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# Cerium oxide-based electrolytes for low- and intermediate-temperature solid oxide fuel cells: state of the art, challenges and future prospects

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Solid oxide fuel cells (SOFCs) are important, efficient, and environmentally friendly energy conversion devices that also serve as solid oxide electrolyzers, producing hydrogen and oxygen by reversing chemical reactions. Research and development of electrode and electrolyte materials is still very much needed for their efficient working in low ( $\leq 650$  °C) and intermediate (650–850 °C) temperature regimes. The present article reviews undoped and doped ceria-based electrolytes in light of processing parameters such as synthesis methods, sintering time, temperature and different doping strategies. The article focuses primarily on the various factors that affect the conductivity of ceria-based electrolytes. Different approaches to enhance the conductivity and improve the cell parameters have also been discussed. Conclusion, challenges and direction for further research are also provided at the end of this article.

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## 1. Introduction

Electricity and water are the basic amenities for the sustainable development of society. However, with the depletion of resources and the increasing population, there is a need to produce clean energy with less carbon and unprocessed waste. The most sought-after way to reduce carbon footprints and meet

global energy demands is by using renewable, cleaner, greener energy sources. Hydrogen-based energy sources are an alternative to conventional fuels, such as natural gas, coal, fossil fuels, *etc.* There are many different sources of hydrogen production based on which they are colour-coded, as shown in Fig. 1.<sup>1,2</sup> Green hydrogen is produced from renewable energy sources and produces zero greenhouse gas emissions. Energy conversion devices, *i.e.*, solid oxide fuel cells (SOFCs), utilise green hydrogen as a fuel, and solid oxide electrolysis cells (SOECs) produce green hydrogen.<sup>3,4</sup>

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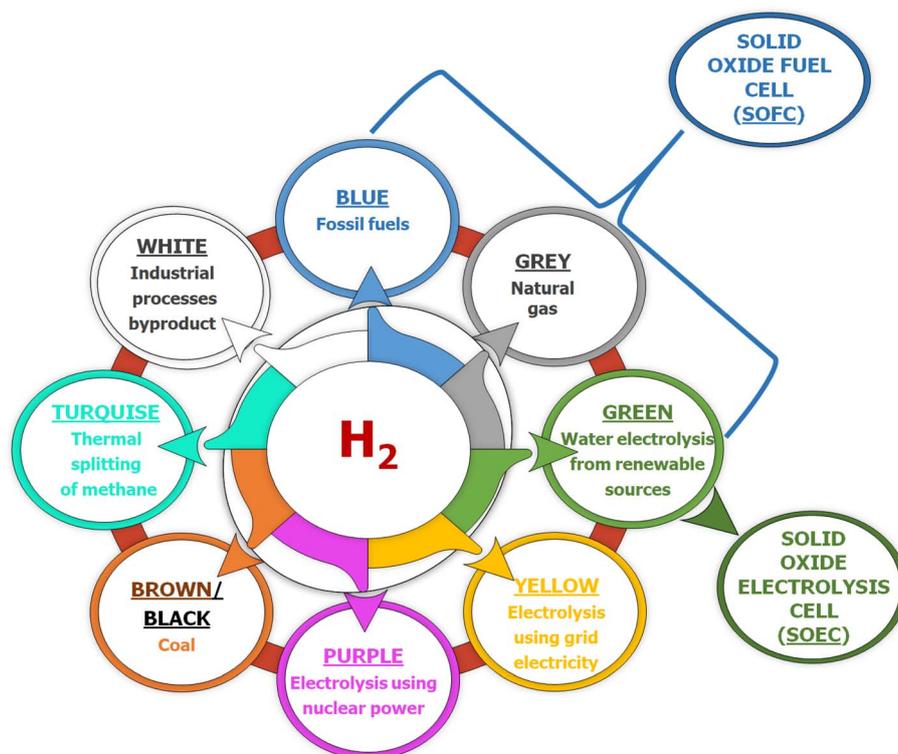


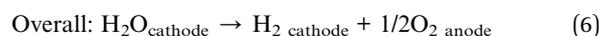
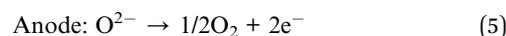
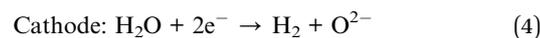
Fig. 1 Sources of hydrogen production and technological applications of green hydrogen.

SOFCs are efficient electrochemical energy conversion devices that produce electricity through a chemical reaction between the fuel ( $\text{H}_2$ ) and air. With fuel flexibility, SOFCs are good candidates for electricity production, having the highest efficiency compared to other fuel cells.<sup>5–8</sup> Additionally, SOFCs are also being used for water production in space missions. Thus, SOFCs could be a future energy source and a strategic source of water production. A single unit of SOFCs consists of two electrodes (anode and cathode) and an electrolyte, having an output of only  $\sim 1$  volt (V) and power density  $< 2 \text{ W cm}^{-2}$ . Therefore, multiple single cells are connected using (metallic or ceramic) interconnects to enhance overall electricity production. The design of SOFCs also incorporates an additional component, such as a glass sealant, in the case of the planar configuration.<sup>9,10</sup>

SOFCs are multipurpose devices that can also be used as electrolyzers, *i.e.*, SOECs, to produce hydrogen and oxygen by reversing the reactions to split water into its constituent gases.<sup>11–14</sup> The diagrammatic illustration of SOFCs *versus* SOECs is shown in Fig. 2(a) and (b). In SOFCs, air or oxygen is fed to the cathode and is converted into oxide ions. These oxide ions travel through the electrolyte towards the anode, where they react with the fuel ( $\text{H}_2$ ) to form water ( $\text{H}_2\text{O}$ ).<sup>15</sup> The reactions that occur at the electrodes are given as follows:



On the other hand, in the case of SOECs, steam ( $\text{H}_2\text{O}$ ) is fed to the cathode and electricity is applied. At the cathode–electrolyte interface,  $\text{H}_2\text{O}$  decomposes into  $\text{H}_2$  and  $\text{O}^{2-}$ .  $\text{H}_2$  gas travels through the pores of the cathode to its surface, where it is collected. The  $\text{O}^{2-}$  ions travel through the electrolyte towards the anode, and at the anode–electrolyte interface,  $\text{O}^{2-}$  gets oxidized into  $\text{O}_2$  gas. The reactions occurring at SOEC electrodes are as follows:<sup>16</sup>



Therefore, the same device can also produce hydrogen and oxygen. The hydrogen produced from SOECs that use electricity from renewable sources is known as green hydrogen and can be stored in any form: solid, liquid or gas. However, solid-state storage provides many benefits, such as higher volumetric energy density than other storage methods.

In addition to direct biogas and many other fuels, carbon monoxide can also be used in SOFCs. It is converted into less dangerous carbon dioxide during the operation of SOFCs. In fact, oxygen could also be used for many applications, particularly in the medical field, due to its purity, using both these



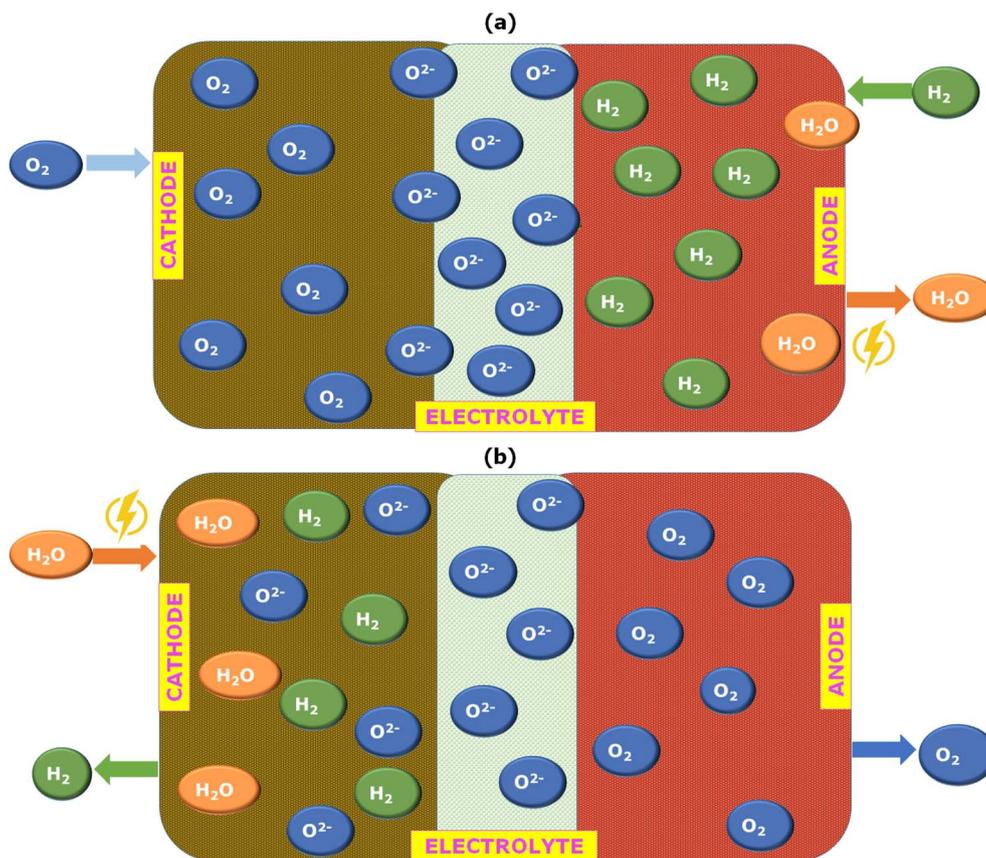


Fig. 2 A schematic illustration of the working of (a) SOFC and (b) SOEC.

