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# Dual back interface engineering optimized charge carrier dynamics in $\text{Sb}_2(\text{S,Se})_3$ photocathodes for efficient solar hydrogen production†

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Antimony sulfoselenide ( $\text{Sb}_2(\text{S,Se})_3$ ) is a promising sunlight absorber material for solar energy conversion in photovoltaic (PV) cells and photoelectrochemical (PEC) photoelectrodes due to its excellent photoelectric properties. However, the obtained thin-film and back contact properties significantly influence the PEC performance of photocathodes, causing severe bulk recombination, carrier transport loss, and deteriorating half-cell solar-to-hydrogen (HC-STH) efficiency. This study introduces an intriguing dual back interface engineering strategy for  $\text{Sb}_2(\text{S,Se})_3$  photocathodes by incorporating an intermediate  $\text{MoO}_2$  layer and a secondary carrier transport channel of Au to strengthen charge carrier dynamics. The synergistic assembly of these dual back interface layers improves the growth kinetics and achieves the optimal orientation of  $\text{Sb}_2(\text{S,Se})_3$  thin films by increasing substrate wettability. Moreover, by shortening the back contact barrier height and passivating defect-assisted recombinations, these dual back underlayers simultaneously enhance carrier transport and separation efficiencies. As a result, the photocurrent density of the champion  $\text{Sb}_2(\text{S,Se})_3$  photocathode increases from 5.89 to 32.60  $\text{mA cm}^{-2}$ , and the HC-STH conversion efficiency improves significantly from 0.30% to 3.58%, representing the highest value for  $\text{Sb}_2(\text{S,Se})_3$ -based photocathodes. This work highlights the effectiveness of dual back interface engineering in promoting the PEC performance of chalcogenide photocathodes for solar hydrogen evolution applications.

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## 1. Introduction

Recent advancements in photoelectrochemical (PEC) characteristics have explored various semiconductor materials, including silicon, metal oxides, metal sulfides, metal tellurides, and organic-inorganic perovskites.<sup>1–8</sup> Among these,  $\text{Sb}_2(\text{S,Se})_3$  is a popular absorber because of its low toxicity, high absorption coefficient with a tunable bandgap, benign hole mobility, and superior stability.<sup>9–11</sup> Despite ongoing efforts to improve its film quality and power conversion efficiencies in PV and PEC cells,  $\text{Sb}_2(\text{S,Se})_3$  photoelectric devices still fall short of their superior counterparts.<sup>12–14</sup> This significant performance deficit is

primarily associated with the complex defect chemistry, leading to severe charge carrier recombination.<sup>9</sup> Thus, a comprehensive understanding and optimization of  $\text{Sb}_2(\text{S,Se})_3$  device efficiency is indispensable.

Synthesizing high-quality absorber films with a compact, smooth morphology, devoid of secondary phases and defects, is a prerequisite for optimal performance in photoelectric applications. However, synthesis challenges of the  $\text{Sb}_2(\text{S,Se})_3$  absorber stem from its low-symmetry crystal structure and intricate bulk defect characteristics.<sup>11</sup> Particularly, defects at bulk and deep levels are considered detrimental, significantly deteriorating performance by trapping charge carriers and decreasing carrier extraction efficiency.<sup>15–17</sup> Several fabrication approaches for chalcogenide materials (*i.e.*,  $\text{Sb}_2(\text{S,Se})_3$  and  $\text{Sb}_2\text{Se}_3$  thin films), including the successive low-temperature pulsed electron deposition technique (LT-PED), magnetron sputtering deposition (MSD), vapour transport deposition (VTD), using molecular ink, spin coating, electrodeposition, chemical bath deposition (CBD), and hydrothermal deposition (HD), have resulted in 7–10% PV cell efficiencies.<sup>10,17–21</sup> Notably, the HD process is particularly effective in producing compact and homogeneous  $\text{Sb}_2(\text{S,Se})_3$  films owing to its low processing temperature, which impedes interfacial element diffusion and

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additional defects.<sup>19,20</sup> Furthermore, the HD approach involves reactive ion deposition in aqueous solutions, followed by nucleation and crystal growth processes.<sup>22</sup>

In 2017, Moon *et al.* first investigated a pure  $\text{Sb}_2\text{Se}_3$  photocathode for PEC water splitting,<sup>23</sup> which sparked a range of subsequent studies on this intriguing scenario in areas like co-catalyst engineering, absorber engineering, interface engineering, and tandem engineering.<sup>2,7,24–27</sup> Despite these advances, current research predominantly focuses on pure  $\text{Sb}_2\text{Se}_3$  absorbers, with limited research on  $\text{Sb}_2(\text{S,Se})_3$  alloy-type photocathodes, which are isomorphous and share identical unit-cell parameters.<sup>28–32</sup> The  $\text{Sb}_2(\text{S,Se})_3$  and  $\text{Sb}_2\text{S}_3$  films grown *via* the hydrothermal method provide a better (*hk1*) orientation, preventing lattice mismatch and deep-level defects due to *in situ* substitution of S and Se.<sup>28,29</sup> Furthermore, a gradient S concentration nurtures charge carrier transport and separation, and extends the band-bending region.<sup>30</sup> Recently, the  $\text{Sb}_2(\text{S,Se})_3$  photocathode fabricated through the VTD method achieved a photocurrent density ( $J_{\text{ph}}$ ) of  $16.5 \text{ mA cm}^{-2}$  and an STH efficiency of 1.1%.<sup>17</sup> However, the performance of the  $\text{Sb}_2(\text{S,Se})_3$  photocathode is far inferior compared to its  $\text{Sb}_2\text{Se}_3$  counterpart, which has already obtained a benchmark  $J_{\text{ph}}$  value above  $30 \text{ mA cm}^{-2}$ .<sup>2,8,33</sup> Therefore, optimizing back interface engineering is essential for improving thin film quality and PEC performance of  $\text{Sb}_2(\text{S,Se})_3$  photocathodes.

To date, most studies have focused on preparing  $\text{Sb}_2(\text{S,Se})_3$  devices with superstrate structures due to simplicity and ohmic contacts. However, substrate configurations offer significant advantages like direct sunlight absorption, enhanced interface quality, and a customizable absorber layer.<sup>34</sup> Unfortunately, insufficient research exists related to  $\text{Sb}_2(\text{S,Se})_3$  devices with a substrate structure, which exhibits potential advantages for photocathodes. Back interface engineering is significantly important for enhancing performance efficiencies, such as  $J_{\text{ph}}$ , onset potential ( $V_{\text{on}}$ ), and HC-STH.<sup>35–37</sup> Effective carrier transport and extraction rely on optimizing the back interface, which involves reducing the back contact barrier height and the absorber layer's development mechanisms.<sup>36,37</sup> On the other hand, post-annealing can improve substrate wettability by reducing the contact angle and enhancing interfacial bonding strength.<sup>38</sup> Besides, it increases surface energy and adhesion, improving compatibility with the substrate and buffer layers.<sup>39,40</sup> To encourage charge transport, the incorporation of the carrier transport channel as an underlayer (interfacial layer) considerably influences carrier dynamics at the interface. Atomic-level interactions between adjacent components form numerous chemical bonds in heterojunctions, which facilitate efficient carrier transport and separation, such as Au–O bonds at the Au– $\text{MoO}_2$  interface acting as an electronic-transmission medium for promoting the hydrogen evolution reaction (HER).<sup>41,42</sup> The study on the modification of wettability, charge carrier dynamics, and back contact barrier height at the  $\text{Mo}/\text{Sb}_2(\text{S,Se})_3$  interface is under-researched, requiring further examination for improvement and potential advancement in PEC.

This study explores a dual back interface engineering approach for optimizing charge carrier dynamics in planar-type  $\text{Mo}/\text{MoO}_2/\text{Au}/\text{Sb}_2(\text{S,Se})_3/\text{CdS}/\text{TiO}_2/\text{Pt}$  photocathodes. The

synergy of dual back interface (an intermediate layer of  $\text{MoO}_2$  followed by a secondary carrier transport channel of Au) layers strengthens the growth kinetics by acquiring the ideal orientation of the  $\text{Sb}_2(\text{S,Se})_3$  film through better substrate wettability. Moreover, this approach shortens the back contact barrier height and suppresses defect-assisted recombination, leading to simultaneously enhanced charge carrier transport and separation efficiencies. Under this engineering effort, the champion photocathode offers advantageous perceptions of regulating the bulk and interface properties, leading to a remarkable  $J_{\text{ph}}$  of  $\sim 32.60 \text{ mA cm}^{-2}$  (at 0 V *versus* the reversible hydrogen electrode (RHE), *i.e.*,  $V_{\text{RHE}}$ ). An HC-STH conversion efficiency of  $\sim 3.58\%$  undoubtedly strengthens its potential for applications in solar hydrogen production.

## 2. Experimental section

### 2.1. Preparation of the Mo substrate

This study describes the use of the hydrothermal method to deposit an  $\text{Sb}_2(\text{S,Se})_3$  film onto Mo-coated soda lime glass (SLG) substrates. Initially, the deposition was very weak and inhomogeneous (Fig. S1a and b†). To address this issue, post-annealing was used to enhance the substrate's wettability. The Mo substrates were ultrasonically washed with deionized water, detergent, and ethanol, and then transferred to a furnace. Before moving the Mo substrates, the furnace tube was thoroughly cleaned with detergent and distilled water. As the furnace temperature reached  $100^\circ\text{C}$ , the furnace tube was vacuumed and cleaned three times with argon, and then filled with a pre-determined volume of air, and tightened from both ends. The Mo substrates were annealed at various temperatures ( $200^\circ\text{C}$ ,  $300^\circ\text{C}$ ,  $400^\circ\text{C}$ , and  $500^\circ\text{C}$ ) for 15 minutes to produce a  $\text{MoO}_2$  interface layer. After annealing, three types of Mo substrates were selected for further processing: unannealed, post-annealed at  $400^\circ\text{C}$ , and post-annealed at  $400^\circ\text{C}$  followed by Au sputtering.

### 2.2. Preparation of $\text{Sb}_2(\text{S,Se})_3$ thin films

The as-prepared Mo substrates were subjected to deposition of the thin films of  $\text{Sb}_2(\text{S,Se})_3$  *via* the hydrothermal method. To prepare the precursor solution, 0.025 g of  $\text{SeC}(\text{NH}_2)_2$ , 0.267 g of  $\text{K}_2\text{Sb}_2(\text{C}_4\text{H}_2\text{O}_6)_2 \cdot 3\text{H}_2\text{O}$ , and 0.794 g of  $\text{Na}_2\text{S}_2\text{O}_3 \cdot 5\text{H}_2\text{O}$  were dissolved in 40 mL of deionized water and stirred to form a homogeneous yellow solution. This solution was added to a Teflon container, with Mo substrates angled appropriately opposite to the wall. The hydrothermal reaction was conducted at  $135^\circ\text{C}$  for 5 h. Afterward, the samples were cleaned with deionized water and ethanol, and then dried with compressed nitrogen. Finally, the films were selenized at  $410^\circ\text{C}$  for 15 minutes using 0.4 g of high-purity Se powder in a tube furnace.<sup>34</sup>

### 2.3. Preparation of the $\text{Sb}_2(\text{S,Se})_3$ photocathode

The buffer layer (CdS) was produced using the CBD method, while the  $\text{TiO}_2$  protective layer was deposited using an atomic layer deposition (ALD) technique, according to previous research.<sup>2</sup> Afterwards, Pt was sputtered on the top side as a co-catalyst for 50 seconds at a current of 20 mA using a 108 Auto



Sputter Coater. Prior to performance testing, Ag colloids were coated over the exposed surface of the Mo substrate to establish metal contact. A detailed schematic of the preparation procedure is illustrated in Fig. S2.†

## 2.4. Characterization

The phase and crystal structure of the  $\text{Sb}_2(\text{S,Se})_3$  thin films were examined by using an X-ray diffractometer using  $\text{CuK}\alpha$  radiation (XRD, Ultima-iv). The cross-section and surface morphologies of the films were observed by scanning electron microscopy (SEM, Zeiss SUPRA 55), and the corresponding chemical compositions were analyzed with an energy dispersive spectroscope (EDS, BRUKER QUANTAX 200). The states of the film surface were investigated by X-ray photoelectron spectroscopy (XPS, ESCALAB 250Xi). A contact angle meter was employed to measure contact angles at ambient temperature (PERFECT WAM-100). The thin film surface roughness and morphologies were investigated by using an atomic force microscope (AFM) operated *via* NT-MDT Spectrum Instruments in semi-contact mode. For analyzing the bonding information, Raman spectroscopy was employed (Renishaw, InVia). Topography and surface potential characterization studies of  $\text{Sb}_2(\text{S,Se})_3$  films were performed through a Kelvin probe force microscope (KPFM, Bruker Dimension ICON). The  $\text{Sb}_2(\text{S,Se})_3$  film's absorption and reflection spectra were obtained through a Shimadzu UV-3600 spectrophotometer. PEC measurements were carried out by using a CHI660e electrochemical workstation. The characterization was carried out in a 0.5 M  $\text{H}_2\text{SO}_4$  electrolyte with 100 mW  $\text{cm}^{-2}$  AM 1.5G simulated solar illumination, and the details are provided in Note S1.† A PHI 5000 VersaProbe was used to conduct ultra-violet photoelectron spectroscopy (UPS) coupled with a He I source at 21.22 eV. Under simulated sunlight illumination, photoelectrochemical impedance spectroscopy (PEIS) was performed. To determine the flat-band potential ( $E_{\text{fb}}$ ) of the  $\text{Sb}_2(\text{S,Se})_3$  films, Mott-Schottky ( $M-V$ ) characterization studies were performed in the dark using a 30 mV AC amplitude plus a frequency of  $10^4$  Hz and a scanning voltage between  $-0.50$  and  $0.10$  V. The temperature-dependent dark  $J-V$  ( $J-V-T$ ) characterization studies were carried out by utilizing a Keithley 4200A-SCS system coupled with a Lakeshore 325 temperature controller. Capacitance-voltage ( $C-V$ ) measurements were carried out at a 30 mV AC amplitude,  $10^4$  Hz frequency, and a voltage range of  $-0.50$  to  $0.10$  V in the dark. Drive-level capacitance profiling (DLCP) was performed using AC amplitudes of 20–140 mV and DC voltages of  $-0.25$  to  $0$  V. Admittance spectroscopy of the devices was performed in a Janis VPF (Lake Shore, 325 Cryogenic Temperature Controller)  $-100$  cryostat with the frequency range of  $10^2$ – $10^6$  Hz and the temperature range of 340–110 K.

