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A self-powered and stretchable magnetic film for human–machine interface applications

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Developing stretchable, self-powered electronic interfaces for ambient energy harvesting is crucial for next-generation wearable electronics and human–machine interface applications. We present a stretchable magnetoelectric composite film comprising $\text{Ni}_{0.5}\text{Co}_{0.5}\text{Fe}_2\text{O}_4$ magnetic nanoparticles embedded in an Ecoflex matrix. The nanoparticles, synthesized *via* co-precipitation, exhibit a strong magnetic response, while Ecoflex ensures high stretchability and skin-mountable adaptability. The comprehensive structural, morphological, and magnetic analyses confirm the formation of a uniform and multifunctional film. The optimized device delivers a peak output voltage of ~ 8.3 V and a power density of 3.16 mW cm^{-3} under ambient magnetic fields, outperforming conventional soft nanogenerators. The films demonstrate excellent durability under repeated deformation and maintain stable performance at tensile strains up to $\sim 315\%$. Integration into a soft wearable platform enables real-time gesture recognition, with distinct voltage signals for finger bends and gestures under low-intensity magnetic fields. This work highlights the potential of magnetic/Ecoflex-based nanogenerators in self-powered, wearable, stretchable electronics, smart prosthetics, and intelligent human–machine interfaces.

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1. Introduction

Integrating multifunctional, flexible, and stretchable electronics into wearable technologies has accelerated the development of next-generation human–machine interfaces (HMIs), soft robotics, healthcare monitoring, smart prosthetics, and interactive electronics.^{1–5} These advancements highlight the demand for skin-compatible, wearable, self-powered systems capable of real-time energy harvesting and signal detection with high mechanical adaptability.^{6–9} Artificial sensory systems mimicking skin functions and responding to diverse stimuli have gained increasing attention.^{10,11} A key challenge for wearable electronic devices is the absence of efficient and flexible power sources, as conventional batteries remain bulky and prone to leakage. To overcome this, researchers have advanced self-powered devices such as triboelectric nanogenerators (TENGs), piezoelectric nanogenerators (PENGs), and magnetoelectric (ME) nanogenerators. A V_2CT_x MXene/silicone-based TENG has been reported with 400% stretchability and a power density of 19.75 W m^{-2} , enabling real-time sign-language interpretation.¹² Design strategies for wearable and implantable TENGs have also been highlighted for advancing HMI devices.¹³ Polyurethane/ BaTiO_3 -based PENGs achieved 336% stretchability with an output of 31 V, successfully charging capacitors from human motion.¹⁴ Beyond mechanical

sources, ME nanogenerators based on ferromagnetic–ferroelectric core–shell nanofibers have demonstrated high AC magnetic sensitivity (760 V/T).¹⁵ By uniquely harvesting ambient magnetic noise through strain-mediated coupling, ME devices enable wireless power supply and magnetic sensing, making them promising for IoT systems and skin-conformable wearables.^{16–19}

HMI systems enable intuitive interactions between humans and machines, soft robotics, advancing wearables, and healthcare. They provide flexibility, real-time feedback, and energy efficiency, with soft sensors standing out for their adaptability, stretchability, and skin-like responsiveness. These sensors operate through various transduction principles, including capacitive mechanisms (*e.g.*, organo-hydrogel films²⁰ and Au-PDMS flexible films²¹), piezoelectric mechanisms (*e.g.*, ZnO-PVDF composite films²² and ZnO-PDMS stretchable films²³), and triboelectric mechanisms (*e.g.*, flexible PTFE films²⁴ and nitrocellulose membrane films²⁵). TENGs and PENGs enable energy harvesting but rely on continuous deformation, limiting wearable stability. In contrast, ME nanogenerators harvest ambient magnetic noise without deformation, offering wireless and self-powered operation. They are promising for health-monitoring patches, biosensors, and smart textiles, though their use in HMIs is still limited.^{26,27} Conventional ceramic-based ME composites are rigid, while emerging polymer-based systems provide stretchable, lightweight, and skin-conformable alternatives for next-generation wearable HMIs.

To address these challenges, we fabricated a stretchable ME nanogenerator film by embedding $\text{Ni}_{0.5}\text{Co}_{0.5}\text{Fe}_2\text{O}_4$

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nanoparticles in an Ecoflex matrix. The spinel ferrite $\text{Ni}_{0.5}\text{Co}_{0.5}\text{Fe}_2\text{O}_4$ exhibits an excellent magnetostrictive response, chemical stability, and high resistivity.²⁸ Ecoflex, a silicone-based elastomer, offers an ultralow modulus, high strain, and biocompatibility and is widely used in soft robotics and wearable sensors for its flexibility and moisture resistance.²⁹ Unlike hydrogels or liquid metals, Ecoflex withstands large strain cycles while maintaining viscoelastic and dielectric stability, making it an ideal host for rigid fillers. However, ME composites based on Ecoflex remain underexplored. The resulting $\text{Ni}_{0.5}\text{Co}_{0.5}\text{Fe}_2\text{O}_4$ /Ecoflex film combines elasticity and durability with efficient low-frequency magnetic energy harvesting, a resource largely untapped by TENGs and PENGs.

In this work, we have designed a highly stretchable and self-powered ME composite film by embedding $\text{Ni}_{0.5}\text{Co}_{0.5}\text{Fe}_2\text{O}_4$ nanoparticles into a soft Ecoflex matrix for skin-compatible magnetic field sensors, self-powered HMIs, and energy harvesting in wearable healthcare. Combining ferrite's magnetic properties with Ecoflex's stretchability and biocompatibility ensures stable, deformation-free operation under bending or stretching. With optimized power density, these films enable real-time applications such as self-powered biosensors, smart patches, and gesture-based interfaces for continuous health monitoring.