operations (SOFCs and SOECs).<sup>17,18</sup> It is a fact that once a technology is developed in one device, others can be modified slightly and used for various purposes. So much research is going on to develop this technology in parallel to other devices, such as batteries, supercapacitors, *etc.*, for use in different applications.<sup>19</sup> Many excellent reviews are available on materials development for various components of SOFC technology.<sup>7,20–25</sup>

The present article focuses mainly on developing electrolyte materials since they are integral to SOFCs and SOECs. An electrolyte is a medium through which ions are conducted from one electrode to another, and the dispersion of anions and cations at an applied potential is responsible for current generation. In fact, the overall device resistance also depends on the ionic flow through the electrolyte. Different fuel cells are also named after the type of electrolyte used (molten carbonate fuel cells, alkaline fuel cells, polymer electrolyte membrane fuel cells, direct methanol fuel cells, phosphoric acid fuel cells, solid oxide fuel cells and reversible fuel cells). Solid electrolytes offer many advantages over aqueous electrolytes and can be used in many applications.<sup>26</sup> Even the temperature categorisation of SOFCs is based on the operating temperature of the electrolyte, *i.e.*, high-temperature (HT-SOFC): 850–1000 °C, intermediate-temperature (IT-SOFC): 650–850 °C and low-temperature (LT-SOFC): <650 °C.

Ceramic materials are predominantly used for SOFCs or SOECs as electrodes and electrolytes. Ceramic materials with

high chemical stability, good mechanical strength, and low activation energy ( $E_a$ ) for ionic conduction are required to qualify as electrolyte materials. Materials with good relative density ( $\sim >95\%$ ) preclude open porosity and avoid reactant crossover from the anode to the cathode and *vice versa*. The material requirements for different SOFC components are clearly discussed in the literature.<sup>20,27–36</sup> As mentioned earlier, the conducting properties of electrolyte materials are of utmost importance. Therefore, in the present article, the primary focus is to analyse the conductivity of electrolyte materials and correlate other properties with conductivity.

## 2. Electrolyte materials for SOFCs

Since the inception of SOFCs, many materials such as fluorite-structured  $ZrO_2$ ,  $CeO_2$ ,  $Bi_2O_3$ -based oxides, perovskite-structured  $LaGaO_3$ ,  $SrTiO_3$ ,  $Bi_4V_2O_{11}$ ,  $La_2Mo_2O_9$ ,  $Ba_2In_2O_5$  oxides, brownmillerite and pyrochlore-structured materials have been investigated and developed for use as electrolytes for SOFCs.<sup>20,37–45</sup> SOFC electrolytes could be oxygen, proton or dual (oxygen and proton) conducting.

Eight mol% yttria stabilised zirconia (8-YSZ) is a widely used oxide ion electrolyte material in HT-SOFCs since it is reported to have an ionic conductivity of  $0.1 \text{ S cm}^{-1}$  at 1000 °C. It also exhibits good mechanical properties without compromising the stability of the cell and the durability of its performance.<sup>30,46</sup>



However, in IT- and LT-SOFCs, the ionic conductivity of 8-YSZ decreases drastically to  $\sim 7.2 \times 10^{-4} \text{ S cm}^{-1}$  at 500 °C.<sup>47</sup> This issue of poor ionic conduction can be resolved by reducing the thickness of the electrolyte or by finding a substitute for YSZ.<sup>48–50</sup> Other than YSZ, scandia stabilised zirconia (ScSZ) is also known to exhibit high ionic conductivity. The close ionic radii of  $\text{Zr}^{4+}$  and  $\text{Sc}^{3+}$  decrease the association enthalpy of the defects, resulting in higher conductivity for ScSZ, *i.e.*,  $3 \times 10^{-1} \text{ S cm}^{-1}$  at 1000 °C, than that of YSZ. However, the high cost and rarity of scandia limit the use of ScSZ, and the reaction of zirconia with strontium or lanthanum present in the cathode limits their use as electrolytes.<sup>51,52</sup>

Compared to YSZ and ScSZ, bismuth-based fluorite-structured materials ( $\delta\text{-Bi}_2\text{O}_3$ ) exhibit the highest oxygen ionic conductivity. This is due to a high concentration of oxygen vacancies and easy anion mobility in these electrolytes. However, the ionic conduction decreases significantly in these oxides when the operating temperature is lowered. A large dopant concentration is used to stabilise these oxides. Gd, La, Cu, Ti, Al, Ga, *etc.*, are commonly used dopants.<sup>43,44,53–55</sup> The dopant ionic radius and polarizability affect the conductivity and stability of these bismuth oxide-based electrolytes.  $\gamma\text{-Bi}_4\text{V}_2\text{O}_{11}$  doped with transition metals, *i.e.*, BIMEVOX, demonstrates high ionic conductivity and higher stability at 600 °C. It exhibits three polymorphs ( $\alpha$ ,  $\beta$ , and  $\gamma$ ) with respect to temperature, and the higher temperature  $\gamma$ -phase has a higher oxygen vacancy disorder in the O–V polyhedra. The major drawback of  $\text{Bi}_4\text{V}_2\text{O}_{11}$  is the slow phase transformation ( $\delta \rightarrow \alpha$ ) occurring between 500 and 600 °C, which decreases its conductivity and limits its usage in LT- and IT-SOFCs. Additionally,  $\text{Bi}_2\text{O}_3$  decomposes into metallic Bi in reducing environments, has poor mechanical strength and a high coefficient of thermal expansion (CTE) and is chemically reactive with other SOFC components, thus limiting its usage as electrolyte.<sup>52,56–60</sup>

Perovskite-based oxides are another popular electrolyte material choice with high SOFC performance. At 500 °C, the oxide ion conductivity of  $\text{Sr}_{0.55}\text{Na}_{0.45}\text{SiO}_{2.755}$  is  $> 10^{-2} \text{ S cm}^{-1}$ , having an activation energy of 0.3 eV. A SOFC with  $\text{Sr}_{0.55}\text{Na}_{0.45}\text{SiO}_{2.755}$  electrolyte has high power densities of 431 and 213  $\text{mW cm}^{-2}$  at 600 and 500 °C, respectively. It is a promising SOFC electrolyte candidate with activation energy that is much lower than that of other commonly used oxygen ion conductors and high power density.<sup>61</sup> Mo-substituted  $\text{SrFeO}_3$  achieved power densities between 0.24 and 1.12  $\text{W cm}^{-2}$  across 600–800 °C. A SOFC single cell employing a  $\text{SrFe}_{0.93}\text{Mo}_{0.07}\text{O}_{3-\delta}$  cathode exhibited excellent operational stability over 270 h at 700 °C.<sup>62</sup> Lanthanum-based oxides such as  $\text{LaAlO}_3$ ,  $\text{LaSrO}_3$ ,  $\text{LaInO}_3$ ,  $\text{LaScO}_3$ ,  $\text{LaYO}_3$ , *etc.*, exhibit minimum electronic conduction and high stability at lower operating temperatures. Adding Co, Ni, or Bi in small quantities at the gallium site and co-doping at the La and Ga sites enhances ionic conductivity.<sup>63–67</sup> However, phase instability, gallium volatilisation at high temperatures, and chemical incompatibility with nickel limit the use of these materials.<sup>20,68</sup>

Fluorite-structured electrolytes offer many advantages over traditionally used materials; therefore, they are widely used as

SOFC electrolyte materials. The following sub-section discusses ceria-based electrolytes in detail.

## 2.1. Ceria-based electrolytes

Cerium dioxide ( $\text{CeO}_2$ ) with different dopants is used in many applications.<sup>69–73</sup> As mentioned in the introduction section, the primary focus of the present review is on the various parameters affecting the conductivity of  $\text{CeO}_2$  and discussing its applicability as an electrolyte for SOFCs.  $\text{CeO}_2$ , commonly known as ceria, has a fluorite structure ( $\text{AX}_2$ ) with A as the cation and X as the anion. Structurally, each  $\text{Ce}^{4+}$  cation is coordinated to eight  $\text{O}^{2-}$  anions. Each  $\text{O}^{2-}$  anion is located at the tetrahedral interstices of four  $\text{Ce}^{2+}$  cations.<sup>74</sup> The electronic configuration of cerium is  $[\text{Xe}] 4f^2 6s^2$  with two common valence states, cerium(III) and cerium(IV). A detailed overview of the structure of  $\text{CeO}_2$  is given by Sun *et al.* and shown in Fig. 3.<sup>69</sup> The fluorite structure with the space group  $Fm\bar{3}m$  is stable over a wide temperature range (room temperature–2400 °C). Unlike  $\text{ZrO}_2$ ,  $\text{Bi}_2\text{O}_3$ , *etc.*, electrolytes, the phase transition does not occur up to their melting point. In some electrolytes, it can be stabilised using different dopants and their concentration. The task is stabilising the high conducting phase, such as  $\gamma$ -phase in  $\text{Bi}_4\text{V}_2\text{O}_{11}$  and the cubic phase of  $\text{ZrO}_2$ , to use as electrolytes in SOFC technology. In the case of  $\text{CeO}_2$ , the cubic phase already exists with unoccupied octahedral sites necessary for oxide ion diffusion. The cationic or anionic vacancies can be further increased by introducing appropriate dopants and their concentrations. These vacancies are required since ionic conduction occurs *via* the vacancy diffusion mechanism.

