RSC Advances

ROYAL SOCIETY OF CHEMISTRY

PAPER

View Article Online
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Cite this: *RSC Adv.*, 2026, **16**, 2873

Numerical modeling to enhance the efficiency of experimentally fabricated Sb_2Se_3-based solar cell

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Remarkable optical and electrical characteristics make antimony selenide (Sb_2Se_3) a potential absorber layer for heterojunction solar cells. In this work, a novel heterojunction Sb_2Se_3-based thin film solar cell using non-toxic tin sulfide (SnS_2) as buffer layer instead of toxic cadmium sulfide (CdS) is designed utilizing Solar Cell Capacitance Simulator in one-dimension (SCAPS-1D). To validate the simulation model, the results of experimentally fabricated glass/SnO_2:F(FTO)/CdS/Sb_2Se_3/Au solar cell structure with efficiency of 5.17% is reproduced in SCAPS. SnS_2 buffer layer provides better band alignment with the Sb_2Se_3 absorber than CdS buffer layer and improves efficiency. The device performance is optimized by altering thickness, doping concentration, bandgap, defect density, interface defect and capture cross-section for the different layers. The maximum efficiency obtained for the optimized FTO/SnS_2/Sb_2Se_3/Au photovoltaic structure is 12.31% when the Sb_2Se_3 absorber, SnS_2 buffer and FTO layer thickness are optimized at 0.4 μm, 0.03 μm, and 0.1 μm respectively and their doping are optimized at 10^{16} cm^{-3}, 10^{18} cm^{-3} and 10^{20} cm^{-3} respectively. Addition of tin monosulfide (SnS) as back surface field (BSF) layer boosts the efficiency by decreasing carrier recombination and preventing electrons from reaching back contact due to proper band alignment formed at SnS/Sb_2Se_3 interface. The efficiency of 24.86% with V_{OC} = 0.94 V, J_{SC} = 31.98 mA cm^{-2}, and FF = 83.09% is obtained for the proposed FTO/SnS_2/Sb_2Se_3/SnS/Au photovoltaic structure with SnS BSF layer at thickness of 0.2 μm and doping of 10^{20} cm^{-3}. Moreover, the impacts of operating temperature, parasitic resistance and back contact work function on the performance parameters of the designed solar cell are analyzed. These findings indicate that non-toxic SnS and SnS_2 can be utilized as a promising BSF and buffer layer respectively to produce cost-effective, environmental friendly and extremely efficient Sb_2Se_3-based thin film solar cell.

Received 20th June 2025
Accepted 2nd January 2026

DOI: 10.1039/d5ra04411a

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1. Introduction

At present, the expeditious exhaustion of fossil fuels because of large-scale industrialization as well as the quick rise in requirement for conventional energy sources has resulted in severe economic and environmental concerns.[1–4] In this respect, solar cell is a promising solution for ecological and sustainable energy generation which can convert sunlight into high-efficient and cost-effective electrical energy.[5–7] The photovoltaic (PV) researchers are introducing different novel concepts of solar-cell architectures and production considering the stability, climate issues, efficacy and cost in terms of industrial production. Thin film solar cells (TFSCs) have achieved widespread attention because of high performance and fast growth among the various types of PV solar cells.[8–10] At present, metallic chalcogenides copper-indium-gallium-selenide (CIGS) and cadmium telluride (CdTe) based TFSCs are considered as promising candidates for electricity generation with efficiency beyond 23%.[11,12] But these absorbers have several disadvantages such as toxicity, high cost and scarcity.[13,14] Conventional kesterite-based absorbers such as copper zinc tin sulphide selenide (CZTSSe) obtained highest efficiency of 12.6% due to problems of controlling the composition and defects during fabrication.[15] Recently, Sb_2Se_3, a binary compound, has displayed superb potential as an absorber layer in TFSC technology.[16–18] It is composed of earth-abundant and less-toxic elements. It has a band gap of 1.1–1.3 eV, long carrier lifetime, a high absorption coefficient over the visible spectrum (>10^5 cm^{-1}), low melting point (550 °C) and decent carrier mobility (hole mobility up to 42 cm^2 V^{-1} s^{-1} and electron mobility above 16.9 cm^2 V^{-1} s^{-1}).[12,17,19–21] Moreover, benign grain boundary structure of Sb_2Se_3 makes it a potential absorber material.[22] An efficiency of 0.66% was obtained by Messina *et al.* in 2009 using CdS as a buffer layer.[23] Choi *et al.* and Zhou *et al.* obtained 3.21% and 2.26% efficiency using TiO_2 buffer layer in 2014.[24,25] In 2017, Chen *et al.* and Wang *et al.* achieved 6.5% and 5.93% efficiency with CdS and ZnO buffer layers respectively.[16,18] By employing a vapor-transport method, Wen *et al.* obtained 7.6% efficiency using CdS buffer layer in 2018.[26] In 2019, Li *et al.* obtained highest efficiency of 9.2% using CdS buffer layer for Sb_2Se_3 based solar cells by junction

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interface engineering.[19] In 2021, Guo *et al.* obtained an efficiency of 7.15% by incorporating NiO_x as back surface field (BSF) layer.[27] Recently, Tang *et al.* have obtained efficiency of 8.64% by sputtering method.[28] In 2022, Dong *et al.* obtained an efficiency of 6.7% by optimizing deep defects containing V_{Se} on the Sb_2Se_3 film.[29] The efficiency of Sb_2Se_3-based solar cells still far from the theoretical value of 31% according to Shockley–Queisser limit.[30] Different methods namely electrodeposition, spin coating, sputtering, spray pyrolysis, chemical bath deposition and vacuum evaporation have been employed to achieve high quality Sb_2Se_3 film.[31] Sb_2Se_3 has various applications in memory gadgets, solar cells, photodetectors and batteries.[32] To obtain the theoretical efficiency of Sb_2Se_3 based solar cells, various simulation studies have been performed. Basak *et al.* have obtained efficiency of 12.62% for Sb_2Se_3/CdS heterojunction solar cell structure.[33] An efficiency of 13.20% was obtained by Baig *et al.* using CNT/Cu_2O/Sb_2Se_3/In_2S_3/ITO photovoltaic architecture.[34] Kumari *et al.* achieved 24% efficiency in Mo/Sb_2Se_3/ZnSe/Ag solar cell structure.[17] Mamta *et al.* gained 27.84% efficiency in Sb_2Se_3/CdS/ZnO solar cell structure.[35] Ahmed *et al.* obtained 29.35% efficiency for Mo/$BaSi_2$/Sb_2Se_3/CdS/FTO/Al solar cell architecture.[36] Sunny *et al.* achieved 29.89% efficiency for Al/F:SnO_2(FTO)/CdS/Sb_2Se_3/SnS/Mo solar cell structure.[37]

An ideal buffer layer should have high electrical conductivity, decent carrier mobility and a proper band alignment with minimum conduction band offset (CBO).[38] In experimental Sb_2Se_3 based solar cell, CdS functions as mostly used buffer layer due to its electrical and chemical stability.[12,39,40] The main problem with CdS is its toxicity which causes human and environmental health issues.[41,42] Moreover, large lattice mismatch and diffusion of S and Cd into the Sb_2Se_3 film degrades cell performance.[17] Several works have used other buffer layers such as ZnO,[43] TiO_2 (ref. 44) and SnO_2 (ref. 45) instead of CdS layer. The two-dimensional (2D) chalcogenide sulfur (S)-based tin sulfide (SnS_2) with an appropriate bandgap of 1.82–2.88 eV and a large absorption coefficient of $\sim 10^5$ cm^{-1} is a promising buffer material for producing high-performance solar cells.[46,47] It is cheap, non-toxic and has high electron mobility values of 50 cm^2 V^{-1} s^{-1}.[48] The wide bandgap of SnS_2 allows loss-free passage of incident light spectrum. Moreover, proper band alignment with absorber layer provides efficient transporting of electrons from absorber layer to the contacts reducing the recombination of holes and electrons and thus boosting the cell efficiency. It can be deposited employing spray pyrolysis, hydrothermal, co-precipitation, chemical vapor deposition (CVD) and chemical bath deposition.[49–52] In this work, SnS_2 is used as a buffer layer for the proposed Sb_2Se_3 based solar cell.

Ineffective carrier transport and collection by the front and back contacts and carrier recombination at the back contact are the main reasons for poor solar cell efficiency. By inserting the back surface field (BSF) layer between the back contact and absorber layer, the solar cell performance can be enhanced by lowering the surface recombination rate (SRV) and delivering easy transportation of holes to the back electrode by minimizing the barrier height of the back electrode.[53,54] Many researchers have added inorganic and organic BSF layers such as NiO_x, Cu_2O, VO_x, CZTA, P3HT, PEDOT:PSS, SpiroMeOTAD.[12,34,55–58] Due to toxicity of inorganic BSFs and instability of organic BSFs, researchers are looking for non-toxic and stable BSF layer. In previous studies, inorganic tin monosulfide (SnS) is employed as a BSF layer to reduce carrier recombination at BSF/back contact interface.[37,59,60] It has excellent optoelectronic characteristics such as suitable bandgap of 1.1–1.4 eV, high hole mobility, nontoxicity, cheap and large absorption coefficient (>10^4 cm^{-1}).[61–64] Various techniques such as spray pyrolysis, electron beam evaporation, chemical synthesis, sputtering, atomic layer deposition (ALD), thermal evaporation (TE) and vapor transport deposition (VTD) have been used for deposition of SnS films.[62,65–71] In this work, SnS is proposed as BSF layer for Sb_2Se_3 based TFSC due to its proper band alignment with absorber layer. Though SnS and SnS_2 are used as BSF and buffer layer respectively in previous studies,[37,72] this novel SnO_2: F(FTO)/SnS_2/Sb_2Se_3/SnS/Au dual-heterojunction (DH) structure using combined use of SnS and SnS_2 as BSF and buffer layer respectively in Sb_2Se_3 based solar cell has never been simulated to the best of my knowledge. The reason for high efficiency and light trapping of DH solar cell has been achieved as a result of the longer wavelength photon absorption in the p^+-SnS BSF layer through a tail-states assisted (TSA) two-steps photon upconversion phenomenon. Most previous studies have explored on single absorber structures, overlooking the promising efficiency enhancements obtained by dual absorber layer architectures. There is also limited research on how such dual-heterojunction structures effect efficiency and carrier transport mechanisms in thin film solar cells. The present study aims to systematically explore a novel thin-film solar cell architecture comprising Sb_2Se_3, SnS_2 and SnS as absorber, buffer and BSF layer respectively to examine how such an architecture can enhance solar cell performance while eliminating toxic element dependency, thereby bestowing to both material sustainability and technological evolution in next-generation solar cells.

In this present work, a numerical modeling is applied employing SCAPS-1D software to compare simulation results with experimental findings of glass/SnO_2:F(FTO)/CdS/Sb_2Se_3/Au solar cell structure by Li *et al.*[73] After that, toxic CdS is replaced with non-toxic SnS_2 buffer layer which boosts device performance. Then investigation is performed by tuning thickness, doping density, bandgap, defect density and capture cross section of different layers to boost efficiency of proposed cell. Afterwards, SnS is inserted as BSF layer and its physical parameters are optimized to enhance device performance. Finally, the influence of back contact work function, temperature and series and shunt resistance on electrical parameters such as open circuit voltage (V_{OC}), short-circuit current density (J_{SC}), fill factor (FF) and efficiency (η) of proposed cell is also analyzed. The proposed architecture has the potential to notably enhance the stability and performance of Sb_2Se_3 based photovoltaic by enhancing the carrier collection and decreasing the back surface recombination.

2. Numerical simulation and methodology

2.1 Simulation methodology and device architecture

To analyze the proposed glass/FTO/SnS_2/Sb_2Se_3/SnS/Au photovoltaic, the one-dimensional Solar Cell Capacitance Simulator (SCAPS) software version 3.3.09 is applied for numerical simulations. SCAPS-1D application was invented at the Department of Electronics and Information Systems of the University of Ghent, Belgium. There are several other programs to model and simulate solar cell characteristics depending on the device's input hierarchy, including SILVACO ATLAS, COMSOL, AMPS, AFORS-HET, PECSIM and Wx-AMPS.[74,75] However, most of them require expensive licensing fees and high computational resources, making them rarely available for quick device optimization and design. But SCAPS software has many advantages compared to others including the potential to carry out performance examination across up to seven levels, in depth and batch analyses, and simple findings to comprehend and investigate.[76] It is the best accurate non-commercial tool with friendly dialog box, straightforward in operation and supports multi-junction solar cells.[77] Interestingly, the SCAPS-1D is available cost-free and provides results that matches with experimental findings. It is designed to simulate and model solar cells with a heterojunction and homojunction. Thus, providing it a significant edge over the other solar cell simulators. It incorporates complicated simulations of carrier transport, recombination, generation, defects and interface impacts in solar cells which makes it effective and reliable for simulation of photovoltaic devices.[78] All input files that are provided in SCAPS are user-accessible text files, for example the spectral data. Moreover, it is very fast which other programs may lag significantly and the incorporation of metal contacts, shunt resistance, series resistance, capacitance and frequency response and capacitance and voltage relation make this software robust.[79] It has been extensively validated across solar cell research community and different material systems, highlighting its predictive correctness and reliability.[80] Thus, the present research is carried out using the SCAPS-1D simulation tool. It is applied to predict and analyze the optoelectronic parameters of solar cell architectures such as open circuit voltage (V_{OC}), short-circuit current density (J_{SC}), fill factor (FF) and efficiency (η) by dealing fundamental equations such as drift-diffusion equation, Poisson's equation and carrier continuity equation.[81] These equations are numerically solved in one dimension by this program.