2. Experimental section

2.1. Materials used

Nickel nitrate hexahydrate [$\text{Ni}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$, Sigma-Aldrich, India], cobalt nitrate hexahydrate [$\text{Co}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$, Sigma-Aldrich, India], iron nitrate nonahydrate [$\text{Fe}(\text{NO}_3)_3 \cdot 9\text{H}_2\text{O}$, Sigma-Aldrich, India], and sodium hydroxide pellets [NaOH, Loba Chemie, India] were used as the initial materials. Also, EcoflexTM was obtained from Smooth-On Inc., USA. All chemicals were used as received without additional purification. Deionized (DI) water, sourced from double-distilled water, was used as the solvent for precursor salts during the synthesis of $\text{Ni}_{0.5}\text{Co}_{0.5}\text{Fe}_2\text{O}_4$ nanoparticles.

2.2. Synthesis of $\text{Ni}_{0.5}\text{Co}_{0.5}\text{Fe}_2\text{O}_4$ nanoparticles and the Ecoflex film and device fabrication

$\text{Ni}_{0.5}\text{Co}_{0.5}\text{Fe}_2\text{O}_4$ nanoparticles were prepared *via* co-precipitation following the reported literature.³⁰ Stoichiometric amounts of $\text{Ni}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$, $\text{Co}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$, and $\text{Fe}(\text{NO}_3)_3 \cdot 9\text{H}_2\text{O}$ were dissolved in 20 mL of DI water, then combined and stirred magnetically at room temperature for 8 h at 400 rpm using a magnetic stirrer (REMI-1MLH, India). The solution mixture was kept under magnetic stirring to obtain a homogeneous solution. Then, the mixture was heated to 85 °C, and 1 M NaOH was added dropwise to achieve a pH of 12. A dark brown precipitate formed, which was further stirred at 85 °C for 6 hours until the completion of the reaction. This precipitate was separated by centrifugation, washed twice with DI water and ethanol, and dried in an oven at 200 °C for 10 h. The centrifugation was carried out at 10000 rpm for 10 minutes for each washing medium. We used a centrifuge machine

(MICROSIL, India) for this process. The precipitate was washed with DI water and acetone for the first two times. Thereafter, ethanol was utilized twice for washing. Then the precipitate was collected and dried further. The resulting nanoparticles were then subjected to further characterization and analysis. To prepare the Ecoflex solution, EcoflexTM 00-50's part A and part B were combined in a 1:1 ratio in 20 mL plastic vials. For the EcoflexTM- $\text{Ni}_{0.5}\text{Co}_{0.5}\text{Fe}_2\text{O}_4$ composite films, $\text{Ni}_{0.5}\text{Co}_{0.5}\text{Fe}_2\text{O}_4$ nanoparticles were incorporated into the Ecoflex solution at 0.6 wt% and 2 wt% in a glass beaker by simple manual mixing with a wooden spatula until uniform distribution was achieved. The mixtures were then drop-cast onto Petri dishes and dried at RT for 24 h. The resulting flexible and stretchable films (NC1 and NC2) were carefully peeled from the Petri dishes and used for further characterization. The steps involved in film preparation are shown in Fig. S1 (SI). The dimensions of both films were maintained with a tolerance of $2.5 (\pm 0.1) \times 1 (\pm 0.05) \text{ cm} \times 0.1 (\pm 0.01) \text{ cm}$. For the analysis and demonstration of energy harvesting and real-time applications, copper electrodes were attached to both sides of the top and bottom surfaces of the films. Fig. 1(a) illustrates magnetic field harvesting and HMI application using a stretchable magnetic Ecoflex film. Furthermore, the device was fabricated in a horizontal configuration with copper electrodes attached to the top and bottom surfaces of the film due to its glue and easy stickiness, enabling stable contact and reliable output measurement, and a complete set of copper electrode films are shown in Fig. S2 (SI).

2.3. Characterization techniques

The phase formation of the synthesized spinel ferrite $\text{Ni}_{0.5}\text{Co}_{0.5}\text{Fe}_2\text{O}_4$ was confirmed through X-ray diffraction (XRD) analysis using a diffractometer (Bruker D8 Advance) equipped with $\text{Cu-K}\alpha$ radiation ($\lambda = 1.540 \text{ \AA}$). Fourier-transform infrared (FTIR) spectroscopy was carried out using a NEXUS 870 instrument, covering the spectral range of 400–4000 cm^{-1} . Surface morphology was examined using a field-emission scanning electron microscope (FE-SEM, Thermo Fisher Apreo) and an analytical transmission electron microscope (analytical TEM). To assess the device performance, a custom-designed Helmholtz coil was fabricated using 3D printing technology (Pratham, Make3D.in). Each coil's base was 3D-printed using the PLA material with a diameter of 8 cm. A 0.5-mm-thick enameled copper wire was wound 25 times around each base to form a pair of identical coils. The enamel coating at the wire ends was stripped to ensure proper electrical connectivity. To achieve the maximum magnetic field at the center, the coils were positioned 4 cm apart. Both coils were connected in parallel to a variable 2.2 A current source, with the polarity configured to ensure the current in each coil flowed in the same direction, producing a magnetic field of 1.33 mT. Further details on the schematic experimental setup and the fabrication of the Helmholtz coil are given in Fig. S3(a)–(c) (SI). Strain–stress analysis of the films was carried out using a universal tensile testing machine (UTTM). The electrical response of the ME devices was measured using a digital oscilloscope (Tektronix, TBS 1000C series), allowing precise output voltage evaluation.