Pure  $\text{CeO}_2$  ceramic is a poor oxide ion conductor ( $\sim 0.24 \times 10^{-3} \text{ S cm}^{-1}$  at 700 °C) since it lacks sufficient vacant sites for oxide ion transport, as shown in Fig. 3(a).<sup>75–77</sup> At lower temperatures, the reduction of  $\text{Ce}^{4+}$  to  $\text{Ce}^{3+}$  leads to the generation of more oxygen vacancies and electrons. These electrons act as polarons as they are localised to  $\text{Ce}^{3+}$ ; therefore, electron hopping between  $\text{Ce}^{3+}$  and  $\text{Ce}^{4+}$  leads to n-type conductivity, which reduces the open circuit voltage (OCV) to a large extent. This causes the electrolyte to be a mixed ionic-electronic conductor rather than a pure ionic conductor. Also, the larger ionic radius of  $\text{Ce}^{3+}$  ( $r_{\text{ionic}} = 1.01 \text{ \AA}$ ) than  $\text{Ce}^{4+}$  ( $r_{\text{ionic}} = 0.87 \text{ \AA}$ ) obstructs the migration of  $\text{O}^{2-}$  ions, thereby reducing the ionic conductivity in this temperature range.<sup>78,79</sup> Additionally, the electrolyte should be a purely ionic conductor; therefore, the presence of electrons in the electrolyte hinders its performance and poses a risk of short-circuiting. Unwanted reactions at the electrode–electrolyte interface lead to the degradation of the electrolyte, reducing the device's efficiency.<sup>80</sup>

The ionic radii of the dopant cation significantly affect the ionic conductivity of the electrolyte. Doping with larger cation sizes can block the migration of vacancies, leading to higher  $E_a$  of ionic conduction. Thus, a better strategy is to have the dopant and host cation size comparable for better ionic conductivity. Additionally, to sufficiently increase the ionic conductivity of  $\text{CeO}_2$ , doping of lower valence cations is done to increase the oxygen vacancy concentration.<sup>81</sup> When a lower valence cation (aliovalent) replaces a higher valence cation, oxide ion vacancies



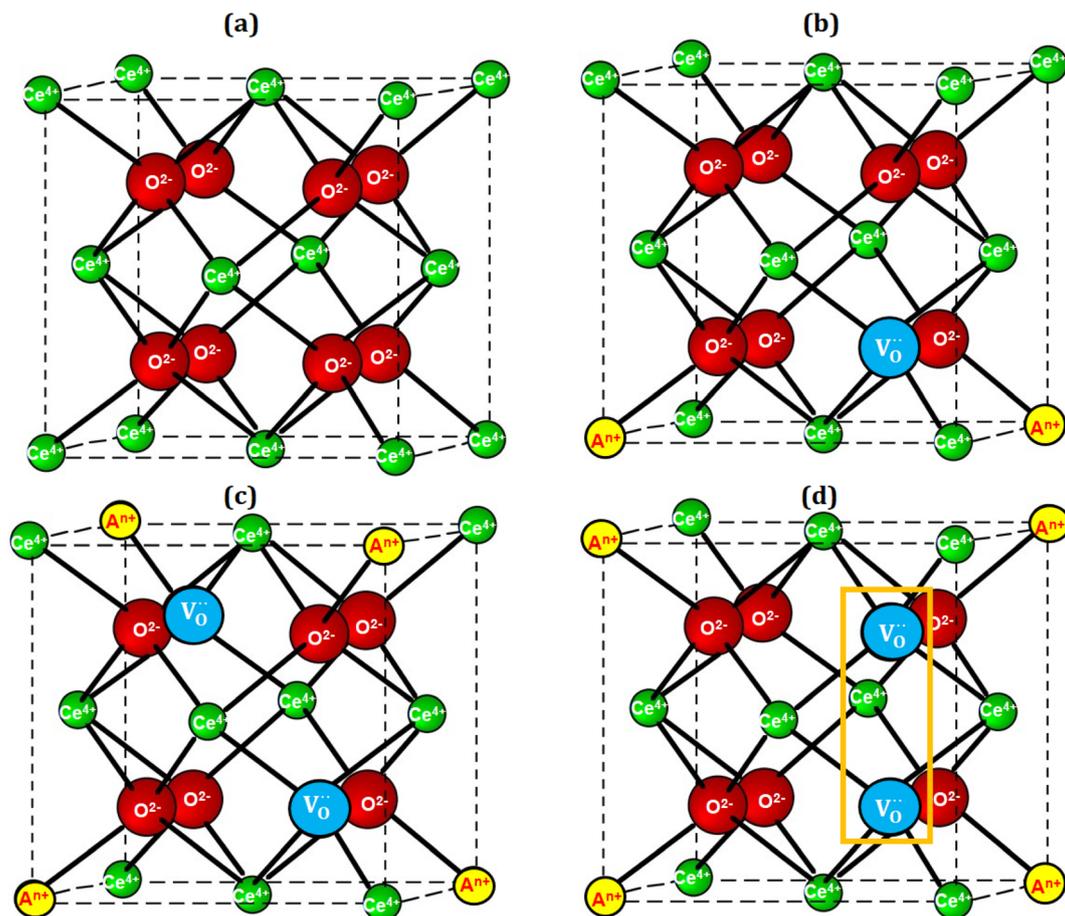


Fig. 3 Schematic representation of the effect of doping on the crystal structure of  $\text{CeO}_2$ . (a) The undoped  $\text{CeO}_2$  structure. (b) and (c)  $\text{Ce}^{4+}$  replacement by lower valence cations ( $\text{A}^{n+}$ ;  $n = 3, 2, 1$ ) leads to the formation of disordered oxide ion vacancies ( $\text{V}_\text{O}$ ), and (d) vacancy clustering. The higher number of vacancy clusters lowers the ionic mobility, which decreases the ionic conductivity.

are introduced to maintain overall charge neutrality. This is when the fluorite structure of  $\text{Ce}^{4+}$  becomes distorted. It allows transportation of the oxide ions on thermal activation through the lattice by hopping from one crystal lattice site to its neighbouring vacant site, as shown in Fig. 3(b) and (c). Therefore, aliovalent doping is better than isovalent doping for enhancing oxide ion conductivity in  $\text{CeO}_2$  due to defect engineering. Replacement by a dopant of different ionic radii (aliovalent) creates point defects (vacancies) in the system. These vacancies expedite the ionic conduction in  $\text{CeO}_2$ . Dopants cause unit cell expansion and contraction *via* altering the average size of cations and the lengthening or contracting of the cation–oxygen bond length, which are determined by the host's and dopant's oxidation states and their ionic radius. The unit cell expands or contracts due to both factors working together.<sup>22</sup> A smaller ionic radius causes a compressive strain responsible for charge neutrality. Therefore, aliovalent doping in  $\text{CeO}_2$  causes a local lattice strain, which facilitates the formation and migration of oxygen vacancies.

Aliovalent-doped ceria has received significant attention due to its superior ionic conductivity between 500 and 800 °C in air.<sup>82,83</sup>  $\text{Sr}^{2+}$  and  $\text{Ca}^{2+}$  doping improve the oxide ion conductivity

of ceria-based electrolytes significantly.  $\text{Sr}^{2+}$  doped  $\text{CeO}_2$ ,  $\text{Ce}_{0.925}\text{Sr}_{0.075}\text{O}_{2-\delta}$  has a relative density, conductivity and power density of 97%,  $6.46 \times 10^{-3} \text{ S cm}^{-1}$  and  $89 \text{ mW cm}^{-2}$ , respectively, at 600 °C. Here,  $\text{Sr}^{2+}$  doping serves a dual purpose. It creates oxygen vacancies in  $\text{CeO}_2$  and acts as a sintering aid.<sup>84</sup> Doping of  $\text{Ce}_{0.8}\text{Sm}_{0.2}\text{O}_{2-\delta}$  with  $\text{Bi}^{3+}$ ,  $\text{Mg}^{2+}$  and  $\text{Li}^+$  results in a higher conductivity of  $0.089 \times 10^{-3}$ ,  $0.39 \times 10^{-3}$ , and  $0.13 \times 10^{-3} \text{ S cm}^{-1}$  and power density of 716, 929 and  $1097 \text{ mW cm}^{-2}$  in comparison to undoped  $\text{Ce}_{0.8}\text{Sm}_{0.2}\text{O}_{2-\delta}$ , having a conductivity and power density of  $0.11 \times 10^{-3} \text{ S cm}^{-1}$  and  $281.5 \text{ mW cm}^{-2}$ , respectively. The higher conductivity and power density in the doped samples were attributed to the small amount of impurities in the ceria lattice.<sup>85</sup> Generally, alkaline earth dopants are cost-effective, readily available and eco-friendly. The small amount of these oxides works as sintering aids when used as dopants in  $\text{CeO}_2$  electrolytes. However, their solid solubility is limited compared to rare earth dopants, leading to secondary phase formations. Additionally, larger ionic radii of some of the alkaline earth dopants cause the lattice to expand and decrease the ionic mobility.<sup>86</sup>

