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A leveling–shielding dual strategy enabling stable zinc anodes to exhibit ultra-low interfacial impedance

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Aqueous zinc-ion batteries have demonstrated great potential for large-scale energy storage, but still suffer from severe dendrites and corrosion problems. Uneven distributions of crystalline planes and passivation layers on the zinc anode are the key factors causing dendrites and corrosion. However, the synergistic construction of uniform crystal planes and shielding layers is still challenging. Herein, we propose a novel leveling–shielding dual strategy to stabilize the zinc anode. The low-melting-point indium (In) layer not only serves as a leveling agent to repair surface defects, but also induces uniform and fast deposition of zinc by exposing a single $(101)_{In}$ plane on the anode. Besides, the outer ZnF_2 shielding layer can inhibit corrosion and accelerate the de-solvation of $Zn(H_2O)_6^{2+}$, which improves the electrochemical reaction kinetics. As a result, the $ZnF_2@In@Zn$ symmetric cell shows an ultra-low interfacial impedance of $<10\ \Omega$ and a stable cycle life of >2800 h with a low polarization voltage of 21.8 mV at 5 mA cm^{-2} and 2 mAh cm^{-2}, compared with bare Zn (140 h and 75.8 mV). Besides, the $ZnF_2@In@Zn//NH_4V_4O_{10}$ full cell maintains a high capacity of 112.4 mAh g^{-1} with a retention rate of 79.5% after 10 000 cycles at 3 A g^{-1}. This work provides a novel, effective leveling–shielding dual strategy for interfacial modification of zinc anodes, which can also be applied in other metal anodes.

1 Introduction

During the critical stage of global energy structure transformation, energy security has become a core issue for the sustainable development of human civilization.[1,2] Currently, fossil fuels still dominate the global primary energy consumption structure (accounting for 79.6%), and 73.2% of the greenhouse gas emissions stem from energy activities.[3] While clean energy technologies like photovoltaics and wind power can reduce carbon emission intensity by over 90%, their inherent geographical unevenness and intermittent nature necessitate supporting energy storage systems for stable power output.[4–6] Among existing energy storage technologies, lithium-ion batteries are subject to high costs and thermal runaway risks,

which hinder their ability to meet large-scale storage needs;[7] pumped storage, though economical, demands strict geographical conditions (requiring elevation drops exceeding 400 m).[8] Thanks to high volumetric energy density (5850 mAh cm^{-3}), cost-effectiveness, and inherent non-flammability, aqueous zinc ion batteries have emerged as promising candidates for large-scale energy storage.[9–12] However, uncontrolled dendrite growth and interfacial side reactions of the zinc anode during cycling degrade battery cycle stability, thereby restricting industrial application.[13–15]

The uneven distribution of crystal planes and passivation layers (such as $Zn_2(OH)_2CO_3$ and ZnO) on the zinc anode is a key factor leading to zinc dendrites and corrosion. Various crystal planes, including $(002)_{Zn}$, $(100)_{Zn}$ and $(101)_{Zn}$, are randomly distributed on the initial zinc anode. Due to differences in the adsorption energy of zinc on different crystal planes, the zinc anode exhibits uneven zinc deposition dynamics across various regions.[16] Meanwhile, the corrosion potentials of different crystal planes vary, leading to the uneven distribution of corrosion and passivation layers.[17,18] These differences in deposition dynamics and the uneven distribution of corrosion and passivation layers synergistically accelerate dendrite growth. Additionally, owing to the low overpotential of zinc (-0.76 V *vs.* the Hydrogen Evolution Reaction (HER)), prolonged corrosion is thermodynamically inevitable in weakly acidic electrolyte (Fig. 1a). Among numerous modification strategies,

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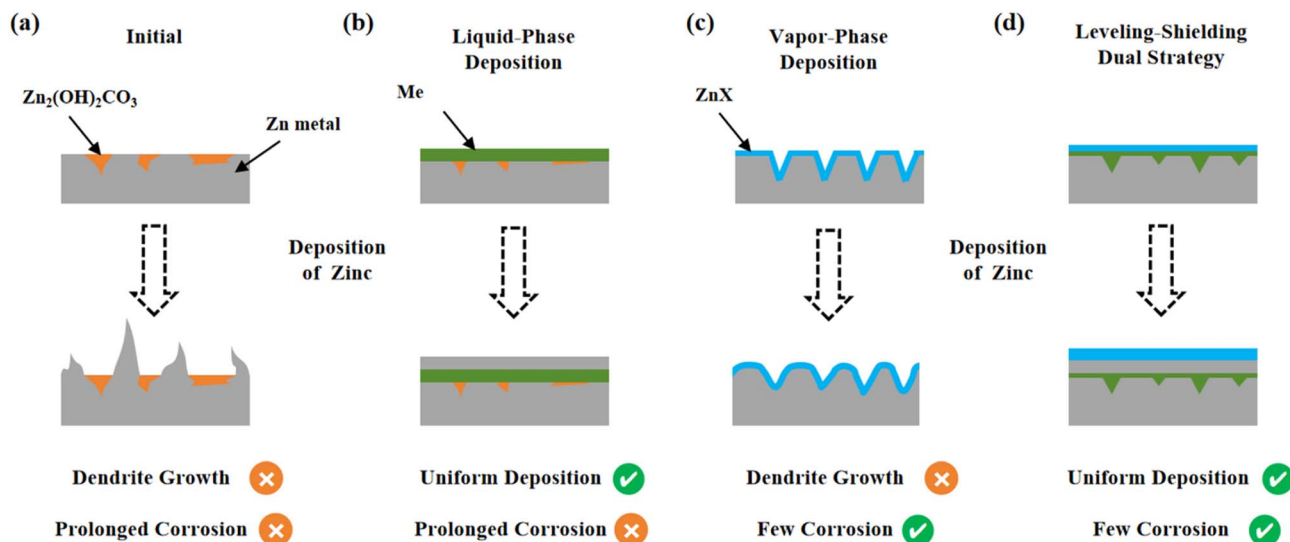
Fig. 1 Schematic illustration of dendrite growth and corrosion at the modified interface. (a) Bare Zn, (b) metal modified layer by liquid-phase deposition, (c) metal compound modified layer by vapor-phase deposition and (d) metal and metal compound composite layer by a leveling–shielding dual strategy.

such as using electrolyte additives,[19,20] high-concentration electrolytes,[21,22] and hydrogel electrolytes,[23,24] significant progress has been achieved in mitigating dendrite formation and corrosion. However, these approaches have exhibited limited efficacy in addressing the uneven distributions of crystal planes and passivation layers on the anode. Interfacial modification, which can improve the surface properties of the anode, has garnered substantial research attention and is considered a promising strategy to solve these challenges.[25,26]

Commonly used interface modification methods can be categorized into physical coating, liquid-phase deposition, and vapor-phase deposition. Physical coating relies on adhesive bonding with the anode, which struggles to achieve molecular-level coverage and offers limited enhancement to the properties of initial zinc.[26] In contrast, liquid-phase and vapor-phase deposition are *in situ* growth methods requiring chemical reactions with zinc metal, which can improve the surface properties of initial zinc. For instance, some high-potential metals (such as In,[27] Cu[28] and Sn[29]) can replace zinc through liquid-phase deposition to form a metal modification layer on the zinc anode. The specific crystal planes of these metals facilitate uniform zinc deposition (Fig. 1b). However, the corrosion issue of deposited zinc remains unsolved. Depositing metal compounds (such as ZnF_2,[30–32] $ZnSe$[33] and ZnS[33]) with high ionic conductivity on the anode through vapor-phase deposition can hinder the contact between the deposited zinc and the electrolyte, thereby inhibiting the prolonged corrosion of zinc (Fig. 1c). However, the decomposition of $Zn_2(OH)_2CO_3$ results in holes on the anode during vapor-phase deposition, which is detrimental to uniform deposition. Additionally, the uneven distribution of zinc crystal planes within the coating layer still poses the risk of dendrite growth. Therefore, it is urgent to develop a modified layer with uniformly distributed crystal planes and passivation layers to simultaneously inhibit dendrites and corrosion.