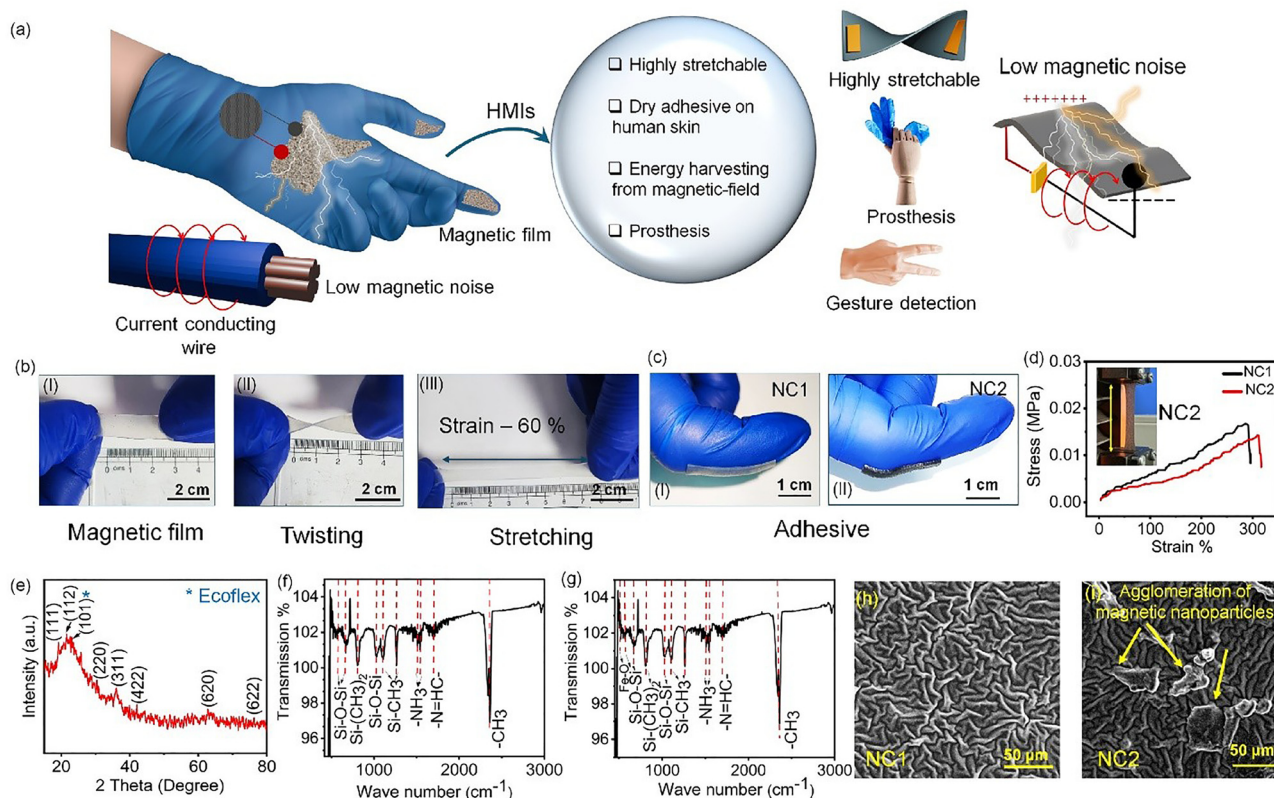


Fig. 1 (a) Magnetic field harvesting, an HMI application using a wearable and stretchable magnetic Ecoflex film. Digital images of the (b) flat, twisted, and stretched orientations of NC1 films. (c) adhesiveness of NC1 and NC2 on the glove. (d) stress–strain graph of NC1 and NC2 films (inset: digital image of the NC2 film with the UTM setup), (e) XRD pattern of the NC1 film, (f) FTIR spectrum of the NC1 film, and (g) FTIR spectrum of the NC2 film. FESEM images of (h) NC1 and (i) NC2 films.

3. Results and discussion

3.1. Structural, functional, and morphological analyses

The digital images of NC1 films in flat, twisted, and stretched orientations are shown in Fig. 1(b)(I), (b)(II), and (b)(III), respectively, demonstrating their mechanical flexibility. The digital image of the NC1 and NC2 films illustrating its adhesion to the glove is shown in Fig. 1(c). Similarly, the flat, twisting, and stretchable characteristics of the NC2 film are shown in Fig. S4(a) of the SI. For mechanical strength testing, both films with similar dimensions (25 mm × 10 mm × 1 mm) were mounted on a universal tensile testing machine, with a constant elongation rate of 5 mm per minute to ensure uniform deformation. The NC1 film exhibited a progressive increase in strain with applied stress, achieving a maximum elongation of ~291% of its original length before fracture, which occurred at ~295% beyond its peak elongation. The corresponding load at failure was 0.15 kgF, and the peak tensile strength was calculated as 0.167 MPa. In comparison, the NC2 film demonstrated a maximum elongation of ~311% and failed at ~317% elongation, with a breakdown load of 0.13 kgF and a peak tensile strength of 0.142 MPa. The stress–strain profiles of the NC1 and NC2 composite transducer films are shown in Fig. 1(d). The inset of Fig. 1(d) shows the digital image of the NC2 film during mechanical strength measurements. Similarly,

the digital image of straightness measurement for NC1 is shown in Fig. S4(b) (SI). Also, the Young's moduli of NC1 and NC2 are 4.9×10^{-5} MPa and 3.9×10^{-5} MPa, respectively. Furthermore, during the experimental procedures, both films were analyzed under strains of up to only 60%. These findings highlight the mechanical robustness and high strain tolerance of NC1 and NC2 films, underscoring their potential for use in flexible and stretchable electronic applications. The diffraction peaks of the embedded $\text{Ni}_{0.5}\text{Co}_{0.5}\text{Fe}_2\text{O}_4$ magnetic nanoparticles match the standard JCPDS cards (No. 74-2081) and (No. 22-1086) for NiFe_2O_4 and CoFe_2O_4 , respectively, confirming the successful formation of a pure $\text{Ni}_{0.5}\text{Co}_{0.5}\text{Fe}_2\text{O}_4$ ferrite phase³⁰ with a cubic crystal structure as shown in Fig. S4(c). Furthermore, Fig. 1(e) presents the XRD pattern of the NC1 films and a broad peak is observed at 22.4° , corresponding to the (101) plane of the Ecoflex matrix, consistent with the amorphous nature of silicone-based elastomers.²⁹ Also, the XRD pattern of the NC2 film is shown in Fig. S4(d) to distinguish the peaks of Ecoflex in the compositions. The HR-TEM image of $\text{Ni}_{0.5}\text{Co}_{0.5}\text{Fe}_2\text{O}_4$ nanoparticles is provided in the SI (Fig. S4(e)). The HR-TEM analysis revealed the crystalline nature of $\text{Ni}_{0.5}\text{Co}_{0.5}\text{Fe}_2\text{O}_4$ nanoparticles. The magnetic measurement of $\text{Ni}_{0.5}\text{Co}_{0.5}\text{Fe}_2\text{O}_4$ is shown in Fig. S4(f), and the nanoparticles are found to have ferromagnetic nature. FTIR spectroscopy of NC1 and NC2 was further conducted to verify the composite's chemical structure and bonding characteristics,