## 3. Results and discussion

### 3.1. Dual back interface engineering for optimized growth kinetics of $\text{Sb}_2(\text{S,Se})_3$ films

Wettability is determined by using the contact angle (CA) between the fluid and solid surface and can be categorized as completely wettable ( $\text{CA} = 0^\circ$ ), hydrophilic ( $\text{CA} < 90^\circ$ ), or

hydrophobic ( $\text{CA} > 90^\circ$ ).<sup>39</sup> For  $\text{Sb}_2(\text{S,Se})_3$  thin films on Mo substrates, the CA was measured with water droplets. The CA produced by dropping a deionised water droplet depends mainly on the roughness and surface energies of the interfaces between the solid and liquid surfaces.<sup>7</sup> Fig. 1a–c display pristine Mo (unannealed), post-annealed Mo (at  $400^\circ\text{C}/15$  min), and post-annealed Mo (at  $400^\circ\text{C}/15$  min) sputtered with Au, corresponding to CAs  $44.2^\circ$ ,  $19.8^\circ$ , and  $31.7^\circ$ , respectively. For comparison, the CAs ( $37.3^\circ$ ,  $14.7^\circ$ , and  $21.9^\circ$ , respectively) of the identical samples were also measured with glycerol droplets which showed similar tendencies (Fig. S3a–c†). Besides, post-annealing at lower temperatures ( $200^\circ\text{C}$  and  $300^\circ\text{C}$ ) resulted in CAs of  $20.5^\circ$  and  $17.9^\circ$ , respectively (Fig. S4a and b†). Typically, the CA decreases as post-annealing temperature increases, because the annealing process increases the surface energy of thin films, which improves wettability by reducing the CA and strengthening the interfacial bonding.<sup>38,40</sup> Consequently, Mo substrates show better wettability at annealing temperatures up to  $400^\circ\text{C}/15$  min, enabling high-quality  $\text{Sb}_2(\text{S,Se})_3$  film deposition. However, annealing at  $500^\circ\text{C}/15$  min weakened the adhesion between the glass and Mo, causing the thin film to peel off after gradual washing with deionized water (Fig. S4c†). This could explain the deformation or distortion observed as a result of the high-temperature annealing process.<sup>38</sup>

After the HD of the  $\text{Sb}_2(\text{S,Se})_3$  absorber on three distinct Mo substrates, pristine Mo (unannealed), post-annealed Mo (at  $400^\circ\text{C}/15$  min), and post-annealed Mo sputtered with Au were chosen for further analysis, and they were named HS1, HS2, and HS3, respectively. According to Fig. 1d and e, the HS1 and HS2 thin-film surfaces exhibit inferior hydrophilic behaviour with CAs of  $87.9^\circ$  and  $73.3^\circ$ , respectively. The CA of the HS3 film is  $61.6^\circ$  (Fig. 1f), which indicates a superior hydrophilic nature, suggesting an obvious improvement in wettability. The glycerol droplet measurements for the identical samples showed similar CAs tendency:  $85.5^\circ$ ,  $71.0^\circ$ , and  $59.1^\circ$  (Fig. S3d–f†). The changes in CA values are attributed to differences in chemical composition, grain size, roughness, and surface energy of the  $\text{Sb}_2(\text{S,Se})_3$  films. However, improved wettability can enhance PEC performance by increasing exposed reaction sites and facilitating photoelectron transfer, thus triggering the HER.<sup>7</sup> Moreover, the effects of introducing the  $\text{MoO}_2$  oxide layer and the subsequent insertion of carrier transport channel Au on the associated surface morphologies, wettability, and roughness of the corresponding HS1, HS2, and HS3 thin films were examined using AFM measurements. Fig. 1g and h show crystal grain profiles for HS1, with an average root-mean-square (RMS) surface roughness of  $41.5$  nm and  $57.4$  nm for the HS2 thin film surface. However, Wenzel's roughness-dependent wettability model suggests that roughness will increase the hydrophilicity of a naturally hydrophilic surface ( $\text{CA} < 90^\circ$ ).<sup>39</sup> Thus, a higher RMS roughness value of  $77.2$  nm as shown in Fig. 1i (Table S1†), which is  $\approx 60\%$  rougher than HS1, increases the wettability of the  $\text{Mo}/\text{MoO}_2/\text{Au}/\text{Sb}_2(\text{S,Se})_3$  film (HS3). Generally speaking, variations in the CA and roughness are caused by the formation of the  $\text{MoO}_2$  oxide layer resulting from the post-annealing process and the insertion of the carrier transport channel Au layer.



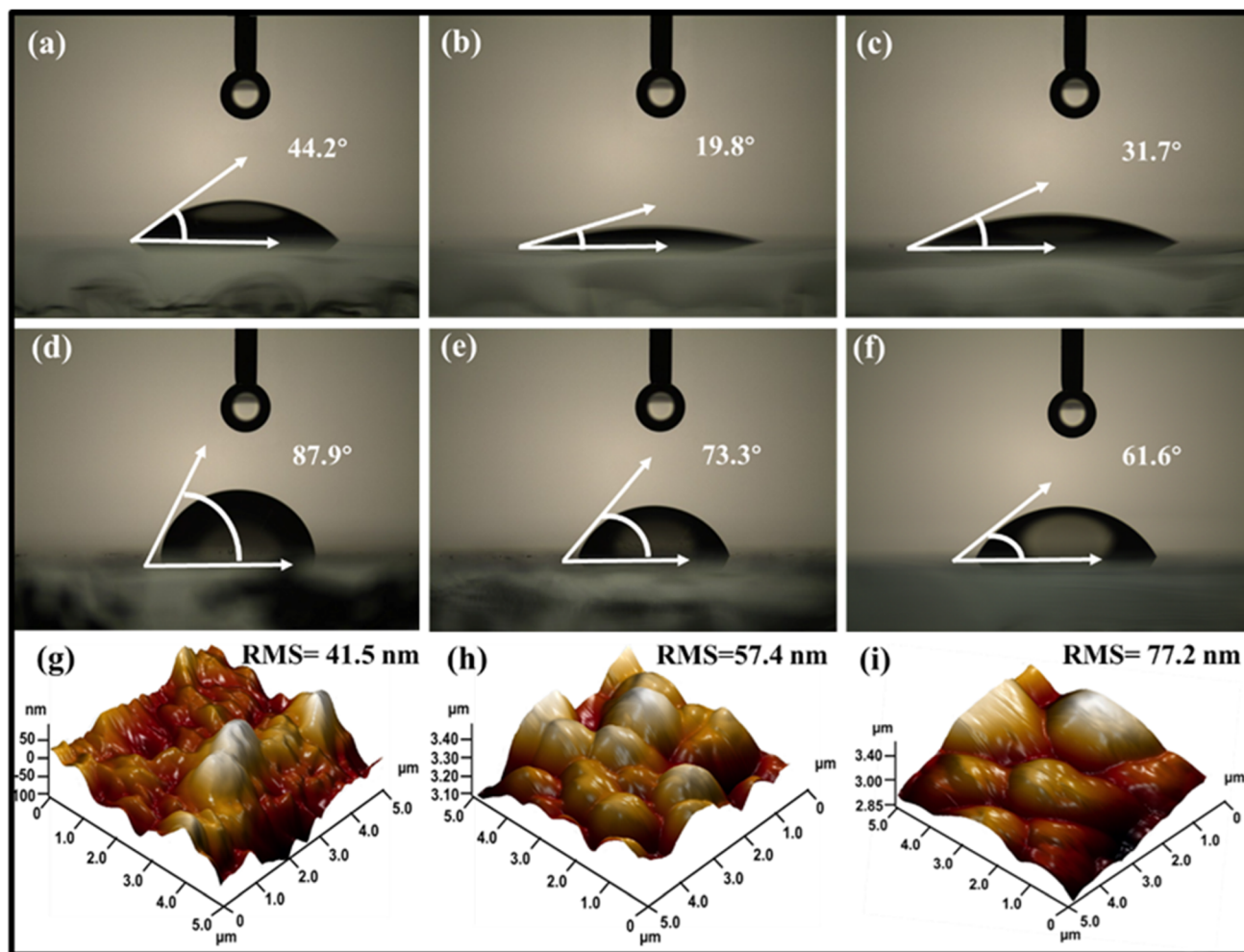


Fig. 1 (a–c) The measured CAs (using water droplets) of pristine Mo, post-annealed Mo at 400 °C/15 min, and post-annealed Mo sputtered with Au, respectively. (d–f) The measured CAs of the thin films from HS1, HS2, and HS3 samples and (g–i) the corresponding AFM topographical images of the thin films from HS1, HS2 and HS3 samples.

The XRD measurements were conducted to investigate how post-annealing influences the Mo substrate and  $\text{Sb}_2(\text{S,Se})_3$  thin-film crystalline structures to assess variations in device performance. Fig. 2a shows the development of a thin and smooth  $\text{MoO}_2$  intermediate layer in the form of crystal phases (JCPDS#32-0671) on the Mo substrate surface, where pristine Mo represents an unannealed substrate, and post-annealed Mo denotes the annealed (at 400 °C/15 min) substrate. The XRD data stipulate that the formation of the  $\text{MoO}_2$  intermediate layer on the Mo substrate surface resulted in a decreased contact angle and enhanced bonding strength by increasing surface energy.<sup>43</sup> To further confirm the existence of the  $\text{MoO}_2$  oxide layer, the identical specimens' surface and cross-sectional morphologies were investigated *via* SEM (Fig. S5a–f†). It is evident that the annealed sample's surface got rougher compared to pristine Mo (Fig. S5a and b†), and it has a compact and smooth layer of  $\text{MoO}_2$  (Fig. S5e†). Furthermore, a combined thin layer of the intermediate layer  $\text{MoO}_2$  and the charge transport channel Au is also observed (Fig. S5f†). Besides, the XRD data of the HS1, HS2, and HS3 films are demonstrated in

Fig. 2b. All the peaks of HS1, HS2, and HS3 thin films match well with JCPDS (No. 15-0861 for  $\text{Sb}_2(\text{S,Se})_3$  and (No. 42-1393 for  $\text{Sb}_2\text{S}_3$ ) having no secondary phases. The presence of S in the samples is shown by the dot-filled dark yellow lines (Fig. 2b). Additionally, there is an improvement in crystallinity and an effective suppression of random orientations. The preferred orientations corresponding to the (211), (221), and (002) planes of  $\text{Sb}_2(\text{S,Se})_3$  peaks are observed in the HS2 and HS3 films, which are expected to influence the performance diversity of the photocathodes. Compared with HS1, the (020), (120), and (130) orientations of the HS3 film decreased, while the (211) and (221) orientations progressively increased. Such growth in the (211) and (221) oriented peaks of  $\text{Sb}_2(\text{S,Se})_3$  is connected to the synergetic effect of  $\text{MoO}_2$  and Au dual back underlayers on inhibiting the hopping-type transport based on ( $h$  $k$ 0).<sup>44</sup> The results were further confirmed by analyzing the TC (texture coefficient) to examine the preferred orientation peaks in  $\text{Sb}_2(\text{S,Se})_3$  thin films, and the following equation can be used to calculate the TC:<sup>34,37</sup>