Herein, we propose a leveling–shielding dual strategy to construct a stable Zn anode (Fig. 1d). The low-melting-point In metal serves as a leveling agent to repair surface defects caused by the decomposition of $Zn_2(OH)_2CO_3$ during heat treatment. The exposed single $(101)_{In}$ plane can induce uniform and rapid deposition of zinc. The outermost ZnF_2 shielding layer can inhibit the corrosion of deposited zinc and accelerate the desolvation process of $Zn(H_2O)_6^{2+}$, which further improves the electrochemical reaction kinetics. As a result, the $ZnF_2@In@Zn$ symmetric cell demonstrates an ultra-low interfacial impedance of less than 10 Ω and achieves stable cycling for over 2800 h with a polarization voltage of 21.8 mV at 5 mA cm^{-2} and 2 mAh cm^{-2}, a significant improvement over that of bare Zn (140 h, 75.8 mV). Additionally, the $ZnF_2@In@Zn//NH_4V_4O_{10}$ full cell retains a capacity of 112.4 mAh g^{-1} after 10 000 cycles at 3 A g^{-1}, corresponding to a capacity retention rate of 79.5%.

2 Results and discussion

The leveling–shielding dual strategy involves two stages of *in situ* deposition: the In metal layer is constructed through liquid-phase deposition and the ZnF_2 layer is constructed by vapor-phase deposition (Fig. 2a). Based on the Zn–In binary metal phase diagram (Fig. S1), during vapor-phase deposition, the In metal and surface Zn metal undergo eutectic melting to form a homogeneous melt. Given that Zn has a lower potential than In, HF produced by the decomposition of NH_4F selectively reacts with Zn to produce ZnF_2, which deposits on the surface. As cooling begins, Zn preferentially precipitates from the melt with the formation of grain boundaries. With further cooling, the ZnIn alloy can infiltrate into the grain boundaries and holes, precipitating within them and effectively healing surface defects. The reactions involved in this entire process are as follows:
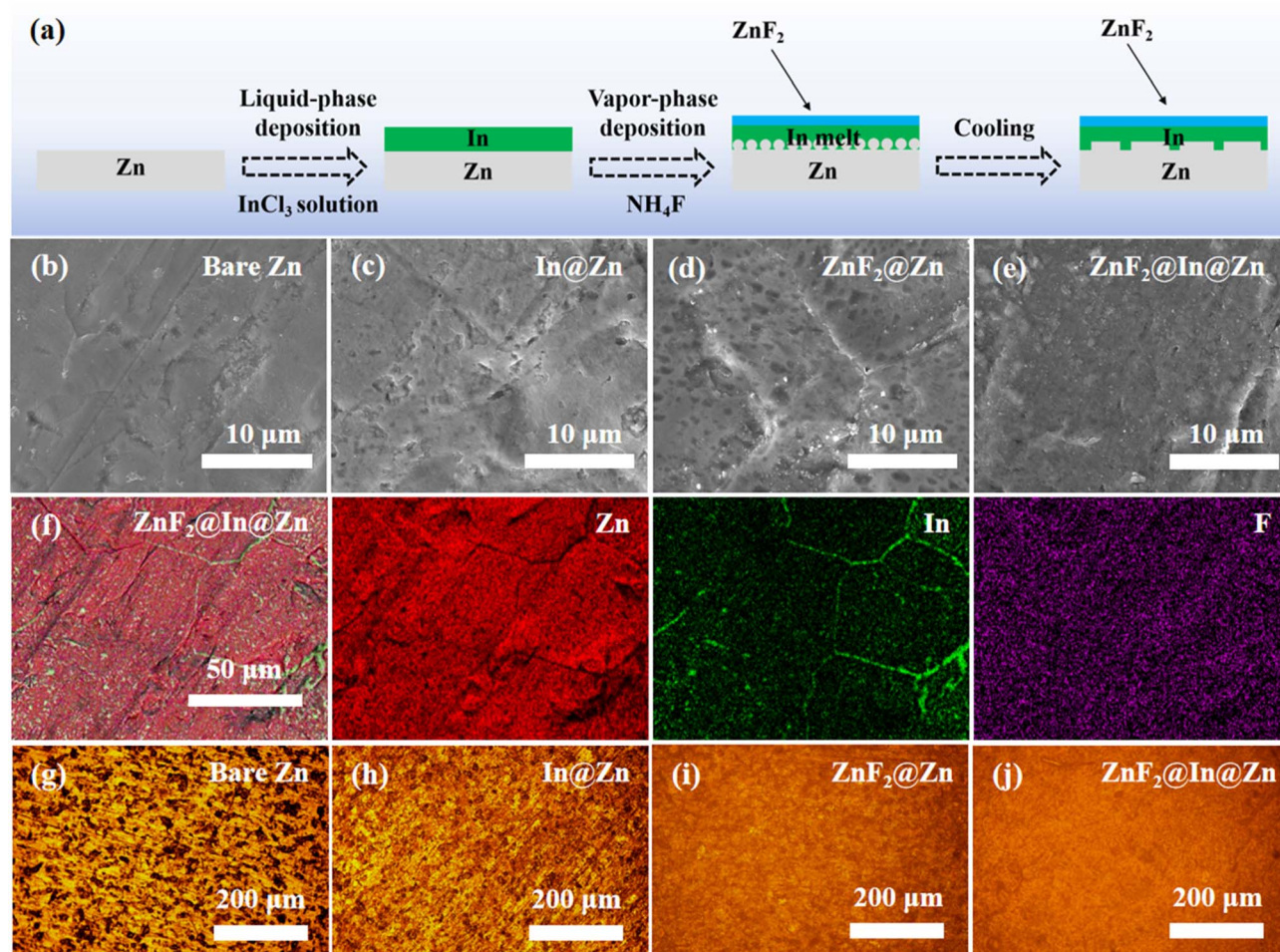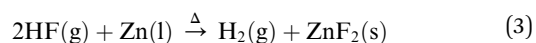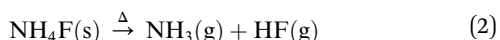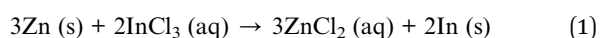
Fig. 2 Surface morphology analysis of various anodes. (a) Schematic diagram of the preparation of a ZnF$_2$@In@Zn anode by the leveling–shielding dual strategy. SEM images of (b) bare Zn, (c) In@Zn, (d) ZnF$_2$@Zn and (e) ZnF$_2$@In@Zn. (f) Mapping images of ZnF$_2$@In@Zn. Metallographic microscope image of (g) bare Zn, (h) In@Zn, (i) ZnF$_2$@Zn and (j) ZnF$_2$@In@Zn.