Apart from alkaline earth dopants, there is extensive literature on doping ceria with rare-earth elements such as  $\text{La}^{3+}$ ,



$\text{Nd}^{3+}$ ,  $\text{Gd}^{3+}$ ,  $\text{Y}^{3+}$ ,  $\text{Sm}^{3+}$ ,  $\text{Eu}^{3+}$ , *etc.*, since they exhibit higher bulk ionic conductivities than other elements.<sup>27,87–90</sup> Gd-doped ceria (GDC) has been a popular electrolyte material since it has higher conductivity ( $10^{-2} \text{ S cm}^{-1}$ ) than YSZ ( $10^{-3} \text{ S cm}^{-1}$ ) at 500 °C. This is because it reduces the reduction of Ce, which restricts electronic conduction. Also, the ionic radius of  $\text{Ce}^{4+}$  ( $r_{\text{ionic}} = 0.87 \text{ \AA}$ ) is greater than that of  $\text{Zr}^{4+}$  ( $r_{\text{ionic}} = 0.72 \text{ \AA}$ ); therefore,  $\text{CeO}_2$  has a more open fluorite structure than YSZ. It leads to an increase in the Ce–O bond lengths and a decrease in the  $E_{\text{a}}$ , which is responsible for the increase in the ionic conductivity of  $\text{CeO}_2$ .<sup>20,91–93</sup> Similarly, the ionic radii of  $\text{Gd}^{3+}$  ( $r_{\text{ionic}} = 0.938 \text{ \AA}$ ) and  $\text{Sm}^{3+}$  ( $r_{\text{ionic}} = 0.958 \text{ \AA}$ ) are closer to that of  $\text{Ce}^{4+}$  ( $r_{\text{ionic}} = 0.87 \text{ \AA}$ ); therefore, these dopants show maximum ionic conductivity with minimum lattice distortion due to size difference. The differences in ionic sizes of the dopants influence the localisation of oxygen vacancies by defect association, formation of secondary phases, *etc.*, all of which modify grain and grain-boundary conductivity. The conductivity of divalent ions is less than that of trivalent ions because of the larger ionic radius mismatch between divalent ions and cerium ions ( $\text{Ce}^{4+}$ ).<sup>20,94,95</sup>

Doping can be done only up to a specific concentration of the dopant. It happens for several reasons, such as vacancy clustering, vacancy repulsion and a rampant increase in the solid solubility limit. As reported in the literature, the ionic conductivity of doped ceria can reach a maximum only up to a certain extent of dopant concentration. After this limit, there is an increase in the defect interactions that gives rise to the clustering of vacancies, after which the mobile ions reduce, as shown in Fig. 3(d). Larger clusters require more atoms that need to be displaced for ionic motion. This requires larger  $E_{\text{a}}$ , and there is a decrease in the ionic conductivity.<sup>96,97</sup> The solid solubility limits of some commonly used dopants are given in Fig. 4. The maximum solubility limit is observed where the ionic radii of dopants are close to that of  $\text{Ce}^{4+}$ , after which there is formation of secondary phases which are usually segregated along the grain boundaries, hindering the movement of mobile ions.<sup>98–100</sup>

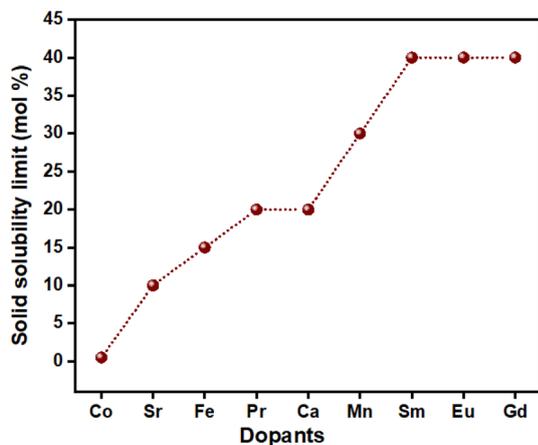


Fig. 4 Solid solubility limits of common dopants used in  $\text{CeO}_2$  synthesised using the solid-state reaction and wet-chemical routes.<sup>98–100</sup>

The following thermodynamic relations are responsible for governing the solubility limit of the dopants at equilibrium:

$$\Delta G = \Delta H - T\Delta S \quad (7)$$

$$\Delta G = \frac{1}{2}RT \ln p\text{O}_2 \quad (8)$$

$$\frac{1}{2} \ln p\text{O}_2 = \frac{\Delta H}{RT} - \frac{\Delta S}{R} \delta = \text{constant} \quad (9)$$

where  $G$ ,  $H$ ,  $T$ ,  $S$ ,  $R$ , and  $p\text{O}_2$  refer to Gibbs free energy, enthalpy, temperature and entropy, gas constant and oxygen partial pressure, respectively.  $\Delta$  refers to the changes in the thermodynamic quantities, and  $\delta$  represents the oxygen non-stoichiometry. The slope and intercept of  $\ln p\text{O}_2$  versus  $1/T$  for a constant  $\delta$  give  $\Delta H$  and  $\Delta S$  as a function of  $\delta$ . The Gibbs free energy must be negative for a dopant to be completely soluble. This is because entropy always increases with temperature. Increased atomic mobility at elevated temperatures facilitates dopant diffusion and incorporation into thermodynamically favourable lattice sites, promoting equilibrium solubility. In contrast, low temperatures suppress diffusion kinetics, limiting dopant activation and incorporation into the crystal structure.<sup>101–103</sup>

On the whole, the dopant type and concentration affect the electrolyte performance. Higher and lower ionic radius dopants introduce cationic and oxide ion vacancies, respectively. Dopants only up to a certain limit can be introduced in the system since higher concentrations lead to the formation of secondary phases that disrupt the conductivity of the electrolyte. Several factors affect the ionic conductivity of the electrolytes, many of which are discussed in the following sections.

### 3. Role of processing parameters in conductivity and other properties

The selection of starting materials is essential for better homogeneity of a mixture. It is imperative to understand the starting chemicals used for different synthesis methods. Generally, oxides and carbides are used as starting materials for the solid-state reaction and nitrates are used for the sol-gel (chemical wet) method. Chemicals used for synthesis can vary in purity depending on the studied property. For example, point defects (oxide vacancies) are introduced into the system for better ionic conduction. Raw materials with lower purity can provide the necessary defects in this case. Apart from the selection of raw materials, microstructural uniformity, particle size, grain growth, grain size and shape, density, sintering time, and temperature are also important for different synthesis methods.<sup>104</sup>

For a homogeneous mixture, it is necessary to consider the grain size of the composition, which varies from one synthesis method to another. In powder methods, the mixing/ball milling of powders is done before sintering. The difference in grain size may be attributed to the particles' composition, which introduces defects and internal stress to their structure.<sup>105</sup> The effect of calcining composition,  $\text{Li}_{6.4}\text{Fe}_{0.2}\text{La}_3\text{Zr}_2\text{O}_{12}$ , using the solid-



state and sol-gel methods was studied by Paulus *et al.*<sup>106</sup> A mixture of the cubic and tetragonal structures was observed in the solid-state reaction method due to the inhomogeneous distribution of iron in the sample. However, samples calcined using the sol-gel method yielded homogeneous, single-phase cubic structures. Calcination by sol-gel also decreased the sintering time by 2 hours. The sample exhibited a total ionic conductivity of  $1.82 \times 10^{-3} \text{ S cm}^{-1}$  at 25 °C, the highest for garnet-related materials. Therefore, the exact composition synthesised using different techniques yields different results.

Control over the grain size is essential for the dielectric response of CeO<sub>2</sub>. There are several ways to control the grain size: ball-milling, varying sintering temperature and doping.<sup>107</sup> Smaller grains have a more intense dielectric response. Due to the greater concentration of grain boundaries in smaller grains, the effect of grain size is primarily caused by increased surface stress.<sup>108,109</sup> Cationic diffusion governs the grain boundary mobility through an interstitial mechanism that is influenced by oxygen vacancies.<sup>110</sup> Densification occurs by grain boundary diffusion rather than lattice diffusion. Sintering is dependent on the reduction of the excess surface energy, in which the following equation gives the flux of atoms ( $J$ ) along a grain boundary:

$$J = MC\nabla\mu \quad (10)$$

where  $M$  is the mobility of the atoms along the grain boundary,  $C$  is the vacancy concentration, and  $\nabla\mu$  is the gradient in the chemical potential between the atoms in the materials and the neck of adjacent particles.<sup>111,112</sup> Dopants that increase any of these parameters lead to lower sintering temperatures.