Fig. 1a depicts the Sb_2Se_3 baseline superstrate glass/SnO_2:F(FTO)/CdS/Sb_2Se_3/Au solar cell structure manufactured experimentally by Li *et al.* implementing close-space sublimation (CSS) method which provides higher quality of Sb_2Se_3 absorber film deposition and improved device heterojunctions due to independent control of the substrate and source temperatures.[73] Fig. 1b illustrates proposed glass/FTO/SnS_2/Sb_2Se_3/SnS/Au photovoltaic architecture for the maximum efficiency that is the objective of this article. A p-type Sb_2Se_3 absorber layer, n-type SnS_2 buffer, and FTO (fluorine-doped tin oxide) window

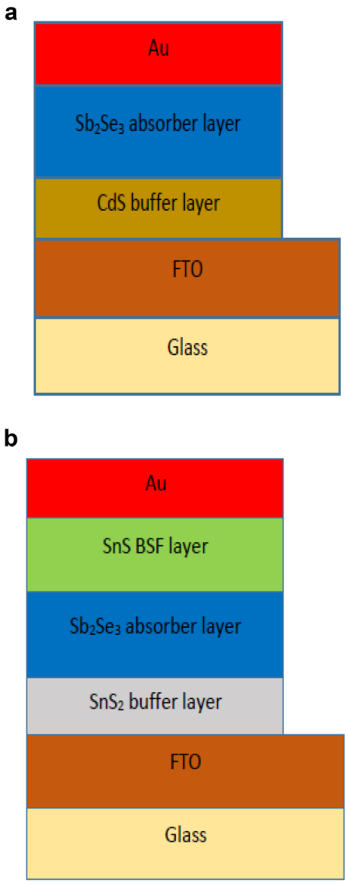

Fig. 1 (a). Schematic diagram of the reference glass/FTO/CdS/Sb_2Se_3/Au solar cell. (b) Schematic diagram of the proposed glass/FTO/SnS_2/Sb_2Se_3/SnS/Au solar cell.

layer compose the proposed solar cell. Moreover, SnS is added as the BSF layer to boost efficiency. FTO and gold (Au) are used as front and back contacts respectively. Table 1 represents material parameters applied in the proposed Sb_2Se_3-based photovoltaic with BSF layer obtained from both simulation and practical works. In order to find equality between experimental and simulation findings, bulk layers and absorber/buffer interface are incorporated with defects. The interfacial defect and contact parameters applied in this work are listed in Tables 2 and 3 respectively. To reproduce experimental results, the BSF layer is not inserted in the initial section of simulation. The simulation study has been performed under AM 1.5 G spectral irradiation (100 mW cm^{-2}) at 300 K. Moreover, the absorption coefficient $\alpha(\lambda)$ for films is obtained using the new modified E_g-sqrt model, which is an updated version of the traditional sqrt $(h\nu - E_g)$ model. The "Tauc law" demonstrates this relationship as illustrated in eqn (1).

$$\alpha(\lambda) = \left(\alpha_0 + \beta_0 \frac{E_g}{h\nu}\right)\sqrt{\frac{h\nu}{E_g} - 1} \quad (1)$$

Here, $\alpha(\lambda)$ represents the optical absorption coefficient as a function of wavelength (λ) or photon energy ($h\nu$) and E_g denotes the bandgap. Eqn (2) and (3) relate the model constants

Table 1 Material parameters employed for simulating Sb_2Se_3 based thin film solar cell

Parameter	Sb_2Se_3 (ref. 20)	CdS[20]	SnS_2 (ref. 5)	FTO[20]	SnS[86]
Absorption co-efficient (α) (cm^{-1})	SCAPS	SCAPS	SCAPS	SCAPS	SCAPS
Thickness (μm)	0.54	0.05	0.05	0.5	0.1
Bandgap (eV)	1.03	2.4	2.24	3.6	1.2
Electron affinity (eV)	4.15	4.0	4.2	4.0	4.2
Dielectric permittivity	14.5	10	10	9	13
CB effective density of states (cm^{-3})	8×10^{17}	2.2×10^{18}	2.2×10^{18}	2.2×10^{18}	1.18×10^{18}
VB effective density of states (cm^{-3})	1.8×10^{19}	1.8×10^{19}	1.8×10^{19}	1.8×10^{19}	4.76×10^{18}
Electron thermal velocity (cm s^{-1})	1×10^{7}	1×10^{7}	1×10^{7}	1×10^{7}	1×10^{7}
Hole thermal velocity (cm^{-1})	1×10^{7}	1×10^{7}	1×10^{7}	1×10^{7}	1×10^{7}
Electron mobility (cm^2 V^{-1} s^{-1})	15	80	50	20	30
Hole mobility (cm^2 V^{-1} s^{-1})	15	25	50	10	90
Shallow uniform donor density, N_D (cm^{-3})	0	1×10^{18}	1×10^{18}	1×10^{17}	0
Shallow uniform acceptor density, N_A (cm^{-3})	1×10^{13}	0	0	0	1×10^{18}
Defect type	Donor	Acceptor	Acceptor	Donor	Donor
Energetic distribution	Single	Single	Single	Single	Single
Capture cross section of electrons (cm^2)	2.3×10^{-11}	1.5×10^{-12}	1.5×10^{-12}	1×10^{-12}	1×10^{-15}
Capture cross section of holes (cm^2)	4.39×10^{-11}	1.5×10^{-12}	1.5×10^{-12}	1×10^{-14}	1×10^{-15}
Defect density, N_t (cm^{-3})	1×10^{13}	1×10^{18}	1×10^{15}	1×10^{16}	1×10^{14}

α_0 and β_0 to the conventional model constants A and B as illustrated below:

$$\alpha_0 = A\sqrt{E_g} \quad (2)$$

$$\beta_0 = \frac{B}{\sqrt{E_g}} \quad (3)$$

The material absorption spectra is produced automatically depending on the $\sqrt{E_g}$ model and the input parameters supplied, including A and B in SCAPS-1D.[82,83] The sub-bandgap absorption impact on solar cell performance is automatically accounted by SCAPS software once the optical data are supplied. Conversely, there are limitations of SCAPS. One of its limitations is that it can provide imprecision results if applied to complex structures or long simulation times because it uses a simplified optical model. It can overestimate the incident light intensity that generates charge due to its inability to account automatically reflection losses that is present at intermediate interfaces. Additionally, there is an uncertain illustration for a secondary barrier or n–p (rather than p–n) junction.[75] Nanostructural characteristics or plasmonic impacts are some vital light-management methods that are not precisely simulated by it.[84] It is required to incorporate wavelength–dependent complex refractive index (n–k) values for materials in SCAPS to increase the simulation correctness.[80,85] Despite these limitations, SCAPS is still advantageous due to its ability to produce results close to experimental findings and its flexible configurations.

2.2 Methodology for optimizing solar cell performance parameters

At first, the parameters listed in Tables 1–3 are used to produce solar cell performance parameters that matches experimental findings to validate the simulation model in this research. Afterwards, 15 steps are carried out to obtain optimal values based on varied parameters listed in Tables 1–3. The optimized

Table 2 Interface defect parameters used in simulation

Parameters	Sb_2Se_3/CdS	Sb_2Se_3/SnS_2	Sb_2Se_3/SnS
Defect type	Neutral	Neutral	Neutral
Energetic distribution	Single	Single	Single
Capture cross section of electrons/holes (cm^2)	1×10^{-10}	1×10^{-10}	1×10^{-19}
Defect density, N_t (cm^{-2})	5×10^{17}	5×10^{17}	1×10^{10}

Table 3 Contact parameters used in simulation

Parameter	Back contact	Front contact
Work function	5.1 eV	4.4 eV
Surface recombination velocity of holes (cm s^{-1})	1×10^{7}	1×10^{7}
Surface recombination velocity of electrons (cm s^{-1})	1×10^{7}	1×10^{7}

result obtained in each step is used for the reference cell for the next step.

Step 1: except for the thickness of Sb_2Se_3 absorber layer that is varied from 0.1 μm to 1.5 μm, the rest of the parameters are kept constant.

Step 2: the optimum thickness of Sb_2Se_3 from the previous step is used as a constant parameter in this step and the carrier density of this layer is changed from 10^{12}–5×10^{16} cm^{-3}.

Step 3: the defect density of Sb_2Se_3 is varied in the range of 10^{10}–10^{15} cm^{-3} to study its impact on optimized cell obtained in the previous step.

Step 4: in this step, the bandgap of Sb_2Se_3 in the range of 1–1.3 eV is investigated to study its impact on the proposed cell performance.

Step 5: after optimizing the Sb_2Se_3 absorber layer, the thickness of SnS_2 buffer layer is varied from 0.01 μm to 0.1 μm to study its impact on device performance.

Step 6: the impact of SnS_2 buffer layer carrier density on the photovoltaic parameters of the optimized cell in the previous step is studied by varying it between 10^{13} cm^{-3} and 10^{18} cm^{-3}.

Step 7: the defect density of the SnS_2 layer is varied between 10^{10} cm^{-3} and 10^{18} cm^{-3} while the rest parameters are kept at their optimum values.

Step 8: the effect of FTO window layer thickness is investigated in the range of 0.1–0.6 μm.

Step 9: the carrier concentration of FTO layer is explored in the range of 10^{17}–10^{20} cm^{-3} to optimize its value.

Step 10: the impact of Sb_2Se_3/SnS_2 interface defect on performance parameters of the proposed cell is explored in the defect density range of 10^{7}–10^{18} cm^{-2}.

Step 11: the capture cross-section of electron and hole of the Sb_2Se_3 layer is varied between 10^{-19} cm^{-2} and 10^{-9} cm^{-2} while the rest parameters are kept at their optimum values.

Step 12: in this step, the impact of the capture cross-section of electron and hole of the Sb_2Se_3/SnS_2 interface layer is explored to study its impact on performance parameters of optimized cell in the previous step in the range of 10^{-20}–10^{-8} cm^{-2}.

Step 13: after optimizing Sb_2Se_3, SnS_2 and FTO layer, the thickness of SnS BSF layer is changed from 0.02 μm to 0.2 μm to optimize its value.

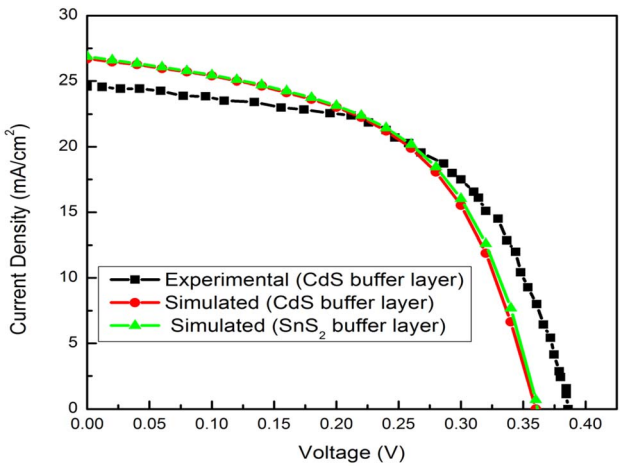

Fig. 2 Comparison of experimental and simulated *J*–*V* curves of Sb_2Se_3-based solar cells.

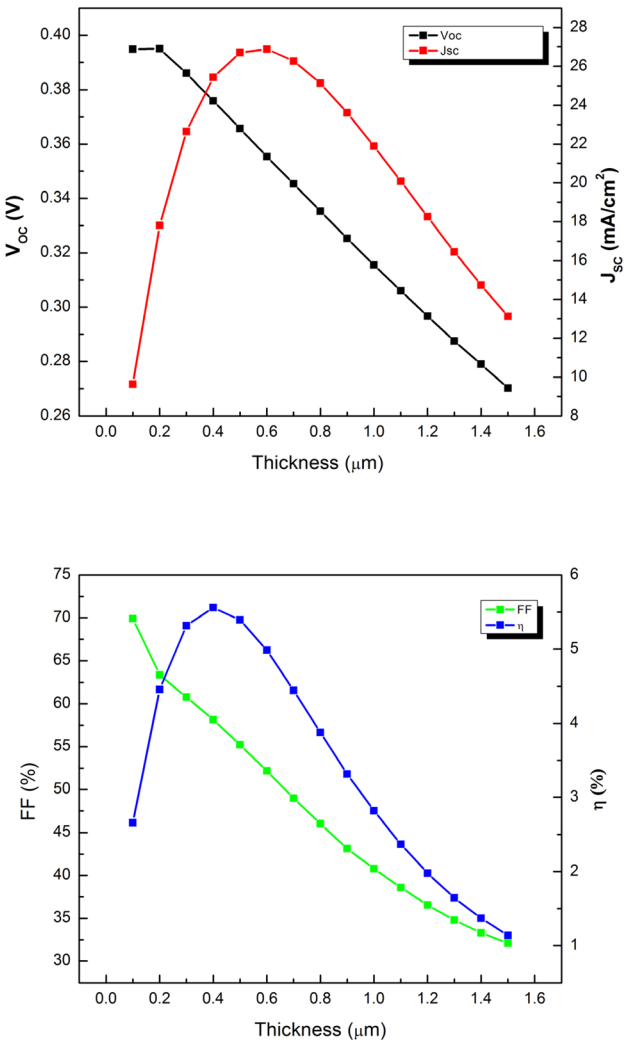

Fig. 3 Impact of Sb_2Se_3 absorber layer thickness on solar cell electrical parameters.

Table 4 Comparison of electrical parameters of Sb_2Se_3-based photovoltaic

Solar cell	V_{OC} (V)	J_{SC} (mA cm^{-2})	FF (%)	η (%)
Experimental[73]	0.386	24.6	54.5	5.17
Simulated[20]	0.362	27.51	51.95	5.17
Simulated (this work) (CdS buffer layer)	0.358	26.71	54.05	5.17
Simulated (this work) (SnS_2 buffer layer)	0.362	26.89	54.02	5.25

Step 14: the acceptor concentration of SnS layer is investigated in the range of 10^{15}–10^{20} cm^{-3} to study its impact on device output.

Step 15: to optimize defect density in SnS BSF layer, defect density is investigated in the range of 10^{10}–10^{20} cm^{-3} in this last step.

Finally, the effect of back contact work function (4.5–5.4 eV), temperature (300–400 K), series resistance (0–8 Ω cm^2) and shunt resistance (200–1600 Ω cm^2) on the optimized cell is explored.

3. Results and analysis

3.1 Validation and comparison of simulation model

The reproduced, experimental and proposed current density–voltage characteristics of the Sb_2Se_3 based photovoltaic are compared, as depicted in Fig. 2. Table 4 displays the obtained performance parameters of simulation results in consideration with experimental outcomes. The device outputs including V_{OC} of 0.358 V, J_{SC} of 26.71 mA cm^{-2}, FF 54.05%, and efficiency of 5.17% are achieved from the simulated *J–V* characteristics with CdS buffer layer by neglecting series and shunt resistances. On the contrary, the efficiency of 5.17% with V_{OC} of 0.386 V, J_{SC} of 24.6 mA cm^{-2}, and FF 54.5% is found for the experimental Sb_2Se_3 based photovoltaic.[73] The approximately same result obtained from the experimental and simulation works validates this simulation model. To limit extreme illumination instability due to the diffusion of Cd^{2+} from the buffer layer and toxicity of CdS buffer layer, non-toxic SnS_2 is used as a buffer layer in this simulation work.[73] An efficiency of 5.25% with V_{OC} of 0.362 V, J_{SC} of 26.89 mA cm^{-2}, and FF 53.99% is obtained for the proposed Sb_2Se_3 based photovoltaic with SnS_2 as a buffer layer. The result indicates that SnS_2 can be used as a novel buffer layer for Sb_2Se_3 based reference solar cell instead of toxic CdS buffer

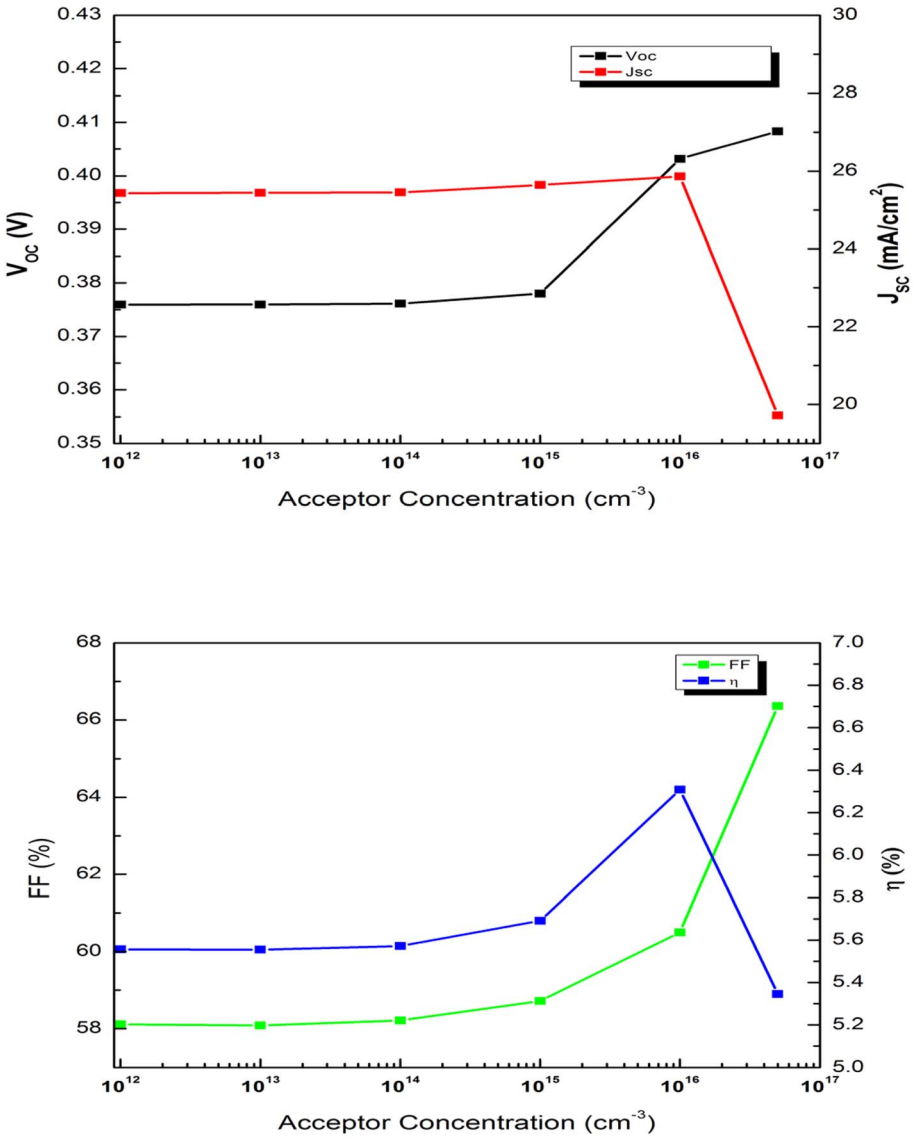

Fig. 4 Impact of Sb_2Se_3 absorber layer acceptor concentration on device performance.

layer as it provides better efficiency. As a result, SnS_2 is used as a buffer layer for Sb_2Se_3 based reference photovoltaic in this simulation study.

