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Condensation on soft substrates: a mesoscopic perspective

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We consider the condensation and evaporation of a volatile partially wetting liquid on a soft substrate in contact with a homogeneously saturated gas phase. Recent experiments demonstrated a strong dependence of nucleation density on the substrate softness. Motivated by these experiments, we approach the problem considering both macroscale and mesoscale models. On the macroscale, we employ thermodynamic considerations to determine the critical nuclei energies and the resulting nucleation probabilities in the limits of rigid and liquid substrates. On the mesoscale, we use a gradient dynamics model for a drop of volatile liquid on a soft substrate with Kelvin–Voigt viscoelasticity in Winkler–foundation form. The governing energy functional incorporates elastic and interface energies as well as bulk liquid energy. We show that nucleation probabilities obtained with the two models agree for small supersaturation, but display differences when drop nuclei are small. Finally, we use the mesoscopic model to investigate the condensation and evaporation dynamics of drops in the intermediate elastic regime and relate the results to the experimental findings.

1 Introduction

When breathing against a cold window pane, one notices how it becomes opaque. A close look reveals, that this results from a rather dense random arrangement of numerous tiny drops that scatter light. Such breath figures form on cool surfaces due to condensation of liquid from the adjacent vapor and are extensively investigated.^{1–5} Depending on the surface properties, the liquid condenses into droplets or into a uniform film. The spontaneous local gathering of vapor particles that initiate the formation of drops of another thermodynamic phase is called nucleation. While condensation, *i.e.*, the clustering of vapor molecules into liquid drops, is accessible to observation and study, it is triggered by nucleation, a microscopic process that normally occurs at scales that make it challenging to study. Yet nucleation plays a central role in a wide range of phenomena, from crystallization,⁶ electron condensation in solids,⁷ tectonic events such as earthquakes⁸ and volcanic eruptions,⁹ to

meteorological processes like cloud formation, snow, and rainfall,^{10,11} pathological conditions such as decompression sickness,¹² and even the formation of black holes.¹³ In general, nucleation is important for phase transitions of first order, which is a subject of great interdisciplinary interest and practical importance. Since Gibbs achieved the first insights into the matter¹⁴ various theories have been developed. The widely used classical nucleation theory (CNT)^{15–18} determines the energy cost of cluster formation based on purely macroscopic quantities such as interface and bulk energies. The CNT is extended, *e.g.*, by the dynamic nucleation theory (DNT) and by the extended modified liquid drop (EMLD) model that incorporate translational motion and small fluctuations in the particle number, respectively.^{18–20} In contrast to these phenomenological approaches, kinetic theory calculates the energy of cluster formation by directly considering the molecular interactions on the microscale thereby avoiding the use of macroscopic quantities. Considering the particles to be hard shapes molecular dynamics (MD) and Monte Carlo simulations are often utilized.^{21–24} In contrast, density functional theory (DFT) describes the system in terms of a microscale ensemble-averaged density and is used, *e.g.*, to consider colloidal crystals.²⁵ The direct observation of nuclei of only a few molecules in size still remains an experimental challenge.^{18,20}

Here, we consider how a soft substrate influences nucleation and growth of sessile drops of a partially wetting liquid from vapor, *i.e.*, condensation onto soft substrates. It is known that the ability of a substrate to deform under external pressure

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crucially influences the nucleation density.²⁶ This observation is confirmed by ref. 27 using MD simulations. There, it is further found that also condensation rate and heat transfer efficiency increase with the softness of the substrate. It also affects the condensation mode, *i.e.*, whether drops or films are formed. Sharma *et al.*²⁸ observe that even though the overall condensation of drops increases with the softness of the substrate, the growth of individual drops may be reduced by cloaking effects, *e.g.*, by uncrosslinked PDMS chains leaking from the substrate. Further it is found that coalescence is significantly delayed as the substrate softness increases^{26,29} and it is confirmed by gradient dynamics models that as well the coarsening mode is affected by the substrate softness.³⁰

Recently, experiments on dew formation presented in ref. 31 were performed on substrates of different softness. There, flat homogeneous layers (millimetric thickness) of silicone elastomers are deposited on a cooling stage in a chamber with controlled humidity (mixture of water vapor and N₂) as illustrated in Fig. 1(a). Condensation is achieved by cooling down the gel while simultaneously fixing the chamber humidity and pressure until a phase transition is induced [see Appendix A]. The threshold of phase transition is referred to as saturation. The impact of substrate elasticity on dew formation is investigated by tuning the gel stiffness through its crosslinking density. The breath figures are recorded from above using a high resolution magnifying objective. Since the resolution of

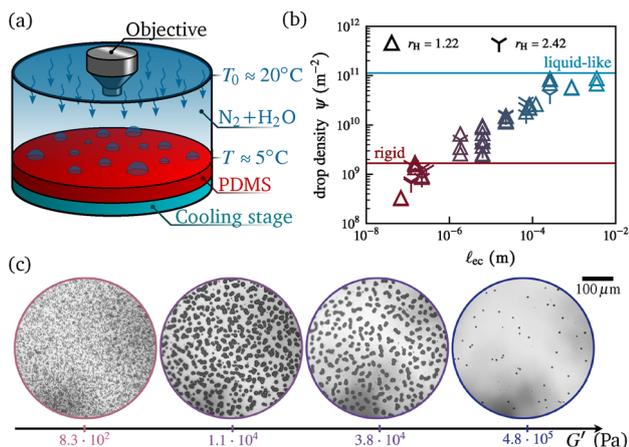


Fig. 1 (a) Schematic of the experimental setup. A gel substrate (red) is placed inside a controlled-humidity chamber and cooled down to $T_s = 5^\circ\text{C}$ using a Peltier element (green). (b) Drop density ψ as a function of substrate softness quantified via the elasto-capillary length ℓ_{ec} , based on data from ref. 31. The experiment used various PDMS gels – Sylgard 184 with mixing ratios ranging from 10 : 1 to 80 : 1, CY52-276 (Dow Corning) with ratios of 1.3 : 1 and 1 : 1, and PVS Elite16 (1 : 1). Measurements were conducted at two imposed relative humidities: $r_H = 2.42$ (γ) and $r_H = 1.22$ (Δ). Horizontal lines indicate the limiting cases of a rigid substrate (red; nanometric PDMS brush grafted on a silicon wafer, see ref. 32) and a liquid-like substrate (blue; uncrosslinked PDMS). The color gradient from red to blue indicates the transition between these two limits. (c) Top-view images of breath figures formed on substrates with different softness levels, taken at the onset of drop visibility. The apparent nucleation density decreases with increasing substrate stiffness, characterized by the shear storage modulus G' .

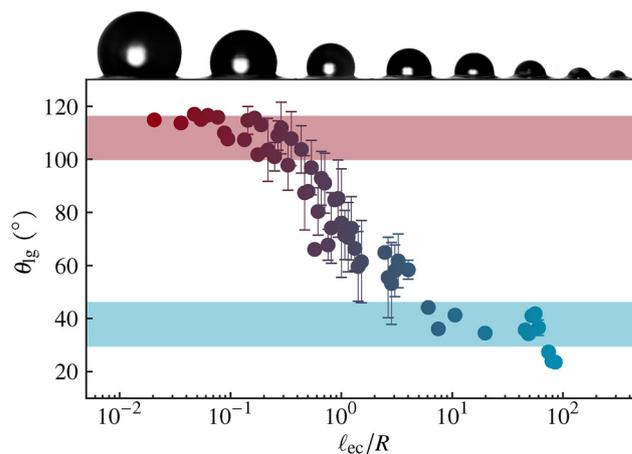


Fig. 2 Liquid–gas contact angle θ_{lg} relative to the horizontal as a function of the gel softness ℓ_{ec}/R . Angles are measured on side-view images of droplets with radii ranging from $R \approx 10\ \mu\text{m}$ to $\approx 1\ \text{mm}$, *i.e.*, recorded at later stages, sitting on gels with storage modulus G' ranging from 100 Pa to 10^6 Pa. The lightly shaded bands indicate the contact angles experimentally determined on short PDMS brushes, *i.e.*, in the rigid limit (red), and on uncross-linked PDMS oligomers, representing the liquid-like limit (blue) for the same material. Again, the red to blue color gradient indicates the transition between these two limits.

the objective is $\approx 1\ \mu\text{m}$ the experiment does not directly record the nucleation process but rather the subsequent mesoscopic dynamics. Fig. 1(c) provides examples of the resulting breath figures, each taken as soon as drops are visible, for decreasing substrate softness (from left to right) quantified by the shear storage modulus G' . As the latter increases, that is, with decreasing elasto-capillary length $\ell_{ec} = \gamma/G'$, the initial number of drops is found to decrease. Remarkably, once condensation has started, there are no further nuclei forming in the dry regions between the already growing drops, which is due to the decrease of vapor concentration below saturation in the proximity of the substrate as discussed in ref. 24 and 31. In Fig. 1(b) the drop density ψ is displayed as a function of ℓ_{ec} for two different humidities, $r_H = 1.22$ (Δ) and $r_H = 2.42$ (γ).[†] Remarkably, while the drop density appears to be strongly affected by the substrate softness, *i.e.*, it increases with ℓ_{ec} , it is barely affected by changes in the supersaturation, that is the relative humidity r_H at the substrate. Consider ref. 24 and 31 for a more extensive discussion regarding the later stages of droplet condensation.

Further, in ref. 33–36 it is predicted, that in the regime of intermediate softness the contact angles of steady drops transit smoothly between Young's and Neumann's laws, which is experimentally confirmed (see Fig. 2).[‡] This transition in the contact angle is reminiscent of the transition observed in the drop density ψ when going from rigid to liquid-like substrates

[†] These values correspond to the relative humidity in the proximity of the substrate, that is at $T = 5^\circ\text{C}$ and can be related to the relative humidity at different temperatures, *e.g.*, $T_0 = 20^\circ\text{C}$ at the chamber roof, using eqn (43).

[‡] The droplets on which the angles are measured are above micron size and therefore not nuclei, but what they become after some time of condensation.



[cf. Fig. 1(b)]. The cross-over between the Young regime and the Neumann regime can be inferred from Fig. 2 to occur when the elasto-capillary length becomes comparable to the drop base radius $\ell_{ec} \sim R$ (cf. Fig. 3). In Fig. 1(b) the transition is found at $\ell_{ec} \approx 10 \mu\text{m}$ and thus elasticity is expected to play a role when $\ell_{ec} \approx R \approx 10 \mu\text{m}$. This observation is enigmatic for the typical nuclei size at the employed humidities is known to be $R^* \ll 10 \mu\text{m}$, *i.e.*, too small to feel the elasticity of the substrate. As the drops grow larger, due to condensation, they automatically undergo a size-controlled transition in ℓ_{ec}/R and elasticity gains impact. The transition shown in Fig. 2 may occur even before the diffusive boundary layer has formed.