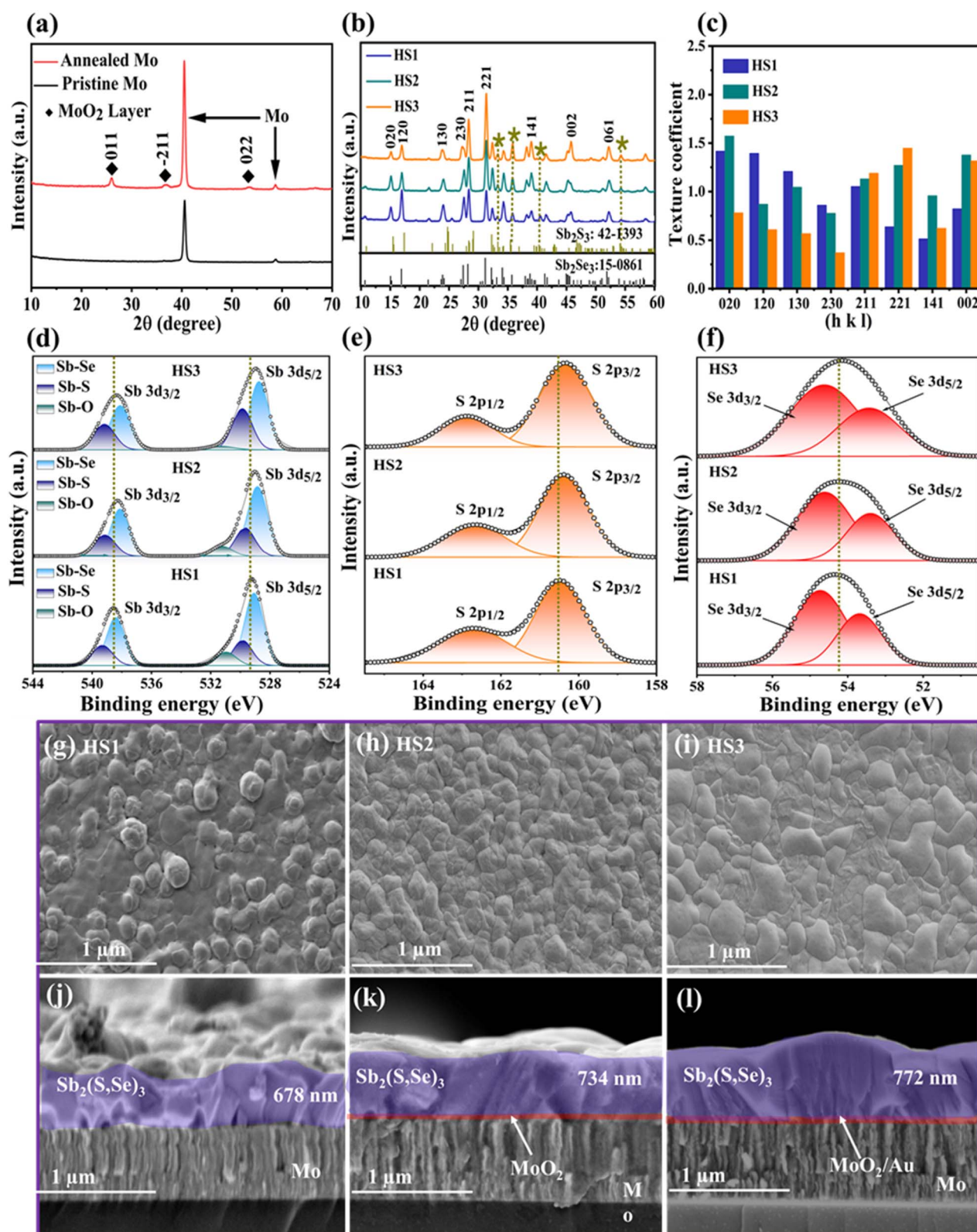


Fig. 2 (a) XRD patterns of pristine and post-annealed (400 °C/15 min) Mo substrates. (b) XRD patterns, (c) texture coefficients, and (d–f) XPS peaks of thin films from HS1, HS2 and HS3 samples. (g–i) SEM images of the surface morphology, and (j–l) cross-sectional SEM images of thin films from HS1, HS2 and HS3 samples.

$$TC(hkl) = \frac{\frac{I(hkl)}{I_0(hkl)}}{\frac{1}{N} \sum_{i=1}^N \frac{I(h_i k_i l_i)}{I_0(h_i k_i l_i)}} \quad (1)$$

where  $N$ ,  $I(hkl)$ , and  $I_0(hkl)$  represent the utilized peak number during calculation and the intensity of the measured and reported diffractions (PDF card), respectively. Fig. 2c illustrates a decrease in the TC of the  $(hk0)$  planes and an increase in the TC of the  $(hk1)$  planes after the sequential introduction of the  $\text{MoO}_2$  and Au dual back underlayers. Remarkably, the minimal TC of the  $(hk0)$  planes and the maximum TC of the  $(hk1)$  planes are observed when the  $\text{Sb}_2(\text{S,Se})_3$  thin-film is deposited hydrothermally on the substrate ( $\text{Mo}/\text{MoO}_2/\text{Au}$ ). Higher TC values for the  $(hk1)$  planes indicate better orientation and denser packing along this direction.<sup>34</sup> The FWHM (full-width at half-maximum) analysis suggests larger grains inside the HS3 thin film compared to HS1 (Fig. S6†). The  $(hk1)$ -oriented grains are stacked on the substrate; hence, their structure and bonding nature must enhance the carrier transport in the (221) and (211)-oriented films.<sup>45</sup> The calculations carried out using the Scherrer equation reveal average particle sizes of 16 nm (HS1), 19 nm (HS2), and 25 nm (HS3) (Note S2 and Table S1†). According to the particle size results, the HS3 film's surface energy is higher than that of HS1 because the larger grains of the annealed material have considerable gaps between adjacent grains.<sup>45</sup> Gap widening diminishes support between the crystal grains, resulting in large grain size, strong adhesion, high surface energy and reduced contact angle.

The total XPS spectra were recorded from HS1, HS2, and HS3 films (Fig. S7†) to analyze the elemental composition of  $\text{Sb}_2(\text{S,Se})_3$  thin films. The XPS spectra of the three primary elements (Sb 3d, S 2p, and Se 3d) in  $\text{Sb}_2(\text{S,Se})_3$  films are illustrated in Fig. 2d–f. The two prominent peaks at 538.7 and 529.5 eV are the spin–orbit components of Sb 3d<sub>3/2</sub> and 3d<sub>5/2</sub>, respectively. The binding energies of Sb 3d (Fig. 2d) significantly decreased after adding dual back interface layers, signifying a remarkable reduction in  $\text{Sb}_2\text{O}_3$  impurities. The concentration of oxides falls from 18.6% in the HS1  $\text{Sb}_2(\text{S,Se})_3$  film to 7.3% on comparing the peak regions of Sb–O (Table S2†), suggesting the formation of fewer defects due to lower oxide content.<sup>41</sup> Moreover, Fig. 2e shows peaks for S 2p<sub>1/2</sub> and S 2p<sub>3/2</sub> (at 162.5 and 161.3 eV), shifted to lower binding energy, reflecting increased electron density around Sb atoms due to the higher electronegativity of S compared to Se,<sup>9,46</sup> even though the Se 3d peak remained almost constant (Fig. 2f). The FWHM values of S and Se peaks in HS1, HS2, and HS3, thin films were also calculated (Table S3†). In the HS3 film, the FWHM values for the S 2p<sub>1/2</sub> and S 2p<sub>3/2</sub> peaks are smaller compared to those of HS1, indicating an increase in the concentration of S. Conversely, the FWHM values for the Se 3d<sub>3/2</sub> and Se 3d<sub>5/2</sub> peaks are higher in HS3, suggesting a decrease in Se content. Overall, reduced oxide content and improved bonding with Au contribute to lower defect formation and better film performance.

SEM images of the surface morphology in Fig. 2g–i show that HS2 and HS3 films have a more compact and flat morphology with larger grains than HS1. The grains in HS2 and HS3 tend to

merge and fuse into larger grains, consistent with the XRD and grain size analyses. These findings indicate that dual back interface engineering contributes to forming (211)-oriented large grains in the  $\text{Sb}_2(\text{S,Se})_3$  layer. The EDS results confirm the presence of S and show that the atomic percentage of Se decreases while that of S slightly increases in HS2 and HS3 films compared to HS1 (Fig. S8 and Table S1†). The S atom evaporates more readily at high temperatures compared to Se owing to differences in vapor pressures.<sup>34</sup> However, this change can be attributed to the formation of various chemical bonds amongst S, Au, and  $\text{O}_2$  elements present in the  $\text{MoO}_2/\text{Au}/\text{Sb}_2(\text{S,Se})_3$  interfaces.<sup>42</sup> This also indicates that the employed selenization temperature of 410 °C or a duration of 15 min is insufficient for readily evaporating S, suggesting that dual back interface engineering plays a crucial role in regulating the atomic percentage of S. Furthermore, under a constant deposition time of 5 h, the average thicknesses of the  $\text{Sb}_2(\text{S,Se})_3$  films gradually become thicker, corresponding to ~678, ~734, and ~772 nm for HS1, HS2, and HS3, respectively (Fig. 2j–l). The HS1 and HS2 films exhibit cracks and micro-voids between the Mo substrate and thin film, which can lead to carrier recombination and current leakage. Remarkably, a well-adherent layer-structured HS3 sample exhibits a quasi-uniform and highly compact thin film. A thin interfacial layer of Au is partially visible since the loading content of Au is too low to be detected clearly. Notably, the rough surface after deposition of Au can enhance surface area and offer more active sites for amplified surface reaction kinetics. Meanwhile, a strong contact/interaction is developed between  $\text{Mo}/\text{MoO}_2$  and the  $\text{Sb}_2(\text{S,Se})_3$  film owing to carrier transport channel layer Au, which is advantageous for fast carrier generation, separation, and transport.<sup>42</sup> The Raman spectrum further confirms the formation of the ternary  $\text{Sb}_2(\text{S,Se})_3$  thin film in HS1, HS2, and HS3 samples (Fig. S9†). The prominent peak at 191 cm<sup>−1</sup> represents the Sb–Se vibration, while the 201 cm<sup>−1</sup> peak is associated with the heteropolar stretching vibration of Sb–Se in Se chains.<sup>7</sup> The weak 282 and 310 cm<sup>−1</sup> vibrations for both HS2 and HS3 films can be assigned to the Sb–S bond vibrations.<sup>34</sup> Generally speaking, the HS3 film's adequate thickness, large crystals, and benign interface due to dual interface engineering contribute to higher PEC performance by improving charge transport and reducing recombination losses. The  $\text{MoO}_2$  underlayer and the carrier transport channel Au exhibit obvious interfacial interaction with the  $\text{Sb}_2(\text{S,Se})_3$  film, thereby offering favourable channels for optimized charge carrier dynamics.

KPFM was used to inspect the surface topography and potential of the thin films from the HS1, HS2, and HS3 samples. The results are depicted in Fig. 3. As seen in Fig. 3a, e and i, the surface topography and SEM photographs fairly resemble each other. The HS3 sample shows a large and compact crystal structure, while HS1 displays small crystals. A randomly selected potential line profile (Fig. 3b, f and j) illustrates the synchronous disparity in topography. A comparably equal dispersion of surface topography with high potential is seen in the HS3 sample compared to the others (Fig. 3c, g and k), showing limited defects in the surface and a fluctuating defect-induced potential, both of which are advantageous for



