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## Heterogeneous silicotungstic acid constructed via defect and morphology engineering for boosting the oxidative desulfurization of fuel oil†

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It is well-known that defect engineering and morphology engineering are key strategies for giving an impetus to the catalytic activity of catalysts. This study reports the successful regulation of oxygen vacancy ( $O_V$ ) defects and the morphology of a Keggin-type silicotungstic acid ( $SiW_{12}$ )-loaded N-doped carbon (NC) matrix, which is obtained by calcining a copolymer of acryloyloxyethyl trimethyl ammonium chloride (DAC) and acrylamide (AM) as precursors in air. It was unveiled that adjusting the proportion of AM in the copolymer could be simultaneously conducive to the targeted regulation of  $O_V$  defects of catalysts and their morphological evolution from bowls to spheres. The as-prepared  $O_V$ - $SiW_{12}$ /SNC sphere catalyst showed an excellent oxidative desulfurization (ODS) performance with  $H_2O_2$  as a green oxidant. Complete removal of DBT (2000 ppm) was achieved within 12 minutes at 60 °C with a large rate constant of 0.4055 min<sup>-1</sup>. The outstanding ODS performance was critically ascribed to the highly active W sites promoted by the abundant  $O_V$  defects, and the easy diffusion and contact between the substrate and W sites were led by the spherical structure. Moreover, the as-prepared catalyst exhibited prominent reusability. This ODS reaction was found to follow a  $HO^\cdot$  radical mechanism.

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### 1. Introduction

Despite the continuous development of the new energy industry, crude oil remains the most commonly used energy source in most industries in the modern world.<sup>1–3</sup> However, fuel reserves continue to dwindle, leading to the use of low-quality fossil fuels containing a large amount of refractory sulfides, such as thiophene (Th), dibenzothiophene (DBT), benzothiophene (BT), 4,6-dimethylbenzothiophenes (4,6-DMDBT), and other derivatives. The combustion of these sulfides could result in the release of sulfur oxides into air so as to the acid and smog, therefore posing serious threats to human health and ecosystems.<sup>4–6</sup> Moreover, thiophene compounds can poison catalysts used for automobile exhaust treatment and corrode refining equipment.<sup>7</sup> Currently, the limit for sulfur content in liquid fuels are becoming increasingly strict in various countries (even less than 60 ppb for organic sulfur compounds).<sup>8</sup> Therefore, it is urgent to develop highly efficient and feasible desulfurization techniques.

Although traditional hydrodesulfurization (HDS) has high efficiency for removing mercaptan, sulfide and disulfide from

fuel feedstocks, it finds difficulty in removing refractory sulfides (such as DBT and its derivatives), and it requires harsh conditions (such as high temperature, high pressure, and substantial hydrogen consumption).<sup>4</sup> Recently, some non-hydrodesulfurization methods, including extractive desulfurization (EDS), adsorptive desulfurization (ADS), biological desulfurization (BDS), and oxidative desulfurization (ODS), have been developed to supplement HDS for the removal of refractory sulfides.<sup>4,9,10</sup> In particular, ODS is an attractive method with strong elimination ability for refractory sulfides under mild operating conditions, and hence, it is expected to produce ultra-clean fuels.<sup>9,11</sup> During ODS process, aromatic sulfur compounds are usually oxidized into sulfones, which could be then easily separated and recovered through adsorption, crystallization, rectification, extraction, and so on.<sup>9,11–13</sup>

A cost-effective and highly active catalyst is always a key factor for boosting the commercial viability of ODS technology.<sup>1</sup> To date, various catalysts, including polyoxometalates (POMs),<sup>14,15</sup> metal–organic frameworks (MOFs),<sup>16,17</sup> transition metal oxides ( $VO_x$ ,  $WO_x$ , and  $MoO_x$ ) or nitrides ( $W_2N$  and  $Mo_2N$ ),<sup>1,18–21</sup> transition metal carbides ( $Mo_2C$  and  $W_2C$ ),<sup>22,23</sup> and transition metals ( $Co$ ),<sup>24</sup> have been widely explored for ODS of fuel oil. Among them, POMs, as a class of metal–oxygen clusters consisting of early transition metals (W, V, Mo, etc.) in their high oxidation states, have received significant attention as effective catalysts owing to their appealing properties, such as their particular structure, excellent redox activity, good stability, and mild reaction conditions.<sup>25,26</sup> Notably, the heterogeneous POMs with  $SiO_2$ ,