To investigate the role of elasticity in nucleation, we use a mesoscopic gradient dynamics model³⁷ similar to the one presented in ref. 30, coupling a classic thin-film equation (TFE) for a simple liquid^{38,39} to the dynamics of the soft adaptive substrate employing a Kelvin–Voigt-type dynamics in Winkler-foundation form. In comparison to ref. 30, the model is extended to capture condensation and evaporation applying the one-sided approach of ref. 40–43 for evaporating sessile drops. Thereby, the saturation of the vapor phase is considered homogeneous as is the case in the very early stages of the experiment where the nucleated droplets are below the optical resolution of the equipment and therefore experimentally inaccessible. The advantage of the gradient dynamics approach is that it is derived directly from the governing energy functional, which makes it very versatile and easily adaptable to many scenarios. A somewhat similar model has been used in ref. 43 to study the dynamics of droplet growth and coalescence due to imposed local influx in dependence of the substrate softness and viscous damping. Here, the full curvature formulation³⁷ is used which more exactly describes the static drop behavior, *cf.* ref. 44. The model is utilized to investigate the increase of nucleation density with increasing softness in an extended range of supersaturation that goes beyond the range considered in the experiment. In particular, we consider

values where the size of the nuclei becomes comparable to the elasto-capillary length.

First, in Section 2 the macroscopic CNT is used to estimate the nucleation energy barrier in the limiting cases of perfectly rigid and liquid substrates, considering unstable steady macroscopic drops to represent the nuclei. In Section 3 the mesoscopic gradient dynamics model is used to investigate the critical nucleus in the regime of intermediate softness. We compare mesoscopic and macroscopic results in the liquid and rigid limits. Finally, the influence of substrate softness on the nucleation energy barrier is investigated in the context of the experimentally observed phenomena.

2 Macroscopic nuclei

According to CNT the change in energy associated with the creation of a new phase is given by the difference in Gibbs free energy \mathcal{G} , implying constant temperature T , particle number N and external pressure p .^{18,45–48} The bulk contribution is given by the difference $\Delta\mu$ in chemical potentials, between initial and final state, to which the interface energies are added. In the present case of vapor condensing into liquid at a solid substrate, the change in Gibbs free energy is (see Appendix B for details)^{18,46–48}

$$\mathcal{G}_{\text{macro}} = \gamma_{lv}A_{lv} + \gamma_{sl}A_{sl} + \gamma_{sv}(A_{sv} - A'_{sv}) - \rho_{\ell}V_{\ell}\Delta\mu, \quad (1)$$

with γ_{ij} and A_{ij} respectively being the energies and areas of the liquid–vapor (lv), substrate–liquid (sl) and substrate–vapor (sv) interfaces and the difference in chemical potentials per particle is

$$\Delta\mu = \mu_v - \mu_{\ell} = k_B T \ln(r_{\text{H}}). \quad (2)$$

The substrate–vapor interface area of the initial dry substrate state is A'_{sv} and ρ_{ℓ} is the particle density of the liquid. The Gibbs free energy eqn (1) combines surface energy penalties, which in case of drop-like structures of size R scale with $\sim R^2$, with the decrease in chemical potential per particle when changing from the vapor to the liquid phase, scaling with the created volume $\sim R^3$. This balance results in an energy barrier \mathcal{G}^* that must be overcome to nucleate and which defines a critical size R^* . Since the nucleation of droplets on a substrate is a stochastic process driven by random fluctuations¹⁸ the nucleation probability P is estimated using a Boltzmann factor

$$P \sim \exp\left(-\frac{\mathcal{G}^*}{k_B T}\right). \quad (3)$$

The ratio in the exponent relates the energy barrier \mathcal{G}^* to the thermal energy $k_B T$. In the following, we calculate this energy barrier for a radially symmetric drop (w.r.t. the z -axis) of base radius R sitting on a deformable substrate, extended in the (x, y) -plane as shown in Fig. 3. In the limits of a perfectly rigid ($\ell_{ec} = 0$) and liquid-like ($\ell_{ec} = \infty$) substrate, elasticity can be neglected and the equilibrium drop shape is exclusively governed by the interface and bulk phase energies, *i.e.*, it adapts spherical-cap shapes.

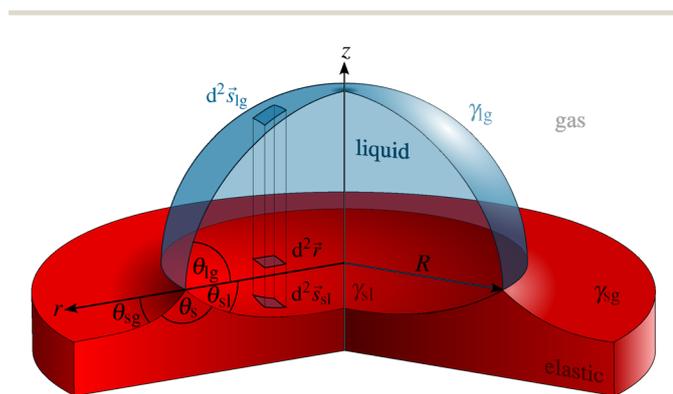


Fig. 3 Sketch of a radially symmetric drop of partially wetting liquid with base radius R . The spherical cap meets the elastic substrate along a circular three phase contact line. The macroscopic contact angle θ is governed by the energies γ_{sv} , γ_{sl} and γ_{lv} of the interfaces between the respective phases. The ratio of a surface element ds and its projection onto the (x, y) -plane defines the metric factor $\sqrt{1 + (\nabla\phi)^2}$ of the respective profile $\phi(r)$.



2.1 Rigid limit

In the rigid limit the substrate is flat and the liquid–vapor interface of a drop or nucleus takes the shape of a spherical cap with curvature κ_{lv} as shown in Fig. 4(a). While the contact angle θ_Y is given by the interface energies according to Young's law

$$\gamma_{lv} \cos \theta_Y + \gamma_{sl} = \gamma_{sv}, \quad (4)$$

the curvature depends on the volume of the nucleus which is yet to be determined. In terms of κ_{lv} and θ_Y the volume is

$$V = \frac{8\pi}{3\kappa_{lv}^3} (2 + \cos \theta_Y) (1 - \cos \theta_Y)^2, \quad (5)$$

while the interface areas are

$$A_{lv} = \frac{8\pi}{\kappa_{lv}^2} (1 - \cos \theta_Y), \quad A_{sl} = \frac{4\pi}{\kappa_{lv}^2} \sin^2 \theta_Y. \quad (6)$$

Since the substrate is perfectly flat, the total area, that is the area A'_{sv} of the dry reference state, is $A'_{sv} = A_{sv} + A_{sl}$. With eqn (4)–(6) the energy (1) becomes

$$\begin{aligned} \mathcal{G}_{\text{macro}} = & \gamma_{lv} \frac{4\pi}{\kappa_{lv}^2} (2 - 3 \cos \theta_Y + \cos^3 \theta_Y) \\ & - \rho_\ell \Delta\mu \frac{8\pi}{3\kappa_{lv}^3} (2 + \cos \theta_Y) (1 - \cos \theta_Y)^2. \end{aligned} \quad (7)$$

With $(2 + \cos \theta_Y) (1 - \cos \theta_Y)^2 = 2 - 3 \cos \theta_Y + \cos^3 \theta_Y$ we then find

$$\begin{aligned} \mathcal{G}_{\text{macro}} = & \pi (2 + \cos \theta_Y) (1 - \cos \theta_Y)^2 \left(\frac{4\gamma_{lv}}{\kappa_{lv}^2} - \frac{8\rho_\ell \Delta\mu}{3\kappa_{lv}^3} \right) \\ = & \pi g(\theta_Y) \left(\gamma_{lv} R^2 \sin \theta_Y - \frac{1}{3} R^3 \rho_\ell \Delta\mu \right), \end{aligned} \quad (8)$$

where the base radius $R = 2 \sin \theta_Y / \kappa_{lv}$ has been introduced and the function

$$g(\theta) = (2 + \cos \theta) (1 - \cos \theta)^2 / \sin^3 \theta \quad (9)$$

is a geometric prefactor that monotonically increases with θ . Therefore, the energy barrier increases with increasing hydrophobicity of the substrate, *i.e.* with increasing contact angle θ_Y .

The critical nucleus has to satisfy $\partial_R \mathcal{G}_{\text{macro}} = 0$ and its resulting base radius is

$$R^* = \frac{2\gamma_{lv} \sin \theta_Y}{\rho_\ell \Delta\mu}. \quad (10)$$

In consequence, at fixed $\Delta\mu$ a nucleated drop of base radius $R < R^*$ will shrink (evaporate) leaving behind the dry state, whereas a nucleus of base radius $R > R^*$ will grow (condense) without bound. The corresponding energy barrier is

$$\begin{aligned} \mathcal{G}_{\text{macro}}^* = \mathcal{G}_{\text{macro}}(R^*) = & \frac{4\pi\gamma_{lv}^3}{3(\rho_\ell \Delta\mu)^2} g(\theta_Y) \sin^3 \theta_Y \\ = & \frac{\pi}{3} \gamma_{lv} R^{*2} g(\theta_Y) \sin \theta_Y. \end{aligned} \quad (11)$$

With $r_H \approx 2.41$, $\gamma_{lv} = 70 \times 10^{-3} \text{ J m}^{-2}$, $\rho_\ell = 3.34 \times 10^{28} \text{ m}^{-3}$ and $\theta_Y = 70^\circ$ the critical nucleus has a size of $R^* \approx 1.166 \text{ nm}$ with an associated energy barrier $\mathcal{G}_{\text{macro}}^* / k_B T \approx 30$. Note, that the θ_Y -dependent factor of $\mathcal{G}_{\text{macro}}^*$ in eqn (11) increases monotonically from $g(\theta_Y) \sin(\theta_Y)^3 = 0$ in the complete wetting case ($\theta_Y = 0^\circ$) to $g(\theta_Y) \sin(\theta_Y)^3 = 4$ in the non-wetting case ($\theta_Y = 180^\circ$). In other words, low contact angles will drastically reduce the nucleation barrier.