as shown in Fig. 1(f) and (g). The NC1 and NC2 films display characteristic stretching bands around 480 and 490 cm^{-1} , which are attributed to Fe–O stretching vibrations within the $\text{Ni}_{0.5}\text{Co}_{0.5}\text{Fe}_2\text{O}_4$ phase. Additional prominent peaks at 574, 654, 804, and 1015 cm^{-1} correspond to the Si–O–Si stretching vibrations, indicative of the siloxane characteristic of Ecoflex.²⁹ Peaks at 1257 and 787 cm^{-1} are assigned to Si–C stretching in Si–CH₃ and Si–(CH₃)₂ groups, respectively. Furthermore, the bands at 1509 and 1548 cm^{-1} are associated with the symmetric and asymmetric bending vibrations of –NH₃ groups, while a notable peak at 1704 cm^{-1} corresponds to the stretching vibration of imine groups (–HC=N–) in the film. A distinct absorption band at 2367 cm^{-1} is attributed to C–H stretching in the methyl groups of the Ecoflex matrix.³¹ The FE-SEM images of NC1 and NC2 films are shown in Fig. 1(h) and 1(i), respectively. From the FESEM analysis, NC1 and NC2 films contain magnetic nanoparticles uniformly embedded in the Ecoflex matrix. In the FESEM image of NC1, the nanoparticles are well dispersed within the bulk matrix and are not prominently visible on the surface, as shown in Fig. 1(h). In contrast, the NC2 film contains a higher wt% of magnetic nanoparticles, and some of these particles or their agglomerates are exposed at the surface, which appear as brighter features in the FESEM image, as shown in Fig. 1(i). The surface morphology impels the film's adherence to human

skin, which displays a textured structure reminiscent of human skin. The synthetic skin-like surface morphology enhances conformal contact with soft and irregular surfaces, such as human skin, by mimicking its flexible, stretchable, and adaptive properties, ensuring stable operation of wearable HMI devices during body movements. This morphology improves adhesion to the body's contours and maintains consistent contact for reliable sensor or electrode function.²⁹

3.2. Wireless power transmission analysis

A ME nanogenerator, utilizing nanoparticle–Ecoflex composites, was experimentally designed to efficiently harvest energy from low-intensity ambient magnetic fields, as illustrated in Fig. 2(a). A Helmholtz coil generated an alternating magnetic field of 1.33 mT at 50 Hz, and a DSO was utilized for the measurement of the device's output voltage, as shown in Fig. 2(b) and Fig. S3. The reorientation of magnetic domains causes magnetostrictive deformation of the spinel-structured $\text{Ni}_{0.5}\text{Co}_{0.5}\text{Fe}_2\text{O}_4$ nanoparticles when exposed to an external magnetic field. An alternating voltage signal is produced when this dynamic strain is transmitted to the interface *via* the elastic Ecoflex matrix, causing an electrical response.³² Here, we have measured the peak-to-peak voltage (V_{pp}) for the NC1 devices in three deformation states such as flat (Fig. 2(c)), twisted