3.2 Impact of Sb_2Se_3 absorber layer thickness

An optimal absorber layer thickness ensures that photo-generated electron–hole pairs reach their respective contacts without recombination. The influence of the Sb_2Se_3 absorber layer thickness is examined by tuning absorber layer thickness from 0.1–1.5 μm, while different layers material parameters are kept unchanged. Solar cell output corresponding to absorber layer thickness variation are shown in Fig. 3. It is observed that J_{SC} increases from 9.63 mA cm^{-2} to 26.88 mA cm^{-2} as absorber layer thickness is increased from 0.1–0.6 μm due to increase in electron–hole pair generation. Afterwards it starts decreasing due to recombination and reaches 13.13 mA cm^{-2} as absorber layer thickness is enhanced to 1.5 μm. V_{OC} remains almost constant at 0.395 V as absorber layer thickness is enhanced from 0.1–0.2 μm. Then, it starts decreasing due to recombination and reaches 0.27 V as absorber layer thickness is enhanced to 1.5 μm.[87,88] FF decreases from 69.9–32.1% because of rise in series resistance as absorber layer thickness is increased from 0.1–1.5 μm. The combined impact of FF, V_{OC} and J_{SC} cause efficiency to rise from 2.66–5.56% as absorber layer thickness is increased from 0.1–0.4 μm. Then efficiency starts to decline as absorber layer thickness is increased and reaches 1.14% as absorber layer thickness is enhanced to 1.5 μm. A thin absorber layer results in low both J_{SC} and efficiency due to reduction of absorption capacity of light. Enhancement of absorber layer

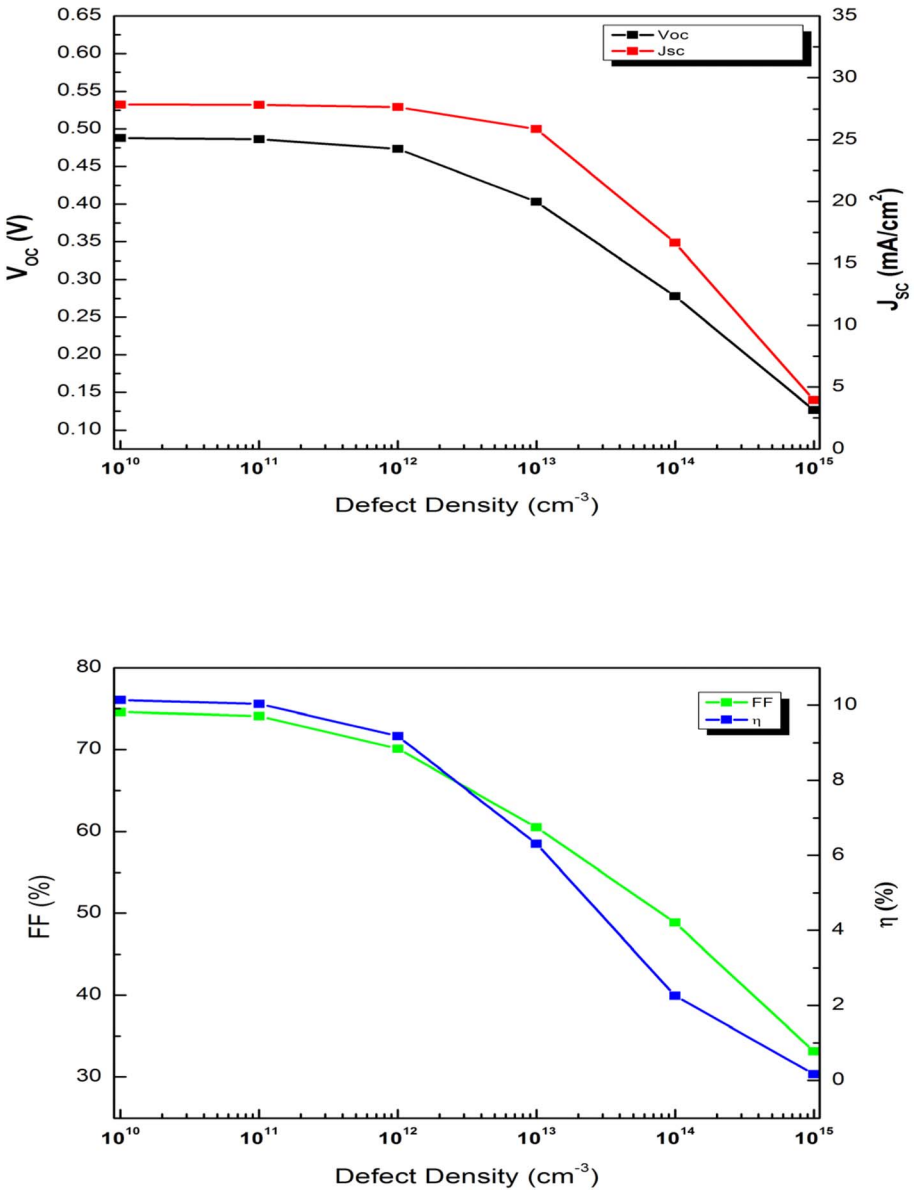

Fig. 5 Impact of Sb_2Se_3 absorber layer defect density on solar cell output.

thickness increases efficiency of the solar cell due to large number of photons being absorbed and rise in carrier generation.[14] Efficiency declines as absorber layer thickness is enhanced above 0.4 μm due to recombination as the path length covered by photo-generated carriers become very large.[89] So absorber layer thickness is optimized at 0.4 μm which falls within range published in previous works.[12,34]

3.3 Influence of Sb_2Se_3 absorber layer carrier density

The effect of the Sb_2Se_3 absorber layer carrier density on device output is examined and simulation outcomes are displayed in Fig. 4. The Sb_2Se_3 absorber layer acceptor density is tuned from 10^{12}–5×10^{16} cm^{-3}. V_{OC} increases from 0.38 V to 0.41 V and FF rises from 58.12–66.36% as absorber layer acceptor concentration is increased in considered range. J_{SC} increases slightly from 25.43 mA cm^{-2} to 25.86 mA cm^{-2} as doping density is tuned from 10^{12}–10^{16} cm^{-3} after which it starts decreasing. An enhanced doping density results in rise in the bulk and interface recombination rate, thereby declining J_{SC}.[54] The combined effect of V_{OC}, J_{SC} and FF causes efficiency to rise from 5.56–6.31% with increase in acceptor concentration from 10^{12}–10^{16} cm^{-3}. Afterwards, efficiency degrades. Increase in the carrier density creates the built-in potential at the interface which decreases the recombination and rises the efficiency up to a certain limit.[90] Additional hole recombination centers created at high doping density in the absorber due to increased acceptor impurity increase recombination and declines efficiency.[14] So the optimal absorber layer doping density chosen is 10^{16} cm^{-3} which is within doping concentration value used in previous works.[12,37]

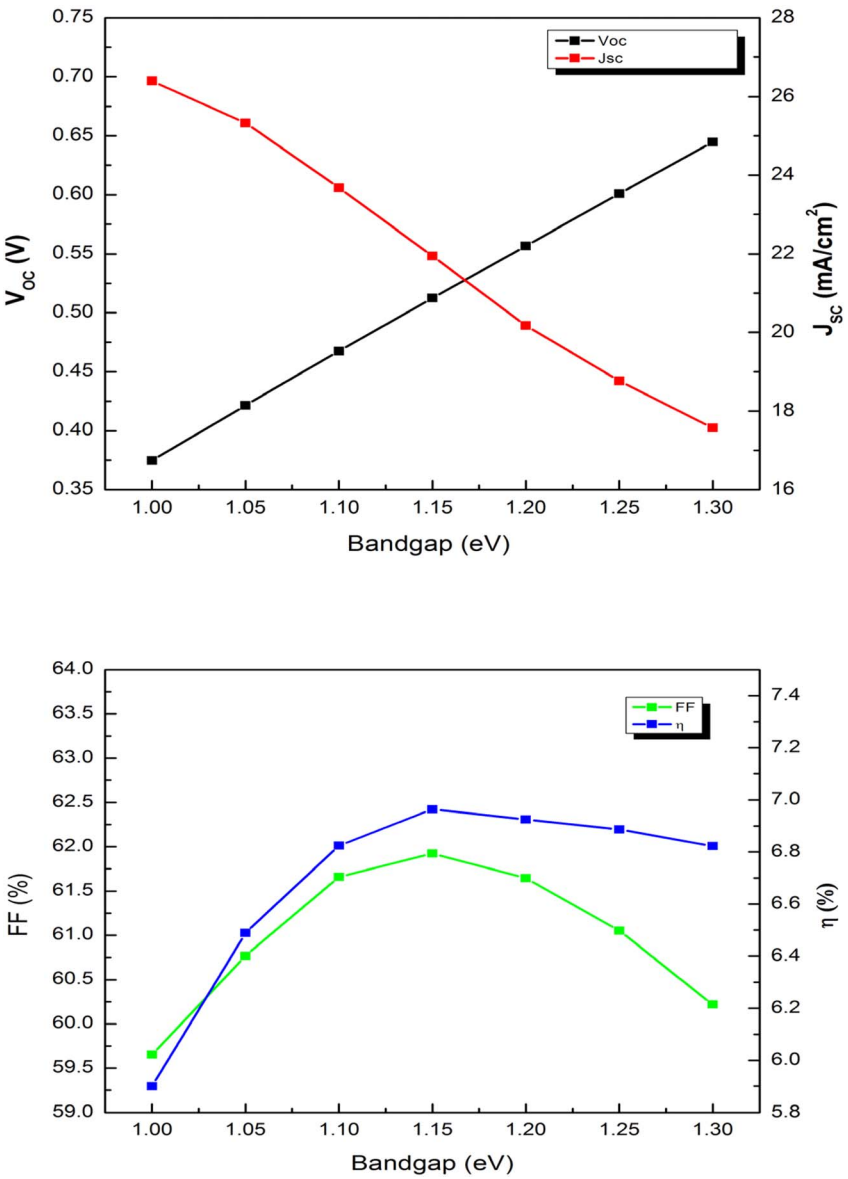

Fig. 6 Solar cell characteristics with respect to Sb_2Se_3 absorber layer bandgap.

3.4 Effect of Sb_2Se_3 absorber layer defect density

The defect density of the absorber layer which are inevitable during the fabrication plays a vital role in impacting the performance of solar cells. Defects in the absorber layer results from antisite defects, point defects, crystal imperfections and interstitials. The effect of the Sb_2Se_3 absorber layer defect density is examined and outcomes are depicted in Fig. 5. The Sb_2Se_3 absorber layer defect density is altered from 10^{10}–10^{15} cm^{-3}. Both V_{OC} and J_{SC} remain almost fixed up to defect density of 10^{12} cm^{-3}. Thereafter, both decline significantly as defect density is increased in considered range. FF and η remain unaltered as defect density is increased from 10^{10}–10^{11} cm^{-3}. Then both decrease significantly. It is observed that J_{SC}, V_{OC}, FF and η decrease from 27.86 mA cm^{-2} to 3.94 mA cm^{-2}, 0.49 V to 0.126 V, 74.58–33.13%, and 10.14–0.16% respectively as defect density is increased from 10^{10}–10^{15} cm^{-3}. Increase in absorber layer defect density causes increase in Shockley Read Hall (SRH) recombination of carriers which reduces the carrier lifetime and diffusion length.[14,91,92] As a result, the production of electron–hole is reduced due to prevention of the carriers from reaching the junctions which degrades the solar cell performance parameters.[93] The absorber layer defect density selected is 10^{13} cm^{-3} for maximum efficiency which is in good agreement with research works.[17,53]

3.5 Optimization of Sb_2Se_3 absorber layer bandgap

The effect of the Sb_2Se_3 absorber layer bandgap is examined by altering absorber layer bandgap from 1–1.3 eV. Solar cell output parameter changes corresponding to absorber layer bandgap variation are depicted in Fig. 6. It is observed that J_{SC} decreases from 26.4 mA cm^{-2} to 17.57 mA cm^{-2} as bandgap rises from 1 to 1.3 eV. V_{OC} increases from 0.375 V to 0.64 V with rise in bandgap in considered range due to decline in radiative recombination rate.[94] Both FF and η rise up to bandgap of 1.15 eV. Afterwards, both degrade with rise in bandgap. The generated rate of carriers is enhanced due to improved absorber/buffer junction which causes efficiency to increase as bandgap rises from 1 to 1.15 eV.[95] The mismatch between Sb_2Se_3 and SnS_2 bandgap creates recombination centers which increases carriers' recombination with further increase of Sb_2Se_3 bandgap above 1.15 eV and declines efficiency.[96] So the absorber layer bandgap is optimized at 1.15 eV at which η reaches 6.96%.

3.6 Effect of SnS_2 buffer layer thickness

The influence of SnS_2 buffer layer thickness on solar cell output parameters is also explored. The thickness is tuned from 0.01–0.1 μm. Fig. 7 displays the simulation findings obtained. It is observed that both V_{OC} and J_{SC} decrease and FF remains almost constant as buffer layer thickness is enhanced in considered range. The photo-generated carriers need to travel longer distance to go to the active region with the rise in the thickness of buffer layer which increases the recombination rate which in turn decreases both J_{SC} and V_{OC}.[97] The efficiency decreases from 7.34–6.6% as buffer layer thickness is varied from 0.01–0.1 μm.

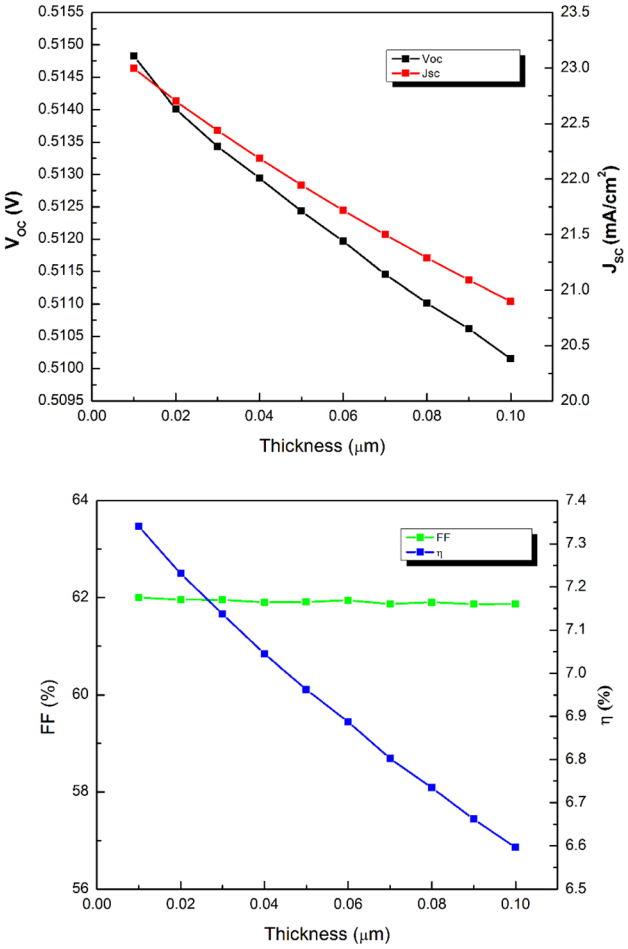

Fig. 7 Impact of SnS_2 buffer layer thickness on cell performance parameters.

