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# Computational optimization of MASnI<sub>3</sub> perovskite solar cells using SCAPS-1D simulations and machine learning techniques

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The lead-free methylammonium tin iodide (MASnI<sub>3</sub>) has gained significant interest in perovskite solar cell (PSC) technology due to its ideal band gap and environmentally friendly composition, offering a promising alternative to traditional lead-based perovskites. In this computational work, the SCAPS-1D simulator is utilized to create and assess several PSC structures by merging two electron transport layers and three hole transport layers. Among them, the MASnI<sub>3</sub>-based device architecture of Al/FTO/WS<sub>2</sub>/MASnI<sub>3</sub>/Zn<sub>3</sub>P<sub>2</sub>/Ni provides superior performance, including efficiency of 32.30%, fill factor (FF) of 87.35%, short-circuit current density ( $J_{sc}$ ) of 34.19 mAcm<sup>-2</sup> and open-circuit voltage ( $V_{oc}$ ) of 1.08 V. The influence of thickness, carrier density, defect concentration, and carrier lifetime of the MASnI<sub>3</sub> perovskite layer on the photovoltaic performance metrics is investigated meticulously. Furthermore, the effects of interface recombination, operating temperature, and capacitance–voltage (C–V) and capacitance–frequency (C–F) on the performance characteristics of the proposed structure are analyzed. Moreover, we present a comparative analysis conducted among three machine learning algorithms to identify the model that provides the highest accuracy in predicting the efficiency of the specified device. The results demonstrate that the XGBoost model achieves superior performance, yielding an  $R^2$  value of 0.9999, along with a low mean squared error (MSE) of 0.0092 and mean absolute error (MAE) of 0.051. In addition, the individual influence of several input parameters on the device efficiency has been assessed using the feature importance method. Among the evaluated features, defect density emerged as the most influential parameter, indicating that it plays a significant role in defining the overall performance of the photovoltaic (PV) device.

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## 1. Introduction

The worldwide transition to renewable energy has been accelerated by the urgent necessity to alleviate global warming and decrease reliance on fossil fuels.<sup>1,2</sup> Solar energy is one of the most abundant and sustainable renewable sources.<sup>3</sup> Scientists are diligently investigating different substances and device structures for effectively harvesting sunlight. Based on the materials and manufacturing processes, scientists have already evaluated various solar cell types.<sup>4</sup> Among them, the third-generation solar modules, particularly perovskite solar cells (PSCs), are garnering focus for their low production costs, experimental reproducibility, and high efficiency.<sup>2,5</sup> Perovskite materials, with the generic synthesis ABX<sub>3</sub>, where ‘A’, ‘B’, and ‘X’ are respective cation, metal ion and halide, have revolutionized

solar cell research.<sup>1,6</sup> The quick development of solar cells made of perovskites, with their efficiency soaring from 3.8% in 2009 to above 26% in just over a decade, reveals their exceptional optoelectronic properties and potential to compete with the traditional silicon-based photovoltaics.<sup>7,8</sup> Among the various perovskites, the methylammonium tin iodide (MASnI<sub>3</sub> or CH<sub>3</sub>-NH<sub>3</sub>SnI<sub>3</sub>) emerges as a lead-free perovskite alternative, addressing toxicity concerns associated with lead-based counterparts.<sup>9</sup> Additionally, MASnI<sub>3</sub> exhibits a suitable bandgap (~1.3 eV), high carrier mobility, and strong absorption in the visible spectrum, making it an ideal contender for efficient and eco-friendly PSCs.<sup>9,10</sup> Despite the MASnI<sub>3</sub>-based PSCs demonstrating excellent PV properties, the Sn<sup>2+</sup> ion of the MASnI<sub>3</sub> layer is oxidized into Sn<sup>4+</sup> in an open environment.<sup>11</sup> This instability issue in tin-based perovskites can be effectively mitigated through optimized fabrication techniques, including the incorporation of tin fluoride (SnF<sub>2</sub>) or tin iodide (SnI<sub>2</sub>), which helps to suppress Sn<sup>2+</sup> oxidation.<sup>12,13</sup>

Furthermore, the Goldschmidt tolerance ( $t$ ) and octahedral factors ( $\mu$ ) are widely used to describe the stability of perovskite material.<sup>14–16</sup> For stable perovskite crystal structure, the value of

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$t$  and  $\mu$  should be in the range of  $0.8 < t < 1.0$  and  $0.414 < \mu < 0.732$ .<sup>15–17</sup> Moreover, non-perovskite structure with intermolecular distortion forms when the tolerance factor is less than 0.8 and greater than 1.<sup>14,16</sup> However, the value of  $t$  and  $\mu$  for MASnI<sub>3</sub> crystal structure is 0.904 and 0.555. Which falls between the ideal range of Goldschmidt tolerance and octahedral factors.<sup>18</sup> Additionally, among the Sn-based perovskite materials, MASnCl<sub>3</sub> and MASnBr<sub>3</sub> provides better stability compared to the MASnI<sub>3</sub>, due to their higher tolerance factor close to 1.<sup>18,19</sup> However, MASnI<sub>3</sub> has often been regarded as the most promising of the MASnX<sub>3</sub> perovskites for solar-cell applications because of its favorable bandgap (~1.3 eV) and strong light absorption, which together support relatively high short-circuit current densities ( $J_{sc}$ ) and good carrier transport properties.<sup>20</sup>

The initial MASnI<sub>3</sub>-based PSC was fabricated by Noel *et al.* in 2014 and attained a PCE of 6.4% with a  $V_{oc}$  of 0.88 V.<sup>21</sup> In the same year, an additional research obtained a PCE of 5.23% for the MASnI<sub>3</sub>-based PSC with Spiro-OMeTAD as an HTL.<sup>22</sup> The PCE of 5.44% is achieved for the structure of TiO<sub>2</sub>/MASnI<sub>3</sub>/Spiro-OMeTAD with  $V_{oc}$  of 0.716 V,  $J_{sc}$  of 15.18 mA cm<sup>-2</sup>, and FF of 50.07%.<sup>23</sup> In 2019, the mesoporous MASnI<sub>3</sub>-based PSCs were fabricated with excellent reproducibility, demonstrating a maximum efficiency of 7.13%.<sup>24</sup> In addition to the experimental studies, several research groups perform numerical investigation to improve the device performance significantly. By systematically optimizing several layer parameters, researchers have reported theoretical efficiencies exceeding 25%, which are significantly higher than current experimental values.<sup>4,9,25–31</sup> These findings not only highlight the strong potential of MASnI<sub>3</sub> as a viable lead-free absorber but also provide valuable guidelines for experimentalists aiming to close the gap between theoretical and practical efficiencies.

A significant problem that degrades the efficiency of heterojunction PSCs is carrier recombination at the rear contact. Therefore, improving their performance requires careful optimization of the structural design, material properties, and carrier transport mechanisms.<sup>32,33</sup> One effective approach is to use suitable transport layers to ensure proper alignment of band with the absorber layer. In this case, we can replace the commonly used toxic CdS electron transport layer (ETL) with environmentally friendly, non-toxic alternatives, which can provide appropriate band arrangement at the absorber/ETL interface.<sup>34–36</sup> Additionally, reducing the energy barrier at the interface of absorber/back contact helps suppress minority carrier recombination, thereby improving overall cell efficiency.<sup>32,33,37</sup> Adding an interlayer within the absorber and back contact can effectively lower the Schottky barrier and improve interface quality in heterojunction structures.<sup>38</sup> Moreover, the integration of heavily doped HTLs at the rear side of heterojunction PSCs has been shown to enhance carrier collection by minimizing surface recombination through better band alignment.<sup>39–42</sup>

In the past few years, machine learning (ML) has been recognized as a transformational method in the field of photovoltaic research, offering a data-driven alternative to accelerate the discovery and optimization of materials and device architectures.<sup>43</sup> By learning patterns from existing datasets, ML models can predict key performance parameters, identify critical material properties,

and uncover complex nonlinear relationships that are difficult to capture through conventional methods.<sup>31,44</sup> In the context of PSCs, ML enables the rapid screening of material candidates, optimization of device layer properties, and performance prediction under various operating conditions. In recent years, numerous research groups have incorporated a variety of ML algorithms into PV technology to evaluate both the predictive accuracy of models and the influence of individual physical variables on the performance metrics of PSCs.<sup>31,43–51</sup> This approach not only minimizes the time and expenses related to experimental development but also provides deeper insights into the physical mechanisms governing device behavior.<sup>43,47</sup> Incorporating ML into the design workflow of perovskite solar cells provides a promising pathway for developing high-performance, resilient, and scalable photovoltaic technologies.

This study employs SCAPS-1D to architect and evaluate the performance of Al/FTO/WS<sub>2</sub>/MASnI<sub>3</sub>/Zn<sub>3</sub>P<sub>2</sub>/Ni heterojunction PSC. Here, heavily doped p<sup>+</sup>-type Zn<sub>3</sub>P<sub>2</sub> is employed as a rear passivation layer to optimize the band alignment with the MASnI<sub>3</sub> active layer.<sup>52,53</sup> A minimal valence band offset (VBO) at the Zn<sub>3</sub>P<sub>2</sub>/MASnI<sub>3</sub> junction is observed, which facilitates efficient hole extraction from the absorber to the rear contact, ultimately contributing to enhanced device performance. Moreover, its key advantages include a suitable bandgap, high hole mobility, non-toxicity, low cost, and improved device stability.<sup>36,51</sup> Additionally, WS<sub>2</sub> is utilized as an alternative to the conventional CdS ETL in combination with the MASnI<sub>3</sub> absorber. It is a promising electron transport layer due to its non-toxic nature, cost-effectiveness, high electrical conductivity, suitable bandgap, and excellent carrier mobility.<sup>53,54</sup> However, the influences of perovskite layer thickness, defect density, doping concentration, and the device temperature and parasitic resistances on the suggested solar cell performance metrics are also explored in this numerical investigation. It also incorporates ML techniques, utilizing SCAPS-generated data to train and evaluate models and determine the most influential physical parameters, which are highly beneficial for the experimental scientist to design highly efficient PV cells without depending on time consuming trial and error processes.

## 2. Methodology for simulation

### 2.1. SCAPS-1D simulation

In order to develop and study the heterojunction PSC structure of Al/FTO/WS<sub>2</sub>/MASnI<sub>3</sub>/Zn<sub>3</sub>P<sub>2</sub>/Ni, we have used user-friendly and reliable SCAPS-1D simulation software.<sup>55</sup> The software can provide various electrical characteristics, such as external quantum efficiency (EQE), capacitance–voltage ( $C$ – $V$ ), capacitance–frequency ( $C$ – $F$ ), current density–voltage ( $I$ – $V$ ), and operating temperature. Moreover, The Poisson equation, drift diffusion, and the continuity equations governing electron and hole behavior form the foundation of this simulator.<sup>35,56</sup>

$$\frac{d^2}{dx^2}\Psi(x) = \frac{e}{\epsilon_0\epsilon_r}p(x) - n(x) + N_D - N_A + \rho_p - \rho_n \quad (1)$$

where  $\psi$ ,  $\epsilon_0$ , and  $\epsilon$  are denoted as electrostatic potential, permittivity of vacuum, and semiconductor, respectively.  $N_D$  and  $N_A$  are respective donor and acceptor density.



$$\frac{\partial n}{\partial t} = -\frac{\partial}{\partial x} J_n - U_n + G,$$

$$\frac{\partial p}{\partial t} = -\frac{\partial}{\partial x} J_p - U_p + G$$
(2)

The letters  $U_n$  and  $G$  stand for recombination rate and carrier generation, respectively.

$$J_p = +\frac{\mu_p P}{q} \frac{\partial E_{Fp}}{\partial x},$$

$$J_n = -\frac{\mu_n n}{q} \frac{\partial E_{Fn}}{\partial x}$$
(3)

The current densities of the electron and hole are symbolized by  $J_n$  and  $J_p$ , respectively.  $\mu_p$  and  $\mu_n$  are the electron and hole mobility, respectively, and  $E_{Fp}$  and  $E_{Fn}$  are the Fermi levels of the hole and electron, respectively.<sup>31,56</sup>

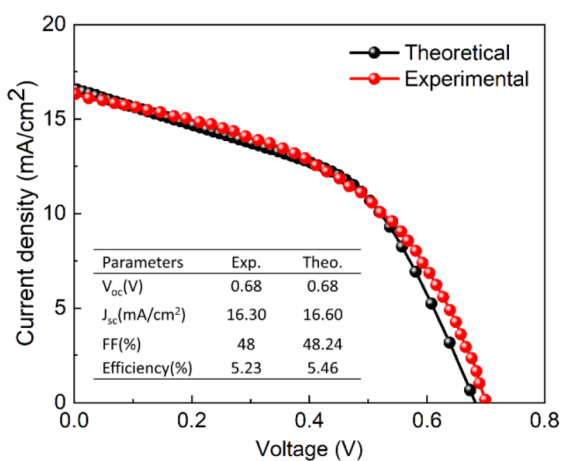


Fig. 1 Simulation and experimental  $J$ - $V$  curves of  $MASnI_3$ -based PSCs.<sup>31</sup>