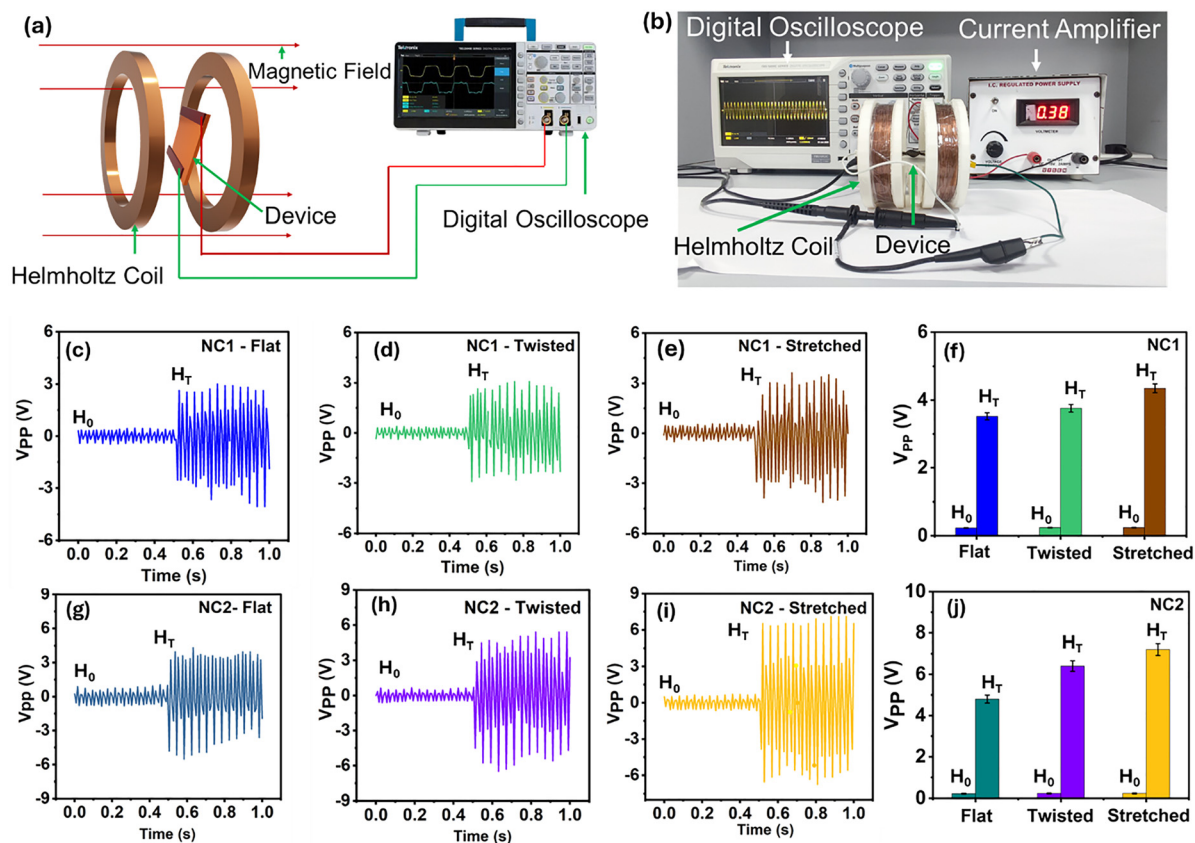


Fig. 2 (a) Schematic diagram of the low-intensity magnetic field harvesting experimental setup. (b) Digital image of the experimental setup. (c)–(e) Output V_{pp} from the NC1 device in flat, twisted, and stretched orientations. (f) Output V_{pp} from the NC1 device at H_0 and H_T (trial number, $n = 10$). (g)–(i) Output V_{pp} from the NC2 device in flat, twisted, and stretched orientations. (j) Output V_{pp} from the NC2 device at H_0 and H_T .



(Fig. 2(d)), and stretched (Fig. 2(e)) in the absence ($H_0 = 0$ T) and presence ($H_T = 1.33$ mT) of magnetic fields. The corresponding output voltage with error bars, are presented for comparison in the bar diagram in Fig. 2(f). Similar procedures were performed for the NC2 device, and the results are shown in Fig. 2(g)–(j). Each experimental result was obtained through multiple measurements. To evaluate the stability of the output voltage from the wearable HMI device, measurements were conducted repeatedly ($n = 10$), and the results are presented in Fig. 2(f) and (j), with error bars representing the standard deviation to indicate measurement consistency and reliability. The output voltage was recorded across 10 trials, with each data point reflecting the mean value of the recorded voltages. This statistical approach ensures a robust assessment of the device's performance, thereby confirming the device's stability and reproducibility under dynamic conditions. These results show that changing the device's shape (stretching and twisting) strengthens its electrical response with a constant magnetic field. The comparison analysis showed that NC2 outperformed NC1, likely due to its higher magnetic nanoparticle density, which increases strain and transduction efficiency. Higher nanoparticle content enhances magnetic dipole interactions with the Ecoflex matrix, amplifying the magnetostrictive effect and enabling more effective conversion of magnetic stimuli into electrical signals in NC2 for wearable HMI devices.

While keeping the magnetic excitation constant, the device's performance was assessed in various mechanical deformation states, including flat, twisted, and stretched (demonstrating stable operation at $\sim 60\%$ strain) conditions. These setups mimic mechanical challenges pertinent to stretchable and wearable HMI systems. Consistent with previous research on stretchable ME composites, improved strain transfer, optimized magnetic domain alignment, and enhanced interfacial coupling between the magnetostrictive filler and the elastomeric host have been associated with the increased voltage output under deformation.^{33,34} $\text{Ni}_{0.5}\text{Co}_{0.5}\text{Fe}_2\text{O}_4$ was selected due to its significantly higher piezomagnetic constant ($\frac{\partial \lambda}{\partial H} = 1.74 \times 10^{-9} \text{ A}^{-1} \text{ m}$) than other compositions, as reported in the literature,³² resulting in superior piezomagnetic performance. In spinel ferrites (AB_2O_4), the magnetic moments of ions in tetrahedral (A) and octahedral (B) sites are oriented antiparallel to each other. In NiFe_2O_4 , the spins of Fe^{3+} ions at A and B sites are antiparallel and largely cancel each other, yielding a net magnetic moment of $\sim 2\mu_B$ due to the presence of Ni^{2+} ($2\mu_B$, two unpaired electrons) at B sites. Substituting Co^{2+} ($3\mu_B$, two unpaired electrons) preferentially into B sites replaces Ni^{2+} and increases the number of unpaired electrons at octahedral sites, which enhances the magnetic properties. Furthermore, Co^{2+} exhibits higher magnetic anisotropy than Ni^{2+} , resulting in an increased coercivity (H_c) with Co substitution. This arises from the higher anisotropy field associated with Co^{2+} , which increases the domain wall energy and thus contributes to a more substantial piezomagnetic effect.^{33,35,36} This mixed-metal composition allows for the adjustment of magnetic sensitivity, making it work more effectively than

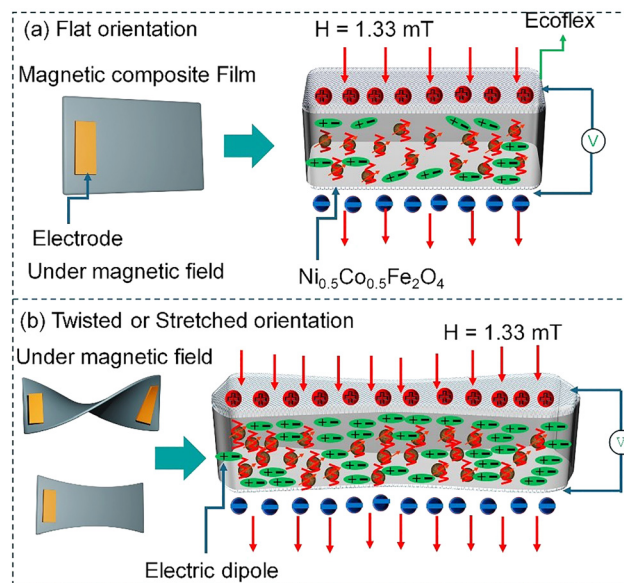


Fig. 3 Illustration of magnetic–electric dipole interactions in ME films in (a) flat and (b) twisted or stretched orientations.

