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## Numerical optimization of $\text{Rb}_2\text{AuScBr}_6$ and $\text{Rb}_2\text{AuScCl}_6$ -based lead-free perovskite solar cells: device engineering and performance mapping

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Perovskite solar cells (PSCs) exhibit significant potential for next-generation photovoltaic technology, integrating high power conversion efficiency (PCE), cost-effectiveness, and tunable optoelectronic properties. This report presents a comprehensive numerical optimization of  $\text{Rb}_2\text{AuScBr}_6$  and  $\text{Rb}_2\text{AuScCl}_6$ -based PSCs, with particular emphasis on the influence of electron transport layers (ETLs) and critical device parameters. The configuration ITO/TiO<sub>2</sub>/Rb<sub>2</sub>AuScBr<sub>6</sub>/CBTS/Ni achieves a PCE of 27.49%, whereas the configuration ITO/WS<sub>2</sub>/Rb<sub>2</sub>AuScCl<sub>6</sub>/CBTS/Ni attains 22.41%, thereby underscoring the high efficiency of these lead-free materials. Device performance is markedly improved through increased perovskite layer thickness and reduced defect density. Further stabilization of performance is achieved by optimizing electron affinity, series resistance, and shunt resistance. Additionally, thermal stability is enhanced through the adjustment of operational temperature. The superior PCE observed in Rb<sub>2</sub>AuScBr<sub>6</sub> is ascribed to the selection of the ETL, an optimal band gap, absorber layer thickness, lower defect density, and appropriate contact interfaces. Overall, these Rb<sub>2</sub>AuScBr<sub>6</sub> and Rb<sub>2</sub>AuScCl<sub>6</sub> perovskites demonstrate exceptional promise for practical, efficient, and stable PSC applications, thereby encouraging further experimental validation and device engineering.

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### 1. Introduction

The growing global need for energy, fueled by rapid population growth and industrial development, has spurred a concerted search for sustainable and eco-friendly energy sources.<sup>1</sup> Among these, solar energy provides an ample, renewable resource that can be harnessed to overcome the constraints of fossil fuels in a cost-efficient manner.<sup>2</sup> With its unique characteristics and advantages, photovoltaic (PV) technology is a rather efficient method for converting sunlight into electricity, which presents low operation cost and less environmental pollution than other traditional energy generation methods.<sup>3</sup>

Perovskite materials have garnered widespread attention in recent years owing to their outstanding light-harvesting capabilities, tunable band gaps, and exceptional power conversion efficiencies (PCEs).<sup>4</sup> Within this family, double perovskites—typically denoted  $\text{A}_2\text{BB}'\text{X}_6$  ( $\text{X}$  = halide)—offer a particularly promising avenue.<sup>5</sup> Unlike traditional single-cation  $\text{ABX}_3$  perovskites, their expanded B-site cation combinations facilitate precise tuning of

electronic structures and band gaps. This flexibility enables the creation of lead-free, environmentally benign alternatives with band gaps better matched to the solar spectrum.<sup>6,7</sup>

One notable candidate,  $\text{Cs}_2\text{AgBiBr}_6$ , exhibits a large but stable indirect band gap of around 2.2 eV. Treating conventional perovskites with  $\text{Cs}_2\text{AgBiBr}_6$  nanoparticles has yielded enhanced stability and an impressive PCE of 19.52%, underscoring the advantage of its passivation capabilities.<sup>8</sup> Through compositional engineering, this band gap can be further tuned: Tl-doping narrows it to 1.57 eV, while Sb-for-Bi substitution reaches 1.86 eV, improving absorption and photovoltaic potential.<sup>9</sup>

Similarly,  $\text{Cs}_2\text{AgInBr}_6$  has been explored using first-principles and optical studies, revealing a direct band gap of approximately 1.427 eV and excellent absorption ( $>10^4 \text{ cm}^{-1}$ ), positioning it as a viable PV absorber.<sup>10</sup> Another intriguing family,  $\text{A}_2\text{AgIrCl}_6$  ( $\text{A}$  = Cs, Rb, K), displays direct band gaps of about 1.43–1.55 eV ( $\text{Cs}_2 = 1.43 \text{ eV}$ ;  $\text{Rb}_2 = 1.50 \text{ eV}$ ;  $\text{K}_2 = 1.55 \text{ eV}$ ), alongside low effective electron masses and strong visible-light absorption, making them highly promising for solar cell applications.<sup>11</sup>

A different strategy involves alloying: in  $\text{Cs}_2\text{Ag}(\text{Sb}_x\text{Bi}_{1-x})\text{Br}_6$ , band gaps reduce below those of the pure end members down to about 2.08 eV when  $x = 0.9$ , thanks to band-gap bowing from Sb–Bi orbital mixing.<sup>12</sup> Additional studies have explored  $\text{Cs}_2\text{AgBiBr}_6$  doped with aluminum: the pristine material shows  $E_g$

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$\approx 1.91$  eV, whereas Al-doped films exhibit a slightly lowered  $E_g$  of 1.82 eV, resulting in improved device metrics (PCE from  $\sim 3.02\%$  to  $\sim 3.40\%$ ).<sup>13</sup> Another notable double perovskite,  $\text{Cs}_2\text{CuBiCl}_6$ , has emerged *via* SCAPS-1D simulation as a lead-free absorber with high predicted efficiencies; optimized devices yielded PCE up to 24.51%,  $V_{oc} = 1.73$  V, and  $J_{sc} = 32.82$  mA  $\text{cm}^{-2}$ .<sup>14</sup> These theoretical models affirm the material's considerable promise for durable, high-performance photovoltaics.

Collectively, these studies underscore the diverse strategies available—doping, substitution, alloying, and novel compounds—to engineer double perovskites with direct, suitably low band gaps (spanning  $\sim 1.4$  to 2.2 eV). Realizing these tunable properties positions them as key materials for next-generation, lead-free, high-efficiency solar technologies, potentially even surpassing conventional limits.<sup>15</sup> Several electron transport layers (ETLs) have been explored to improve the performance of perovskite solar cells (PSCs).  $\text{WS}_2$ , a transition metal dichalcogenide, offers suitable conduction band alignment and decent electron mobility, enhancing power conversion efficiency (PCE).<sup>16</sup>  $\text{ZnO}$ , with its wide band gap ( $\sim 3.3$  eV), high electron mobility, and transparency, is attractive, though interfacial reactions with perovskites may cause stability issues requiring surface modification.<sup>17</sup> PCBM, a fullerene derivative, is widely used for its strong electron-accepting ability and reduced recombination losses.<sup>18</sup>  $\text{TiO}_2$  is the most common ETL due to its band alignment, chemical stability, and transparency, but its low electron mobility and recombination tendencies necessitate surface treatments or doping.<sup>19</sup> IGZO, with high electron mobility and optical transparency, and  $\text{C}_{60}$ , with strong electron transport properties, are also promising ETLs.<sup>20,21</sup>

For hole transport layers (HTLs), CBTS has demonstrated strong potential owing to its favorable energy level alignment and ability to enhance hole extraction and stability.<sup>22</sup> Other candidates include  $\text{CdTe}$ ,  $\text{CuI}$ , PTAA, P3HT, and PEDOT:PSS, each offering distinct advantages such as high hole mobility, thermal stability, or compatibility with perovskite layers, though limitations like poor conductivity or stability often require doping or modification.<sup>23–27</sup>

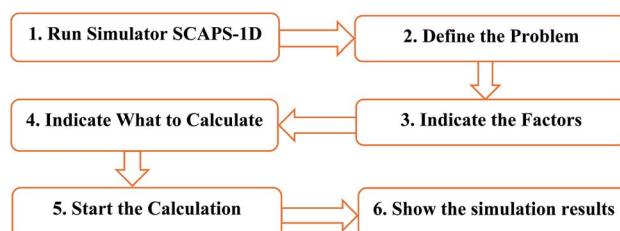
In this work, we present the simulation and optimization of lead-free double perovskite solar cells based on  $\text{Rb}_2\text{AuScBr}_6$  and  $\text{Rb}_2\text{AuScCl}_2$  absorbers. Using SCAPS-1D, we systematically investigate n-i-p planar heterojunction structures with various ETLs (IGZO,  $\text{WS}_2$ ,  $\text{ZnO}$ , PCBM,  $\text{C}_{60}$ , and  $\text{TiO}_2$ ) and HTLs (CBTS,  $\text{CdTe}$ ,  $\text{CuI}$ , PTAA, P3HT, and PEDOT:PSS). Among the HTLs, CBTS demonstrates superior performance for both absorbers. Device parameters such as absorber thickness, defect density, resistances, and operating temperature are tuned to optimize photovoltaic performance. The results indicate that these double perovskite materials hold great promise for high-efficiency, environmentally friendly PSCs, contributing to the development of next-generation renewable energy technologies.<sup>28–31</sup>

## 2. Methodology

The numerical studies of this work were performed using the Solar Cell Capacitance Simulator (SCAPS-1D), the widely used one-dimensional solar cell simulation tool developed at the University

of Ghent, Belgium. Data analysis of a wide range of photovoltaic device parameters, such as energy band alignment, charge transport mechanisms, recombination losses, and current–voltage ( $I$ – $V$ ) characteristics, can be performed through SCAPS-1D.<sup>32</sup>

The simulation process adheres to the usual operating routine of SCAPS-1D as follows:<sup>33</sup>



The SCAPS-1D simulator is built upon three key semiconductor equations: Poisson's equation, the electron continuity equation, and the hole continuity equation. These equations define how electric potential and charge carriers (electrons and holes) behave and distribute within a semiconductor device. SCAPS-1D numerically solves these equations to model the internal physics of solar cells and predict their performance. Poisson's equation is given as:<sup>34–36</sup>

$$\frac{\partial}{\partial x} \left( \epsilon(x) \frac{\partial \psi}{\partial x} \right) = \frac{-q}{\epsilon_0} \left[ p - n + N_D^+ - N_A^- + \frac{\rho_{\text{def}}(n, p)}{q} \right] \quad (1)$$

Here,  $\psi$  (psi) is the electric potential,  $\epsilon$  (epsilon) is the material's ability to store electric charge (called the dielectric constant),  $q$  is the charge of an electron, and  $\rho$  (def) is the charge from defects inside the material.

Eqn (2) and (3) are used to show how free electrons and free holes are conserved or balanced inside the solar cell device.

$$\frac{\partial p}{\partial t} = \frac{1}{q} \frac{\partial J_p}{\partial x} + (G_p - R_p) \quad (2)$$

$$\frac{\partial n}{\partial t} = \frac{1}{q} \frac{\partial J_n}{\partial x} + (G_n - R_n) \quad (3)$$

Here,  $\frac{\partial p}{\partial t}$  is the rate of change of hole concentration  $p$  with time,  $q$  is the charge of an electron or hole,  $\frac{\partial J_p}{\partial x}$  is the change of hole current density  $J_p$  over distance  $x$ ,  $G_p$  is the hole generation rate,  $R_p$  is the hole recombination rate,  $\frac{\partial n}{\partial t}$  is the rate of change of electron concentration,  $\frac{\partial J_n}{\partial x}$  is the change of electron current density  $J_n$  over distance  $x$ ,  $G_n$  is the electron generation rate and  $R_n$  is the electron recombination rate.

Eqn (4) and (5) are used to calculate the drift current and the diffusion current.

$$J_n = q\mu_n n e + qD_n \delta n \quad (4)$$

$$J_p = q\mu_p n e - qD_p \delta p \quad (5)$$

where  $\mu_n$  is the mobility of electrons,  $\mu_p$  is the mobility of holes and the diffusion coefficient ( $D_n$  for electrons,  $D_p$  for holes) shows how fast they spread out from high to low concentration.



### 3. Results & discussion

The design configuration of the  $\text{Rb}_2\text{AuScBr}_6$ - and  $\text{Rb}_2\text{AuScCl}_6$ -based perovskite solar cell (PSC) follows an n-i-p planar heterojunction structure (Fig. 1), where the ETL is in the n-region, the perovskite absorber layer in the i-region, and the HTL in the p-region. When exposed to sunlight, excitons (electron–hole pairs) are generated within the perovskite layer.<sup>37,38</sup> The built-in electric field at the interfaces aids in exciton dissociation, directing electrons toward the n-layer and holes toward the p-layer for efficient charge extraction.<sup>39</sup> Indium-doped tin oxide (ITO) is used as the transparent conductive front contact. Different ETL materials, including IGZO,  $\text{WS}_2$ ,  $\text{ZnO}$ , PCBM,  $\text{C}_{60}$ , and  $\text{TiO}_2$ , are investigated to optimize electron transport. The  $\text{Rb}_2\text{AuScCl}_6$  and  $\text{Rb}_2\text{AuScBr}_6$  perovskites serve as the absorber layer, enabling efficient light absorption. Among 36 different ETL–HTL combinations, CBTS is selected as the HTL due to its superior hole transport properties and compatibility with the absorber. The Ni completes the device structure and collects the extracted charges.

Simulations were performed under AM1.5 G solar spectrum conditions to analyze the impact of different ETL and HTL combinations, aiming to determine the most efficient structure. The study explores lead-free, stable perovskite materials as potential candidates for environmentally friendly and high-performance solar cells.

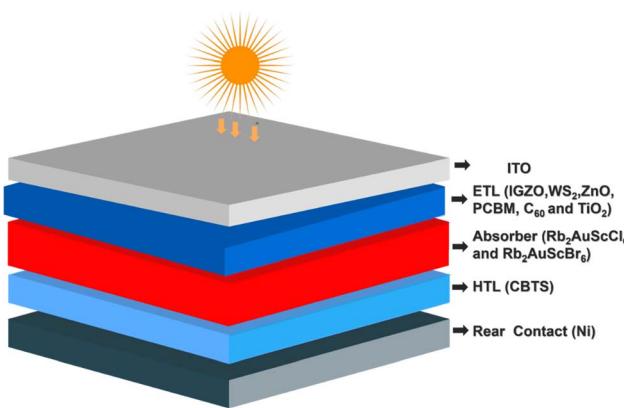


Fig. 1 The design configuration of the  $\text{Rb}_2\text{AuScCl}_6$  and  $\text{Rb}_2\text{AuScBr}_6$ -based PSC.