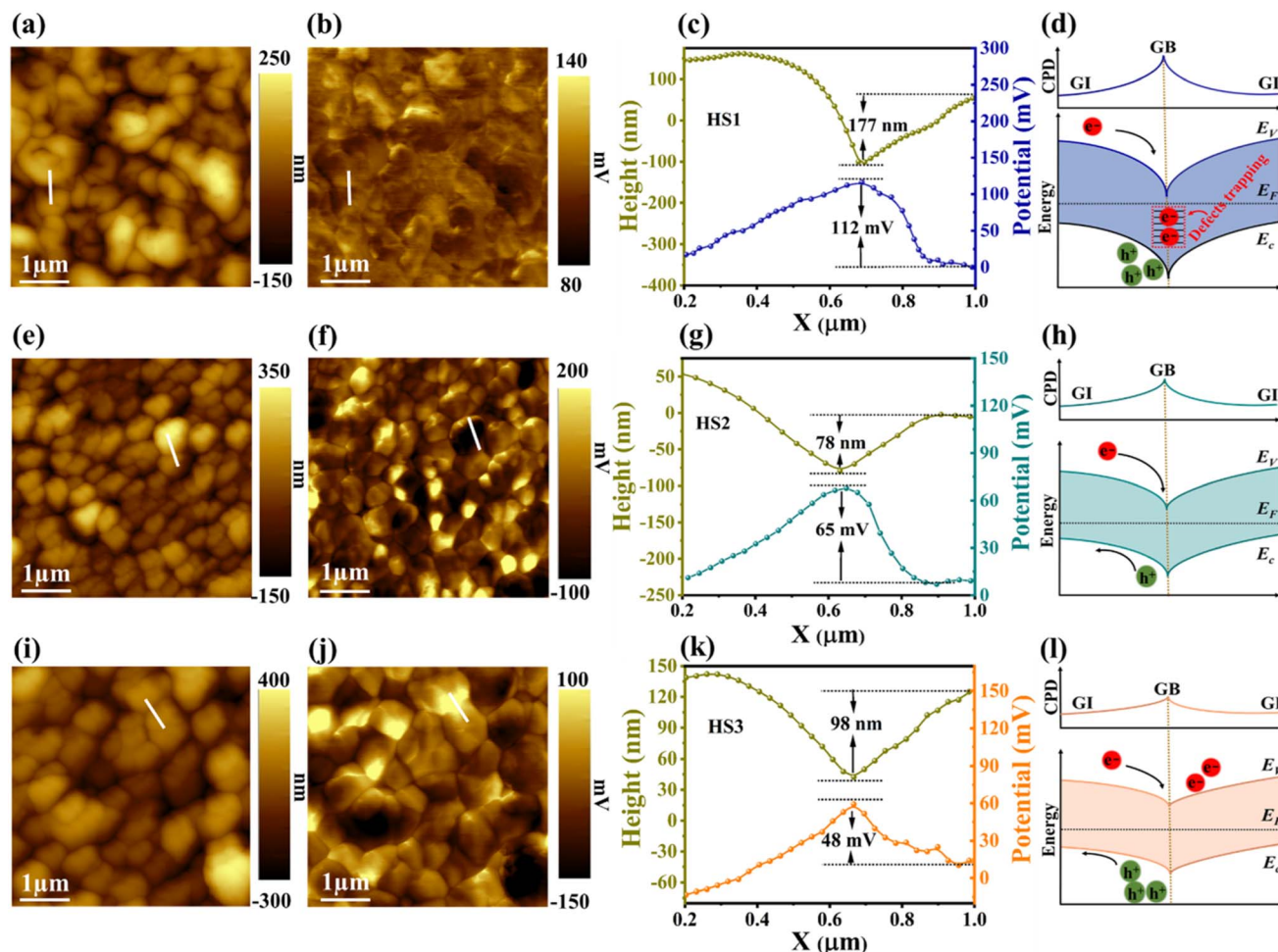


Fig. 3 KPFM characterization of thin films from HS1 (a–d), HS2 (e–h), and HS3 (i–l) samples. (a) Topography, (b) surface potential, (c) topography and potential line profile scans and (d) a schematic band bending diagram, respectively. (e–h) and (i–l) The equivalent KPFM analysis of thin films from HS2 and HS3 samples.

improving the PEC performance.<sup>47</sup> Associating the HS1 with the HS2 and HS3 samples, the contact potential difference ( $V_{CPD}$ ) value among the grain boundaries (GBs) and grain interiors (GIs) was considerably abridged from 112 to 48 mV. This represents a lower degree and incredibly apposite band-bending at the GBs of the HS3 specimen. Moreover, this benign band-bending assists charge carrier transport and collection, hinders electron entrapment by defects at the GBs, and prevents carrier recombination. The schematics of the band-bending diagrams of the HS1, HS2, and HS3 samples are shown in Fig. 3d, h and l. It is noticeable in all samples that the  $V_{CPD}$  is significantly higher at GBs than in the GIs, suggesting that the Fermi energy and vacuum levels of GBs are closer to each other, resulting in a band-bending downward at the GBs that enables a spatial separation of charge carriers.<sup>48</sup> In p-type thin films, these GBs are highly useful for attracting minority carriers (electrons) and deterring majority carriers (holes). As a result, charge carrier recombination at the GBs is reduced by strengthening the extraction of minority carriers, thus delivering the minority carriers with a current path to the interface, and this is expected to achieve higher  $J_{ph}$ .

To further delve into the influence of dual back interface engineering, the reflection spectra of  $Sb_2(S,Se)_3$  thin films were attained, employing a glass substrate and covering the 300–1500 nm wavelength range (Fig. S10a†). The spectrum clearly shows that the reflectance of the thin films from the HS2 and HS3 samples dropped gradually compared to those of HS1, especially in the shorter wavelength region. This can be associated with the evolution of surface compactness, crystallinity, and grain size, as validated by the SEM and XRD results.<sup>49</sup> Additionally, there was a synchronized blue shift related to the absorption cut-off edge that inferred a modification in the band structure. Hence, the energy bandgap ( $E_g$ ) was calculated according to Note S3,† and its values ranged from 1.226 to 1.231 eV (Fig. S10b†). This implies high composition-dependent adjustability and microstructure-dependent tolerance of band structures. Furthermore, the ideal low bandgap of  $Sb_2(S,Se)_3$  enables efficient sunlight harvesting of a broad spectrum, marking it a desirable nominee for PEC photocathodes in solar hydrogen production. Alloying  $Sb_2Se_3$  with  $Sb_2S_3$  to form  $Sb_2(S,Se)_3$  theoretically enables bandgap tuning between  $\sim 1.1$  eV ( $Sb_2Se_3$ ) and  $\sim 1.7$  eV ( $Sb_2S_3$ ) due to differences in



electronegativity and atomic sizes. However, the limited bandgap change observed in this study with varying S/Se ratios is attributed to the non-linear bandgap behaviour of the alloy system, driven by complex atomic interactions. This non-linear bandgap shift, common in mixed chalcogenides, arises from factors like lattice strain and defect states, resulting in modest bandgap adjustments despite sulfur incorporation. Moreover, Mott-Schottky (M-S) characterization studies were performed to confirm the flat-band-potential ( $E_{fb}$ ) for  $Sb_2(S,Se)_3$  thin films.<sup>47,50</sup> The M-S characterization studies of thin films from

HS1, HS2, and HS3 samples were also conducted (Fig. S11a–c†). This indicates that the  $1/C^2$  declines with potential  $V$ . The obtained  $E_{fb}$  values are approximately  $-0.074$ ,  $0.082$ , and  $0.131$   $V_{NHE}$  (for HS1, HS2, and HS3 films, respectively), showing that all three films are inherent p-type semiconductors.

### 3.2. PEC performance of $Sb_2(S,Se)_3$ photocathodes

The HS1, HS2, and HS3 films were used to fabricate the Mo/ $Sb_2(S,Se)_3$ /CdS/TiO<sub>2</sub>/Pt, Mo/MoO<sub>2</sub>/ $Sb_2(S,Se)_3$ /CdS/TiO<sub>2</sub>/Pt, and Mo/MoO<sub>2</sub>/Au/ $Sb_2(S,Se)_3$ /CdS/TiO<sub>2</sub>/Pt photocathode devices,

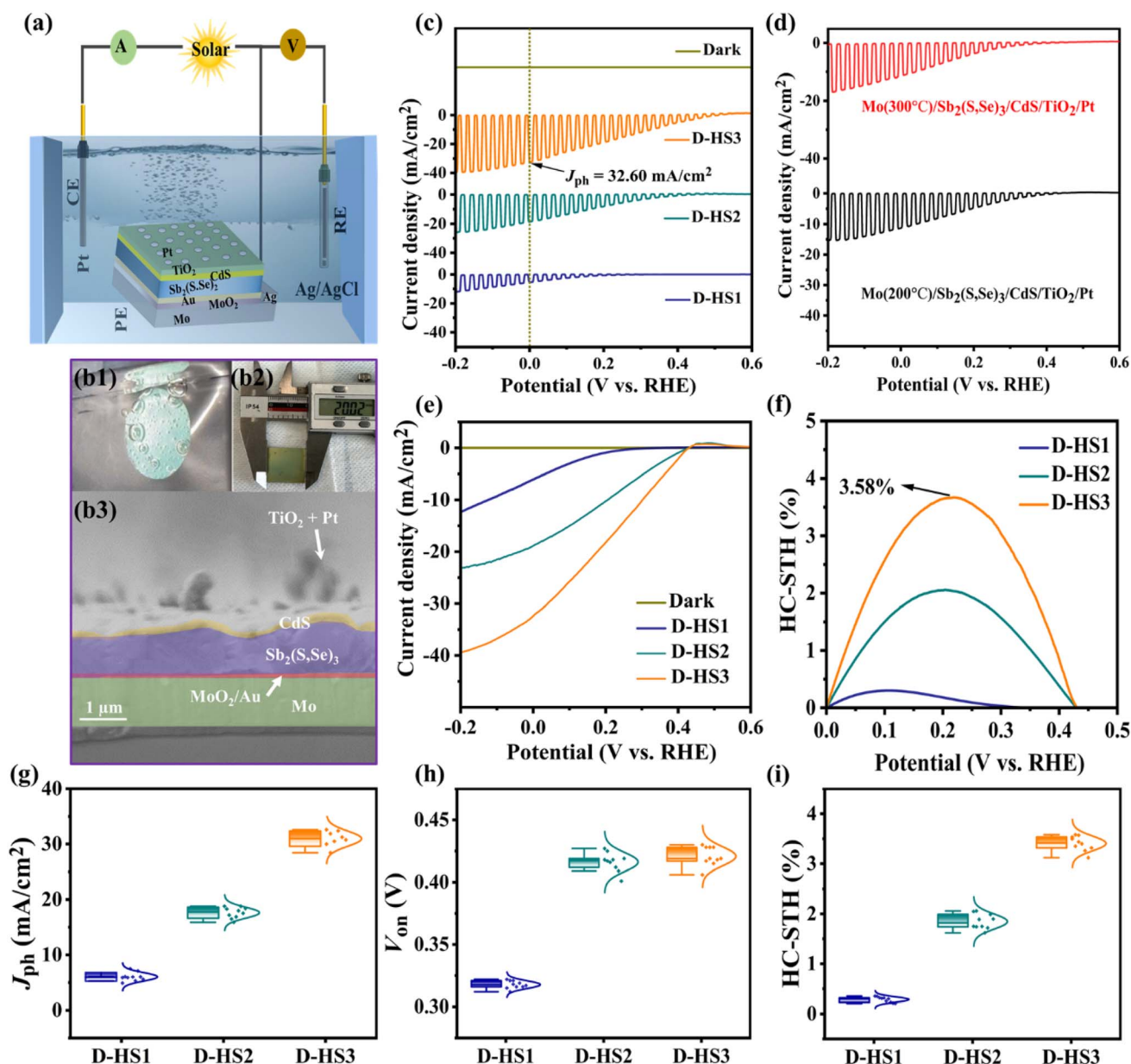


Fig. 4 (a) Schematic illustration of a PEC measurement using three electrodes. (b1) An image showing bubbles of hydrogen, (b2) a photograph of a representative  $2 \times 2$  cm<sup>2</sup>  $Sb_2(S,Se)_3$ -based photocathode, and (b3) the cross-sectional SEM photograph of the D-HS3 photocathode. (c) Chopped  $J$ - $V$  curves of the D-HS1, D-HS2, and D-HS3 photocathodes. (d) Chopped  $J$ - $V$  curves of the photocathodes based on a post-annealed (200 °C and 300 °C) Mo substrate in the dark and under chopped sunlight illumination. (e)  $J$ - $V$  curves of the D-HS1, D-HS2, and D-HS3 photocathodes in the dark and under continuous sunlight illumination. (f) The measured HC-STH conversion efficiencies of the corresponding photocathodes and (g–i) the D-HS1, D-HS2, and D-HS3 photocathodes' statistical distribution and characterization of key performance.