2.2 Liquid-like limit

In the liquid-like case, *i.e.*, for $\ell_{ec} \rightarrow \infty$, the substrate is deformed under the influence of the Laplace pressure caused by the curved liquid–vapor interface until it is balanced by the Laplace pressure of the substrate–liquid interface. This results in the shape of a liquid lens as shown in Fig. 4(c) characterized by constant curvatures of both interfaces. While the drop sinks into the substrate the liquid–vapor and substrate–liquid interfaces form angles θ_{lv} and θ_{sl} w.r.t. the horizontal, respectively. The angles are again governed by the interface energies according to the components of Neumann's law:

$$\text{horizontal: } \gamma_{lv} \cos \theta_{lv} + \gamma_{sl} \cos \theta_{sl} = \gamma_{sv}, \quad (12)$$

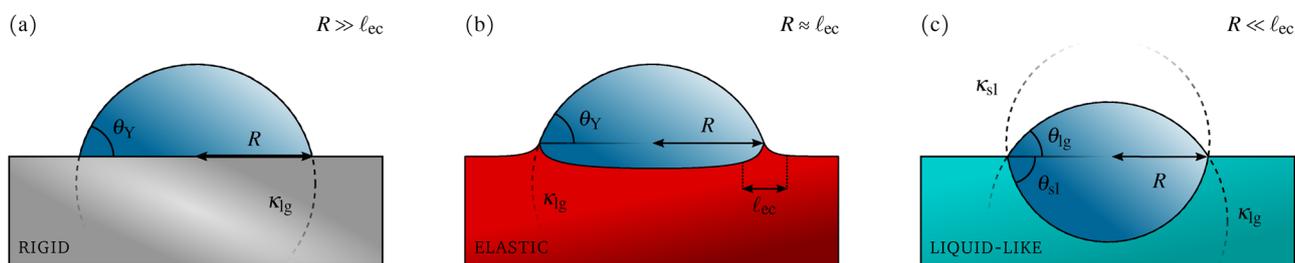


Fig. 4 Characteristic drop shapes of partially wetting liquid on substrates of different softness. (a) The substrate is rigid and very resistant against deformations, $R \gg \ell_{ec}$. The drop adopts the shape of a spherical cap with curvature κ_{lv} and contact angle θ_Y selected by Young's law. (b) The substrate is elastic and soft enough to allow for the formation of wetting ridges at the contact lines, $R \approx \ell_{ec}$, but stiff enough to prevent the drop from sinking. The local angles at the tip of the wetting ridge are given by Neumann's law and as the softness increases the region rotates inwards such that the liquid–vapor contact angle and curvature increasingly deviate from those in the rigid case. (c) The substrate is so soft that it is considered liquid-like and elasticity is negligible, $R \ll \ell_{ec}$. The drop resembles a liquid lens described by the intersection of two spherical caps with curvatures κ_{lv} and κ_{sl} . The angles at the three-phase contact are still related by Neumann's laws but the slope of the solid–liquid interface approaches zero.



$$\text{vertical: } \gamma_{lv} \sin \theta_{lv} = \gamma_{sl} \sin \theta_{sl}. \quad (13)$$

Note, that the substrate beyond the drop is considered to remain perfectly horizontal. Similar to eqn (5) the lens volume can be expressed in terms of the curvatures and Neumann angles

$$V = \frac{8\pi}{3\kappa_{lv}^3}(2 + \cos \theta_{lv})(1 - \cos \theta_{lv})^2 + \frac{8\pi}{3\kappa_{sl}^3}(2 + \cos \theta_{sl})(1 - \cos \theta_{sl})^2. \quad (14)$$

The balance of Laplace pressures results in a fixed ratio of curvatures given by the inverse ratio of the corresponding interface energies

$$\frac{\kappa_{sl}}{\kappa_{lv}} = \frac{\gamma_{lv}}{\gamma_{sl}} = \frac{\sin \theta_{sl}}{\sin \theta_{lv}}, \quad (15)$$

with the second equal sign resulting from eqn (13). Note, that the curvature of a profile is considered negative if it is convex, as is the case for the substrate–liquid interface beneath the drop, and positive if it is concave, like the liquid–vapor interface (cf. Fig. 4). In consequence, the difference in the Gibbs free energy (1) becomes

$$\mathcal{G}_{\text{macro}} = \pi[g(\theta_{lv}) + g(\theta_{sl})] \left(\gamma_{lv} R^2 \sin \theta_{lv} - \frac{1}{3} R^3 \rho_{\ell} \Delta\mu \right), \quad (16)$$

where $g(\theta_{lv}) + g(\theta_{sl}) = 3V/(\pi R^3)$. The critical radius and energy are then

$$R^* = \frac{2\gamma_{lv} \sin \theta_{lv}}{\rho_{\ell} \Delta\mu} \quad \text{and} \quad (17)$$

$$\begin{aligned} \mathcal{G}_{\text{macro}}^* &= \frac{4\pi\gamma_{lv}^3}{3(\rho_{\ell}\Delta\mu)^2} [g(\theta_{lv}) + g(\theta_{sl})] \sin^3 \theta_{lv} \\ &= \frac{\pi\gamma_{lv} R^{*2}}{3} [g(\theta_{lv}) + g(\theta_{sl})] \sin \theta_{lv}, \end{aligned} \quad (18)$$

respectively. Note, that the form of the expression for the critical radius R^* is identical in the rigid and liquid-like limit [cf. eqn (10) and (17)] and that the energy for the case of a rigid substrate [eqn (8)] is recovered from eqn (16) in the limit $\theta_{lv} = \theta_Y$ and $g(\theta_{sl}) = 0$. Further, the ratio $\mathcal{G}_{\text{rigid}}^*/\mathcal{G}_{\text{liquid}}^* \geq 1$ and depends only on the interface energies but not on supersaturation, *i.e.*, not on R^* and $\Delta\mu$. For example, if the interface energies are $\gamma_{lv} = 70 \times 10^{-3} \text{ N m}^{-1}$, $\gamma_{sl} = 48 \times 10^{-3} \text{ N m}^{-1}$ and $\gamma_{sv} = 72 \times 10^{-3} \text{ N m}^{-1}$ the nucleation barrier differs by a factor $\mathcal{G}_{\text{rigid}}^*/\mathcal{G}_{\text{liquid}}^* = 2.28$ between the rigid and liquid-like case.

3 Mesoscopic model

In contrast to the rigid and liquid-like limit, in the intermediate elastic regime the substrate profile is not analytically known. We denote the corresponding radially symmetric height profiles by $\chi(r)$ for the liquid–vapor interface and $\zeta(r)$ for the substrate profile. The liquid layer thickness profile is then $h(r) = \chi(r) - \zeta(r)$ (see Fig. 5). So far, only steady macroscopic drops have been considered. We now formulate a fully dynamic

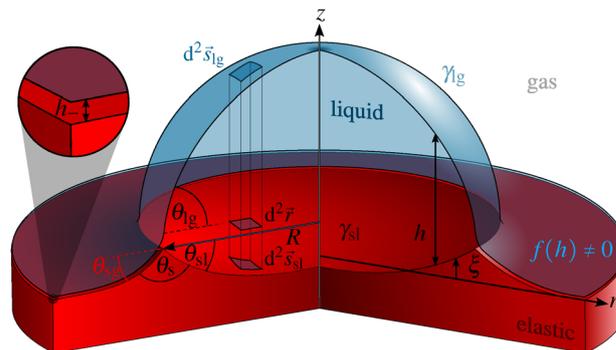


Fig. 5 Sketch of a mesoscopic radially symmetric drop of partially wetting liquid on an elastic substrate. The local liquid layer thickness and the substrate–liquid interface are described by scalar functions $h(r)$ and $\zeta(r)$, respectively. Both resemble spherical caps centered at $r = 0$ and transit into the precursor layer of height h_- (see the zoom) along a circular three phase contact region at $r = R$. The macroscopic base radius R is estimated by the position of maximal curvature of the liquid–vapor interface and the solid–gas interface energy is modeled by the wetting energy $f(h)$.

mesoscopic model that is applicable in the intermediate elastic regime as well as in the rigid and liquid-like limits. To do so, we include the mesoscopic wetting energy $f(h)$ that governs the effective interaction of the solid–liquid and liquid–vapor interface. It is assumed to result from long-range van der Waals interactions and short-range repulsive interactions

$$f(h) = \frac{A}{2h^2} \left[\frac{2}{5} \left(\frac{h_a}{h} \right)^3 - 1 \right]. \quad (19)$$

The minimum of $f(h)$ at $h = h_a$ [cf. thin lines in Fig. 6(a)] ensures that a macroscopically dry substrate is always covered by an ultra-thin adsorption layer of height h_a , the energy of which has to be taken into account. The precise thickness h_- of

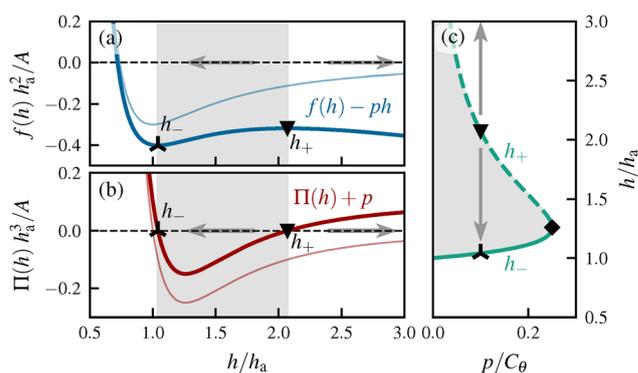


Fig. 6 Dimensionless (a) wetting energy f and (b) Derjaguin (disjoining) pressure Π as functions of the film thickness h with $C_\theta = 1$. Since $\Pi = -\partial_h f$ the zeros of the Π correspond to the extrema of f and reflect steady film states. At saturation, *i.e.* $p = 0$ (thin lines), the functions allow for only one stable steady film state h_- (λ). For $p > 0$, *e.g.*, $p = 0.1$ (thick lines). A second unstable film state h_+ (\blacktriangledown) exists. (c) With increasing p the two states approach each other and annihilate in a saddle-node bifurcation (\blacklozenge). The sign of $\Pi + p$ determines whether the film grows due to condensation or shrinks by evaporation (gray shaded), as indicated by the arrows for $p = 0.1$.



this layer depends on supersaturation and equals h_a only for $\Delta\mu = 0$ as will be further discussed in Section 3.1. In consequence, in the mesoscopic description, the macroscopic substrate–vapor interface energy is represented by the sum of the energies of the adsorption layer, substrate–liquid interface and liquid–vapor interface.

Demanding consistency between the meso- and macroscopic descriptions at $\Delta\mu = 0$ leads to the condition⁴⁹

$$\gamma_{sv} = \gamma_{lv} + \gamma_{sl} + f(h_a). \quad (20)$$

Then, together with Young's law (4), the Hamaker constant A corresponds to

$$A = \frac{10}{3} h_a^2 \gamma_{lv} (1 - \cos \theta_Y). \quad (21)$$

Further, the energy associated with the elastic deformation of the substrate is now taken into account. Employing the Winkler-foundation model⁵⁰ it is given by

$$\mathcal{F}_{el} = \frac{1}{2S} \int \xi^2(r) 2\pi r dr, \quad (22)$$

with S being an effective softness, *i.e.*, the inverse of the elastic stiffness. This formulation effectively describes the substrate as a continuous spring and follows from the fundamental solution for a finite-thickness layer with linear elasticity exposed to a localized force at the free surface. For a detailed discussion *cf.* ref. 30.

