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# TCR parameter study for examining the possibility of the usefulness of perovskite $\text{Pr}_{0.8}\text{K}_{0.2-x}\text{Na}_x\text{MnO}_3$ ( $x = 0.0, 0.05$ and $0.1$ ) systems for thermistor and bolometer applications

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We report a comprehensive experimental and theoretical investigation of the electrical transport properties in  $\text{Pr}_{0.8}\text{K}_{0.2-x}\text{Na}_x\text{MnO}_3$  ( $x = 0.0, 0.05$ , and  $0.1$ ) compounds synthesized *via* the sol–gel route. Temperature-dependent resistivity measurements revealed a robust and composition-independent metal–semiconductor transition ( $T_{M-SC} \approx 160$  K), an uncommon behavior for chemically substituted manganites. The transport characteristics were quantitatively examined using multiple conduction frameworks, including percolation theory, small-polaron hopping (SPH), and Mott variable-range hopping (VRH). These approaches enabled the extraction of activation energies, hopping exponents, charge-carrier localization parameters, and disorder-related scaling factors. Among the tested models, percolation theory yielded the most consistent description of the semiconducting regime across all samples. Temperature coefficient of resistance (TCR) values, calculated within phase-separation and phase-coexistence transport schemes, exhibited pronounced enhancement in the 180–200 K interval. The combined modeling-driven analysis demonstrated that Na substitution substantially modulated the intrinsic electronic transport parameters—even while preserving a fixed transition temperature—establishing these compositions as promising candidates for high-performance uncooled bolometric infrared sensing.

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## 1. Introduction

Perovskite manganites with the universal formula  $\text{AMnO}_3$  (where A can be a trivalent element like La, Pr, and Sm, bivalent like Sr and Ca or monovalent like Na, K, and Ag) have received extensive attention due to their interesting electrical and magnetic properties, and they have also been extensively studied by researchers both experimentally<sup>1,2</sup> and theoretically.<sup>3,4</sup> Small changes in dopant concentration,<sup>5,6</sup> preparation method or cation deficiency can cause huge changes in structural,<sup>7,8</sup> electrical, optical and magnetic characteristics.<sup>9</sup> Most of the studies have focused on trivalent rare earth doping in  $\text{AMnO}_3$  compounds *via* either partial or complete replacement with a monovalent element such as Ag, Na and K. These doped monovalent cations not only change the structure of the manganites but also affect their magneto-transport properties.<sup>10,11</sup> Doped manganite systems exhibit important structural, optical, electrical and magnetic characteristics.<sup>3,12,13</sup> Perovskite-like praseodymium manganites display both strong ferromagnetism and metallic conductivity when trivalent  $\text{Pr}^{3+}$  ions are partially

substituted by monovalent ions like Ag, Na, K, *etc.*<sup>14,15</sup> It has been reported that doped manganite materials exhibit multi-functional properties, including magnetic refrigeration, electrical transport, bolometric applications, and high-density magnetic recording technologies (such as read heads for hard disks and non-volatile magnetic random-access memory, MRAM).<sup>16</sup> Significant efforts have been devoted to addressing the challenges associated with uncooled bolometric applications. In this context, and given that doped manganites are composed of phase-separated ferromagnetic metallic and paramagnetic insulating regions. Li *et al.*<sup>17</sup> proposed a simple phenomenological model to describe the temperature dependence of electrical resistivity. Recently, Alexandrov *et al.*<sup>18</sup> described the resistivity of manganites near the ferromagnetic transition using the so-called current carrier density collapse (CCDC). Using this result, Wang *et al.*<sup>19</sup> can explain the behavior of TCR in manganites. In order to study the electrical transport mechanism and correlation between magnetic and electric properties, we prepared  $\text{Pr}_{0.8}\text{K}_{0.2-x}\text{Na}_x\text{MnO}_3$  ( $x = 0.00, 0.05$  and  $0.1$ ) samples. Due to their ability to exhibit a metal–semiconductor transition ( $T_{M-SC}$ ) near room temperature,  $\text{Na}^+$ - and  $\text{K}^+$ -doped  $\text{PrMnO}_3$  manganites are considered promising candidates for practical applications.<sup>20,21</sup> Specifically, the transport properties above  $T_{M-SC}$  are generally interpreted using the small polaron hopping (SPH)<sup>22</sup> or variable

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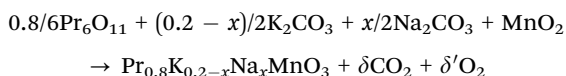


range hopping (VRH)<sup>23</sup> models, while the metallic regime is governed by electron–magnon scattering and polaron formation near the transition. Additionally, Li *et al.*<sup>24</sup> proposed a theoretical percolation model, based on phase separation between metallic and insulating regions, to explain the transport process across the whole temperature range. Typical TCR values are found to be closely related to intrinsic parameters such as activation energy, disorder, and transition temperature.

In this paper, in order to describe the electrical behavior of Pr<sub>0.8</sub>K<sub>0.2-x</sub>Na<sub>x</sub>MnO<sub>3</sub> ( $x = 0.00, 0.05$  and  $0.1$ ) synthesized by the sol–gel method, we employed these models to calculate resistivity as a function of temperature and TCR<sub>max</sub>, with particular attention paid to the role of adiabatic small polaron hopping conduction in the insulating and ferromagnetic phases. Meanwhile, detailed analysis confirmed that these theoretical approaches are quantitatively consistent with our experimental observations. Interestingly, the Na<sup>+</sup> substitution was found to significantly influence the electrical transport mechanism and TCR behavior, opening perspectives for their application in infrared detection devices.

## 2. Experimental details

In this work, the under-investigated perovskite powders have been formed by using the modified sol–gel method that is known as Pechini. Thus, Pr<sub>6</sub>O<sub>11</sub> (>99.9%), Na<sub>2</sub>CO<sub>3</sub> (>99.9%), K<sub>2</sub>CO<sub>3</sub> (>99.9%), and MnO<sub>2</sub> (>99.9%) precursors revealing an elevated purity are mixed according to the following chemical reaction:



After mixing the initial powders, the obtained solution is mixed with citric acid (C<sub>6</sub>H<sub>8</sub>O<sub>7</sub>) and ethylene glycol (C<sub>2</sub>H<sub>6</sub>O<sub>2</sub>). To synthesize the desired manganites, heat treatment was applied in the second step of the preparation. After that, to remove organic matter and obtain a viscous gel, the obtained mixture is evaporated on a thermal plate at 120 °C. To obtain a crude powder, the obtained gel is dried at 300 °C. Two calcination steps at 600 °C for 10 hours and at 800 °C for 14 hours are also effectuated. Such kind of annealing treatment changes the raw powders into materials with a well-established crystalline structure and chemical composition. Using hydraulic press, each package of powder is pressed into pellets to obtain the samples, or they are subjected to different thermal heating (at 900 °C and 1000 °C). After the elaboration of the desired compounds, the obtained materials are electrically characterized using an impedance analyzer (Agilent 4294 A) by taking the materials in the form of electrical dipoles. To conduct the electrical measurements and to obtain a capacitor configuration, thin layers of silver are made on each pellet's two opposite faces to serve as electrodes. The experimental measurements (conductance and capacitance) as a function of frequency are conducted over a wide temperature range from 80 to 500 K to confirm that our compounds facilitate the future applications of manganites.

## 3. Experimental and theoretical (TCR) parameters for testing the possibility of the usefulness of some manganites for technological applications

### 3.1. Transport properties

To investigate the electrical properties of Pr<sub>0.8</sub>K<sub>0.2-x</sub>Na<sub>x</sub>MnO<sub>3</sub> ( $x = 0.0, 0.05$  and  $0.1$ ) samples, the variation of resistivity  $\rho(T)$  with temperature was measured in the temperature range [80–500 K]. Using the derivative of resistivity with respect to temperature ( $d\rho/dT$ ) as a criterion for the type of electrical behavior, we observed that the samples ( $x = 0.0, 0.05$  and  $0.1$ ) exhibit metallic behavior ( $d\rho/dT > 0$ ) at low temperatures (for  $T < T_{M-SC}$ ) and adopt semiconductor behavior ( $d\rho/dT < 0$ ) above the  $T_{M-SC}$  temperature, where  $T_{M-SC}$  represents the temperature associated with the maximum value of resistivity  $\rho_{max}$  (Fig. 1). For samples  $x = 0.0, x = 0.05$ , and  $x = 0.1$ , the transition temperature occurs at  $T_{M-SC} = 160$  K.

**3.1.1 Low-temperature behavior ( $T < T_{M-SC}$ ).** At low temperatures ( $T < T_{M-SC}$ ), Pr<sub>0.8</sub>K<sub>0.2-x</sub>Na<sub>x</sub>MnO<sub>3</sub> ( $x = 0.0, 0.05$  and  $0.1$ ) manganites exhibit metallic behavior. This behavior can be modeled by the charge carrier diffusion model,<sup>25</sup> which is often used to fit experimental data for electrical resistivity as a function of temperature. The data are fitted using the following general expression:  $\rho(T) = \rho_0 + \rho_n T^n$  ( $n = 1, 2, 2.5, 4.5, 5$  and  $7.5$ ). To identify the appropriate fit to the resistivity data ( $\rho(T)$ ) of our manganites, we use the following equations:

$$\rho(T) = \rho_0 + \rho_1 T \quad (1)$$

$$\rho(T) = \rho_0 + \rho_2 T^2 \quad (2)$$

$$\rho(T) = \rho_0 + \rho_{2.5} T^{2.5} \quad (3)$$

$$\rho(T) = \rho_0 + \rho_2 T^2 + \rho_{4.5} T^{4.5} \quad (4)$$

$$\rho(T) = \rho_0 + \rho_2 T^2 + \rho_5 T^5 \quad (5)$$

$$\rho(T) = \rho_0 + \rho_{2.5} T^{2.5} + \rho_{7.5} T^{7.5} \quad (6)$$

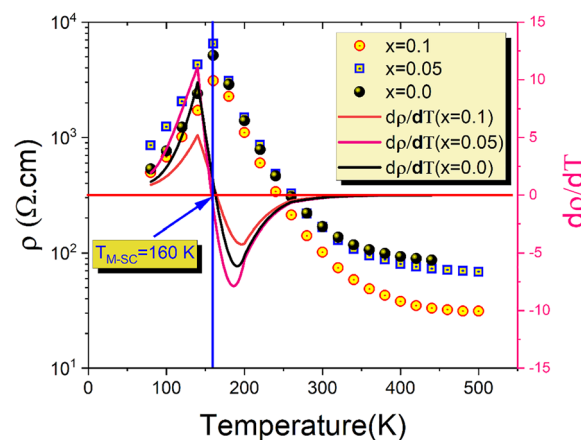


Fig. 1 Temperature evolution of resistivity  $\rho$  and  $d\rho/dT$  for the Pr<sub>0.8</sub>Na<sub>0.2-x</sub>K<sub>x</sub>MnO<sub>3</sub> ( $x = 0.00$  and  $x = 0.05$ ) compounds.