respectively, and they were labelled as D-HS1, D-HS2, and D-HS3, respectively. Fig. 4a provides a schematic representation of the PEC measurement procedure. Under illumination, apparent hydrogen bubbles formed at the photocathode surface and moved towards the electrolyte (Fig. 4b1), implying a productive HER. With an area over  $2\text{ cm}^2$  (Fig. 4b2), the as-prepared  $\text{Sb}_2(\text{S,Se})_3$  photocathode was quasi-homogeneous, indicating great potential in large-area application circumstances. As shown in Fig. 4b3, the champion device has an apparent layered structure of  $\text{Mo}/\text{MoO}_2/\text{Au}/\text{Sb}_2(\text{S,Se})_3/\text{CdS}/\text{TiO}_2/\text{Pt}$ . The CdS buffer layer evenly covered the larger columnar and vertically grown grains in the  $\text{Sb}_2(\text{S,Se})_3$  layer. Between the interfaces of  $\text{Mo}/\text{MoO}_2$ ,  $\text{MoO}_2/\text{Au}$ ,  $\text{Au}/\text{Sb}_2(\text{S,Se})_3$ , and  $\text{Sb}_2(\text{S,Se})_3/\text{CdS}$ , a smooth and void-free contact is observed, which is advantageous for hindering any potential interfacial recombination loss. Using chopped light, the measured current density ( $J$ - $V$ ) curves of the D-HS1, D-HS2, and D-HS3 photocathodes are depicted in Fig. 4c, suggesting an increasing tendency in the current density. The photocathode HS1 based on pristine Mo lacked an appreciable PEC photo response with a very low cathodic  $J_{\text{ph}}$  of  $\sim 5.89\text{ mA cm}^{-2}$ , as displayed in Fig. 4c. Chopped  $J$ - $V$  curves of  $\text{Mo}(200\text{ }^\circ\text{C})/\text{Sb}_2(\text{S,Se})_3/\text{CdS}/\text{TiO}_2/\text{Pt}$  and  $\text{Mo}(300\text{ }^\circ\text{C})/\text{Sb}_2(\text{S,Se})_3/\text{CdS}/\text{TiO}_2/\text{Pt}$  photocathodes are also illustrated in Fig. 4d, showing a slight improvement in photocurrent density, corresponding to a  $J_{\text{ph}}$  of  $\sim 10.70\text{ mA cm}^{-2}$  and  $\sim 13.50\text{ mA cm}^{-2}$ , respectively. This indicates that the post-annealing process has increased the Mo substrates' wettability through a synchronous development in the  $\text{MoO}_2$  oxide layer, which changed the active sites, weakened the back contact barrier, and encouraged hole transportation on its surface. Remarkable improvement in  $J_{\text{ph}}$  ( $\sim 18.80\text{ mA cm}^{-2}$ ) is noticeable upon further increasing the post-annealing temperature of the Mo substrate ( $400\text{ }^\circ\text{C}/15\text{ min}$ ), as observed in the D-HS2 photocathode (Fig. 4c). This infers that the photogenerated electron and hole pairs are effectively separated and transferred, consequently facilitating triggered electrochemical reactions at the interface between the electrode and electrolyte. Hence, the Mo substrates annealed at  $200\text{ }^\circ\text{C}$  and  $300\text{ }^\circ\text{C}$  were omitted from further analysis. The  $\text{MoO}_2$  oxide layer's functions include decreasing the back contact barrier, obtaining the preferable crystal orientation, encouraging grain growth, and lengthening the minority carrier diffusion length.<sup>35–37</sup> Moreover, by introducing a thin underlayer of carrier transport channel Au on the post-annealed Mo substrate at  $400\text{ }^\circ\text{C}$ , the D-HS3 photocathode illustrated a dramatic increase in  $J_{\text{ph}}$  ( $\sim 32.60\text{ mA cm}^{-2}$ ), as illustrated in Fig. 4c. As aforementioned, Au contributes to higher PEC performance by establishing different chemical bonds, recommending that the  $\text{MoO}_2/\text{Au}/\text{Sb}_2(\text{S,Se})_3$  assemblage connected by Au–O and Au–S bonds can accomplish the synergy acceleration of surface active sites and carrier transport channels. Additionally, the dual back interface engineering through  $\text{MoO}_2$  and Au provides robust interfacial contact between Mo and  $\text{Sb}_2(\text{S,Se})_3$  thin films, leading to augmented carrier transport. As a result, it induces the suppression of interfacial charge recombination loss, improving charge transport and separation, and producing an exceptional improvement in the performance of the D-HS3

photocathode. This enhancement can also be associated with a superior absorber layer and crystal growth kinetics (*i.e.*, the preferred (*hkl*) orientation) that prevent recombination loss and amplify carrier transport.

The linear swept current-density potential ( $J$ - $V$ ) of the D-HS1, D-HS2, and D-HS3 photocathodes under continuous and dark simulated sunlight illumination is displayed in Fig. 4e, depicting a similar variance upon the post-annealing of the Mo substrate at different temperatures and the integration of a thin carrier transport channel Au underlayer. The linear  $J$ - $V$  and HC-STH conversion efficiencies for the excluded Mo substrate samples ( $200\text{ }^\circ\text{C}$  and  $300\text{ }^\circ\text{C}$ ) were also measured (Fig. S12a and b†). The corresponding HC-STH conversion efficiencies for D-HS1, D-HS2, and D-HS3 photocathodes were determined, as shown in Fig. 4f. The highest HC-STH values for the D-HS1, D-HS2, and D-HS3 devices are  $0.30\%$  at  $0.159 V_{\text{RHE}}$ ,  $2.04\%$  at  $0.199 V_{\text{RHE}}$ , and  $3.58\%$  at  $0.218 V_{\text{RHE}}$ , respectively. Thus,  $V_{\text{on}}$  was precisely measured by broadening the linearly swept  $J$ - $V$  curves in the region where they are rapidly increasing. Consequently, the values of  $V_{\text{on}}$  were positively shifted from  $0.351 V_{\text{RHE}}$  to  $0.431 V_{\text{RHE}}$ , which coordinated well with the fluctuations in  $J_{\text{ph}}$ , implying a fully effective contribution to the HER. The samples containing a single back contact underlayer  $\text{MoO}_2$  (D-HS2) and dual back contact underlayers  $\text{MoO}_2/\text{Au}$  (D-HS3) have a larger positive  $V_{\text{on}}$ , which can be explained by the  $\text{Sb}_2(\text{S,Se})_3$  film's reduced defect density followed by the crystallographic orientation change, as confirmed by the XRD analysis (Fig. 2b).<sup>49</sup> As shown in Fig. 3, for HS2 (D-HS2) and HS3 (D-HS3) thin films, the defect density was likewise decreased, because both samples exhibit a relatively equal dispersion of surface topography with high potential in comparison to HS1, indicating limited surface defects and fluctuating defect-induced potential, which is significantly beneficial for enhancing the PEC performance parameters such as  $V_{\text{on}}$  and  $J_{\text{ph}}$ . Moreover, the passivation of surface states is essential for improving charge separation and lowering recombination because they are known to function as trapping and recombination sites. Meanwhile, the bulk recombination centres formed by cation–anion defects are often suppressed by increasing the S content in materials like  $\text{Sb}_2\text{Se}_3$  and  $\text{Sb}_2(\text{S,Se})_3$ .<sup>6,51</sup> The XPS (Fig. 2d–f; and Table S3†) and EDS studies show that the S concentration is slightly increased for both HS2 and HS3 samples, which encourages the suppression of bulk recombination centres even further to enhance  $V_{\text{on}}$ . However, the limited improvement in the onset potential of  $\text{Sb}_2(\text{S,Se})_3$  compared to pristine  $\text{Sb}_2\text{Se}_3$  is likely due to the complex defect chemistry in the mixed-anion system. Incorporating sulfur into  $\text{Sb}_2\text{Se}_3$  can introduce shallow donor states, increasing recombination at grain boundaries and negatively affecting the onset potential. While sulfur incorporation might enhance charge carrier separation, it can also increase defect density or carrier recombination, leading to competing effects. The onset potential is influenced not only by the bandgap but also by surface states and recombination dynamics at the photocathode-electrolyte interface. Sulfur incorporation may alter the electronic structure or create additional recombination sites, offsetting potential gains in onset potential. It is noteworthy to mention that the finest



values among the  $\text{Sb}_2(\text{S,Se})_3$  photocathodes are demonstrated in this work, with a maximum  $J_{\text{ph}}$  ( $\sim 32.60 \text{ mA cm}^{-2}$ ) and  $V_{\text{on}}$  ( $\sim 0.431 V_{\text{RHE}}$ ). Fig. S13† shows the incident photon-to-current conversion efficiency (IPCE) spectra for  $\text{Sb}_2(\text{S,Se})_3$  photocathodes (D-HS1, D-HS2, and D-HS3), both with and without dual back-layer engineering, across 300–1000 nm. The D-HS3 device, which includes dual back underlayers (D-HS3), displays superior photon absorption and conversion, especially from 550 to 750 nm. Integrated photocurrents from the IPCE spectra are  $\sim 5.10 \text{ mA cm}^{-2}$  for D-HS1,  $\sim 17 \text{ mA cm}^{-2}$  for D-HS2, and  $\sim 31.4 \text{ mA cm}^{-2}$  for D-HS3, aligning well with  $J_{\text{ph}}$  data from  $J$ - $V$  measurements, though slightly lower due to the difference in conditions between chopped LSV and IPCE measurements such as calibration, wavelength of photons, size of the light source, *etc.* In parallel, the statistical distributions of the D-HS1, D-HS2, and D-HS3 photocathode performance parameters are shown in Fig. 4g–i. The dual back underlayers including  $\text{MoO}_2$  and carrier transport channel Au have a strong and credible positive impact on the performance of the D-HS3 photocathode. Table 1 compares key parameters of this study's champion  $\text{Mo/MoO}_2/\text{Au/Sb}_2(\text{S,Se})_3/\text{CdS/TiO}_2/\text{Pt}$  photocathode to those of some of the best chalcogenide photocathodes that have been previously reported, including  $\text{Sb}_2\text{Se}_3$ ,  $\text{Sb}_2\text{S}_3$ , and  $\text{Sb}_2(\text{S,Se})_3$ .<sup>2,8,17,30,32,33,51,52</sup> The comparison clearly shows that this device can achieve a comparable  $V_{\text{on}}$  of  $\sim 0.431 V_{\text{RHE}}$  and  $\sim 3.58\%$  HC-STH efficiency, leading to a simultaneously superior  $J_{\text{ph}}$  of  $32.60 \text{ mA cm}^{-2}$  amongst the  $\text{Sb}_2(\text{S,Se})_3$ -based reported photocathodes so far. Moreover, the PEC performance of this device is analogous to that of other state-of-the-art chalcogenide-based (*i.e.*,  $\text{Sb}_2\text{Se}_3$ ) photocathodes presented at the top of the table.

Furthermore, efficient solar harvesting can also be stimulated by using such a perfect narrow bandgap. Therefore, the theoretical  $J_{\text{ph}}$  of the  $\text{Sb}_2(\text{S,Se})_3$ -based photocathodes was calculated using the absorbance (Fig. S14 and Note S4†), LHE (wavelength-dependent light harvesting efficiency) and AM 1.5G standard solar spectrum. Since the  $\lambda_{\text{e}}$  is  $\approx 1070 \text{ nm}$ , the  $J_{\text{ph}}$  for D-HS3 is  $40.80 \text{ mA cm}^{-2}$  as portrayed in Fig. 5a, and  $32.30$  and  $37.70 \text{ mA cm}^{-2}$  for D-HS1 and D-HS2, respectively (Fig. S15a and b†). Moreover, the photocurrent transient method is a widely accepted approach for calculating charge transfer ( $\eta_{\text{tran}}$ ) and charge separation ( $\eta_{\text{sep}}$ ) efficiencies, particularly in

photocathode systems. The following eqn (2) and (3), commonly used for this analysis, reliably reflect charge carrier dynamics when experimental parameters are well-controlled.<sup>2,47,52</sup> This method provides valuable insights into interfacial processes without altering the experimental environment and offers a realistic assessment of charge separation and transfer under practical PEC water-splitting conditions, especially for  $\text{Sb}_2(\text{S,Se})_3$ -based photocathodes. Fig. 5b displays the transient photocurrent attenuation spectra of the D-HS1, D-HS2, and D-HS3 photocathodes. The presence of the carrier recombination effect is evident in the D-HS1 photocathode, as it reveals an obvious “spike-like” transit under abrupt illumination. In contrast, the D-HS2 and D-HS3 photocathodes exhibit almost no “spike-like” transit, indicating boosted carrier transfer and attenuated charge recombination.<sup>7</sup> The  $\eta_{\text{tran}}$  could be calculated using the determined photocurrents related to the “light off” and “light on” states due to the transient accumulation of charges at the electrode/electrolyte interface.<sup>53</sup> In detail, the  $\eta_{\text{sep}}$  could be investigated as follows:<sup>47</sup>

$$\eta_{\text{tran}} = \frac{J_{\text{ss}}}{J_{\text{inst}}} \quad (2)$$

$$J_{\text{ph}} = J_{\text{abs}} \times \eta_{\text{tran}} \times \eta_{\text{sep}} \quad (3)$$

where  $J_{\text{ss}}$  and  $J_{\text{inst}}$  are the steady-state photocurrent density and instantaneous photocurrent density, respectively. The D-HS1, D-HS2, and D-HS3 devices exhibit high  $\eta_{\text{tran}}$  values of 93.1%, 96.3%, and 98.4%, respectively, demonstrating that the functional electron and hole transport layers accelerate photoelectron transfer from the photocathode bulk to the electrode or electrolyte interface and the transmission of holes between the Mo substrate and  $\text{Sb}_2(\text{S,Se})_3$  absorber. On the other hand, the determined  $\eta_{\text{sep}}$  values are 18.4%, 51.9%, and 81.5%, respectively, indicating reliability with the previously discussed analysis of the absorber layer's impact on charge transport and separation. The variation in  $\eta_{\text{sep}}$  values can be directly related to the  $\text{Sb}_2(\text{S,Se})_3$  film quality,  $\text{Sb}_2(\text{S,Se})_3/\text{CdS}$  heterojunction, and improved back contact interface ( $\text{Mo/MoO}_2/\text{Au/Sb}_2(\text{S,Se})_3$ ) interaction between the absorber and Mo substrate. The synergistic introduction of both underlayers as a dual back interface engineering strategy noticeably enhanced the effective

**Table 1** Summary of the PEC performance for some of the best chalcogenide photocathodes reported recently, containing  $\text{Sb}_2\text{Se}_3$ ,  $\text{Sb}_2\text{S}_3$ , and  $\text{Sb}_2(\text{S,Se})_3$