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porous carbon materials, and MOFs as supports, are attracting increasingly widespread interest owing to more exposed active sites triggered by the good distribution of active components.<sup>27,28</sup> Morphology engineering is always a good strategy for improving the catalytic activity of catalysts. Generally, the spherical shape has the advantages of good fluidity and high specific surface area, which makes it easier for reactant molecules to come into contact with the active center, thus exhibiting an excellent catalytic effect.<sup>27,29</sup> Furthermore, defect engineering has been found to be promising for greatly improving the performance of catalysts.<sup>5,30-33</sup> Typically, the oxygen vacancy ( $O_V$ ) defect can generate favorable effects for regulating the surface-electron state and boosting the redox reaction (such as the oxidative desulfurization reaction).<sup>5</sup> Ma *et al.*<sup>34</sup> synthesized an  $O_V$ -defective catalyst,  $H_4PVMo_4W_7O_{40}@\text{rht-MOF-1-De}$ , using a one-pot method for fuel oil desulfurization. It exhibited high catalytic activity and recyclability, achieving 99% DBT and 96% 4,6-DMDBT removal under optimized conditions. In the context of oxidative desulfurization (ODS) reactions, Jiao *et al.*<sup>1</sup> discovered that the presence of oxygen vacancies significantly promoted the generation of active intermediates, thereby enhancing the overall rate of the ODS reaction. This observation underscores the crucial role of oxygen vacancies in facilitating efficient sulfur removal.

Herein, a novel strategy for effectively modulating oxygen vacancy ( $O_V$ ) defects and the morphology of a Keggin-type silicotungstic acid ( $\text{SiW}_{12}$ )-loaded N-doped carbon (NC) matrix is developed by adjusting the content of acrylamide (AM) in a copolymer of acryloyloxyethyl trimethyl ammonium chloride (DAC) and acrylamide (AM) (abbreviated as CPAD) as precursors. Finally, by *in situ* low-temperature calcination of CPAD in air, a spherical catalyst with abundant  $O_V$  defects ( $O_V\text{-SiW}_{12}/\text{SNC}$ ) was successfully prepared and applied to the deep ODS of fuel oil. The as-prepared  $O_V\text{-SiW}_{12}/\text{SNC}$  catalyst shows an excellent oxidative desulfurization (ODS) performance, wonderful adaptability to fuel oils with a wide range of sulfur concentrations, and remarkable reusability. In addition, a series of radical scavenging studies were performed to elucidate the ODS mechanism of  $O_V\text{-SiW}_{12}/\text{SNC}$ .

## 2. Experimental

### 2.1. Materials

Acrylamide (AM, AR,  $C_3H_5NO$ , Tianjin Dengfeng Chemical Reagent Factory); acryloyloxyethyl trimethyl ammonium

chloride (DAC, 80 wt% in  $H_2O$ ,  $C_8H_{16}ClNO_2$ , Shanghai Maclean Biochemical Technology Co., Ltd); silicotungstic acid ( $H_4\text{-SiW}_{12}O_{40}\cdot xH_2O$ , abbreviated as  $\text{SiW}_{12}$ , AR, Shanghai Maclean Biochemical Technology Co., Ltd); dibenzothiophene (DBT, ≥99%,  $C_{12}H_8S$ , Aladdin); 4,6-dimethyl dibenzothiophene (4,6-DMDBT) (97%,  $C_{14}H_{12}S$ , Aladdin); thiophene (BT, 99%,  $C_4H_4S$ ); *n*-octane (AR, Tianjin Damao Chemical Reagent Factory);  $H_2O_2$  aqueous solution (AR, 30 wt%, Tianjin Damao Chemical Reagent Factory); and acetonitrile (AR,  $CH_3CN$ , Tianjin Concord Technology Co., Ltd). All the other chemicals and reagents are commercially available and analytically pure (see Section 1 in the (ESI)<sup>†</sup> for more details).