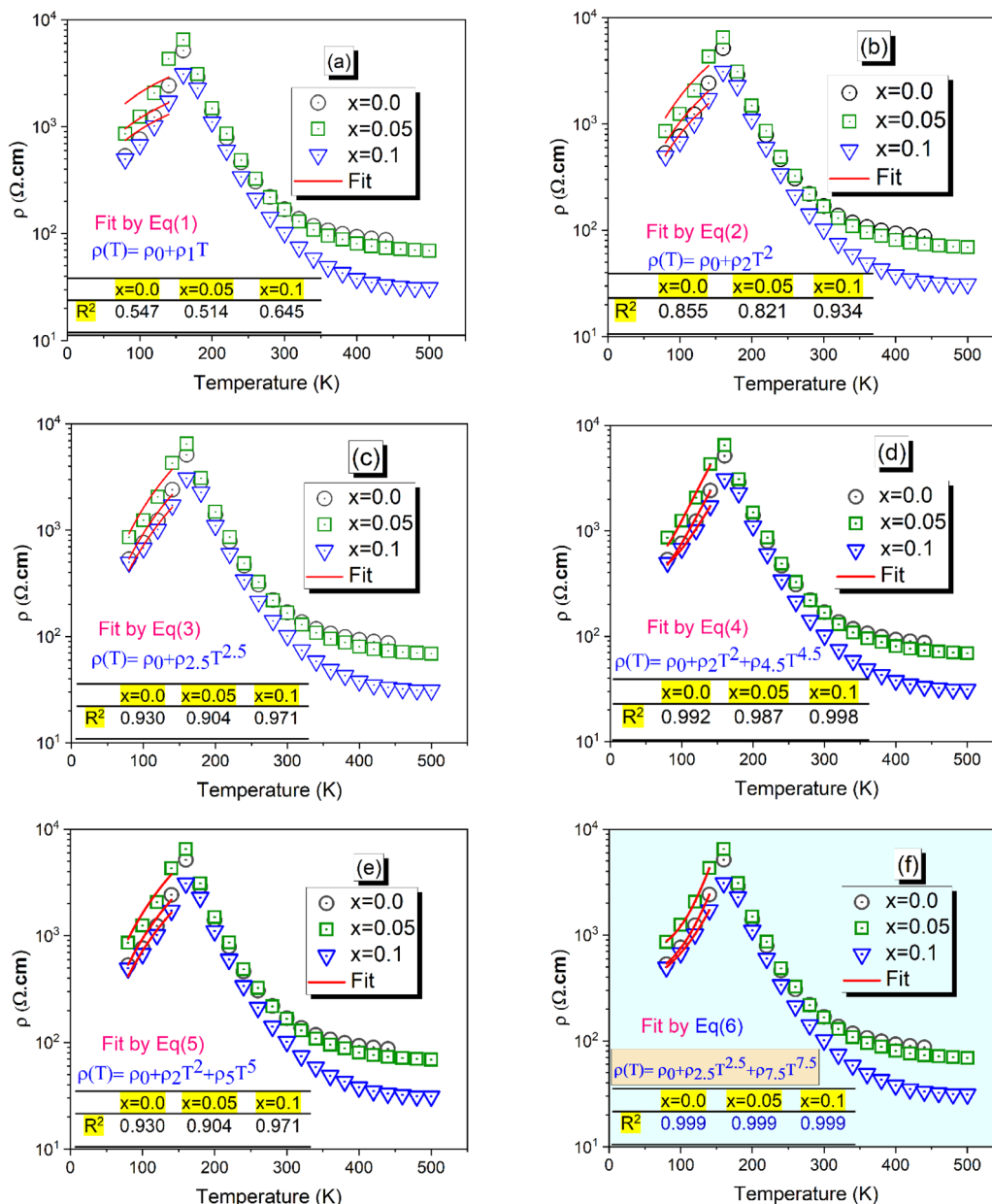


Fig. 2 The electrical resistivity  $\rho(T)$  as a function of temperature for  $\text{Pr}_{0.8}\text{K}_{0.2-x}\text{Na}_x\text{MnO}_3$  ( $x = 0.00, 0.05$  and  $0.1$ ) samples (a–f). The red line is the fit of the experimental data in the metallic region below ( $T_{M-SC}$ ) using all the six equations.

where the term  $\rho_1 T$  is a thermal diffusive conductive process and  $\rho_2 T^2$  in eqn (2), (4) and (5) represents the electrical resistivity due to the electron–electron process.<sup>26,27</sup> The other representation  $\rho_{2.5} T^{2.5}$  is the electrical resistivity caused by the electron-magnon scattering process in the FM phase.<sup>28</sup> The term  $\rho_{4.5} T^{4.5}$  is a combination of electron–electron, electron-magnon and electron–phonon scattering processes.<sup>29,30</sup> On the other hand,  $\rho_5 T^5$  represents the electron–phonon interaction<sup>31</sup> and  $\rho_{7.5} T^{7.5}$  originates partly from the formation of polarons close to metal-semiconductor transition temperature.<sup>32</sup>

In this case, the experimental data of the  $\text{Pr}_{0.8}\text{K}_{0.2-x}\text{Na}_x\text{MnO}_3$  ( $x = 0.0, 0.05$  and  $0.1$ ) sample are fitted to the aforementioned six equations (Fig. 2). The best fit can be derived by comparing

the square of the linear correlation coefficient ( $R^2$ ) determined for each equation. The corresponding parameters of the fit are shown in the Table inserted in Fig. 2. It is noteworthy to mention that the obtained values of  $R^2$  for all samples were as high as 99.9% for eqn (6), supporting the view that eqn (6) is most suitable to fit the experimental results. This indicates that the electrical characteristics at  $T < T_{M-SC}$  are controlled by the effects of the contribution of the electron-magnon scattering processes and the polaron formation. In the metallic regime ( $T < T_{M-SC}$ ), the reduction of resistivity with increasing Na substitution ( $x$ ) is primarily attributed to the enhancement of double-exchange (DE) electron hopping between  $\text{Mn}^{3+}$  and  $\text{Mn}^{4+}$  ions. Introducing  $\text{Na}^+$  (monovalent) in place of  $\text{K}^+$



(also monovalent) subtly modifies the local electronic environment around the Mn–O network. Doping  $K^+$  with  $Na^+$  in manganite oxides primarily affects the structure and electronic bandwidth rather than the Mn mixed valence state, because both  $K^+$  and  $Na^+$  are monovalent cations. Substituting the larger  $K^+$  with the smaller  $Na^+$  reduces the A-site ionic radius and lowers the tolerance factor, which increases  $MnO_6$  octahedral tilting and decreases the Mn–O–Mn bond angle. These structural distortions weaken the double-exchange interaction, leading to reduced electrical conductivity and lower ferromagnetic transition temperatures. The  $Mn^{3+}/Mn^{4+}$  ratio generally remains unchanged during  $K^+ \rightarrow Na^+$  substitution since the charge balance is preserved; however, Mn valence can be indirectly affected if the substitution alters the oxygen stoichiometry of the lattice. Overall, Na doping influences lattice distortion and transport/magnetic properties more significantly than it affects Mn valence. The corresponding parameters of fitting are collected and listed in Table 1.