Firstly, SCAPS-1D is a widely accepted solar cell simulator, and the performance of solar cells designed using SCAPS-1D is compared with experimental results in numerous published works.<sup>31,57-60</sup> Their works found strong agreement between SCAPS-1D simulations and experimental results, which validated the reliability of our SCAPS-1D simulation in supporting and interpreting the experimental findings. Here, the comparison of  $J$ - $V$  curves and performance metrics of experimental and simulation results is illustrated in Fig. 1.<sup>31</sup>

Our proposed  $Al/FTO/WS_2/MASnI_3/Zn_3P_2/Ni$  heterojunction cell structure is exhibited in Fig. 2(a). Additionally, in order to enhance PV performance, highly doped  $Zn_3P_2$  plays the role of HTL that reduces the carrier recombination rate at the  $MASnI_3/Zn_3P_2$  junction,  $WS_2$  acts as an ETL, and FTO is used for the window layer. For front and back contact, we have selected Al and Ni with work function value of 4.06 eV and 5.35 eV, respectively.<sup>61</sup> However, precise temperature control is critical in thin-film deposition as it governs fundamental processes such as precursor decomposition, atomic surface mobility, and interfacial adhesion, directly determining the crystallinity, density, and electronic quality of each functional layer. In the fabrication of the proposed  $Al/FTO/WS_2/MASnI_3/Zn_3P_2/Ni$  solar cell, the temperature must be carefully tailored for each material. Commercially prepared FTO films, typically deposited *via* spray pyrolysis, achieve optimal polycrystalline conductivity when processed between 250 °C and 450 °C.<sup>62</sup> For the  $WS_2$  electron-transport layer, sputtering or chemical vapor deposition at a substrate temperature near 200 °C yields films with greater crystal size, superior crystallinity, and reduced micro-strain, significantly enhancing their electronic properties.<sup>63</sup> Conversely, the tin-based perovskite  $MASnI_3$  absorber presents a stringent thermal constraint; it can be deposited *via* hybrid evaporation at room temperature to form highly crystalline films without requiring  $SnF_2$  additives or post-deposition annealing, thereby avoiding the thermal degradation of  $Sn^{2+}$ .<sup>64</sup> The  $Zn_3P_2$  hole-transport layer, typically deposited by thermal evaporation, introduces another thermal consideration, as its decomposition and undesirable gas-phase reactions become significant above

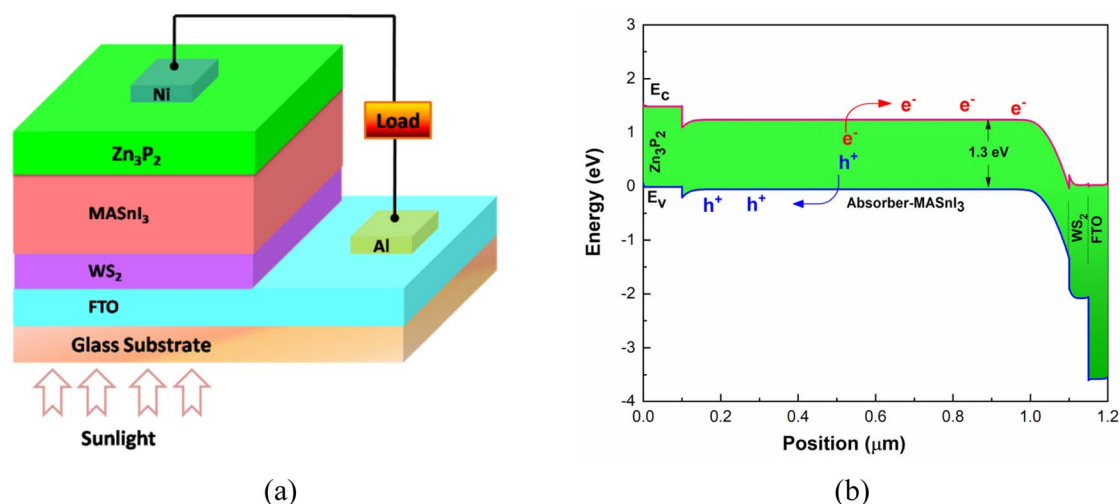


Fig. 2 (a) Structural schematic and (b) energy band diagram of proposed  $MASnI_3$ -based PSC.



Table 1 Physical parameters of different layers of the designed MASnI<sub>3</sub>-based PSCs.<sup>29,42,46,52,66–69</sup>

Parameters (unit)	ETL			HTL			
	Window (FTO)	(CdS)	(WS <sub>2</sub> )	Absorber (MASnI <sub>3</sub> )	(Zn <sub>3</sub> P <sub>2</sub> )	(CuI)	(PEDOT:PSS)
Thickness (μm)	0.05	0.05	0.05	1	0.1	0.1	0.1
Band gap (eV)	3.6	2.4	2.1	1.3	1.5	3.1	2.2
Electron affinity (eV)	4	4.45	4.05	4.2	3.8	2.1	2.9
Dielectric permittivity (relative)	9	9	13.6	8.2	9	6.5	3.0
CB effective DOS (cm <sup>-3</sup> )	2.20 × 10 <sup>18</sup>	2.20 × 10 <sup>18</sup>	2.0 × 10 <sup>18</sup>	1.00 × 10 <sup>18</sup>	2.20 × 10 <sup>18</sup>	2.8 × 10 <sup>19</sup>	2.2 × 10 <sup>15</sup>
VB effective DOS (cm <sup>-3</sup> )	1.80 × 10 <sup>19</sup>	1.80 × 10 <sup>19</sup>	2.0 × 10 <sup>18</sup>	1.00 × 10 <sup>18</sup>	1.80 × 10 <sup>19</sup>	1.0 × 10 <sup>19</sup>	1.8 × 10 <sup>18</sup>
Electron thermal velocity (cm s <sup>-1</sup> )	10 <sup>7</sup>	10 <sup>7</sup>	10 <sup>7</sup>	10 <sup>7</sup>	10 <sup>7</sup>	10 <sup>7</sup>	10 <sup>7</sup>
Hole thermal velocity (cm s <sup>-1</sup> )	10 <sup>7</sup>	10 <sup>7</sup>	10 <sup>7</sup>	10 <sup>7</sup>	10 <sup>7</sup>	10 <sup>7</sup>	10 <sup>7</sup>
Electron mobility (cm <sup>2</sup> V <sup>-1</sup> s <sup>-1</sup> )	100.00	100.00	100.00	1.6	1	100	0.02
Hole mobility (cm <sup>2</sup> V <sup>-1</sup> s <sup>-1</sup> )	25.00	25.00	25	1.6	3.8	43.9	0.004
Donor density, N <sub>D</sub> (cm <sup>-3</sup> )	10 <sup>18</sup>	10 <sup>18</sup>	10 <sup>18</sup>	0	0	0	0
Acceptor density, N <sub>A</sub> (cm <sup>-3</sup> )	0	0	0	10 <sup>17</sup>	10 <sup>19</sup>	10 <sup>18</sup>	10 <sup>18</sup>
Defect type		Neutral	Neutral	Neutral	Neutral	Neutral	Neutral
Energetic distribution		Gaussian	Gaussian	Gaussian	Gaussian	Gaussian	Gaussian
Defect density, N <sub>t</sub> (cm <sup>-3</sup> )		10 <sup>15</sup>	10 <sup>15</sup>	10 <sup>14</sup>	10 <sup>15</sup>	10 <sup>15</sup>	10 <sup>15</sup>

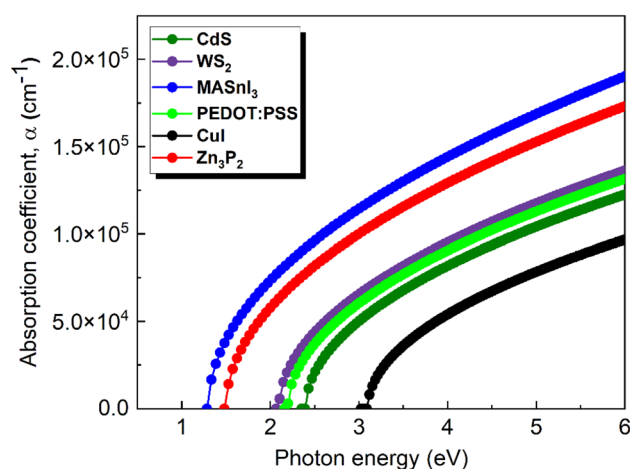
<sup>a</sup> Variable.

approximately 390 °C.<sup>65</sup> Finally, the Ni and Al metal contacts are deposited *via* thermal evaporation at room temperature to preserve the integrity of all underlying temperature-sensitive layers. This careful, descending thermal profile—from a high-temperature FTO substrate to room-temperature metal contacts—is essential to sequentially build a functional, multi-layered device without degrading previously deposited films.

Finally, with the aim of securing the highly efficient solar cells, higher CBO and lower VBO at the interface of HTL/absorber play a crucial part. The minor VBO and large CBO ensure the hindrance of the passage of electrons and boost the transportation of holes from the absorber to back terminal by conducting the HTL.<sup>51</sup> From the schematic energy band diagram, the CBO and VBO can be calculated. Fig. 2(b) illustrates the architecture of band alignment of our proposed MASnI<sub>3</sub> heterojunction PSC. It is transparent that the conduction band is higher for Zn<sub>3</sub>P<sub>2</sub> HTL than MASnI<sub>3</sub> absorber. For the purpose of conducting the simulation, all the parameters of Table 1 for different materials have been gathered from previous theoretical and experimental studies.<sup>29,42,46,52,66–69</sup> On the other hand, Table 2 presents the interface parameters for both ETL and HTL with MASnI<sub>3</sub> absorber material. Under the sunlight of AM 1.5G and a standardized temperature of 300 K, the cell device is illuminated at 100 mW cm<sup>-2</sup> of incident power density. The absorption coefficient ( $\alpha$ ) for each layer of the proposed PSC is calculated by the equation below.<sup>36</sup>

$$\alpha = A_{\alpha} \sqrt{(h\nu - E_g)} \quad (4)$$

where photon energy and energy band are implied by  $h\nu$  and  $E_g$ , respectively, and the pre-factor  $A_{\alpha}$  is set to 10<sup>5</sup> cm<sup>-1</sup> eV<sup>-1/2</sup> for every material.  $\alpha$  is the amount of light that may pass through a medium before being absorbed. It is determined on the wavelength of the light and the material.<sup>70</sup> A semiconductor material possessing high

Fig. 3 Absorption coefficient of various layers of the proposed MASnI<sub>3</sub> solar cell as a function of photon energy.Table 2 Parameters at the WS<sub>2</sub>/MASnI<sub>3</sub> and MASnI<sub>3</sub>/Zn<sub>3</sub>P<sub>2</sub> interface

Parameters (unit)	WS <sub>2</sub> /MASnI <sub>3</sub> junction	MASnI <sub>3</sub> /Zn <sub>3</sub> P <sub>2</sub> junction
Defect type	Neutral	Neutral
Capture cross-section of electrons (cm <sup>2</sup> )	10 <sup>-19</sup>	10 <sup>-19</sup>
Capture cross-section of holes (cm <sup>2</sup> )	10 <sup>-19</sup>	10 <sup>-19</sup>
Reference for defect energy level E <sub>t</sub>	Above the highest E <sub>v</sub>	Above the highest E <sub>v</sub>
Energy with respect to reference (eV)	0.6	0.6
Total density (cm <sup>-2</sup> )	10 <sup>7</sup> to 10 <sup>17</sup>	10 <sup>8</sup> to 10 <sup>18</sup>



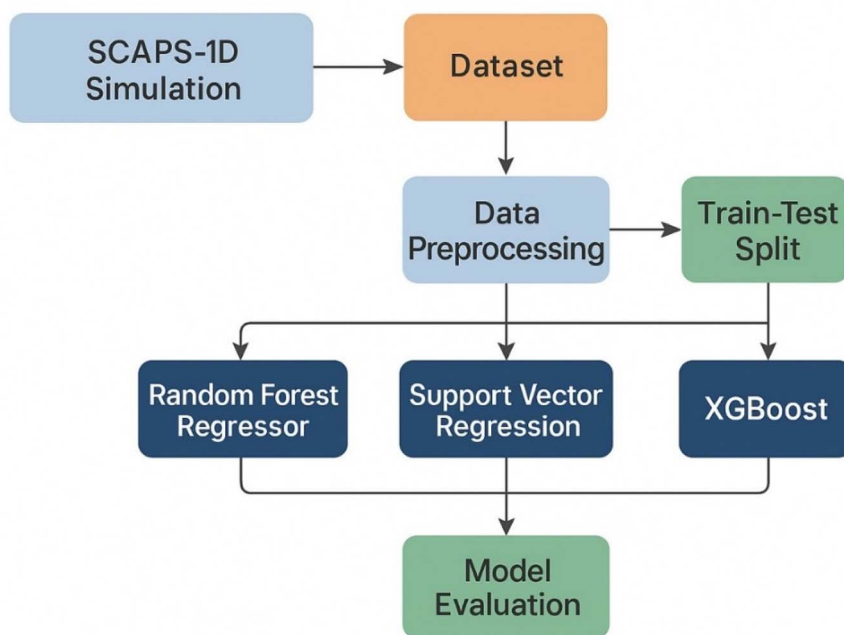


Fig. 4 Workflow of machine learning algorithms.

absorption coefficient characteristics absorbs comparatively more light than those materials that have low absorption coefficients. This process occurs when high-energy light photons drive electrons from the valence band to the conduction band, allowing them to travel more easily and improving light absorption. The value of  $\alpha$  for the  $\text{MASnI}_3$  film and different ETLs ( $\text{CdS}$ ,  $\text{WS}_2$ ) and HTLs ( $\text{CuI}$ ,  $\text{Zn}_3\text{P}_2$  and  $\text{PEDOT:PSS}$ ) is collected from the SCAPS-1D simulator. Fig. 3 shows how the absorption coefficient varies with photon energy. Each layer ensures outstanding light gathering capabilities with a substantial absorption co-efficient (over  $10^5 \text{ cm}^{-1}$ ). According to the figure, the  $\text{MASnI}_3$  absorber has the greatest absorption coefficient among the various layers.