Table 1 Input parameters of HTLs<sup>42</sup>

Parameters	CBTS	CdTe	P3HT	PEDOT : PSS	PTAA	CuI
$t$ (nm)	100	200	50	50	150	100
$E_g$ (eV)	1.9	1.5	1.7	1.6	2.96	3.1
$X$ (eV)	3.6	3.9	3.5	3.4	2.3	2.1
$E_r$	5.4	9.4	3	3	9	6.5
$N_C$ (cm <sup>-3</sup> )	$2.2 \times 10^{18}$	$8 \times 10^{17}$	$2.0 \times 10^{21}$	$2.2 \times 10^{18}$	$2.0 \times 10^{21}$	$2.8 \times 10^{19}$
$N_V$ (cm <sup>-3</sup> )	$1.8 \times 10^{19}$	$1.8 \times 10^{19}$	$2.0 \times 10^{21}$	$1.8 \times 10^{19}$	$2.0 \times 10^{21}$	$1 \times 10^{19}$
$\mu_e$ (cm <sup>2</sup> V <sup>-1</sup> s <sup>-1</sup> )	30	$3.2 \times 10^2$	$1.8 \times 10^{-3}$	$4.5 \times 10^{-2}$	1	100
$\mu_h$ (cm <sup>2</sup> V <sup>-1</sup> s <sup>-1</sup> )	10	$4 \times 10^1$	$1.86 \times 10^{-2}$	$4.5 \times 10^{-2}$	40	43.9
$N_D$ (cm <sup>-3</sup> )	0	0	0	0	0	0
$N_A$ (cm <sup>-3</sup> )	$10^{18}$	$2.0 \times 10^{14}$	$10^{18}$	$10^{18}$	$10^{18}$	$10^{18}$
$N_t$ (cm <sup>-3</sup> )	$10^{15}$	$10^{15}$	$10^{15}$	$10^{15}$	$10^{15}$	$10^{15}$

To determine the input parameters required for the equations mentioned above, the following calculation procedures are employed, with all relevant values detailed in Tables 1–3. Eqn (6) defines the carrier's effective mass  $m^*$  in terms of the curvature of the energy–momentum relation:<sup>40</sup>

$$m^* = \frac{\hbar^2}{(d^2E/dK^2)} \quad (6)$$

where  $\hbar$  is the reduced Planck constant ( $1.05 \times 10^{-34}$  J s<sup>-1</sup>) and  $d^2E/dK^2$  is the second derivative of the band energy  $E$  with respect to the wavevector  $k$ .

Eqn (7) and (8) then use these effective masses to compute the effective density of states in the valence band ( $N_v$ ) and conduction band ( $N_c$ ), respectively, at temperature  $T$ :

$$N_v = 2 \frac{(2\pi m_h^* K_B T)^{3/2}}{\hbar^3} \approx 2.5409 \times 10^{19} \left( \frac{m_h^*}{m_0} \right)^{3/2} \quad (7)$$

$$N_c = 2 \frac{(2\pi m_e^* K_B T)^{3/2}}{\hbar^3} \approx 2.5409 \times 10^{19} \left( \frac{m_e^*}{m_0} \right)^{3/2} \quad (8)$$

where  $K_B$  is Boltzmann's constant,  $\hbar$  is Planck's constant, and  $m_h^*$  and  $m_e^*$  are the hole and electron effective masses. Eqn (9) and (10) relate the carrier mobilities  $\mu_e$  (electron mobility) and  $\mu_h$  (hole mobility) to the carrier charge  $q$ , the relaxation time  $\tau$ , and the respective effective masses:<sup>41</sup>

$$\mu_e = \frac{q\tau}{m_e} \quad (9)$$

$$\mu_h = \frac{q\tau}{m_h} \quad (10)$$

#### 3.1. Absorber material parameters and band alignment of $\text{Rb}_2\text{AuScBr}_6$ and $\text{Rb}_2\text{AuScCl}_6$ -based absorbers with different ETLs and HTLs

The electronic and optical suitability of  $\text{Rb}_2\text{AuScBr}_6$  and  $\text{Rb}_2\text{AuScCl}_6$  as absorber materials has been theoretically validated through density functional theory (DFT) calculations. DFT results confirm indirect band gaps of 1.71 eV and 1.93 eV,<sup>45</sup> respectively, within the optimal photovoltaic range (1.4–2.2 eV), with high absorption coefficients ( $\approx 10^6$  cm<sup>-1</sup>) and low reflectivity (<15%), indicating their potential as efficient light-absorbing semiconductors.

Table 2 Input parameters of ETLs<sup>43</sup>

Parameters	WS <sub>2</sub>	ZnO	TiO <sub>2</sub>	PCBM	IGZO	C <sub>60</sub>
<i>t</i> (nm)	100	50	30	50	30	50
<i>E<sub>g</sub></i> (eV)	1.8	3.3	3.2	2	3.05	1.7
<i>X</i> (eV)	3.95	4	4	3.9	4.16	3.9
<i>E<sub>r</sub></i>	13.6	9.00	9	3.9	10	4.2
<i>N<sub>C</sub></i> (cm <sup>-3</sup> )	$1 \times 10^{18}$	$3.7 \times 10^{18}$	$2.0 \times 10^{18}$	$2.5 \times 10^{21}$	$5 \times 10^{18}$	$8 \times 10^{19}$
<i>N<sub>V</sub></i> (cm <sup>-3</sup> )	$2.4 \times 10^{19}$	$1.8 \times 10^{19}$	$1.8 \times 10^{19}$	$2.5 \times 10^{21}$	$5 \times 10^{18}$	$8 \times 10^{19}$
$\mu_e$ (cm <sup>2</sup> V <sup>-1</sup> s <sup>-1</sup> )	100	100	20	0.2	15	$8 \times 10^{-2}$
$\mu_h$ (cm <sup>2</sup> V <sup>-1</sup> s <sup>-1</sup> )	100	250	10	0.2	0.1	$3.5 \times 10^{-3}$
<i>N<sub>D</sub></i> (cm <sup>-3</sup> )	$10^{18}$	$10^{18}$	$9 \times 10^{16}$	$2.93 \times 10^{17}$	$10^{17}$	$10^{17}$
<i>N<sub>A</sub></i> (cm <sup>-3</sup> )	0	0	0	0	0	0
<i>N<sub>t</sub></i> (cm <sup>-3</sup> )	$10^{15}$	$10^{15}$	$10^{15}$	$10^{15}$	$10^{15}$	$10^{15}$

Table 3 Input parameters of Front contact (ITO) and Absorber Rb<sub>2</sub>AuScCl<sub>6</sub> and Rb<sub>2</sub>AuScBr<sub>6</sub> for initial optimization<sup>44</sup> <sup>a</sup>

Parameters	ITO	Rb <sub>2</sub> AuScBr <sub>6</sub>	Rb <sub>2</sub> AuScCl <sub>6</sub>
<i>t</i> (nm)	500	1200	1200
<i>E<sub>g</sub></i> (eV)	3.5	1.71	1.93
<i>X</i> (eV)	4	3.95	3.75
<i>E<sub>r</sub></i>	9	6.34	6.01
<i>N<sub>C</sub></i> (cm <sup>-3</sup> )	$2.2 \times 10^{18}$	$1.33 \times 10^{18}$	$1.94 \times 10^{18}$
<i>N<sub>V</sub></i> (cm <sup>-3</sup> )	$1.8 \times 10^{19}$	$4.56 \times 10^{18}$	$4.59 \times 10^{18}$
$\mu_e$ (cm <sup>2</sup> V <sup>-1</sup> s <sup>-1</sup> )	20	83.20	64.71
$\mu_h$ (cm <sup>2</sup> V <sup>-1</sup> s <sup>-1</sup> )	10	43.14	36.40
<i>N<sub>D</sub></i> (cm <sup>-3</sup> )	$10^{21}$	0	0
<i>N<sub>A</sub></i> (cm <sup>-3</sup> )	0	$10^{15}$	$10^{15}$
<i>N<sub>t</sub></i> (cm <sup>-3</sup> )	$10^{15}$	$10^{15}$	$10^{15}$

<sup>a</sup> [*t* = thickness, *X* = electron affinity, *E<sub>r</sub>* = dielectric relative permittivity, *N<sub>C</sub>* and *N<sub>V</sub>* = effective density of states in the conduction band and valence band,  $\mu_e$  and  $\mu_h$  = electron mobility and hole mobility, and *N<sub>D</sub>*, *N<sub>A</sub>*, and *N<sub>t</sub>* = donor, acceptor, and defect density in Tables (1–3)].

Fig. 2(a) illustrates the band alignment of the Rb<sub>2</sub>AuScBr<sub>6</sub> absorber with various ETLs and HTLs. The energy band offsets at these interfaces are critical for efficient charge carrier separation and transport, directly influencing solar cell performance. To explore the dynamics of charge carriers, the conduction band minimum (CB), valence band maximum (VB), and quasi-Fermi levels for electrons (*F<sub>n</sub>*) and holes (*F<sub>p</sub>*) are analyzed. Rb<sub>2</sub>AuScBr<sub>6</sub> has a conduction band at 1.47574 eV, a valence band at -0.23426 eV, and a bandgap (*E<sub>g</sub>*) of 1.71 eV, which favors photon absorption and contributes to better overall power conversion efficiency (PCE). Among the ETLs, TiO<sub>2</sub> and ZnO exhibit closely matched conduction band levels (-3.11 eV and -3.26 eV), allowing comparable electron injection capabilities.

WS<sub>2</sub> (-1.78 eV) and PCBM (-1.74 eV) also demonstrate suitable alignments, making them promising ETL alternatives. IGZO (-2.94 eV) and C<sub>60</sub> (-1.49 eV) offer diverse work functions and conduction band offsets, introducing flexibility for device tuning.

On the HTL side, CBTS (conduction band edge ~0.15 eV) aligns effectively with the absorber, promoting smooth hole extraction. Other HTLs such as P3HT (0.45 eV), CdTe (0.25 eV), CuI (0.45 eV), PEDOT:PSS (0.65 eV), and PTAA (0.39 eV) exhibit

various energy level alignments, influencing hole extraction efficiency. CuI and PTAA, in particular, have high valence band energies (3.55 eV and 3.35 eV, respectively), favoring hole mobility. Nickel (Ni), with a work function of 5.5 eV, ensures efficient hole collection by aligning well with these HTLs, reducing recombination at the back contact.

Fig. 2(b) shows the band alignment of the Rb<sub>2</sub>AuScCl<sub>6</sub> absorber with the same ETLs and HTLs. While the alignment is generally analogous to the Rb<sub>2</sub>AuScBr<sub>6</sub> system, subtle differences are observed in the energy levels, which slightly alter charge transport. Rb<sub>2</sub>AuScCl<sub>6</sub> has a conduction band at 1.67588 eV, a valence band at -0.25412 eV, and a larger bandgap of 1.93 eV. Due to the wider bandgap, Rb<sub>2</sub>AuScCl<sub>6</sub> tends to absorb fewer photons in the solar spectrum, which can reduce current generation and thus lower the overall PCE compared to its Br-based counterpart.<sup>46–48</sup>

### 3.2. Optimization of the HTL layer and the ETL layer

The selection of optimal ETL and HTL materials for the Rb<sub>2</sub>AuScBr<sub>6</sub>- and Rb<sub>2</sub>AuScCl<sub>6</sub>-based perovskite solar cells was guided by both photovoltaic performance parameters (PCE, *V<sub>oc</sub>*, *J<sub>sc</sub>*, and FF) and key physical considerations, including energy-band alignment, carrier mobility, defect density, material stability, and interfacial charge-transport behavior. Efficient charge extraction requires precise band matching, wherein the conduction band of the ETL lies slightly below that of the absorber to facilitate electron transfer while suppressing hole leakage, and the valence band of the HTL aligns closely with that of the absorber to enable rapid hole transport. Such optimized alignment minimizes interfacial barriers and recombination losses, thereby enhancing *V<sub>oc</sub>*, *J<sub>sc</sub>*, and FF. Secondary selection criteria included high carrier mobility, low trap density, and strong chemical and thermal stability to ensure robust and loss-free charge transport pathways. Among the investigated materials, IGZO and WS<sub>2</sub> emerged as the most effective ETLs due to their high electron mobility, low defect density, and superior environmental stability, while CBTS proved to be an excellent HTL owing to its favorable energy-level alignment, high hole mobility, and long-term durability. Furthermore, optimized acceptor doping in the absorber enhanced the internal electric field, promoting efficient charge separation and reducing recombination. The IGZO/CBTS



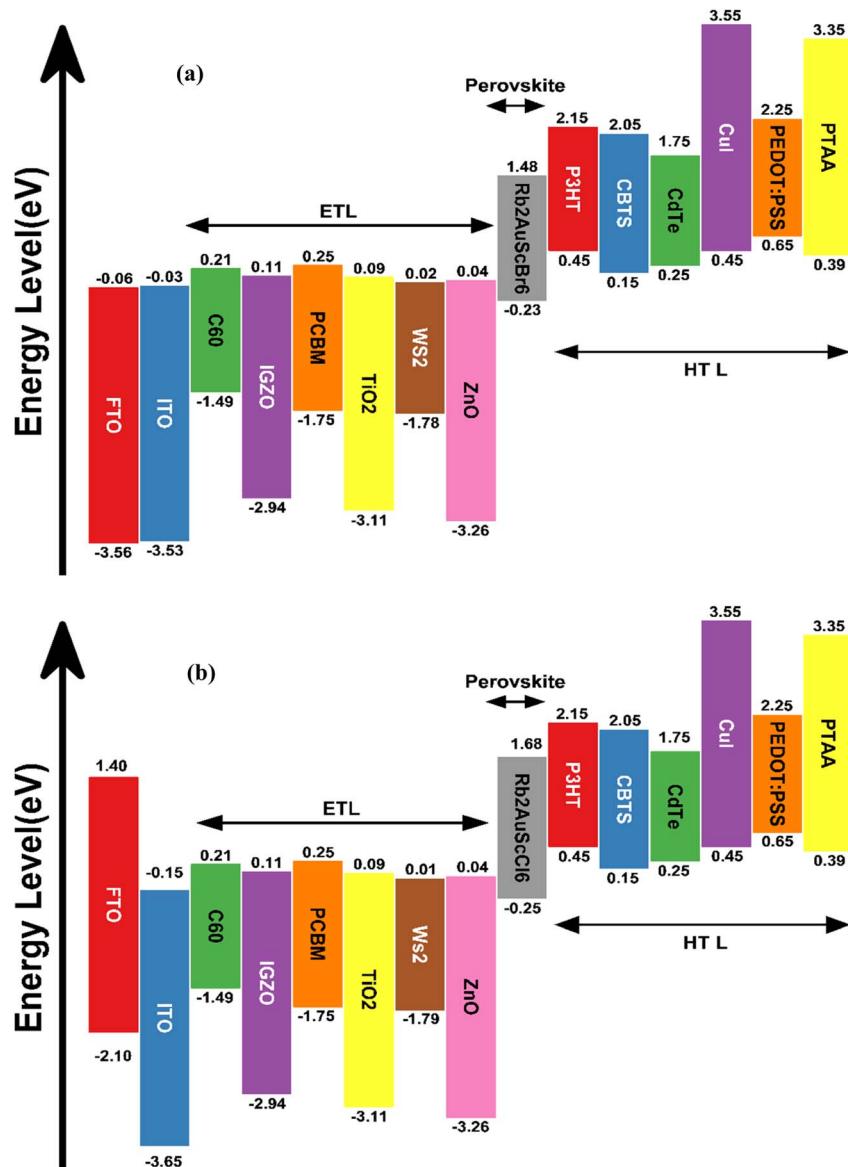


Fig. 2 Energy band alignment between the different ETL and HTL materials of (a) Rb<sub>2</sub>AuScBr<sub>6</sub> absorber and (b) Rb<sub>2</sub>AuScCl<sub>6</sub> absorber.

combination for the Rb<sub>2</sub>AuScBr<sub>6</sub> device and the WS<sub>2</sub>/CBTS combination for the Rb<sub>2</sub>AuScCl<sub>6</sub> device provided the most favorable band alignment and carrier extraction pathways, leading to the highest PCEs.