**3.1.2 High-temperature behavior ( $T > T_{M-SC}$ ).** In this range of temperature, ( $T > T_{M-SC}$ ), the variation in the electrical resistivity with temperature can be explained on the basis of two different models:

- Emin–Holstein’s theory, called small polaron hopping (SPH), is considered for temperatures above  $\theta_D/2$  ( $\theta_D$  is the Debye temperature).<sup>33</sup>

- The variable range hopping (VRH) model has been suggested to explain the electrical conduction above  $T_{M-SC}$ , that is, in the range  $\theta_D/4 < T < \theta_D/2$ .<sup>34</sup>

**3.1.2.1 SPH model.** This model is based on the phenomenon of hopping of a self-trapped electron (small polaron) to localized states. The hopping movements, associated with the transport mechanism to the nearest sites, are assisted by phonons.<sup>13,25</sup> The conduction mechanism of our manganites at high temperatures ( $T > \theta_D/2$ ) is governed by the small polaron hopping model according to two possible approximations, one is called adiabatic (ASPH) (eqn (7)) and the other non-adiabatic (NSPH) (eqn (8)). These approximations are given by the following equations:<sup>33</sup>

$$\rho = \rho_0 \cdot T \cdot e^{\left(\frac{E_a}{k_B T}\right)} \quad (\text{adiabatic}) \quad (7)$$

$$\rho = \rho_0 \cdot T^{\frac{3}{2}} \cdot e^{\left(\frac{E_a}{k_B T}\right)} \quad (\text{non-adiabatic}) \quad (8)$$

where  $\rho_0$  is the residual resistivity and  $E_a$  is the energy needed for the activation of a hopping conduction process. For the studied samples, the well-known Debye temperature ( $\theta_D$ ) values were estimated using the curve of  $\ln(\rho/T)$  versus  $1/T$  (Fig. 3(a)–(c)). The optical phonon frequency ( $\nu_{ph}$ ) can be obtained from the relation ( $h \cdot \nu_{ph} = k_B \cdot \theta_D$ ), where  $h = 4.14375 \times 10^{-15}$  eV s and  $k_B = 8.61733326 \times 10^{-5}$  eV  $K^{-1}$  are Planck’s and Boltzmann’s constants, respectively. For all studied compounds, the deduced  $\nu_{ph}$  and  $\theta_D$  values are  $1.331 \times 10^{13}$  Hz and 320 K, respectively. These results are in good agreement with the results reported in the literature.<sup>35</sup> From eqn (7) and (8), the parameter “ $E_a$ ” describes the activation energies required for a charge carrier to hopping

**Table 1** The obtained parameters of the experimental data fitted by the appropriate models below and above  $T_{M-SC}$  of the  $Pr_{0.8}K_{0.2-x}Na_xMnO_3$  ( $0 \leq x \leq 0.15$ ) samples

| $x$        | $\rho(T) = \rho_0 + \rho_{2.5}T^{2.5} + \rho_{7.5}T^{7.5}$ |   |   | (ASPH model) $\rho = \rho_0 \cdot T \cdot e^{\left(\frac{E_a}{k_B T}\right)}$ |             |          | (NSPH model) $\rho = \rho_0 \cdot T^{\frac{3}{2}} \cdot e^{\left(\frac{E_a}{k_B T}\right)}$ |             |       | (SE-VRH model) $\rho(T) = \rho_0 \exp\left(\frac{T_0'}{T}\right)^{-1/2}$ |  |       |
|------------|--|---|---|---|-------------|----------|---|-------------|-------|--|--|-------|
|            | $\rho_0$ ( $\Omega$ cm)                                    | $\rho_{2.5}$ ( $\Omega$ cm $K^{-2.5}$ ) | $\rho_{7.5}$ ( $\Omega$ cm $K^{-7.5}$ ) | $R^2$   | $E_a$ (meV) | $\gamma$ | $R^2$   | $E_a$ (meV) | $R^2$ | $T_0'$ ( $10^4$ K)   | $N'(E_F)$ ( $10^{20}$ e $V^{-1}$ $cm^{-3}$ ) | $R^2$ |
| $x = 0.0$  | 35.656   | $2.821 \times 10^{-4}$                  | $1.120 \times 10^{-14}$                 | 0.999   | 76          | 2.756    | 0.995   | 92          | 0.997 | 3.3  | 6.156  | 0.996 |
| $x = 0.05$ | 62.845   | $3.547 \times 10^{-4}$                  | $2.271 \times 10^{-14}$                 | 0.999   | 81          | 2.937    | 0.990   | 103         | 0.996 | 3.5  | 5.804  | 0.998 |
| $x = 0.1$  | 30.983   | $3.105 \times 10^{-4}$                  | $5.527 \times 10^{-15}$                 | 0.999   | 109         | 3.953    | 0.988   | 130         | 0.994 | 3.9  | 5.209  | 0.999 |



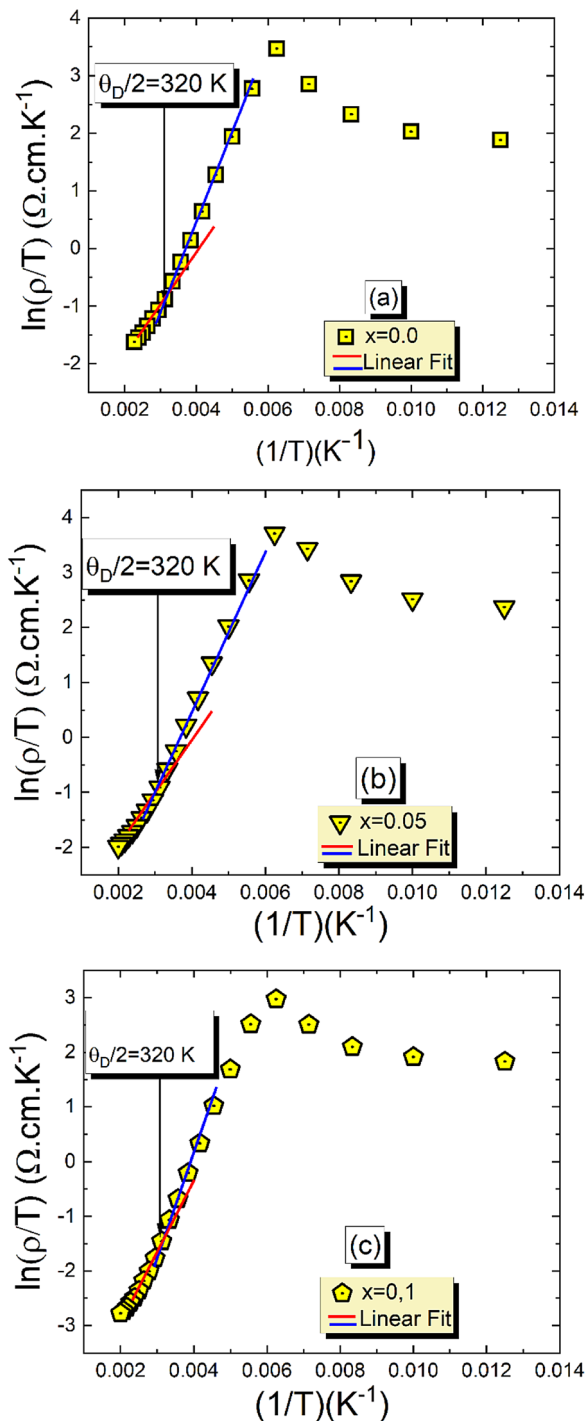


Fig. 3 Evolution of  $\ln(\rho/T)$  against the inverse of temperature for the  $\text{Pr}_{0.8}\text{Na}_{0.2-x}\text{K}_x\text{MnO}_3$  ( $x = 0.00$  and  $x = 0.05$ ) compounds (a)–(c).

and participate in electrical conduction in each temperature range. Electrical resistivity is supported by the size imbalance of the cations present in manganite. This imbalance generates cationic disorder energy. The term cation size imbalance refers to the difference in ionic radii between the A-site cations ( $\text{Pr}^{3+}$ ,  $\text{K}^+$ , and  $\text{Na}^+$ ) in the perovskite structure. Substituting  $\text{K}^+$  (ionic radius  $\approx 1.64 \text{ \AA}$ ) with the smaller  $\text{Na}^+$  ( $\approx 1.39 \text{ \AA}$ ) increases the A-site size mismatch, which enhances structural disorder and

modifies the Mn–O–Mn bond geometry. This disorder contributes to the cationic disorder energy and directly influences the carrier localization and therefore the electrical resistivity. While the electrical changes cannot be attributed to a single numerical value, the degree of A-site mismatch can be estimated through the well-known variance parameter  $\sigma^2 = \sum_i y_i r_i^2 - \langle r_A \rangle^2$  which increases with Na substitution ( $\sigma^2 = 2.23 \text{ \AA}^2$  for  $x = 0.0$  and  $\sigma^2 = 1.72 \text{ \AA}^2$  for  $x = 0.05$  and  $\sigma^2 = 1.22 \text{ \AA}^2$  for  $x = 0.1$ ).<sup>36,37</sup> In regions of high and low temperatures, the activation energy  $E_a$  is given by the following equation:<sup>38</sup>

$$E_a = \begin{cases} E_H + E_D/2 & \left( \text{for } T \geq \frac{\theta_D}{2} \right) \\ E_D & \left( \text{for } T < \frac{\theta_D}{2} \right) \end{cases} \quad (9)$$

among them,  $E_H$  is the polaron hopping energy and  $E_D$  is the disorder energy resulting from the energy difference between neighboring sites. To identify which small-polaron hopping mechanism is dominant in our samples, we compared the experimental resistivity data to both the adiabatic small-polaron hopping (ASPH) and non-adiabatic small-polaron hopping (NSPH) models. As a consequence, the variation in  $\ln(\rho/T)$  versus  $(1/k_B T)$  and  $\ln(\rho/T^{3/2})$  as a function of  $(1/k_B T)$  is plotted in Fig. 4(a)–(c) and 5(a)–(c). Then, the aforementioned curves are fitted using the last equations (eqn (7) and (8)), respectively. The obtained parameters are presented in Table 1. It can be clearly seen from this table that the linear correlation coefficients ( $R^2$ ) for the used models are very close. For this reason, it is so difficult to judge the appropriate hopping mechanism SPH model. The orthorhombic perovskite structure and the distortion of the  $\text{MnO}_6$  octahedra influence the Mn–O–Mn bond angles, lattice strain, and consequently, the electronic bandwidth. These structural factors directly affect the hopping probability between  $\text{Mn}^{3+}/\text{Mn}^{4+}$  ions and therefore play an essential role in determining the observed electrical transport behavior. To better understand which model is most suitable to describe the electrical transport phenomena at high temperatures, for all compounds, we used Holstein's condition.<sup>39</sup> This restriction assumes that the polaron bandwidth represented by “ $J$ ” should meet the expectations of the following inequality:

$$\left. \begin{aligned} J &> \phi && \left( \text{for adiabatic condition} \right) \\ J &< \phi && \left( \text{for non-adiabatic condition} \right) \end{aligned} \right\} \quad (10)$$