## 2.2. Machine learning algorithm

In this study, a structured machine learning workflow was developed to predict the power conversion efficiency (PCE) of the  $\text{MASnI}_3$ -based solar cell using the dataset generated from SCAPS-1D simulations. The workflow begins with the import of key Python libraries required for data processing, model development, and visualization. Pandas and NumPy were utilized for data handling, scikit-learn for preprocessing and classical regression models, XGBoost for gradient-boosted regression, matplotlib and seaborn for plotting. The dataset was initially loaded using pandas and examined for missing values. To ensure data consistency and avoid bias during model training, all rows containing missing entries were removed using the *dropna()* method. Following data cleaning, an 80 : 20 train-test split was performed using *train\_test\_split*, with a fixed random state to maintain reproducibility. Because machine learning models—particularly distance-based and gradient-based regressors—are sensitive to feature scaling, all input features were standardized using *StandardScaler*, transforming them to zero mean and unit variance to improve training stability and convergence.

Three regression algorithms were implemented to estimate device efficiency based on the selected physical parameters: Random Forest Regressor (RF), Support Vector Regression (SVR), and Extreme Gradient Boosting (XGBoost). Each model was trained on the training subset and subsequently evaluated on the unseen test subset to assess predictive generalization. Model performance was quantified using three widely accepted regression metrics: the coefficient of determination ( $R^2$ ), mean squared error (MSE), and mean absolute error (MAE). Here,  $R^2$  measures the goodness of fit, and MSE and MAE quantify the magnitude of prediction errors.<sup>71</sup> Together, these metrics provide a comprehensive assessment of each model's predictive capability. Here, Fig. 4 presents the overall workflow of the study, illustrating each step of the process—from data generation to model development and performance evaluation.

## 3. Result and evaluation

### 3.1. Performance improvement of $\text{MASnI}_3$ perovskite solar cell

The performance of a solar module is fundamentally influenced by how quickly charge carriers recombine. Reducing the intensity of recombination enhances performance. Recombination is affected by the factors such as band alignment and barrier height at the p-n junction. Selecting suitable HTL and ETL is crucial in mitigating carrier recombination. This reduction in the rate of recombination is reflected in the improved current-voltage ( $J$ - $V$ ) properties and external quantum efficiency (EQE) metrics.

Fig. 5(a) illustrates the  $J$ - $V$  characteristics of  $\text{MASnI}_3$ -based heterojunction perovskite solar cells incorporating numerous ETLs such as  $\text{WS}_2$  and  $\text{CdS}$ , and HTLs including  $\text{PEDOT:PSS}$ ,  $\text{Zn}_3\text{P}_2$  and  $\text{CuI}$ . The PV outputs of cells with HTLs are notably



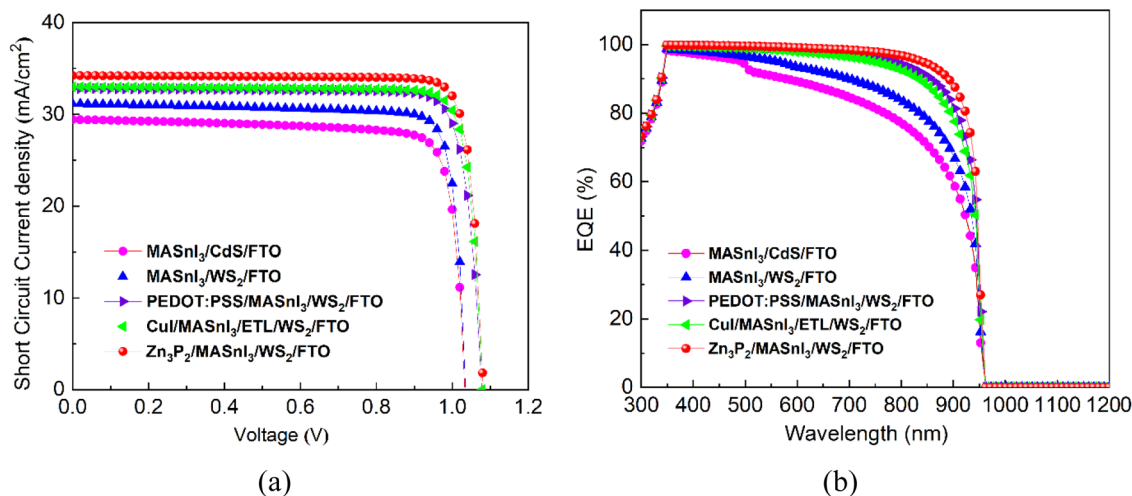


Fig. 5 Comparative analysis of (a)  $J$ - $V$  characteristics and (b) EQE responses of MASnI<sub>3</sub>-based PSCs incorporating different ETLs and HTLs.

Table 3 PV performance parameters and CBO and VBO values of MASnI<sub>3</sub>-based architecture with various ETLs and HTLs

Architectures	CBO (eV)	VBO (eV)	$V_{oc}$ (V)	$J_{sc}$ (mA cm <sup>-2</sup> )	FF (%)	PCE (%)
Al/FTO/CdS/MASnI <sub>3</sub> /Ni	-0.25	—	1.0342	29.44	83.14	25.32
Al/FTO/WS <sub>2</sub> /MASnI <sub>3</sub> /Ni	0.15	—	1.0361	31.16	85.38	27.57
Al/FTO/WS <sub>2</sub> /MASnI <sub>3</sub> /PEDOT:PSS/Ni	1.3	0.4	1.0785	32.81	85.38	30.21
Al/FTO/WS <sub>2</sub> /MASnI <sub>3</sub> /CuI/Ni	2.1	0.3	1.08	32.97	86.80	30.91
Al/FTO/WS <sub>2</sub> /MASnI <sub>3</sub> /Zn <sub>3</sub> P <sub>2</sub> /Ni	0.4	0.2	1.0815	34.19	87.35	32.30

superior to those of the conventional cell structure without an HTL, as clearly depicted in the figure. Performance metrics for each architecture are detailed in Table 3. The data also reveal that the  $J_{sc}$  for the MASnI<sub>3</sub>/WS<sub>2</sub> cell configuration surpasses that of the configuration with a CdS ETL. Specifically, for WS<sub>2</sub> ETL, a  $J_{sc}$  of 31.16 mAcm<sup>-2</sup> and a  $V_{oc}$  of 1.0363 V are achieved, while the MASnI<sub>3</sub> solar cell with CdS ETL shows a  $J_{sc}$  of 29.44 mAcm<sup>-2</sup> and a  $V_{oc}$  of 1.0342 V, respectively. Among all the configurations studied, the best performance is observed in the Ni/Zn<sub>3</sub>P<sub>2</sub>/MASnI<sub>3</sub>/WS<sub>2</sub>/FTO/Al architecture, which records efficiency of 32.30%, an FF of 87.35%, a  $J_{sc}$  of 34.19 mAcm<sup>-2</sup> and a  $V_{oc}$  of 1.08 V. The decrease in carrier recombination losses within the heterojunction is responsible for these higher efficiencies in cells containing HTLs. Minority electron passage toward the rear contact is blocked by a significant potential barrier created by a highly doped HTL placed at the rear of the absorber.<sup>39</sup>

The role of ETLs and HTLs on the output characteristics of MASnI<sub>3</sub> cells is highlighted through their EQE variation with wavelength, as illustrated in Fig. 5(b). The EQE reflects the capability of PV devices to produce and collect charge carriers from photons of specific energies.<sup>72</sup> The EQE profiles are shown across the 300–1200 nm wavelength range. The functionality of MASnI<sub>3</sub>-based solar cells has been evaluated using CdS and WS<sub>2</sub> as ETLs. The results indicate that the MASnI<sub>3</sub>/WS<sub>2</sub> solar cell outperforms the MASnI<sub>3</sub>/CdS cell. This improvement is attributed not to higher optical transparency, but to the favorable band alignment and reduced interfacial recombination provided by WS<sub>2</sub> compared to CdS. With a band gap of ~2.1 eV, WS<sub>2</sub> still absorbs part of the visible spectrum, but its superior

electronic properties and efficient charge transfer to MASnI<sub>3</sub> enhance the overall device efficiency. Additionally, the EQE curve for the Zn<sub>3</sub>P<sub>2</sub> HTL combined with the MASnI<sub>3</sub> absorber demonstrates a greater performance enhancement in the 700–900 nm wavelength range compared to other HTLs like CuI and PEDOT:PSS. This improvement attributes to the back surface field formed at the Zn<sub>3</sub>P<sub>2</sub>/MASnI<sub>3</sub> interface, which effectively collects more charge carriers from the absorber, leading to improved device performance. Moreover, when the incident photon energy is lower than the band gap of the absorber layer, the photons cannot be absorbed, leading the quantum efficiency (QE) to drop to zero. This effect is also observed in this study when the wavelength exceeds 950 nm.

The energy level diagram of the MASnI<sub>3</sub> perovskite, ETLs (CdS and WS<sub>2</sub>), and HTLs (CuI, PEDOT:PSS, and Zn<sub>3</sub>P<sub>2</sub>) is shown in Fig. 6(a). Two types of band offsets, CBO and VBO, emerge at the interface and can be computed as follows.<sup>73</sup>

$$\Delta E_c = \Delta \chi \quad (5)$$

$$\Delta E_v = \Delta E_g - \Delta E_c \quad (6)$$

The parameter  $\Delta E_g$  represents the band gap difference between the two interface materials, whereas  $\Delta \chi$  corresponds to the difference in their electron affinities.