$$3Zn\ (s) + 2InCl_3\ (aq) \rightarrow 3ZnCl_2\ (aq) + 2In\ (s) \quad (1)$$

$$NH_4F(s) \xrightarrow{\Delta} NH_3(g) + HF(g) \quad (2)$$

$$2HF(g) + Zn(l) \xrightarrow{\Delta} H_2(g) + ZnF_2(s) \quad (3)$$

Scanning electron microscopy (SEM) reveals the morphological evolution during the construction of the ZnF$_2$@In@Zn anode. The initial zinc surface is smooth and flat (Fig. 2b and S2a). After liquid-phase deposition, the surface morphology of the In@Zn anode remains largely unchanged, possibly due to the strong binding energy between In and Zn, which allows In to be embedded within the Zn lattice to form a ZnIn alloy (Fig. 2c and S2b). In the absence of In, tiny holes emerge on the surface of ZnF$_2$@Zn (Fig. 2d and S2c). In contrast, the ZnF$_2$@In@Zn anode maintains a relatively flat surface (Fig. 2e and S2d). Compared to ZnF$_2$@Zn, the heat-treated Zn exhibits larger and denser holes in the Ar atmospheres (Fig. S2e and f). This indicates that the holes are formed by the decomposition of Zn$_2$(OH)$_2$CO$_3$ on the zinc surface. Notably, the ZnF$_2$ produced by vapor-phase deposition

can partially fill these holes. The mapping diagram illustrates the distribution of elements. The surface of bare Zn is covered with C, O, and Zn elements, and EDS also detected a certain amount of C and O elements, indicating the presence of Zn$_2$(OH)$_2$CO$_3$ on the bare Zn surface (Fig. S3). In both the In@Zn and ZnF$_2$@Zn anodes, elements are uniformly distributed, indicating an even modification layer on the zinc surface (Fig. S4). For the ZnF$_2$@-In@Zn anode, F and Zn elements are also evenly distributed, showing that the ZnF$_2$ layer is uniformly constructed (Fig. 2f). However, In distribution on the ZnF$_2$@In@Zn surface is localized in spots and lines (Fig. 2f). This suggests that during cooling, In metal fills the grain boundaries and pores of zinc, repairing surface defects. Besides, the ZnF$_2$@In@Zn anode exhibits a distinct trilayer structure. Layer A is a ZnF$_2$ layer, layer B mainly consists of In, and layer C is primarily composed of Zn. The thickness of the ZnF$_2$ layer is approximately 6.8 μm and the thickness of the In layer is about 1 μm (Fig. S5). As shown in the In element distribution mapping, In metal tends to concentrate in the depressions. This further confirms that In metal fills the grain boundaries and pores of zinc. The metallographic microscope image reveals the occurrence form of metals on the surface. The

inert passivation layer appears black due to its low reflectivity, whereas metals with high reflectivity exhibit a bright golden color. On the bare Zn surface, bright golden and black spots are randomly distributed, indicating an uneven passivation layer

(Fig. 2g). For the In@Zn anode, the black spots are reduced, yet the color distribution remains non-uniform, suggesting that some passivation layer exists (Fig. 2h). Thanks to the uniform
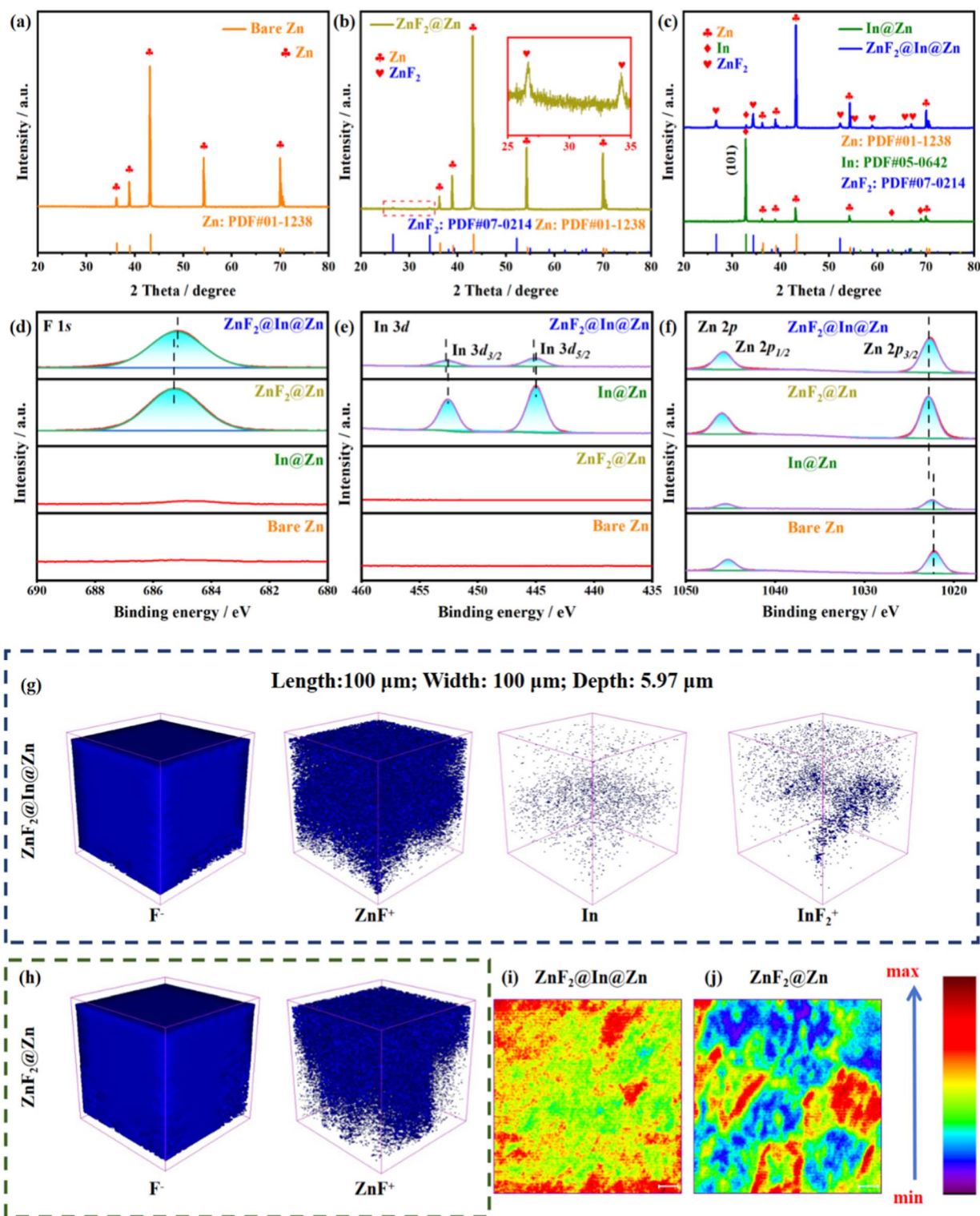

Fig. 3 Study of element distribution on various anode surfaces. XRD spectra of (a) bare Zn, (b) ZnF$_2$@Zn, (c) In@Zn and ZnF$_2$@In@Zn. High-resolution (d) F 1s, (e) In 3d and (f) Zn 2p XPS spectra. TOF-SIMS images of (g) ZnF$_2$@In@Zn and (h) ZnF$_2$@Zn. ZnF$^+$ signal intensity of (i) ZnF$_2$@In@Zn and (j) ZnF$_2$@Zn (length: 100 μm; width: 100 μm; depth: 5.97 μm).

distribution of ZnF_2, the ZnF_2@Zn and ZnF_2@In@Zn anodes show a uniform orange-yellow color (Fig. 2i and j).