Processing parameters play an important role in modifying various properties of ceramic materials.<sup>113</sup> The dopant composition, the thickness of the electrolyte, the microstructure, the sintering temperature, *etc.*, affect the cell's overall performance as illustrated in Fig. 5. The shape and size of grains potentially

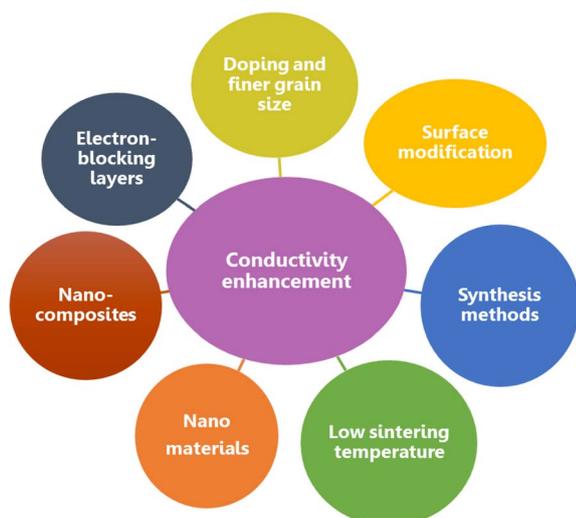


Fig. 5 Factors that increase the ionic conductivity of CeO<sub>2</sub>-based electrolytes.

affect the interaction of dopant-oxygen vacancies, affecting ion migration and ionic conductivity. The microstructure can have regularly or irregularly arranged grains of different shapes, such as hexagonal, polygonal, globular, *etc.* Finer grain sizes lead to more grain boundaries necessary for ionic conduction. As reported in the literature, CeO<sub>2</sub> generally deviates from the stoichiometric composition by releasing gaseous oxygen; this process could also be monitored from the morphology of the samples (bubbles on the surface).<sup>114,115</sup> Surface modifications (synthesis techniques and sintering temperature) can significantly enhance the ionic conductivity of CeO<sub>2</sub> without using dopants. Hydrogen treatment leads to the formation of chemical defects in CeO<sub>2</sub>, facilitating the reduction of Ce<sup>4+</sup> to Ce<sup>3+</sup>. Surface-modified CeO<sub>2- $\delta$</sub>  shows a conductivity and power density of 0.1 S cm<sup>-1</sup> and 660 mW cm<sup>-2</sup> at 550 °C.<sup>116</sup>

Synthesis methods play an essential role in the densification of the microstructure, affecting the conducting properties of SOFCs.<sup>117</sup> Different methods have been used to synthesise doped CeO<sub>2</sub>, such as co-precipitation, hydrothermal, sol-gel and solution combustion.<sup>117-123</sup> A comparative diagrammatic representation of the high- and low-temperature synthesis methods is given in Fig. 6. Synthesis of calcium-doped ceria electrolyte using two different synthesis methods, the solid-state reaction and sol-gel, resulted in varying microstructures. The sol-gel method resulted in well-defined homogeneous grains compared with the solid-state reaction method. Furthermore, the samples synthesised using sol-gel exhibited better conductivity than those synthesised by the solid-state reaction method. Therefore, the low-temperature synthesis method yielded better results.<sup>124</sup>

Sol-gel, co-precipitation, hydrothermal, *etc.*, are some low-temperature synthesis methods. Sol-gel is based on the polymerisation of molecular precursors. It involves the preparation of inorganic polymers or ceramics from a solution through a transformation from liquid precursors into a sol and then into a network structure called a gel. This high-purity process leads to a homogenised composition.<sup>125,126</sup> Smaller crystallite size, the low energy band gap value, and the homogeneous distribution of Sm<sup>3+</sup> in the ceria lattice, with its high ionic mobility, accounted for the high conductivity of (CeO<sub>2</sub>)<sub>0.96</sub>Sm<sub>0.04</sub> solid electrolyte synthesised by the sol-gel process.<sup>127</sup>

CeO<sub>2</sub>-based electrolytes exhibit rapid grain growth when sintered at high temperatures. This leads to poor mechanical stability, partial reduction of Ce<sup>4+</sup> to Ce<sup>3+</sup>, undesirable chemical expansion, high energy cost, phase diffusion and chemical interaction between the components, thus affecting the electrochemical performance of the cell.<sup>49,128</sup> Therefore, there has been a shift in the synthesis of CeO<sub>2</sub> towards lower-temperature methods. The literature reports far more publications on the low-temperature synthesis of CeO<sub>2</sub> electrolytes than the high-temperature methods. Low-temperature methods are generally wet chemical methods. They differ from powder methods in that the starting materials, in this case, are synthetically derived. This reduces the additional step of removing the impurities. Synthetically derived materials have uniform grain sizes and high purity without any agglomerates.



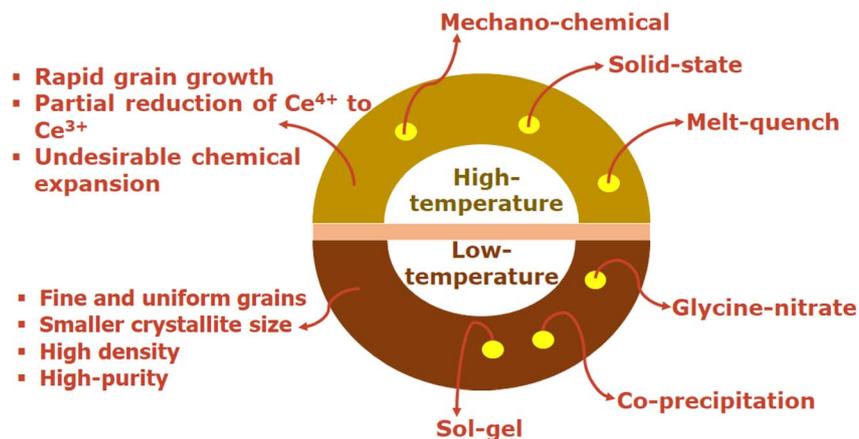


Fig. 6 Comparative representation of the high- and low-temperature synthesis methods.

Accardo *et al.* reported that the conductivity of 20 mol% of GDC is  $1.9 \times 10^{-2}$  to  $5.5 \times 10^{-2}$  S cm $^{-1}$  at 600 °C and 800 °C, respectively. However, doping of Bi $^{3+}$  increased the conductivity of GDC to  $3.1 \times 10^{-2}$ – $1.7 \times 10^{-1}$  S cm $^{-1}$  between 600 and 800 °C. The dense microstructure of the GDC pellets is composed of highly packed spherical grains due to the decrease in particle size ( $\sim$ 30 and 28 nm).<sup>117,129</sup> In another case, GDC powders were prepared using three complexing agents/fuels (ethylene glycol, glycerol, and tartaric acid) with sinterability strongly dependent on the microstructure, which in turn depended on the processing route.<sup>130</sup> Low-temperature methods usually result in crystallite and grain sizes in the nanometer and micrometre range, respectively. Smaller crystallite sizes favour better crystallinity with densities >90%. Single-phase Ce $_{0.8}$ Sm $_{0.2}$ O $_{1.9}$  synthesised by sol-gel with gelatin as a polymerising agent exhibited a dense, regular polygonal microstructure with a density, crystallite and particle size of > 97%, 12 nm and 15  $\mu$ m, respectively. The conductivity of the samples was in the order of 10 $^{-3}$  S cm $^{-1}$ , and the  $E_a$  was  $\sim$ 0.94 eV at 600 °C.<sup>131</sup>

In the case of doped ceria electrolytes, high ionic conductivity is essentially due to low  $E_a$ , which, in turn, is related to an optimal balance between elastic and electronic coulombic defect interactions. The Arrhenius curve is instrumental in identifying the  $E_a$  based on the temperature range. As shown in

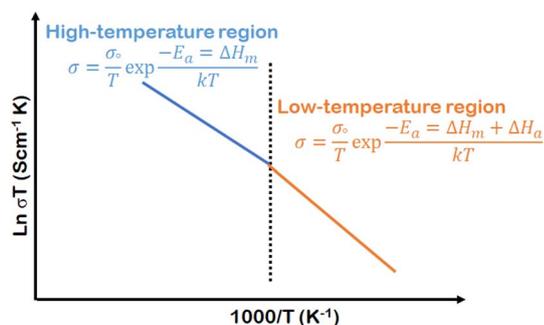


Fig. 7 Representative Arrhenius curve. The dotted line represents the change in the type of conduction.