The variations in efficiency among different ETL/HTL configurations can be primarily attributed to differences in interfacial recombination, which were modeled through interface defect densities ( $N_t = 10^{15} \text{ cm}^{-3}$ ). These optimized configurations exhibited lower recombination losses owing to improved interfacial quality and energetically well-matched interfaces.

**3.2.1. Selection of ETL and HTL for Rb<sub>2</sub>AuScBr<sub>6</sub>-based solar cells.** Fig. 3(a) shows that using WS<sub>2</sub> as ETL and CBTs as HTL results in a PCE of 23.68%, with an open-circuit voltage ( $V_{oc}$ ) of 1.258 V, short-circuit current density ( $J_{sc}$ ) of 21.433 mA  $\text{cm}^{-2}$ , and fill factor (FF) of 87.85%. WS<sub>2</sub>, a two-dimensional

transition metal dichalcogenide, exhibits high electron mobility and favorable energy level alignment with the perovskite absorber, enabling efficient electron extraction. This combination maintains stable charge transport and hinders recombination, leading to high efficiency. However, the lower  $V_{oc}$  and FF than that of IGZO translate to slightly lower PCE. Fig. 3(b) depicts that using ZnO as the ETL and CBTs as the HTL lead to PCE 23.65% ( $V_{oc} = 1.257 \text{ V}$ ,  $J_{sc} = 21.414 \text{ mA cm}^{-2}$ , FF = 87.83%). ZnO is a common ETL with high electron transport properties, but its electron mobility being lower than IGZO and WS<sub>2</sub>, makes its efficiency take a hit. Even though ZnO has good performance, its interface properties and energy level alignment are not as good as IGZO, resulting in a relatively low PCE. In Fig. 3(c) achieves 23.57% PCE is achieved with  $V_{oc} = 1.256 \text{ V}$ ,  $J_{sc} = 21.378 \text{ mA cm}^{-2}$ , and FF = 87.80% with a combination of PCBM ETL and CBTs HTL. A well-known electron acceptor,



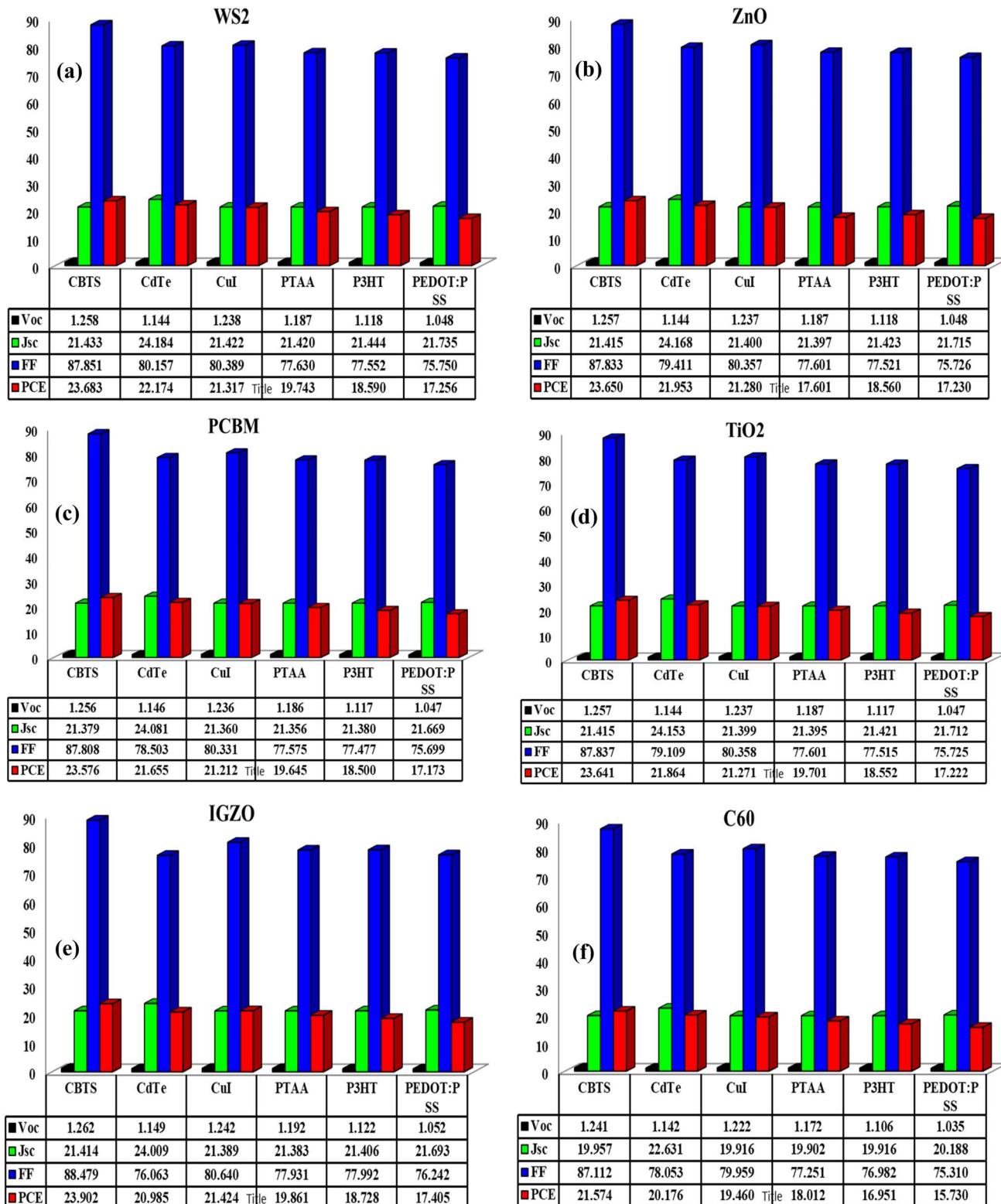


Fig. 3 HTL & ETL selection for  $\text{Rb}_2\text{AuScBr}_6$  of (a) WS<sub>2</sub> (b) ZnO (c) PCBM, (d) TiO<sub>2</sub>, (e) IGZO and (f) C<sub>60</sub> with HTL of CBTS, CdTe, CuI, PTAA, P3HT and PEDOT:PSS.

PCBM, has much lower electron mobility than IGZO, WS<sub>2</sub>, and ZnO, resulting in lower efficiency. Although the fill factor is indeed high, the reduced electron mobility results in a mild

drop of the charge collection efficiency, which ends up decreasing the PCE. Fig. 3(d) demonstrates TiO<sub>2</sub> as ETL and CBTS as HTL yields a PCE of 23.64% ( $V_{\text{oc}} = 1.257 \text{ V}$ ,  $J_{\text{sc}} = 21.415$

mA cm<sup>-2</sup>, and FF = 87.83%). TiO<sub>2</sub> is known to have great electron transport properties and high stability, which makes it a widespread choice for ETL. Nevertheless, due to its low conductivity and moderate energy level alignment, its efficiency is slightly lower than that obtained with WS<sub>2</sub> and IGZO. TiO<sub>2</sub> is not considered the most optimal in terms of charge transport properties, even though it is widely used. Fig. 3(e) shows that the best performance of 23.90% PCE achieved with IGZO ETL and CBTS HTL,  $V_{oc} = 1.262$  V,  $J_{sc} = 21.414$  mA cm<sup>-2</sup>, and FF = 88.48%. IGZO possesses good electron transport properties, thanks to its high electron mobility, which allows for rapid extraction of charge. Also, its low trap density minimizes recombination losses, which leads to better performance. As an HTL, the CBTS offers excellent stability and improved hole transport. The synergy between IGZO ETL and CBTS HTL results in a low recombination with high charge transport, providing the best photovoltaic efficiency with the total highest PCE in all tested combinations. Fig. 3(f) demonstrates that C<sub>60</sub> as ETL with CBTS as HTL provide the lowest PCE of 21.57% ( $V_{oc} = 1.240$  V,  $J_{sc} = 19.957$  mA cm<sup>-2</sup>, and FF = 87.11%). C<sub>60</sub> has reasonable electron transport, but its higher electron mobility than other ETLs leads to the lowest efficiency. While the CBTS is still effective as an HTL, the overall device performance is limited by the reduced electron extraction efficiency of C<sub>60</sub>. IGZO ETL + CBTS HTL has the highest PCE among all combinations, exceeding 23.90% in the most optimum conditions, thus qualifying as the best performing pair. Thus, the high electron mobility, excellent energy-level alignment and chemical stability of IGZO lead to superior electron extraction, while CBTS provides efficient hole collection with minimal recombination losses. This combination optimizes both charge separation as well as charge transport, yielding the highest overall efficiency.<sup>49,50</sup>

**3.2.2. Selection of ETL and HTL for Rb<sub>2</sub>AuScCl<sub>6</sub>-based solar cells.** Fig. 4(a) depicts the optimal performance of 20.99% PCE of WS<sub>2</sub> ETL/CBTS HTL is obtained with  $V_{oc}$ ,  $J_{sc}$ , FF of 1.447 V, 16.289 mA cm<sup>-2</sup>, and 89.04% respectively. The high electron mobility of WS<sub>2</sub>, together with good alignment of its energy levels with the perovskite material, gives better electron extraction than TiO<sub>2</sub> and ZnO. These also match well with CBTS, which provides ideal hole transport; thus, the pair yields the highest PCE attributed to ideal transport properties of both electrons and holes, resulting in minimized recombination and maximized efficiency during transport. Fig. 4(b) illustrates that when use ZnO as ETL with CBTS as HTL (PCE = 20.21%  $V_{oc} = 1.451$  V, 15.659 mA cm<sup>-2</sup>, 88.92% FF). Though ZnO has excellent electron transport layer properties, its performance is slightly less favorable than WS<sub>2</sub> due to slight differences in the energy level alignment and a lower electron mobility than WS<sub>2</sub>, yielding a slightly lower PCE. Fig. 4(c) shows PCE reaches 19.68% with this structure obtained by ETL of PCBM and HTL of CBTS, while showing  $V_{oc}$  of 1.401 V,  $J_{sc}$  of 15.634 mA cm<sup>-2</sup> and FF of 89.84%. While PCBM is known to be a good electron acceptor, the relatively lower mobility of electrons compared to WS<sub>2</sub> and ZnO results in a slight decrease in PCE value. Assure that the fill factor is high, the net efficiency is reduced by a factor of lower electron mobility. While the configuration of

TiO<sub>2</sub> ETL and CBTS HTL enables a PCE of 20.33% ( $V_{oc} = 1.452$  V,  $J_{sc} = 15.659$  mA cm<sup>-2</sup>, and FF = 89.41%) (Fig. 4(d)). This arrangement strikes a good trade-off between the extraction of electrons and collection of holes, and thus their resulting performance is moderate, whereas the material characteristics of TiO<sub>2</sub> do not allow for the most optimal conversion efficiency. In Fig. 4(e) achieves PCE of 19.04% with  $V_{oc}$ ,  $J_{sc}$ , FF of 1.416 V, 15.657 mA cm<sup>-2</sup>, 85.85% respectively using IGZO as ETL and CBTS as HTL combination. IGZO possesses high electron mobility yet is somewhat less efficient than WS<sub>2</sub> and ZnO, which is likely a result of interface effects and energy level mismatches with the perovskite layer. This means that despite IGZO's electron mobility, the performance is not as good. Fig. 4(f) depicts the composition of C<sub>60</sub> ETL and CBTS HTL gives the lowest PCE of 16.51%, with  $V_{oc}$  of 1.266 V,  $J_{sc}$  of 14.888 mA cm<sup>-2</sup>, and FF of 87.61%. While C<sub>60</sub> offers decent electron transport, its lower electron mobility compared to the other ETLs results in the overall lowest device efficiency. CBTS is efficient as the HTL, but its reduced electron mobility hampers performance.<sup>51</sup>

### 3.3. Role of absorber thickness and ETL thickness on solar cell performance

Fig. 5 demonstrates a series of contour plots showing the PCE of perovskite solar cells. We are testing various materials as the ETL, while using Rb<sub>2</sub>AuScBr<sub>6</sub> as the perovskite absorber material. Each sub-figure (a-f) represents a different ETL configuration.

Fig. 5(a) shows the PCE achieved is around 21.80% when C<sub>60</sub> is used as the ETL. The contour lines indicate how the PCE changes with varying thicknesses of both the absorber and the C<sub>60</sub> ETL. Fig. 5(b) demonstrates that using Indium Gallium Zinc Oxide (IGZO) as the ETL results in the highest PCE of 24.07%. The contour lines are more spread out compared to C<sub>60</sub>, suggesting a wider range of thicknesses for both the absorber and IGZO that yield high efficiency. This indicates that the performance is less sensitive to small variations in the thicknesses. Fig. 5(c) illustrates the use of PCBM as the ETL, achieving a peak PCE of approximately 23.80%. The optimal performance region appears to be in the lower left corner, implying that thinner layers of both the absorber and PCBM are generally preferred for maximizing efficiency in this configuration. Fig. 5(d) shows that using WS<sub>2</sub> is the ETL reaches PCE is approximately 23.91%. Similar to PCBM, the optimal performance seems to be achieved with thinner layers, as indicated by the concentration of contour lines in the lower-left region. From Fig. 5(a-d) the highest PCE of absorber thicknesses is  $\geq 1200$  nm and ETL thicknesses are  $\leq 50$  nm. Fig. 5(e) employs titanium dioxide (TiO<sub>2</sub>) as the ETL and achieves a comparable peak PCE of approximately 23.87%, where the optimal condition is observed at absorber thicknesses  $\geq 1200$  nm and an ETL thickness precisely at 200 nm. The contour lines are closely packed, suggesting a narrow region of high efficiency. This implies that the performance is quite sensitive to the thicknesses of both the absorber and TiO<sub>2</sub>, and precise control is crucial. Fig. 5(f) demonstrates that Zinc Oxide (ZnO) is the ETL, and peak PCE is about 23.88%. Where absorber thicknesses are  $\geq 1200$  nm and



ETL thicknesses are 450 nm. Like  $\text{TiO}_2$ , the contour plot indicates a narrow region of high efficiency and thus sensitivity to thickness variations.