X-ray diffraction (XRD) and X-ray photoelectron spectroscopy (XPS) reveal the surface material composition. The XRD pattern of bare Zn corresponds well with the standard spectrum (PDF #01-1238) (Fig. 3a). A weak peak attributable to ZnF_2, in accordance with PDF #07-0214, is present in the diffraction profile of the ZnF_2@Zn anode (Fig. 3b). For the In@Zn anode, an intense indium peak at 33°, linked to the (101) plane and consistent with PDF #05-0642, is observed. This indicates substantial exposure of the $(101)_{In}$ plane on the anode surface (Fig. 3c). Compared with the ZnF_2@Zn anode, the ZnF_2@In@Zn anode exhibits a more pronounced ZnF_2 peak, suggesting that the melt facilitates the fluorination reaction (Fig. 3c). Additionally, the ZnF_2@In@Zn anode shows a reduced In peak intensity, with only the $(101)_{In}$ plane detectable, which could be attributed to the ZnF_2 layer partially shielding the In signal (Fig. 3c). It is worth noting that the ZnF_2@In@Zn anode displays a higher $I_{(101)Zn}/(I_{(002)Zn} + I_{(100)Zn})$ peak intensity ratio ($\sim$6.87) compared to bare Zn ($\sim$3.99) (Fig. S6a). Conversely, the In@Zn and ZnF_2@Zn anodes exhibit lower ratios than bare Zn (Fig. S6b). This implies that the replacement and fluorination processes do not enhance the exposure of the $(101)_{Zn}$ plane. The increased exposure of the $(101)_{Zn}$ plane on the ZnF_2@In@Zn anode may result from the recrystallization of the Zn–In melt along the (101) plane. The full XPS spectrum detects Zn, F, and In peaks on the ZnF_2@In@Zn anode (Fig. S7). The Cl peak is found at the In@Zn anode, attributed to residual Cl from the $InCl_3$ solution (Fig. S7). In the high-resolution F 1s XPS spectrum, the F peak in ZnF_2@In@Zn is right-shifted relative to ZnF_2@Zn (Fig. 3d), likely due to the binding of some of the In and F. The high-resolution In 3d XPS spectrum shows that the In peak in ZnF_2@In@Zn is left-shifted compared to In@Zn (Fig. 3e), further indicating the binding of In and F. In the high-resolution Zn 2p XPS spectrum, ZnF_2@In@Zn and ZnF_2@Zn show left-shifted peaks compared to bare Zn and In@Zn (Fig. 3f), which is because the binding energy between Zn and F is stronger than that between Zn and O.

Time-of-flight secondary ion mass spectrometry (TOF-SIMS) offers a more intuitive analysis of the elemental distribution on the surfaces of the ZnF_2@Zn and ZnF_2@In@Zn anodes. Both anode surfaces are densely covered with F^- and ZnF^+ signals, indicating complete coverage of the outermost layer by ZnF_2 (Fig. 3g and h). In the ZnF_2@In@Zn anode, the weak In signal suggests that the In layer is enveloped by the ZnF_2 layer, which can suppress the corrosion of deposited zinc. Furthermore, the detection of InF_2^+ signals in the ZnF_2@In@Zn anode provides additional evidence of In–F bonding (Fig. 3g). The intensity of the ZnF^+ signal on the ZnF_2@In@Zn anode is stronger and more uniform than that on the ZnF_2@Zn anode (Fig. 3i and j). This may be because the melt accelerates the fluorination reaction, enhancing its completeness, and exhibits good wettability, allowing it to spread evenly across the anode surface.

Benefiting from its surface defect repair and the abundant coverage of ZnF_2, the ZnF_2@In@Zn anode demonstrates ultrafast electrochemical kinetics, achieving polarization voltages of

7.2, 10.9, 14.6, 21.8, and 38 mV at current densities of 1, 2, 3, 5, and 10 mA cm^{-2}, respectively (Fig. 4a, c and S8). Similarly, ZnF_2@Zn (22.4, 25.9, 29.7, 38.8, and 59.8 mV) and In@Zn anodes (12.5, 18.9, 23.9, 34.4, and 58.2 mV) exhibit comparatively low polarization voltages at the same current densities (Fig. 4b, c and S8). In contrast, bare Zn shows significantly highest polarization voltages of 41.6, 53, 62, 75.8, and 96.9 mV at these current densities (Fig. 4a, c and S8). This difference is attributed to interfacial corrosion and dendrite issues in bare Zn. Moreover, ZnF_2@In@Zn has a much lower nucleation overpotential of 4.2 mV compared to bare Zn (108.6 mV), In@Zn (36.5 mV), and ZnF_2@Zn (32.4 mV) (Fig. 4d, e and S9). This indicates a faster zinc nucleation process and a higher zinc nucleation density for the ZnF_2@In@Zn anode. Moreover, compared with bare Zn, the ZnF_2@In@Zn anode exhibits superior wettability with electrolytes, which is beneficial for reducing polarization voltage and nucleation overpotential (Fig. S10). To more accurately evaluate the deposition kinetics, we calculated the exchange current density during zinc deposition. As shown in Fig. S11a, bare Zn has a low exchange current density of only 8.7 mA cm^{-2}, whereas ZnF_2@In@Zn has a significantly higher value of 14.6 mA cm^{-2}, indicating faster deposition kinetics. Additionally, In@Zn and ZnF_2@Zn also exhibit increased exchange current densities compared to bare Zn, demonstrating that both the In layer and the ZnF_2 layer can enhance the deposition kinetics (Fig. S11b).