Fig. 7, the Arrhenius curve is fitted separately with two lines, one for the high-temperature range and the other for the low-temperature range. The low-temperature line is slightly curved since the vacancies are temperature-dependent. In the low-temperature range, the  $E_a$  is the sum of enthalpies, association ( $\Delta H_a$ ) and migration ( $\Delta H_m$ ) for conduction, while for the high-temperature range, it is equal to only the  $\Delta H_m$ . This is because most oxygen vacancies are free to migrate in the high-temperature region. It is worth noting that for electrolytes to work in the low-temperature region,  $\Delta H_a$  should be a minimum.<sup>132–135</sup>

Other processes, such as microwave sintering, can further enhance densification. In a particular case, GDC nanoparticles with lithium as an additional dopant were used as a liquid-phase sintering aid during synthesis by the co-precipitation method. Furthermore, microwave sintering resulted in a decrease in the sintering temperature to 600 °C. The grain sizes of the Li-doped samples exhibited a grain size of 150 nm compared to pristine GDC (30 nm). At 600 °C, Li-doped samples showed an ionic conductivity of  $1 \times 10^{-2}$  S cm $^{-1}$  in air with an  $E_a$  of 0.53 eV.<sup>136</sup> As discussed before, the partial electronic conductivity at high temperatures is related to the reduction of Ce $^{4+}$  to Ce $^{3+}$ . The electrons thus created participate in the conduction process through the small polaron hopping mechanism. The decrease in the OCV due to this partial electronic conductivity also lowers the cell's overall efficiency and might lead to an electrical short-circuit. This is a paramount concern when synthesising doped ceria electrolytes at high temperatures. Therefore, many researchers are synthesising doped ceria electrolytes at low temperatures. Out of the various synthesis methods listed in Table 1, sol-gel and auto-combustion methods result in highly dense ( $\geq$ 95%) electrolytes with good conductivity values ( $\sim$ 10 $^{-1}$  S cm $^{-1}$ ).

Sometimes, liquid phase formation occurs at high temperatures, where a liquid phase is formed during the sintering process that coexists with the solid particles. The liquid during the liquid-phase sintering eliminates the solid-vapour interface. With further sintering, the driving force for the densification results from the decreasing liquid-vapour pore surface



Table 1 Comparative analysis of different ceria-based electrolytes

Composition	Synthesis method	$\rho_{\text{rel}}$ (%)	$\sigma$ (S cm <sup>-1</sup> )	$E_a$ (eV)	References
Ce <sub>0.8</sub> Gd <sub>0.2</sub> O <sub>1.95</sub>	Combustion	—	$3.34 \times 10^{-3}$ (680 °C)	—	105
Ce <sub>0.9</sub> Gd <sub>0.1</sub> O <sub>1.95</sub>	Sol-gel combustion	95	$1.67 \times 10^{-2}$ (600 °C)	0.81	92
Ce <sub>0.8</sub> Ca <sub>0.2</sub> O <sub>1.95</sub>	Combustion	—	$6.90 \times 10^{-4}$ (680 °C)	—	105
Ce <sub>0.9</sub> Dy <sub>0.1</sub> O <sub>2-<math>\delta</math></sub>	Solid state reaction	—	$1 \times 10^{-1.91}$ (650 °C)	0.71	115
Ce <sub>0.8</sub> Nd <sub>0.2</sub> O <sub>1.9</sub>	Molten salt	92	$0.15 \times 10^{-2}$ (600 °C)	0.87	142
Ce <sub>0.83</sub> Er <sub>0.17</sub> O <sub>2</sub>	Sol-gel	—	$1.57 \times 10^{-3}$ (700 °C)	—	143
Ce <sub>0.8</sub> Yb <sub>0.2</sub> O <sub>1.9</sub>	Solid state reaction	94	$1.30 \times 10^{-2}$ (800 °C)	1.07	144
Ce <sub>0.9</sub> Pr <sub>0.1</sub> O <sub>2</sub>	EDTA citrate	—	$1.21 \times 10^{-2}$ (700 °C)	1.28	109
Ce <sub>0.9</sub> La <sub>0.1</sub> O <sub>2-<math>\delta</math></sub>	Auto-combustion	—	$1.01 \times 10^{-2}$ (750 °C)	0.70	145
Ce <sub>0.8</sub> La <sub>0.2</sub> O <sub>2-<math>\delta</math></sub>	Co-precipitation	—	$0.81 \times 10^{-2}$ (650 °C)	0.86	165
Ce <sub>0.8</sub> Zr <sub>0.2</sub> O <sub>2-<math>\delta</math></sub>	Co-precipitation	—	$0.15 \times 10^{-2}$ (650 °C)	0.88	158
Ce <sub>0.7</sub> Sm <sub>0.3</sub> O <sub>1.85</sub>	Solid state reaction	97	$1.6 \times 10^{-3}$ (500 °C)	0.92	146
Ce <sub>0.8</sub> Sm <sub>0.2</sub> O <sub>1.95</sub>	Combustion	—	$8.32 \times 10^{-3}$ (680 °C)	—	105
Ce <sub>0.8</sub> Sm <sub>0.2</sub> O <sub>2-<math>\delta</math></sub>	Sucrose-pectin modified sol-gel	95	$1.0 \times 10^{-2}$ (600 °C)	0.89	134
Ce <sub>0.8</sub> Sm <sub>0.2</sub> O <sub>1.9</sub>	Solid state reaction	97	$5 \times 10^{-2}$ (800 °C)	1.03	147
Ce <sub>0.95</sub> Sm <sub>0.05</sub> O <sub>1.95</sub>	Auto-combustion	93	$3.26 \times 10^{-3}$ (500 °C)	0.87	148
Ce <sub>0.96</sub> Sm <sub>0.04</sub> O <sub>1.92</sub>	Sol-gel	—	$0.17 \times 10^{-2}$ (500 °C)	—	127
Ce <sub>0.8</sub> Gd <sub>0.10</sub> Pr <sub>0.10</sub> O <sub>1.90</sub>	Citric acid nitrate combustion	94	$5.1 \times 10^{-2}$ (750 °C)	0.58	135
Ce <sub>0.8</sub> Y <sub>0.18</sub> La <sub>0.02</sub> O <sub>2-<math>\delta</math></sub>	Sol-gel	97	$5.7 \times 10^{-2}$ (800 °C)	0.87	150
Ce <sub>0.6</sub> Zr <sub>0.2</sub> La <sub>0.2</sub> O <sub>2-<math>\delta</math></sub>	Co-precipitation	—	$0.32 \times 10^{-2}$ (650 °C)	0.87	165
Ce <sub>0.8</sub> Nd <sub>0.10</sub> Mg <sub>0.10</sub> O <sub>2-<math>\delta</math></sub>	Sol-gel	98	$26.81 \times 10^{-2}$ (450 °C)	0.74	152
Ce <sub>0.8</sub> Sm <sub>0.05</sub> Mg <sub>0.15</sub> O <sub>2-<math>\delta</math></sub>	Solid state reaction	96	$1.18 \times 10^{-2}$ (600 °C)	0.60	153
Ce <sub>0.8</sub> Er <sub>0.1</sub> Gd <sub>0.1</sub> O <sub>2</sub>	Sol-gel	—	$2 \times 10^{-3}$ (700 °C)	—	165
Ce <sub>0.875</sub> Gd <sub>0.1</sub> Sr <sub>0.025</sub> O <sub>1.925</sub>	Sol-gel combustion	96	$1.20 \times 10^{-2}$ (600 °C)	0.96	154
Ce <sub>0.65</sub> Sm <sub>0.2</sub> Bi <sub>0.15</sub> O <sub>1.825</sub>	Co-precipitation	94	$5.6 \times 10^{-2}$ (800 °C)	0.83	155
Ce <sub>0.80</sub> Ba <sub>0.10</sub> Ga <sub>0.10</sub> O <sub>3-<math>\delta</math></sub>	Co-precipitation	—	$7.1 \times 10^{-2}$ (650 °C)	0.46	156
Ce <sub>0.76</sub> La <sub>0.08</sub> Pr <sub>0.08</sub> Sm <sub>0.08</sub> O <sub>2-<math>\delta</math></sub>	Sol-gel auto combustion	98	$1.4 \times 10^{-2}$ (500 °C)	0.76	151
Ce <sub>0.80</sub> Sm <sub>0.10</sub> Er <sub>0.05</sub> Ba <sub>0.05</sub> O <sub>2-<math>\delta</math></sub>	Solid state reaction	89	$1.86 \times 10^{-2}$ (800 °C)	—	157
Ce <sub>0.76</sub> Pr <sub>0.08</sub> Sm <sub>0.08</sub> Gd <sub>0.08</sub> O <sub>2-<math>\delta</math></sub>	Sol-gel auto combustion	95	$1.86 \times 10^{-2}$ (600 °C)	0.56	158
Ce <sub>0.76</sub> Pr <sub>0.08</sub> Sm <sub>0.08</sub> Gd <sub>0.08</sub> O <sub>2-<math>\delta</math></sub>	Microwave-assisted sol-gel auto-combustion route	98	$3.47 \times 10^{-2}$ (600 °C)	0.69	159
Ce <sub>0.82</sub> La <sub>0.06</sub> Sm <sub>0.06</sub> Gd <sub>0.06</sub> O <sub>2-<math>\delta</math></sub>	Sol-gel	91	$3.8 \times 10^{-2}$ (600 °C)	0.59	160
Ce <sub>0.8</sub> Sm <sub>0.2</sub> O <sub>1.9</sub> ·(CuO) <sub>1.0</sub>	Combustion	96	$1.46 \times 10^{-2}$ (600 °C)	0.59	149
[Ce <sub>0.82</sub> La <sub>0.06</sub> Sm <sub>0.06</sub> Gd <sub>0.06</sub> O <sub>2-<math>\delta</math></sub> -(Li-Na) <sub>2</sub> CO <sub>3</sub> ]	Sol-gel	86	$4.2 \times 10^{-1}$ (600 °C)	1.51	161
[Ce <sub>0.76</sub> La <sub>0.08</sub> Pr <sub>0.08</sub> Sm <sub>0.08</sub> O <sub>2-<math>\delta</math></sub> -(Li-Na) <sub>2</sub> CO <sub>3</sub> ]	Solid state reaction	87	$4.6 \times 10^{-1}$ (600 °C)	1.03	169