where  $J$  and  $\phi$  are expressed as follows:

$$J = 0.67 h \nu_{\text{ph}} \left( \frac{T}{\theta_D} \right)^{1/4} \quad (11)$$

$$\phi = \frac{1}{\pi^{3/4}} (2k_B T E_a)^{1/4} (h \nu_{\text{ph}})^{1/2} \quad (12)$$

the ratio  $J/\phi$  was expressed as follows:

$$J/\phi = 1.33 \left( \frac{k_B \theta_D}{E_a} \right)^{1/4} \quad (13)$$



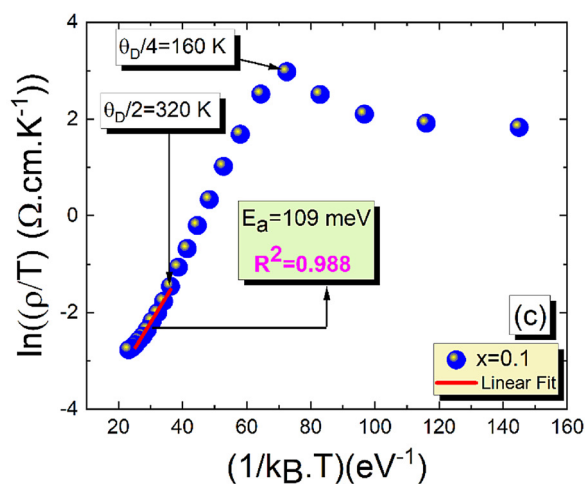
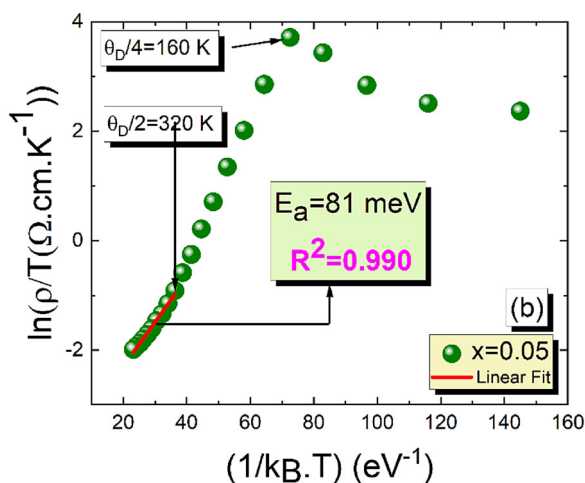
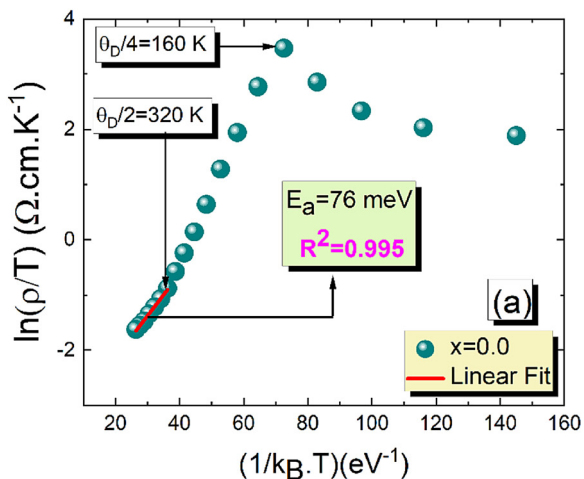


Fig. 4 Variation in  $\ln(\rho/T)$  vs.  $(1/k_B T)$  for the  $\text{Pr}_{0.8}\text{Na}_{0.2-x}\text{K}_x\text{MnO}_3$  ( $x = 0.00$  and  $x = 0.05$ ) compounds (a)–(c).

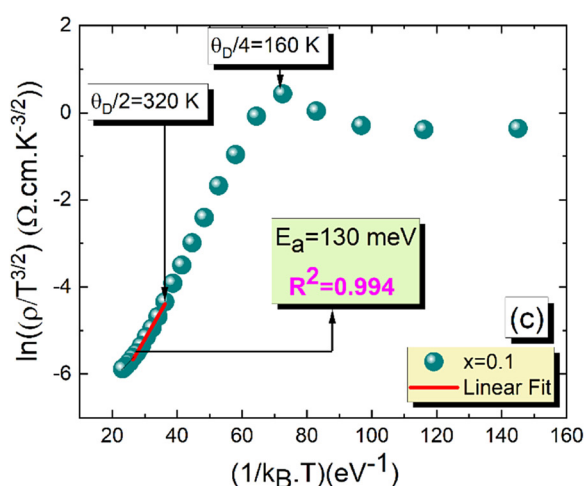
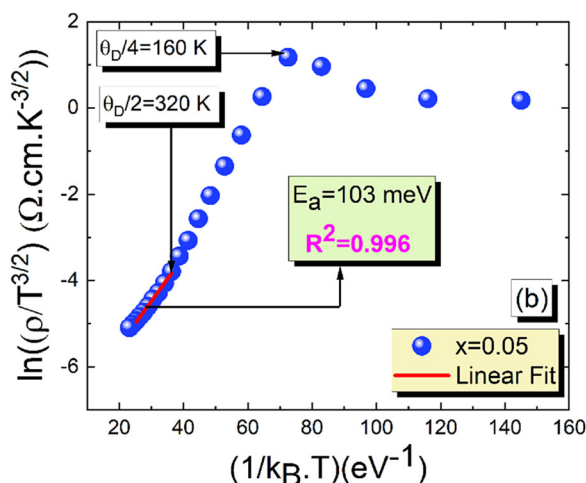
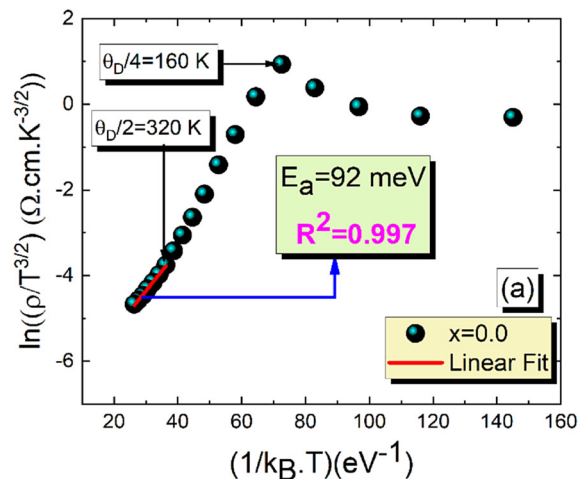


Fig. 5 Variation in  $\ln(\rho/T^{3/2})$  vs.  $(1/k_B T)$  for the  $\text{Pr}_{0.8}\text{Na}_{0.2-x}\text{K}_x\text{MnO}_3$  ( $x = 0.00$  and  $x = 0.05$ ) compounds (a)–(c).

Using the  $\theta_D$  and  $E_a$  values, computed from the slope of the straight-line curve (above  $\theta_D/2$ ), the  $J/\phi$  ratios (Table 2) are determined. Although all samples exhibit  $J/\phi > 1$ , which indicates that adiabatic hopping is possible, this criterion alone is not sufficient to identify the correct small-polaron regime. The selection of the adiabatic SPH (ASPH) mechanism is instead

based on a combination of quantitative and physical arguments. First, the values predicted by the non-adiabatic model (NSPH) are significantly lower and physically inconsistent. Second, the ASPH model provides superior fitting quality, with higher linear correlation coefficients and smaller residuals compared to NSPH, demonstrating a more accurate description of the temperature



dependence of  $\ln(\rho/T)$  versus  $1/(k_B T)$ . Finally, the mixed  $Mn^{3+}/Mn^{4+}$  valence and the associated double-exchange pathways lead to a sufficiently large electron-transfer integral and bandwidth to promote adiabatic hopping rather than phonon-assisted non-adiabatic transport. For these combined reasons, ASPH-not NSPH best describes the conduction mechanism in the investigated  $Pr_{0.8}K_{0.2-x}Na_xMnO_3$  compounds. It is also essential to check if the coupling of small polarons occurs through strong or weak e-ph interactions. According to the theories of Austin and Mott,<sup>40</sup> the values of small-polaron coupling constant ( $\gamma$ ) can be reckoned from the relation  $\gamma = 2E_a/h \cdot v_{ph}$ . According to this standard, the small polaron coupling constant ( $\gamma$ ) must satisfy the following conditions:<sup>41</sup>

$$\left. \begin{aligned} \gamma > 4 & \text{ (strong e-ph interactions)} \\ \gamma < 4 & \text{ (weak e-ph interactions)} \end{aligned} \right\} \quad (14)$$

Therefore, the e-ph coupling constant  $\gamma$  is a key parameter to control various characteristics in the sample. Consequently, the value of  $\gamma$  is an important indicator of the type of interactions between electrons and phonons. Table 1 shows that this value ranges from 2.756 to 3.953, suggesting that doping with  $Na^+$  cations enlarge the interactions between electrons and phonons. At this point, the rapport between the polaron mass  $m_p$  and rigid lattice effective mass  $m^*$  is related to  $\gamma$  using the following equation:<sup>42,43</sup>

$$m_p = \left( \frac{h^2}{8\pi^2 J R^2} \right) \exp(\gamma) = m^* \exp(\gamma) \quad (15)$$

The obtained  $m_p/m^*$  ratio is  $m_p/m^* = 15.736$ ,  $m_p/m^* = 18.859$ , and  $m_p/m^* = 52.091$  for  $x = 0.0, 0.05$  and  $0.1$ , respectively. The ratio  $m_p/m^*$  provides a quantitative indication of the strength of electron-phonon coupling in small-polaron systems. According to the established SPH model in the literature, including the work of Khan *et al.* on  $Ca_{0.85}Gd_{0.15}MnO_3$ , the values of  $m_p/m^* \approx 1-5$  correspond to weak-to-moderate coupling, whereas the ratios in the range of 10–20 are typically associated with weak adiabatic interaction where charge carriers retain significant mobility.<sup>42</sup> In contrast, values exceeding ~30–40 indicate strong polaron binding and enhanced localization. In our samples, the extracted values  $m_p/m^* = 15.736, 18.859$ , and  $52.091$  for  $x = 0.0, 0.05$ , and  $0.1$ , respectively, fall clearly within these established regimes. The first two compositions lie in the weak-interaction domain, consistent with adiabatic small-polaron hopping, while the composition with  $x = 0.1$  exhibits a significantly larger mass enhancement, indicative of a transition toward strong electron-phonon coupling due to increased structural disorder.<sup>42</sup> These results validate the interpretation that the nature of carrier-lattice interaction evolves with Na substitution.