To evaluate the corrosion resistance of ZnF_2@In@Zn, electrochemical impedance spectroscopy (EIS) is conducted at various resting times. Fig. S12 presents the equivalent circuit diagram, and Table S1 lists the values of solution resistance (R_s), solid electrolyte interfacial impedance (R_{EIS}), and charge transfer impedance (R_{ct}) for various anodes at different resting times. As the resting time increased, bare Zn exhibited a continuous rise in both R_{EIS} and R_{ct}, indicative of ongoing corrosion (Fig. 4f). During the resting period, In@Zn showed fluctuations in R_{EIS} and R_{ct}, likely due to temperature variations in the testing environment (Fig. S13a). However, overall, the In@Zn anode maintained extremely low R_{EIS} and R_{ct}, highlighting superior corrosion resistance and electronic transport properties of In. The ZnF_2@Zn anode experienced a gradual increase in R_{EIS} and R_{ct}, possibly due to electrolyte penetration through surface pores (Fig. S13b). Nonetheless, its impedance remained significantly lower than that of bare Zn. Benefiting from In's role in repairing interfacial defects, ZnF_2@In@Zn demonstrated the lowest and most stable R_{EIS} and R_{ct} of less than 10 Ω (Fig. 4g). This underscores its rapid electrochemical kinetics and excellent corrosion resistance. It is also worth noting that R_{EIS} and R_{ct} of In@Zn are marginally higher than those of ZnF_2@In@Zn. This slight discrepancy may stem from partial oxidation of In metal during storage and construction. Furthermore, the ZnF_2@In@Zn anode similarly demonstrates low polarization voltage and low charge transfer impedance at high current densities compared to other studies on anode modification (Fig. 4h). To further assess the ability of the ZnF_2@In@Zn anode to suppress interfacial side reactions, linear sweep voltammetry (LSV) curves of bare Zn and ZnF_2@In@Zn anode were measured. Compared with bare Zn (−1.83 V), the
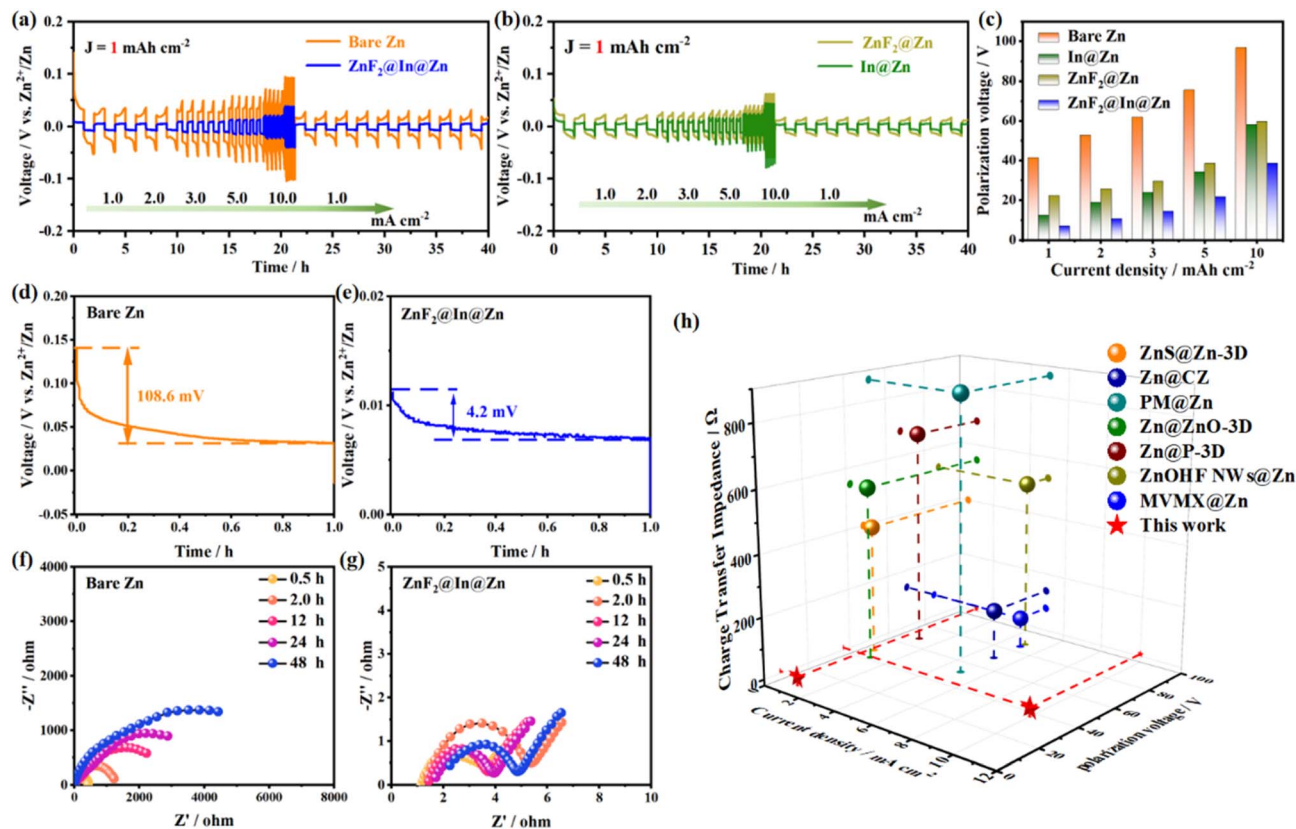
Fig. 4 Study of kinetic processes in symmetric cells. Multiplication performance of symmetric cells assembled with (a) bare Zn, ZnF_2@In@Zn, (b) In@Zn and ZnF_2@Zn anodes. (c) Polarization voltage histograms of various anodes at different current densities. Voltage–time plots of symmetric cells assembled with (d) bare Zn and (e) ZnF_2@In@Zn. EIS of symmetric cells assembled from (f) bare Zn and (g) ZnF_2@In@Zn anode at various resting times. (h) Comparison of this work with published studies in terms of current density, polarization voltage and charge transfer impedance.[34–40]

ZnF_2@In@Zn anode has a lower hydrogen evolution over-potential of −2.01 V (vs. Ag/AgCl) (Fig. S14). This indicates that the ZnF_2@In layer effectively suppresses the hydrogen evolution reaction.

The cycle life of ZnF_2@In@Zn symmetric cells was further evaluated. Under 1 mA cm^{-2}/1 mAh cm^{-2} conditions, the ZnF_2@In@Zn anode demonstrates stable cycling for over 4000 h, a significant improvement over bare Zn, which fails after only 350 h (Fig. S15). When the current density and deposition amount are increased to 5 mA cm^{-2}/2 mAh cm^{-2}, the ZnF_2@In@Zn anode maintains a cycle life exceeding 2800 h, whereas bare Zn survives only for 140 h (Fig. 5a). Under more demanding conditions of 10 mA cm^{-2}/5 mAh cm^{-2}, the ZnF_2@In@Zn anode achieves a cycle life of over 500 h with a low polarization voltage of 37 mV, whereas bare Zn fails after 41 h with a polarization voltage of 79 mV (Fig. 5b). Additionally, under 10 mA cm^{-2}/5 mAh cm^{-2} conditions, ZnF_2@Zn and In@Zn anodes also show extended cycle lives of 344 and 100 h (Fig. S16), respectively, compared to bare Zn. This shows that a single protective layer can also improve the cycle stability of the anode. Moreover, the ZnF_2@In@Zn anode demonstrates superior cycling stability at various rates compared to other reported studies (Fig. 5c).