Photocathode	Electrolyte	$J_{\text{ph}}$ ( $\text{mA cm}^{-2}$ at 0 $V_{\text{RHE}}$ )	$V_{\text{on}}$ ( $V_{\text{RHE}}$ )	HC-STH (%)	Ref.
FTO/Au/ $\text{Sb}_2\text{Se}_3$ /CdS/ $\text{TiO}_2$ /SnO <sub>2</sub>	0.1 M $\text{H}_2\text{SO}_4$	29	0.50	3.8	33
FTO/Au/ $\text{Sb}_2\text{Se}_3$ /PABA/ $\text{TiO}_2$ /Pt	0.1 M $\text{H}_2\text{SO}_4$	35	0.50	4.7	8
Glass/Mo/ $\text{Sb}_2\text{Se}_3$ /CdS (In)/ $\text{TiO}_2$ /Pt	0.5 M $\text{H}_2\text{SO}_4$	35.7	0.54	5.6	2
Mo/ $\text{Sb}_2\text{S}_3$ /CdS/ $\text{TiO}_2$ /Pt	0.5 M $\text{Na}_2\text{SO}_4$	6.0	0.50	0.64	32
SLG/Mo/Ag/ $\text{Sb}_2\text{S}_3$ /CdS/Pt	0.5 M $\text{Na}_2\text{SO}_4$	9.4	0.56	1.20	51
SLG/Mo/Ag/ $\text{Sb}_2\text{S}_3$ /Al <sub>2</sub> O <sub>3</sub> /CdS/Pt	0.5 M $\text{Na}_2\text{SO}_4$	13.0	0.68	2.78	52
FTO/Au/ $\text{Sb}_2\text{S}_3$ / $\text{TiO}_2$ /Pt	0.1 M $\text{H}_2\text{SO}_4$	22.5	0.52	0.69	17
Mo/grad-S: $\text{Sb}_2\text{Se}_3$ / $\text{TiO}_2$ /Pt	1 M $\text{H}_2\text{SO}_4$	14.2	0.42	2	30
FTO/Au/ $\text{Sb}_2(\text{S,Se})_3$ / $\text{TiO}_2$ /Pt	0.1 M $\text{H}_2\text{SO}_4$	16.5	0.44	1.1	17
SLG/Mo/ $\text{MoO}_2$ /Au/ $\text{Sb}_2(\text{S,Se})_3$ /CdS/Pt	0.5 M $\text{H}_2\text{SO}_4$	32.60	0.431	3.58	This work



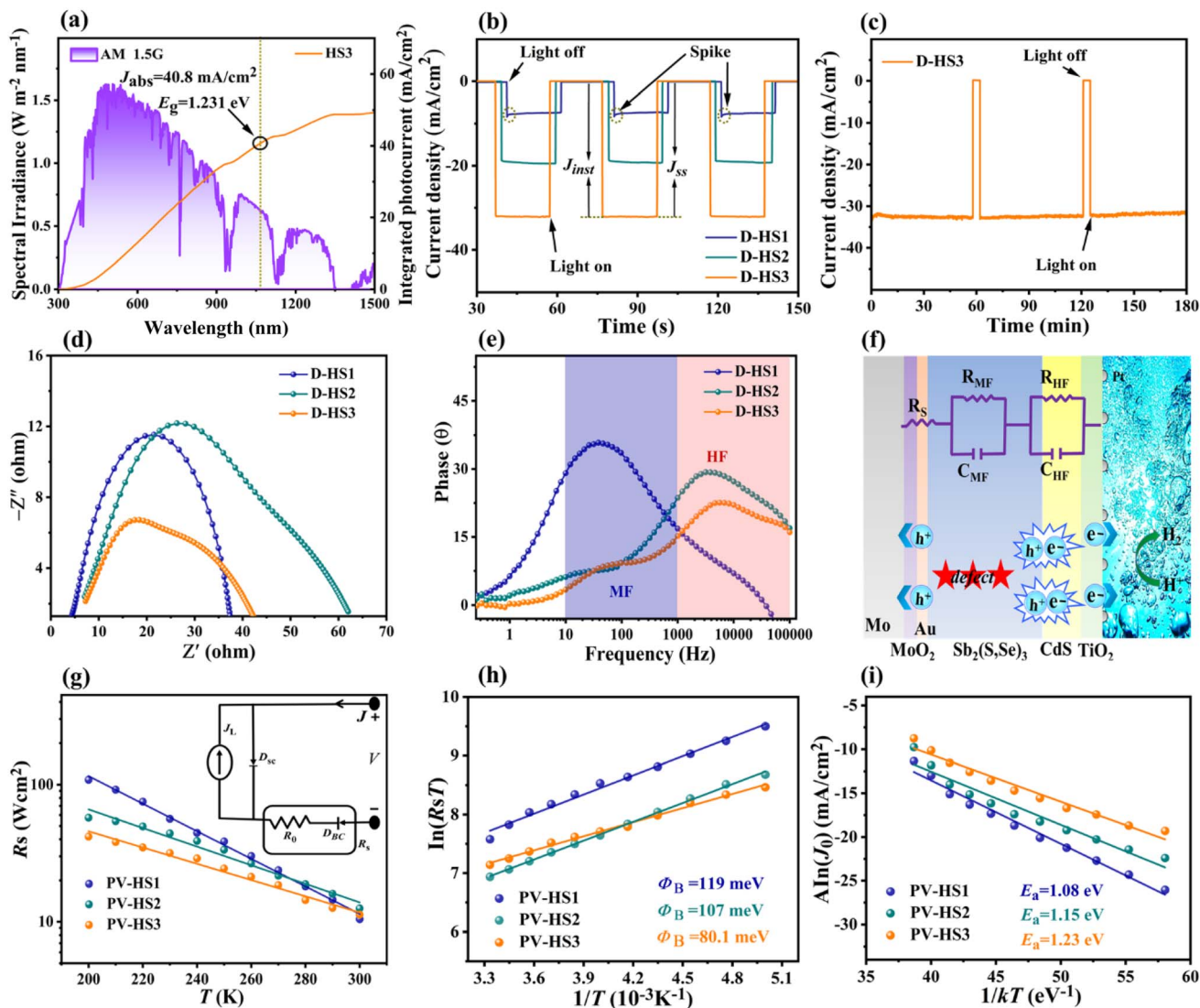


Fig. 5 (a) Energy density flux for the AM 1.5G standard solar spectrum and integrated photocurrent density of the HS3 sample. (b) Transient photocurrent response of D-HS1, D-HS2 and D-HS3 photocathodes. (c) Photocurrent stability test of the D-HS3 photocathodes (at 0  $V_{\text{RHE}}$ ) for 3 h under illumination. (d) Nyquist and (e) Bode plots of the D-HS1, D-HS2 and D-HS3 photocathodes. (f) Schematic diagram along with the equivalent circuit system related to the charge carrier dynamics procedures. (g) Temperature-dependent  $R_s$  of the devices and the inset figure illustrates a circuit model. (h) Blocking contact barrier height determination of the PV-HS1, PV-HS2 and PV-HS3 photovoltaic devices using the temperature-dependent  $J$ - $V$  measurement. (i)  $A \ln(J_0)$  versus  $1/kT$  plot of the corresponding photovoltaic devices.

extraction and collection of carriers by suppressing the interface and bulk recombination (this will be discussed in more detail later).

A similar  $J_{\text{ph}}$  variation with  $\text{Sb}_2(\text{S,Se})_3$  film thickness is shown in the chopped  $J$ - $T$  (photocurrent-density-time) curves collected under AM 1.5G solar irradiation, indicating remarkable reversibility and stability (Fig. S16a-c†). Especially after operating for 3 h (Fig. 5c), the champion device D-HS3 retained around  $\sim 94.7\%$  of its  $J_{\text{ph}}$  ( $\sim 30.9 \text{ mA cm}^{-2}$ ), and even demonstrated the validity of hydrogen production after 6 h of operation (Movie S1, ESI†), indicating long-term stability. The literature suggests that partial photocorrosion of the CdS buffer layer occurs to some extent due to the assembly of injected charges, driven by thermodynamically favorable CdS redox

transformations.<sup>54</sup> The enhanced stability of the optimized D-HS3 device compared to D-HS1 and D-HS2 is primarily due to the synergistic effects of dual back interface engineering, which includes a  $\text{MoO}_2$  underlayer and a thin Au film. This design improves substrate wettability, enhances adhesion, and promotes a uniform, compact thin film, thereby reducing grain boundaries and defects that act as recombination centres. The  $\text{MoO}_2$  underlayer serves as a hole-blocking layer, minimizing charge carrier losses, while the Au underlayer provides an additional pathway for electron transport, further enhancing charge carrier separation and reducing recombination. In contrast, a clear decline in stability is evident for D-HS1 and D-HS2 photocathodes (Fig. S17a and b†). D-HS1 and D-HS2 show a rapid decrease in photocurrent density over time due to non-

uniform thin films and poor back contact, which limits efficient charge carrier transport and increases recombination rates. Prolonged light exposure also contributes to photo-induced degradation in these samples, exacerbating performance loss (Movie S2†). Overall, the additional Mo/MoO<sub>2</sub>, MoO<sub>2</sub>/Au, and Au/Sb<sub>2</sub>(S,Se)<sub>3</sub> junctions may have been advantageous since they enhanced the thin film's crystallinity, stability, and void-free interface, resulting in boosted carrier transportation, extraction, and collection efficiency. These optimizations are specifically accomplished through dual back interface engineering, which improves back contact modifications, promotes preferred Sb<sub>2</sub>(S,Se)<sub>3</sub> crystal growth, and enhances the Sb<sub>2</sub>(S,Se)<sub>3</sub>/CdS heterojunction interface, ensuring the long-term stability of the D-HS3 photocathode.

The PEIS analysis of the Sb<sub>2</sub>(S,Se)<sub>3</sub>-based photocathodes was carried out to explore the specific charge carrier recombination and transfer features. Fig. 5d shows Nyquist plots with a single arc for D-HS1 and two arcs for the D-HS2 and D-HS3 photocathodes, illustrating consistency with the corresponding Bode diagrams (Fig. 5e), which include two regions with frequencies ranging from 10–100 kHz. In addition, Fig. 5f displays the schematic diagram and the analogous circuit system connected to the charge transfer procedure. Generally speaking, the bulk semiconductor capacitance ( $C_{\text{HF}}$ ) and the photoelectrode's internal charge transfer resistance ( $R_{\text{HF}}$ ) are affected by the PEIS-achieved high-frequency arc ( $\approx 10^3$ – $10^5$  Hz), the capacitance ( $C_{\text{MF}}$ ), and the charge capture resistance ( $R_{\text{MF}}$ ). Under the surface, trapping states in the bandgap are reflected by the middle-frequency arc ( $\approx 10^1$ – $10^3$  Hz), and the electrode and electrolyte interface's capacitance ( $C_{\text{LF}}$ ) and the resistance related to electro-chemical-charge-transfer reactions ( $R_{\text{LF}}$ , e.g., HER) are indicated by the low-frequency arc ( $\approx 10^{-1}$ – $10^1$  Hz).<sup>27</sup> In this scenario, the low-frequency dependent resistor-capacitor ( $R_{\text{LF}}-C_{\text{LF}}$ ) component cannot be clearly observed due to the high concentration of oxidizing species ( $\text{H}^+$ ) on the electrode surface and in the electrolyte. As a result, it is supposed that hydrogen would be generated by the transport of all photoelectrons towards the electrode or electrolyte and holes from the absorber at the substrate interface, demonstrating 100% Faraday efficiency. The PEIS data were fitted with an equivalent circuit design that consisted of two pairs of parallel resistor capacitors ( $R-C$ ) and a series resistance ( $R_s$ ). The Mo/Sb<sub>2</sub>(S,Se)<sub>3</sub> back contact interface resistance is specifically responsible for the  $R_s$ ; the space charge region's capacitance for the Sb<sub>2</sub>(S,Se)<sub>3</sub>/CdS heterojunction of these three devices is denoted by the  $R_{\text{HF}}$  and  $C_{\text{HF}}$  interfaces; and the associated charge transport resistance and the internal defect capacitance and resistance in Sb<sub>2</sub>(S,Se)<sub>3</sub> films are represented by  $C_{\text{MF}}$  and  $R_{\text{MF}}$ , respectively. PEIS-fitted parameters for all three D-HS1, D-HS2, and D-HS3 photocathodes were determined (Table S4†), where the increased  $R_s$  values ( $\sim 3.2$ – $3.8 \Omega$ ) specify a benign back contact interface, particularly by applying dual back interfacial layers of MoO<sub>2</sub> and Au to enhance carrier transport and diminish recombination. The D-HS3 sample has an incredibly lower  $C_{\text{HF}}$  value ( $\sim 1.18 \times 10^{-6}$  F), implying that the charge accumulation occurs in a shorter time; the significantly lowered value of  $R_{\text{HF}}$  ( $\sim 1.37 \Omega$ ) also recommends more efficient carrier separation

and interface transportation. A remarkably lower  $R_{\text{MF}}$  value of  $5.04 \Omega$  shows reduced bulk defects inside the D-HS3 absorber thin film due to an optimum connection between frequency and impedance at medium or low frequencies.