The superior PCE of IGZO is mainly attributed to its favorable energy band alignment with the  $\text{Rb}_2\text{AuScBr}_6$  absorber, which enables electron extraction and prevents the leakage of

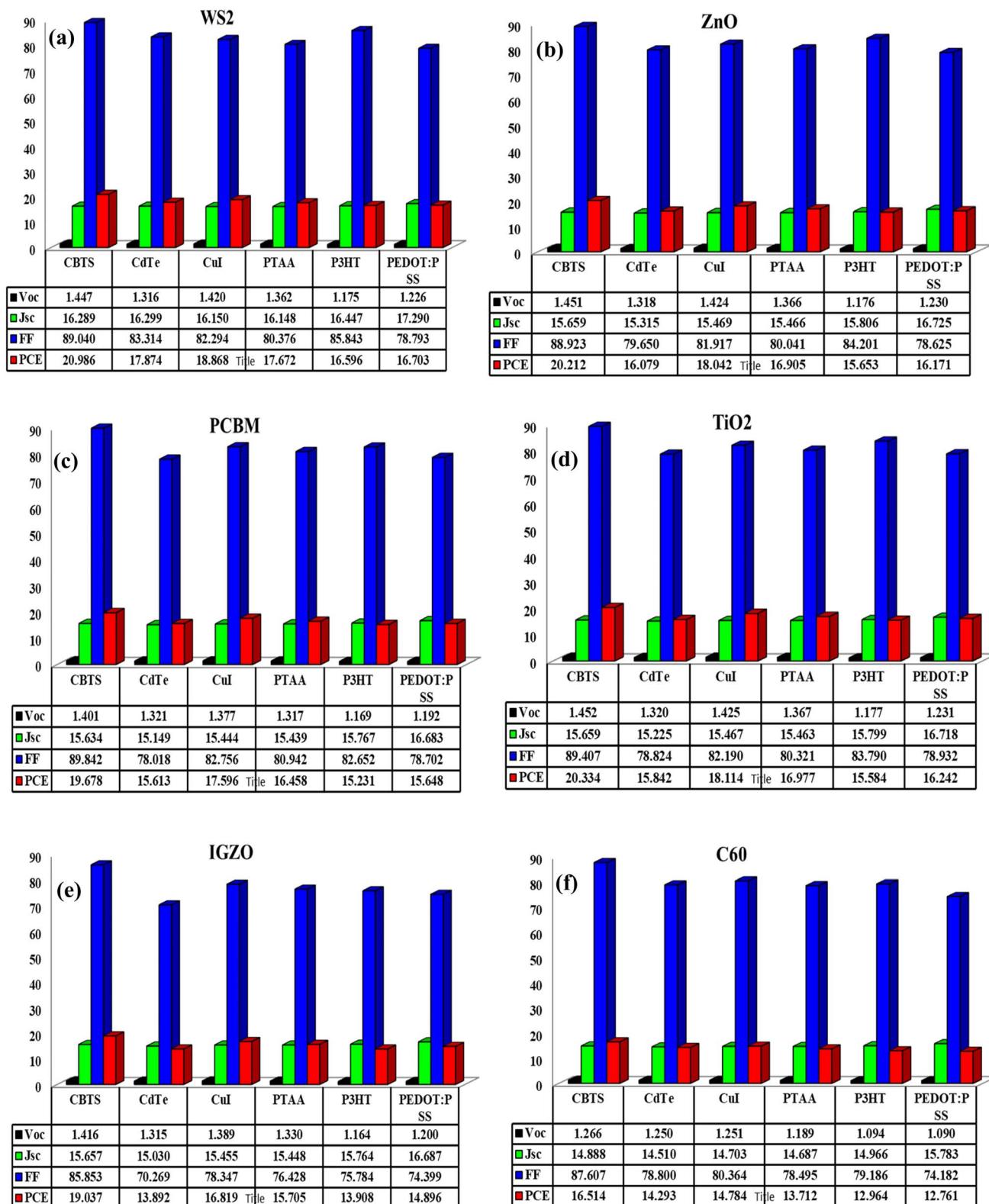


Fig. 4 HTL & ETL Selection for  $\text{Rb}_2\text{AuScCl}_6$  of (a)  $\text{WS}_2$  (b)  $\text{ZnO}$  (c) PCBM, (d)  $\text{TiO}_2$ , (e) IGZO and (f)  $\text{C}_{60}$  with HTL of CBTS, CdTe, CuI, PTAA, P3HT and PEDOT:PSS.

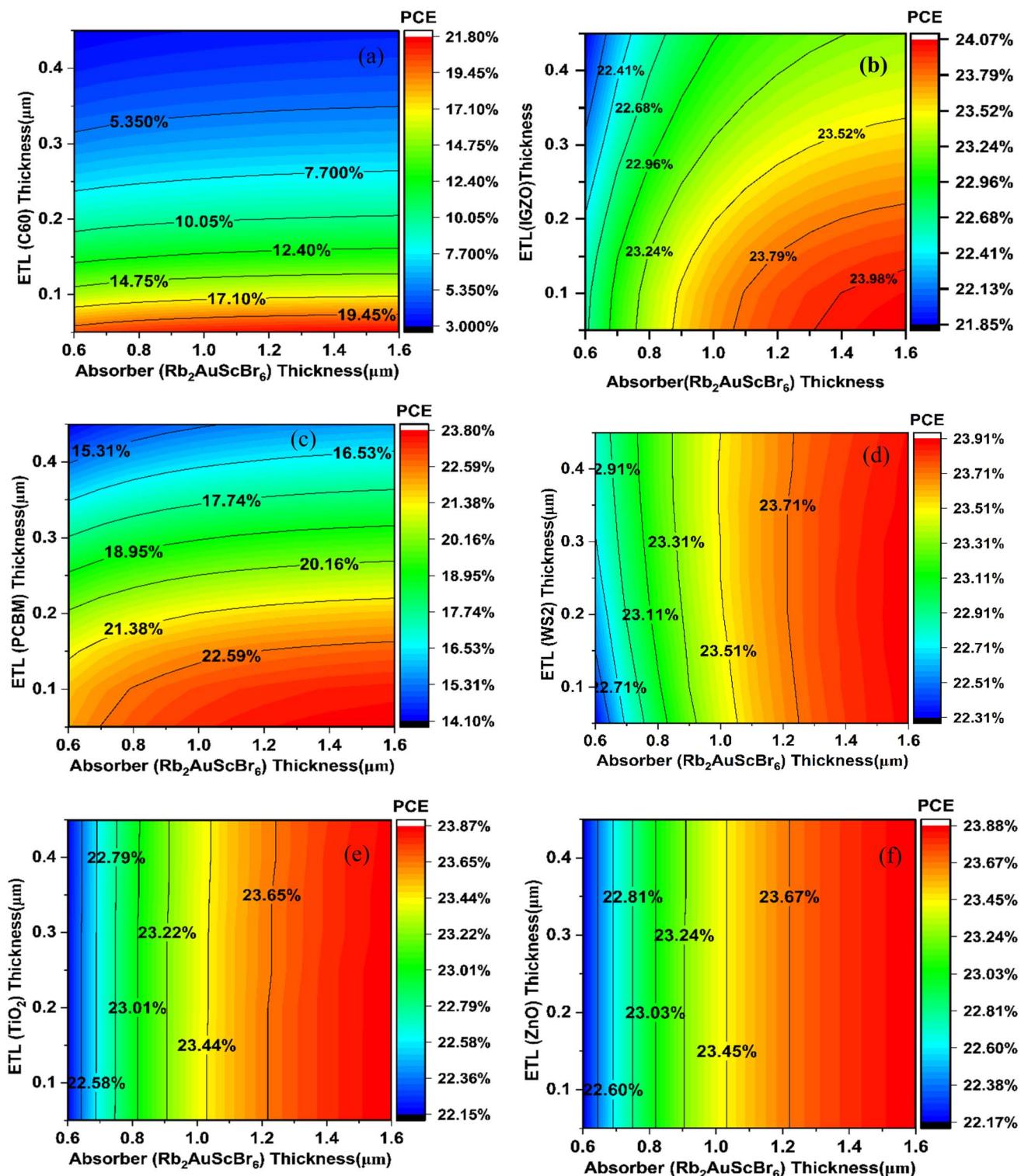


Fig. 5 Contour mapping of PCE, when the absorber is  $\text{Rb}_2\text{AuScBr}_6$  and ETLs as (a)  $\text{C}_{60}$ , (b)  $\text{IGZO}$ , (c)  $\text{PCBM}$ , (d)  $\text{WS}_2$ , (e)  $\text{TiO}_2$  and (f)  $\text{ZnO}$ .

holes into the ETL. Moreover, the high electron mobility of  $\text{IGZO}$  decreases recombination losses by quickly transporting charge carriers to the contact. The wide thickness tolerance (shown as contours that are further apart) means that even with small variations in the thickness of the absorber or ETL layer high efficiency can be obtained. This upon favorable band

alignment, fast charge transport, and thickness-independence, which altogether result in the superior device performances of  $\text{IGZO}$ . Fig. 6 shows how the PCE of perovskite solar cells changes when using different electron transport layers (ETLs) with the perovskite material  $\text{Rb}_2\text{AuScCl}_6$ . Each of the six sub-figures (a-f) represents a different ETL. Fig. 6(a) ( $\text{C}_{60}$  ETL)

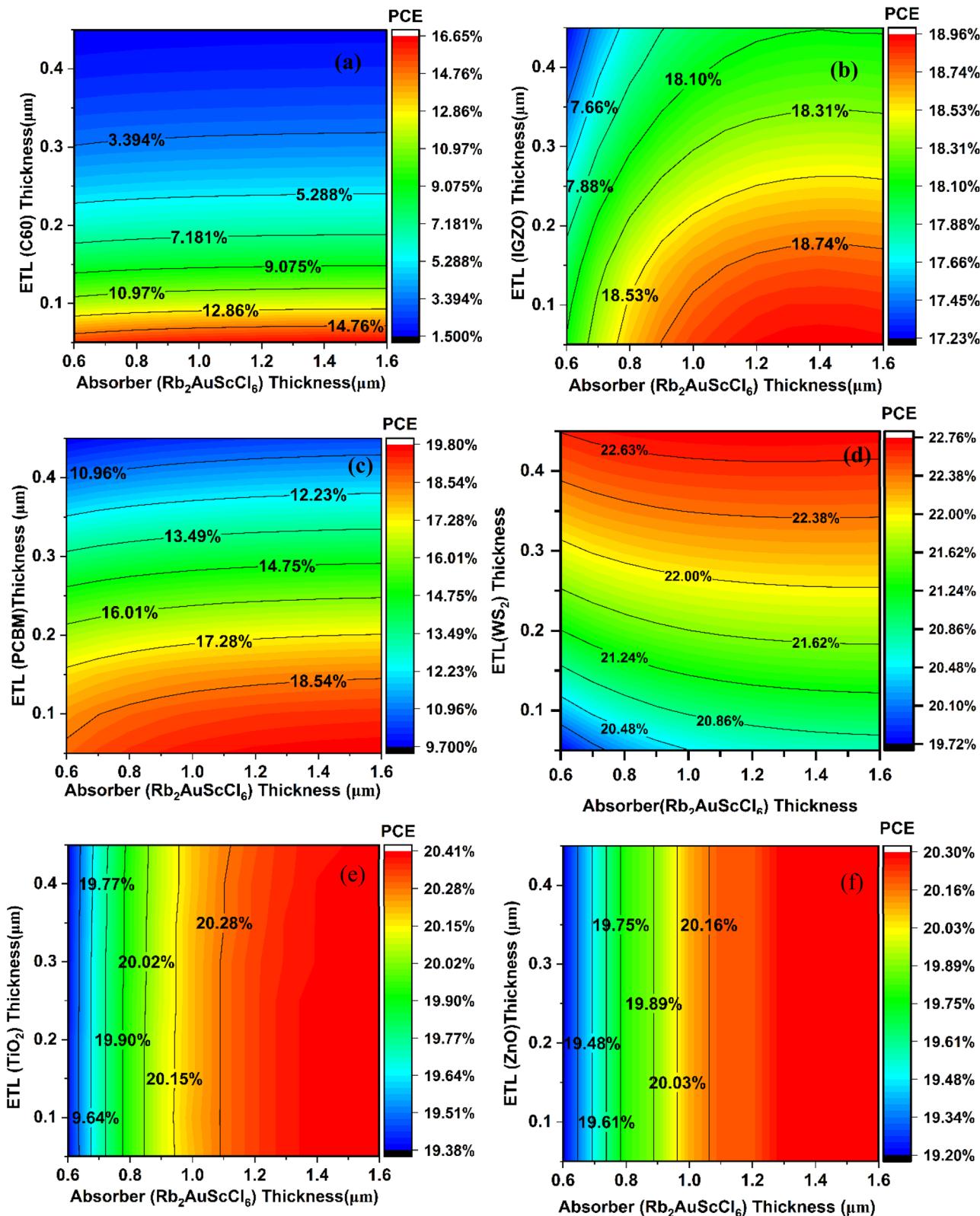


Fig. 6 Contour mapping of PCE when absorber is  $\text{Rb}_2\text{ScCl}_6$  and ETLs as (a)  $\text{C}_{60}$ , (b)  $\text{IGZO}$ , (c)  $\text{PCBM}$ , (d)  $\text{WS}_2$ , (e)  $\text{TiO}_2$  and (f)  $\text{ZnO}$ .

shows a maximum PCE of 16.65%. Where absorber thicknesses are  $\geq 1000$  nm and ETL thicknesses are  $\leq 50$  nm. The contour lines are relatively spread out, suggesting a less critical dependence on precise thickness control compared to some other

ETLs. Fig. 6(b) (IGZO ETL) exhibits a significantly higher maximum PCE, reaching approximately 18.96%. Where absorber thicknesses are  $\geq 1500$  nm and ETL thicknesses are  $\leq 450$  nm. The high PCE region is broad, indicating good

tolerance to variations in both absorber and ETL thicknesses. Fig. 6(c) (PCBM ETL) achieves a maximum PCE around 19.80%. The optimal performance seems to be associated with a specific range of thicknesses, as indicated by the concentrated contour lines. Fig. 6(d) (WS<sub>2</sub> ETL) shows a maximum PCE of about 22.76%. This is the highest PCE among the tested ETLs in this figure. The contour plot suggests a well-defined region of optimal performance. From the Fig. 6(c) and (d) reveal that the highest PCEs are achieved when the absorber thicknesses are  $\geq 1200$  nm and ETL thicknesses are  $\leq 50$  nm. Fig. 6(e) (TiO<sub>2</sub> ETL) reaches a maximum PCE of approximately 20.41% when absorber thicknesses are equal to 1200 nm and ETL thicknesses are less than or equal to 50 nm. Fig. 6(f) (ZnO ETL) exhibits a maximum PCE of 20.30% where the thicknesses are equal to 1400 nm and ETL thicknesses are equal to 450 nm. Based on Fig. 6, WS<sub>2</sub> is the best-performing ETL layer, achieving the highest maximum PCE of approximately 22.76%. This suggests that WS<sub>2</sub>, in combination with the Rb<sub>2</sub>ScCl<sub>6</sub> perovskite absorber, facilitates the most efficient charge transfer and transport among the materials tested. WS<sub>2</sub> performs best because its energy band alignment with the Rb<sub>2</sub>ScCl<sub>6</sub> absorber is optimal for efficient electron extraction. Its conduction band level is ideally positioned to collect electrons while preventing hole injection, thereby reducing recombination losses. Additionally, WS<sub>2</sub>'s high electron mobility and layered structure facilitate rapid charge transport, ensuring that the generated carriers are efficiently transferred through the device, which in turn maximizes the power conversion efficiency.<sup>52</sup>

#### 3.4. Impact of absorber thickness with best ETL

Absorber thickness had a large impact on the performance of ITO/ETL/Rb<sub>2</sub>ScBr<sub>6</sub>/CBTS/Ni and ITO/ETL/Rb<sub>2</sub>ScCl<sub>6</sub>/CBTS/Ni structures. The absorber thickness was varied from 400 nm to 2000 nm to improve the efficiency of devices and the effect has been studied on performance parameters. All the results obtained in the PSC showed that the  $V_{oc}$  tended to decrease as the absorber thickness increased. This drop is accompanied by the increase of reverse saturation current, resulting in charge recombination losses.<sup>53,54</sup> The Rb<sub>2</sub>ScBr<sub>6</sub>-based device exhibited a decrease in  $V_{oc}$  from 1.299 V at 400 nm to 1.25 V at

2000 nm; however, Rb<sub>2</sub>ScCl<sub>6</sub> remained at a more stable  $V_{oc}$  of 1.44–1.46 V. As illustrated in Fig. 7(a)  $J_{sc}$  increased as a result of improved light absorption with increasing absorber thickness. This trend is explained by the better spectral response at longer wavelengths for thicker absorbers. The  $J_{sc}$  increased from 18.46 mA cm<sup>-2</sup> (400 nm) to 21.87 mA cm<sup>-2</sup> (2000 nm) for the Rb<sub>2</sub>ScBr<sub>6</sub>-based structure and from 15.65 mA cm<sup>-2</sup> (600 nm) to 16.46 mA cm<sup>-2</sup> (2000 nm for the Rb<sub>2</sub>ScCl<sub>6</sub>).