**3.1.2.2 VRH model.** As observed in Fig. 1, we found that all the studied compounds exhibit a metallic behavior below the

characteristic Debye temperature  $\theta_D/4$ . In this case, we can assume that the Mott-VRH conduction mechanism does not contribute to the transport properties of the materials at low temperatures. Beyond such characteristic temperature  $\theta_D/4 = 160$  K, we found from Fig. 4 and 5 that each curve exhibits two linear slopes, indicating the activation of two mean conduction processes. At high temperatures, the occurrence of semiconductor behavior is attributed to the hopping motion of the small polarons. However, the origin of the observed semiconductor behavior, in the intermediate temperature range, is not yet discussed for the studied compounds. In the literature, the occurrence of a semiconductor behavior, in the intermediate temperature range, is mainly attributed to the contribution of the Shklovskii-Efros-VRH (SE-VRH) conduction mechanism.<sup>44</sup> To testify the validity of the SE-VRH on describing the electrical behavior of the materials in the intermediate temperature range, we plotted the evolution of  $\ln(\rho(T) \cdot T^{-1/2})$  versus  $T^{-1/2}$  (Fig. 6(a)–(c)) for all the prepared samples. In this temperature range, Shklovskii and Efros suggested that the material has a high density of charge carriers around the Fermi level.<sup>44</sup> The SE-VRH model takes into consideration the charge carrier interaction effects on electrical resistivity, as compared to the proposed Mott-VRH model. Based on the SE-VRH model, the variation in DC resistivity as a function of temperature can be examined using the following expression:<sup>44</sup>

$$\rho(T) = \rho_0 \exp\left(\frac{T'_0}{T}\right)^{-1/2} \quad (16)$$

where the characteristic SE-VRH temperature  $T'_0$  and the pre-exponential factor  $\rho_0$  are constants. For the studied compounds, the validity of the SE-VRH model was confirmed via the evolution of  $\ln(\rho(T) \cdot T^{-1/2})$  versus  $T^{-1/2}$  (Fig. 6(a)–(c)). In addition, the linear curves are used to calculate the characteristic SE-VRH temperature for each compound. From the relationship between  $T'_0$  and the density of states at the Fermi level ( $N'(E_F)$ ) given by  $T'_0 = 16\alpha^3 / (k_B \cdot N'(E_F))$ , we can determine  $N'(E_F)$ . The inverse of the localization length of the trapped charge carriers  $\alpha$  was found to be  $2.22 \text{ nm}^{-1}$ .<sup>45</sup> The deduced values of  $T'_0$  and  $N'(E_F)$  for all samples are summarized in Table 1. From Table 1, it is obvious that a remarkable decrease in  $N'(E_F)$  could be observed. In the intermediate temperature interval, more information about the dynamics of the charge carriers can be equally obtained. Using the Shimakawa theory,<sup>46</sup> the transfer of localized electrons via tunneling conduction processes also accounts for the origin of the electrical resistivity for  $\theta_D/4 \leq T \leq \theta_D/2$ . Consequently, the evolution of  $\rho$  against temperature, for  $\theta_D/4 \leq T \leq \theta_D/2$ , can be analyzed using the relation  $\rho = \rho_0 \cdot T^{-n}$ . From Fig. 6(d) and (e), the value of the exponent factor  $n$  was deduced. The corresponding parameters of the fit are shown in Table 1 inserted in Fig. 6(d) and (e). The  $n$  parameter was employed to examine the electron-lattice interaction force. From Fig. 6(d) and (e), the obtained  $n$  value confirmed that the electrical transport is governed by the contribution of the multi-phonon tunnel effect and indicated

**Table 2** Values of the  $J/\phi$  ratio for the case of adiabatic and non-adiabatic SPH models for the  $Pr_{0.8}K_{0.2-x}Na_xMnO_3$  ( $0 \leq x \leq 0.15$ ) samples

|                              | $x = 0.0$ | $x = 0.05$ | $x = 0.1$ |
|------------------------------|-----------|------------|-----------|
| $J/\phi$ (adiabatic SPH)     | 1.228     | 1.208      | 1.121     |
| $J/\phi$ (non adiabatic SPH) | 1.170     | 1.137      | 1.073     |



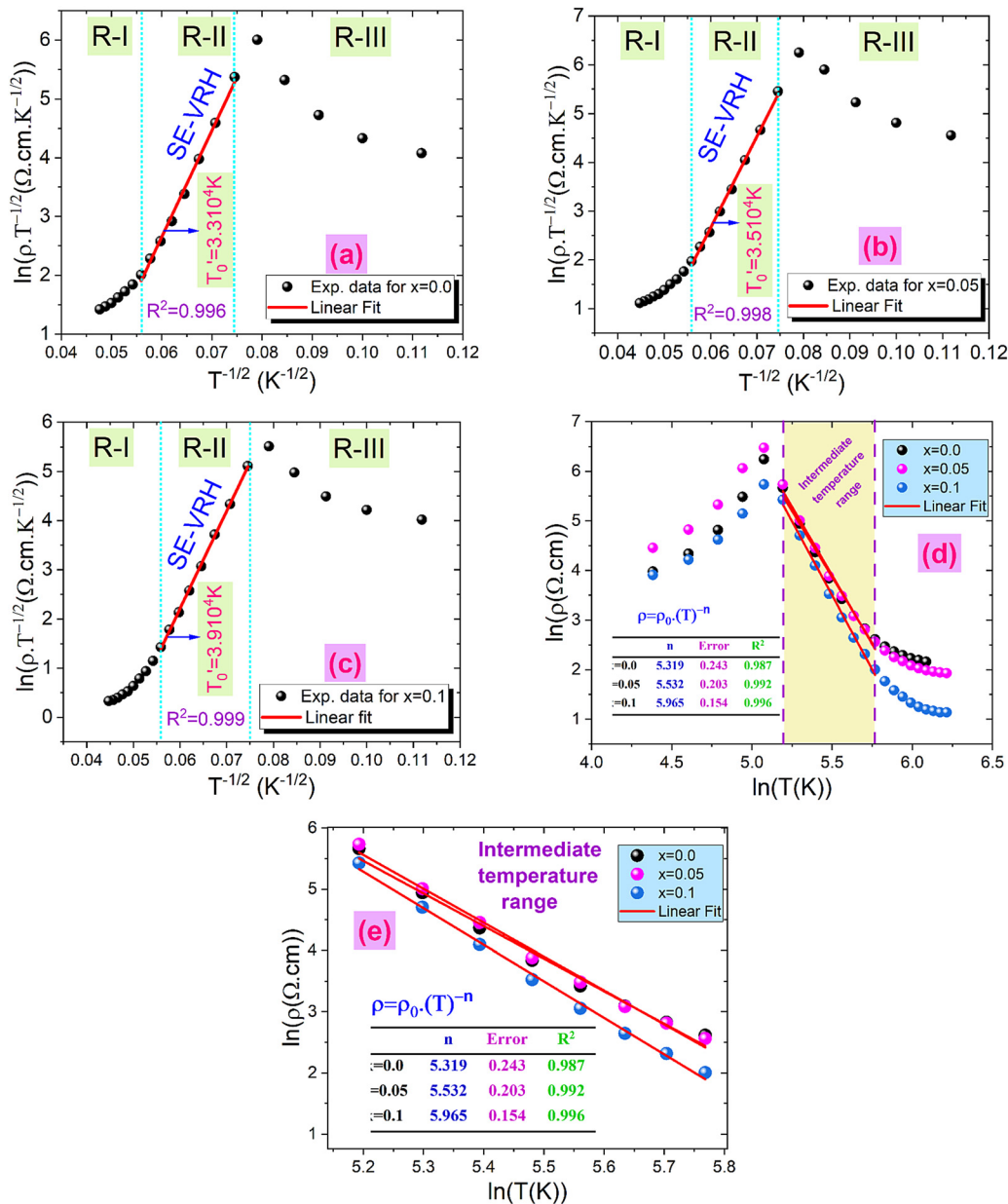


Fig. 6 Variation in  $\ln(\rho T^{-1/2})$  vs.  $T^{-1/2}$  (a)–(c). Variation in  $\ln(\rho)$  vs.  $\ln(T)$  for the  $\text{Pr}_{0.8}\text{Na}_{0.2-x}\text{K}_x\text{MnO}_3$  ( $x = 0.00$  and  $x = 0.05$ ) compounds (d and e).

that  $\text{Pr}_{0.8}\text{K}_{0.2-x}\text{Na}_x\text{MnO}_3$  ( $x = 0.0, 0.05$  and  $0.1$ ) system again reveals a weak electron-lattice interaction.<sup>46</sup>