Less number of photons reach the Sb_2Se_3 layer which led to reduction of the production of electron–hole pair with increase in the thickness of SnS_2 layer due to the increase in absorption of photons in the buffer layer which declines efficiency.[93] When the SnS_2 layer is very thin, the space charge width of the junction is decreased and the pinholes might be created so that Sb_2Se_3 directly connects to the front contact.[20] So the optimal buffer layer thickness chosen is 0.03 μm which is also used in published researches.[98,99]

3.7 Influence of SnS_2 buffer layer donor density

The effect of the SnS_2 buffer layer donor concentration is examined and simulation findings are displayed in Fig. 8. The SnS_2 buffer layer donor density is altered from 10^{13}–10^{18} cm^{-3}. FF declines as donor density is enhanced in considered range. V_{OC} and J_{SC} increase from 0.45 V to 0.51 V and 15.36 mA cm^{-2} to 22.44 mA cm^{-2} respectively which causes η to rise from 5.86–7.14% as buffer layer carrier density is enhanced from 10^{13}–10^{18} cm^{-3}. At low carrier concentration, the depletion region extends out of the buffer layer thickness and the diode behavior of the device is decreased.[48] The electric field on the Sb_2Se_3/SnS_2

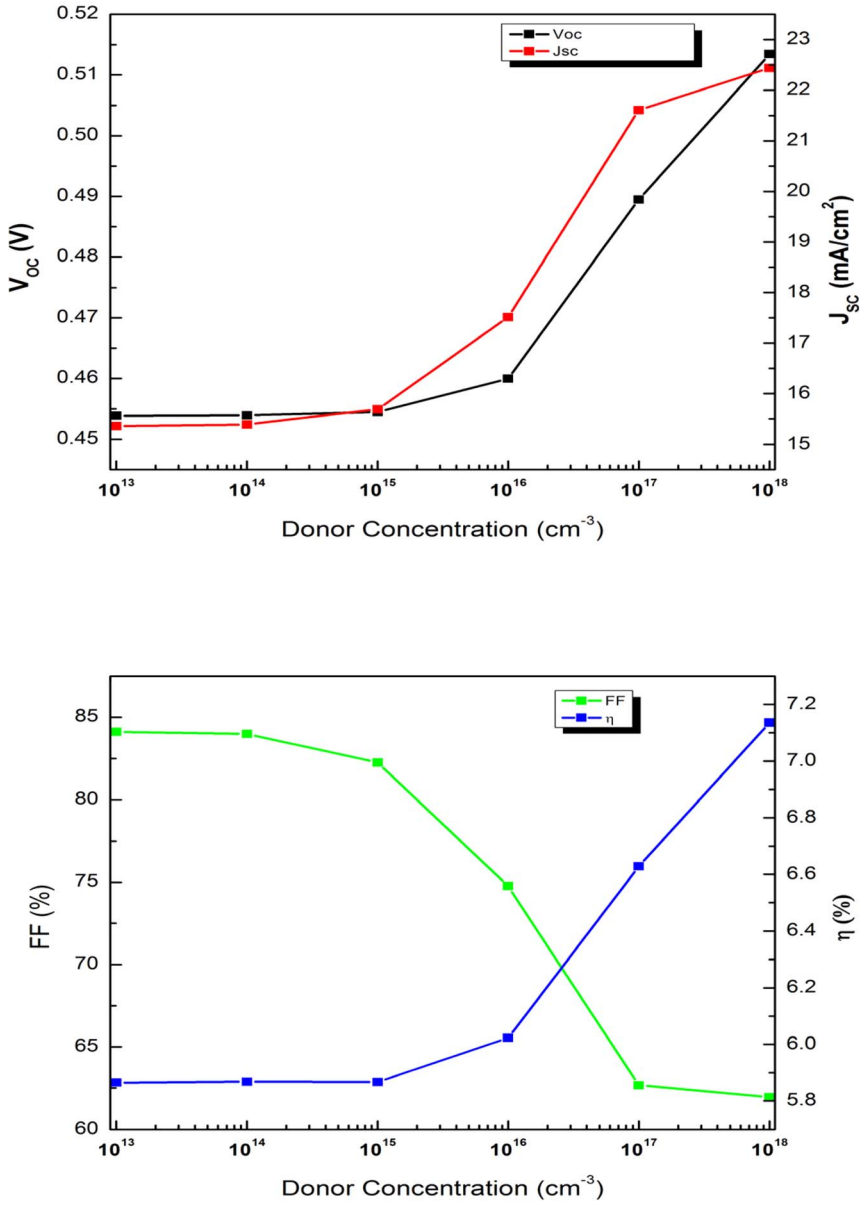

Fig. 8 Photovoltaic output as a function of SnS_2 buffer layer donor concentration.

junction and the SnS_2//FTO junction rise which augments the separation of the photo-generated charges and efficiency with rise in buffer layer doping concentration.[100] So the buffer layer donor density is optimized at 10^{18} cm^{-3} which is compatible with published work.[48]

3.8 Effect of SnS_2 buffer layer defect density

To examine the influence of SnS_2 buffer layer defect density on photovoltaic characteristics, the defect density is altered from 10^{10}–10^{18} cm^{-3} and photovoltaic output changes obtained are displayed in Fig. 9. All the electrical parameters remain almost constant up to defect density of 10^{17} cm^{-3}. Thereafter, all parameters start to degrade drastically. FF starts increasing particularly at 10^{17} cm^{-3} because of rise in energy barrier height.[93,101] The efficiency decreases from 7.12–5.87% as defect density is increased from 10^{17}–10^{18} cm^{-3}. The enhanced defect density reduces the carriers' diffusion length and life time and as a result, efficiency decreases as photo-generated carriers find it hard to travel.[102] So buffer layer defect density of 10^{15} cm^{-3} is chosen as optimum value which matches with previous work.[12]

3.9 Effect of FTO window layer thickness

The influence of FTO window layer thickness on solar cell output is also simulated. The thickness is altered from 0.1–0.6 μm. Fig. 10 displays the simulation outcomes obtained. It is observed that both V_{OC} and J_{SC} decrease very slightly and FF

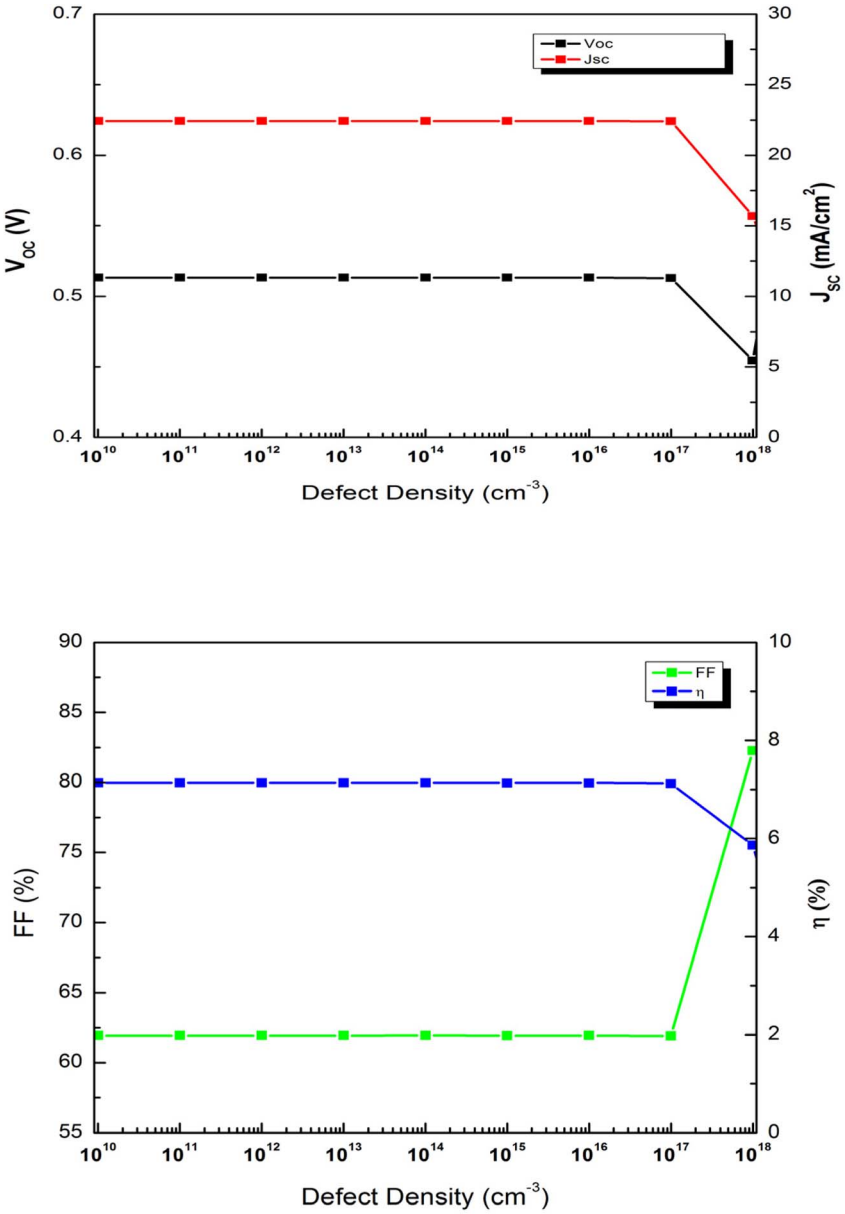

Fig. 9 Effect of SnS_2 buffer layer defect density on photovoltaic output.

remains almost constant as window layer thickness is enhanced within 0.1–0.6 μm. The efficiency decreases from 7.16–7.13% as window layer thickness is varied from 0.1–0.6 μm. As FTO layer thickness rises, the absorption of a large part of the light which incidents in the FTO layer declines transmission, which creates an optical loss and as a result degrades efficiency in the solar cell.[103] So the optimal window layer thickness chosen is 0.1 μm.

3.10 Influence of FTO window layer doping concentration

The effect of the FTO window layer donor concentration is examined and simulation results are outlined in Fig. 11. The FTO window layer doping concentration is tuned from 10^{17}–10^{20} cm^{-3}. V_{OC} remains constant and both FF and J_{SC} increase with increase in window layer donor concentration in considered range. Efficiency increases very slightly from 7.16–7.21% as window layer donor concentration is increased from 10^{17}–10^{20} cm^{-3}. It is concluded that the FTO layer doping density has insignificant effect on the performance of the proposed Sb_2Se_3 based solar cell when compared to the effect of the absorber and buffer layer. The photo-generated carries may be collected by electrodes efficiently with rise of FTO layer donor density and thus increases efficiency.[104] The optimal window layer donor density chosen is 10^{20} cm^{-3} which is compatible with research work.[105]

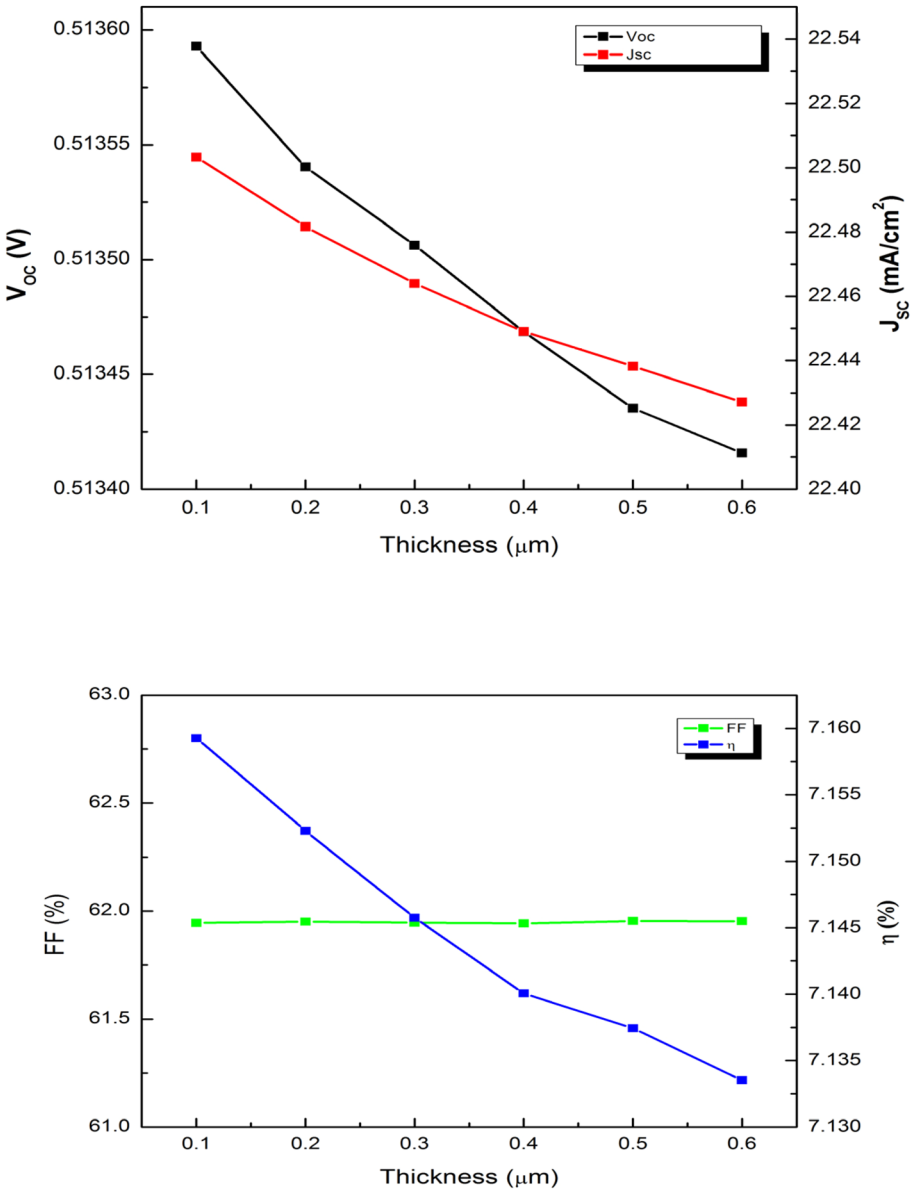

Fig. 10 Impact of FTO window layer thickness on cell output parameters.