The complete energy functional combines eqn (1) and (22), thereby expressing the interface areas and volumes in terms of h and ξ and the substrate–vapor interface energy γ_{sv} in terms of the wetting potential f [eqn (19) and (20)]. The energy \mathcal{G}_{meso} of a substrate with liquid coverage (drop or thick film) relative to the reference state of a macroscopically dry flat substrate is given by

$$\mathcal{G}_{meso} = \mathcal{G}_{meso}^{wet} - \mathcal{G}_{meso}^{dry}, \quad (23)$$

with

$$\begin{aligned} \mathcal{G}_{meso}^{wet} = 2\pi \int_0^L \left[\gamma_{lv} \sqrt{1 + (\partial_r h + \partial_r \xi)^2} \right. \\ \left. + [\gamma_{sl} + f(h)] \sqrt{1 + (\partial_r \xi)^2} - \rho_\ell \Delta\mu h + \frac{\xi^2}{2S} \right] r dr, \end{aligned} \quad (24)$$

$$\mathcal{G}_{meso}^{dry} = \pi L^2 [\gamma_{lv} + \gamma_{sl} + f(h_-) - \rho_\ell \Delta\mu h_-], \quad (25)$$

where the domain has been restricted to a circular area of radius $L \gg R$. The dry substrate state is characterized by $h = h_-(\Delta\mu)$. Note, that the constant $\rho_\ell \Delta\mu$ can either be seen as an imposed chemical potential (relative humidity) or as a Lagrange multiplier for volume conservation

$$\rho_\ell \Delta\mu \int_0^L (h - h_0) 2\pi r dr = \rho_\ell \Delta\mu \Delta V = 0, \quad (26)$$

with h_0 being an arbitrary mean liquid layer thickness that is to be conserved.

The energy is extremized by calculating its variations w.r.t. the variables h and ξ yielding

$$\frac{\delta \mathcal{G}_{meso}}{\delta h} = -\gamma_{lv} \kappa(h + \xi) - \Pi(h) \sqrt{1 + (\partial_r \xi)^2} - \rho_\ell \Delta\mu \quad (27)$$

$$\begin{aligned} \frac{\delta \mathcal{G}_{meso}}{\delta \xi} = & -\gamma_{lv} \kappa(h + \xi) \\ & - \left(\frac{1}{r} + \partial_r \right) \left(\frac{[\gamma_{sl} + f(h)] \partial_r (h + \xi)}{\sqrt{1 + (\partial_r h + \partial_r \xi)^2}} \right) + \frac{1}{S} \xi \end{aligned} \quad (28)$$

with the local curvature $\kappa(\varphi) = \left(\frac{1}{r} + \partial_r \right) \left(\frac{\partial_r \varphi}{\sqrt{1 + (\partial_r \varphi)^2}} \right)$ of a field φ and the Derjaguin (disjoining) pressure $\Pi(h) = -\partial_h f(h)$ (*cf.* Fig. 6).§ Note, that for $h \gg h_a$ one has $\Pi \rightarrow 0$ and eqn (27) depends only on $\chi = h + \xi$, indicating that (at uniform supersaturation) the liquid–vapor interface of a steady drop always forms a spherical cap of curvature $\kappa_{lv} = -\rho_\ell \Delta\mu / \gamma_{lv}$, entirely independent of elasticity. In consequence, at fixed contact angles also the volume of a steady drop is directly determined by the supersaturation.

To capture the time evolution we employ a gradient dynamics approach,^{30,37,51} *i.e.*, we use the kinetic equations

$$\frac{\partial h}{\partial t} = \nabla \cdot \left[Q(h) \nabla \frac{\delta \mathcal{G}_{meso}}{\delta h} \right] - M \frac{\delta \mathcal{G}_{meso}}{\delta h}, \quad (29)$$

$$\frac{\partial \xi}{\partial t} = -\frac{1}{\zeta} \frac{\delta \mathcal{G}_{meso}}{\delta \xi}. \quad (30)$$

The dynamics of the liquid layer thickness h corresponds to a thin-film equation with mobility $Q(h) = h^3/3\eta$ and dynamic viscosity η ⁵² which is extended by a non-conserved term that incorporates phase transition-limited mass exchange between liquid and vapor^{37,42,53} driven by the variation $\delta \mathcal{G}/\delta h$ with the transfer mobility M . For a discussion of other evaporation models see ref. 54. The dynamics of the substrate corresponds to the Kelvin–Voigt model and describes an exponential relaxation in time scaled by the effective substrate viscosity ζ .³⁰ To reduce the number of parameters, the equations are non-dimensionalized using characteristic length and time scales

$$t = T\tilde{t}, \quad r = h_a \tilde{r}, \quad \xi = h_a \tilde{\xi}, \quad h = h_a \tilde{h}. \quad (31)$$

with $T = 3\eta h_a / \gamma_{lv}$. After dropping the tildes one obtains

$$\begin{aligned} \partial_t h = & - \left(\frac{1}{r} + \partial_r \right) \left(h^3 \partial_r \left[\kappa(h + \xi) + C_\theta \Pi(h) \sqrt{1 + (\partial_r \xi)^2} \right] \right) \\ & + m \left[\kappa(h + \xi) + C_\theta \Pi(h) \sqrt{1 + (\partial_r \xi)^2} + p \right] \end{aligned} \quad (32)$$

$$\partial_t \xi = \frac{1}{\tau} \left[\kappa(h + \xi) + \left(\frac{1}{r} + \partial_r \right) \left(\frac{[\sigma + C_\theta f(h)] \partial_r \xi}{\sqrt{1 + (\partial_r \xi)^2}} \right) - \frac{\xi}{s} \right] \quad (33)$$

§ Thereby, $\kappa(h + \xi)$ corresponds to the curvature κ_{lv} and $\kappa(\xi)$ to κ_{sl} .



with the dimensionless parameters

$$C_\theta = \frac{A}{\gamma_{lv} h_a^2} = \frac{10}{3}(1 - \cos \theta_V),$$

$$p = h_a \frac{\rho_\ell \Delta \mu}{\gamma_{lv}} = \rho_\ell h_a^3 \log(r_H) = h_a \kappa_{lv}^*,$$

$$\tau = \frac{\zeta h_a}{\gamma_{lv} T} = \frac{\zeta}{3\eta}, \quad m = \frac{3\eta}{h_a} M, \quad \sigma = \frac{\gamma_{sl}}{\gamma_{lv}}, \quad s = \frac{\gamma_{lv} S}{h_a^2}. \quad (34)$$

Here, $\kappa_{lv}^* = 2 \sin \theta_{lv} / R^*$ is the predicted curvature of the liquid–vapor interface of the macroscopic critical nucleus [eqn (17)]. From here on, p refers to the (dimensionless) supersaturation, defined above. The thickness of the adsorption layer is chosen as the thermal capillary length $h_a = \sqrt{k_B T / \gamma_{lv}}$, which is used in molecular kinetic theory (MKT) of wetting and capillary wave theory (CWT).^{55–57} It scales the thermal fluctuation of the liquid–vapor interface and in that sense the diffusivity of the latter. From an energetic perspective it defines the scale at which the thermal energy competes with the energy penalty associated with an increased interfacial area due to the interface tension $\gamma_{lv} h_a^2 = k_B T$. Hence, in the following all energies are expressed in terms of the thermal energy $k_B T$. With $\mathcal{O}(\gamma) \sim 10^{-2} \text{ N m}^{-1}$ and $\mathcal{O}(T) \sim 10^2 \text{ K}$ it follows that $\mathcal{O}(h_a) \sim 10^{-9} \text{ m}$. The elastocapillary length used in Fig. 4 is related to the softness s by³⁰

$$s = \left(\frac{\ell_{ec}}{h_a} \right)^2. \quad (35)$$

The shape of a steady drop sitting on an elastic substrate and the profile of the latter are usually characterized by the ratio of elastocapillary length to drop size, e.g., ℓ_{ec}/R or $\ell_{ec}/\sqrt[3]{V}$ [cf. Fig. 4].[¶]

3.1 Steady film states

Before turning to the critical nuclei, we consider the case of a steady liquid layer of uniform thickness $h(r) = h_0$ on an undisturbed flat substrate $\zeta(r) = 0$. Then, the Laplace pressures vanish and the dimensionless total pressures [eqn (27) and (28)] reduce to

$$\frac{\delta \mathcal{G}_{\text{meso}}}{\delta h} = -C_\theta \Pi(h_0) - p, \quad \frac{\delta \mathcal{G}_{\text{meso}}}{\delta \zeta} = 0. \quad (36)$$

In Fig. 6(b) the total pressure $\delta \mathcal{G}_{\text{meso}} / \delta h$ [eqn (36)] is shown as a function of uniform liquid layer thickness for $p = 0.1$. Fig. 6(a) displays the associated energy $f(h) - ph$. The respective thin lines give the case $p = 0$. According to eqn (36) a steady film

[¶] It should be kept in mind, that at constant supersaturation p the volume V^* and thus also the radius R^* of the critical nucleus are unknown functions of the softness s . In consequence, the ratios ℓ_{ec}/R^* and $\ell_{ec}/\sqrt[3]{V^*}$ can not be assumed to be $\sim \sqrt{s}$ in such a scenario.

state may only exist if the supersaturation is balanced by the Derjaguin pressure, leading to

$$-\Pi(h_0) = \frac{p}{C_\theta}, \quad \text{i.e.,} \quad h_\pm = \left[\frac{C_\theta}{2p} \left(1 \pm \sqrt{1 - 4 \frac{p}{C_\theta}} \right) \right]^{\frac{1}{3}}. \quad (37)$$

Hence, two different steady film states may exist depending on the value of p , controlled by the relative humidity r_H . The adsorption layer height h_- represents the dry substrate state and corresponds to a minimum in the energy $f(h) - ph$, i.e., it is linearly stable [cf. Fig. 6(c)]. Note, that, as h_- changes with p , the value of $f(h_-)$ changes as well resulting in turn in an increased substrate–vapor interface energy, according to the consistency condition (20).

From eqn (37) it is found, that in the limit $p \rightarrow 0$ the liquid layer thickness either diverges to $h_+ \rightarrow \infty$ or becomes $h_- = 1$, i.e., $h_- = h_a$ in dimensional terms. From there, the two flat film states asymptotically follow $h_- \approx 1 + p/3C_\theta$ and $h_+ \approx (C_\theta/p)^{1/3}$. Increasing the supersaturation to $p > 0$ the pressure is correspondingly shifted while the energy is tilted by the linear term $-ph$. This results in a second zero crossing of the pressure, i.e., an additional maximum of the energy, associated with h_+ . The latter is hence unstable and represents a threshold similar to a nucleus but for uniform film states, that is, every uniform film of thickness $h > h_+$ grows by condensation while for $h < h_+$ it shrinks by evaporation until the dry state h_- is reached. As p increases further, h_- and h_+ approach each other until they finally meet and vanish in a saddle-node bifurcation at $p_c = -\Pi_{\text{min}} = C_\theta/4$ where $h_\pm = \sqrt[3]{2}$ [eqn (37)] as shown in Fig. 6(c). For $p > -\Pi_{\text{min}}$ the Derjaguin pressure cannot compete with the supersaturation any more and nothing prevents the vapor from condensing into the liquid film.