### 2.2. Preparation of catalysts

First, copolymerized crosslinked microspheres (CPAD) of acrylamide (AM) and acryloyloxyethyl trimethyl ammonium chloride (DAC) were prepared by applying the reverse suspension polymerization method (see Section 2 of the (ESI)<sup>†</sup> for more details). Then, a certain amount of silicotungstic acid ( $\text{SiW}_{12}$ ) can be combined with CPAD through the electrostatic interaction to produce the spherical precursor  $\text{SiW}_{12}/\text{CPAD}$  (Fig. S1<sup>†</sup>). Finally,  $\text{SiW}_{12}/\text{CPAD}$  is calcined at different temperatures to obtain spherical catalysts, *i.e.*  $\text{SiW}_{12}/\text{CPAD-300}$ ,  $\text{SiW}_{12}/\text{CPAD-400}$ ,  $\text{SiW}_{12}/\text{CPAD-500}$ , and  $\text{SiW}_{12}/\text{CPAD-700}$ , where the numbers represent calcination temperatures. Importantly, during the synthesis process, the feed ratio of DAC and AM is explored in the range of 4 : 0-4 : 3 to regulate the morphology of the final calcination products. Unless otherwise specified, the DAC/AM feed ratio is determined to be 4 : 2, and the corresponding precursor and spherical  $\text{SiW}_{12}/\text{CPAD-400}$  product are denoted as  $\text{SiW}_{12}/\text{CPAD}$  and  $O_V\text{-SiW}_{12}/\text{SNC}$ , respectively. Besides, to highlight  $O_V\text{-SiW}_{12}/\text{SNC}$ , the obtained calcinating products of pure  $\text{SiW}_{12}$  and the  $\text{SiW}_{12}/\text{CPAD}$  precursor with a feed molar ratio of DAC to AM of 4 : 0 at 400 °C are marked as  $\text{SiW}_{12-400}$  and  $\text{SiW}_{12}/\text{NC}$ , respectively. The preparation process of  $O_V\text{-SiW}_{12}/\text{SNC}$  is schematically shown in Fig. 1, and the molecular structures of DAC, AM, MBA, and CPAD are depicted in Fig. S2.<sup>†</sup>

### 2.3. Characterizations

Fourier Infrared Spectrometer (FT-IR, KBr method, L1600300 Spectrum Two Lita Model, Liantrisant, UK); UV-Visible Spectrophotometer (UV-Vis, UV-2802, Unico, China); High

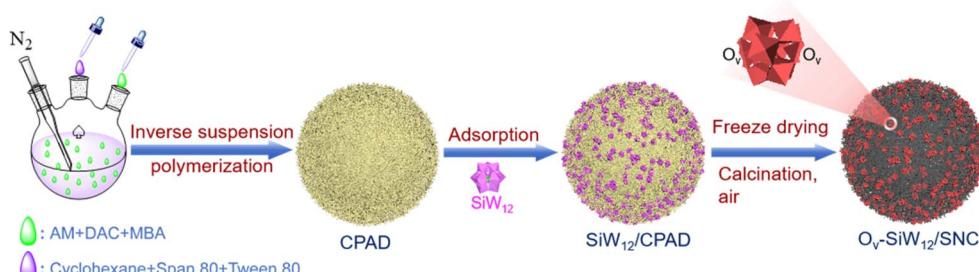


Fig. 1 Preparation process of  $O_V\text{-SiW}_{12}/\text{SNC}$ .



Performance Liquid Chromatograph (HPLC, Model Classical 3100, Dalian Yi lite Analytical Instrument Co., Ltd, Dalian, China); element analyser (EA, PE2400 Series II CHNS/O type, Qingdao Huaqing Group Co., Ltd China); and a Powder X-ray diffractometer (XRD, Empyrean, PANalytical B.V., Holland, Cu K( $\alpha$ ) radiation ( $\lambda = 1.5418 \text{ \AA}$ , 40 kV and 40 mA) over a range of  $2\theta = 5\text{--}90^\circ$ ). Electron paramagnetic resonance spectroscopy (EPR) was performed using a MiniScope MS 5000 spectrometer (Magnettech, Germany) in the dark at room temperature. Scanning electron microscopy (SEM, Zeiss Merlin Compact, Germany); X-ray photoelectron spectroscopy (XPS, Thermo Scientific K-Alpha+, USA); Synchronous thermal analysis (TG-DSC, LF-1100, Mettler Toledo Instruments Co., Ltd, Shanghai, China, air atmosphere, a heating rate of  $5 \text{ }^\circ\text{C min}^{-1}$ ); and High-performance liquid chromatography (HPLC, EClassical 3100, Dalian Yelite Analytical Instrument Co., Ltd, Dalian, China). Inductively coupled plasma optical emission spectrometry (ICP-OES, Agilent 5110, USA) was used to determine the W content.