3.11 Effect of Sb_2Se_3/SnS_2 interface defect density

Metallurgical discontinuities, lattice mismatch and symmetry breaking at the interfaces result in interface defects. Interface with low lattice mismatch results in low both interfacial defects and recombination rate and enhances performance parameters. The Sb_2Se_3/SnS_2 interface defect density is altered from 10^7 cm^{-2} to 10^{18} cm^{-2} to investigate its impact on device output. Simulation findings are depicted in Fig. 12. It is observed that all performance parameters decrease significantly as interface defect density is increased from 10^7 cm^{-2} to 10^{10} cm^{-2}. Afterwards, all performance parameters remain nearly constant. The V_{OC}, J_{SC}, FF and efficiency decreases from 0.52 V to 0.5135 V, 24.19 mA cm^{-2} to 22.52 mA cm^{-2}, 63.3–62.36% and 7.96–7.21% respectively as interface defect density is increased from 10^7–10^{18} cm^{-2}. Enhanced recombination centers at the Sb_2Se_3/SnS_2 interface due to increase in electron trap centers at high density of Sb_2Se_3/SnS_2 interface defects are responsible for the degradation of performance parameters.[106] The optimal Sb_2Se_3/SnS_2 interface defect density selected is 10^{10} cm^{-2} which is in good agreement with earlier research works.[107,108]

3.12 Effect of Sb_2Se_3 absorber layer capture cross section

The influence of the Sb_2Se_3 absorber layer capture cross section is investigated by altering the Sb_2Se_3 absorber layer electron and

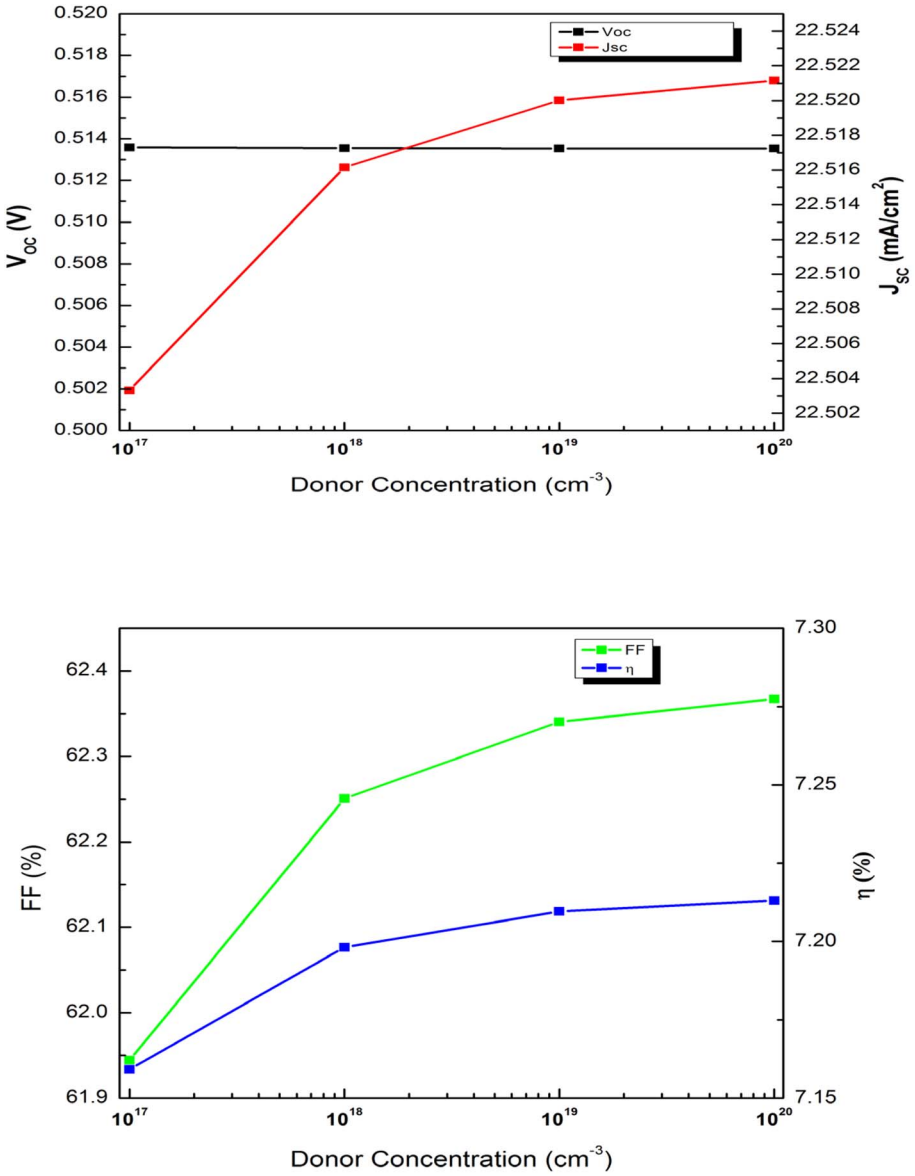

Fig. 11 Impact of FTO window layer donor density on device performance.

hole capture cross section from 10^{-19}–10^{-9} cm^{-2}. Simulation results are displayed in Fig. 13. It is observed that both V_{OC} and J_{SC} remain almost constant as capture cross section is enhanced from 10^{-19}–10^{-12} cm^{-2}. Then both decrease as capture cross section is increased in considered range. Both FF and η remain unaltered as capture cross section is enhanced from 10^{-19}–10^{-13} cm^{-2}. Afterwards, both decline as capture cross section is increased in considered range. Efficiency decreases from 10.23–1.24% as capture cross section is enhanced from 10^{-19}–10^{-9} cm^{-2}. Both carrier diffusion length and lifetime is declined because of large lattice mismatch and enhancement of recombination rate as capture cross-section of defect is increased which degrades device performance parameters.[109,110] The optimal Sb_2Se_3 absorber layer capture cross section selected is 10^{-15} cm^{-2} which matches with reported earlier work.[12]

3.13 The influence of Sb_2Se_3/SnS_2 interface capture cross-section

The Sb_2Se_3/SnS_2 interface capture cross section of electron and hole is tuned from 10^{-20}–10^{-8} cm^{-2} to examine its impact on

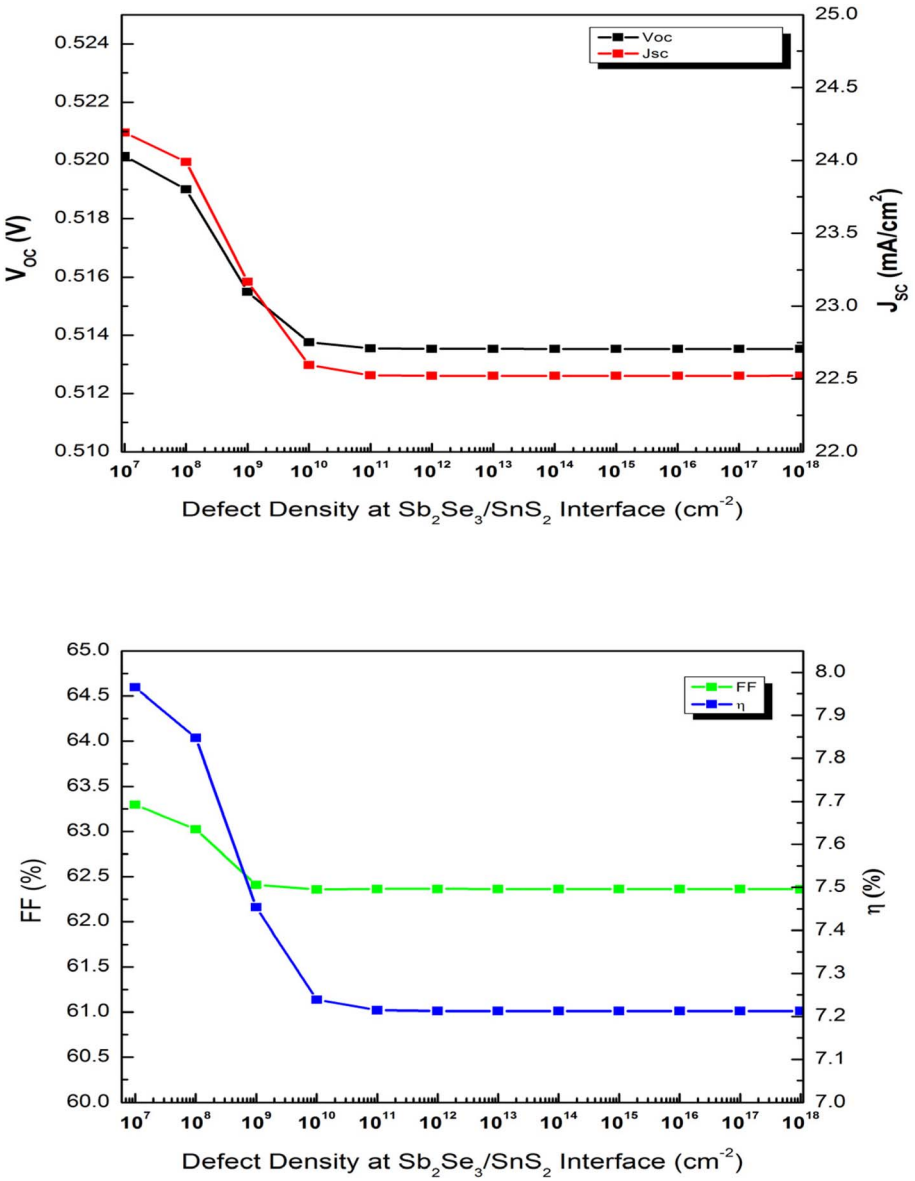

Fig. 12 Influence of Sb_2Se_3/SnS_2 interface defect density on cell output.

device output and simulation results are depicted in Fig. 14. It is observed that all performance parameters remain almost constant as capture cross section is enhanced from 10^{-20}–10^{-13} cm^{-2}. Then all parameters decline as capture cross section is increased in considered range. Efficiency decreases from 12.31–10.18% as capture cross section is enhanced from 10^{-20} cm^{-2} to 10^{-8} cm^{-2}. It is evident that interface capture cross-section has less effect on device output compared to absorber capture cross-section of carriers. Enhancement in capture cross-section of electron and hole results in degradation of the Sb_2Se_3/SnS_2 interface quality, enhancement in recombination and as a result, the efficiency declines.[111,112] The optimal Sb_2Se_3/SnS_2 interface capture cross section chosen is 10^{-19} cm^{-2} which is compatible with research work.[111]

3.14 Impact of SnS BSF layer thickness

The BSF layer allows easy transportation of holes and blocks the electrons to the back contact simultaneously. Thus BSF layer has a major role in solar cell performance. The effect of SnS BSF layer thickness on solar cell characteristics is also explored. The thickness is varied from 0.02–0.2 μm. Device performance changes with respect to SnS thickness variation are displayed in

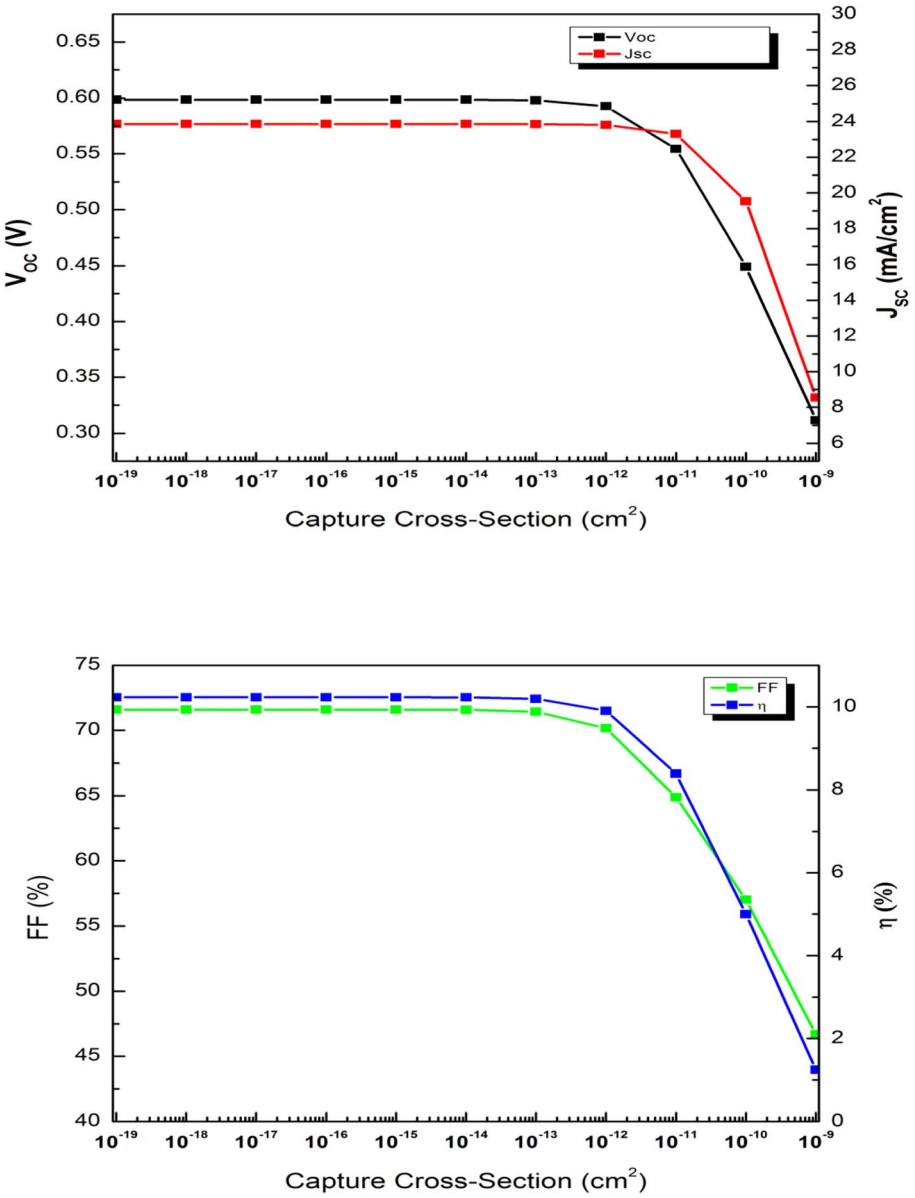

Fig. 13 Effect of Sb_2Se_3 absorber layer capture cross-section on device electrical parameters.

Fig. 15. The acceptor concentration and defect density of BSF layer is maintained fixed at 10^{18} cm^{-3} and 10^{14} cm^{-3} respectively. It is observed that the thickness of SnS shows significant effect on the solar cell performance parameters. V_{OC},J_{SC}, FF and η increases from 0.7 V to 0.83 V, 26.76 mA cm^{-2} to 31.91 mA cm^{-2}, 80.97–85.96% and 15.12–22.87% as SnS BSF layer thickness is increased from 0.02–0.2 μm. The decrease of recombination rate of carriers with increasing BSF thickness improves both V_{OC} and J_{SC}.[105] The generation of carriers is increased with the rise in the thickness of BSF layer with the same amount of incident photon and thus improves efficiency.[91] To minimize production cost and the quantity of material used by the absorber layer, the optimal SnS BSF layer thickness chosen is 0.2 μm which matches with reported study.[98]

3.15 Influence of SnS BSF layer acceptor concentration

The effect of the SnS BSF layer acceptor density is examined and simulation outcomes are represented in Fig. 16. The SnS BSF layer doping concentration is tuned from 10^{15}–10^{20} cm^{-3}. All electrical parameters except FF enhance with rise in SnS BSF