area.<sup>137</sup> Sintering aids such as transition metals (cobalt, copper, lithium and iron) are used to increase the mobility of the atoms along the grain boundaries, promoting liquid phase sintering.<sup>111,138,139</sup> A comparison of the sintering aids (Li, Co, Cu, and Fe) used in samarium-doped CeO<sub>2</sub> (SDC) concluded that CuO was the best, as it lowered the sintering temperature between 750 and 1100 °C. CuO also has better relative density and maximum shrinkage rate than other electrolytes. Cobalt-sintered SDC had a more prominent grain size, while FeO had better conductivity than the others.<sup>140</sup> The impact of different dopants (Li, Co, Fe and Mg) on the sintering temperature of Ce<sub>0.9</sub>Pr<sub>0.1</sub>O<sub>2</sub> showed that the dopants had a different impact on the sintering temperature. Li and Co reduced the sintering temperature, Fe increased it, and Mg had little effect on the sintering temperature. The reduction in the sintering temperature resulted in rapid densification due to the formation of a liquid phase in the grain boundaries of the sample. This is attributed to the diffusion of the liquid phase under capillary action and the rearrangement of grains during the sintering process.<sup>49</sup> Ca doping also acts as a suitable sintering aid, and doping with an appropriate ratio of Gd/Ca also enhances conductivity. Ce<sub>0.8</sub>Gd<sub>0.12</sub>Ca<sub>0.06</sub>O<sub>1.87</sub> exhibits a relative density of

>95% when sintered at 1400 °C, denser than the ceria sintered at 1600 °C. This lowering of sintering temperature is due to grain refining, the modified gel-casting synthesis route, and Ca as a sintering aid. The samples had a conductivity and an  $E_a$  of 0.082 S cm<sup>-1</sup> and 0.786 eV, respectively, at 800 °C. The conductivity increases with increasing Ca content due to the majority of oxygen vacancies being fluid.<sup>141</sup>

Each cell component must be chemically and thermally stable. All the SOFC components must have good chemical compatibility; there should be no or negligible mismatch. If this mismatch persists, it will lead to cell degradation. Also, the components must be stable in both oxidising and reducing oxygen partial pressure atmospheres. During SOFC fabrication, the long duration of operation often leads to mechanical and thermal stress. However, the addition of dopants improves the mechanical strength and leads to an increase in CTE. Therefore, research is needed to balance these properties to avoid any mismatch during operation. The mismatch in CTE among various SOFC components leads to interface delamination; in fact, multiple SOFC components form different interfaces, as shown in our recent review article.<sup>10</sup> Also, the increase in the oxygen vacancies contributes to weakening the binding energy,



which increases CTE. In the planar design of SOFCs, electrolytes form interfaces with the cathode, anode and sealants. If the CTE largely differs in every component, a SOFC device will not form. However, with the proper selection of dopants, CTE can be tailored accordingly. In the case of anode-supported SOFCs, the CTE difference between electrolyte and the anode substrate leads to a significant thermoelastic bending of the cells that causes cell fracture in stack assembling.<sup>161–163</sup> La-doped CeO<sub>2</sub> exhibited a CTE of  $13.4 \times 10^{-6}$  per °C without compromising the conductivity ( $0.81 \times 10^{-2}$  S cm<sup>-1</sup> at 650 °C).<sup>164</sup> However, tri-doped ceria, Ce<sub>0.76</sub>Pr<sub>0.08</sub>Sm<sub>0.08</sub>Gd<sub>0.08</sub>O<sub>2-δ</sub>, exhibits comparable CTE ( $13.25 \times 10^{-6}$  per °C) between 30 and 800 °C.<sup>158</sup>

Mechanical properties must be checked and verified thoroughly for any fuel cell design under all conditions, *i.e.*, operation, start-up, and shutdown. Wettability, joint strength, fracture toughness, elastic modulus, and hardness are some pointers to be checked for SOFC materials. The change in the crystal structure affects the elastic modulus and stiffness of SOFC materials.<sup>165–168</sup> The correlation between electrical and mechanical properties of the La<sub>0.90</sub>Sr<sub>0.10</sub>Ga<sub>0.8</sub>Mg<sub>0.2</sub>O<sub>3-δ</sub> and La<sub>0.85</sub>Sr<sub>0.15</sub>Ga<sub>0.8</sub>Mg<sub>0.2</sub>O<sub>3-δ</sub> ceramics showed that significant segregation of secondary phases occurs at the grain boundaries. This led to a substantial drop in the hardness and grain boundary conductivity, which decreased the total ionic conductivity.<sup>170</sup> An increase in sintering temperature facilitates enhanced grain growth, reducing the grain boundary area per unit volume. Consequently, these grains are less resistant to localised plastic deformation and exhibit poorer hardness.<sup>171</sup>

Enhancement of strength over that of zirconia would lower the likelihood of fracture and enhance ionic conductivity at the same thickness, which would lower ohmic loss. Materials such as ceria would enable highly dependable and energy-efficient SOFCs.<sup>172</sup> It has been observed that ceria-based materials exhibit slightly lower hardness and toughness values compared with commonly used electrolyte materials such as 8-YSZ (12.83 GPa and 2.73 MPa√m), as shown in Table 2.<sup>173–176</sup> The mechanical strength can be improved without compromising the electrical conductivity by reduction-annealing the sample. In such a case, a compressed surface layer is formed by the chemical expansion that occurs during contact reduction of its surface.<sup>177</sup> Doping CeO<sub>2</sub> enhances the fracture toughness of the solid solution by promoting a greater extent of stress-induced tetragonal to monoclinic phase transformation.<sup>178</sup>

**Table 2** A comparison of hardness and fracture toughness of some of the ceria-based electrolytes with those of 8-YSZ

Composition	Hardness (GPa)	Fracture toughness (MPa√m)
8-YSZ	12.83	2.73
GDC	5.46	1.16
Ce <sub>0.8</sub> Y <sub>0.2</sub> O <sub>2</sub>	7.9	2.16
Ce <sub>0.8</sub> Sm <sub>0.2</sub> O <sub>2</sub>	8.2	2.3
Ce <sub>0.8</sub> Sm <sub>0.1</sub> Y <sub>0.1</sub> O <sub>2</sub>	8.34	2.28
Gd <sub>0.1</sub> Ce <sub>0.89</sub> Ge <sub>0.01</sub> O <sub>0.01</sub>	10.85	3.18
Ce <sub>0.9</sub> Sm <sub>0.1</sub> O <sub>1.95</sub>	5.37	2.95

## 4. Approaches to improve conductivity and cell parameters

The reduction of Ce<sup>4+</sup> to Ce<sup>3+</sup> under low oxygen partial pressures leads to high electronic conductivity; therefore, they show low OCV and low efficiency due to the leakage current. Thus, there are different ways through which these problems could be solved. Some of the suggestions to solve the above issues related to ceria-based electrolytes are given in the following points:

(1) Nanomaterials and thin films can effectively improve the properties of ceria-based electrolytes. It is generally observed that compared to conventional single crystalline and polycrystalline materials, the ionic conductivities of nanocrystalline materials such as cubic zirconia, ceria and titania are much higher. It is reported that CeO<sub>2</sub> nanoparticles under high pressure exhibit an ionic conductivity of  $3 \times 10^{-3}$  S cm<sup>-1</sup> at 300 °C under 5 GPa for 6 mol% SDC nanoparticles.<sup>179,180</sup> Apart from nanoparticles, GDC thin film electrolytes have a higher power density than YSZ electrolytes. This is due to the higher conductivity of the GDC electrolyte against that of the YSZ electrolyte and the expansion of the electrochemical reaction zone. The improved ionic conductivity increases the oxygen transport rate at the electrolyte–electrode interface, which reduces the electrode overpotential. The surface area availability increases significantly in nanoparticles compared to bulk materials.<sup>181–183</sup>