### 3.2. Percolation model

In order to understand the transport properties in the whole temperature range explored, in particular around the transition temperature, a new phenomenological model based on the phase segregation mechanism (percolation approach) was developed.<sup>15,17</sup> Following this model and for the determination of the percolation threshold dependence, we carried out a quantitative analysis for the resistivity temperature dependence for the explored samples. According to Li *et al.*,<sup>15,17</sup> due to the competition between FM and PM regions, the total resistivity can be expressed as follows:

$$\rho = f\rho_1 + (1 - f)\rho_2 \quad (17)$$

where  $\rho_{1,2}$  is the resistivity of each phase,  $f$  is the volume fraction of the (FM) area, and  $(1 - f)$  is the volume fraction of the (PM) area. The volume fractions of FM and PM phases satisfy the Boltzmann distribution expressed as follows:

$$f = \frac{1}{1 + e^{\left[\frac{\Delta U}{k_B T}\right]}} = \frac{1}{1 + e^{\left[\frac{-U_0 \left(1 - \frac{T}{T^{\text{mod}}}\right)}{k_B T}\right]}} \quad (18a)$$

$$= \frac{1}{1 + e^{\left[\frac{-U_0}{k_B T} + \frac{U_0}{k_B T^{\text{mod}}}\right]}}$$



$$1 - f = \frac{e^{\left[\frac{\Delta U}{k_B T}\right]}}{1 + e^{\left[\frac{\Delta U}{k_B T}\right]}} = \frac{e^{\left[\frac{-U_0}{k_B T} \left(1 - \frac{T}{T_C^{\text{mod}}}\right)\right]}}{1 + e^{\left[\frac{-U_0}{k_B T} \left(1 - \frac{T}{T_C^{\text{mod}}}\right)\right]}}$$

$$= \frac{e^{\left[\frac{-U_0}{k_B T} + \frac{U_0}{k_B T_C^{\text{mod}}}\right]}}{1 + e^{\left[\frac{-U_0}{k_B T} + \frac{U_0}{k_B T_C^{\text{mod}}}\right]}} \quad (18b)$$

where  $\Delta U = -U_0 \left(1 - \frac{T}{T_C^{\text{mod}}}\right)$  is the energy difference between FM and PM states,  $T_C^{\text{mod}}$  represents the temperature in the vicinity of which the resistivity reaches a maximum value and  $U_0$  is the energy difference for temperatures well below  $T_C^{\text{mod}}$ .<sup>17</sup> Therefore, the complete expression describing the temperature dependence of resistivity over the entire temperature range can be written in the following form:

$$\rho = (\rho_0 + \rho_{2.5} T^{2.5} + \rho_{7.5} T^{7.5}) \frac{1}{1 + e^{\left[\frac{-U_0}{k_B T} + \frac{U_0}{k_B T_C^{\text{mod}}}\right]}}$$

$$+ CT e^{\frac{E_a}{k_B T}} \frac{e^{\left[\frac{-U_0}{k_B T} + \frac{U_0}{k_B T_C^{\text{mod}}}\right]}}{1 + e^{\left[\frac{-U_0}{k_B T} + \frac{U_0}{k_B T_C^{\text{mod}}}\right]}} \quad (19)$$

From eqn (18), one can find that,

(i)  $f = 0$  for  $T \gg T_C^{\text{mod}}$ ,  $f = 1$  for  $T \ll T_C^{\text{mod}}$  and

$$f = f_c = \frac{1}{2} \text{ at } T = T_C^{\text{mod}} \quad (20)$$

(ii)  $1 - f = 1$  for  $T \gg T_C^{\text{mod}}$ ,  $1 - f = 0$  for

$$T \ll T_C^{\text{mod}} \text{ and } 1 - f = f_c = \frac{1}{2} \text{ at } T = T_C^{\text{mod}} \quad (21)$$

where  $f_c$  is the percolation threshold. It is worth mentioning that when  $f < f_c$ , the sample remains semiconducting, and when  $f > f_c$ , the sample becomes metallic. The simulated curves of the resistivity (red line) of these samples are shown in Fig. 7. Obviously, the calculated results are in good agreement with the experimental data. The best parameters obtained after fitting are summarized in Table 3. In addition, the excellent agreement between the calculated graph and the experimental graph shows that the percolation model is applicable to these samples and confirms the coexistence of the FM domain and the PM area near the  $T_C$ . In addition, the relationship between the FM phase volume fraction ( $f$ ) of the sample and the temperature determined by the fitting of the resistivity data is shown in Fig. 8(a). The common behavior between samples was obtained. The function  $f(T)$  is equal to 1 under  $T_{M-SC}$ , which

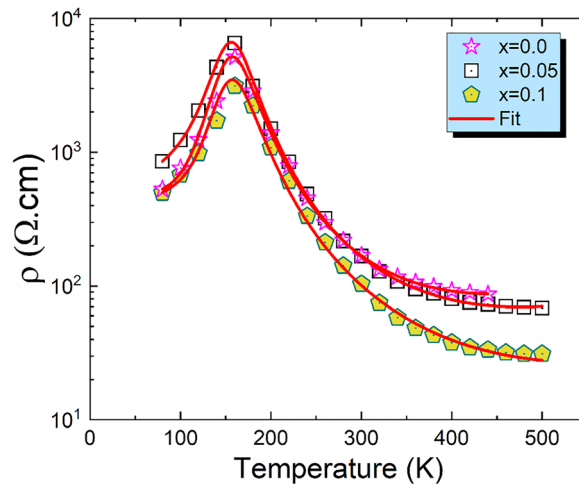


Fig. 7 The electrical resistivity  $\rho(T)$  as a function of temperature. The red line is the percolation model calculated using eqn (19).

indicates that the FM score in this part has a strong advantage. Then, above  $T_{M-SC}$ , the curve tends to decrease to zero and enter the PM insulator state. The final behavior of  $f(T)$  confirms the effectiveness of the percolation method, which assumes that the FM state transitions to the PM state when the temperature rises.

Fig. 8(b)–(d) shows the temperature dependence of the volume fraction of the FM phase  $f$  and the volume fraction of the PM phase  $1 - f$ . In the present approach, as shown in Fig. 8(b)–(d), the transition from the PM state ( $f = 0$ ) to the FM state ( $f = 1$ ) occurs over a wide temperature range ( $\sim 75$  K) near  $T_C$ . This may be more supported by the values of Curie temperature  $T_C$  determined by the volume fraction of the FM region  $df/dT$ , as shown in Fig. 8(b)–(d). We found that the obtained values of  $T_C$  for all samples are very close.

### 3.3. Correlation of the temperature coefficient of resistivity (TCR) for doped manganites to the transition temperature

The temperature coefficient of resistance (TCR), the percentage of which is defined by the following relationship:<sup>47,48</sup>

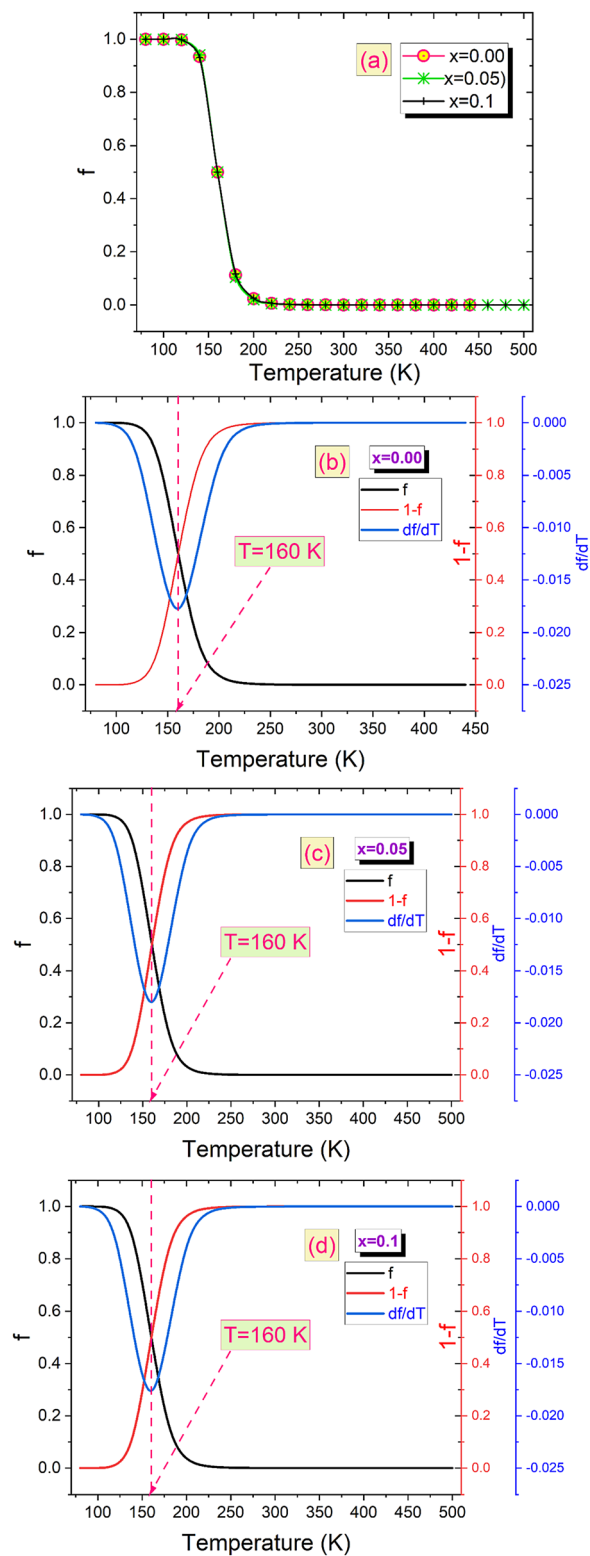
$$\text{TCR}\% = \left(\frac{1}{\rho} \frac{d\rho}{dT}\right) \times 100\% \quad (22)$$

represents the basic parameters of the device application related to the infrared detector (IR) of the night vision technology (bolometer).<sup>47,49</sup> TCR% is closely related to the resistivity and the slope of the  $\rho(T)$  curve. To understand the sensitivity of the infrared detector to a temperature in manganites, we must have a material with a high TCR value. The curves representing the temperature coefficient of resistance (TCR%) of the samples are shown in Fig. 9(a). In fact, the TCR values of the obtained  $\text{Pr}_{0.8}\text{K}_{0.2-x}\text{Na}_x\text{MnO}_3$  ( $x = 0.00, 0.05$  and  $0.1$ ) samples are comparable to some systems used for infrared sensors such as amorphous silicon ( $-2.1\%$ ) and vanadium oxide (from  $-2$  to  $-4\%$ ).<sup>47,50</sup> Fig. 9(b) collects the TCR peak and TCR peak temperature changes as a function of Na doping content. With the increase in Na content, the maximum value of TCR first decreases and then increases. Obviously, when  $x = 0.00$ , the maximum TCR value reaches  $-3.748\% \text{ K}^{-1}$ , and the peak temperature of TCR reaches