In Fig. 7(b), the Rb<sub>2</sub>ScBr<sub>6</sub>-based device exhibited FF of up to 88.4–88.5%, while that of Rb<sub>2</sub>ScCl<sub>6</sub> stayed constant at 88.4–89.1%. With respect to power conversion efficiency (PCE), both materials exhibit an increase in PCE with increasing absorber thickness, peaking and subsequently declining slightly due to recombination losses.

For Rb<sub>2</sub>ScBr<sub>6</sub>, the highest was 24.08% at 2000 nm, and Rb<sub>2</sub>ScCl<sub>6</sub> reached 21.07% at 1600 nm. Although an optimized absorber thickness of 1600 nm for both Rb<sub>2</sub>ScBr<sub>6</sub> and Rb<sub>2</sub>ScCl<sub>6</sub> results in the highest device performance, a thinner absorber layer is generally more desirable for perovskite solar cells (PSCs).<sup>55</sup> Therefore, an absorber thickness of 1200 nm was selected as the optimal design choice for this study.

#### 3.5. Influence of metal back contact on solar cell performance

Fig. 8 illustrates the influence of the metal back contact's work function (WF) on key performance parameters  $V_{oc}$ ,  $J_{sc}$ , PCE, and FF for two device configurations: ITO/IGZO/Rb<sub>2</sub>ScBr<sub>6</sub>/CBTS/Metal and ITO/WS<sub>2</sub>/Rb<sub>2</sub>ScCl<sub>6</sub>/CBTS/Metal. In the case of the Rb<sub>2</sub>ScBr<sub>6</sub>-based device, the highest performance is achieved with a work function of 5.5 eV, where the device exhibits a  $V_{oc}$  of 1.36 V,  $J_{sc}$  of 21.42 mA cm<sup>-2</sup>, FF of 87.14%, and a maximum PCE of 25.3%. Notably, enhancing the work function beyond 5.5 eV does not significantly affect the PCE, indicating stability in device performance. Due to this optimized performance and the favorable alignment with the Ni back contact (WF = 5.5 eV), nickel is selected as the preferred back electrode for this device. For the Rb<sub>2</sub>ScCl<sub>6</sub>-based device, the highest PCE of 22.48% is observed at a work function of 5.8 eV, with corresponding values of  $V_{oc} = 1.53$  V,  $J_{sc} = 16.15$  mA cm<sup>-2</sup>, and FF = 90.78%.

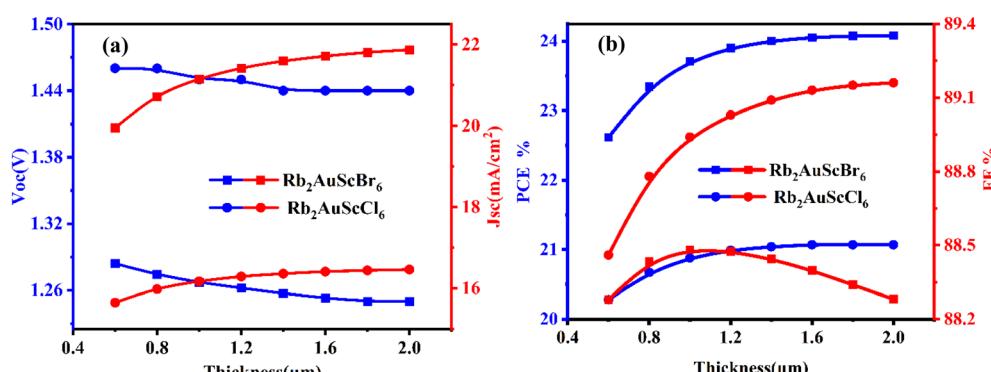


Fig. 7 Effect of absorber thickness on performance parameters (a)  $V_{oc}$ , and  $J_{sc}$ , (b) PCE and FF of (ITO/IGZO/Rb<sub>2</sub>ScBr<sub>6</sub>/CBTS/Ni) (ITO/WS<sub>2</sub>/Rb<sub>2</sub>ScCl<sub>6</sub>/CBTS/Ni) devices.



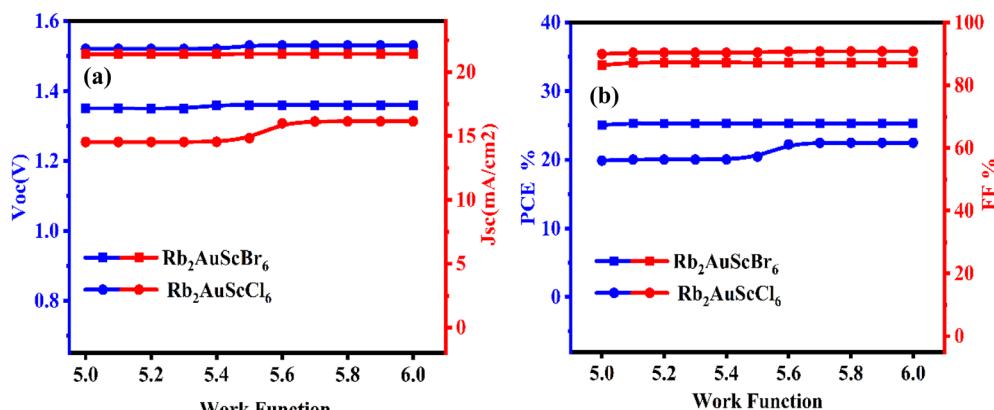


Fig. 8 Effect of Metal Back Contact on performance parameters (a)  $V_{oc}$ , and  $J_{sc}$ , (b) PCE and FF of (ITO/IGZO/ $\text{Rb}_2\text{AuScBr}_6$ /CBTS/Ni) (ITO/WS<sub>2</sub>/ $\text{Rb}_2\text{AuScCl}_6$ /CBTS/Ni) devices.

However, metals with a work function of 5.8 eV, such as platinum (Pt), are highly expensive and thus less viable for commercial use. Therefore, nickel (WF = 5.5 eV) is adopted as a cost-effective alternative. With Ni as the back contact, the device still demonstrates respectable performance, achieving a PCE of 20.45%,  $V_{oc}$  of 1.53 V,  $J_{sc}$  of 14.83 mA cm<sup>-2</sup>, and FF of 90.43%.

In summary, the feasibility and cost-effectiveness of using nickel as the back contact support its selection for both device architectures.<sup>56</sup>

### 3.6. Effect of acceptor density on the solar cell PCE

The impact of acceptor density on PCE has been analyzed for two device architectures: ITO/IGZO/ $\text{Rb}_2\text{AuScBr}_6$ /CBTS/Ni and ITO/WS<sub>2</sub>/ $\text{Rb}_2\text{AuScCl}_6$ /CBTS/Ni. Fig. 9 illustrates variations in  $V_{oc}$ ,  $J_{sc}$ , FF, and PCE as functions of acceptor density, highlighting efficiency trends in both configurations. From Fig. 9(b), PCE follows a similar trend with the increase of acceptor density, reaches a maximum value, and then decreases steadily. The maximum value of PCE (25.81%) occurs for the  $\text{Rb}_2\text{AuScBr}_6$ -based device with an acceptor density of  $10^{18}$  cm<sup>-3</sup>, at  $V_{oc} = 1.37$  V,  $J_{sc} = 21.26$  mA cm<sup>-2</sup>, and FF = 88.94%. Likewise,

the  $\text{Rb}_2\text{AuScCl}_6$ -based device exhibits a maximum PCE of 22.41% at the acceptor density of  $10^{17}$  cm<sup>-3</sup>, at  $V_{oc} = 1.53$  V,  $J_{sc} = 16.16$  mA cm<sup>-2</sup>, and FF = 90.65%, after which the efficiency drops. The increase in  $V_{oc}$  may be attributed to the increased charge carrier separation due to increased internal electric field as a result of increased acceptor density.

Increase in doping concentration contributes to a reduction in series resistance (as such, improving FF) and a reduction in surface recombination losses. In contrast with  $V_{oc}$  and FF,  $J_{sc}$  is almost unchanged, suggesting that the doping variations have little impact on light absorption and carrier generation. The results highlight the critical role of optimizing acceptor density in enhancing solar cell efficiency. Among the studied devices,  $\text{Rb}_2\text{AuScBr}_6$ -based solar cells demonstrated superior performance compared to  $\text{Rb}_2\text{AuScCl}_6$  counterparts, which can be attributed to their improved charge transport characteristics and more favorable optical properties.

### 3.7. Influence of absorber defect density on solar cell behavior

The value of defect density ( $N_t$ ) in the absorber layer has a great impact on the overall efficiency of solar cell devices.<sup>57</sup> Fig. 10(a)

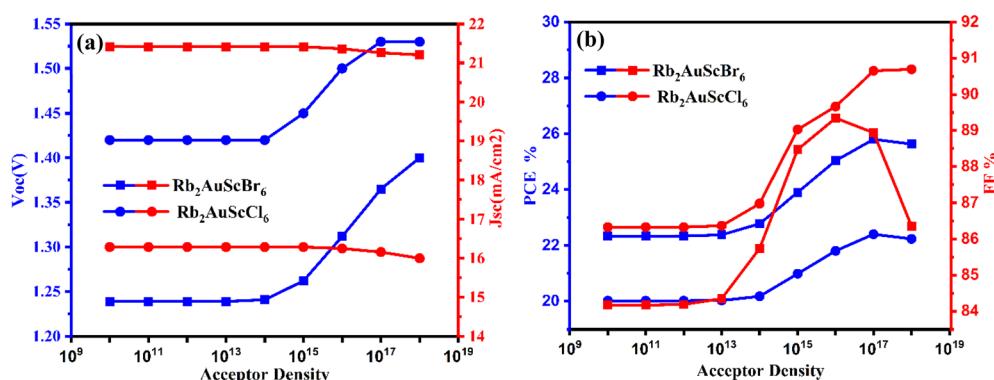


Fig. 9 Variation of cell parameters with changing acceptor density (a)  $V_{oc}$  and  $J_{sc}$ , (b) PCE and FF of (ITO/IGZO/ $\text{Rb}_2\text{AuScBr}_6$ /CBTS/Ni) and (ITO/WS<sub>2</sub>/ $\text{Rb}_2\text{AuScCl}_6$ /CBTS/Ni) devices.



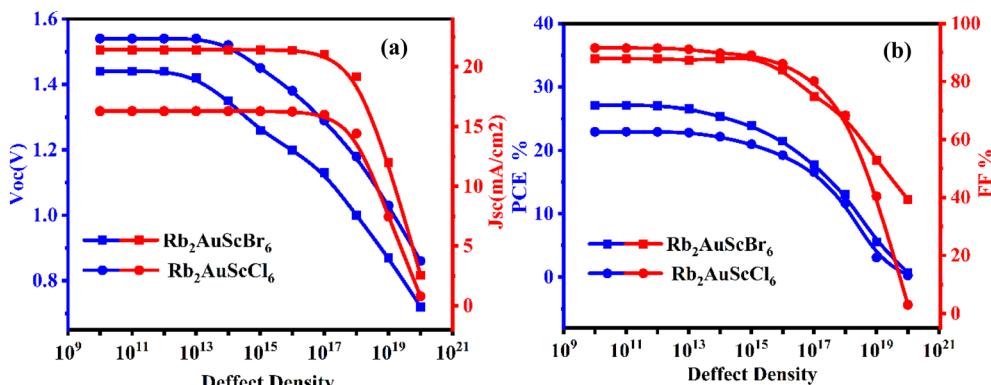


Fig. 10 Effect of absorber defect density ( $N_t$ ) on performance parameters (a)  $V_{oc}$  and  $J_{sc}$ , (b) PCE and FF of (ITO/IGZO/ $\text{Rb}_2\text{AuScBr}_6$ /CBTS/Ni) (ITO/WS<sub>2</sub>/ $\text{Rb}_2\text{AuScCl}_6$ /CBTS/Ni) devices.

and (b) of devices based on  $\text{Rb}_2\text{AuScBr}_6$  and  $\text{Rb}_2\text{AuScCl}_6$ , respectively. The characteristic of increasing  $N_t$  leads to the reduction of  $V_{oc}$ ,  $J_{sc}$ , FF, and PCE in both devices. Under these conditions, the best PCE of 27.11% can be obtained for the  $\text{Rb}_2\text{AuScBr}_6$ -based device with the parameters of  $V_{oc} = 1.44$  V,  $J_{sc} = 21.42$  mA cm<sup>-2</sup>, and FF = 87.88%. This high efficiency is maintained when the defect density in the absorber layer is at  $10^{10}$  cm<sup>-3</sup>. In a similar, the  $\text{Rb}_2\text{AuScCl}_6$ -based device reaches its highest PCE = 22.96% with  $V_{oc} = 1.54$  V,  $J_{sc} = 16.29$  mA cm<sup>-2</sup>, and FF = 91.53%.

Although the highest PCEs of 27.11% for the  $\text{Rb}_2\text{AuScBr}_6$ -based absorber and 22.96% for the  $\text{Rb}_2\text{AuScCl}_6$ -based absorber were obtained at a defect density of  $10^{10}$  cm<sup>-3</sup>, such a low defect density is not considered realistic or acceptable. In practical conditions, the defect density cannot be reduced below  $10^{14}$  cm<sup>-3</sup> and must at least be maintained at this level. At a more acceptable defect density of  $10^{15}$  cm<sup>-3</sup>,<sup>58</sup> the  $\text{Rb}_2\text{AuScBr}_6$ -based absorber achieves a PCE of 23.90%, while the  $\text{Rb}_2\text{AuScCl}_6$ -based absorber reaches a PCE of 20.99%.

### 3.8. Influences of electron affinity on solar cell behavior

Solar cell efficiency is influenced by the electron affinity of the absorber layer. Fig. 11(a) and (b) depict the variations of  $V_{oc}$ ,  $J_{sc}$ ,

FF, and PCE with electron affinity for the  $\text{Rb}_2\text{AuScBr}_6$  and  $\text{Rb}_2\text{AuScCl}_6$ -based devices, respectively.