#### 2.4. ODS experiments

First, the model oil with a sulfur content of 500–4000 ppm (parts per million by weight) was produced by dissolving DBT (or BT, 4,6-DMDBT) into *n*-octane. The extraction-catalyzed ODS reaction was carried out in a two-phase system consisting of model oil and acetonitrile. Specifically, 20 mL of the model oil and 20 mL of acetonitrile were mixed and stirred at the reaction

temperature for 20 min to achieve extraction equilibrium. Subsequently, an ODS reaction occurred, followed by the addition of  $\text{O}_\text{V}\text{-SiW}_{12}/\text{SNC}$  and 30 wt% of  $\text{H}_2\text{O}_2$  aqueous solution with a certain  $\text{H}_2\text{O}_2/\text{sulfur}$  (O/S) molar ratio into the above two-phase system. During the reaction, trace samples were periodically removed from the two phases and then diluted with *n*-octane and acetonitrile to detect the residual sulfur concentration by employing the HPLC external standard method (see Section 3 of the ESI† for details). At the end of the reaction, the catalyst was collected, washed with acetonitrile and ethanol, dried at  $50 \text{ }^\circ\text{C}$ , and then recovered for reuse.

### 3. Results and discussion

#### 3.1. Characteristics of catalysts

The morphology of the calcination products with the feed ratios of DAC and AM in the range of 4 : 0–4 : 3 at  $400 \text{ }^\circ\text{C}$  was observed by SEM. As displayed in Fig. 2(a–c) and S3,† with the feed DAC/AM ratio in the range of 4 : 0–4 : 3 during the preparation of precursors, the morphology of the calcination products varies from bowl shape with thin walls to the bowl with increased wall thickness and then to spherical structure, which may be related to the thermal decomposition of CPAD microspheres. Herein, the feed DAC/AM ratio is determined to be 4 : 2 to guarantee the spherical  $\text{O}_\text{V}\text{-SiW}_{12}/\text{SNC}$  catalyst. Moreover, the EDX element mapping in Fig. 2(d) shows that the C, N, O, Si, and W elements are evenly distributed in the  $\text{O}_\text{V}\text{-SiW}_{12}/\text{SNC}$  microspheres,

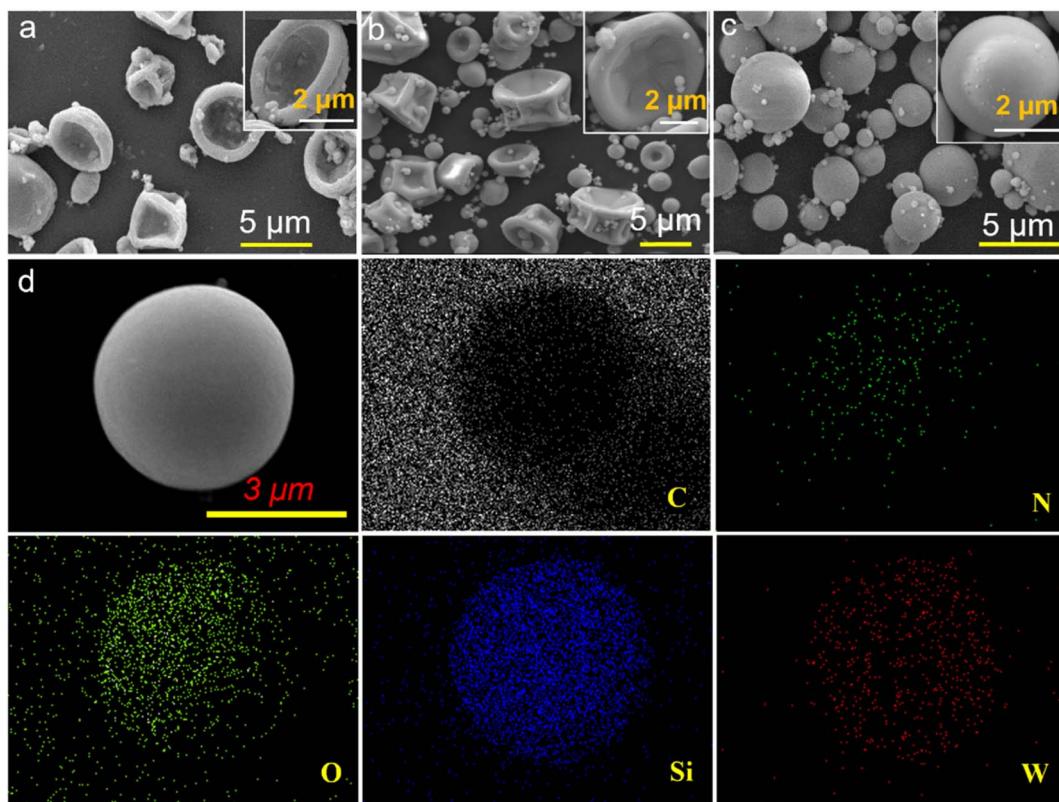


Fig. 2 SEM images of  $\text{O}_\text{V}\text{-SiW}_{12}/\text{SNC}$  derived from different DAC/AM feed molar ratios of (a) 4 : 0, (b) 4 : 1, (c) 4 : 2 and (d) HADDF and EDX elemental mapping images of  $\text{O}_\text{V}\text{-SiW}_{12}/\text{SNC}$ .