single-metal ferrites. It is observed that the twisted or stretched conditions of the NC1 and NC2 nanogenerators yield higher output voltages compared to the conditions without strain. This phenomenon can be explained as follows: when the magnetic nanoparticle-embedded Ecoflex film is flat, a limited number of electric dipoles inside the matrix are aligned, resulting in a weak magnetic–electric interaction, and this limited coupling leads to lower voltage generation, as shown schematically in Fig. 3(a). However, mechanical stress redistributes through the Ecoflex matrix when the film twists or stretches, encouraging more electric dipoles to align effectively and enhancing the dipole.^{37,38} This enhanced dipole alignment increases the interfacial interactions between the dipoles in the matrix and embedded magnetic nanoparticles, resulting in a stronger ME coupling, as shown in the schematic in Fig. 3(b). Consequently, the film's voltage generation is significantly enhanced, which can be rationalized through mathematical formulation. The general expression can be represented by the ME voltage coefficient (α_V^H).^{39–41} The ME voltage coefficient establishes a direct correlation between the induced electric field (E) and the externally applied magnetic field (H), expressed as $\alpha_V^H = \frac{\partial V}{\partial H}$. A higher α_V^H value indicates stronger magneto-electric coupling, explaining the increased output voltage generation. Such dependence highlights the fundamental role of interfacial strain transfer and dipole alignment in boosting the ME response. The detailed derivation of this formulation, including the role of interfacial strain transfer, is provided in the SI.

Furthermore, the ME nanogenerator was connected with a rectification system capable of harvesting, converting, and storing the generated electrical energy in storage elements such as capacitors or batteries, as shown in Fig. 4(a). The system was systematically tested across various external load resistances



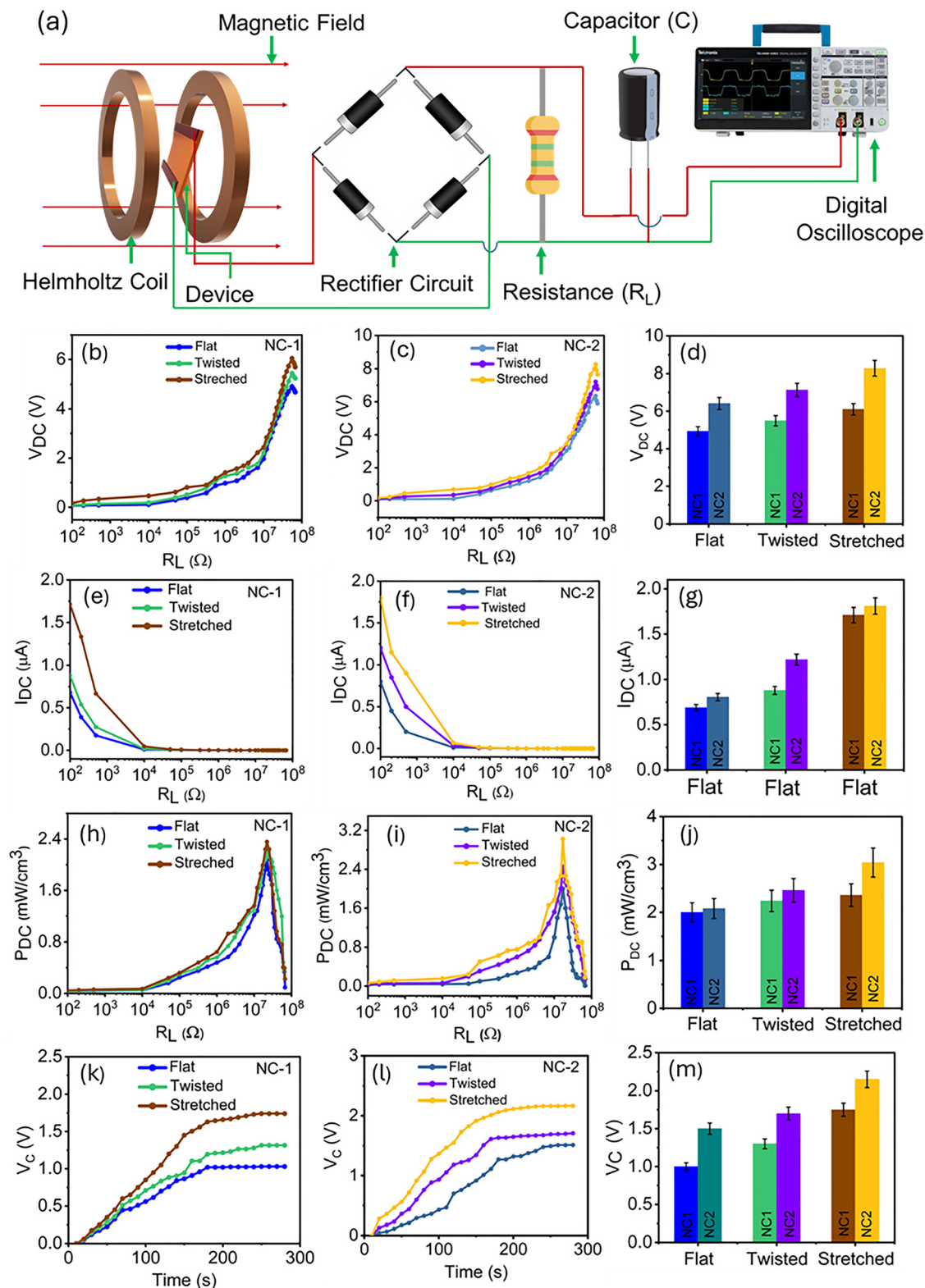


Fig. 4 (a) Schematic of the simplified circuit diagram with a ME transducer, a full-bridge rectifier, a capacitor, and a load resistance. V_{DC} under varying loads for (b) NC1 and (c) NC2 devices. (d) Bar chart comparing the V_{DC} of NC1 and NC2. I_{DC} output from (e) NC1 and (f) NC2. (g) Bar chart comparing the I_{DC} of NC1 and NC2. P_{DC} with load resistance for (h) NC1 and (i) NC2. (j) Bar chart comparing the P_{DC} of NC1 and NC2. Charge accumulation dynamics in capacitors for (k) NC1 and (l) NC2 transducers. (m) Bar chart of the V_C of NC1 and NC2.