To ensure efficient electron transfer from the absorber to the front electrode, the CBO at the ETL/absorber interface must be minimal.<sup>31,39,74</sup> Specifically, a “cliff-like” band formation occurs at the ETL/perovskite interface when the CBO is negative, while



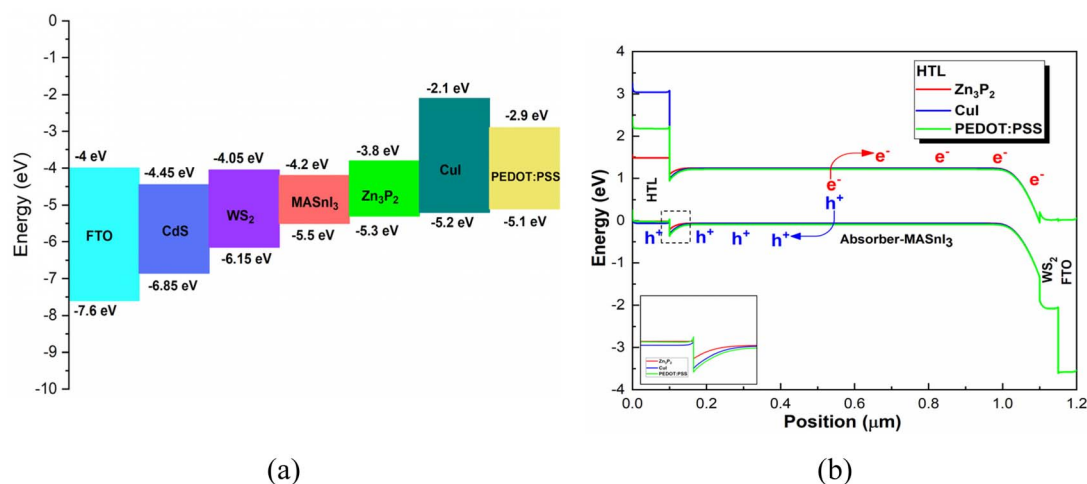


Fig. 6 (a) Energy-level arrangement in MASnI<sub>3</sub>-based PSCs and (b) schematic representation of the band diagram for devices with HTLs.

an energy “spike-like” forms at the ETL/perovskite interface when the CBO is positive.<sup>75–77</sup> This “cliff” structure introduces interface recombination, which results in reduced PV performance.<sup>78</sup> By contrast, “spike” band alignment promotes efficient electron transfer from the perovskite layer to the front contact through the ETL; meanwhile it also reduces the amount of recombination at the ETL/perovskite interface.<sup>76</sup> In this study, the CBO at the MASnI<sub>3</sub>/WS<sub>2</sub> interface is found to be 0.15 eV compared to  $-0.25$  eV at the MASnI<sub>3</sub>/CdS interface. As a result, the MASnI<sub>3</sub>/CdS interface tends to form a “cliff-like” band alignment, while the MASnI<sub>3</sub>/WS<sub>2</sub> interface exhibits a “spike-like” band configuration. This spike shape is favorable since it drops carrier recombination at the front junction, therefore boosting the overall efficiency of PSCs.<sup>76,79</sup> This evidence indicates that WS<sub>2</sub> is a more suitable candidate as an ETL, as it supports smooth electron transport. Furthermore, for effective hole transport from the absorber to the rear contact through the HTL, the CBO at the HTL/MASnI<sub>3</sub> interface needs to be positive, while the VBO should ideally be near zero or marginally negative.<sup>31,39,74</sup> The CBO and VBO values for all the interfaces are provided in Table 3. The CBO values for CuI,

PEDOT:PSS, and Zn<sub>3</sub>P<sub>2</sub> have been determined to be 2.1 eV, 1.3 eV, and 0.4 eV, respectively, while the respected VBO values are 0.3 eV, 0.4 eV, and 0.21 eV, respectively. It is clear that the value of VBO at the CuI/MASnI<sub>3</sub> and PEDOT:PSS/MASnI<sub>3</sub> interfaces is higher than the VBO at the Zn<sub>3</sub>P<sub>2</sub>/MASnI<sub>3</sub> interface. The small value of VBO at the Zn<sub>3</sub>P<sub>2</sub>/MASnI<sub>3</sub> interface may facilitate hole transport, thereby improving the overall PV performance of the solar cell. As a result, integrating a Zn<sub>3</sub>P<sub>2</sub> HTL at the rear and a WS<sub>2</sub> ETL at the front of the absorber is recommended to significantly enhance the efficiency of MASnI<sub>3</sub>-based PSCs. The schematic band diagram of MASnI<sub>3</sub>-based PSCs with various HTLs is illustrated in Fig. 6(b). It is evident from the diagram that the VBO at the Zn<sub>3</sub>P<sub>2</sub>/MASnI<sub>3</sub> interface is smaller compared to other interfaces. Minimizing the VBO at the junction promotes seamless hole transport, thereby reducing interfacial resistance and enhancing overall device performance.<sup>72,80</sup>

Furthermore, to show that the proposed MASnI<sub>3</sub>-based perovskite solar cell using WS<sub>2</sub> as the ETL and Zn<sub>3</sub>P<sub>2</sub> as the HTL performs better than the other investigated material combinations, we used Nyquist plots to evaluate the effects of the conduction band offset (CBO) and valence band offset (VBO) at

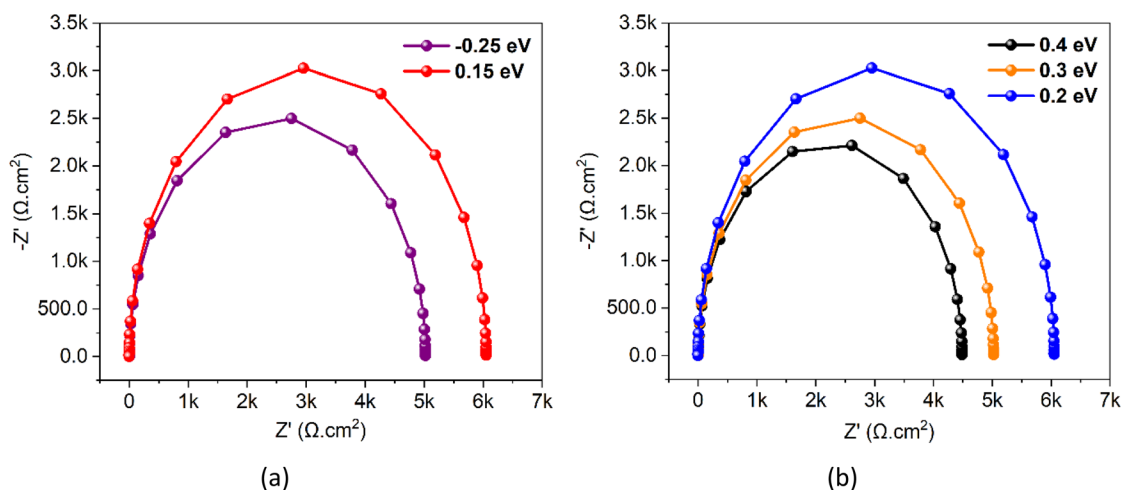


Fig. 7 Nyquist plots for different (a) CBO at the interface of MASnI<sub>3</sub>/ETL and (b) VBO at the interface of HTL/MASnI<sub>3</sub>.



the ETL/absorber and HTL/absorber interfaces, respectively. The Nyquist plots exhibit a typical semicircular pattern, where the left side corresponds to the high-frequency region and the right side represents the low-frequency region.<sup>81</sup> The simulation covers a frequency range from 1 Hz to 1 MHz, allowing us to interpret both charge-transport and recombination mechanisms accurately. The effects of CBO and VBO on the device impedance appear in Fig. 7(a) and (b). In these figures, the horizontal axis represents the real impedance ( $Z'$ ), whereas the vertical axis denotes the imaginary impedance ( $-Z''$ ).<sup>82,83</sup> Based on interface band-alignment considerations, a positive CBO at the ETL/absorber interface is essential because it creates a small spike that facilitates electron transport toward the front contact while reducing interface recombination.<sup>83</sup> Consequently, as shown in Fig. 7(a), the semicircle corresponding to a CBO of +0.15 eV at the WS<sub>2</sub>/MASnI<sub>3</sub> interface appears larger than that formed from a CBO of -0.25 eV at the CdS/MASnI<sub>3</sub> interface, indicating lower recombination and improved electron extraction for WS<sub>2</sub>.

Similarly, to minimize recombination at the back interface and ensure smooth hole extraction, the VBO at the HTL/absorber interface must be small and preferably close to zero.<sup>31,39,74</sup> As illustrated in Fig. 7(b), the semicircle associated with Zn<sub>3</sub>P<sub>2</sub>, which has a VBO of +0.2 eV, is larger than those corresponding to CuI (0.3 eV) and PEDOT:PSS (0.4 eV). This observation suggests that Zn<sub>3</sub>P<sub>2</sub> offers reduced recombination and enhanced hole-transport capability compared with the other HTLs. Overall, based on the Nyquist-plot analysis, WS<sub>2</sub> as the ETL and Zn<sub>3</sub>P<sub>2</sub> as the HTL demonstrate superior interface alignment and transport characteristics. As a result, the optimized device structure, Al/FTO/WS<sub>2</sub>/MASnI<sub>3</sub>/Zn<sub>3</sub>P<sub>2</sub>/Ni, achieves excellent photovoltaic performance, delivering a  $J_{sc}$  of 34.19 mA cm<sup>-2</sup>, a  $V_{oc}$  of 1.08 V, a fill factor of 87.35%, and a power conversion efficiency of 32.30%.

Moreover, investigating the lattice mismatch between the absorber and other films is crucial for optimizing device performance. We have calculated the percentage of lattice mismatch using based on the equation below.<sup>74,76</sup>

$$\delta = \frac{2|a_s - a_e|}{a_s + a_e} \times 100\% \quad (7)$$

here,  $a_s$  refers to substrates' lattice constant on which the overlaid layer is deposited, and  $a_e$  signifies the lattice constant of the layer itself. Table 4 displayed mismatches of MASnI<sub>3</sub> absorber with HTLs (Zn<sub>3</sub>P<sub>2</sub>, CuI, and PEDOT:PSS) and ETLs (CdS and WS<sub>2</sub>) and the least mismatch of MASnI<sub>3</sub> happens to be with Zn<sub>3</sub>P<sub>2</sub> HTL and WS<sub>2</sub> ETL.<sup>84-89</sup> Therefore, the proposed Ni/Zn<sub>3</sub>P<sub>2</sub>/MASnI<sub>3</sub>/WS<sub>2</sub>/FTO/Al cell structure exhibits a  $J_{sc}$  of 34.19 mA cm<sup>-2</sup>,  $V_{oc}$  of 1.08 V, PCE of 32.30%, and FF of 87.35%.

### 3.2. Optimization of absorber thickness and acceptor density ( $N_A$ ) for enhancing MASnI<sub>3</sub>-based perovskite solar cell performance

The impact of MASnI<sub>3</sub> absorber thickness on the performance of PV solar cells is systematically examined by shifting the thickness from 0.01  $\mu$ m to 2  $\mu$ m and is illustrated in Fig. 8(a). The study reveals that as the absorber thickness increases, all

Table 4 Lattice mismatch of MASnI<sub>3</sub> absorber with ETLs and HTLs.<sup>84-89</sup>

Layers	Lattice parameters			Lattice mismatch (%)
	$a$ ( $\text{\AA}$ )	$b$ ( $\text{\AA}$ )	$c$ ( $\text{\AA}$ )	
MASnI <sub>3</sub> (absorber)	8.73	8.95	12.5	—
WS <sub>2</sub> (ETL)	3.153	3.153	12.323	1.42%
CdS (ETL)	—	—	6.677	11.17%
Zn <sub>3</sub> P <sub>2</sub> (HTL)	8.0785	8.0785	11.3966	7.75%
PEDOT:PSS (HTL)	4.28	11.41	3.96	9.12%
CuI (HTL)	6.14	6.14	6.14	34.83%

performance metrics improve, with the PCE rising from 10.71% to 32.76%, the FF enhancing from 85.01% to 87.16%, and the  $J_{sc}$  increasing from 10.32 mA cm<sup>-2</sup> to 34.23 mA cm<sup>-2</sup>. Conversely, the  $V_{oc}$  started to decline from 1.18 V to 1.06 V. The observed improvement in PCE, FF, and  $J_{sc}$  with increased thickness is ascribed to improved light absorption and more efficient charge carrier collection within the thicker absorber layer.<sup>66,90,91</sup> This trend continues up to a thickness of approximately 1.0  $\mu$ m, beyond which the performance metrics stabilize, indicating a saturation point. In a thin absorber layer, the capacity for light absorption diminishes, resulting in a decrease in both  $J_{sc}$  and overall efficiency. The downturn in  $V_{oc}$  with growing thickness is likely results from intensified non-radiative carrier losses in the thicker absorber layer, which adversely affects the open-circuit voltage despite the gains in other performance parameters. Conversely, the increase in dark saturation current with greater thickness contributes to a decline in  $V_{oc}$ , contributing to greater electron-hole recombination.<sup>39,92</sup> The behavior of  $V_{oc}$  with varying absorber thickness can be explained using the equation below.<sup>36</sup>

$$V_{oc} = \frac{AK_B T}{q} \left[ \ln \left( 1 + \frac{J_{sc}}{J_0} \right) \right] \quad (8)$$

where the ideality factor is  $A$ , the fundamental charge is  $q$ ,  $K_B T/q$  represents the thermal voltage, and  $J_0$  indicates the reverse saturation current concentration.

This numerical study rigorously examines how the  $N_A$  Effects on PV solar cell performance metrics. The absorber doping is systematically changed over a range from 10<sup>12</sup> to 10<sup>19</sup> cm<sup>-3</sup>, as illustrated in Fig. 8(b). The PCE remains constant at 28.92% as increasing of doping density from 10<sup>12</sup> to 10<sup>15</sup> cm<sup>-3</sup>.