Lower polarisation voltage is closely related to deposition kinetics. In general, zinc deposition can be divided into four processes: (1) diffusion of $Zn(H_2O)_6^{2+}$ to the anode surface; (2) de-solvation of $Zn(H_2O)_6^{2+}$; (3) transport of Zn^{2+} from the passivation layer to the surface of the metal layer; (4) the electrical crystallisation. The diffusion of $Zn(H_2O)_6^{2+}$ to the anode surface is usually consistent as the electrolyte composition remains unchanged. To investigate the effect of bare Zn and ZnF_2@In@Zn on the de-solvation of $Zn(H_2O)_6^{2+}$, the EIS of the symmetric cell was obtained at different temperatures. As the temperature increases, the R_{ct} and R_{SEI} of the bare Zn symmetric battery drop sharply (Fig. S18a), whereas those of the ZnF_2@In@Zn symmetric battery decrease only slightly (Fig. 5d). The activation energies for the two impedances of the ZnF_2@In@Zn anode, calculated via the Arrhenius equation based on R_{ct} and R_{SEI} at different temperatures, are lower than those of the bare Zn, indicating faster de-solvation of $Zn(H_2O)_6^{2+}$ (Fig. 5e and S18b). Additionally, ZnF_2 exhibits a higher binding energy for Zn^{2+} (−21.8 eV) compared to H_2O (−4.8 eV), indicating its ability to accelerate the de-solvation of $Zn(H_2O)_6^{2+}$ (Fig. 5f). To evaluate Zn^{2+} transport in the passivation layer, the ionic transference numbers of the bare Zn and ZnF_2@In@Zn anodes were tested and calculated. Compared to bare Zn (0.16), the ZnF_2@In@Zn anode has a higher Zn^{2+} transference number (0.72), showing
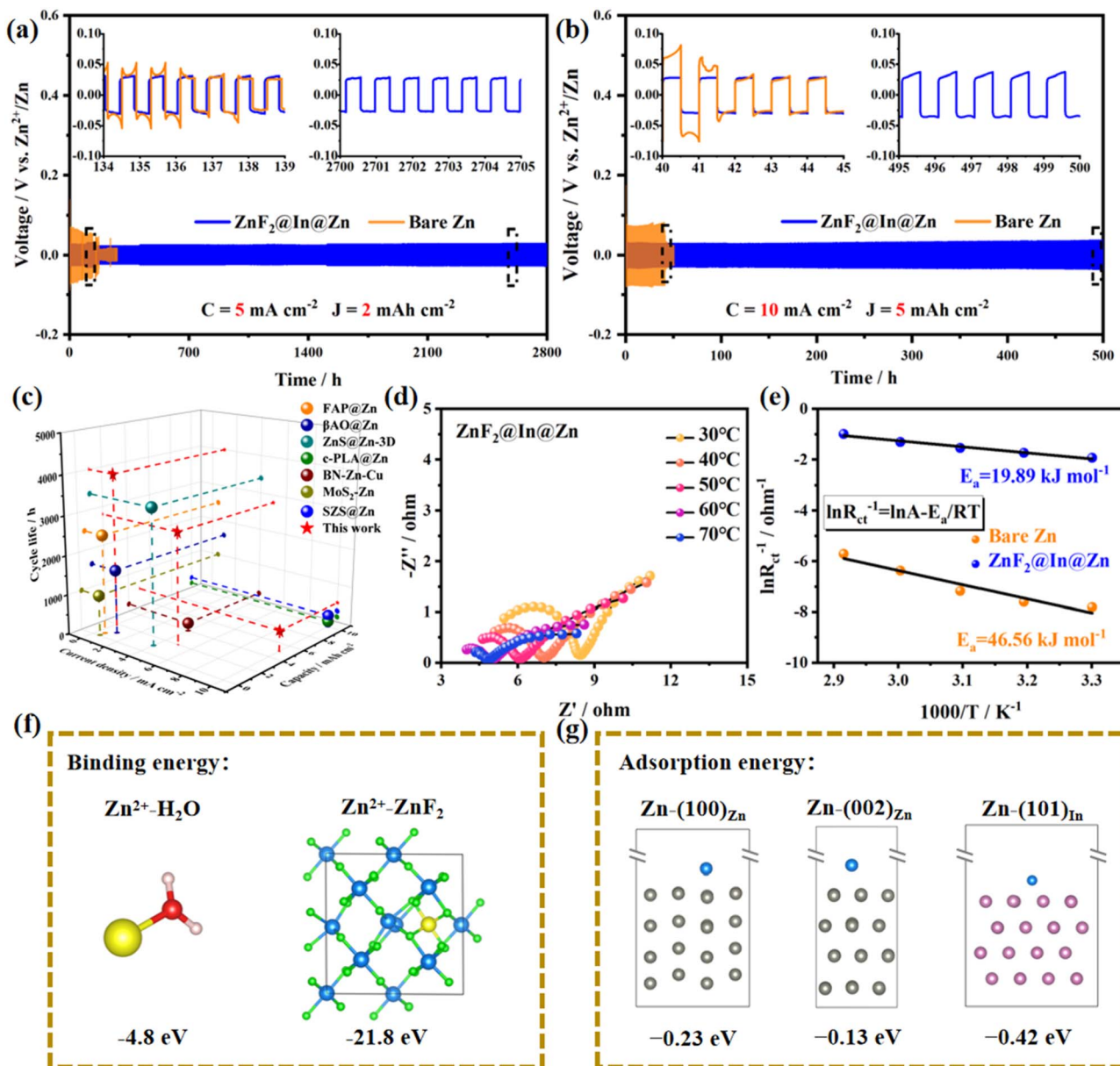
Fig. 5 Study of cycling stability in symmetric cells. Cycling performance test of bare Zn and ZnF_2@In@Zn symmetric cells at (a) 5 mA cm^{-2}/2 mAh cm^{-2} and (b) 10 mA cm^{-2}/5 mAh cm^{-2}. (c) Comparison of this work with published work on cycle stability of symmetric cells.[34,41–46] (d) EIS of the ZnF_2@In@Zn symmetric cell at different temperatures. (e) Arrhenius curve and activation energy of bare Zn and ZnF_2@In@Zn anodes based on R_{ct}. (f) Binding models and energies for Zn^{2+} binding to H_2O and ZnF_2. (g) Adsorption models and energies of zinc atoms with $(100)_{Zn}$, $(002)_{Zn}$ and $(101)_{In}$ planes.

faster Zn^{2+} transport through the ZnF_2 layer (Fig. S19). Moreover, the $(101)_{In}$ plane has a higher adsorption energy for zinc atoms (-0.42 eV) than the $(002)_{Zn}$ (-0.13 eV) and $(100)_{Zn}$ (-0.23 eV) planes, indicating that the In layer can speed up electrocrystallization of zinc (Fig. 5g). In summary, the faster desolvation of $Zn(H_2O)_6^{2+}$, Zn^{2+} transport, and electrocrystallization processes give the ZnF_2@In@Zn anode quicker deposition kinetics than bare Zn, resulting in lower nucleation potential and polarization voltage.

High cycle stability is closely related to uniformity of zinc deposition. When a fixed voltage is applied, a sustained increase in current density over time signifies 2D diffusion,

which is prone to dendrite formation. In contrast, the stabilization of current density after an initial increase indicates 3D diffusion, suggesting uniform zinc deposition. The ZnF_2@-In@Zn and ZnF_2@Zn anodes transition to 3D diffusion shortly after the initial 2D diffusion ($\sim$2 s), indicating uniform zinc deposition (Fig. S20). Conversely, the In@Zn anode and bare Zn show continuous 2D diffusion, implying dendrite formation (Fig. S20).

Fig. S21 presents the cyclic voltammetry (CV) curves for bare Zn and ZnF_2@In@Zn symmetric cells. Compared to bare Zn, the ZnF_2@In@Zn symmetric cell achieves a higher current density as voltage increases, indicative of faster electrochemical

kinetics. The voltage sweep from 0 V to 0.15 V is labeled as step 1, and the reverse sweep from 0.15 V to 0 V is step 2. For the bare Zn symmetric cell, the step 2 current density (i_2) is more than the step 1 current density (i_1) (Fig. S21a). According to the polarization overpotential eqn (4), when the voltage is constant, the limiting current density (i_{lim2}) should be more than the i_{lim1}. According to the relationship between the i_{lim} and the diffusion distance (δ) formula (5), the δ_2 is shorter than δ_1, indicating the formation of dendrites on the bare Zn surface. In contrast, for the ZnF$_2$@In@Zn symmetric cell, the current densities in steps 1 and 2 are nearly identical, suggesting uniform zinc deposition (Fig. S21b). Moreover, the crystal surface specific energy will affect the current density. In the ZnF$_2$@In@Zn symmetric cell, the current densities in steps 1 and 2 are nearly identical, which also reflects the stable surface energy, which is conducive to uniform deposition.

$$\eta_{conc} = \frac{RT}{nF} \ln \left(1 - \frac{i}{i_{lim}} \right) \qquad (4)$$

$$i_{lim} = \frac{nFDC_0}{\delta} \qquad (5)$$

The $(101)_{Zn}$ plane is known for its lower lattice distortion rate and smaller distortion surface energy change.[47,48] Under the condition of 1 mA cm^{-2}/1 mAh cm^{-2}, after 25 cycles, ZnF$_2$@In@Zn shows a higher specific intensity ($\sim$9.60) of (101) relative to the sum of (002) and (100) (Fig. S22), compared to (6.87) before cycling (Fig. S6a). This indicates that zinc grows along the (101) plane and increases its exposure. Conversely, bare Zn exhibits a reduced specific intensity ($\sim$2.25) (Fig. S22), which can lead to lattice distortion and uneven surface energy distribution, resulting in dendrite growth.

Confocal laser scanning microscopy (CLSM) was used to analyze the surface roughness (S_a) of the anode. Under 1 mA cm^{-2}/1 mAh cm^{-2} conditions after 25 cycles, the ZnF$_2$@In@Zn anode shows lower surface roughness ($S_a = 1.71$) than bare Zn ($S_a = 3.09$), indicating more uniform deposition (Fig. 6a and b). Additionally, the height profile of ZnF$_2$@In@Zn exhibits smaller fluctuations than bare Zn, further confirming its uniform deposition (Fig. S23). SEM reveals the morphological evolution at varying deposition amounts. For bare Zn with a deposition of 0.5 mAh cm^{-2}, the surface shows small particle accumulation (Fig. 6c). As the deposition increased to 5 mAh cm^{-2}, particle accumulation became more pronounced, with some areas showing no zinc deposition (Fig. 6d). In contrast, the ZnF$_2$@In@Zn anode with a deposition of 0.5 mAh cm^{-2} displays a uniform distribution of hexagonal zinc particles (Fig. 6e). When the deposition increased to 5 mAh cm^{-2}, these particles merge into a more uniform surface, indicating that they coalesced during deposition (Fig. 6f). Moreover, mapping and the EDS results of the ZnF$_2$@In@Zn anode with a deposition amount of 5 mAh cm^{-2} show that F remains evenly distributed, whereas In is almost undetectable (Fig. S24). This suggests that zinc deposition occurred between the In layer and the ZnF$_2$ layer, inhibiting corrosion of the deposited zinc. Optical microscopy further revealed the morphological

evolution of zinc during deposition. For bare Zn, as deposition progressed, noticeable surface protrusions formed, along with bubble formation (Fig. S25a), which indicates dendrite growth and corrosion. Conversely, the ZnF$_2$@In@Zn anode shows relatively uniform surface deposition with no bubble formation (Fig. S25b).