($R_L \approx 100 \Omega$ – $100 \text{ M}\Omega$). The DC voltage (V_{DC}) for the NC1 and NC2 devices is shown in Fig. 4(b) and 4(c), respectively, and summarized as a bar diagram in Fig. 4(d). The output voltage from the NC1 and NC2 devices was repeatedly recorded to ensure stability, and the results are presented in Fig. 4(d). Similar procedures were used to measure the current and power calculations. The generated DC current (I_{DC}) as a function of R_L is plotted for both devices in Fig. 4(e) and (f). As expected, increasing load resistance led to higher DC voltage output, while I_{DC} decreased accordingly, a typical behavior governed by ohmic and power transfer principles. Fig. 4(g) presents a comparative analysis of I_{DC} values for NC1 and NC2 under different loading conditions. Under stretched configurations, the maximum open-circuit DC voltages were $\sim 6.06 \text{ V}$ for NC1 and 8.3 V for NC2. The corresponding short-circuit DC currents were measured at $\sim 1.8 \mu\text{A}$ and $\sim 1.7 \mu\text{A}$, respectively. The equation used to calculate the DC power density (P_{DC})⁴² of the various ME transducers is as follows (eqn (1)):

$$P_{\text{DC}} = \frac{V_{\text{DC}} \times I_{\text{DC}}}{\text{Volume of the device}} \quad (1)$$

In this context, the calculated P_{DC} values for NC1 and NC2 devices under varying load resistances are shown in Fig. 4(h) and 4(i), respectively. These plots display Gaussian-like distribution curves, highlighting the dependence of power output on external R_L . A comparative analysis of the maximum P_{DC} values across different transducers is shown in Fig. 4(j). Among the two, the NC2 device, comprising a higher concentration of magnetostrictive nanoparticles, achieves a power density of $\sim 3.16 \text{ mW cm}^{-3}$, surpassing the NC1 device, which generates $\sim 2.36 \text{ mW cm}^{-3}$ under the same magnetic field conditions (1.33 mT at 50 Hz). Remarkably, the DC power densities obtained in this work exceed those reported in previous studies of ME energy harvesters, as shown in Fig. 4(j). For instance, a PVDF/ CoFe_2O_4 -based ME transducer generated a maximum power output of $11 \mu\text{W}$,⁴³ while a PVDF/ YFeO_3 composite-based harvester achieved a power density of $2 \mu\text{W cm}^{-3}$.⁴⁴ Additionally, a polymer ink printed on a Metglas substrate yielded a power density of 0.64 mW cm^{-3} .⁴⁵ These findings underscore the enhanced energy harvesting capability of the NC2 ME nanogenerator, making it a promising candidate for powering next-generation wearable HMI systems. To assess the energy storage capability of our ME transducers in a capacitor, we carried out a charging process until the voltage (V_C) reached a saturation point over time, as illustrated in Fig. 4(k) and Fig. 4(l) for NC1 and NC2, respectively. Also, V_C is summarized as shown in the bar graph in Fig. 4(m). The stored electrical energy in the capacitor was determined using eqn (2):⁴²

$$E_C = \frac{1}{2} C V_C^2 \quad (2)$$

In this analysis, C refers to the capacitance of the storage capacitor ($100 \mu\text{F}$), and it took approximately 5 minutes for the ME transducers to charge the capacitor to their respective saturation voltages. The NC1 and NC2 devices successfully

stored maximum electrical energies of approximately $87.5 \mu\text{J}$ and $107.5 \mu\text{J}$, respectively. These energy levels are sufficient to power low-energy electronic components and sensor nodes typically used in wearable and soft HMI systems, where operating power demands range from nanowatts to a few microwatts. The mechanical stretchability of the ME film was further assessed under durability testing, showing outstanding robustness as it maintained its full output performance without degradation even after 1000 continuous stretching–release cycles at 100% strain as shown in Fig. S5(a) and (b) (SI).

3.3. Gesture-induced voltage in ME transducer films for HMI applications

To explore the feasibility of the developed ME composite film in real-time gesture-controlled HMI systems, distinct finger bending and gestures, namely ‘Victory’, ‘Ok’, and ‘Stop’, were employed as representative input modalities, as shown in the schematic of Fig. 5(a). The NC1 and NC2 ME nanogenerators demonstrated enhanced electrical output performance. However, the HMI demonstrations in this study primarily highlight NC2, with the corresponding results for NC1 provided in the SI (Fig. S6). For this demonstration of gesture-based voltage generation, a power cord connected to a primary power source supplying 1 A current at 50 Hz was employed as a stray magnetic field generator, and the application was performed at a 2 cm distance from the power cord to achieve higher efficiency and output voltage recorded using a DSO. A flexible NC2 nanogenerator was connected to electrodes and subjected to index finger bending at four different angles of 0° , 5° , 65° , and 125° (Fig. 5(b)), which simulate natural finger motions during gesture input. As the bending angle increased, a corresponding increase in output voltage from $\sim 2 \text{ V}$ to 7 V was observed, as shown in Fig. 5(c). The clear voltage differentiation at each bending angle highlights the film’s soft pressure or motion sensor capability. This energy-harvesting approach enables a self-powered system suitable for real-time motion tracking. Furthermore, for the ‘Victory’ gesture, two NC2 transducers were attached to the index and middle fingers at joint positions as shown in Fig. 5(d) and the output voltage was measured to be $\sim 6 \text{ V}$. For the ‘Ok’ gesture, two NC2 transducers were attached to the thumb and index finger and an output voltage of $\sim 10 \text{ V}$ was measured. Similarly, for the ‘Stop’ gesture, three NC2 transducers were attached to the index, middle and ring fingers, the output voltage was measured to be $\sim 14 \text{ V}$, and the comparatively recorded output voltages are shown in Fig. 5(e). From the observation, the real-time voltage output corresponding to each gesture exhibited unique signal amplitudes, enabling reliable differentiation. The ‘Stop’ configuration generated the highest output voltage among the tested gestures because three NC2 films were connected in series, resulting in a higher voltage output for this gesture than for the other gestures. This behavior demonstrates the capability of the ME nanogenerator to translate subtle gesture motions into distinct electrical signatures. Such gesture-specific signal responses confirm the device’s high sensitivity and rapid signal transduction, validating its applicability in