### 3.3. Analyzing the mechanisms of enhanced device performance

To gain a deeper understanding of these Mo/MoO<sub>2</sub>, MoO<sub>2</sub>/Sb<sub>2</sub>(S,Se)<sub>3</sub>, Au/Sb<sub>2</sub>(S,Se)<sub>3</sub>, and Sb<sub>2</sub>(S,Se)<sub>3</sub>/CdS heterojunction interfaces and their influence on the performance of photoelectric devices, the corresponding photovoltaic cells having identical device configurations (e.g., Mo/MoO<sub>2</sub>/Au/Sb<sub>2</sub>(S,Se)<sub>3</sub>/CdS/ITO/Ag) were prepared and denoted as PV-HS1, PV-HS2, and PV-HS3, respectively.

Temperature-dependent measurements ( $J-V-T$ ) were used in a dark environment in the temperature range of 200–300 K (Fig. S18a–c†) to further elucidate the sample's improved performance with the dual back interface modification. When the temperature decreased, the PV-HS1 device behaved like an open diode, but the devices (PV-HS2 and PV-HS3) that were treated with single or dual back interface layers continued to exhibit suppressed diode properties, indicating a decrease in the transfer barrier.<sup>55</sup> To estimate temperature-dependent series-resistance ( $R_s$ ), the specimen  $J-V-T$  curves are plotted in Fig. 5g. The  $R_s$  of the PV-HS1 sample grew drastically by about 11 times from 300–200 K, compared with the 5 and 3 times rise noted for the PV-HS2 and PV-HS3 samples, respectively. The deviation in  $R_s$  values with declining temperature implies that the background series resistance and the blocking barrier are responsible for the back contact barrier height, which confines charge transport.<sup>56</sup> The inset photograph of Fig. 5g illustrates the device's back-contact junction model as a Schottky diode. Two diodes are included in the circuit model: the primary solar cell diode ( $D_{\text{SC}}$ ) and the back contact diode ( $D_{\text{BC}}$ ).<sup>37</sup> The  $D_{\text{BC}}$  is normally reverse biased when the  $D_{\text{SC}}$  is forward biased; however, the reverse biased  $D_{\text{BC}}$  is fairly detrimental to the production of photogenerated current. Consequently, the back contact barrier value is reduced by the dual back underlayers MoO<sub>2</sub> and Au, greatly minimizing the detrimental effect of the reverse biased  $D_{\text{BC}}$  on the photo-generated current output.

Furthermore, the back contact diode barrier height ( $\Phi_{\text{B}}$ ) was determined by plotting  $\ln(R_s T)$  versus  $1/T$  (Fig. 5h). The PV-HS2 sample's  $\Phi_{\text{B}}$  value was 107 meV, which was lower than the PV-HS1 device's (119 meV), implying that the PV-HS2 device has a lower barrier height. Moreover, the PV-HS3 dual back underlayer (MoO<sub>2</sub> and Au) treatment produced a back contact barrier height of 80.1 meV, significantly improving charge transport and optimizing the device's performance. Generally, repressing the height of the back contact barrier is an important factor for augmenting carrier transport.  $J-V-T$  analysis can be used to ascertain the dominant recombination path present in devices by plotting  $A \ln(J_0)$  versus  $1/kT$ , as shown in Fig. 5i. The activation energy ( $E_a$ ) of interface recombination is normally approximated by using  $A \ln(J_0)$  vs.  $1/kT$ , and its value can be attributed to as the predominance of both interface and bulk recombination.<sup>56</sup> The PV-HS1 sample has an inferior  $E_a$  value of



1.08 eV compared with the bandgap, demonstrating the dominating interface recombination, while PV-HS2 and PV-HS3 devices have superior  $E_a$  values of 1.15 and 1.23 eV, respectively, which are in close proximity to the bandgap. As a result, interface recombination was greatly reduced by dual back interface layer modulation, improving junction quality and lowering the back contact barrier height.

Admittance spectroscopy was performed to find out the influence of dual back interface engineering by incorporating an intermediate layer of  $\text{MoO}_2$  followed by carrier transport channel Au on the bulk defect properties. Fig. 6a, d and g show the  $C$ - $f$ - $T$  (temperature-dependent capacitance-frequency) of PV-HS1, PV-HS2, and PV-HS3 devices measured in varying temperature ranges of 340–110 K with 10 K increments and frequency ranges increasing from  $10^2$ – $10^6$  Hz. Only one defect

level can be identified against frequency, indicating that only one type of defect can be found. The inflection frequencies ( $\omega_0 = 2\pi f_0$ ) were obtained through the angular frequency point  $\omega$  at the maximum value of the plot of  $\omega dC/d\omega$ . The slopes of a linear fit of the Arrhenius plots were used to determine the defect activation energies based on the following equation:<sup>48</sup>

$$\ln\left(\frac{\omega_0}{T^2}\right) = \ln(2\nu_0) - \frac{E_A}{K_B T} \quad (4)$$

where  $\nu_0$  represents the attempt-to-escape frequency,  $E_A$  denotes the mean defect energy-level to either the conduction-band edge or valence-band edge, and  $K_B$  denotes the Boltzmann constant. The  $E_A$  values of 477, 447 and 388 meV were obtained from PV-HS1, PV-HS2 and PV-HS3 devices, respectively, as shown in Fig. 6b, e and h. These  $E_A$  values belong to the same type of

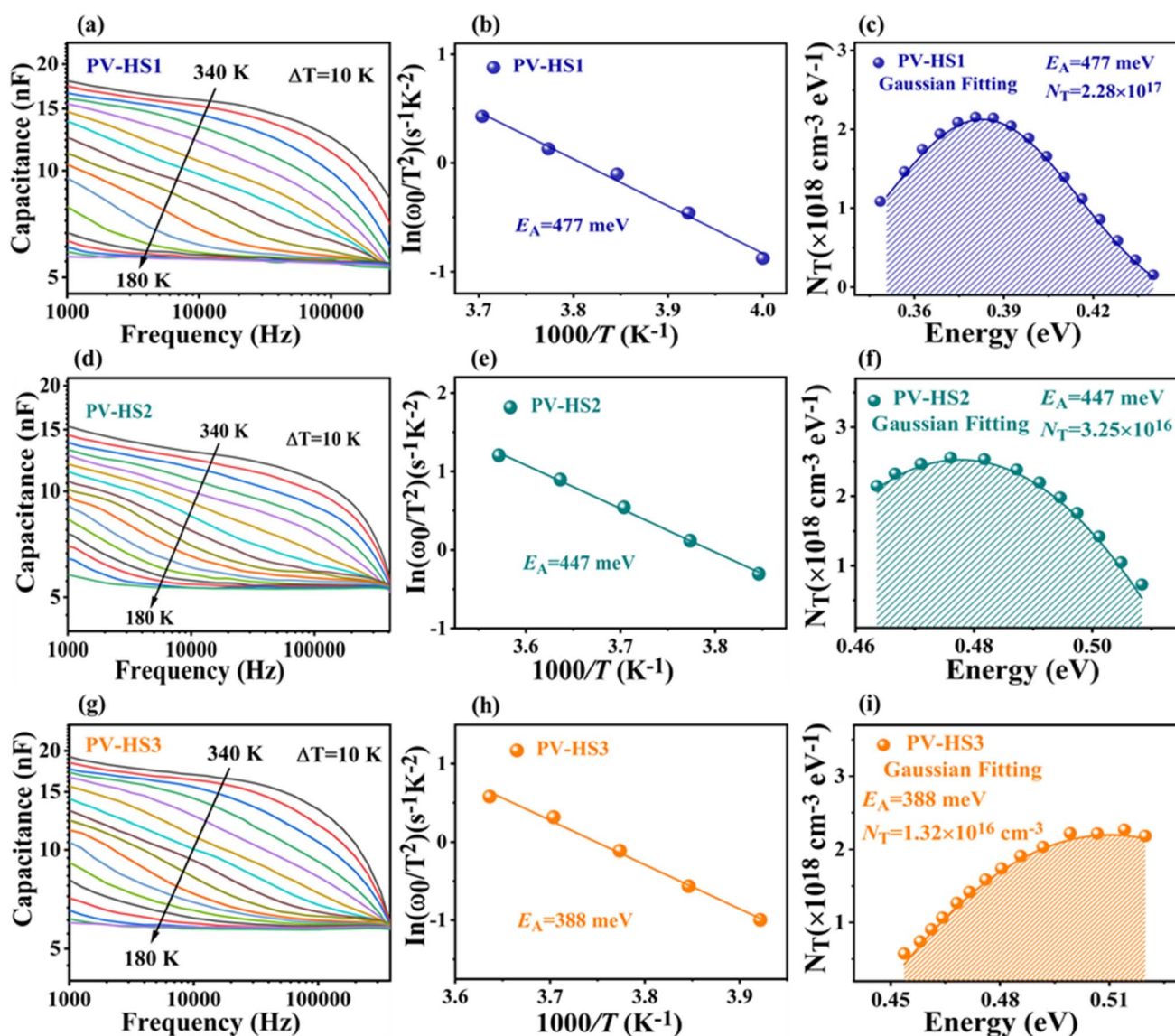


Fig. 6 Characterization of temperature-dependent admittance spectroscopy for  $\text{Sb}_2(\text{S,Se})_3$  photovoltaic devices. (a, d and g) Variation of capacitance at different frequencies and temperatures. (b, e and h) Using the Arrhenius plots of the characteristic frequencies to acquire the defect activation energy. (c, f and i) Defect distributions of PV-HS1, PV-HS2 and PV-HS3 devices.



relatively shallow defect based on first-principles calculations for  $\text{Sb}_2\text{Se}_3$  that are known to function as recombination centres in the  $\text{Sb}_2\text{Se}_3$ -based PEC devices.<sup>48,57</sup> The lower value of  $E_A$  obtained for the intrinsic defects can be attributed to the Se vacancy ( $V_{\text{Se}}$ ) defect. Theoretical calculations suggest that the  $V_{\text{Se}}$  defects can be involved in the trapping of hole carriers. To gain further insights, the defect densities ( $N_T$ ) were fitted with Gaussian by applying the Kimerling model:<sup>57</sup>

$$\begin{cases} E(\omega) = kT \ln\left(\frac{2\pi\nu_0 T^2}{\omega}\right) \\ N_T[E(\omega)] = -\frac{V_{\text{bi}}}{q\omega} \cdot \frac{dC}{d\omega} \cdot \frac{\omega}{kT} \end{cases} \quad (5)$$

where  $E$  reflects the energetic-distance between the defect energy-level and either the conduction-band minimum (CBM)

or the valence-band maximum (VBM).  $N_T[E(\omega)]$  and  $V_{\text{bi}}$  are the defect density and integrated potential of the P-N junction. The defect densities of the PV-HS1, PV-HS2 and PV-HS3 devices are presented in Fig. 6c, f and i, and their values are  $2.28 \times 10^{17}$ ,  $3.25 \times 10^{16}$  and  $1.32 \times 10^{16} \text{ cm}^{-3}$ , respectively. The variation in defect density values in the absorber layer shows efficient bulk defect passivation and nonradiative recombination. However, the deep-level defects are not found in admittance spectroscopy, and the defect density  $V_{\text{Se}}$  in the  $\text{Sb}_2(\text{S,Se})_3$  thin-film of the PV-HS3 device is condensed with a slightly higher S concentration. Due to the severe trap-assisted space-charge region (SCR) recombination that results from these defects, the carrier lifetime is reduced and cannot be ignored.<sup>57</sup> Thus, it can be inferred that the dual back underlayers  $\text{MoO}_2$  and Au reduced the defect density of the devices, leading to a decrease in recombination between the interfacial and absorber layers.