COMSOL Multiphysics was used to analyze the distributions of current density and Zn^{2+} concentration on the anode surface during deposition. For the bare Zn, uneven passivation layers cause localized deposition. Areas with localized deposition show high current density, whereas the passivation zones (orange) have low current density, worsening zinc deposition unevenness (Fig. 6g). As deposition becomes more uneven, so does the current density distribution. Throughout the deposition process of bare Zn, Zn^{2+} tend to gather at surface protrusions with larger specific surface areas (Fig. S26a). For the ZnF$_2$@In@Zn anode, the current density stays uniform during deposition (Fig. 6h). In the field of Zn^{2+} concentration, the ZnF$_2$ layer (yellow) ensures uniform Zn^{2+} distribution, promoting uniform zinc deposition on the In layer (olive green) (Fig. S26b).

To evaluate the impact of the ZnF$_2$@In@Zn anode on the charge/discharge performance of the cathode, a full cell with NH$_4$V$_4$O$_{10}$ as the cathode (NHVO) is assembled. Given that the NHVO cathode undergoes structural changes during the first cycle, the second cycle of the cyclic voltammetry (CV) curve is analyzed. The ZnF$_2$@In@Zn//NHVO full cell exhibits lower oxidation peak potentials (1.054 V and 0.758 V) compared to the bare Zn//NHVO full cell (1.097 V and 0.771 V), attributed to its smaller polarization voltage (Fig. 7a). Meanwhile, the reduction peak potential of the ZnF$_2$@In@Zn//NHVO full cell increases from 0.595 V (bare Zn//NHVO full cells) to 0.604 V, indicating improved full cell energy efficiency (Fig. 7a).

Fig. S27 presents the equivalent circuit diagram of the Zn//NHVO full cell, and Table S2 lists the values of solution resistance (R_s), solid electrolyte interfacial impedance (R_{EIS}), and charge transfer impedance (R_{ct}) for various anodes at different resting times. Electrochemical impedance measurements of the ZnF$_2$@In@Zn//NHVO full cell at various voltages reveal that the R_{ct} of the ZnF$_2$@In@Zn anode remains stable throughout discharging (Fig. 7b). However, the ion transport rate declines with decreasing voltage, primarily due to Zn^{2+} embedding in the cathode, hindering Zn^{2+} transport (Fig. 7b). Bare Zn suffers from inert products caused by side reactions, leading to slower surface ion migration (Fig. 7c). During the discharge process, the R_{ct} drops sharply when internal uncorroded Zn is exposed, accelerating the ion transport. Nevertheless, the R_{ct} of the ZnF$_2$@In@Zn//NHVO full cell remains lower than that of the bare Zn//NHVO full cell. During charging, the ZnF$_2$@In@Zn//NHVO full cell also demonstrates higher ion migration ability and lower R_{ct} than the bare Zn//NHVO full cell, which results in superior rate performance (Fig. S28). At low current density, the NHVO cathode is not fully activated, making the ion transport on the cathode surface the rate-controlling step, so no significant capacity improvement of the ZnF$_2$@In@Zn//NHVO full cell is observed. Once activated at low current, the benefits of high ion migration ability and low R_{ct} enhance high-current-density
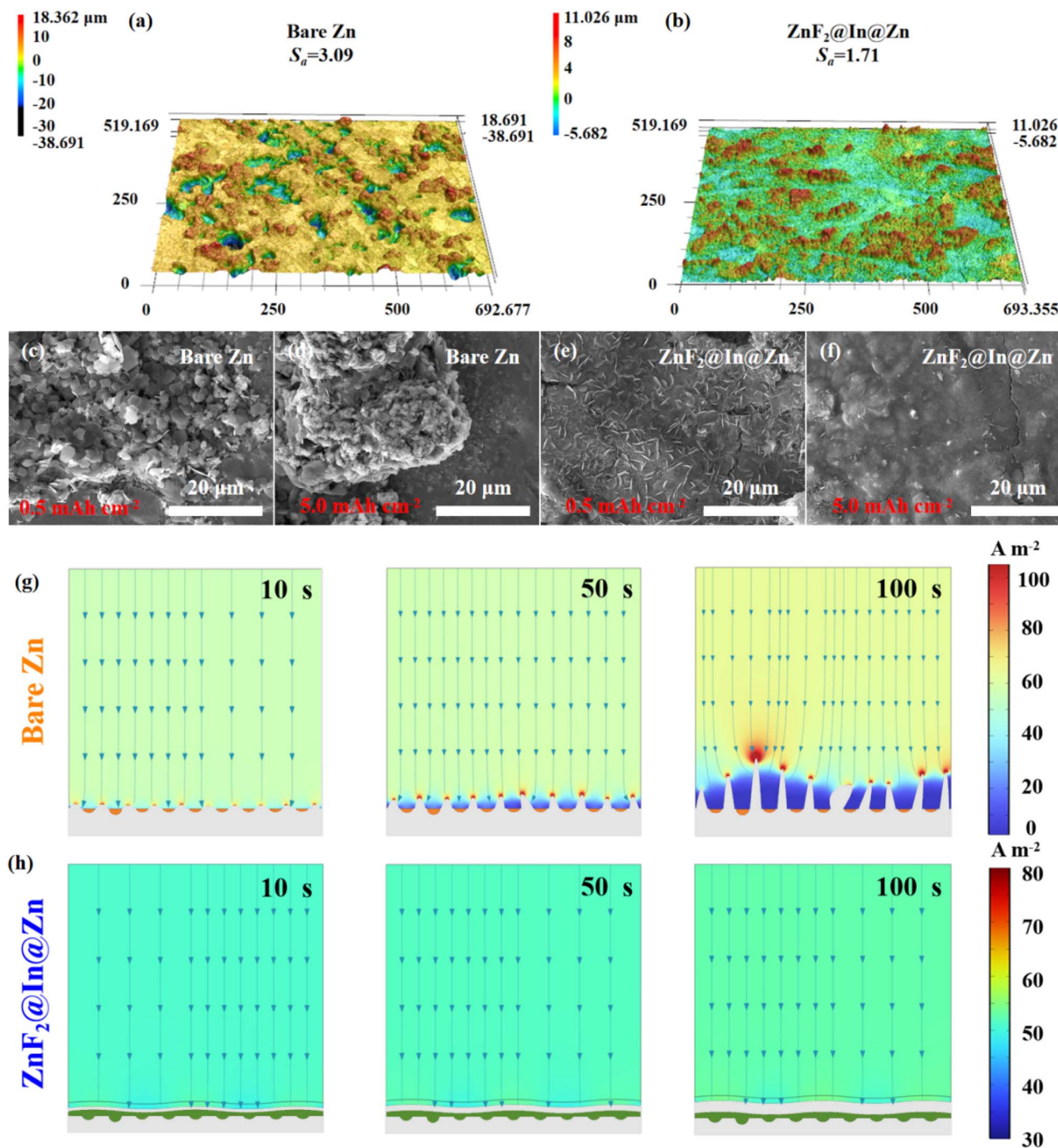
Fig. 6 Study of anode deposition behavior. CLSM images of (a) bare Zn and (b) ZnF$_2$@In@Zn anodes after 25 cycles at 1 mA cm^{-2}/1 mAh cm^{-2}. SEM images of (c and d) bare Zn and (e and f) ZnF$_2$@In@Zn anodes deposited with (c and e) 0.5 mAh cm^{-2} and (d and f) 5 mAh cm^{-2} after 25 cycles at 1 mA cm^{-2}/1 mAh cm^{-2}. Current density profiles of (g) bare Zn and (h) ZnF$_2$@In@Zn anode surfaces in different deposition states.