3.2 Critical nuclei

3.2.1 Numerical approach and parameters. The mesoscopic model is now utilized to explore the critical nuclei in the regime of intermediate elasticity by numerically solving eqn (32) and (33). To this end, the open source C++ library Oomph-lib⁵⁸ is used to perform parameter continuation and time simulations. As discussed before, the critical nucleus is associated with a maximum of the Gibbs free energy \mathcal{G} . Thus, in the mesoscopic model one has to solve $\delta \mathcal{G}_{\text{meso}} / \delta h = \delta \mathcal{G}_{\text{meso}} / \delta \zeta = 0$. To do so numerically, by using a Newton solver, a proper starting state is required, which has to closely resemble the final solution. While in the rigid and liquid-like limit the macroscopic spherical cap profiles might be sufficiently suited, this is usually not the case in the intermediate elastic regime $0 < s < \infty$. Further the critical nucleus cannot be found using time simulations as it is associated with a maximum of the Gibbs free energy and thus unstable. Therefore, we make use of a trick; instead of an isothermal–isobaric ensemble, a canonical ensemble is considered. The drop state then corresponds to a minimum of the Helmholtz free energy and can thus be approached using time simulations. Thereby, the supersaturation is used as a Lagrange multiplier and adapts freely during the simulation to enforce conservation of an imposed volume V_0 . The stable steady drop found in the canonical ensemble



exactly corresponds to a critical nucleus in the isothermal-isobaric ensemble if the supersaturation is set to $p = \delta\mathcal{F}/\delta h$.

From this given critical nucleus, a continuation routine may be used to obtain the critical nucleus at a specific value of p . Such continuation techniques rely on the concept that small changes in a parameter, e.g., p , cause only small changes to a steady state in turn. Hence, if a steady state is known for a given parameter value p_0 , it is assumed to be well suited as initial condition to find the steady state at $p = p_0 + \Delta p$ if Δp is sufficiently small. This way, a steady state can be followed in parameter space.^{59–61}

For all results the parameters are fixed to the values

$$\begin{aligned} \gamma_{lv} &= 70 \times 10^{-3} \text{ N m}^{-1}, & \gamma_{sl} &= 48 \times 10^{-3} \text{ N m}^{-1}, \\ \gamma_{sv} &= 72 \times 10^{-3} \text{ N m}^{-1} \\ \rho &= 3.34 \times 10^{28} \text{ m}^{-3}, & k_B T &= 3.8 \times 10^{-21} \text{ kg m}^2 \text{ s}^{-2}, \\ r_H &= 1.055 \end{aligned} \quad (38)$$

if not stated otherwise. The adsorption layer thickness is $h_a = \sqrt{k_B T / \gamma_{lv}} = 2.33 \times 10^{-10} \text{ m}$. The corresponding values of the dimensionless parameters are $p \approx 0.0226$, $C_\theta \approx 2.2$ and $\sigma \approx 0.6857$. Note, that in this setting a steady drop on a rigid substrate exhibits $\theta_Y = 70^\circ$ and $R^*/h_a \approx 83$.

3.2.2 Consistency in the rigid and liquid limit. To validate our numerical results, first, the mesoscopic pendant of the macroscopic radius-dependent energy $\mathcal{G}_{\text{macro}}(R)$ [eqn (16)] is calculated for comparison. In the mesoscopic picture, the base radius R of a steady drop, i.e., a critical nucleus, is not known *a priori*. However, the macroscopic calculations in the rigid and liquid-like cases provide reasonable estimates also for the elastic regime, since R is assumed to transit monotonically between these two limits. Since there is no sharp three phase contact line in the mesoscopic description, the base radius is instead defined by the position R of maximal curvature of the liquid–vapor interface, i.e., $\kappa(h + \xi)|_{r=R} = \max[\kappa(h + \xi)]$ (cf. Fig. 5), which is equivalent to $\Pi(h)|_{r=R} = \min[\Pi(h)]$. It is thus encoded in the profiles h and ξ such that $\mathcal{G}_{\text{meso}}[h, \xi]$ can be seen as $\mathcal{G}_{\text{meso}}(R)$. Note, that the adsorption layer height h_- specifies a lower bound for the liquid layer thickness h , which in turn imposes a restriction to the minimal critical nucleus size $\min(R^*) \sim h_-$, in contrast to the macroscopic picture where no such limit exists. This restriction in turn sets a critical supersaturation p_c , since $R^* \sim p^{-1}$, beyond which no steady nucleus states are possible anymore. The energy $\mathcal{G}_{\text{meso}}(R)$ can be calculated in two different ways:

(1) Quasi-static relaxation: in the first method, we consider the dynamics of a drop state as given by eqn (32) and (33) using a very small transfer mobility m such that all hydrodynamic relaxation processes due to capillarity and wettability (the conserved part of the dynamics) take place much faster than the exchange of mass between the phases. Starting from the critical nucleus state, the liquid height profile h is disturbed using white noise with a small positive or negative mean to nudge condensation or evaporation, respectively. While the drop then slowly shrinks or grows, the base radius and energy

are calculated. Due to the very slow mass transfer, the drop is considered quasi-static during the process, which allows for $\mathcal{G}_{\text{meso}}(R)$ to be faithfully recovered.

(2) Continuation: in the second method, continuation is used to trace the critical nucleus state over a range of p . As the size of the critical nucleus is $R^*(p) \sim p^{-1}$, a continuation in p effectively corresponds to a continuation in R^* . Inserting the p values from the continuation into eqn (24) and (25) along with the corresponding profiles $h^*(r;p)$ and $\xi^*(r;p)$ gives the nucleation energy barrier as a function of supersaturation or base radius $\mathcal{G}_{\text{meso}}[h^*(r;p), \xi^*(r;p); p] \rightarrow \mathcal{G}_{\text{meso}}^*(p) \Leftrightarrow \mathcal{G}_{\text{meso}}^*(R)$. However, right now we are not looking for the energy barrier $\mathcal{G}_{\text{meso}}^*(R)$ but for $\mathcal{G}_{\text{meso}}(R)$, the two of which differ only by the value of p used in the calculation, at otherwise fixed parameters. Basically we ask: How does the energy of the critical nucleus characterized by h^* and ξ^* look like, if we evaluate it at another value of p than the one at which it is a steady state? From eqn (24) and (25) it is seen, that the difference in $\mathcal{G}_{\text{meso}}[h, \xi; p]$ caused by a change Δp is given by

$$\mathcal{G}_{\text{meso}}[h, \xi; p] - \mathcal{G}_{\text{meso}}[h, \xi; p + \Delta p] = 2\pi \int \Delta p (h - h_-) r dr. \quad (39)$$

Hence, the energy barriers $\mathcal{G}_{\text{meso}}^*[h^*(r;p), \xi^*(r;p); p]$ obtain for a set of values p during the continuation can be mapped to an arbitrary value \tilde{p} to obtain

$$\begin{aligned} \mathcal{G}_{\text{meso}}[h^*(r;p), \xi^*(r;p); \tilde{p}] &= \mathcal{G}_{\text{meso}}^*[h^*(r;p), \xi^*(r;p); p] \\ &+ 2\pi \int (p - \tilde{p})(h - h_-) r dr. \end{aligned} \quad (40)$$

Fig. 7 shows $\mathcal{G}_{\text{meso}}$ as a function of drop radius in the liquid limit (blue), the rigid limit (red) and for an intermediate elastic case (purple). Both described methods are compared to the macroscopic result. While the mesoscopic values obtained by

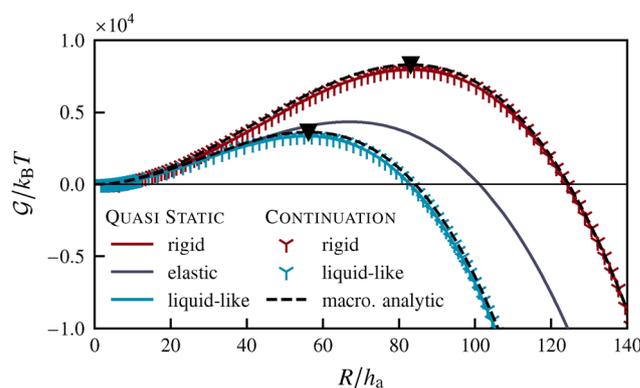


Fig. 7 Comparison of the macroscopic energy $\mathcal{G}_{\text{macro}}$ and mesoscopic energy $\mathcal{G}_{\text{meso}}$ as functions of the base radius R . The macroscopic energies are obtained analytically and plotted as dashed lines for the liquid-like (blue) and rigid (red) limit respectively. The mesoscopic energies are calculated using quasi-static time simulations (1st method, solid lines) and continuation (2nd method, Υ symbols). The critical radii and the energetic maxima are indicated by the \blacktriangledown symbols. The mesoscopic model is also used to capture the regime of intermediate elasticity, here the quasi-static method is used for $s = 10^5$ (dark purple curve).



continuation (γ symbols) agree very well with the ones obtained by the quasi-static approach (solid lines), both are slightly smaller than the macroscopic analytical predictions (black dashed). This results from the differences between the macroscopic and mesoscopic nucleus profiles in the contact line region. More importantly, the positions of the energy maxima, *i.e.*, the critical radii R^* (marked by \blacktriangledown), are correctly recovered. The overall agreement between macroscopic and mesoscopic model is quite satisfactory, allowing us to use the latter for exploring the critical nucleus characteristics in the elastic regime. The purple line in Fig. 7 shows the energy as obtained by the first method for an exemplary intermediate softness $s = 10^3$ and lies between the rigid and liquid-like limits, as expected.

3.2.3 Influence of supersaturation and elasticity. Key to the investigation of the nucleation probability are the critical nuclei, *i.e.*, the steady states corresponding to the maxima in Fig. 7. The corresponding results obtained from the continuation in supersaturation p as explained in Section 3.2.2, are shown in Fig. 8(a), giving the volume as a function of p on a log-log scale. The stable and unstable flat film states h_- and h_+ discussed in Section 3.1 are given as black solid and dashed lines, respectively. The volumes are given by $V_{\pm} = \pi h_{\pm} L^2$. The volumes of the critical nuclei are shown for the rigid (red) and liquid (blue) limit. Thereby, the macroscopically obtained results (thin lines) [eqn (5) and (14)] are compared to the mesoscopically obtained ones (thick lines). The volumes are obtained by integration of the numerically determined thickness profiles, $V = \int_0^L 2\pi h r dr$. The volumes of all states, except for h_- , increase with decreasing supersaturation p . In the low p limit, *i.e.*, at large volumes, the macroscopic and mesoscopic critical nucleus states well agree and show the predicted scaling $V \sim p^{-3}$. As the nucleus size decreases (increasing p), the mesoscopic results deviate from the macroscopic predictions (see Section 3.2), approach $V_{\text{dry}} = \pi h_- L^2$, and eventually end in a pitchfork bifurcation, very close to the saddle-node bifurcation of the uniform states (\blacklozenge symbol). Note further, that the volumes of the mesoscopic states all depend on the system size L , since the adsorption layer, which is present in the macroscopically dry areas, contributes with a volume per unit area h_a . Therefore, we also provide in the inset Fig. 8(b) the effective condensed volume $V_{\text{eff}}^* = V^* - \pi h_- L^2$ for the mesoscopic states, *i.e.*, the volume above the adsorption layer. This measure is independent of system size.