However, as the  $N_A$  further raises from 10<sup>15</sup> to 10<sup>19</sup> cm<sup>-3</sup>, a significant rise in PCE is observed, escalating from 28.92% to 35.37%. This increase implies that a perfect range exists for carrier concentration, maximizing efficiency by boosting carrier generation and minimizing recombination losses.<sup>74,91</sup> Similarly, the FF and  $V_{oc}$  remain stable as the carrier concentration increases up to 10<sup>15</sup> cm<sup>-3</sup>. Beyond these thresholds, the FF increases from 84.36% to 88.97%,  $V_{oc}$  improves from 1.02 to 1.19 V, as the  $N_A$  rises from 10<sup>15</sup> to 10<sup>19</sup> cm<sup>-3</sup>. The enhancement in FF results from a decrease in the series resistance of the solar cell, facilitating higher current flow with minimal resistive losses. The increase in  $V_{oc}$  results from a higher quasi-Fermi level splitting, enabled by diminished radiative recombination



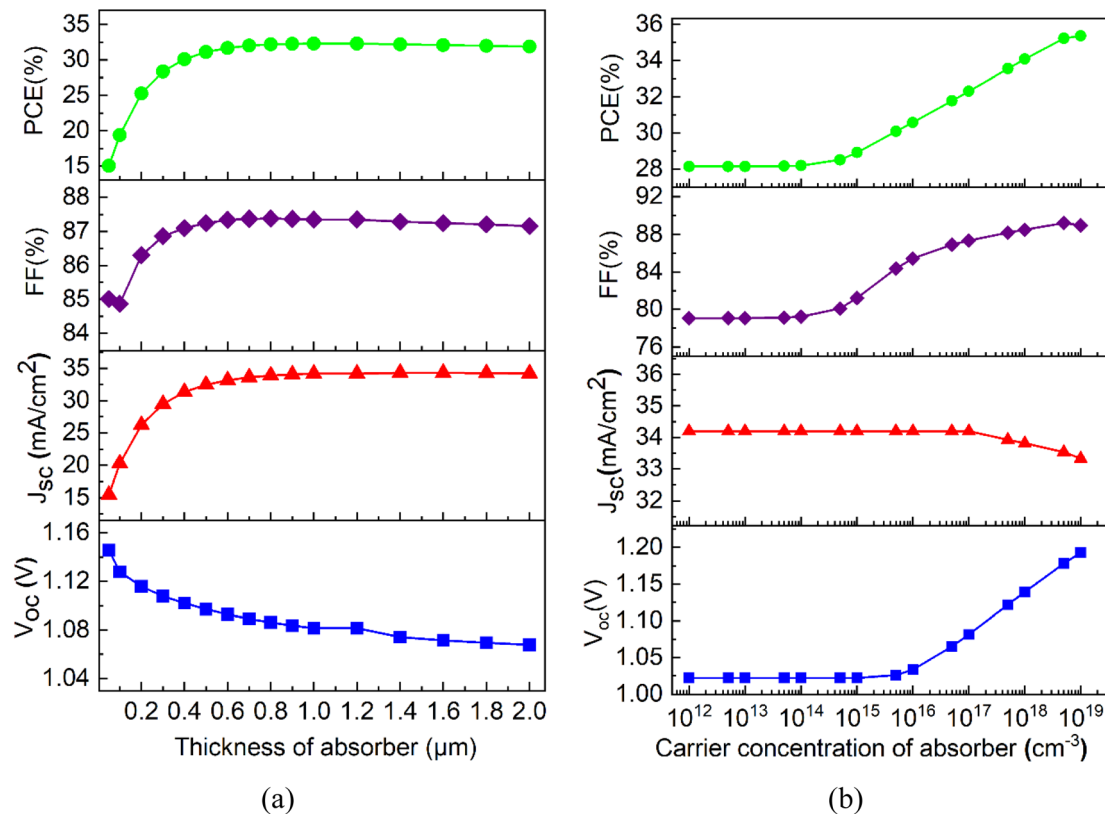


Fig. 8 Impact of absorber (a) thickness and (b) carrier concentration on MASnI<sub>3</sub>-based PSC.

within the device.<sup>76</sup> The  $J_{sc}$  maintains a steady value up to a  $N_A$  of  $10^{15}$  cm<sup>-3</sup>, beyond which it experiences a slight decrease to 33.32 mA cm<sup>-2</sup>. As doping density increases, more holes are created, leading to additional trap sites in the absorber layer, which could be the reason for the decline in  $J_{sc}$  at higher carrier concentrations.<sup>66,72,93</sup> Based on this analysis, the thickness and acceptor density of the absorber layer are chosen to be 1 μm and  $10^{17}$  cm<sup>-3</sup> respectively, for further exploration of the MASnI<sub>3</sub>-based PSC.

### 3.3. The role of defect state ( $N_t$ ) of absorber on MASnI<sub>3</sub>-based PSC

Understanding the effect of defect density ( $N_t$ ) in the MASnI<sub>3</sub> perovskite layer is vital for evaluating PV device performance. Introducing a considerable number of defects into the absorber significantly enhances the recombination rate within the solar cell leading to a significant drop in performance. Consequently, the increase in defect states impedes efficient charge extraction at the absorber/ETL interface, leading to a significant reduction in the solar cell's output characteristics.<sup>39,74</sup> Keeping all other factors constant, the value of  $N_t$  is changed from  $10^{12}$  to  $10^{18}$  cm<sup>-3</sup> to investigate the impact on output metrics. Fig. 9 depicts the corresponding variation. It is evident from the figure that after reaching a defect level of  $10^{14}$  cm<sup>-3</sup>, all performance parameters begin to degrade significantly, whereas before this point, the degradation is more gradual. As the  $N_t$  rises from  $10^{14}$  to  $10^{18}$  cm<sup>-3</sup>, the PCE and FF experience a sharp decline,

dropping from 32.32% to 7.72% and from 87.35% to 67.42%, respectively. Meanwhile, at a defect density of  $10^{12}$  cm<sup>-3</sup>, the  $V_{oc}$  is 1.2 V and the  $J_{sc}$  is 34.88 mA cm<sup>-2</sup>. When the  $N_t$  reaches to  $10^{18}$  cm<sup>-3</sup>, these values fall to 0.73 V for  $V_{oc}$  and 16.72 mA cm<sup>-2</sup> for  $J_{sc}$ . Therefore, the value of  $N_t$  of the MASnI<sub>3</sub> absorber is selected to be  $10^{14}$  cm<sup>-3</sup>. At this concentration, the PCE is determined to be 32.30%, FF is 87.35%, the  $J_{sc}$  is 34.20 mA cm<sup>-2</sup>, and the  $V_{oc}$  is 1.08 V.

### 3.4. Impact of thickness and defect density on carrier lifetime and diffusion length

In this numerical study, we explored the characteristics of carrier lifetime, and diffusion length in terms of the thickness and impurity state of the MASnI<sub>3</sub> absorber. The average period a minority carrier in a semiconductor material takes to recombine with an opposite charge carrier is define as carrier lifetime. Conversely, the diffusion length of a carrier in a material refers to the average distance an excited carrier travels before recombination occurs. Eqn (9) can be used to express and calculate the carrier lifetime.<sup>70</sup>

$$\tau_{n,p} = \frac{1}{\sigma_{n,p} N_t V_{th}} \quad (9)$$

where  $V_{th}$ ,  $\sigma_{n,p}$ , and  $\tau_{n,p}$  serves as thermal velocity of carriers, capture cross-section, and carrier lifetime and  $N_t$  denotes the absorber's defect state.



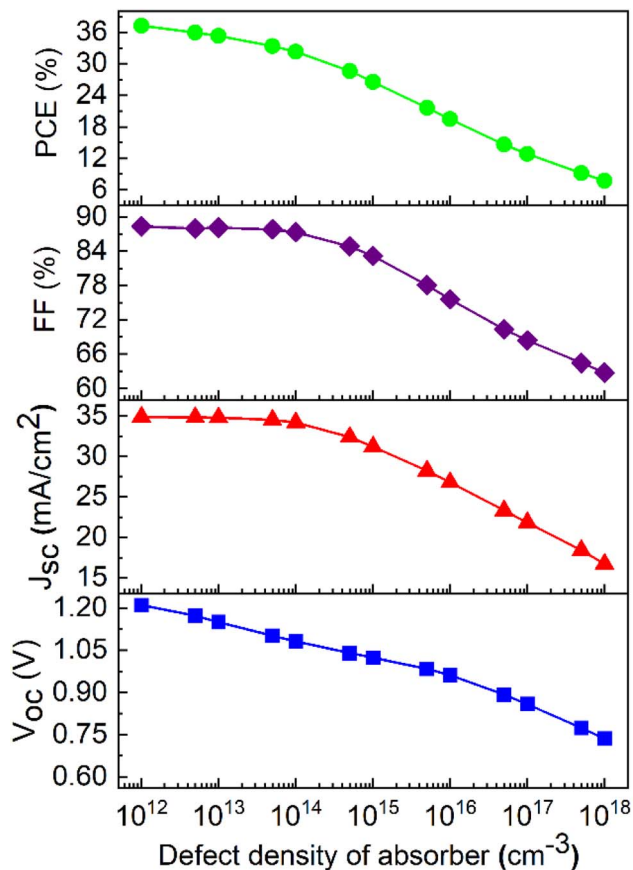


Fig. 9 Impact of absorber defect concentration on the performance of the MASnI<sub>3</sub>-based PSC.

Diffusion length is a function of carrier lifetime and mobility, as shown in the following relation.

$$L_{n,p} = \sqrt{D_{n,p} \tau_{n,p}} \quad (10)$$

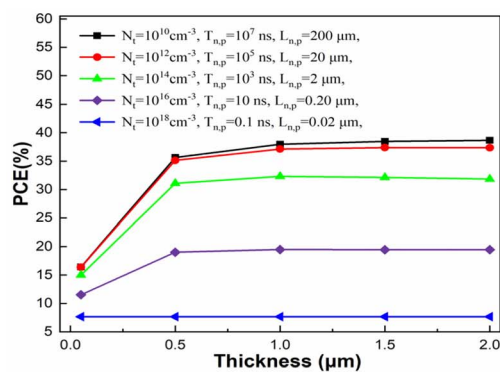
$$D_{n,p} = \frac{K_B T}{q} \mu_{n,p} \quad (11)$$

where  $L_{n,p}$  and  $\mu_{n,p}$  are diffusion length and mobility of electron and hole, respectively. Additionally,  $D$ ,  $K_B$ , and  $q$  are diffusivity,

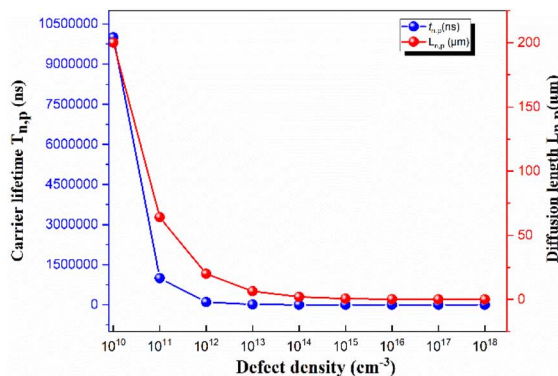
Boltzmann constant, and charge, respectively. The role of the thickness of MASnI<sub>3</sub> active layer on PCE,  $\tau_{n,p}$  and  $L_{n,p}$ , is displayed in Fig. 10(a). The figure reveals that with greater thickness, the PCE improves. At the  $N_t$  of  $10^{14} \text{ cm}^{-3}$ , the  $L_{n,p}$  is  $2 \mu\text{m}$ . Considering the cost of the material, a thickness of  $1 \mu\text{m}$  has been chosen at this defect density. From the Fig. 10(b) it can be seen that, the MASnI<sub>3</sub> absorbers defect has a profound role on  $\tau_{n,p}$  and  $L_{n,p}$ . When  $N_t$  ranges from  $10^{10} \text{ cm}^{-3}$  to  $10^{18} \text{ cm}^{-3}$ , a significant decrease in  $\tau_{n,p}$  and  $L_{n,p}$  is observed. At the impurity state of  $10^{10} \text{ cm}^{-3}$ ,  $\tau_{n,p}$  and  $L_{n,p}$  stands at  $10^7 \text{ ns}$  and  $2 \times 10^2 \mu\text{m}$ . However, at  $N_t$  of  $10^{18} \text{ cm}^{-3}$ , these characteristics dramatically drop to  $0.1 \text{ ns}$  and  $0.02 \mu\text{m}$ . This results indicates that both the degradation of PV performance and the increase in carrier recombination losses at surfaces and interfaces are highly sensitive to even minor changes in  $N_t$  due to the rapid decay of  $\tau_{n,p}$  and  $L_{n,p}$ .<sup>79,94–96</sup>

### 3.5. Effect of interface defect state on the performance of designed PSC

In this numerical simulation of MASnI<sub>3</sub>-based PSC, the influence of defect density at the Zn<sub>3</sub>P<sub>2</sub>/MASnI<sub>3</sub> and WS<sub>2</sub>/MASnI<sub>3</sub> junctions is examined. Fig. 11(a) illustrates the role of  $N_t$  at the interface of Zn<sub>3</sub>P<sub>2</sub>/MASnI<sub>3</sub> on the overall PV cell performance. In this analysis, the defect density is changed from  $10^7 \text{ cm}^{-3}$  to  $10^{17} \text{ cm}^{-3}$ . Both the PCE and FF remain stable at 32.31% and 87.35%, respectively, reaching to the density of  $10^{10} \text{ cm}^{-3}$ . However, beyond this point, they decrease to 27.54% for PCE and 85.36% for FF. Similarly, the values of  $V_{oc}$  and  $J_{sc}$  stay unchanged at 1.08 V and  $34.20 \text{ mA cm}^{-2}$  up to a defect density of  $10^{10} \text{ cm}^{-3}$ . Once the  $N_t$  exceeds this threshold, the values of  $V_{oc}$  and  $J_{sc}$  begin to decline, reaching 1.03 V and  $31.15 \text{ mA cm}^{-2}$ , respectively, as the  $N_t$  increases further. Therefore, the variation in defects at the Zn<sub>3</sub>P<sub>2</sub>/MASnI<sub>3</sub> junction has a significant impact on the performance of the PV device.<sup>31,39,66,69,91</sup> Furthermore, the influence of defect density at the WS<sub>2</sub>/MASnI<sub>3</sub> interface on output metrics of designed PV devices is assessed by varying it from  $10^8$  to  $10^{18} \text{ cm}^{-3}$ . Fig. 11(b) demonstrates the impact of interface defect density on the photovoltaic characteristics. Clearly seen from the picture that no change in performance characteristics occurs until the defect density exceeds  $10^{15} \text{ cm}^{-3}$ . As the defect state



(a)



(b)

Fig. 10 Impact of absorber layer (a) thickness and (b) defect density on charge carrier's lifetime ( $\tau_{n,p}$ ) and diffusion length ( $L_{n,p}$ ).