For the  $\text{Rb}_2\text{AuScBr}_6$ -based device, the optimal electron affinity (3.95 eV, producing the maximum PCE of 23.12% with  $V_{oc} = 1.26$  V,  $J_{sc} = 21.41$  mA cm<sup>-2</sup>, and FF = 88.65%). When the electron affinity becomes larger than this optimal value, the efficiency declines due to a band misalignment, with a corresponding loss of  $V_{oc}$  and FF. However, with further increasing EA at 4.50 eV, PCE decreases sharply to 15.93%, highlighting the negative influences of excessive electron affinity on carrier extraction.

For the device based on  $\text{Rb}_2\text{AuScCl}_6$ , the peak PCE of 21.06% is achieved at 3.70 eV, with  $V_{oc} = 1.45$  V,  $J_{sc} = 16.29$  mA cm<sup>-2</sup>, and FF = 88.94%. Above this region, the efficiency begins to decrease, with a serious drop at 4.30 eV and 4.50 eV, with the value of PCE being as low as 8.54% and 6.33%, respectively. The diminished performance at increased electron affinity can be attributed to larger recombination losses and diminished built-in potential, which compromise charge separation and collection efficiency. Thus, tuning the electron affinity for the absorber is crucial for achieving higher cell efficiency. These findings confirm that  $\text{Rb}_2\text{AuScBr}_6$  is indeed a better candidate for the development of efficient devices than  $\text{Rb}_2\text{AuScCl}_6$ , because its superior electrical properties allow for boosting charge transport and decreasing recombination losses.

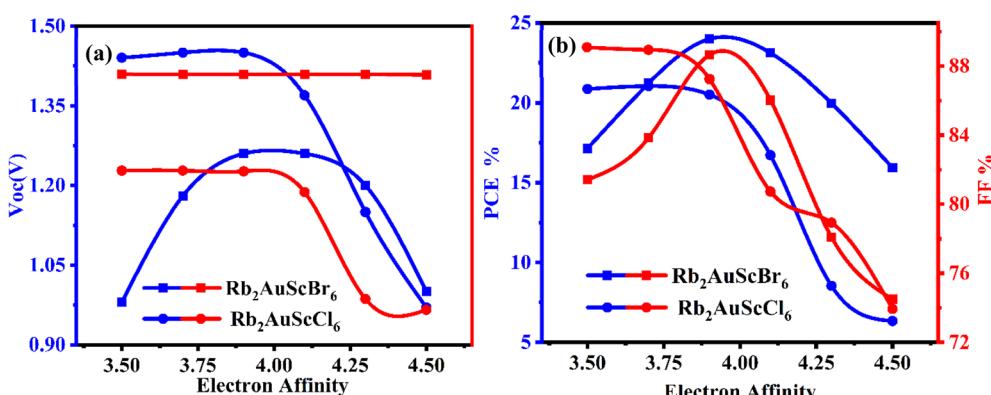


Fig. 11 Effect of absorber electron affinity on performance parameters (a)  $V_{oc}$  and  $J_{sc}$ , (b) PCE and FF of (ITO/IGZO/ $\text{Rb}_2\text{AuScBr}_6$ /CBTS/Ni) (ITO/WS<sub>2</sub>/ $\text{Rb}_2\text{AuScCl}_6$ /CBTS/Ni) devices.

This improvement can be attributed to the better light intensity of  $\text{Rb}_2\text{AuScBr}_6$  caused by the optimal band gap, which leads to better light absorption and efficient excitation of charge carriers.<sup>59,60</sup> It achieves a better conduction-band alignment to maintain a matched band gap, improving the tandems  $V_{\text{oc}}$ ,  $J_{\text{sc}}$ , and FF balance, and therefore higher efficiencies are obtained than for  $\text{Rb}_2\text{AuScCl}_6$ . To put it plainly,  $\text{Rb}_2\text{AuScBr}_6$  is more efficient at absorbing light, produces a lot of more beneficial charge carriers, and minimizes energy losses, which all contribute to it being better suited for high-performance solar cells.

### 3.9. Influences of electron mobility on solar cell performance

In contrast, the power conversion efficiency (PCE) exhibits a slight upward trend, particularly at lower  $\mu_{\text{e}}$  values. For  $\text{Rb}_2\text{AuScCl}_6$ , the PCE increases from 20.73% to 21.00% as  $\mu_{\text{e}}$  reaches  $90 \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$ , while for  $\text{Rb}_2\text{AuScBr}_6$ , it rises from 23.00% to 23.92% within the same range. This improvement is attributed to enhanced charge-transport capability, reduced series resistance, and suppression of electron accumulation at interfaces, which collectively lower recombination losses and improve carrier extraction.

Fig. 12(a) and (b) shows the effect of electron mobility ( $\mu_{\text{e}}$ ) in the range of  $10\text{--}100 \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$  on the photovoltaic performance of  $\text{Rb}_2\text{AuScCl}_6$ - and  $\text{Rb}_2\text{AuScBr}_6$ -based perovskite solar cells. The short-circuit current density ( $J_{\text{sc}}$ ) and open-circuit voltage ( $V_{\text{oc}}$ ) remain largely unchanged with increasing  $\mu_{\text{e}}$ , indicating stable charge generation and extraction across the studied mobility range.

As  $\mu_{\text{e}}$  approaches  $90 \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$ , the PCE reaches a near-saturation region, indicating that carrier transport becomes sufficiently efficient and further mobility enhancement yields minimal benefit. Beyond this point, the device performance is primarily limited by interfacial recombination, optical absorption constraints, and hole-transport efficiency rather than electron mobility alone.

Overall, electron mobility has a positive yet bounded influence on device performance.<sup>61</sup> An optimal mobility window of  $80\text{--}90 \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$  ensures maximum PCE, beyond which additional increases in  $\mu_{\text{e}}$  do not result in notable efficiency gains.

### 3.10. Effect of series resistance ( $R_{\text{s}}$ ) on solar cell performance

The effect of  $R_{\text{s}}$  (series resistance) is a significant factor in solar cell efficiency.  $R_{\text{s}}$  was varied from  $1 \Omega$  to  $8 \Omega \text{ cm}^2$  in order to investigate its effect on output parameters while maintaining shunt resistance ( $R_{\text{sh}}$ ) constant at a value of  $10^5 \Omega \text{ cm}^2$ , as shown in Fig. 13(a) and (b).  $J_{\text{sc}}$ , on the other hand, is relatively insensitive to series resistance;  $J_{\text{sc}}$  remains almost unchanged, but  $V_{\text{oc}}$  and FF gradually decrease as  $R_{\text{s}}$  increases due to more significant resistive losses.<sup>62</sup> For devices based on  $\text{Rb}_2\text{AuScBr}_6$ , the maximum PCE of 23.90% is achieved with  $R_{\text{s}} = 1 \Omega$ ,  $V_{\text{oc}} = 1.26 \text{ V}$ ,  $J_{\text{sc}} = 21.41 \text{ mA cm}^{-2}$ , and FF = 88.48%. In a similar trend for  $\text{Rb}_2\text{AuScCl}_6$ -based devices, a maximum PCE of 20.99% occurs at  $R_{\text{s}} = 1 \Omega$  ( $V_{\text{oc}} = 1.45 \text{ V}$ ,  $J_{\text{sc}} = 16.29 \text{ mA cm}^{-2}$ , and FF = 89.03%). With higher  $R_{\text{s}}$ , PCE decreases due to a fall in FF and a small decrease in  $V_{\text{oc}}$ . The increased resistive losses and suppressed charge transport caused by a higher  $R_{\text{s}}$  result in larger resistive losses and lower power output. Nevertheless,  $\text{Rb}_2\text{AuScBr}_6$ -based devices show higher PCE than their  $\text{Rb}_2\text{AuScCl}_6$  counterparts, revealing better charge carrier mobility and reduced recombination losses.<sup>63,64</sup> We found that reducing  $R_{\text{s}}$  is critical for improving solar cell performance, as lower resistance in series leads to better efficiency and improved charge extraction.<sup>65</sup> Additionally, a higher  $R_{\text{s}}$  increases the voltage drop across the device under forward bias, which limits the charge extraction capability and accelerates recombination within the absorber and interfaces. This results in diminished diode quality and reduced operational stability, particularly under high-intensity illumination or prolonged operation. Therefore, maintaining a low  $R_{\text{s}}$  is essential not only for maximizing PCE but also for ensuring long-term device reliability and efficient carrier transport pathways.

### 3.11. Effect of shunt resistance ( $R_{\text{sh}}$ ) on solar cell performance

Shunt resistance ( $R_{\text{sh}}$ ) is an important parameter for the overall performance of perovskite solar cells (PSCs). Low  $R_{\text{sh}}$  causes power losses mainly resulting from leakage current and non-geminate recombination losses. These losses happen due to partial junction shorts that arise from pinholes and metal filling

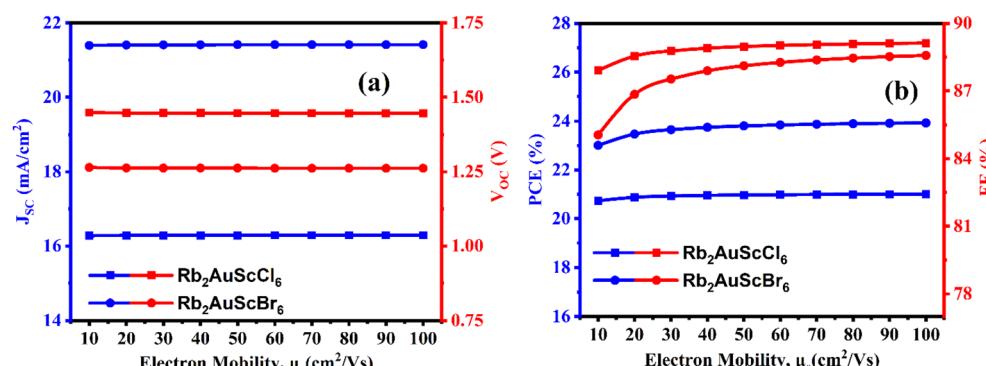


Fig. 12 Effect of absorber electron mobility on performance parameters (a)  $V_{\text{oc}}$  and  $J_{\text{sc}}$ , (b) PCE and FF of (ITO/IGZO/ $\text{Rb}_2\text{AuScBr}_6$ /CBTS/Ni) (ITO/WS<sub>2</sub>/ $\text{Rb}_2\text{AuScCl}_6$ /CBTS/Ni) devices.



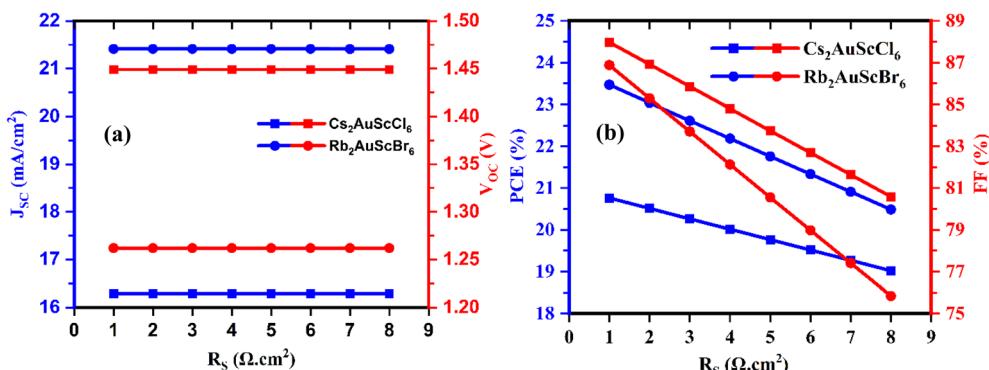


Fig. 13 Effect of series resistance ( $R_s$ ) on performance parameters (a)  $V_{oc}$  and  $J_{sc}$ , (b) PCE and FF of (ITO/IGZO/Rb<sub>2</sub>AuScBr<sub>6</sub>/CBTS/Ni) (ITO/WS<sub>2</sub>/Rb<sub>2</sub>AuScCl<sub>6</sub>/CBTS/Ni) devices.

reaching the junctions. In this case, low  $R_{sh}$  (parallel resistance) allows for a bypass of the solar cell itself and hence reduces voltage ( $V_{oc}$ ) and calculated current flow through the junction.  $R_{sh}$  plays a more important role at low light due to the contribution of current loss being dominant when the light-generated current is already at low levels.<sup>66,67</sup> To reduce these losses, a variety of techniques have been employed to increase  $R_{sh}$ , such as doping the ETL with lead (Pb) to increase resistance further. The  $R_{sh}$  value can be, therefore, conveniently amended for making good device efficiency when the Pb content is carefully adjusted.  $V_{oc}$ ,  $J_{sc}$ , FF, and PCE are analyzed for Rb<sub>2</sub>AuScBr<sub>6</sub> and Rb<sub>2</sub>AuScCl<sub>6</sub>-based solar cells—keeping  $R_{sh}$  in the range of 10 to  $10^8 \Omega$ , while  $R_s$  was fixed throughout at  $1 \Omega \text{ cm}^2$ .

The data are summarized in Fig. 14(a) and (b). The maximum PCE of Rb<sub>2</sub>AuScBr<sub>6</sub>-based devices reached 23.90% at  $R_{sh} = 10^6 \Omega$ , with  $V_{oc} = 1.26 \text{ V}$ ,  $J_{sc} = 21.41 \text{ mA cm}^{-2}$ , and FF = 88.48%. In the same manner, for Rb<sub>2</sub>AuScCl<sub>6</sub>-based devices, 20.99% of the maximum PCE occurs at  $R_{sh} = 10^7 \Omega$ , with  $V_{oc} = 1.45 \text{ V}$ ,  $J_{sc} = 16.29 \text{ mA cm}^{-2}$  and FF = 89.03%. With the increase of  $R_{sh}$ ,  $V_{oc}$  and FF is effectively increased, significantly improving the PCE. But it plateaus above  $10^6 \Omega$  (Rb<sub>2</sub>AuScBr<sub>6</sub>) and  $10^7 \Omega$  (Rb<sub>2</sub>AuScCl<sub>6</sub>), demonstrating that additional increases in  $R_{sh}$  have an insignificant influence on performance.