**Table 3** The obtained parameters of the percolation model using eqn (19) of the  $\text{Pr}_{0.8}\text{K}_{0.2-x}\text{Na}_x\text{MnO}_3$  ( $0 \leq x \leq 0.15$ ) samples

|            | $\rho_0$ ( $\Omega \text{ cm}$ ) | $\rho_{2.5}$ ( $\Omega \text{ cm K}^{-2.5}$ ) | $\rho_{7.5}$ ( $\Omega \text{ cm K}^{-7.5}$ )         | $C$ ( $\Omega \text{ cm}$ )          | $T_C^{\text{mod}}$ (K) | $U_0/k_B$ (K)              | $E_a/k_B$ (K)              | $R^2$ |
|------------|----------------------------------|---|---|--------------------------------------|------------------------|----------------------------|----------------------------|-------|
| $x = 0.0$  | $449.81068 \pm 68.32155$         | $9.5015 \times 10^{-4} \pm 0.0013$            | $1.34397 \times 10^{-13} \pm 7.28119 \times 10^{-14}$ | $0.00123 \pm 3.16228 \times 10^{-4}$ | 160                    | $2972.92613 \pm 136.44094$ | $1618.88704 \pm 107.13246$ | 1     |
| $x = 0.05$ | $546.54552 \pm 72.11806$         | $0.0049 \pm 0.0012$                           | $1.48674 \times 10^{-13} \pm 4.00304 \times 10^{-14}$ | $0.00143 \pm 1.78961 \times 10^{-4}$ | 160                    | $3087.13258 \pm 65.62395$  | $1622.74086 \pm 47.21513$  | 1     |
| $x = 0.1$  | $386.52349 \pm 87.54988$         | $0.00196 \pm 0.00146$                         | $1.42002 \times 10^{-14} \pm 2.15818 \times 10^{-14}$ | $0.00134 \pm 2.62766 \times 10^{-4}$ | 160                    | $2906.38964 \pm 349.19834$ | $1621.62382 \pm 50.2435$   | 0.999 |

**Fig. 8** The temperature dependencies of the volume fractions of the FM ( $f$ ) for the  $\text{Pr}_{0.8}\text{K}_{0.2-x}\text{Na}_x\text{MnO}_3$  ( $x = 0, 0.05$  and  $0.1$ ) compounds (a). The temperature dependencies of the volume fractions of the FM ( $f$ ), PM ( $1 - f$ ) phases and  $df/dT$  for the  $\text{Pr}_{0.8}\text{K}_{0.2-x}\text{Na}_x\text{MnO}_3$  ( $x = 0, 0.05$  and  $0.1$ ) samples using eqn (18a) and (18b) (b)–(d).

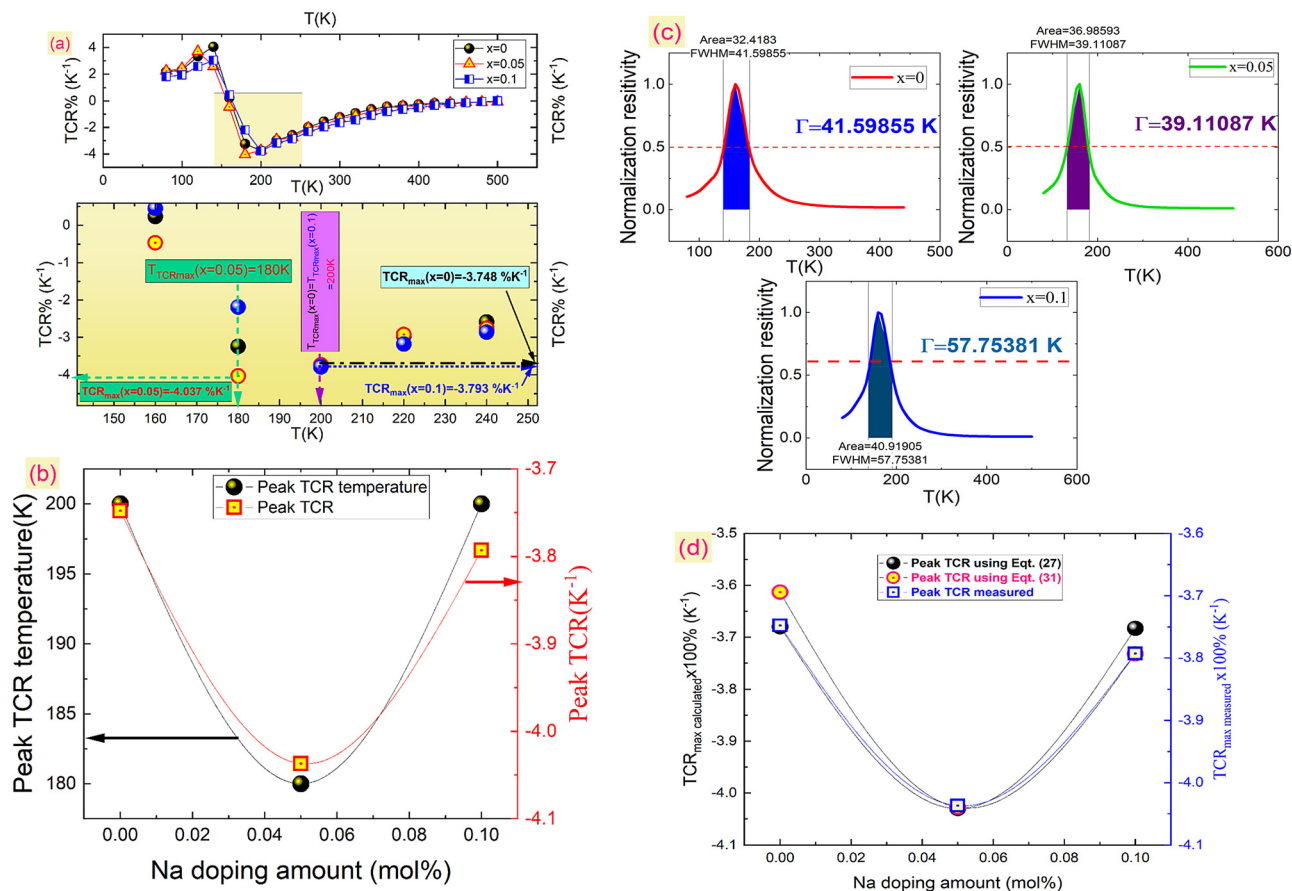


Fig. 9 The variation in TCR % as a function of temperature for the  $\text{Pr}_{0.8}\text{K}_{0.2-x}\text{Na}_x\text{MnO}_3$  ( $x = 0.00, 0.05$  and  $0.1$ ) samples (a). Peak TCR and Peak TCR temperature curves at different Na doping amounts (b). Temperature evolution of the DC normalization of resistivity and the width of the Gaussian distribution  $\Gamma$  for the  $\text{Pr}_{0.8}\text{K}_{0.2-x}\text{Na}_x\text{MnO}_3$  ( $x = 0, 0.05$  and  $0.1$ ) samples (c). The measured  $\text{TCR}_{\text{max}}$  values and the calculated  $\text{TCR}_{\text{max}}$  values at different Na doping amounts calculated using eqn (27) and (31) (d).

200 K. At  $x = 0.05$ , the TCR value reaches  $-4.037\% \text{K}^{-1}$ , but the peak temperature of TCR reaches 180 K. At  $x = 0.1$ , the TCR value drops to  $-3.793\% \text{K}^{-1}$ , but the peak temperature of TCR reaches 200 K. At this time, the main impact on TCR comes from the slope near the metal semiconductor transition region (160 K), depicting TCR with a downward trend.