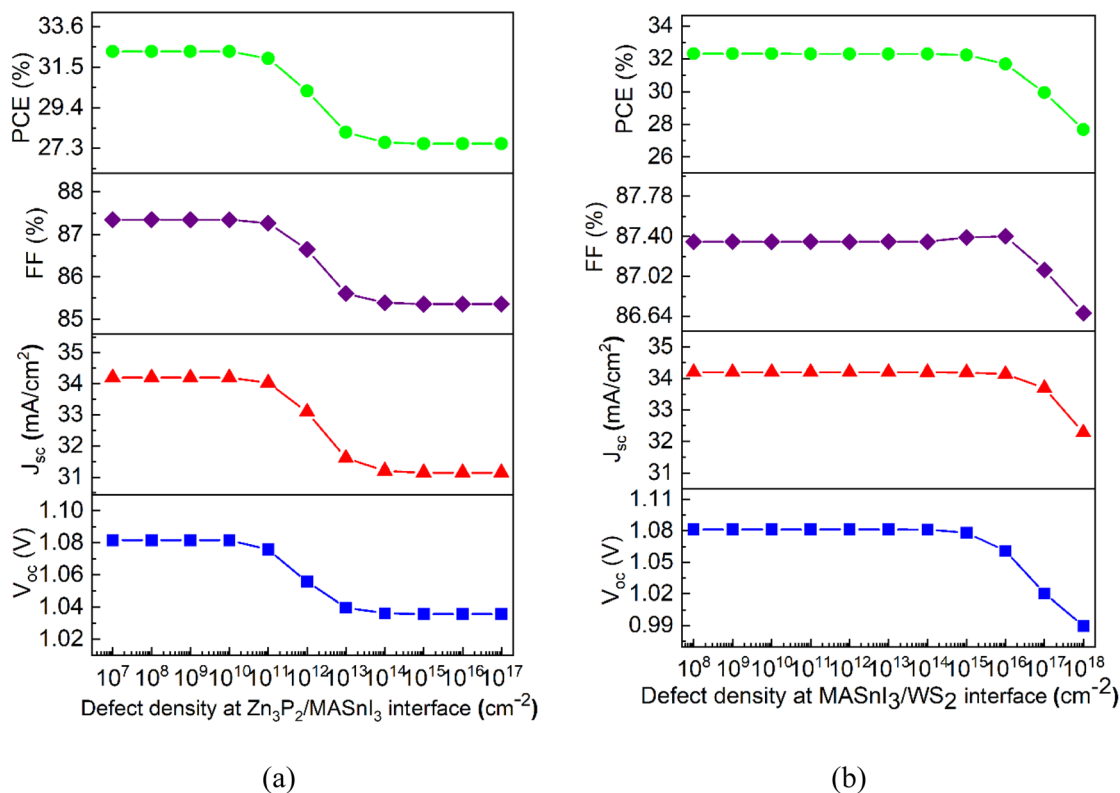


Fig. 11 Impact of defect density at the interface of (a) Zn<sub>3</sub>P<sub>2</sub>/MASnI<sub>3</sub> and (b) MASnI<sub>3</sub>/WS<sub>2</sub> on cell performance.

rises from  $10^{16}$  to  $10^{18}$  cm<sup>-3</sup>, the  $V_{oc}$  declines from 1.08 to 0.98 V. As a consequence, the PCE drops from 32.31% to 26.96%, and the  $J_{sc}$  experiences a reduction to 31.62 mA cm<sup>-2</sup>. The decreased cell efficiency can be ascribed to greater carrier recombination, which is most likely attributable to the increased defect density at the junction.<sup>39,66,69</sup> The findings clearly demonstrate that interface defects play a critical role in determining PV device performance. To enhance the PCE of the proposed MASnI<sub>3</sub> solar device, an optimal defect density of  $10^{10}$  cm<sup>-2</sup> is applied at both the MASnI<sub>3</sub>/Zn<sub>3</sub>P<sub>2</sub> and WS<sub>2</sub>/MASnI<sub>3</sub> interfaces.

### 3.6. C–V and C–F characteristics of the proposed PV device

To optimize the device's characteristics, it is essential to thoroughly understand the capacitance–voltage (C–V) and capacitance–frequency (C–F) characteristics of the proposed MASnI<sub>3</sub>-based PSC. The C–V properties of a solar module provide critical insights into its electrical behavior, material properties, and junction characteristics. These include interface and surface effects, capacitive response under varying biases, depletion region width, and the built-in potential.<sup>97</sup> By evaluating the capacitance under different bias voltages, we can study the interaction between an AC signal and a DC-biased p–n junction, offering valuable information about the dynamic charge behavior across the junction.<sup>98</sup> In this study, the total capacitance and shunt resistance at the interface of structure are modeled as parallel elements in the equivalent circuit. However, describing the entire cell as a single p–n junction is not a reliable approximation, as the proposed solar module is composed

of multiple thin-film layers. Therefore, to capture the influence of secondary p–n junctions within the device, C–V curves have been computed for both the overall architecture and the MASnI<sub>3</sub>/ETL p–n junction. To investigate the effects of deep-level defects, C–V simulations have performed at 1 MHz, since higher frequencies inhibit the ability of these defect states to follow the rapidly oscillating AC voltage. Fig. 12(a) depicts the C–V characteristics of the whole device. As illustrated, the applied voltage causes the capacitance to gradually grow. Notably, when the applied voltage is more than 0.5 V, an apparent rise in capacitance is evident, whereas the increase is more gradual below this threshold. Furthermore, Fig. 12(a) (inset) presents the Mott–Schottky sketch for the studied device. According to the Mott–Schottky relation, the built-in voltage ( $V_{bi}$ ) can be calculated from the correlation between surface capacitance ( $C$ ) and  $N_A$  on the p-doped side of the p–n junction.<sup>51,86</sup> The built-in voltage ( $V_{bi}$ ) is identified at the intersection point between the extrapolated linear region of the Mott–Schottky plot and the midpoint of the voltage axis.<sup>98–101</sup> Ideally,  $V_{oc}$  of a device should match this intrinsic voltage. However, in practice, the measured  $V_{oc}$  is typically lower, which can be attributed to internal recombination losses within the device.<sup>52</sup> In this study, the estimated value of  $V_{bi}$  is 1.16 V for the proposed device structure, where the  $V_{oc}$  of the device is 1.08 V.

The capacitance–frequency (C–F) characteristics, as depicted in Fig. 12(b), the output efficiency of the device is also crucially enhanced by their involvement. In this analysis, the evaluation of capacitance is carried out against frequency, keeping the temperature constant at 300 K, with no external bias



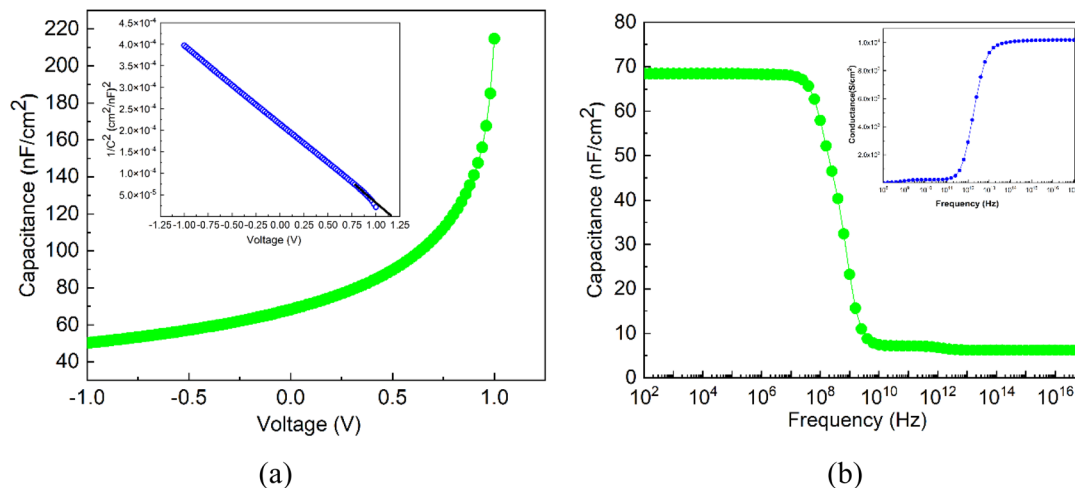


Fig. 12 (a) The  $C-V$  and (b)  $C-F$  properties of proposed  $MASnI_3$ -based solar cells.

applied.<sup>98,100–102</sup> The capacitance declines sharply with increasing frequency and eventually stabilizes at a lower level beyond approximately  $10^{10}$  Hz, can clearly be seen in Fig. 12(b). The frequency between  $10^2$  to  $10^8$  Hz have the largest capacitance values, after which a steep decline is noted as the frequency approaches and surpasses  $10^{10}$  Hz. The inset of Fig. 12(b) further exhibits the conductance behavior of the PSC device across different operating frequencies. The conductance–frequency plot indicates that the device demonstrates minimal conductance at lower frequencies. However, as the

frequency increases, a noticeable rise in conductance begins around  $10^{14}$  Hz, after which it reaches a plateau, indicating stabilization.

### 3.7. Impact of operating temperature and work function on performance of proposed PSC

The performance and long-term stability of PSCs are highly affected by variations in operating temperature, which affects both the physical properties of the perovskite absorber and the interfacial charge dynamics. In our research, we have

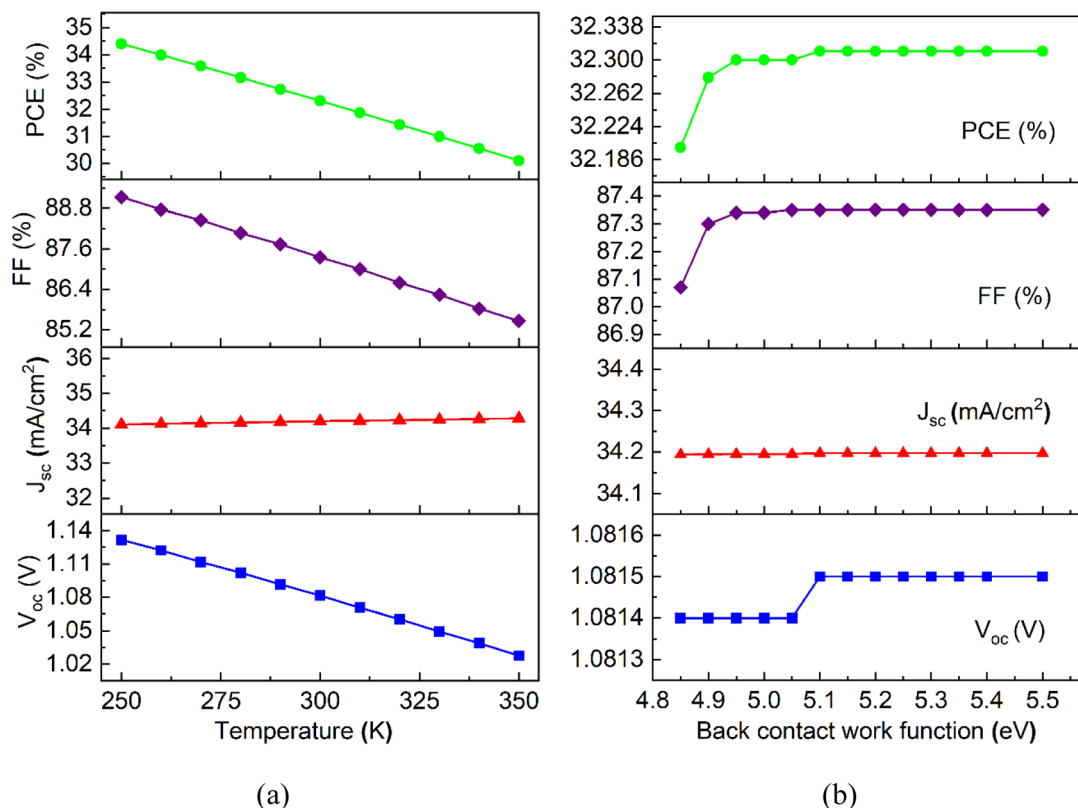


Fig. 13 Impact of (a) operating temperature and (b) work function on the properties of the designed PSC.