performance, giving the ZnF$_2$@In@Zn//NHVO full cell a higher capacity (Fig. 7d). Upon returning to low current density, the ZnF$_2$@In@Zn//NHVO full cell maintains higher capacity compared to the bare Zn//NHVO full cell. In addition, the same phenomenon also occurred in In@Zn and ZnF$_2$@Zn anodes. At high current densities, full cells assembled with In@Zn and ZnF$_2$@Zn anodes also exhibit higher capacity compared to bare Zn (Fig. 7d and S29). Thanks to its ability to

suppress dendrites and corrosion, the ZnF$_2$@In@Zn//NHVO full cell retains a capacity of 112.4 mAh g^{-1} after 10 000 cycles at 3 A g^{-1}, corresponding to a capacity retention rate of 79.5% (Fig. 7e and S30). In contrast, the capacity of the bare Zn//NHVO full cell approaches 0 mAh g^{-1} after 10 000 cycles at 3 A g^{-1}, possibly due to the accumulation of inert products on the anode and cathode (Fig. 7e and S30).
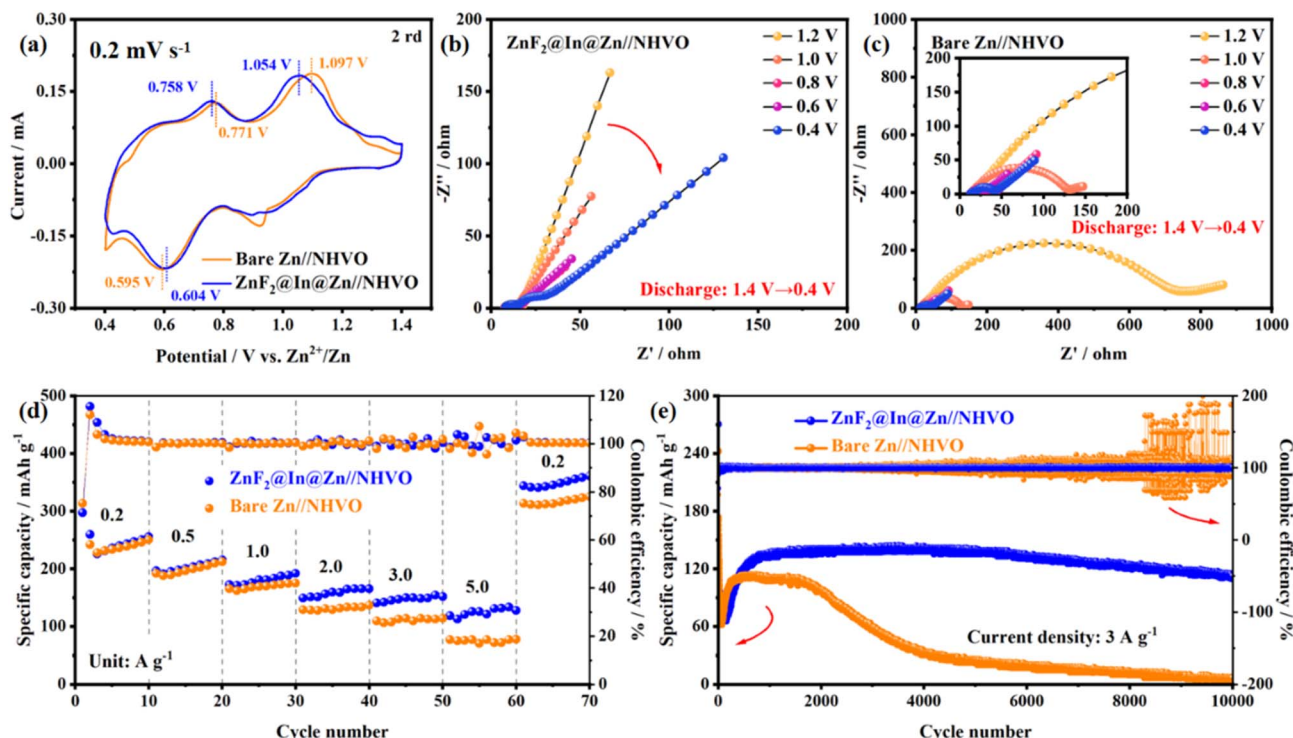
Fig. 7 Study of the Zn//NHVO full cell performance. (a) CV curve of bare Zn//NHVO and $ZnF_2@In@Zn$//NHVO full cells. *In situ* EIS spectra of (b) bare Zn//NHVO and (c) $ZnF_2@In@Zn$//NHVO full cells discharged from 1.4 V to 0.4 V. (d) Rate and (e) cycle performance of the Zn//NHVO full cell.

3 Conclusion

In summary, we have introduced a novel leveling–shielding dual strategy to enhance the performance of zinc anodes. The low-melting-point In metal serves as a leveling agent to repair surface defects due to the decomposition of $Zn_2(OH)_2CO_3$ during heat treatment and induces uniform and rapid zinc deposition by exposing a single $(101)_{In}$ plane. The outermost ZnF_2 layer not only suppresses the corrosion of deposited zinc but also accelerates the de-solvation process of $Zn(H_2O)_6^{2+}$, thereby improving electrochemical reaction kinetics. Therefore, the $ZnF_2@In@Zn$ symmetric cell demonstrates exceptional performance, achieving an ultra-low interfacial impedance of less than 10 Ω and stable cycling for over 2800 h with a polarization voltage of 21.8 mV at 5 mA cm^{-2} and 2 mAh cm^{-2}, which is a significant improvement over bare Zn (140 h and 75.8 mV). Additionally, the $ZnF_2@$-In@Zn//$NH_4V_4O_{10}$ full cell exhibits remarkable long-term stability, retaining a capacity of 112.4 mAh g^{-1} after 10 000 cycles at 3 A g^{-1}, corresponding to a capacity retention rate of 79.5%. Our findings demonstrate that this leveling–shielding dual strategy effectively addresses critical issues such as dendrite formation and corrosion in aqueous zinc ion batteries at no cost to energy efficiency, while providing a promising route for addressing similar issues in other metal anodes.

Author contributions

Qing Wen is responsible for completing most of the experiments, data analysis and article writing. Taixu Hao is responsible for DFT calculations and COMSOL Multiphysics. Tian Chen, Dinghao Le and Pei Yang are responsible for electrochemical performance testing and analysis. Hezhang Chen and Linbo Tang are responsible for XRD and SEM analysis. Qing Wu provided a platform for simulation calculations. Xiahui Zhang and Junchao Zheng are responsible for paper guidance and revision.

Conflicts of interest

The authors declare that they have no conflict of interest.

Data availability

The data that support the findings of this study are available from the corresponding author, Junchao Zheng, jczheng@csu.edu.cn, upon reasonable request.

The supplementary information file contains includes experimental methods, figures, tables, and extended analyses to support data reproducibility and interpretation. See DOI: https://doi.org/10.1039/d5sc04875c.

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