Fig. 8(b) shows a better agreement of mesoscopic and macroscopic results that is maintained up to higher supersaturation. Only as $p_c = C_0/4$ is approached a clear deviation is visible. Linear stability analysis for an infinite domain size shows, that the bifurcation point where the branch of mesoscopic critical nuclei emerges coincides with the saddle-node bifurcation. For a finite domain, however, the bifurcation is shifted a bit along the h_+ branch. Most remarkably, this

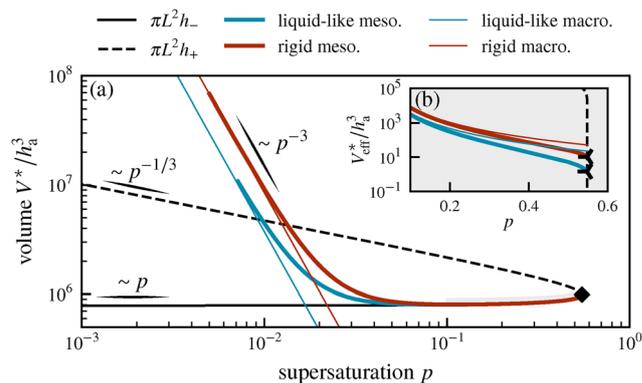


Fig. 8 Volume of the mesoscopic flat uniform steady film states (black) and of the critical nuclei in the rigid (red) and liquid-like (blue) limit as a function of the supersaturation p . (a) The total volume of the steady states, which in the mesoscopic picture includes the adsorption layer and therefore depends on system size. For small p the mesoscopic (thick lines) and macroscopic (thin lines) results agree and recover the scaling law $V \sim p^{-3}$. For larger p , the mesoscopic nuclei deviate from the macroscopic ones. All branches of mesoscopic states end at or near the saddle-node bifurcation of the film states (\blacklozenge symbol). (b) The inset gives the effective condensed volume, namely the volume above h_- , as a function of p in the range close to the bifurcation shaded gray in (a). The numerical domain was restricted to circular region of radius $L = 500h_a$.

bifurcation is then found at different positions (marked by \blackleftarrow) in the rigid and liquid-like limit. Again, the disagreement of macroscopic and mesoscopic model for $p \rightarrow C_0/4$ is assumably caused by the different nucleus shapes due to the diffuse contact region present in the latter, which gains impact as the nucleus size decreases.

In the same way, the nucleation barrier can be calculated from the mesoscopic profiles using eqn (24) and (25) and compared to the macroscopic prediction eqn (18). In Fig. 9 the energy barrier is shown as a function of supersaturation (using the same line styles as in Fig. 8). Again, both levels of description agree well in the small p limit, recovering the predicted power law $G_{\text{meso}}^* \sim p^{-2}$. The barrier increases with decreasing supersaturation in agreement with Section 3.2. Beyond that, the mesoscopic model estimates the energy barrier for $p \rightarrow p_c$ to be up to several orders of magnitude smaller

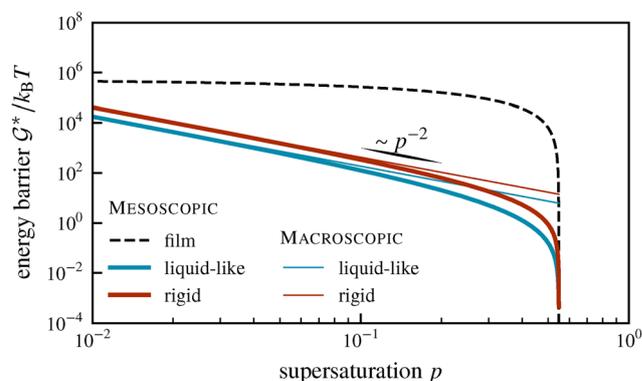


Fig. 9 Nucleation energy barrier G^* as a function of supersaturation p . The presented data are the same as in Fig. 8.

|| This difference is constant and does not depend on drop size. It therefore becomes less important as the drop size and the associated energies increase.



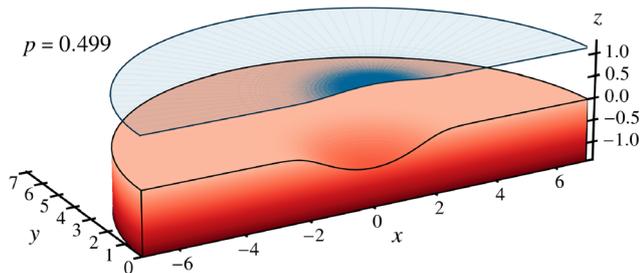


Fig. 10 Shape of a mesoscopic critical nucleus on an elastic substrate for $p \approx p_c = C_\theta/4$. The profiles h and ζ exhibit only slight modulations of $\mathcal{O}(h_a)$ and barely resemble spherical caps.

than the macroscopic value. This indicates, that the CNT, *i.e.*, the employed macroscopic model, strongly underestimates the nucleation probability close to the critical point. In Fig. 10 a mesoscopic critical nucleus on a soft substrate is shown for $p \approx p_c$. At $p_c = C_\theta/4$ the mesoscopic nucleation energy barrier even vanishes, such that the vapor condenses uncontrollably into the liquid phase for $p > p_c$. The dimensionless critical supersaturation $p_c = C_\theta/4$ translates to the critical relative humidity

$$\begin{aligned} r_{\text{H}}^c &= \exp\left(\frac{5}{6} \frac{\gamma_{\text{sl}} + \gamma_{\text{lv}} - \gamma_{\text{sv}}}{\rho \gamma_{\text{lv}} h_a^3}\right) \\ &= \exp\left(\frac{5}{6} \sqrt{\frac{\gamma_{\text{lv}}}{k_{\text{B}} T} \frac{\gamma_{\text{lv}} + \gamma_{\text{sl}} - \gamma_{\text{sv}}}{\rho k_{\text{B}} T}}\right), \end{aligned} \quad (41)$$

which for the values given in eqn (38) is $r_{\text{H}}^c \approx 3.6553$.

Finally, the mesoscopic model is used to investigate the influence of elasticity on the nucleation probability. Once again, continuation is employed, however, this time we explore the substrate softness ℓ_{ec}/R^* at fixed supersaturation p . The resulting energy barrier is displayed in Fig. 11. With the transition from the rigid to the liquid-like limit, *i.e.* with increasing softness, the energy barrier decreases by a factor greater than 2. This decrease in the energy barrier is amplified through the Boltzmann exponent [eqn (3)], and may therefore strongly affect the nucleation probability and, consequently,

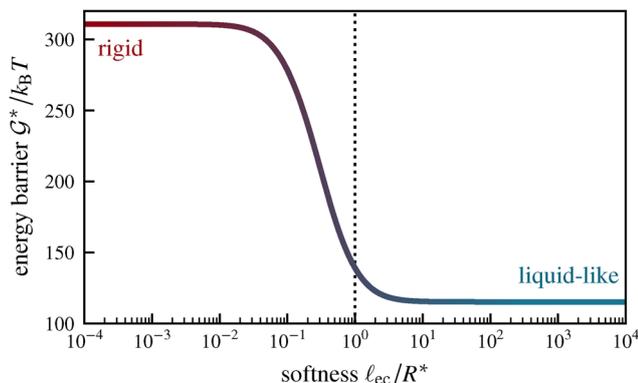


Fig. 11 Threshold energy as a function of substrate softness at fixed supersaturation $p = 0.1$. The energy barrier decreases with increasing softness, resulting in a strongly increased nucleation probability. Note, that the transition takes place at about $\ell_{\text{ec}} \sim R^*$.

the observed droplet density, (qualitatively) explaining recent observations in ref. 31. Note that the transition occurs approximately when $R^* \sim \ell_{\text{ec}}$.

4 Conclusion

Recent experiments showed that the nucleation density of dew is strongly affected by the softness of the elastic substrate controlled by the crosslinking ratio of a gel. The nucleation probability can be predicted as a Boltzmann factor and is therefore governed by the energy barrier \mathcal{G}^* given by the critical nucleus. This barrier in Gibbs free energy has been calculated in the macroscopic picture in both, the rigid and the liquid-like limit. For the given interface energies the nucleation energy in the liquid-like limit is about half the one in the rigid limit. To further explore the regime of intermediate elasticity, a mesoscopic gradient dynamics model has been employed to determine the energy as a function of supersaturation p and softness ℓ_{ec}/R^* . The macroscopic and mesoscopic models were found to agree in the limit of rigid and liquid substrates, as long as the critical nucleus is of sufficiently large volume, *i.e.*, when a relatively small supersaturation is considered. Both models predict a decrease in the energy barrier with increasing supersaturation, indicating an overall increased nucleation density at higher supersaturation. At large supersaturation, the macroscopic model considerably overestimates the energy barrier by several orders of magnitude as compared to the mesoscopic theory, resulting in an underestimated nucleation probability. This deviation is caused by the difference in nucleus shape; while mesoscopic nuclei exhibit diffuse contact regions that increasingly influence their shape as $R^* \rightarrow h_-$, the shape of macroscopic nuclei is (in the rigid and the liquid-like limit) invariant under changes in size, which is most likely not justified as microscopic scales are approached. Next, the change of the energy barrier with increasing substrate softness at fixed supersaturation has been investigated using the mesoscopic model. The decrease in the energy barrier has been shown to coincide with the transition of contact angles from Young (rigid) to Neumann (liquid-like) at $\ell_{\text{ec}} \sim R^*$. However, in the experiments the increase in drop number occurred in the range $10^{-7} \text{ m} < \ell_{\text{ec}} < 10^{-3} \text{ m}$ and since the critical nuclei are considered to be of nanometer size, it is still unclear why nucleation depends on the substrate softness at all. Beyond that, the critical nucleus volume is found to decrease with the substrate softness, allowing for the formation of more nuclei if the vapor access is limited, *e.g.*, by slow transport in the gas phase.

Finally, the nucleation energy barriers, even those predicted by the mesoscopic model, are about two orders of magnitude too large to satisfactorily explain the experimentally observed nucleation densities, even though the tendency with changing softness fits qualitatively. To appreciate the implications of such large energy barriers, we consider the resulting nucleation probabilities in the rigid and liquid-like regimes, for which the difference in energy barriers is about 50%. Using the



Boltzmann factor to estimate the nucleation probability would for $p = 0.1$ yield

$$\frac{p_{\text{rigid}}}{p_{\text{liq}}} \sim \exp\left(\frac{\mathcal{G}_{\text{liq}}^*}{k_{\text{B}}T} - \frac{\mathcal{G}_{\text{rigid}}^*}{k_{\text{B}}T}\right) < 10^{-60}. \quad (42)$$

A similar argument can be applied to the comparison of the energy barrier at different p , resulting in huge differences in the nucleation probability and indicating a strong dependence of the nucleation rate on the supersaturation, which could not be observed in the experiments. That being said, it was found that the mesoscopic nucleation energy barrier drastically decreases as p_c is approached and reaches $\mathcal{O}(1)$ at about $p \approx \frac{1}{2}$ which translates to $r_{\text{H}} \approx 3.2657$ or $r_{\text{H}}^0 = 1.2184$. The behavior at large p depends strongly on the nucleus shape and, in turn, on the functional form of the wetting potential $f(h)$ – many different forms are discussed in the literature.^{38–42,49,52–54,59} Further, the range of attractive microscopic interactions is determined by the rate at which f converges to zero as h increases. Increasing this range increases the width of the contact region, which in turn causes the energy barrier to fall off quicker as p_c is approached.