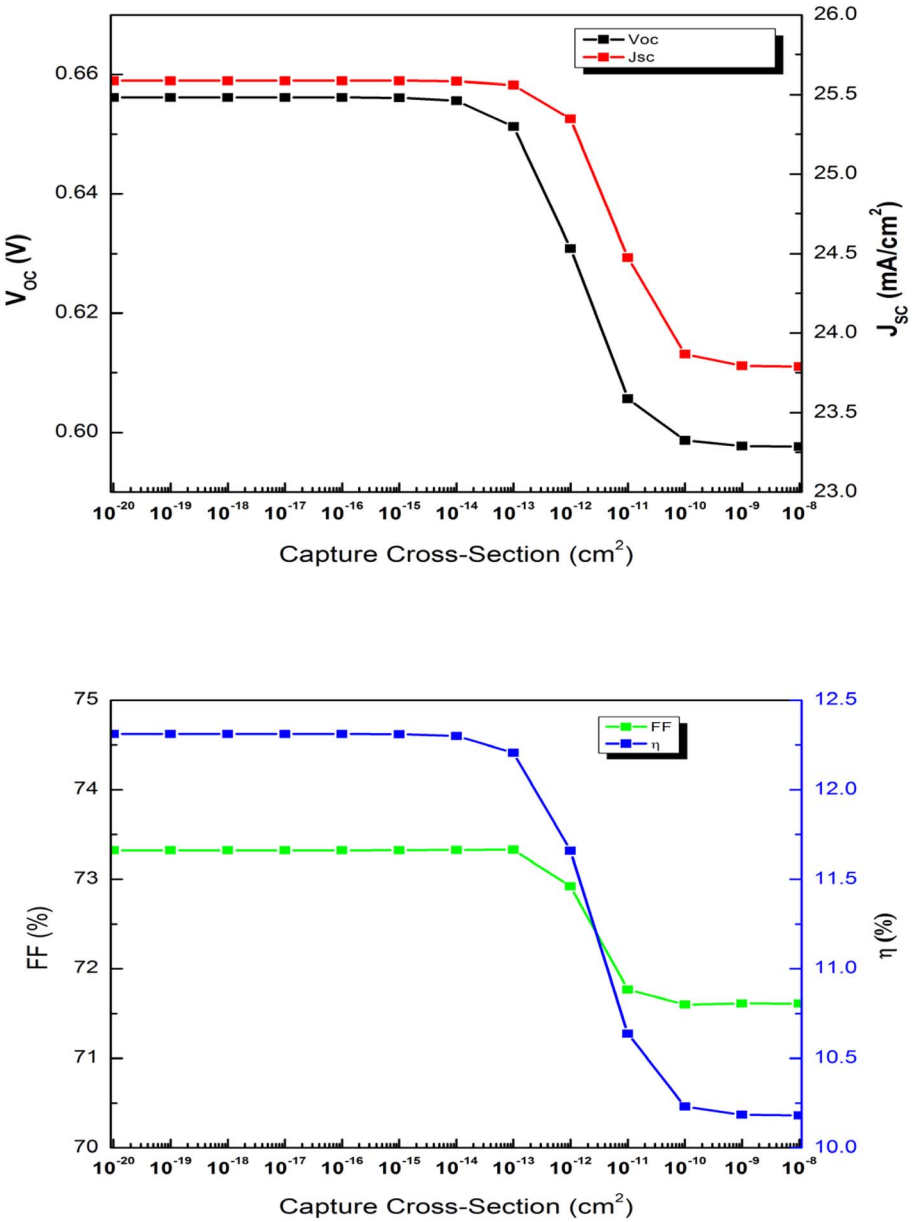

Fig. 14 Solar cell characteristics as a function of Sb_2Se_3/SnS_2 interface capture cross-section.

layer carrier density from 10^{15}–10^{20} cm^{-3}. FF increases from 72.65–85.96% as SnS BSF layer acceptor concentration is enhanced from 10^{15}–10^{18} cm^{-3} due to decrease in series resistance. Afterwards, FF decline due to increase of recombination at high doping. V_{OC}, J_{SC} and efficiency increases from 0.66 V to 0.94 V, 26.6 mA cm^{-2} to 31.98 mA cm^{-2} and 12.74–24.86% as doping density of BSF layer is increased from 10^{15}–10^{20} cm^{-3}. The large potential created at the SnS/Sb_2Se_3 interface reduces recombination rate of carriers at high carrier density of BSF layer. Ohmic contact is created with the back contact due to closeness of BSF Fermi level with the valence band (VB) at high BSF doping density which supports easy transportation of holes towards back electrode and enhances device performance.[113] The optimal BSF layer acceptor density chosen is 10^{20} cm^{-3}. The result is within range of earlier simulation studies.[37,114]

3.16 Effect of SnS BSF layer defect density

The SnS BSF layer defect density is varied from 10^{10}–10^{20} cm^{-3} to examine its impact on device electrical parameters and simulation outcomes are displayed in Fig. 17. The efficiency is

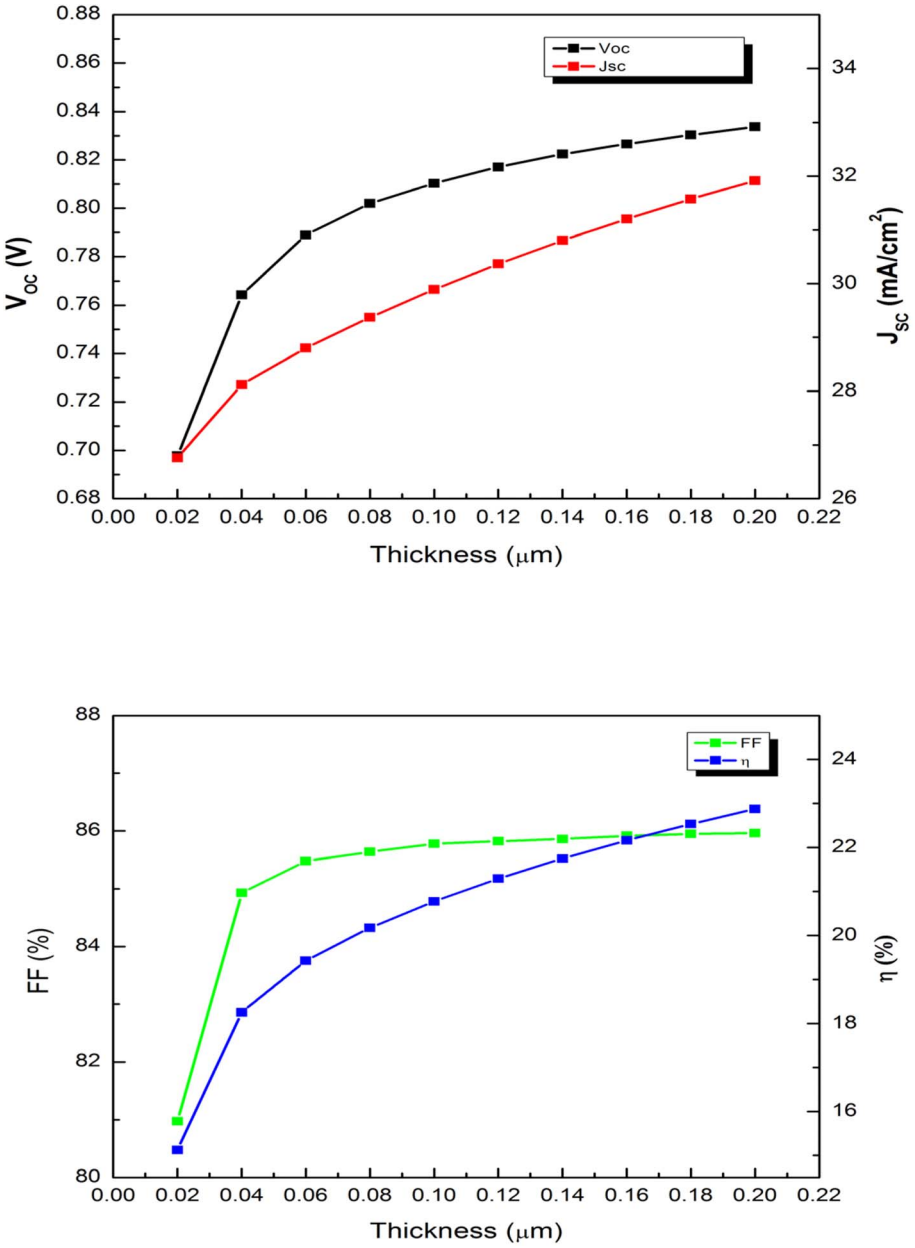

Fig. 15 Effect of SnS BSF layer thickness on device characteristics.

nearly fixed till defect density of 10^{17} cm^{-3}. Afterwards, efficiency starts to degrade. The efficiency declines from 24.86–12.79% as defect density is enhanced from 10^{10}–10^{20} cm^{-3} due to increase in recombination. The sudden rise in FF from defect density 10^{17}–10^{19} cm^{-3} is due to increase in energy barrier height.[93,101] The optimal BSF layer defect density selected is 10^{14} cm^{-3} which matches with earlier study.[114]

3.17 Impact of back contact work function

The back contact work function majorly impacts the efficiency of the solar cell. A high work function back contact is needed for a proper ohmic contact at the absorber or BSF/back contact interface. To explore the influence of back contact on photovoltaic output, back contact work function is tuned from 4.5–5.4 eV and simulation outcomes obtained are represented in Fig. 18. J_{SC} increases by a small margin as work function is enhanced within 4.5–5.4 eV. Both V_{OC} and FF enhance prior to work function of 5 eV and thereafter stay almost saturated. The combined increase of V_{OC} and FF enhances the efficiency till work function of 5 eV and then remain saturated. With rise in work function of the back electrode, the carriers' barrier height at the back surface decreases which enhances device

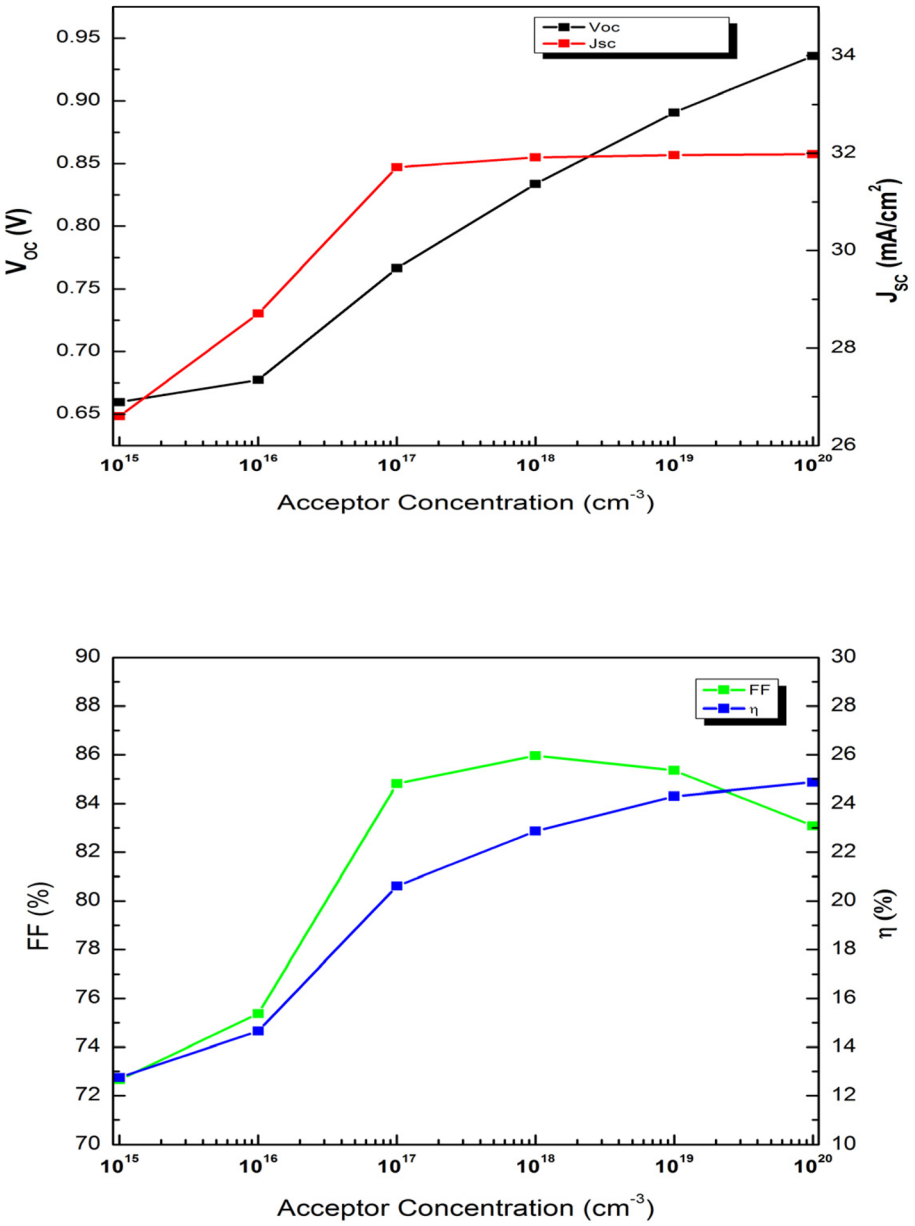

Fig. 16 Impact of SnS BSF layer acceptor density on photovoltaic output.

performance.[14] So for maximum efficiency of proposed solar cell, back electrode work function is required to be larger or equal to 5 eV.

3.18 Impact of temperature

Long-term stability under ambient air condition is a major requirement for the application of photovoltaic device. The influence of the working temperature on solar cell is investigated in a range of 300–400 K and the simulation outcomes are depicted in Fig. 19. J_{SC} increases slightly due to reduction of the bandgap of the absorber which rises the generation of carrier in solar cell as temperature is increased in considered range.[115] The rise of temperature makes thermally generated electrons unstable due to vibration and recombine with the holes before being collected at the electrodes, reducing V_{OC} linearly. Moreover, the rise in temperature impacts the carrier properties such as mobility and carrier density and as a result, declines the FF of device.[116] The combined decrease in V_{OC} and FF declines efficiency from 24.86–20.37% as temperature is enhanced from 300–400 K.

3.19 Influence of parasitic resistance

Series resistance (R_S) and shunt resistance (R_{Sh}) have a vital effect on photovoltaic output. The solar cell performs best at

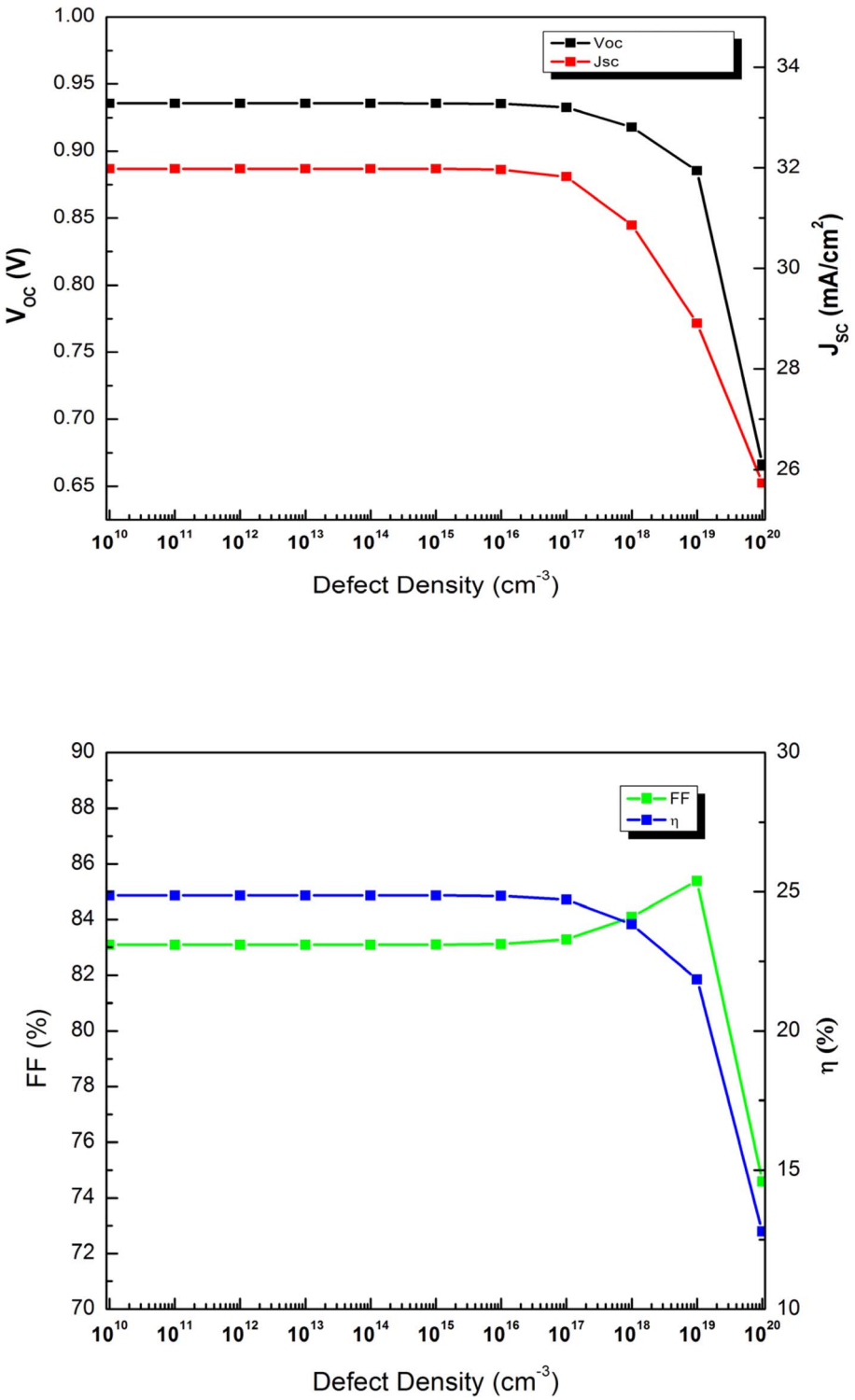

Fig. 17 Influence of SnS BSF layer defect density on cell output parameters.