These data underscore that  $R_{sh}$  is important for optimizing PSC efficiency. High  $R_{sh}$  ( $\geq 10^4 \Omega$ ) is crucial for reducing leakage

currents and recombination losses to guarantee better charge collection and enhanced device performance.<sup>68,69</sup> The improved performance seen in Rb<sub>2</sub>AuScBr<sub>6</sub>-based devices demonstrates that with higher charge transport ability and minimized recombination losses, Rb<sub>2</sub>AuScBr<sub>6</sub>-based devices can outperform their Rb<sub>2</sub>AuScCl<sub>6</sub> analogs. For further insights to better understand the behavior of  $R_{sh}$  and  $R_s$ , an ideal single-diode model has been described using eqn (11).

$$I = I_L - I_0 \left[ \exp \left( \frac{q(M)}{A k_B T} \right) - 1 \right] - \frac{M}{R_{sh}} \quad (11)$$

where  $A$  stands for ideality factor,  $k_B$  for Boltzmann constant,  $T$  for temperature,  $q$  for electron charge, and  $M = V + (I \times R_s)$ . The opposite saturation current of the diode is  $I_0$ , while the light-induced current is  $I_L$ . Eqn (12) and (13) are the  $R_s$  and  $R_{sh}$  equations, respectively, derived from the  $J$ - $V$  curves, in which  $\Delta V$  stands for voltage change and  $\Delta I$  for current change.

$$R_{sh} = -\frac{\Delta V}{\Delta I} (V = 0) \quad (12)$$

$$R_s = -\frac{\Delta V}{\Delta I} (V = V_0) \quad (13)$$

As described in eqn (11), the term  $\frac{M}{R_{sh}}$  represents the parasitic leakage current path, meaning that a lower  $R_{sh}$  increases

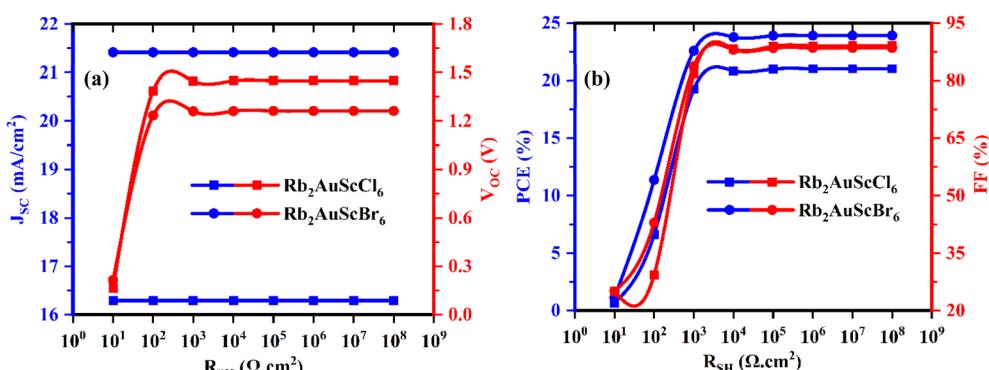


Fig. 14 Effect of shunt resistance ( $R_{sh}$ ) on performance parameters (a)  $V_{oc}$  and  $J_{sc}$ , (b) PCE and FF of (ITO/IGZO/Rb<sub>2</sub>AuScBr<sub>6</sub>/CBTS/Ni) (ITO/WS<sub>2</sub>/Rb<sub>2</sub>AuScCl<sub>6</sub>/CBTS/Ni) devices.

the portion of current that bypasses the junction, thereby reducing the net photocurrent and weakening the diode characteristics. When  $R_{sh}$  is sufficiently high, this leakage component becomes negligible, ensuring efficient charge extraction and sustaining higher  $V_{oc}$  and FF. Therefore, maintaining a large  $R_{sh}$  is critical for suppressing shunt-induced recombination losses and achieving ideal diode behavior and superior device performance.

### 3.12. Role of temperature on solar cell performance

Temperature causes a large change in  $V_{oc}$ ,  $J_{sc}$ , FF, and PCE of PSCs, influencing the efficiency of PSCs. A high temperature can cause  $V_{oc}$  and FF to drop, leading to a corresponding drop in PCE. This decrease is due to increased recombination of charge carriers, thermally activated effects, and changes in material properties that limit device performance. In PSCs,  $J_{sc}$  shows almost no temperature dependence, revealing that the absorption properties of the absorber layers are not affected by the temperature.<sup>70</sup> The temperature (300–440 K) effects on  $V_{oc}$ ,  $J_{sc}$ , FF, and PCE of both  $\text{Rb}_2\text{AuScBr}_6$  and  $\text{Rb}_2\text{AuScCl}_6$ -based solar cells are presented in Fig. 14(a) and (b). The maximum PCE of  $\text{Rb}_2\text{AuScBr}_6$ -based devices is up to 23.901% at 300 K with  $V_{oc} = 1.262$  V,  $J_{sc} = 21.41 \text{ mA cm}^{-2}$ , and FF = 88.475%. Likewise, the PCE of  $\text{Rb}_2\text{AuScCl}_6$ -based devices is 21.013% at 300 K, with  $V_{oc} = 1.449$  V,  $J_{sc} = 16.289 \text{ mA cm}^{-2}$ , and FF = 89.036%. This ensures a negative impact of higher temperatures on the solar cell performance, as well as a positive impact of lower operating temperature on efficiency.<sup>71</sup>

### 3.13. Impact of capacitance, Mott–Schottky, generation and recombination rate

The C–V behavior of  $\text{Rb}_2\text{AuScBr}_6$  and  $\text{Rb}_2\text{AuScCl}_6$ -based PSCs is shown in Fig. 15(a). An increased capacitance with voltage indicates charge accumulation at the interface. Capacitance for  $\text{Rb}_2\text{AuScBr}_6$  is much higher than  $\text{Rb}_2\text{AuScCl}_6$ , suggesting a larger charge storage capability of  $\text{Rb}_2\text{AuScCl}_6$  along with enhanced charge carrier density. This implies that  $\text{Rb}_2\text{AuScCl}_6$  possesses enhanced dielectric behavior and more efficient charge transport, factors that may be responsible for its corresponding higher power conversion efficiency (PCE). The

junction capacitance per area was determined using a known relation:<sup>72</sup>

$$\frac{1}{C^2} = \frac{2\epsilon_0\epsilon_r}{qN_d}(V_{bi} - V) \quad (14)$$

where  $\epsilon_0$  is vacuum permittivity,  $\epsilon_r$  is the dielectric constant,  $q$  is electronic charge, and  $A$  is the area of the device. The value of  $N_d$  is derived from the gradient of the linear region in the M–S plot, while  $V_{bi}$  is the extrapolated segment from the linear segment to the voltage axis.

As seen in Fig. 16(b), the Mott–Schottky plot ( $1/C^2$  vs. Voltage) shows that the equation gives the information on the built-in potential and the carrier density. The flatter slope in the  $\text{Rb}_2\text{AuScCl}_6$  device corresponds to higher  $N_d$ , which improves the internal electric field distribution, leading to better carrier transport and reduced recombination losses. Notably, the built-in potential  $V$  is higher in the  $\text{Rb}_2\text{AuScBr}_6$  cell, supporting stronger band bending and more efficient charge separation at the junction. Fig. 16(c) and (d) demonstrate the spatial profiles of the carrier generation and recombination rates within both device structures. The generation rate profile reveals that  $\text{Rb}_2\text{AuScBr}_6$ -based cells exhibit a peak carrier generation rate of  $\sim 10^{22} \text{ cm}^{-3} \text{ s}^{-1}$ , slightly exceeding that of the  $\text{Rb}_2\text{AuScCl}_6$ -based cells, which peak around  $\sim 10^{21} \text{ cm}^{-3} \text{ s}^{-1}$ . This behavior is described quantitatively by the following relation:

$$G(\lambda, x) = \alpha(\lambda, x)N_{phot}(\lambda, x) \quad (15)$$

Here,  $G(\lambda, x)$  represents the generation rate of electron–hole pairs at a given wavelength  $\lambda$  and depth  $x$  within the absorber. The term  $\alpha(\lambda, x)$  is the absorption coefficient, which reflects how strongly the material absorbs light at different wavelengths and depths, while  $N_{phot}(\lambda, x)$  denotes the photon flux—the number of incident photons available for absorption at that wavelength and position. This equation shows that carrier generation is directly influenced by both the material's optical absorption properties and the incident light intensity. In this context, although  $\text{Rb}_2\text{AuScBr}_6$  shows a slightly higher peak generation rate, the favorable absorption behavior of  $\text{Rb}_2\text{AuScCl}_6$  enables it to harness a wider portion of the solar spectrum effectively, resulting in substantial exciton generation and contributing to

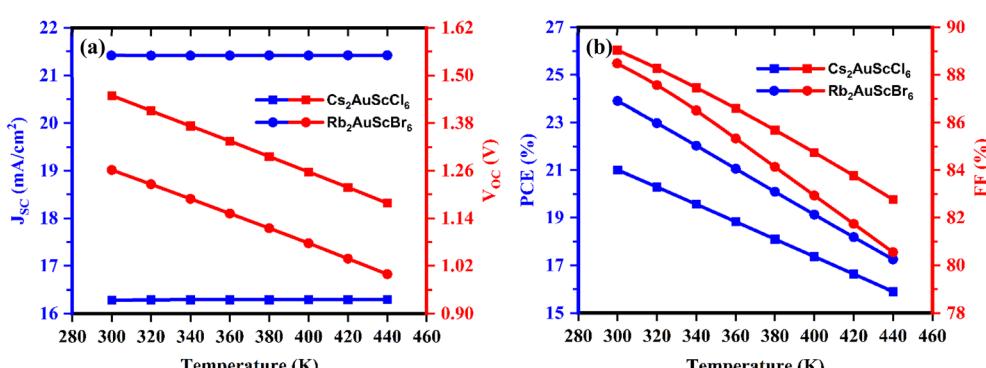


Fig. 15 Effect of temperature on performance parameters (a)  $V_{oc}$  and  $J_{sc}$ , (b) PCE and FF of (ITO/IGZO/ $\text{Rb}_2\text{AuScBr}_6$ /CBTS/Ni) and (ITO/WS<sub>2</sub>/ $\text{Rb}_2\text{AuScCl}_6$ /CBTS/Ni) devices.



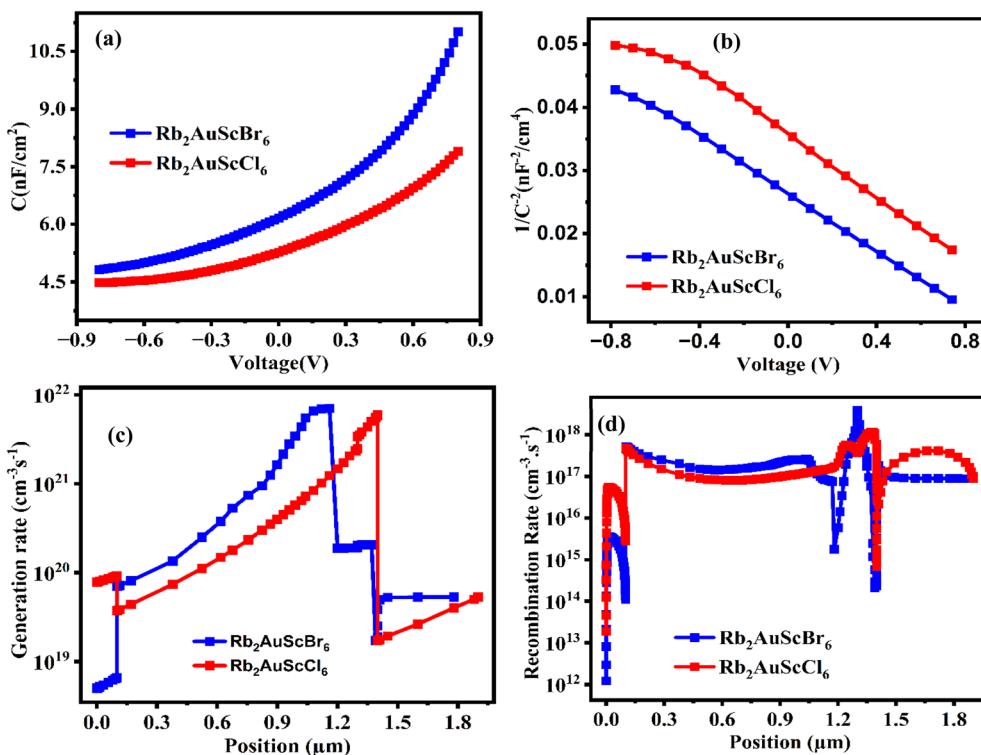


Fig. 16 (a) Capacitance, (b) Mott–Scotty plot ( $1/C^2$ ), (c) generation, and (d) recombination of (ITO/IGZO/Rb<sub>2</sub>AuScBr<sub>6</sub>/CBTS/Ni) and (ITO/WS<sub>2</sub>/Rb<sub>2</sub>AuScCl<sub>6</sub>/CBTS/Ni) devices.

an elevated  $J_{sc}$ . Fig. 16(d) shows that the Rb<sub>2</sub>AuScCl<sub>6</sub>-based device exhibits significantly lower recombination rates throughout both the absorber layer and the interfaces, compared to the Rb<sub>2</sub>AuScBr<sub>6</sub>-based device. This lower recombination indicates that fewer charge carriers are lost before contributing to current, suggesting longer carrier lifetimes and less defect-induced trapping within the material. These advantages are likely due to better crystal quality, optimized interface alignment, and reduced trap densities in Rb<sub>2</sub>AuScCl<sub>6</sub>. As a result, although both devices are capable of generating charge carriers efficiently under illumination, the reduced recombination in Rb<sub>2</sub>AuScCl<sub>6</sub> allows more carriers to reach the electrodes and contribute to the output power. Combined with its strong dielectric properties and higher concentration of mobile carriers, these factors lead to a noticeable improvement in key photovoltaic parameters such as the  $V_{oc}$ , FF, and overall PCE. Therefore, the Rb<sub>2</sub>AuScCl<sub>6</sub>-based perovskite solar cell demonstrates greater promise for high-performance and stable lead-free solar technologies.<sup>73</sup>

### 3.14. Current density vs. voltage ( $J$ - $V$ ) and quantum efficiency (QE) curve

Fig. 17(a) and (b) shows the  $J$ - $V$  characteristics of Rb<sub>2</sub>AuScBr<sub>6</sub> and Rb<sub>2</sub>AuScCl<sub>6</sub> based Absorber investigated perovskite solar cell structures are presented with voltage varying from 0 to 1.50 V; from which the Rb<sub>2</sub>AuScBr<sub>6</sub>-based PSC initially shows a current density of nearly 21.41 mA cm<sup>-2</sup> and finally shows a current density of nearly 21.20 mA cm<sup>-2</sup> the Rb<sub>2</sub>AuScCl<sub>6</sub>-based

device presents initial  $J_{sc}$  of ~16.26 mA cm<sup>-2</sup> and final  $J_{sc}$  of 16.13 mA cm<sup>-2</sup>. Within this analysis, we observe that compared to the initial value slightly decrease final value of  $J_{sc}$ . The initial  $V_{oc}$  is 1.28 V for Rb<sub>2</sub>AuScBr<sub>6</sub> and 1.46 V for Rb<sub>2</sub>AuScCl<sub>6</sub>, and final  $V_{oc}$  1.44 for Rb<sub>2</sub>AuScBr<sub>6</sub> and 1.56 for Rb<sub>2</sub>AuScCl<sub>6</sub> as shown in Fig. 17(a) and (b).

The red curve exhibits an improved and delayed current drop, indicating enhanced charge separation and reduced carrier recombination. Although the maximum current density is slightly lower than the initial case, the extended voltage range suggests an overall improvement in device efficiency. The final curve exhibits an improved and delayed current drop, indicating enhanced charge separation and reduced carrier recombination. Although the maximum current density is slightly lower than the initial case, the extended voltage range suggests an overall improvement in device efficiency.<sup>74</sup> Their maximum QE initial value is 99.91% and final value 99.81% measured at 360 nm for Rb<sub>2</sub>AuScBr<sub>6</sub> and QE initial value 99.99% and final value 99.84% at 410 nm for Rb<sub>2</sub>AuScCl<sub>6</sub> across both curves. In the visible spectrum (especially in the range of 360–450 nm), optimal QE of 100% is achieved for both materials. It is important to highlight that (as shown in Fig. 17(c) and (d)), QE reaches near 100% for both initial and final curves in most of the visible spectrum region, although after the wavelength of 700 nm for (Rb<sub>2</sub>AuScBr<sub>6</sub>) and 650 nm for (Rb<sub>2</sub>AuScCl<sub>6</sub>), QE drops dramatically.