All of this points towards the incompleteness of the procedure to estimate the nucleation probability using only the Boltzmann factor. As discussed in ref. 31 the relation between the observed drops and the nucleation rate is much more intricate than that. On the one hand, the classical nucleation theory is a strongly approximated description that considers macroscopic concepts like interface energies. The validity of the latter is at least questionable in the context of microscopic nuclei of only a few particles in size, which renders the entire CNT obsolete. Even though the mesoscopic model accounts for the influence of microscopic interactions in terms of the wetting potential, the use of a more advanced model, *e.g.*, the dynamic nucleation theory (DNT) or the extended modified liquid drop (EMLD) model or both, might deliver more satisfying results. On the other hand, the experimental capabilities of capturing the nucleation process are strongly confined with regard to spatial as well as temporal resolution, both of which are of importance. In consequence, it cannot be ruled out that other physical processes are interfering. In particular, the halted nucleation of new drops in the dry regions of the initial breath figure is caused by the formation of a saturated diffusive boundary layer close to the substrate,^{24,31} which requires to spatially resolve the vapor density. A suspected cause that might enhance this effect is the cloaking of drops by liquids leaking from the substrate. This would alter the droplet shape and interface energy and therefore explain the discrepancy between experiments and theory. In addition the coarsening of drops was found to be suppressed on softer substrates both experimentally,²⁶ and theoretically³⁰ resulting in an increased drop density in turn. Finally, even though contaminants and impurities were ruled out as an additional source of nucleation in the experiments, there might still be microscopic heterogeneities present at the substrate surface, *e.g.*, due to the molecular structure of the polymer network, which affect the

nucleation rate. The impact of such effects is largely unknown and may be subject of future investigation.

Author contributions

Christopher Henkel: conceptualization, methodology, software, data curation, validation, formal analysis, investigation, visualization, writing – original draft, project administration; Ambre Bouillant: conceptualization, methodology, validation, formal analysis, investigation, writing – original draft; Jacco H. Snoeijer: conceptualization, methodology, writing – review & editing, supervision, funding acquisition; Uwe Thiele: conceptualization, methodology, writing – review & editing, supervision, project administration, funding acquisition.

Conflicts of interest

There are no conflicts to declare.

Data availability

The data presented in this article, including source codes of simulations, data set, data processing and plotting routines, are available *via* a Zenodo repository DOI: <https://doi.org/10.5281/zenodo.16792688>.

Appendices

A Temperature-induced condensation

The threshold of phase transition, *i.e.*, saturation, can be predicted by the Clausius–Clapeyron relation. This relation is, however, often corrected to match experiments. For instance, the Rankine law introduces empirical constants to capture the temperature dependence of latent heat, while the Arden-Buck law further accounts for water vapor non-idealities over a wide temperature range.⁶² We adopt the latter semi-empirical law, which is widely used in meteorology and engineering for its accuracy and practicality

$$p_{\text{sat}}(T) = a \exp\left[\left(b - \frac{T}{c}\right)\left(\frac{T}{d + T}\right)\right], \quad (43)$$

with T in °C and p in kPa and the empirical constants $a \approx 0.61121$ kPa, $b \approx 18.678$, $c \approx 234.5$ °C and $d \approx 257.14$ °C which are valid for $T > 0$ °C. For example, fixing the chamber humidity to $r_{\text{H}}^0 = 0.9$ at the roof and cooling the gel from 20 °C to 5 °C, the relative humidity in the immediate vicinity of the substrate is $r_{\text{H}} \approx 2.41$.

B Classical nucleation theory

The transition of a particle from an initial phase to another one may occur spontaneously only if that process is associated with a decrease in free energy. This condition must be met also in the context of nucleation in order for a new phase to spontaneously emerge and grow. The formation of the latter, however, is always accompanied by the creation of an interface (with the



surrounding initial phase), which represents an energy penalty. Assuming the new cluster to adapt a shape that minimizes the surface to volume ratio (provided the material is able to do that) the energy penalty is minimized as well. Since this ratio usually decreases further with increasing volume, the decrease in free energy per particle entering the new phase eventually predominates the penalty associated with the interface created in the same course. The minimal structure at which that happens corresponds to an energetic maximum and is referred to as a nucleus. It is these nuclei that initiate the formation of a new phase, once the associated energy barrier is overcome. In other words, the nucleus corresponds to a steady yet unstable threshold state, meaning that every smaller structure decays and every larger structure grows. The exact form of the governing energy and thus the characteristics of the nucleus crucially depend on the considered scenario. Two general cases are distinguished:

Homogeneous nucleation

A homogeneous initial phase, consisting of only one particle type, is considered. Due to thermal fluctuations these particles occasionally form small clusters of a new phase, that eventually start growing spontaneously if they exceed a critical size or particle number. In other words, these clusters of the same particle type may serve as nuclei. The energy penalty is exclusively governed by the interface energy between the initial and new phase and a lower bound may be estimated by assuming the nucleus to take a spherical shape.

Heterogeneous nucleation

The initial state is assumed heterogeneous in a sense that particles of different type may be present in some form ranging from microscopic impurities up to macroscopic structures (e.g. a solid substrate). If the interaction of the nucleating particle type with another type (expressed in terms of interface energies) is stronger than the interaction with its own type, nucleation is energetically favored wherever that other type is present. An example are the considered breath figures, where water vapor condenses to the liquid state at the surface of a cooled substrate. The energy penalty is then given by the interplay of interface energies between all the various phases.

The bulk energy gain associated with the nucleation is given by the difference in Gibbs free energy, and thus by the difference in chemical potentials, between initial and final state,^{18,45–48} implying constant temperature T , particle number N and external pressure p .** In the following we consider a small region in the immediate vicinity of the substrate such that the temperature in the gas phase is approximately constant

** In view of the experiments in ref. 31 the assumption of conserved particle number seems rather unjustified since the system has access to an infinite particle reservoir. In fact, it would be more convenient to consider fixed volume V and chemical potential μ instead. In other words, the system represents a realisation of a grand canonical ensemble and is driven by minimization of the corresponding grand canonical potential Ω (or Landau potential). It was shown, though, that the difference in grand potential associated with nucleus formation can be interpreted as a change in Gibbs free energy and is related to the change in Helmholtz free energy^{20,45,63,64} (see Appendix B.1).

and equal to the temperature of the substrate. The chemical potentials μ_ℓ, μ_v of the liquid and vapor phase can be quantified either by employing a real gas theory, e.g. by considering a van der Waals gas, and performing a standard Maxwell construction or by assuming the vapor to behave like an ideal gas and fixing the chemical potential and particle density in the liquid. Following the latter route, the vapor obeys the corresponding equation of state $pV = Nk_B T$ and its chemical potential is

$$\mu_v = k_B T \ln \left(\Lambda^3 \frac{N}{V} \right), \quad (44)$$

with Boltzmann constant k_B and the thermal wavelength Λ , i.e. the de Broglie wave length at thermal energy. Note, that the chemical potential is a function of temperature and pressure $\mu(T, p)$ via the equation of state. Consequently, chemical potential and pressure are not independent variables in an isothermal process. At equilibrium in an isothermal situation, the change in chemical potential associated with a change in pressure is determined by the Gibbs–Duhem relation

$$Nd\mu = Vdp. \quad (45)$$

Including the ideal gas law and after integrating we find for the vapor

$$\mu_v(p_v) - \mu_v(p'_v) = k_B T \ln \left(\frac{p_v}{p'_v} \right), \quad (46)$$

with p'_v being an arbitrary reference pressure. Assuming constant particle density in the liquid $\rho_\ell = N_\ell/V_\ell$ eqn (45) becomes

$$\mu_\ell(p_\ell) - \mu_\ell(p'_\ell) = \frac{V_\ell}{N_\ell} (p_\ell - p'_\ell). \quad (47)$$

Then, the liquid pressure and chemical potential are directly related via the constant particle density. The difference in chemical potentials between liquid and vapor phase results to

$$\begin{aligned} \Delta\mu &= \mu_\ell(p_\ell) - \mu_v(p_v) = \frac{V_\ell}{N_\ell} (p_\ell - p'_\ell) \\ &\quad - k_B T \ln \left(\frac{p_v}{p'_v} \right) + \mu_\ell(p'_\ell) - \mu_v(p'_v). \end{aligned} \quad (48)$$

Demanding phase coexistence at a specific saturation pressure p_v^{sat} , i.e. $\mu_\ell(p_v^{\text{sat}}) = \mu_v(p_v^{\text{sat}})$, the reference pressures have to be set to $p'_\ell = p'_v = p_v^{\text{sat}}$, leading to

$$\Delta\mu = \frac{V_\ell}{N_\ell} (p_\ell - p_v^{\text{sat}}) - k_B T \ln(r_H), \quad (49)$$

with the relative humidity $r_H = p_v/p_v^{\text{sat}}$. Fixing the chemical potential, and hence also the pressure, of the liquid to those of the vapor at saturation, i.e. $\mu_\ell = \mu_\ell(p_v^{\text{sat}})$ and $p_\ell = p_v^{\text{sat}}$, only the logarithmic term remains. If the gas phase is considered an ideal mixture of K species (e.g. water vapor in N_2) its total pressure p is the sum of all partial pressures p_i according to



Dalton's law $p = \sum_i^K p_i$. The Gibbs–Duhem relation then writes

$$V \sum_i d p_i = \sum_i N_i d \mu_i. \quad (50)$$

Allowing only one component, e.g. $i = v$, to condense into a liquid phase coexistence requires $\mu_\ell(p_{\text{sat}}) = \mu_v(p_v^{\text{sat}})$ where now $p_{\text{sat}} = p_v^{\text{sat}} + \sum_{i \neq v} p_i$ is the total pressure of the mixture at saturation of component v . In consequence, the reference pressures in eqn (48) have to be chosen differently, namely $p'_\ell = p_{\text{sat}}$ and $p'_v = p_v^{\text{sat}}$, yielding

$$\Delta \mu = \mu_\ell(p_\ell) - \mu_v(p_v) = \frac{V_\ell}{N_\ell} (p_\ell - p_{\text{sat}}) - k_B T \ln \left(\frac{p_v}{p_v^{\text{sat}}} \right). \quad (51)$$