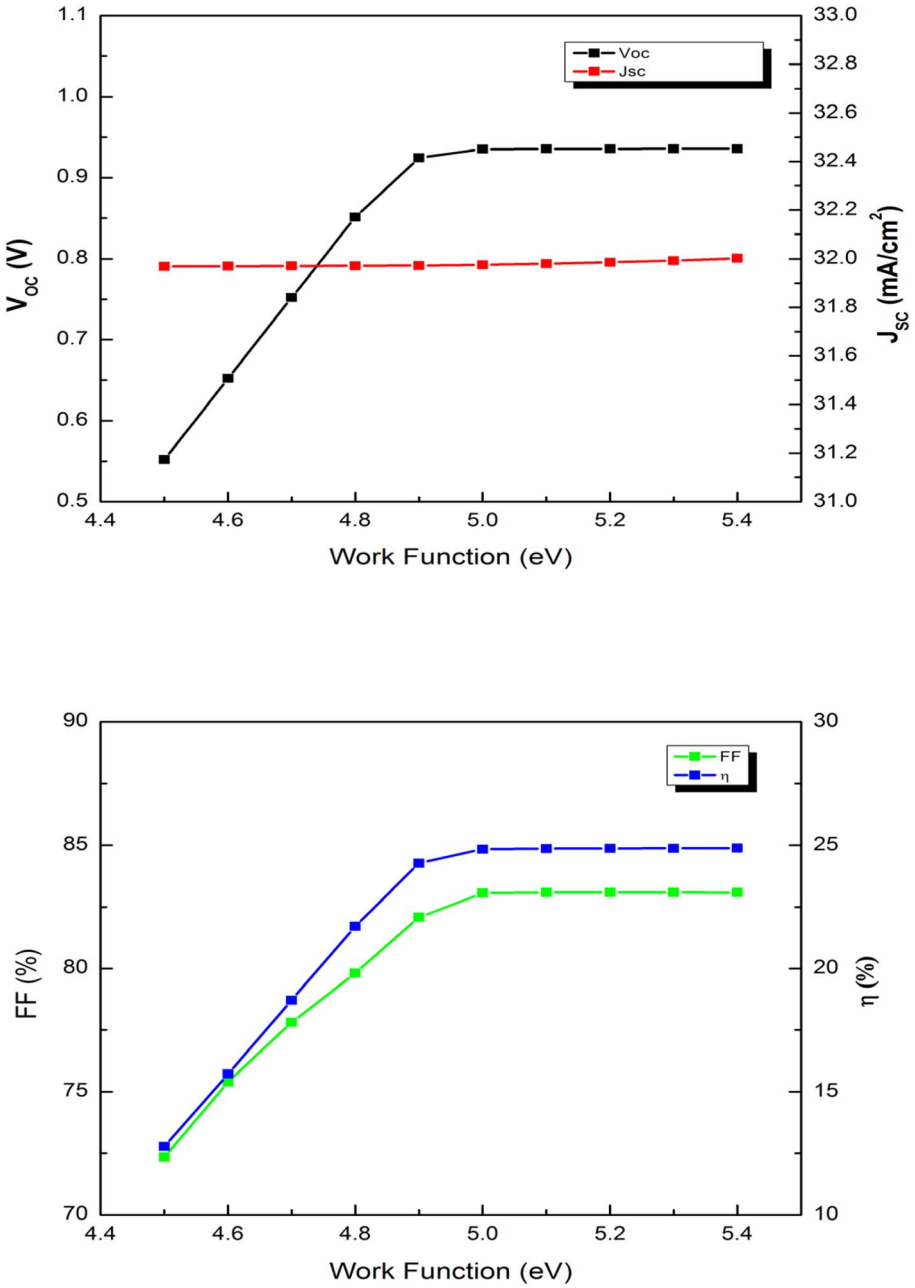

Fig. 18 Impact of back contact work function on device performance with BSF layer.

maximum R_{Sh} and minimum R_s values. R_S is the sum of resistance between different layers of solar cells and at the back and front contacts.[117] When the current created by sunlight flows through the various channels produced by small R_{Sh}, efficiency degrades.[14]

The Sb_2Se_3 solar cell performance parameters with SnS BSF layer is investigated by varying the R_S from 0 to 8 Ω cm^2. The obtained results are shown in Fig. 20. It is observed that V_{OC} remains constant and J_{SC} decreases slightly with rise of series resistance. J_{SC} decreases because of rise in internal resistance which impedes the transport of carriers to the contacts.[118] FF decreases significantly from 83.09–59.1% with increase of series resistance in considered range. As a result, efficiency decreases from 24.86–17.68% for optimized FTO/SnS_2/Sb_2Se_3/SnS/Au solar cell as R_S is increased from 0 to 8 Ω cm^2. R_s should be kept as low as possible to achieve high efficiency.

The R_{Sh} is changed from 200 Ω cm^2 to 1600 Ω cm^2 to investigate its effect on the cell output with SnS BSF layer and

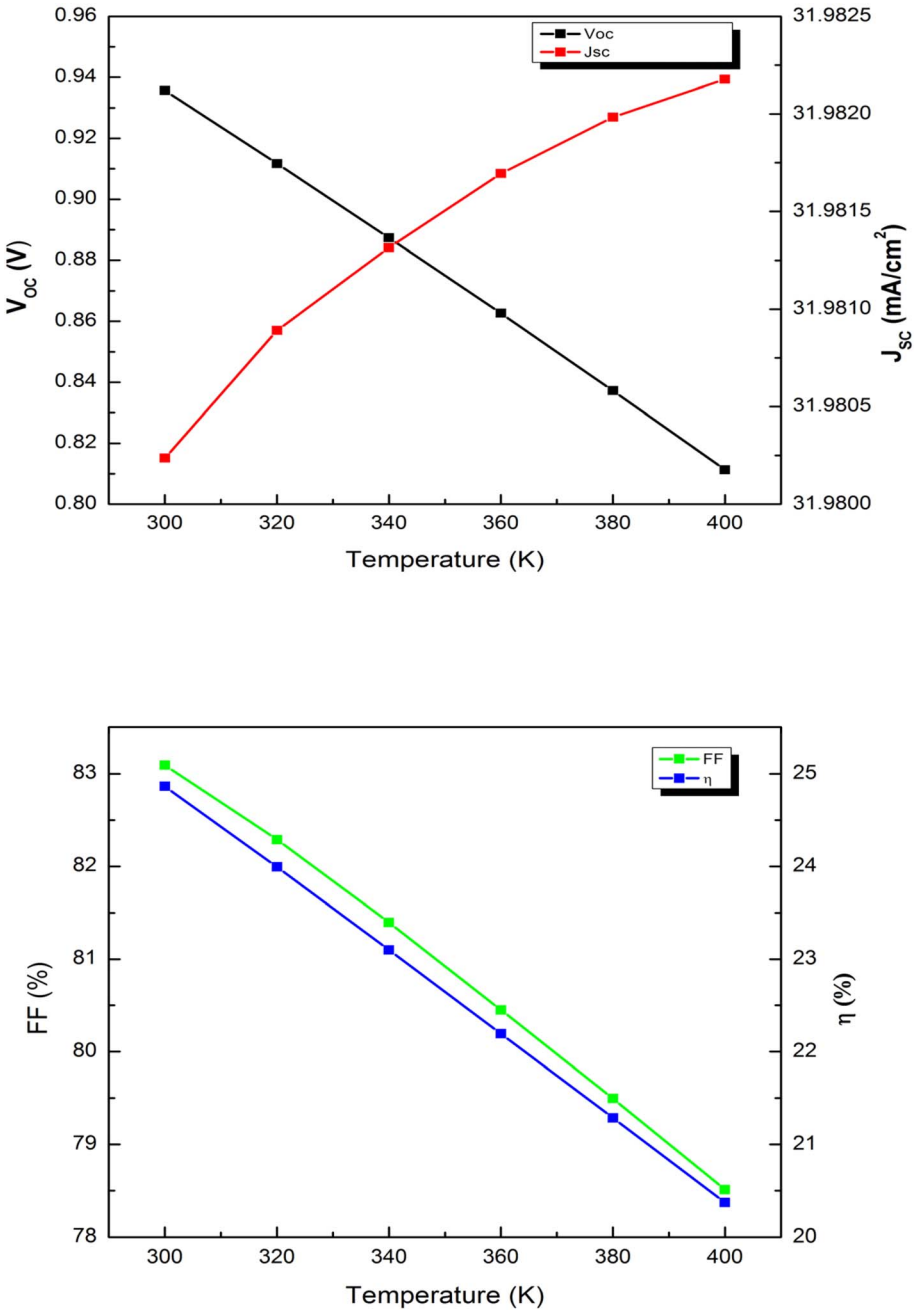

Fig. 19 Solar cell output variation with changes in temperature with BSF layer.

findings are shown in Fig. 21. J_{SC} is found to be unaltered, V_{OC} increases slightly and FF rises significantly with increase of shunt resistance in considered range. Efficiency rises from 21.6–24.45% as shunt resistance is increased from 200–1600 Ω cm^2 for proposed Sb_2Se_3 solar cell with SnS BSF layer mainly due to rise of FF. FF increases with increase in R_{Sh} because of low recombination rates.[119] It is observed that both FF and efficiency rise with increase in the R_{Sh} till 1200 Ω cm^2 and almost saturate on further increase in R_{Sh}. As a result, R_{Sh} should be high to achieve high efficiency.

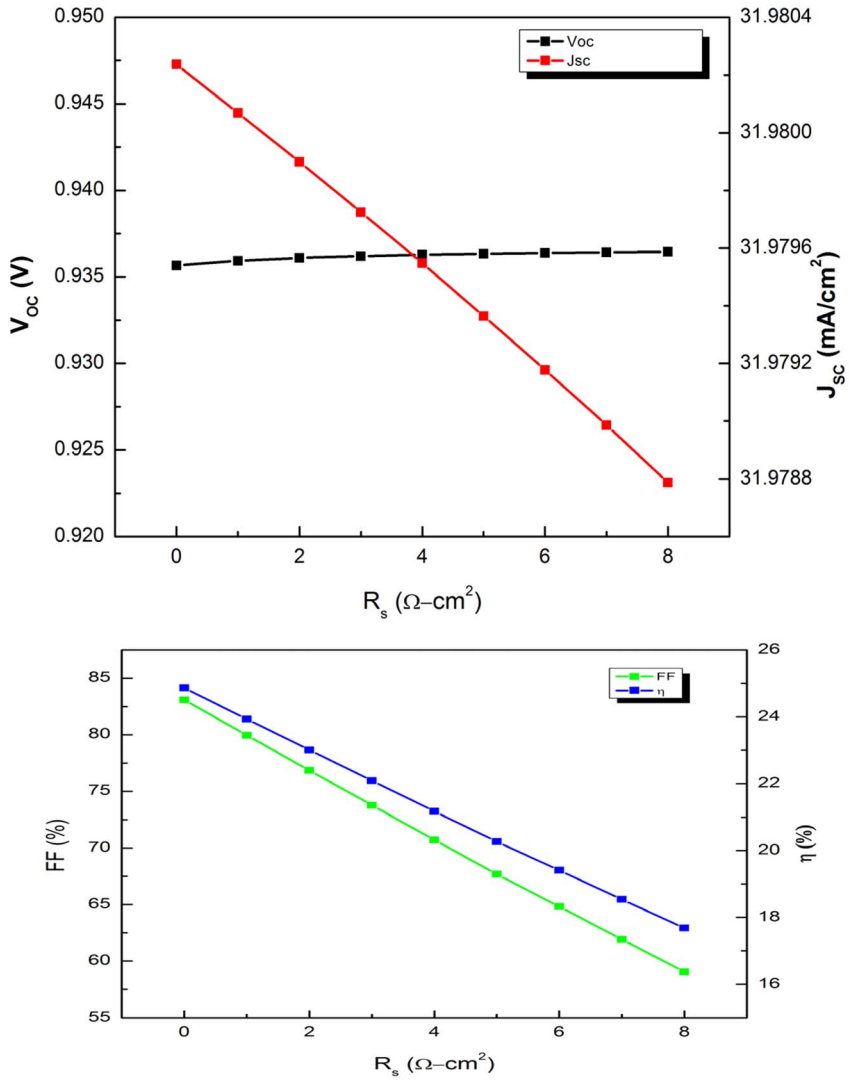

Fig. 20 Effect of series resistance (R_S) on cell output parameters with BSF layer.

3.20 Overall cell performance

The influence of inserting highly doped p-type SnS BSF layer of Sb_2Se_3 based solar cell on the current density–voltage (J–V) is depicted in Fig. 22. The electrical parameters of Sb_2Se_3 based solar cell without and with SnS BSF layer are summarized in Table 5. The optimum parameters of different layers of FTO/SnS_2/Sb_2Se_3/SnS/Au solar cell are illustrated in Table 6. The optimized FTO/SnS_2/Sb_2Se_3/Au solar cell structure obtains V_{OC}, J_{SC}, FF and η of 0.66 V, 25.59 mA cm^{-2}, 73.33% and 12.31% respectively. The insertion of SnS BSF layer enhances V_{OC}, J_{SC}, FF and η to 0.94 V, 31.98 mA cm^{-2}, 83.09% and 24.86% respectively. It is noticed that all electrical parameters are enhanced due to addition of SnS BSF layer. The creation of large built-in potential at the Sb_2Se_3/SnS interface rises the value of V_{OC}.[120] The efficient separation and collection of carriers due to the addition of BSF layer enhances the value of J_{SC}.[121] The improvement of FF is due to rise in the maximum power produced by FTO/SnS_2/Sb_2Se_3/SnS/Au solar cell structure due to reduction of recombination rate at back surface due to the insertion of SnS BSF layer.[122] The efficiency has significantly enhanced due to the insertion of SnS BSF layer because of combined increment of V_{OC}, J_{SC} and FF.