investigated the performance of the device under varying operating temperatures, systematically ranging from 250 K to 350 K and illustrates in Fig. 13(a). From the figure, it is apparent that, with the exception of the  $J_{sc}$ , all other photovoltaic performance parameters (PCE, FF,  $V_{oc}$ ) exhibit a linear decline as the operating temperature increases. Higher temperatures result in an increased generation of photo generated charge carriers, leading to an enhancement in the  $J_{sc}$ . However, the associated narrowing of the bandgap energy shortens the mean free path of the carriers, potentially affecting charge transport and collection efficiency.<sup>103,104</sup> Here, the  $V_{oc}$  exhibited a decrease, shifting from 1.13 V at 250 K to 1.02 V at 350 K, reflecting the impact of temperature-induced changes in the reverse saturation current and recombination processes.<sup>105</sup> Between 250 K and 350 K, the operating temperature increase causes the PCE of the proposed heterojunction PSC to decline from 34.4% to 30.1%, with the FF simultaneously decreasing from 89.13% to 85.46%. On the other hand,  $J_{sc}$  slightly increases from 34.1 mA cm<sup>-2</sup> to 34.27 mA cm<sup>-2</sup>. Following the evaluation of temperature-dependent behavior, the simulation is conducted at an operational set point of 300 K, yielding optimized PV metrics with an efficiency of 32.30%, FF of 87.35%,  $J_{sc}$  of 34.19 mA cm<sup>-2</sup> and  $V_{oc}$  of 1.08 V.

Back-contact materials with an appropriate work function (WF) are essential for efficient charge extraction, thereby directly impacting the performance of solar cells. It defines the energy barrier for carrier injection or extraction at the interfaces between the electrode and the active layers. In particular, a proper band alignment of the rear electrode WF with the energy levels of the transport layers facilitates efficient carrier collection and reduces energy losses due to reduced interfacial recombination. This work considers the role of the back contact WF with its influence clearly demonstrated in Fig. 13(b). Here, the rear electrode WF is adjusted between 4.85 and 5.55 eV to examine how it affects device performance. Fig. 13(b) illustrates that all PV performance parameters rise with the back contact WF up to 5.1 eV, after that there is no significant fluctuation. As the back-electrode work function increases, carrier barrier heights at the back interface are reduced, leading to improved charge extraction and enhanced device performance.<sup>76</sup> As rear

contact work function increases, the creation of back ohmic contact of the heterojunction device, rather than a Schottky contact, helps in increasing solar cell output. This transition allows for more efficient hole collection from the absorber layer.<sup>35,93</sup> This observation suggests that employing a rear contact with a WF exceeding 5.1 eV facilitates optimal energy level alignment, therefore improving the suggested MASn<sub>3</sub> PSCs overall performance. Consequently, Ni is selected as the back electrode, owing to its work function of 5.35 eV.<sup>61</sup> Ni is a compelling option for the back electrode in solar cell technology due to its favorable work function, chemical and thermal stability, and compatibility with common HTLs, all of which contribute to improved device performance and longevity.<sup>61</sup>

### 3.8. Impact of parasitic resistances on the performances of proposed device

This study also examines how the series resistance ( $R_s$ ) and shunt resistance ( $R_{sh}$ ) influence the performance of MASn<sub>3</sub>-based heterojunction PSCs. The corresponding  $J$ - $V$  characteristics are presented in Fig. 14(a) and (b). Series resistance ( $R_s$ ) mainly originates from the electrical interconnections among the device terminals, as well as from the resistive losses in the back metal and front contacts of the heterojunction solar cell. In contrast, the reverse saturation current generated by fabrication-related defects within the solar cell is a major factor influencing the shunt resistance ( $R_{sh}$ ). The solar cell exhibits its best performance under conditions of minimized series resistance ( $R_s$ ) and maximized shunt resistance ( $R_{sh}$ ). Elevated  $R_s$  decreases the fill factor, and very high  $R_s$  can additionally reduce the short-circuit current.<sup>74,91</sup> In this study, varying  $R_s$  from 0 to 5  $\Omega$  cm<sup>2</sup> leads to a noticeable reduction in  $J_{sc}$ , causing the PCE to drop from 32.30% to 26.9% under a constant  $R_{sh}$  of 10<sup>5</sup>  $\Omega$  cm<sup>2</sup>. Hence, reducing  $R_s$  is crucial for maintaining high photovoltaic efficiency. Fig. 14(b) presents the effect of varying shunt resistance ( $R_{sh}$ ) on the electrical outputs of the device. Solar power loss occurs when the photogenerated current is diverted through alternative pathways created by low shunt resistance. Such deviation leads to a decline in both the junction voltage and the current generated within the solar cell.

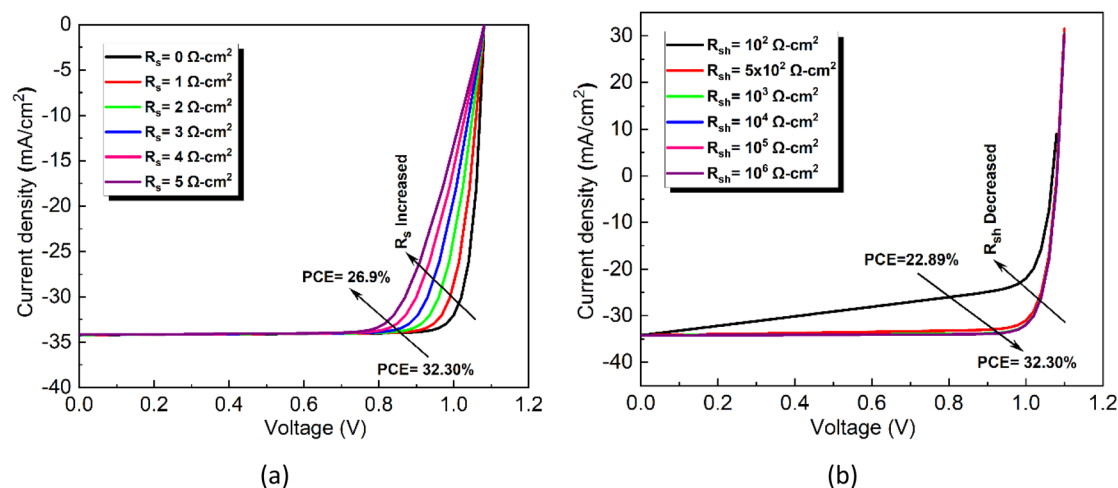


Fig. 14 Effect of (a) series and (b) shunt resistance on MASn<sub>3</sub>-based heterojunction PSCs.



Therefore, preserving a high  $R_{sh}$  value is critical to reducing power losses and enhancing the overall performance of the device. Here,  $R_{sh}$  is raised from  $100$  to  $10^6 \Omega \text{ cm}^2$  while  $R_s$  remains constant at  $0.5 \Omega \text{ cm}^2$ . With  $R_{sh}$  set at  $100 \Omega \text{ cm}^2$  and  $10^6 \Omega \text{ cm}^2$ , the proposed solar cell exhibits PCEs of 22.89% and 32.30%, respectively. It is evident from the figure that increasing shunt resistance improves both the PCE and the  $J-V$  response.

### 3.9. Cell characteristics through various ML algorithm

In this section, a comparison is conducted among three ML models to evaluate their effectiveness in predicting the efficiency of photovoltaic devices. To gain deeper insights into each model's behavior—particularly with respect to overfitting or underfitting—parity plots were employed to visualize predictions on both training and testing datasets. These plots illustrate the

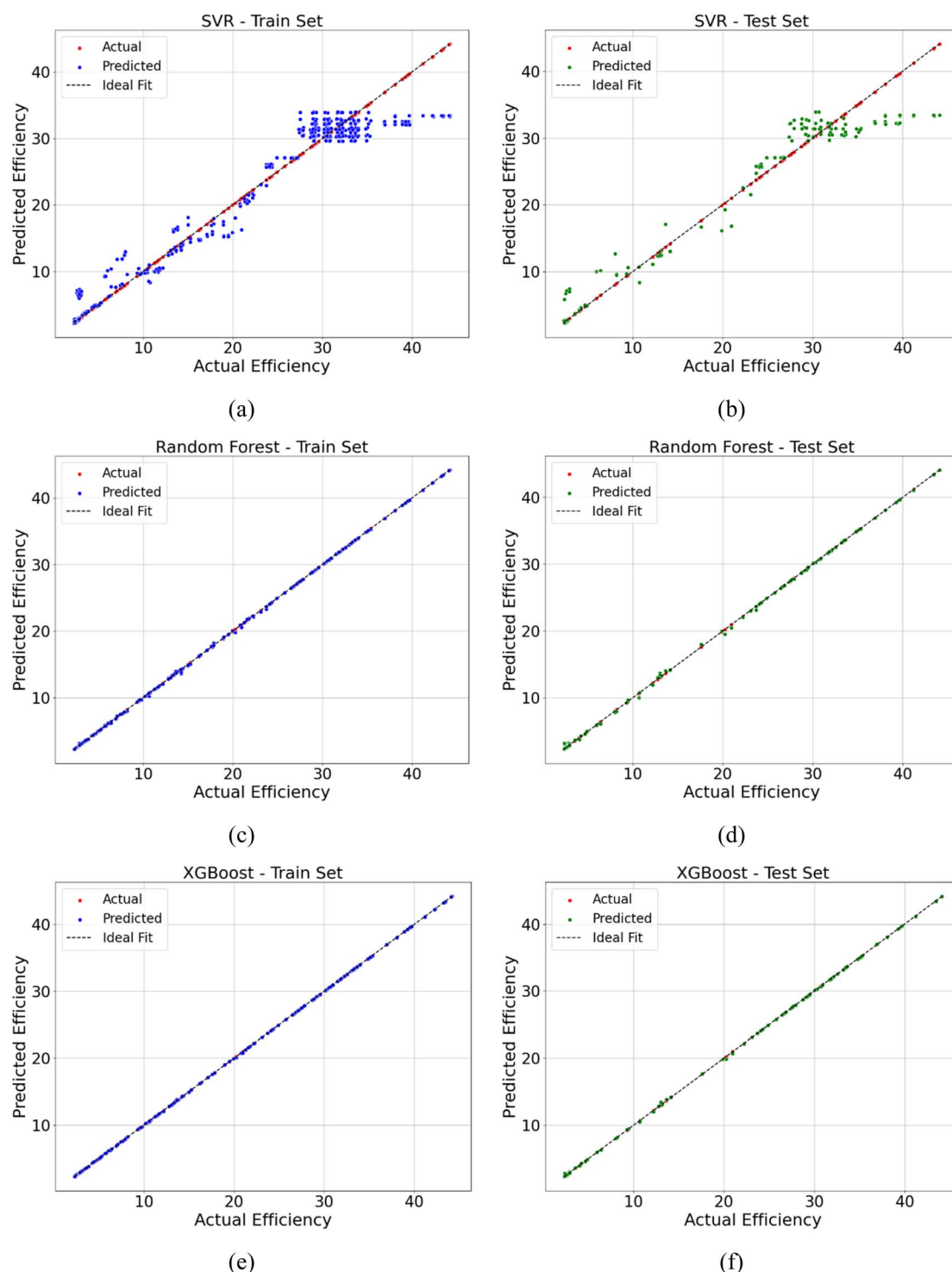


Fig. 15 Parity plot for training and testing data of various algorithms.