In order to further clarify the suitable measured values of TCR, Alexandrov *et al.*<sup>18</sup> proposed a model called Current Carrier Density Collapse (CCDC), where paramagnetic insulating and ferromagnetic metallic phases exist simultaneously, whose resistivity expression is given by the following formula:

$$\rho = \rho_1^{1-\nu} \rho_2^\nu \quad (23)$$

where  $\rho_1 = CT e^{\frac{E_a}{k_B T}}$ ,  $\rho_2 = \rho_0 + \rho_{2.5} T^{2.5} + \rho_{7.5} T^{7.5}$  are the resistivity of each phase, respectively, and  $\nu(T) = \frac{1}{2} \text{erfc} \left[ \frac{T - T_C}{\Gamma} \right]$  is the volume fraction of the second phase where  $\Gamma$  is the width of the Gaussian distribution and  $\text{erfc}$  is the error function given by  $\text{erfc}(x) = 1 - \frac{2}{\sqrt{\pi}} \sum_{n=0}^{\infty} \frac{(-1)^n}{(2n+1)n!} x^{2n+1}$  or more precisely

$$\text{erfc}(x) = 1 - \frac{2}{\sqrt{\pi}} \left[ x - \frac{x^3}{3.1!} + \frac{x^5}{5.2!} - \frac{x^7}{7.3!} + \dots \right]. \quad \text{Using the}$$

expression of  $\text{erfc}$ , we can deduce that  $\nu(T) \approx \frac{1}{2} - \frac{1}{\sqrt{\pi}} \frac{T - T_C}{\Gamma}$

$$\text{and } 1 - \nu(T) \approx \frac{1}{2} + \frac{1}{\sqrt{\pi}} \frac{T - T_C}{\Gamma}.$$

Using eqn (23), TCR can be written as follows:

$$\text{TCR} = \frac{1}{\rho} \frac{d\rho}{dT} = \frac{d \ln \rho}{dT} \quad (24)$$

Thus,

$$\text{TCR} = \frac{d(1-\nu)}{dT} \ln \rho_1 + (1-\nu) \frac{d \ln \rho_1}{dT} + \frac{d\nu}{dT} \ln \rho_2 + \nu \frac{d \ln \rho_2}{dT} \quad (25)$$

Finally, we can write TCR as follows:

$$\begin{aligned} \text{TCR} = & \frac{1}{\sqrt{\pi}} \frac{1}{\Gamma} \left[ \ln \left( \frac{C.T}{\rho_0 + \rho_{2.5} T^{2.5} + \rho_{7.5} T^{7.5}} \right) + \frac{E_a}{k_B T} \right] \\ & + \frac{1}{2} \left[ \frac{1}{T} \left( 1 - \frac{E_a}{k_B T} \right) + \frac{2.5 \rho_{2.5} T^{1.5} + 7.5 \rho_{7.5} T^{6.5}}{\rho_0 + \rho_{2.5} T^{2.5} + \rho_{7.5} T^{7.5}} \right] \\ & + \frac{1}{\sqrt{\pi}} \frac{T - T_C}{\Gamma} \left[ \frac{1}{T} \left( 1 - \frac{E_a}{k_B T} \right) - \frac{2.5 \rho_{2.5} T^{1.5} + 7.5 \rho_{7.5} T^{6.5}}{\rho_0 + \rho_{2.5} T^{2.5} + \rho_{7.5} T^{7.5}} \right] \end{aligned} \quad (26)$$



It can be seen from eqn (26) that the maximum TCR ( $\text{TCR}_{\text{max}}$ ) value occurs at temperature  $T_C$ . Therefore, by substituting  $T = T_C$  into eqn (26) and considering that the residual resistivity is

It is important to note that  $f = 1/2$  when  $T = T_C$ , and the residual resistivity  $\rho_0$  is usually much smaller than the resistivity at  $T_C$ ,  $\text{TCR}_{\text{max}}$  is expressed as follows:

$$\text{TCR}_{\text{max}} \approx \frac{C e^{\frac{E_a}{k_B T_C}} \left( \frac{U_0}{k_B T_C} + 1 - \frac{E_a}{k_B T_C} \right) + 2.5 \rho_{2.5} T_C^{1.5} + 7.5 \rho_{7.5} T_C^{6.5} + \rho_{2.5} \frac{U_0}{2k_B} T_C^{0.5} + \rho_{7.5} \frac{U_0}{2k_B} T_C^{5.5}}{\left[ \rho_{2.5} T_C^{2.5} + \rho_{7.5} T_C^{7.5} + C T_C e^{\left[ \frac{E_a}{k_B T_C} \right]} \right]} \quad (30)$$

generally much smaller than the resistivity at  $T_C$  and  $\Gamma \ll T_C$ , the  $\text{TCR}_{\text{max}}$  value is approximately estimated as follows:

$$\text{TCR}_{\text{max}} = \text{TCR}_{T=T_C} \approx \frac{1}{\sqrt{\pi} \Gamma} \left[ \ln \left( \frac{C}{\rho_{2.5} T_C^{1.5} + \rho_{7.5} T_C^{6.5}} \right) + \frac{E_a}{k_B T_C} \right] \quad (27)$$

Like the measured  $\text{TCR}_{\text{max}}$ , we also presented the calculated  $\text{TCR}_{\text{max}}$  in Fig. 9(d) using eqn (27) and the values of the width of the Gaussian distribution  $\Gamma$  estimated from Fig. 9(c) for all samples. As shown in Fig. 9(d), the calculated  $\text{TCR}_{\text{max}}$  is very close to the measured values of all samples, which shows that eqn (27) can explain experimental data well for  $\text{TCR}_{\text{max}}$  for the samples. We also fitted the experimental resistivity data to the phenomenological model based on the percolation mechanism proposed by Li *et al.*<sup>17</sup> which is studied in the second Section 3.3. Using eqn (17), TCR can be expressed as follows:

$$\text{TCR} = \frac{1}{\rho} \left[ \frac{d(1-f)}{dT} \rho_1 + \frac{d\rho_1}{dT} (1-f) + \frac{df}{dT} \rho_2 + \frac{d\rho_2}{dT} f \right] \quad (28)$$

In addition, the following equations are obtained:

$$\frac{df}{dT} = -\frac{d(1-f)}{dT}$$

$$= -U_0 e^{\left[ \frac{-U_0}{k_B T} + \frac{U_0}{k_B T_C^{\text{mod}}} \right]} \left/ \left[ k_B T \left( 1 + \left[ \frac{-U_0}{k_B T} + \frac{U_0}{k_B T_C^{\text{mod}}} \right] \right) \right]^2 \right.,$$

$$\frac{d\rho_1}{dT} = \left( 1 - \frac{E_a}{k_B T} \right) \cdot C \cdot \exp[E_a/k_B T]$$

$$\text{and } \frac{d\rho_2}{dT} = 2.5 \rho_{2.5} T^{1.5} + 7.5 \rho_{7.5} T^{6.5}.$$

By substituting all the above-mentioned results in eqn (28), TCR is expressed as follows:

$$\text{TCR} = \frac{1}{\rho} \left[ \frac{U_0 e^{\left\{ \frac{-U_0}{k_B T} + \frac{U_0}{k_B T_C^{\text{mod}}} \right\}}}{k_B T \left( 1 + e^{\left\{ \frac{-U_0}{k_B T} + \frac{U_0}{k_B T_C^{\text{mod}}} \right\}} \right)} \right]^2 \left\{ C T e^{\frac{E_a}{k_B T}} - \rho_0 - \rho_{2.5} T^{2.5} - \rho_{7.5} T^{7.5} \right\}$$

$$+ \frac{1}{1 + e^{\left[ \frac{-U_0}{k_B T} + \frac{U_0}{k_B T_C^{\text{mod}}} \right]}} \left\{ 2.5 \rho_{2.5} T^{1.5} + 7.5 \rho_{7.5} T^{6.5} + \left( 1 - \frac{E_a}{k_B T} \right) C e^{\left[ \frac{E_a}{k_B T} + \frac{-U_0}{k_B T} + \frac{U_0}{k_B T_C^{\text{mod}}} \right]} \right\} \quad (29)$$

Finally,

$$\text{TCR}_{\text{max}} = \text{TCR}_{T=T_C}$$

$$\approx \frac{C \cdot e^{\frac{E_a}{k_B T_C}} \left( \frac{U_0}{2k_B T_C} + 1 \right) + 2.5 \rho_{2.5} T_C^{1.5} + 7.5 \rho_{7.5} T_C^{6.5}}{\left[ \rho_{2.5} T_C^{2.5} + \rho_{7.5} T_C^{7.5} + C T_C e^{\left[ \frac{E_a}{k_B T_C} \right]} \right]} \quad (31)$$

As shown in Fig. 9(d), the calculated  $\text{TCR}_{\text{max}}$  value is very close to the measured values of all samples, which shows that eqn (31) can well explain the  $\text{TCR}_{\text{max}}$  experimental data of the samples. Based on eqn (27) and (31),  $\text{TCR}_{\text{max}}$  is governed by several key parameters including the Curie temperature ( $T_C$ ), the disorder factor ( $\Gamma$ ), the electron–magnon scattering constant ( $\rho_{2.5} T^{2.5}$ ), the polaron hopping barrier ( $\rho_{7.5} T^{7.5}$ ), and the FM–PM energy separation ( $U_0$ ). These quantities may originate from intrinsic mechanisms, such as the  $\text{Mn}^{3+}/\text{Mn}^{4+}$  electronic configuration, double-exchange interactions, and intrinsic lattice distortions, or from extrinsic effects arising from A-site substitution (Na/K), oxygen non-stoichiometry, and cationic disorder. Together, these intrinsic and extrinsic contributions modify the charge-carrier hopping landscape, thereby controlling the magnitude and position of  $\text{TCR}_{\text{max}}$  in the studied manganites.

## 4. Conclusion

The electrical transport in  $\text{Pr}_{0.8}\text{K}_{0.2-x}\text{Na}_x\text{MnO}_3$  ( $x = 0.00, 0.05,$  and  $0.1$ ) exhibits two distinct regimes: a low-temperature regime dominated by electron–magnon–phonon scattering and polaron formation near the  $T_{\text{M-SC}}$  transition ( $\approx 160$  K) and a high-temperature regime well described by ASPH and



VRH models. The percolation model successfully captures resistivity across the full temperature range (80–500 K), highlighting the role of connectivity and phase coexistence. Na substitution for K significantly modifies resistivity and TCR, enabling fine-tuning of the transport mechanism, with ASPH providing the most accurate hopping description. High TCR values and their correlation with intrinsic parameters activation energy,  $T_{M-SC}$ , and cationic disorder underscore the sensitivity of these manganites to compositional tuning, establishing them as promising candidates for uncooled bolometric infrared sensors in the 180–200 K range and for advanced thermal sensing applications.

## Conflicts of interest

There are no conflicts to declare.

## Data availability

All data relevant to this study are available from the corresponding author upon reasonable request.

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