(2) Nanocomposite electrolyte materials have the potential for use in LT-SOFCs due to their high ionic conductivity at low temperatures and low cost. Fundamentally, a typical nanocomposite (CeO<sub>2-δ</sub>/CeO<sub>2</sub>, GDC/CoFe<sub>2</sub>O<sub>4</sub>, YSZ/SrTiO<sub>3</sub>, *etc.*) consists of a core–shell type structure on a nano-scale. It has a core (ceria) and a salt (carbonate or another oxide) that develops a shell layer covering the core. The functionality of nanocomposites is determined by the interfaces between the constituent phases, which lead to fast ionic transport at the interfaces. Different ceria-based nanocomposites, such as ceria-carbonate, ceria-halide, ceria-sulphate, ceria-hydroxide, ceria-alumina and ceria-oxide, have been of significant interest for use as SOFC electrolyte materials.<sup>116,184–186</sup> Generally, ionic conductivity and power density of ceria-carbonate nanocomposites have been reported to be  $>0.1$  S cm<sup>-1</sup> at 300 °C and  $\sim 1000$  mW cm<sup>-2</sup> between 450 and 500 °C, respectively.<sup>187</sup> At slightly higher temperatures (600–650 °C), the protonic conductivity of Sm<sub>0.2</sub>Ce<sub>0.8</sub>O<sub>2</sub>–Na<sub>2</sub>CO<sub>3</sub> is reported to be  $\sim 0.044$  S cm<sup>-1</sup> with a power density of 281.5 mW cm<sup>-2</sup>. These results are much higher than those of single-phase oxide proton-conducting electrolytes.<sup>188</sup> Shah *et al.* observed that a 10% coating of Na<sub>2</sub>CO<sub>3</sub> on GDC generates appreciable O<sup>2-</sup> vacancies compared to GDC.<sup>180</sup> This led to high power density (968 mW cm<sup>-2</sup>) and high ionic conductivity (0.2 S cm<sup>-1</sup> at 520 °C) with sufficient OCV (1.013 V). It was due to the formation of a composite core–shell heterostructure between GDC and amorphous Na<sub>2</sub>CO<sub>3</sub>. The formation of a junction suppressed the electronic conduction while enhancing the ionic transportation through the electrolyte membrane. A binary composite, (Li/Na)<sub>2</sub>CO<sub>3</sub> – SDC, exhibited a high conductivity



and cell performance of  $0.31 \text{ S cm}^{-1}$  and  $617 \text{ mW cm}^{-2}$ , respectively, at  $600 \text{ }^\circ\text{C}$  since the interface acted as a superionic highway, which enabled the transportation of ions.<sup>189</sup> Composites with SDC reach power densities as high as  $640$  and  $760 \text{ mW cm}^{-2}$  at low temperatures of  $500$  and  $550 \text{ }^\circ\text{C}$ , respectively.<sup>190</sup> In another study, the addition of a  $\text{Ni}_{0.8}\text{Co}_{0.15}\text{Al}_{0.05}\text{Li}$  membrane into  $\text{Ce}_{0.8}\text{Sm}_{0.2}\text{O}_{2-\delta}\text{-Na}_2\text{CO}_3$  electrolyte eliminated the polarisation between different interfaces and resulted in a high-power density of  $1072 \text{ mW cm}^{-2}$  at  $550 \text{ }^\circ\text{C}$ .<sup>191</sup> Compared to pure  $\text{NaFeO}_2$ , composites such as  $\text{CeO}_2$ -coated  $\text{NaFeO}_2$  have a power output of  $727 \text{ mW cm}^{-2}$  and an OCV of  $1.06 \text{ V}$  at  $550 \text{ }^\circ\text{C}$ . This is due to the hetero-interfaces between  $\text{NaFeO}_2$  and  $\text{CeO}_2$  that provide a fast oxide ion conducting path and to  $\text{CeO}_2$  that creates more oxygen vacancies for protonic transportation. Ionic conduction through the interface is much easier than structural bulk conduction. Principally, point defects in ceria-based materials are responsible for originating ionic charge carriers. Therefore, in LT-SOFCs, interface conduction should be promoted as a new approach for ion-conducting electrolytes.<sup>192,193</sup>

(3) Another solution is to make use of electron-blocking layers. A  $\text{BaCeO}_3$ -Ni-based composite anode achieves higher OCV due to the reaction of diffused Ba ions with doped ceria electrolyte during the sintering process, forming an electron-blocking interlayer. This interlayer eliminates the problem of internal short-circuiting in doped ceria electrolytes. Apart from  $\text{BaCeO}_3$ ,  $\text{ZrO}_2$ ,  $\text{Bi}_2\text{O}_3$ , and  $\text{SrCeO}_3$  are used as electron-blocking layers.<sup>79,194</sup> Another way to solve the short-circuiting problem is to use the bi- and tri-layer electrolyte strategy. The bi-layer electrolyte strategy uses a pure oxygen ion-conducting YSZ layer to block electron conduction. On the other hand, the tri-layer electrolyte system consists of a GDC layer on the anode side, a YSZ electron-blocking layer in the middle and a second GDC buffer layer on the cathode side.<sup>195</sup> In a tri-layer electrolyte system, the first dense GDC electrolyte is fabricated by co-sintering a thin, screen-printed GDC layer with an anode support ( $\text{NiO}$ -8YSZ substrate and a  $\text{NiO}$ -GDC anode). In contrast, the two electrolyte layers are deposited *via* physical vapour deposition. For a tri-doped electrolyte system, the electrolyte resistance is only  $0.01 \text{ } \Omega \text{ cm}^{-2}$  with a power density of  $1.2 \text{ W cm}^{-2}$  at  $650 \text{ }^\circ\text{C}$ .<sup>195</sup> However, problems with low ionic conductivity, low chemical and mechanical stability, undesirable solid solutions, and thermal mismatch of the multilayer electrolytes pose issues in utilising the electron-blocking layer method.<sup>194</sup>

(4) A new approach was proposed wherein surface doping of  $\text{Al}^{3+}$  into  $\text{Ce}^{4+}$  created surface defects and surface  $\text{O}^{2-}$  vacancies at the interface of  $\text{CeAlO}_2$ . This approach enhanced the ionic conductivity ( $0.19 \text{ S cm}^{-1}$ ) and power density ( $1020 \text{ mW cm}^{-2}$ ) at  $520 \text{ }^\circ\text{C}$ . It was observed that surface doping required band alignment between  $\text{CeO}_2$  and  $\text{CeAlO}_2$  due to the difference in the Fermi level. This established a space charge region constituting a built-in field, enhancing charge transportation and minimising e-conduction.<sup>196</sup> Co-doping and tri-doping have effectively been observed to reduce the sintering temperature and enhance the conductivity of ceria-based electrolytes, as observed from the data listed in Table 1. They generate higher

oxygen vacancies than single-cation doping, resulting in higher diffusion due to minimum distortion. Also, ceria-based composites have high conductivities.

Based on the solutions mentioned above, it can be concluded that ceria-based materials show enhanced properties when used in doped, composites, bilayered and hetero-structured composite forms. Nanocomposites, electron-blocking layered structures and surface doping in  $\text{CeO}_2$  resulted in very high power densities of  $>1000 \text{ mW cm}^{-2}$ , thereby increasing the long-term stability of these oxides.

## 5. Conclusion and future direction for research

Solid oxide fuel/electrolyser cells (SOFCs/SOECs) are versatile and multipurpose devices that produce electricity, water, hydrogen and oxygen for different applications. The electrolyte is an essential and integral part of an SOFC. The present article discusses the different aspects that affect the ionic conductivity of ceria-based electrolytes for LT- and IT-SOFCs to make them cost-effective and increase their commercial viability. Gadolinium-doped ceria (GDC) and samarium-doped ceria (SDC) are very good and suitable ionic conducting electrolyte materials for LT- and IT-SOFCs due to the comparable ionic radii of  $\text{Gd}^{3+}$  ( $r_{\text{ionic}} = 0.938 \text{ \AA}$ ) and  $\text{Sm}^{3+}$  ( $r_{\text{ionic}} = 0.958 \text{ \AA}$ ) to  $\text{Ce}^{4+}$  ( $r_{\text{ionic}} = 0.87 \text{ \AA}$ ). The solid solubility limit of both dopants is the highest compared to that of other dopants. However, a high concentration of dopants leads to secondary phase formations and clustering of oxygen vacancies, reducing ionic conductivity.

Different approaches can be used to increase the solid solubility of the dopants, optimise the microstructure and prevent the reduction of  $\text{Ce}^{4+}$  to  $\text{Ce}^{3+}$ . Surface engineering, chemical routes and thin film technology can be used to address these issues. Apart from the processing methods, different mechanisms such as utilising multi-dopants, nanocomposites, electron-blocking layers, and  $\text{CeO}_{2-\delta}/\text{CeO}_2$  composites improve the conductivity of ceria-based electrolytes significantly. The densification of the electrolytes can be achieved by using sintering aids, particularly the addition of small amounts of alkali and alkaline earth metal oxides during processing. Alkali metal oxides increase the liquid phase sintering and wettability of  $\text{CeO}_2$ , while alkaline earth metal oxides avoid the reduction of cerium. As a future prospect, double dopants (alkali and alkaline earth oxides) could be beneficial to achieve high density with a reduced chance of cerium reduction in doped  $\text{CeO}_2$  electrolyte. Additionally, studies on small quantities of nano-size sintering aids and sintering of composites, *i.e.* two suitable ionic conducting materials (doped  $\text{CeO}_2$ -bismuth vanadate, doped  $\text{CeO}_2$ - $\text{LaAlO}_3$ , *etc.*) at appropriate temperatures and durations can be synthesised to obtain highly dense electrolytes for LT- and IT-SOFCs. Using double-layered electrolytes such as GDC-YSZ can also be a good approach to reduce interface-related issues with improved conductivity. Proton-conducting electrolytes could also be explored as electrolytes for intermediate temperature SOFCs/SOECs.



## Data availability

The datasets used to support the findings of this study are available in the referenced publications.

## Author contributions

Paramvir Kaur – conceptualization; data curation; formal analysis; visualization; writing-original draft. K. Singh – conceptualization; funding acquisition; supervision; validation; visualization; writing-review & editing.

## Conflicts of interest

There are no conflicts of interest to declare.

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