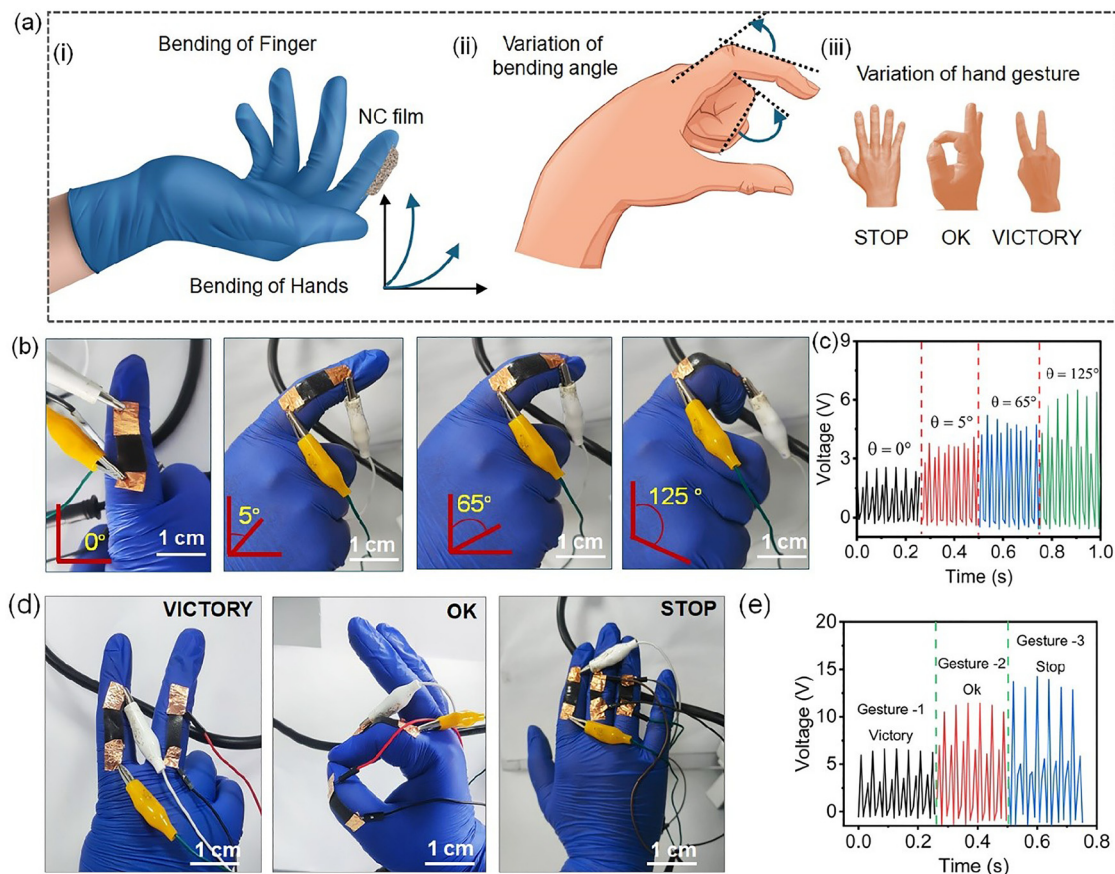


Fig. 5 (a) Illustration of real-time gesture-controlled HMI systems, distinct finger bending, and gestures. (b) Demonstration of index finger bending at 0°, 5°, 65°, and 125° using the NC2 film. (c) Output voltage of finger bending orientation from the NC2 film. (d) Demonstration of 'Victory', 'OK', and 'Stop' gestures using the NC2 film. (e) Recorded output voltage of the gestures from the NC2 film.

next-generation stretchable electronics. The demonstrated approach offers a promising pathway toward the application of low-power, self-powered HMI systems in intelligent prosthetics, sign-language recognition, and personalized healthcare interfaces.

4. Conclusion

In summary, we have designed a highly stretchable and self-powered ME composite film by embedding $\text{Ni}_{0.5}\text{Co}_{0.5}\text{Fe}_2\text{O}_4$ nanoparticles into a soft Ecoflex matrix, aimed at wearable energy harvesting and real-time gesture-responsive human-machine interface applications. The ME films exhibited high mechanical stretchability, sustaining tensile strains up to $\sim 315\%$ without performance degradation. They retained over $\sim 100\%$ of their initial output after 1000 continuous stretching-release cycles, confirming their mechanical durability. The optimized device generated significant ME output voltages, maintained stability under repeated mechanical strain, and enabled efficient energy harvesting from ambient magnetic field sources. The ME device generated a peak output voltage of ~ 8.3 V and a maximum power density of ~ 3.16 mW cm^{-3} , outperforming conventional soft nanogenerators. The ME

device demonstrated high performance in real-time experiments, where distinct output voltages were associated with specific finger bending and hand gestures. Integrating the fabricated flexible ME film into skin-interfaced platforms enables simultaneous powering, sensing, and energy harvesting without requiring an external power source. This work paves the way for the next generation of magnetoelectrically active, skin-conformal devices with applications in smart prosthetics, autonomous soft robotic interfaces, and gesture-based control systems.

Conflicts of interest

All authors declare no competing financial interests.

Data availability

All data is available from the corresponding author upon reasonable request. Supplementary information: Additional experimental details, preparation of the film, optical image of the device, experimental setup, characterization of the nanoparticles, durability test and output voltage under different hand gestures. See DOI: <https://doi.org/10.1039/d5tc03220b>.



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