Table 5 A summary of the accuracy of the ML models

Performance metric	SVR		RF		XGBoost	
	Training	Testing	Training	Testing	Training	Testing
MSE	14.56	12.94	0.068	0.032	0.0103	0.0092
MAE	3.17	2.63	0.41	0.18	0.078	0.051
$R^2$	0.8902	0.9145	0.9991	0.9998	0.9995	0.9999

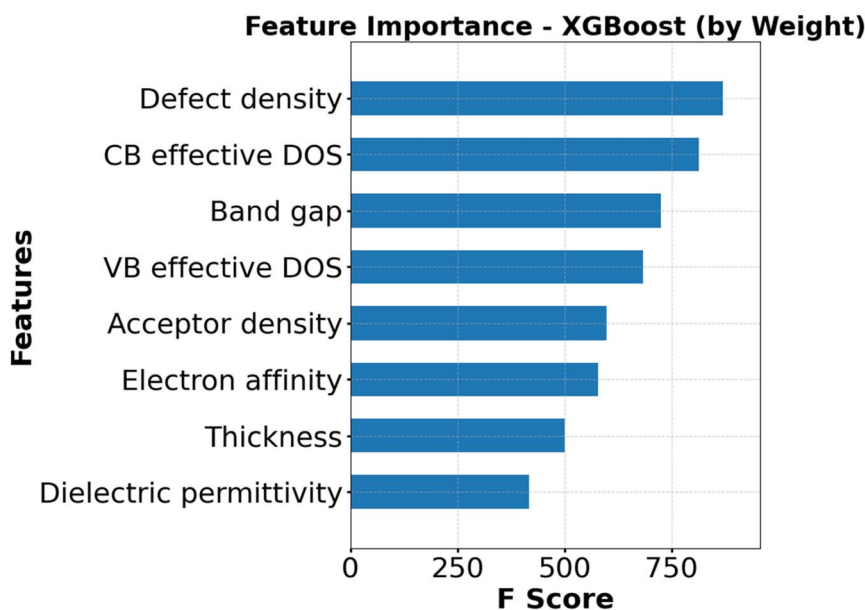


Fig. 16 Feature importance using XGBoost algorithm based on the weight metric.

relationship between actual and predicted efficiency values, with a diagonal reference line indicating the ideal fit, thereby enabling an intuitive visual assessment of model performance. Fig. 15 presents the parity plots for training and testing data across the three regression-based ML models. In addition, Table 5 summarizes the performance metrics, including the coefficient of determination ( $R^2$ ), mean squared error (MSE), and mean absolute error (MAE). Based on both the visual and quantitative evaluations suggesting that XGBoost attains the highest predictive accuracy, yielding an  $R^2$  value of 0.9999, along with a low MSE of 0.0092 and MAE of 0.051 on the testing dataset.

In order to assess the impacts of material properties on the PCE of the proposed PSC, it is essential to evaluate the relative

importance of the features.<sup>43,106</sup> In this study, feature importance was calculated using the XGBoost algorithm based on the weight metric, as illustrated in Fig. 16. Feature importance by weight in XGBoost refers to the number of times a feature is used to split the data across all the trees in the model. It is one of the simplest and most intuitive ways to measure feature importance. The more frequently a feature is used to create a split, the higher its importance score by weight. This method provides a quick overview of which features the model relies on most often during the training process. As shown in the figure, among the eight considered features, defect density exhibits the highest importance score by weight, indicating that it plays the most significant role in influencing the model's prediction of photovoltaic device efficiency.

Table 6 Various physical parameters optimized for the proposed MASnI<sub>3</sub>-based PSC

Optimized parameters (unit)	WS <sub>2</sub> ETL	MASnI <sub>3</sub> absorber	Zn <sub>3</sub> P <sub>2</sub> HTL	Junction defect density	
				MASnI <sub>3</sub> /WS <sub>2</sub>	Zn <sub>3</sub> P <sub>2</sub> /MASnI <sub>3</sub>
Thickness (μm)	0.05	1.0	0.1		
$N_D$ (cm <sup>-3</sup> )	10 <sup>18</sup>	—	—		
$N_A$ (cm <sup>-3</sup> )	—	10 <sup>17</sup>	10 <sup>18</sup>		
$N_t$ (cm <sup>-3</sup> )	10 <sup>15</sup>	10 <sup>14</sup>	10 <sup>15</sup>		
$\sigma_{n,p}$ (cm <sup>2</sup> )				10 <sup>-19</sup>	10 <sup>-19</sup>
Total density (cm <sup>-2</sup> )				10 <sup>10</sup>	10 <sup>10</sup>



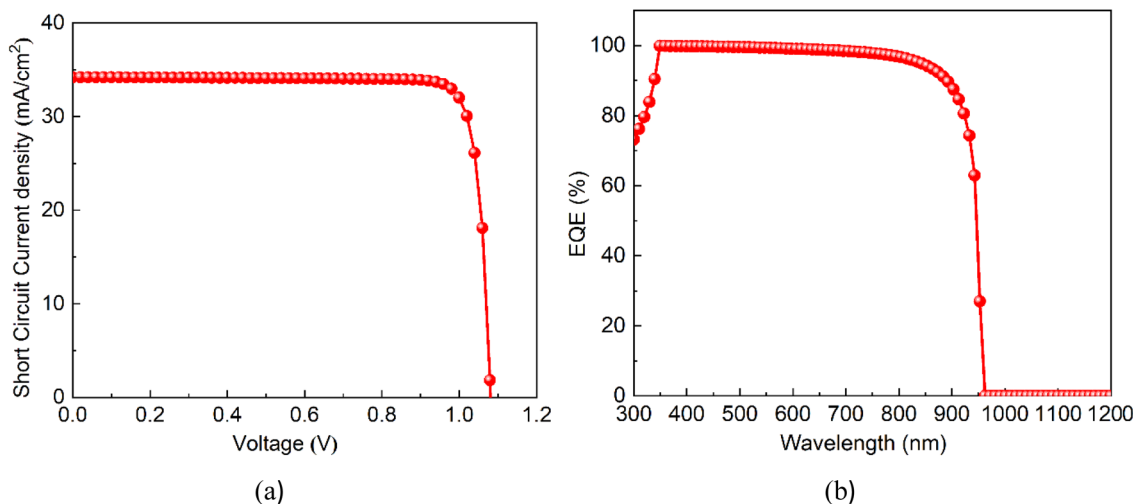


Fig. 17 Optimized (a)  $J$ - $V$  characteristics and (b) EQE spectral response of  $\text{MASnI}_3$ -based PSC.

Table 7 PV performance parameters of  $\text{MASnI}_3$ -based PSCs: comparison of earlier studies and the current investigation

Configurations	Research area	$V_{oc}$ (V)	$J_{sc}$ ( $\text{mA cm}^{-2}$ )	FF (%)	PEC (%)	Ref.
FTO/ $\text{TiO}_2$ / $\text{MASnI}_3$ /Spiro-OMeTAD/Au	Exp.	0.88	16.8	0.42	6.4	21
FTO/ $\text{TiO}_2$ / $\text{MASnI}_{3-x}\text{Br}_x$ /Spiro-OMeTAD/Au	Exp.	0.68	16.30	0.48	5.23	22
FTO/ $\text{TiO}_2$ / $\text{MASnI}_{3-x}\text{P}_x\text{I}_3$ /Spiro-OMeTAD/Au	Exp.	0.72	15.18	50.07	5.44	23
FTO/compact $\text{TiO}_2$ /mp- $\text{TiO}_2$ / $\text{MASnI}_3$ /PTAA/Au	Exp.	0.49	22.91	0.64	7.13	24
FTO/ $\text{TiO}_2$ / $\text{MASnI}_3$ / $\text{Cu}_2\text{O}$ /Au	Theo.	1.20	25.97	87.79	27.43	29
ITO/ $\text{ZnO}$ / $\text{CH}_3\text{NH}_3\text{SnI}_3$ /Spiro-OMeTAD/Au	Theo.	1.81	14.29	75.95	19.66	107
Au/ $\text{CH}_3\text{NH}_3\text{SnI}_3$ /CIGS/ $\text{TiO}_2$ / $\text{ZnO}$ :Al	Theo.	0.86	41.84	80.02	28.69	30
Al/FTO/ $\text{WS}_2$ / $\text{MASnI}_3$ / $\text{Zn}_3\text{P}_2$ /Ni	Theo.	1.08	32.30	87.35	32.30	This work

### 3.10. Overall PV performance of the proposed $\text{MASnI}_3$ -based PSC

A detailed numerical investigation is presented in this research for a novel architecture of perovskite solar cells comprising Al/FTO/ $\text{WS}_2$ / $\text{MASnI}_3$ / $\text{Zn}_3\text{P}_2$ /Ni heterojunction structure. Here,  $\text{Zn}_3\text{P}_2$  is introduced as an HTL to significantly reduce rear-side recombination and improve carrier collection. The various physical parameters optimized in this research are illustrated in Table 6. With an absorber thickness of 1  $\mu\text{m}$  for  $\text{MASnI}_3$  and 0.1  $\mu\text{m}$  for the  $\text{Zn}_3\text{P}_2$  HTL, along with their respective doping concentrations of  $10^{17} \text{ cm}^{-3}$  and  $10^{18} \text{ cm}^{-3}$  we achieve an enhanced performance in the  $\text{MASnI}_3$ -based PSC. Fig. 17(a) shows the  $J$ - $V$  characteristics of the proposed Al/FTO/ $\text{WS}_2$ / $\text{MASnI}_3$ / $\text{Zn}_3\text{P}_2$ /Ni heterojunction. Furthermore, the device performance is reflected in the EQE response, as shown in Fig. 17(b). The  $\text{MASnI}_3$  cells incorporating  $\text{WS}_2$  as the ETL demonstrate improved EQE primarily due to favorable band alignment and reduced interfacial recombination rather than increased optical transparency.<sup>72</sup> Although  $\text{WS}_2$  has a band gap of approximately 2.1 eV and absorbs part of the visible spectrum, its superior electronic properties facilitate efficient charge transfer. In addition, the  $\text{Zn}_3\text{P}_2$  HTL enhances the EQE in the 700–900 nm region due to the back-surface field formed at the  $\text{Zn}_3\text{P}_2$ / $\text{MASnI}_3$  interface, which improves carrier collection. As expected, the EQE drops to zero beyond 950 nm, where the

photon energy falls below the band gap of the absorber. Additionally, Table 7 represents the comparison of different experimental and theoretical  $\text{MASnI}_3$ -based device structures. Among them, our proposed structure demonstrates a remarkable PCE of 32.30%, with FF of 87.35%,  $V_{oc}$  of 1.08 V, and  $J_{sc}$  of 34.19  $\text{mA cm}^{-2}$ . This theoretical analysis provides an overall guideline for the researcher of perovskite solar cell technology to develop environmentally friendly highly efficient, and cost-effective  $\text{MASnI}_3$ -based PV devices.

## 4. Conclusion

In this numerical study, a novel lead-free  $\text{MASnI}_3$ -based perovskite solar cell is designed, and its photovoltaic performance is investigated using the SCAPS-1D simulation tool. Initially, several ETLs and HTLs are introduced and their band alignment and performance metrics are evaluated. Among them,  $\text{WS}_2$  as ETL and  $\text{Zn}_3\text{P}_2$  as HTL have emerged as optimal candidates because of their favorable band alignments, low toxicity, and efficient charge transport properties; consequently, recombination losses are minimized at both the front and rear interfaces, resulting in an impressive PV performance. Additionally, carrier lifetime and diffusion length characteristics regarding the  $\text{MASnI}_3$  absorber layer thickness and defect density are examined here. Moreover, the impact of temperature, metal work function, and defect density of the perovskite/



ETL and HTL/perovskite interfaces on the PV output characteristics is investigated to improve the device performance. After optimizing all the device parameters, an outstanding efficiency of 32.30%, an FF of 87.35%, a  $V_{oc}$  of 1.08 V, and a  $J_{sc}$  of 34.19 mA  $cm^{-2}$  are obtained with an absorber thickness of 1.0  $\mu m$ , an acceptor density of  $10^{17} cm^{-3}$ , and a defect density of  $10^{14} cm^{-3}$ . Finally, three machine learning methods are employed to predict the efficiency of the designed PV device as well as to determine the relative importance of individual physical parameters. Among the three algorithms, XGBoost outperforms the remaining two algorithms (SVR and RF) with an impressive  $R^2$  value of 0.9999 and a lower MSE of 0.0092. However, from the analysis it is seen that defect density exerts the greatest influence on device performance, and the predicted efficiencies closely match the simulation outcomes. These results highlight the promise of integrating theoretical modeling with AI-driven optimization to advance the design of stable, efficient, and eco-friendly lead-free perovskite solar cells.

## Conflicts of interest

There are no conflicts to declare.

## Data availability

The dataset generated and analysed during this study is available at: <https://github.com/TM-Khan-9/MASnI3-perovskite-solar-cell/blob/MASnI3-perovskite-solar-cell/ML.xlsx>, while the Notebook containing the full modelling and analysis code is available at: <https://github.com/TM-Khan-9/MASnI3-perovskite-solar-cell/blob/MASnI3-perovskite-solar-cell/IMPLEMENTATION.ipynb>. All materials are openly accessible through the GitHub repository.

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