However, there is a decrease in the QE for both solar cells at longer wavelengths due to recombination, which occurs when

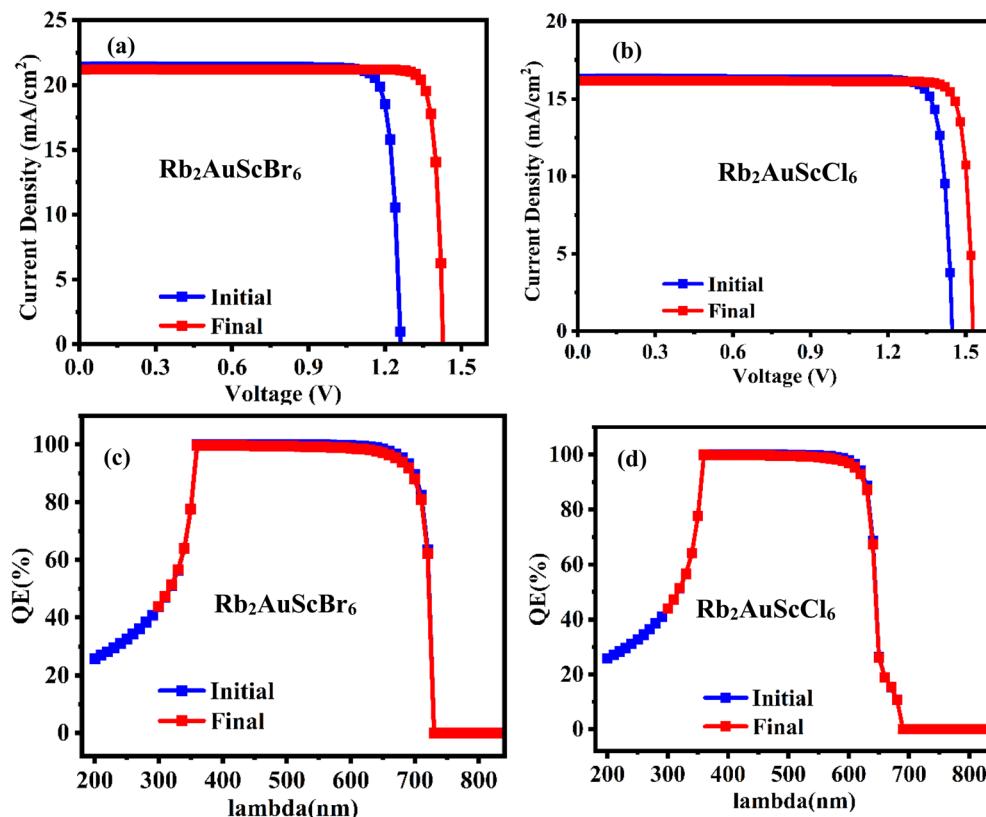


Fig. 17 (a and b)  $J$ - $V$  characteristics and (c and d) QE curve of  $\text{Rb}_2\text{AuScBr}_6$  and  $\text{Rb}_2\text{AuScCl}_6$ -baesd absorber initial and final devices.

charge carriers do not pass into an external circuit. The same processes that influence the collection probability also affect QE. For example, changes to the front surface can affect the carriers that are produced near the surface. High doping on the front surface layers can lead to free carrier absorption, which also has an increase in absorption, leading to a decrease in the QE in longer wavelengths.<sup>75</sup>

### 3.15. Final devices after optimization

Initially, the devices were configured as (ITO/IGZO/Rb<sub>2</sub>AuScBr<sub>6</sub>/CBTS/Ni) and (ITO/WS<sub>2</sub>/Rb<sub>2</sub>AuScCl<sub>6</sub>/CBTS/Ni). For the Br-based absorber, IGZO exhibited superior electron transport performance with a PCE of 23.90%. Upon optimizing absorber layer parameters—including acceptor density, electron affinity, defect density, series resistance, shunt resistance, and temperature—the highest PCE of 25.81% was achieved at an acceptor density of 10<sup>18</sup> cm<sup>-3</sup> using IGZO as the ETL.

Further improvement was observed by replacing IGZO with alternative ETLs, when the acceptor density was maintained at 10<sup>18</sup> cm<sup>-3</sup>, TiO<sub>2</sub>, ZnO, and WS<sub>2</sub> offered enhanced PCEs of 27.49%, 27.37%, and 27.30%, respectively. Among them, TiO<sub>2</sub> demonstrated the best performance, leading to the final optimized device structure for the Br-based absorber:

Glass/ITO (0.500  $\mu\text{m}$ )/TiO<sub>2</sub> (0.030  $\mu\text{m}$ )/Rb<sub>2</sub>AuScBr<sub>6</sub> (1.200  $\mu\text{m}$ )/CBTS (0.100  $\mu\text{m}$ )/Ni (5.5 eV), with a PCE of 27.49% at a defect density of 10<sup>15</sup> cm<sup>-3</sup>.

On the other hand (Fig. 18), the Cl-based absorber initially showed the best performance with WS<sub>2</sub> as the ETL, yielding a PCE of 20.98%. After acceptor density optimization (10<sup>17</sup> cm<sup>-3</sup>), the PCE improved to 22.41% at a defect density of 10<sup>15</sup> cm<sup>-3</sup>. This confirmed the final optimized device configuration as: Glass/ITO (0.500  $\mu\text{m}$ )/WS<sub>2</sub> (0.030  $\mu\text{m}$ )/Rb<sub>2</sub>AuScCl<sub>6</sub> (1.200  $\mu\text{m}$ )/CBTS (0.100  $\mu\text{m}$ )/Ni (5.5 eV).

### 3.16. Comparison with other works

In comparison with previously reported theoretical studies on lead-free perovskite solar cells, the present work demonstrates outstanding photovoltaic (PV) performance, particularly in devices based on the Rb<sub>2</sub>AuScBr<sub>6</sub> and Rb<sub>2</sub>AuScCl<sub>6</sub> perovskite absorbers. The optimized structure ITO/TiO<sub>2</sub>/Rb<sub>2</sub>AuScBr<sub>6</sub>/CBTS/Ni achieves a maximum PCE of 27.49%, with a  $V_{\text{oc}}$  of 1.428 V, ( $J_{\text{sc}}$ ) of 21.280 mA cm<sup>-2</sup>, and FF of 89.951%. Similarly, structures incorporating ZnO and WS<sub>2</sub> as ETLs, ITO/ZnO/Rb<sub>2</sub>AuScBr<sub>6</sub>/CBTS/Ni and ITO/WS<sub>2</sub>/Rb<sub>2</sub>AuScBr<sub>6</sub>/CBTS/Ni—achieved high PCEs of 27.37% and 27.30%, respectively. These performances significantly surpass those of other reported lead-free configurations. For instance, devices such as ITO/PCBM/KgeCl<sub>3</sub>/CBTS/Ni<sup>76</sup> and FTO/C<sub>60</sub>/KgeCl<sub>3</sub>/PEDOT:PSS/Ni<sup>77</sup> exhibited lower efficiencies of 21.79% and 20.46%, respectively. Furthermore, structures like FTO/ZnO/KsnI<sub>3</sub>/CuI/Au<sup>78</sup> PCE of (20.99%), ITO/IGZO/CsSnCl<sub>3</sub>/CBTS/Au PCE of (21.07%), and ITO/WS<sub>2</sub>/CsSnCl<sub>3</sub>/CBTS/Au<sup>79</sup> PCE of (21.32%) also reported considerably lower PCE values. Even the FTO/PCBM/CsSnCl<sub>3</sub>/



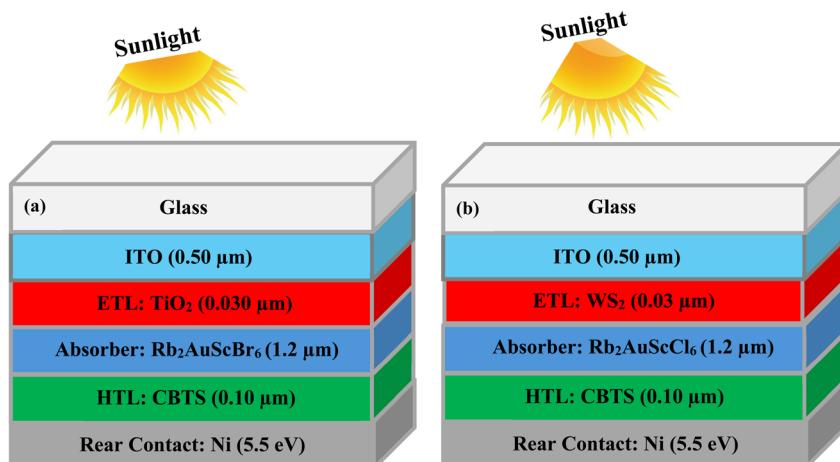


Fig. 18 The final device configuration of the absorber (a)  $\text{Rb}_2\text{AuScBr}_6$  and (b)  $\text{Rb}_2\text{AuScCl}_6$ -based PSC.

Table 4 The comparison of PV parameters of  $\text{Rb}_2\text{AuScBr}_6$ -and  $\text{Rb}_2\text{AuScCl}_6$ -based solar cells

Optimized devices	Types	$V_{oc}$ (V)	$J_{sc}$ ( $\text{mA cm}^{-2}$ )	FF (%)	PCE (%)	Ref.
ITO/TiO <sub>2</sub> /Rb <sub>2</sub> AuScBr <sub>6</sub> /CBTS/Ni	Theo	1.428	21.280	89.951	27.49	This work
ITO/ZnO/Rb <sub>2</sub> AuScBr <sub>6</sub> /CBTS/Ni	Theo	1.428	21.209	90.342	27.37	This work
ITO/WS <sub>2</sub> /Rb <sub>2</sub> AuScBr <sub>6</sub> /CBTS/Ni	Theo	1.426	21.280	89.951	27.30	This work
ITO/WS <sub>2</sub> /Rb <sub>2</sub> AuScCl <sub>6</sub> /CBTS/Ni	Theo	1.210	22.517	83.055	22.41	This work
ITO/PCBM/K <sub>2</sub> GeCl <sub>3</sub> /CBTS/Ni	Theo	0.6745	41.405	78.02	21.79	72
FTO/C <sub>60</sub> /K <sub>2</sub> GeCl <sub>3</sub> /PEDOT:PSS/Ni	Theo	0.632	41.13	78.71	20.46	73
FTO/ZnO/KNi <sub>3</sub> /CuI/Au	Theo	1.44	17.06	85.24	20.99	74
ITO/IGZO/CsSnCl <sub>3</sub> /CBTS/Au	Theo	1.02	26.14	78.69	21.07	30
ITO/WS <sub>2</sub> /CsSnCl <sub>3</sub> /CBTS/Au	Theo	1.01	25.92	81.33	21.32	30
FTO/PCBM/CsSnCl <sub>3</sub> /PTAA/Au	Theo	1.30	15.34	89.90	17.93	75

PTAA/Au<sup>80</sup> configuration yielded a much lower efficiency of 17.93%. Notably, the  $\text{Rb}_2\text{AuScCl}_6$ -based device.

ITO/WS<sub>2</sub>/Rb<sub>2</sub>AuScCl<sub>6</sub>/CBTS/Ni only achieved a PCE of 22.41%, which is substantially lower than that of the  $\text{Rb}_2\text{AuScBr}_6$ -based devices. These results clearly indicate that the combination of IGZO, TiO<sub>2</sub>, or ZnO as ETLs, CBTS as the HTL, and  $\text{Rb}_2\text{AuScBr}_6$  as the absorber forms a highly promising structure for next-generation, high-efficiency, lead-free perovskite solar cells (Table 4).

## 4. Conclusion

This study systematically optimized lead-free PSCs employing  $\text{Rb}_2\text{AuScBr}_6$  and  $\text{Rb}_2\text{AuScCl}_6$  absorbers. Initial screening identified ITO/IGZO/Rb<sub>2</sub>AuScBr<sub>6</sub>/CBTS/Ni and ITO/WS<sub>2</sub>/Rb<sub>2</sub>AuScCl<sub>6</sub>/CBTS/Ni as the best-performing baseline architectures. Device performance was then enhanced through absorber thickness optimization, back-contact work function tuning, doping concentration adjustment, and defect density control.

For  $\text{Rb}_2\text{AuScBr}_6$ -based PSCs, an optimal absorber thickness of  $\sim 1200$  nm balanced light absorption with charge transport, achieving a peak PCE of 25.81% at an acceptor density of  $10^{18} \text{ cm}^{-3}$  and a defect density of  $10^{15} \text{ cm}^{-3}$ . Increasing the back-contact work function to 5.5 eV further improved efficiency. Substituting the IGZO ETL with TiO<sub>2</sub>, ZnO, or WS<sub>2</sub> under these

optimized conditions yielded maximum PCEs of 27.49%, 27.37%, and 27.30%, respectively, with TiO<sub>2</sub> performing best.

For  $\text{Rb}_2\text{AuScCl}_6$ -based PSCs, WS<sub>2</sub> consistently provided superior performance across all optimization stages. The highest recorded efficiency was 22.41% at an acceptor density of  $10^{17} \text{ cm}^{-3}$  and defect density of  $10^{15} \text{ cm}^{-3}$ . Both material systems demonstrated minimal performance degradation under variations in series resistance, shunt resistance, and operating temperature, confirming strong electrical and thermal stability.

The comparative analysis reveals that  $\text{Rb}_2\text{AuScBr}_6$  offers higher ultimate efficiency potential, while  $\text{Rb}_2\text{AuScCl}_6$  provides competitive performance with robust ETL compatibility. The environmentally friendly composition of both absorbers, combined with high efficiency and operational stability, underscores their suitability as sustainable alternatives to toxic lead-based perovskites.

Given their promising efficiency, thermal stability, and non-toxic composition, these devices are particularly well-suited for building-integrated photovoltaics (BIPV), where safety, stability, and aesthetic flexibility are crucial, as well as for next-generation lightweight solar modules for portable and off-grid applications. The findings emphasize that careful device engineering, especially ETL selection, doping control, and absorber layer optimization, can enable lead-free PSCs to achieve



performance levels competitive with their lead-based counterparts, paving the way for their integration into large-scale, eco-friendly solar energy systems.

## Author contributions

Md. Al-Amin: writing – original draft, data calculations, methodology, validation. A. Haque: writing – review & editing, investigation, validation. S. Mahmud: writing – review & editing, methodology, conceptualization, formal analysis, validation. M. M. Hossain: writing – review & editing, validation. M. M. Uddin: writing – review & editing, validation. M. A. Ali: writing – review & editing, supervision, project administration, validation.

## Conflicts of interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

## Data availability

The datasets generated and/or analyzed during the current study are available within the article, and the raw data are available from the corresponding author upon reasonable request.

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