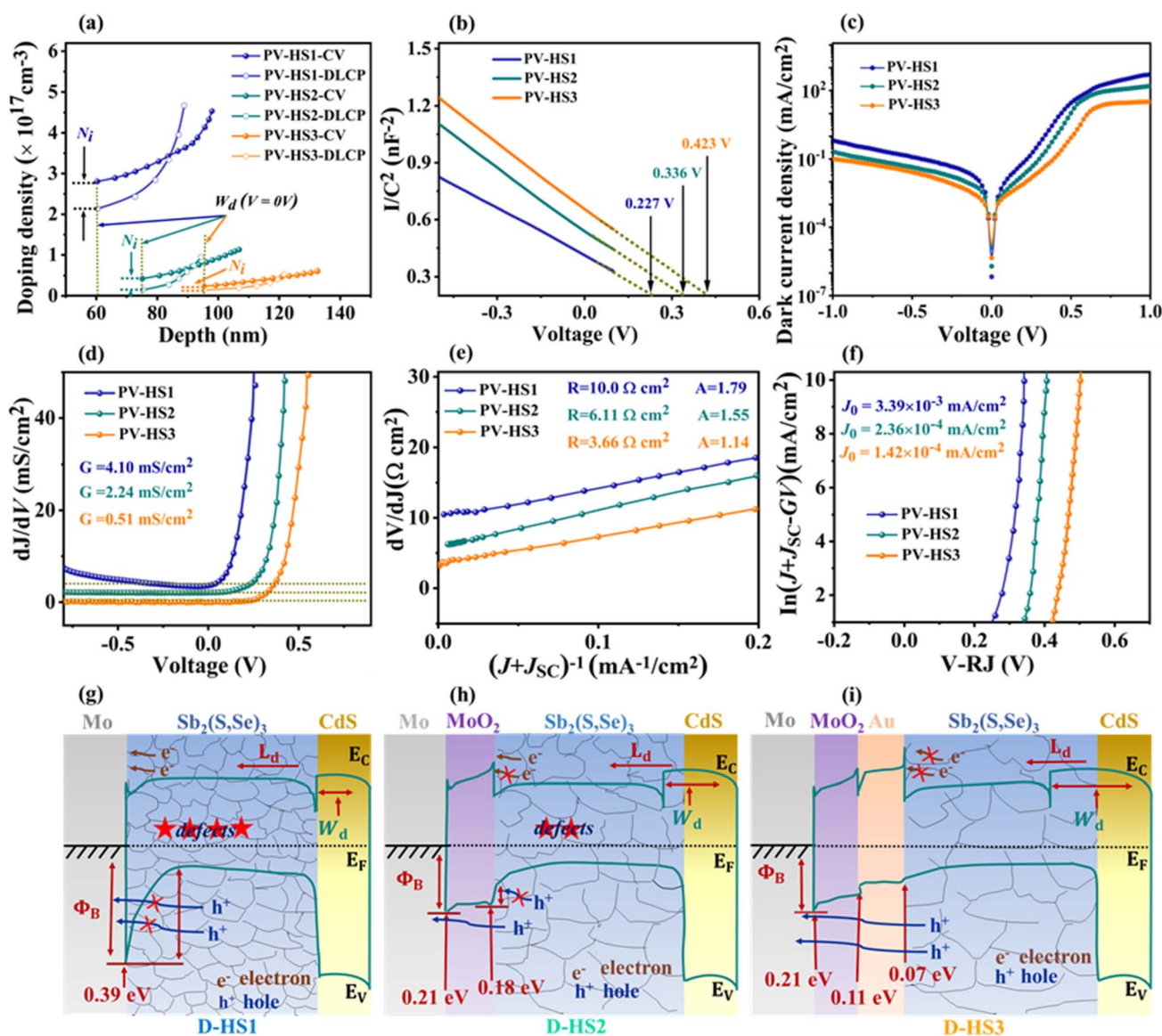


Fig. 7 (a) C-V and DLCP profiles. (b)  $1/C^2$ -V graphs of the PV-HS1, PV-HS2, and PV-HS3 photovoltaic devices. Electrical behaviours of the corresponding three devices: (c) dark  $J$ -V curves, (d) characterization of the shunt conductance  $G$ , (e) the series resistance  $R$ , the ideality factor  $A$ , and (f) the current density  $J_{\text{sc}}$  for reverse saturation. The band diagrams of D-HS1 (g), D-HS2 (h), and D-HS3 (i) devices.

To determine the influence of interfacial recombination, deep-level capacitance profiling (DLCP) and capacitance–voltage ( $C$ – $V$ ) profiling measurements were performed, and the results are displayed in Fig. 7a and b. Bulk defects, interfacial defects, and free carriers are all included in the doping density  $N_{C-V}$  determined by the  $C$ – $V$  profiling, whereas only free carriers and bulk defects are included in the doping density  $N_{DLCP}$  determined by DLCP. The following formulae can be used to get the  $N_{C-V}$  and  $N_{DLCP}$  plots *versus* the profiling width  $x$ :<sup>36</sup>

$$\left\{ \begin{array}{l} N_{C-V} = \frac{-2\varepsilon_{r,n}N_D}{\left(\frac{d(1/C^2)}{dV}\right)qA^2\varepsilon_0\varepsilon_{r,n}\varepsilon_{r,p}N_D + 2\varepsilon_{r,p}} \\ N_{DLCP} = \frac{C_0^3}{2q\varepsilon_0\varepsilon_{r,p}A^2C_1} \\ W_d = \frac{\varepsilon_0\varepsilon_{r,p}A}{C_0} \end{array} \right. \quad (6)$$

where  $N_D$ ,  $A$ ,  $\varepsilon_{r,n}$ ,  $\varepsilon_{r,p}$ ,  $C_0$ ,  $C_1$ , and  $W_d$  are the CdS doping density, the device area, the CdS and  $Sb_2(S,Se)_3$  relative permittivity, two parameters for quadratic fitting obtained from the  $C$ – $V$  curves, and the depletion width of the device, respectively. The relationship between the built-in voltage ( $V_{bi}$ ) and the depletion width ( $W_d$ ) can be approximated by using the following equation:<sup>36</sup>

$$W_d = \sqrt{\frac{2\varepsilon_p\varepsilon_n(N_A + N_D)^2}{qN_A + N_D(\varepsilon_pN_A + \varepsilon_nN_D)}}V_{bi} \quad (7)$$

where  $q$ ,  $\varepsilon_p$ ,  $\varepsilon_n$ ,  $N_D$ , and  $N_A$  are the elementary charge, the permittivity, the donor density, and acceptor density in  $Sb_2(S,Se)_3$  and CdS, respectively. The interfacial defect concentrations of PV-HS1, PV-HS2, and PV-HS3 are calculated to be  $4.67 \times 10^{17} \text{ cm}^{-3}$ ,  $9.44 \times 10^{16} \text{ cm}^{-3}$  and  $4.93 \times 10^{16} \text{ cm}^{-3}$ , respectively. This means that the interfacial defect concentration would be significantly reduced for optimized P–N junction quality with either a single or dual back interface treatment. The difference between low and high-frequency carrier concentrations can be linked to the number of bulk defects. By using  $C^{-2}$ – $V$  analysis, the  $V_{bi}$  values of PV-HS1, PV-HS2 and PV-HS3 are found to be 0.227, 0.336 and 0.423 V, respectively. In general, a higher  $V_{bi}$  value is seen to be more conducive for accelerating charge carrier transport, and improving  $V_{on}$  and  $J_{ph}$ .<sup>47</sup> To validate the enhanced performance of the PV-HS3 device, the quality of the P–N junction of PV-HS1, PV-HS2, and PV-HS3 devices was systematically investigated. Fig. 7c displays the dark  $J$ – $V$  curves of PV-HS1, PV-HS2 and PV-HS3 devices. The following equation was used to determine the  $A$  (diode ideality factor),  $G$  (shunt conductance),  $R$  (series resistance) and  $J_0$  (reverse-saturation current density):<sup>55</sup>

$$J = J_0 \exp\left[\frac{q}{AkT}(V - RJ)\right] + GV - J_L \quad (8)$$

The  $dJ/dV$  against  $V$  plot is depicted in Fig. 7d. The obtained  $G$  values of PV-HS1, PV-HS2, and PV-HS3 devices were 4.10, 2.24, and 0.51  $\text{mS cm}^{-2}$ , respectively. The devices' two parameters,  $A$

and  $R$ , were determined by comparing  $dV/dJ$  to  $(J + J_{sc})^{-1}$ , as shown in Fig. 7e. For the PV-HS1, PV-HS2, and PV-HS3 devices, the observed values of  $R$  were 10.0, 6.11, and 3.66  $\Omega \text{ cm}^2$ , respectively. The obtained  $R$  value for the PV-HS3 device was lower than that of PV-HS2, while the  $R$  value of PV-HS2 was lower than that of PV-HS1. Furthermore, the resulting  $A$  values for PV-HS1, PV-HS2 and PV-HS3 devices were 1.79, 1.55 and 1.14, respectively, inferring that the PV-HS3 device had less interface recombination. Plotting the  $\ln(J + J_{sc} - GV)$  vs.  $V - RJ$  yielded the  $J_0$  values of  $3.39 \times 10^{-3}$ ,  $2.36 \times 10^{-4}$  and  $1.42 \times 10^{-4} \text{ mA cm}^{-2}$  for the PV-HS1, PV-HS2, and PV-HS3 samples, respectively (Fig. 7f). The  $R$  and  $A$  values among the PV-HS1 device and dual back interface engineering treated devices, including PV-HS2 and PV-HS3 devices, suggested a drop in defect recombination at the interfaces and in bulk areas. Moreover, a reduced value of  $J_0$  was noted in the PV-HS3 device, demonstrating a decline in deep-level defect concentration and corresponding mitigation in nonradiative recombination loss.<sup>37</sup>

The D-HS1 device's  $\text{Mo/Sb}_2(\text{S,Se})_3$  interface barrier was further examined because the higher back contact barriers may have contributed to its inferior performance. The schematic band diagrams of D-HS1, D-HS2 and D-HS3 photocathodes are displayed in Fig. 7g–i. The UPS spectra of Mo,  $\text{MoO}_2$ , Au and  $\text{Sb}_2(\text{S,Se})_3$  thin films are displayed in Fig. S19a–d†. The magnified binding energy in the 7.4–6.8 eV region is shown as the inset figures in each graph (Fig. S19†). The barrier heights of  $\text{Mo/Sb}_2(\text{S,Se})_3$ ,  $\text{Mo/MoO}_2$ ,  $\text{MoO}_2/\text{Au}$  and  $\text{Au/Sb}_2(\text{S,Se})_3$  were 0.39, 0.21, 0.18 and 0.07 eV, respectively (Fig. 7g–i). The UPS analysis proves that, of the three devices, D-HS3 has the best performance and superior carrier collection efficiency since it has a lower barrier height compared to D-HS2 and D-HS1. Improved crystalline quality, crystal orientation, and the lowered barrier height all assisted in the boosted  $J_{ph}$  and higher HC-STH efficiency. The  $\text{Sb}_2(\text{S,Se})_3$  band gaps in D-HS1, D-HS2, and D-HS3 devices were 1.226, 1.227, and 1.231 eV, respectively (Fig. S10b†). The band gap of the  $\text{Sb}_2(\text{S,Se})_3$  absorber can possibly be altered by both  $\text{MoO}_2$  and Au underlayers. Overall, incorporating both the intermediate layer of  $\text{MoO}_2$  and carrier transport channel Au interface layers plays several functions, such as facilitating grain growth, achieving the preferred ( $hkl$ ) orientation of  $\text{Sb}_2(\text{S,Se})_3$ , increasing the minority carrier diffusion length, superior carrier collection and separation efficiency and decreasing the back contact barrier. These optimized parameters are certainly the primary factors contributing to the photocathode's elevated performance.

## 4. Conclusion

In summary, this work employed a dual back interface engineering approach by incorporating an intermediate layer of  $\text{MoO}_2$  and a secondary carrier transport channel of Au to strengthen the charge carrier dynamics in  $\text{Sb}_2(\text{S,Se})_3$  photocathodes. The synergistic assembly of dual back underlayers efficiently improved the crystal growth and the preferential orientation in the  $\text{Sb}_2(\text{S,Se})_3$  absorber layer by improving the Mo substrate's wettability. Additionally, back contact barrier height, and bulk and interface defects were significantly



suppressed, leading to inhibited charge carrier recombination loss. As a result, the synergy of MoO<sub>2</sub> and Au dual back interface layers produced a remarkable improvement in charge separation and transport efficiency, as well as lengthened minority carrier diffusion length and depletion width in Sb<sub>2</sub>(S,Se)<sub>3</sub> photocathodes. Therefore, comparing the untreated D-HS1 device and the D-HS3 photocathode with dual back interface engineering modification, the  $J_{ph}$  was enhanced from  $\sim 5.89$  mA cm<sup>-2</sup> to  $\sim 32.60$  mA cm<sup>-2</sup>,  $V_{on}$  improved from  $\sim 0.351$  V<sub>RHE</sub> to  $\sim 0.431$  V<sub>RHE</sub>, and HC-STH conversion efficiency significantly increased from  $\sim 0.30\%$  to  $\sim 3.58\%$ . This work offers great potential of interface engineering for the fabrication of highly efficient chalcogenide thin-film photocathodes.

## Data availability

The data supporting this article have been included as part of the ESI.†

## Author contributions

Hafiz Sartaj Aziz: data curation, investigation, methodology, conceptualization, writing – original draft. Tahir Imran: methodology, writing – original draft, investigation. Munir Ahmad: investigation, writing – original draft. Guo-Jie Chen: data curation, formal analysis. Ping Luo: data curation, investigation. Dong-Lou Ren: data curation, investigation. Bing-Suo Zou: data curation, investigation. Ju-Guang Hu: investigation, methodology. Zheng-Hua Su: visualization, validation. Pei-Guang Yan: supervision, visualization, validation. Guang-Xing Liang: conceptualization, supervision, visualization, validation writing – review & editing. Shuo Chen: conceptualization, formal analysis, writing – review & editing, supervision, funding acquisition.

## Conflicts of interest

There are no conflicts to declare.

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