According to classical thermodynamics the Gibbs free energy is given by $\mathcal{G} = \mathcal{F} + pV$ with Helmholtz free energy $\mathcal{F} = \sum_i^K \mu_i N_i - p_i V_i$, the externally imposed total gas pressure p and the total volume V . The Gibbs free energies of the coexisting liquid and gas phase (including vapor) state \mathcal{G} and the pure gas state \mathcal{G}' are given by

$$\begin{aligned} \mathcal{G}(T, N, p) &= \mathcal{F}(T, N, V) + pV \\ &= \mu_\ell N_\ell - p_\ell V_\ell + \sum_i^K (\mu_i N_i - p_i V_i) + pV, \end{aligned} \quad (52)$$

and

$$\begin{aligned} \mathcal{G}'(T, N, p) &= \mathcal{F}'(T, N, V') + pV' \\ &= \sum_i^K (\mu'_i N'_i - p'_i V'_i) + pV'. \end{aligned} \quad (53)$$

The energy difference then becomes

$$\begin{aligned} \Delta \mathcal{G} = \mathcal{G} - \mathcal{G}' &= \left[\mu_\ell N_\ell - p_\ell V_\ell + \sum_i^K (\mu_i N_i - p_i V_i) + pV \right] \\ &\quad - \left[\sum_i^K (\mu'_i N'_i - p'_i V'_i) + pV' \right] \\ &\stackrel{(1)}{=} \mu_\ell N_\ell - (p_\ell - p)V_\ell + \sum_i^K (\mu_i N_i - \mu'_i N'_i) \\ &\stackrel{(2)}{=} \mu_\ell N_\ell - (p_\ell - p)V_\ell + \mu_v N_v - \mu'_v N'_v + \sum_{i \neq v} (\mu_i - \mu'_i) N_i \\ &\stackrel{(3)}{=} (\mu_\ell - \mu_v) N_\ell - (p_\ell - p)V_\ell + \sum_i^K (\mu_i - \mu'_i) N_i \\ &\stackrel{(4)}{=} -(p_{\text{sat}} - p)V_\ell - N_\ell k_B T \ln \left(\frac{p_v}{p_v^{\text{sat}}} \right) \approx -N_\ell k_B T \ln \left(\frac{p_v}{p_v^{\text{sat}}} \right) \end{aligned} \quad (54)$$

For clarification the separate steps are explained: at (1) the volume of the coexistence state is divided into a liquid and a gas part $V = V_\ell + V_g$. Further, all components of the gas mixture

share the same volume $V_i = V_g = V - V_\ell$ and $V'_i = V'$, such that the respective partial pressure terms cancel with eqn (50). At (2) the particle conservation in the gas phase $N_i = N'_i$ is used for all components of the mixture $i \neq v$. At (3) the global particle conservation of species v is used, i.e. $N'_v = N_\ell + N_v$. At (4) eqn (50) is used again to eliminate the sum since $dp = 0$. Note, that not only the total pressure p but also the partial pressures $p'_i = p_i$ are held constant in the considered system. Hence, since chemical potential and pressure are not independent in an isotherm $\mu'_i = \mu_i$. The difference in chemical potentials is expressed using eqn (51) and finally the pressure difference commonly neglected.^{46,47} Finally, the energy gap is exclusively governed by the difference in chemical potentials. For $r_H > 1$, i.e. $p_v > p_v^{\text{sat}}$, the difference in the Gibbs free energy is always negative such that a transition of particles from vapor to condensed state is always favorable. As mentioned above, this condition, referred to as supersaturation, is a prerequisite for spontaneous nucleation to occur and the new phase to grow. Finally, the change in Gibbs free energy associated with the creation of a liquid cluster of arbitrary shape from its own vapor in contact with a substrate is found by adding the interface energy penalties^{18,46–48}

$$\Delta \mathcal{G} = \gamma_{lv} A_{lv} + \gamma_{sl} A_{sl} + \gamma_{sv} (A_{sv} - A'_{sv}) - \rho_\ell k_B T \ln(r_H) V_\ell, \quad (55)$$

with γ_{ij} and A_{ij} respectively being the energy and area of the liquid–vapor (lv), substrate–liquid (sl) and substrate–vapor (sv) interfaces and the prime referring to the pure gas state. This equation is the starting point for the modeling approach and corresponds to eqn (1).

B.1 Equality of Gibbs free energy and Landau potential barrier. The difference in Landau potential (grand canonical potential) between the state of coexisting liquid and gas phase (including vapor) Ω and the pure gas state Ω' is given by

$$\begin{aligned} \Delta \Omega = \Omega - \Omega' &\stackrel{(1)}{=} \left[\mathcal{F} - \mu_v N_\ell - \sum_i^K \mu_i N_i \right] - \left[\mathcal{F}' - \sum_i^K \mu'_i N'_i \right] \\ &\stackrel{(2)}{=} \left[\mu_\ell N_\ell - p_\ell V_\ell + \sum_i^K (\mu_i N_i - p_i V_i) - \mu_v N_\ell - \sum_i^K \mu_i N_i \right] \\ &\quad - \left[\sum_i^K (\mu'_i N'_i - p'_i V'_i) - \sum_i^K \mu'_i N'_i \right] \\ &\stackrel{(3)}{=} (\mu_\ell - \mu_v) N_\ell - (p_\ell - p)V_\ell + \sum_i^K (p'_i - p_i) V \\ &\stackrel{(4)}{=} -(p_{\text{sat}} - p)V_\ell - \rho_\ell k_B T \ln \left(\frac{p_v}{p_v^{\text{sat}}} \right) V_\ell \approx -\rho_\ell k_B T \ln \left(\frac{p_v}{p_v^{\text{sat}}} \right) V_\ell. \end{aligned} \quad (56)$$

To clarify, the separate steps are explained: at (1) the Landau potentials of the final and initial state are expressed in terms of the Helmholtz free energy as $\Omega = \mathcal{F} - \mu N$. Thereby, the last term refers to the Gibbs free energy of a pure gas state with the same total particle number of the components and at the same



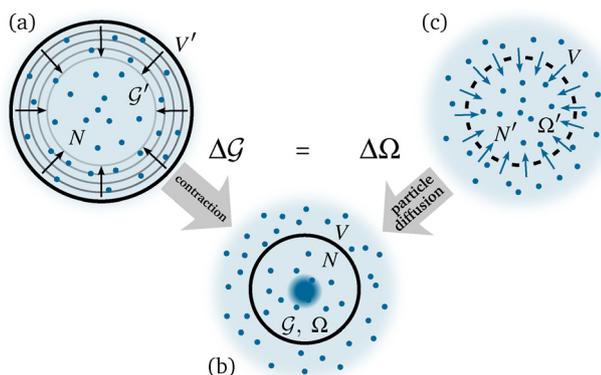


Fig. 12 Visualization of a nucleation process from two different perspectives. (a) Consider a fixed particle number N of vapor particles in an initial volume V' . As the condensation of vapor into the liquid state takes place the pressure p is held constant and the volume occupied by the particles reduces to V . The energy difference is given by the change in Gibbs free energy $\Delta G = G - G'$. (c) Consider a fixed volume V including an initial number of vapor particles N' . As the condensation of vapor into the liquid state takes place the chemical potential μ is held constant and particles diffuse into the area until N is reached. The energy difference is given by the change in grand potential $\Delta\Omega = \Omega - \Omega'$. If the final state (c), *i.e.*, N and V , is the same in both scenarios, the change in Gibbs energy equals the change in grand potential $\Delta G = \Delta\Omega$ under certain assumptions as discussed in the main text.

fixed chemical potentials μ_i . At (2) the Helmholtz free energy is expressed as $\mathcal{F} = \sum_i^K \mu_i N_i - p_i V_i$. At (3) the fixed volume $V = V'$ and the shared gas volume $V'_i = V'$ and $V_i = V - V_\ell$ is used. At (4) eqn (50) is used to eliminate the sum since $dp = 0$. The difference in chemical potentials is expressed using eqn (49) and the pressure difference is neglected, as is common practice.^{46,47} This result is the same as eqn (54), hence $\Delta\Omega = \Delta G$ in this case (Fig. 12).

B.2 Binary mixture of water vapor in N_2 . In the case of a binary mixture, *e.g.* water vapor in N_2 as used in the experiments in Ref. 31, the change in Gibbs free energy can directly be calculated using the chemical potential of an ideal gas (44). The Gibbs free energy of a binary mixture coexisting with a liquid state is

$$\begin{aligned} G &= \mathcal{F} + pV = [\mu_\ell N_\ell - p_\ell V_\ell + \mu_v N_v - p_v V_v + \mu_{N_2} N_{N_2} - p_{N_2} V_{N_2}] \\ &\quad + pV \\ &= (\mu_\ell - \mu_v) N_\ell - (p_\ell - p_v - p_a) V_\ell + \underbrace{\mu_v N_{H_2O} + \mu_{N_2} N_{N_2}}_{G'} \end{aligned} \quad (57)$$

with $p = p_v + p_{N_2}$ being the constant imposed pressure and $V = V_\ell + V_g$ being the total volume with $V_g = V_v = V_{N_2}$. Further, conserved total particle number $N = N_{H_2O} + N_{N_2}$ as well as conserved particle numbers of the two species N_{N_2} and $N_{H_2O} = N_\ell + N_v$ are assumed. Enforcing equilibrium at $p_v = p_v^{\text{sat}}$ leads to

$$\begin{aligned} \frac{dG}{dN_\ell} &= \mu_\ell - \mu_v(p_v^{\text{sat}}) - (p_\ell - p_v^{\text{sat}} - p_{N_2}) / \rho_\ell = 0 \\ \rightarrow \mu_\ell &= \mu_v(p_v^{\text{sat}}) + (p_\ell - \underbrace{(p_v^{\text{sat}} + p_{N_2})}_{p_{\text{sat}}}) / \rho_\ell, \end{aligned} \quad (58)$$

with the liquid particle density $\rho_\ell = N_\ell/V_\ell$. Inserting into eqn (57) and using eqn (44) yields

$$\begin{aligned} G &= -\rho_\ell k_B T \ln\left(\frac{p_v}{p_v^{\text{sat}}}\right) V_\ell - \underbrace{(p_{\text{sat}} - p)}_{\approx 0} V_\ell + \underbrace{\mu_v N_{H_2O} + \mu_{N_2} N_{N_2}}_{G'} \\ \rightarrow \Delta G &= G - G' = -\rho_\ell k_B T \ln\left(\frac{p_v}{p_v^{\text{sat}}}\right) V_\ell \end{aligned} \quad (59)$$

Similarly, using the Landau potential

$$\begin{aligned} \Omega &= \mathcal{F} - \mu N = [\mu_\ell N_\ell - p_\ell V_\ell + \mu_v N_v - p_v V_v + \mu_{N_2} N_{N_2} - p_{N_2} V_{N_2}] \\ &\quad - [\mu_{N_2} N_{N_2} + \mu_v (N_v + N_\ell)] \\ &= (\mu_\ell - \mu_v) \rho_\ell V_\ell - (p_\ell - p_v - p_{N_2}) V_\ell - \underbrace{(p_v + p_{N_2})}_{G'} V_\ell. \end{aligned} \quad (60)$$

Obviously $\Delta\Omega = \Delta G$.

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