cycle stability and high-rate capability.<sup>50</sup> Together, these comparisons confirm that our simulation-based optimization aligns well with experimental observations and provides a quantitative rationale for selecting  $\sim 10$  nm as the practical design window.

The present multiphysics model primarily focuses on the physical confinement of polysulfides by the carbon shell and their dissolution into the electrolyte, without explicitly incorporating the detailed conversion kinetics of polysulfide intermediates (*e.g.*, stepwise reduction *via* Butler–Volmer equations). This simplification assumes rapid equilibrium in polysulfide transformation within the confined cathode environment. Consequently, the predicted ionic resistance may be slightly underestimated, as real-world sluggish kinetics could lead to localized accumulation of soluble polysulfides, increasing electrolyte viscosity and reducing effective  $\text{Li}^+$  mobility. Similarly, temperature profiles might underpredict localized heating from parasitic shuttle reactions or incomplete conversions, which generate additional ohmic and reaction heat. However, the model's excellent validation against experimental data (RMSE =  $0.09 \text{ V}$ ,<sup>42</sup>) suggests that these effects are secondary under the studied conditions (1C rate, carbon-coated architecture), where physical confinement dominates polysulfide control.

## 4. Conclusion

This study advances the understanding of the graphene– $\text{Li}_2\text{S}$ –carbon cathode's performance in lithium–sulfur batteries by analyzing the impact of carbon shell thickness (0, 5, 10, 15, and 20 nm) on thermal, ionic, and electrical properties under a 1C discharge rate at  $35^\circ\text{C}$ . From a chemical perspective, it addresses critical challenges, notably the low ionic and electrical conductivity of  $\text{Li}_2\text{S}$  ( $\sim 10^{-8} \text{ S m}^{-1}$ ) and polysulfide dissolution (*e.g.*,  $\text{Li}_2\text{S}_8$ ,  $\text{Li}_2\text{S}_6$ ), which degrade capacity retention and cycle life by promoting shuttle effects and electrolyte decomposition into insulating species like  $\text{Li}_2\text{SO}_4$ . This decomposition pathway primarily involves the chemical oxidation of soluble polysulfides or their reaction with electrolyte solvents, resulting in insulating sulfate species that passivate the electrode surface. The multiphysics model, validated with an RMSE of  $0.09 \text{ V}$  against experimental data,<sup>42</sup> quantifies how the carbon shell modulates chemical processes. The 10 nm shell emerged as optimal, achieving minimal temperature rise ( $36.5^\circ\text{C}$ ) *via* high thermal conductivity ( $\sim 100 \text{ W (m K)}^{-1}$ ), reducing heat-driven polysulfide formation. It also minimized ionic resistance ( $8.5 \Omega \text{ cm}^2$ ) and current density non-uniformity

( $0.25 \text{ mA cm}^{-2}$ ), ensuring uniform  $\text{Li}^+$  distribution ( $0.95 \text{ mol m}^{-3}$  at the surface,  $1.05 \text{ mol m}^{-3}$  in the electrolyte). Chemically, this shell traps polysulfides through van der Waals interactions within its porous structure, lowering the activation energy for  $\text{Li}^+$  solvation and curbing side reactions like electrolyte oxidation, which forms passivating layers. The incorporation of porosity and tortuosity in the model, *via* the Bruggeman relation, ensures that simulations capture real-world trade-offs in ion transport and polysulfide control, as validated by the low RMSE ( $0.09 \text{ V}$ ). While the absence of explicit polysulfide conversion kinetics simplifies the model and aligns well with experimental validation, future extensions could incorporate these reactions to further refine predictions of long-term ionic resistance and thermal runaway risks.

Incorporating cell-fabrication parameters such as  $\text{Li}_2\text{S}$  proportion, E/S ratio, and lithium excess into the model reveals their profound impact on electrochemical stability, emphasizing the necessity of balanced design to mitigate insulation effects, polarization, and shuttling for commercial Li–S batteries. The conclusions drawn from this simulation study are further supported by recent experimental reports on graphene- and CNT-based carbon hosts, which similarly highlight the critical role of optimized carbon thickness, porosity, and conductivity in regulating electrochemical behavior. This consistency confirms that the identified intermediate carbon shell thickness provides a physically grounded and experimentally relevant design guideline for high-performance lithium–sulfur battery cathodes. These findings offer actionable insights for cathode design, enhancing ion transport and thermal management to mitigate chemical barriers. By elucidating the interplay between carbon shell thickness and electrochemical stability, this study provides a predictive tool for optimizing cathode materials, improving energy density and cycle life. This work is pivotal for advancing lithium–sulfur batteries toward commercial viability, addressing global needs for sustainable, high-capacity energy storage systems. The uncoated particle's ion depletion promotes polysulfide shuttling and subsequent electrolyte decomposition *via* polysulfide oxidation or solvent ring-opening, yielding insulating  $\text{Li}_2\text{SO}_4$ .

## Conflicts of interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

## Data availability

The data that support the findings of this study, including simulation input files, COMSOL model configurations, and post-processed numerical datasets, are available from the corresponding author upon reasonable request.

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