The quantum efficiency (QE) curve for Sb_2Se_3 based solar cell at initial and with optimization with and without SnS BSF layer is displayed in Fig. 23. The strong back surface electric fields at the SnS/Sb_2Se_3 interface due to addition of SnS BSF layer in the simulated cell structure decreases carrier recombination and increases the absorption at the wavelength range from 400 to 1030 nm, which increases the electrical parameters of the

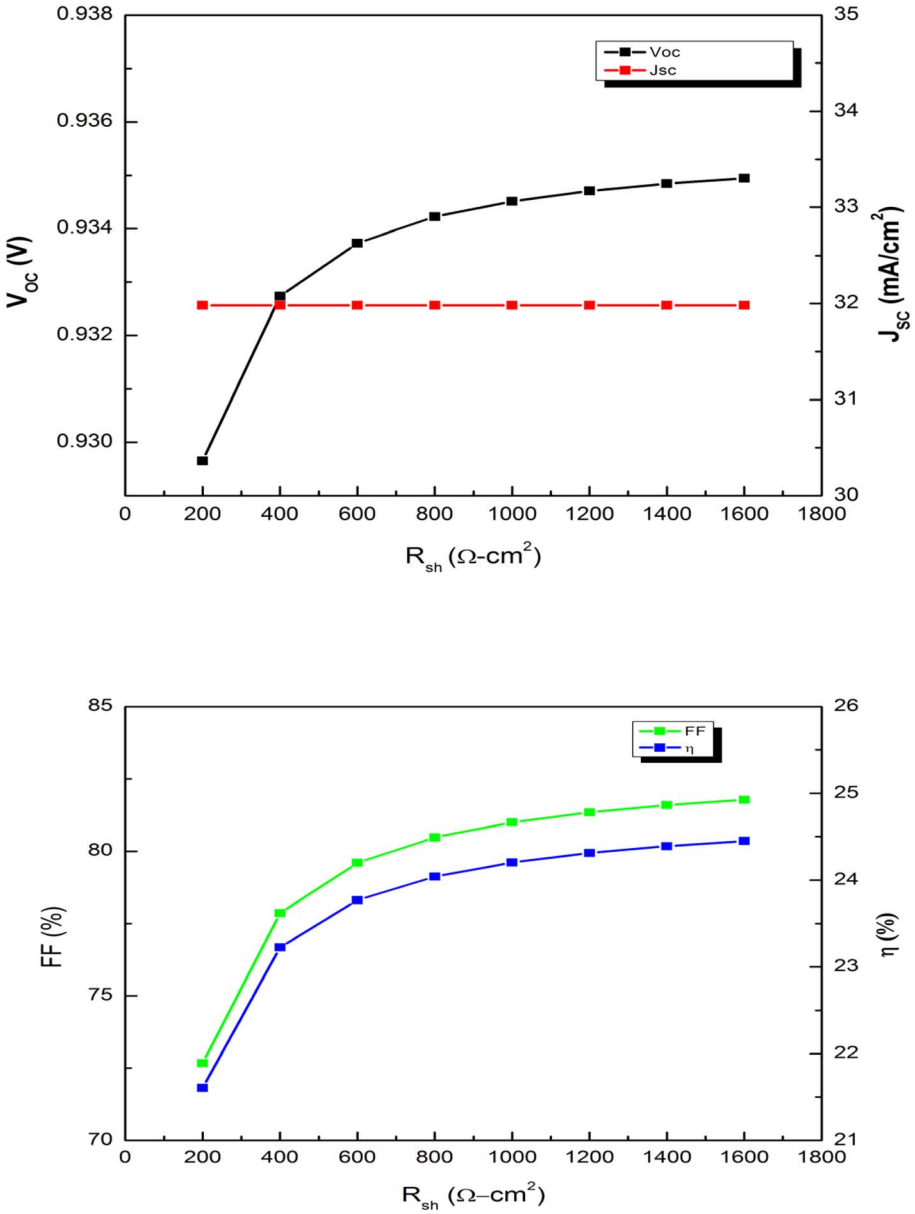

Fig. 21 Impact of shunt resistance (R_{Sh}) on solar cell characteristics with BSF layer.

designed photovoltaic. This results prove that SnS can be a potential BSF layer for improving the efficiency of Sb_2Se_3-based photovoltaic.

In this research, a promising efficiency of 24.86% was obtained by incorporating SnS as a BSF layer due to *n*-SnS_2/p-Sb_2Se_3/p$^+$-SnS forming of *n*–p–p$^+$ double heterojunction cell. This double junction cell efficiency improvement can be demonstrated by Tail-States-Assisted (TSA) two-steps photon upconversion process. In this double heterostructure, with the insertion of SnS BSF layer, the sub-bandgap photons may get absorbed notably, specifically in the longer wavelength, which causes an enhancement in solar cell performance. The sub-bandgap photons may be absorbed by the Urbach energy states and these lower energy sub-bandgap photons participate in tail-state-assisted (TSA) two-steps photon upconversion.[107,123,124] These absorbed photons generate additional electron–hole pairs, resulting in a noticeable improvement in cell photocurrent. A photoactive material such as SnS BSF layer can cause this TSA upconversion effectively when it possesses favorable bandgap, high absorption coefficient and adequate doping concentration.[105,125] Thus, it is believed that this is the main reason of the high-efficiency of 24.86% observed in proposed double heterojunction solar cell. The Urbach energy, E_0, of the photoactive material determines the resulting increase in photocurrent and the degree of upconversion. The higher Urbach energy remarkably promotes to boosting the quantum efficiency (QE), specifically in the longer wavelength.[5,126]

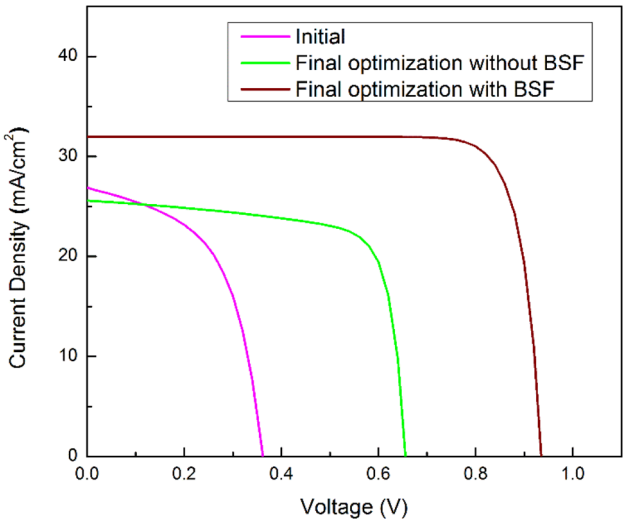

Fig. 22 J–V characteristic curve of Sb_2Se_3 based photovoltaic with and without SnS BSF layer.

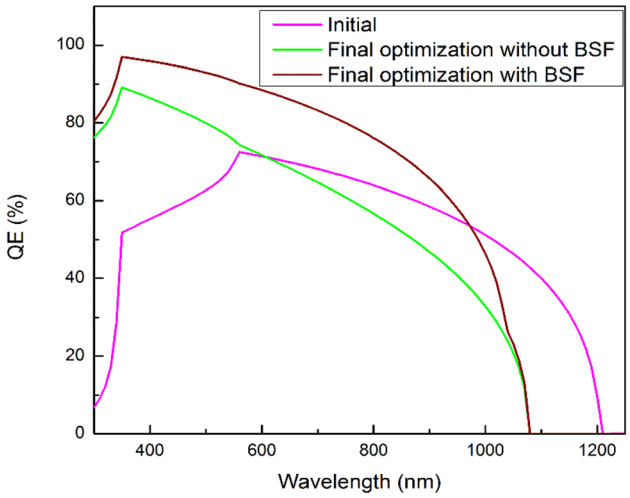

Fig. 23 QE characteristic curve of Sb_2Se_3 based photovoltaic with and without SnS BSF layer.

Table 5 Performance parameters of the proposed FTO/SnS_2/Sb_2Se_3/Au solar cell structure without and with SnS BSF layer

Structure	V_{OC} (V)	J_{SC} (mA cm^{-2})	FF (%)	η (%)
FTO/SnS_2/Sb_2Se_3/Au	0.66	25.59	73.33	12.31
FTO/SnS_2/Sb_2Se_3/SnS/Au	0.94	31.98	83.09	24.86

The energy band diagram of the optimized Sb_2Se_3-based solar cell architecture of FTO/SnS_2/Sb_2Se_3/SnS/Au is displayed in Fig. 24. It is noticed that the energy level of conduction and valence band of SnS_2 buffer layer is lower than the Sb_2Se_3 absorber layer. As a result, electrons can travel easily to the front contact through the Sb_2Se_3/SnS_2 interface due to small conduction band offset (CBO) of −0.05 eV. On the other hand, the valence band offset (VBO) between the SnS_2 buffer layer and Sb_2Se_3 absorber layer is large enough to prevent the flow of holes from Sb_2Se_3 absorber to front contact. For the SnS BSF layer, the energy level of valence and conduction band is higher than the Sb_2Se_3 absorber layer. Moreover, a proper barrier height with a suitable conduction band offset (CBO) at the SnS BSF/Sb_2Se_3 absorber junction hinders electrons from travelling from the absorber to the back electrode which in turn reduces recombination process at the back surface.[14,98] On the contrary, the holes can travel from absorber to the back contact easily due to small VBO of 0.1 eV.

3.21 Comparative study

Table 7 compares various results from past experimental or theoretical work on Sb_2Se_3 based solar cells with various buffer layers without and with BSF layer. In comparison to the previous reported values, enhanced η have been achieved by this simulation study.

Table 6 Optimized parameter values of the FTO/SnS_2/Sb_2Se_3/SnS/Au solar cell

Optimized parameter	Value
Sb_2Se_3 absorber layer thickness	0.4 μm
Sb_2Se_3 absorber layer acceptor concentration	10^{16} cm^{-3}
Sb_2Se_3 absorber layer defect density	10^{13} cm^{-3}
Sb_2Se_3 absorber layer bandgap	1.15 eV
SnS_2 buffer layer thickness	0.03 μm
SnS_2 buffer layer donor concentration	10^{18} cm^{-3}
SnS_2 buffer layer defect density	10^{15} cm^{-3}
FTO window layer thickness	0.1 μm
FTO window layer donor concentration	10^{20} cm^{-3}
Sb_2Se_3/SnS_2 interface layer defect density	10^{10} cm^{-2}
Sb_2Se_3 absorber layer capture cross-section of electron and hole	10^{-15} cm^{-2}
Sb_2Se_3/SnS_2 interface capture cross-section of electron and hole	10^{-19} cm^{-2}
SnS BSF layer thickness	0.2 μm
SnS BSF layer acceptor concentration	10^{20} cm^{-3}
SnS BSF layer defect density	10^{14} cm^{-3}
Back contact work function	5 eV

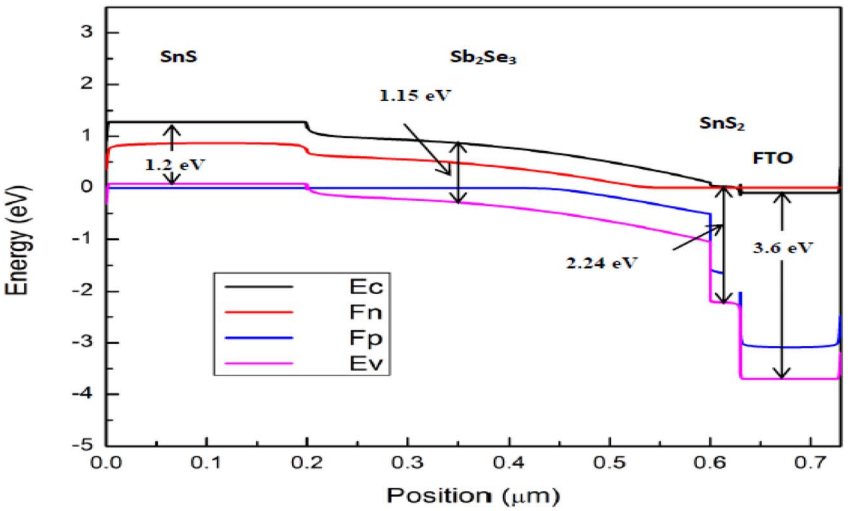

Fig. 24 Energy band diagram of proposed FTO/SnS_2/Sb_2Se_3/SnS/Au solar cell.

Table 7 Comparison of proposed solar cell with other reported Sb_2Se_3 based solar cells

Structure	Study type	Photovoltaic parameters				References
		V_{OC} (V)	J_{SC} (mA cm^{-2})	FF (%)	η (%)	
FTO/CdS/Sb_2Se_3/CZTA/Au	Experimental	0.421	28.40	57.10	6.84	73
Ag/ITO/ZnO/CdS/Sb_2Se_3/Mo/SLG	Experimental	0.454	18.4	50.6	4.22	127
Ag/ITO/CdS/Sb_2Se_3/Mo	Experimental	0.343	16.79	35.3	2.1	128
FTO/CdS/Sb_2Se_3/Spiro-OMeTAD/Au	Experimental	0.360	29.00	51.50	5.40	55
ITO/CdS/Sb_2Se_3/Au	Experimental	0.379	27.93	55.6	5.91	129
AZO/i-ZnO/CdS/TiO_2/Sb_2Se_3/Mo	Experimental	0.4	32.58	70.30	9.20	19
ITO/CdS/Sb_2Se_3/CuSCN/Au	Experimental	0.413	30.51	58.99	7.5	130
ITO/CdS/Sb_2Se_3/Au	Experimental	0.420	29.90	60.40	7.60	26
Metal contact/ZnO:Al/i-ZnO/CdS/Sb_2Se_3/Mo	Simulation	0.56	31.79	70.81	12.62	33
ZnO:Al/ZnO/CdS/TiO_2/Sb_2Se_3/MoS_2/Mo	Simulation	0.4	32.56	70.3	9.17	131
FTO/Zn(Sn,O)/Sb_2Se_3/CZTSe/Au	Simulation	0.66	34.66	81.18	18.50	132
Ag/phenyl-C61-butyric acid methyl ester (PCBM)/Sb_2Se_3/HTL/ITO	Simulation	0.858	34.18	84.04	24.66	133
Ag/ZnSe/Sb_2Se_3/Mo	Simulation	0.85	34	83.6	24.0	17
Al/ITO/CdS/Sb_2Se_3/CuS/Ni	Simulation	0.761	37.59	80.97	23.16	12
FTO/SnS_2/Sb_2Se_3/Au	Simulation	0.66	25.59	73.33	12.31	This work
FTO/SnS_2/Sb_2Se_3/SnS/Au	Simulation	0.94	31.98	83.09	24.86	This work

4. Conclusions

The electrical parameters of Sb_2Se_3-based thin film solar cell with and without SnS BSF layer have been compared in this simulation work using SCAPS-1D. First of all, experimental result is reproduced for FTO/CdS/Sb_2Se_3/Au solar cell structure to validate the numerical model and carry out analysis. Next, non-toxic SnS_2 has been used as a buffer layer instead of the hazardous cadmium sulfide (CdS) for the proposed solar cell which results in enhanced efficiency. Afterwards, to maximize efficiency different parameters such as thickness, doping concentration, bandgap, capture cross section and defect density that effect the electrical output is optimized. The optimal thickness for the Sb_2Se_3 absorber layer, SnS_2 buffer layer and FTO window layer have been chosen to be of 0.4 μm, 0.03 μm and 0.1 μm respectively. The doping density have been optimized to be of 10^{16} cm^{-3}, 10^{18} cm^{-3} and 10^{20} cm^{-3} respectively. The defect density in the Sb_2Se_3 absorber layer, SnS_2 buffer layer and the interface defect at Sb_2Se_3/SnS_2 interface have been selected to be of 10^{13} cm^{-3}, 10^{15} cm^{-3} and 10^{10} cm^{-2} respectively for optimal performance. The capture cross-section in the Sb_2Se_3 absorber layer and at Sb_2Se_3/SnS_2 interface have been optimized to be of 10^{-15} cm^{-2} and 10^{-19} cm^{-2} respectively. The optimized FTO/SnS_2/Sb_2Se_3/Au solar cell structure provides J_{SC} of 25.59 mA cm^{-2}, V_{OC} of 0.66 V, FF of 73.33% and efficiency of 12.31%. The insertion of SnS BSF layer with thickness of 0.2 μm, carrier density of 10^{20} cm^{-3} and defect density of 10^{14} cm^{-3} results in enhanced efficiency of 24.86% including J_{SC} of 31.98 mA cm^{-2}, V_{OC} of 0.94 V and FF of 83.09% for optimized novel FTO/SnS_2/Sb_2Se_3/SnS/Au solar cell structure. The findings of this simulation work provide guidelines

for the production of non-toxic, cost-effective and highly efficient Sb_2Se_3-based solar cell.

Conflicts of interest

The author declares that there is no conflict of interest regarding the publication of this paper.

Data availability

The data will be made available on reasonable request.

Acknowledgements

This research did not receive any specific grant from funding agencies in the public, commercial, or not-for-profit sectors. The author is grateful to Dr Marc Burgelman at University of Ghent, Belgium for allowing to use the SCAPS-1D simulation package.

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