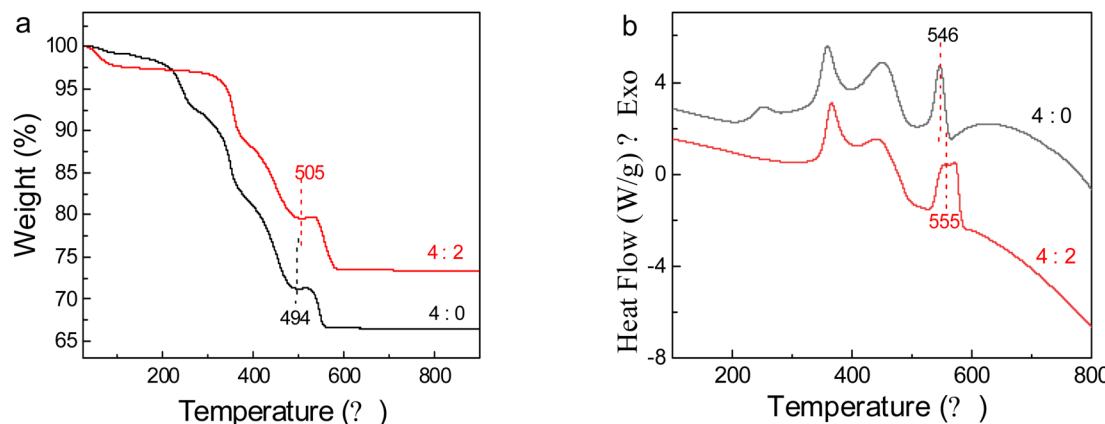


Fig. 3 (a) TG and (b) DSC curves of precursors  $\text{SiW}_{12}/\text{CPAD}$  with feed DAC/AM molar ratios of 4 : 0 and 4 : 2 (in air).

indicating the even distribution of  $\text{O}_\text{v}-\text{SiW}_{12}$  in the spherical NC matrix. Furthermore, the  $\text{SiW}_{12}/\text{CPAD}$  precursors with different DAC/AM feed molar ratios of 4 : 2 and 4 : 0 present similar TG and DSC curves (Fig. 3), in which the precursor with a DAC/AM feed molar ratio of 4 : 0 is named  $\text{SiW}_{12}/\text{CPAD-0}$ . The TG curves of  $\text{SiW}_{12}/\text{CPAD}$  show four distinct weight loss stages. The weight loss below 280 °C is owing to the removal of physically and chemically adsorbed water and decomposition of MBA in CPAD; the weight loss at 280–400 °C with an exothermic peak at 365 °C is ascribed to the damage of the quaternary ammonium group<sup>35,36</sup> and the loss of crystal water in  $\text{H}_4\text{SiW}_{12}\text{O}_{40} \cdot x\text{H}_2\text{O}$ ,<sup>27</sup> the weight loss at 400–505 °C along with an exothermic peak at 441 °C is attributed to the combustion of residual carbon skeleton and the deprotonation of  $\text{H}_4\text{SiW}_{12}\text{O}_{40}$  into  $\text{SiW}_{12}\text{O}_{38}$ ,<sup>27,35,37</sup> which can be further demonstrated by the color of products at 400 and 500 °C (Fig. S4a†); the weight loss at 506–600 °C along with two exothermic peaks at 555 °C and 572 °C is accredited to the transformation of  $\text{SiW}_{12}$  to silicon- and tungsten-oxides.<sup>38,39</sup> Compared to the TG and DSC curves of the  $\text{SiW}_{12}/\text{CPAD-0}$  precursor, it is depicted that the thermodecomposed temperatures of the  $\text{SiW}_{12}/\text{CPAD}$  precursor in each pyrolysis stage increase owing to the addition of AM, which could also be unmasked by comparing their colors at 300–500 °C (Fig. S4†). Therefore, when the temperature increases to 400 °C, the residual weight of  $\text{SiW}_{12}/\text{CPAD}$  (87.9%) is greater than that of  $\text{SiW}_{12}/\text{CPAD-0}$  (80.8%) (Fig. 3a), which favors better preservation of the spherical carbon skeleton after calcining  $\text{SiW}_{12}/\text{CPAD}$ .

The FT-IR spectrum of the CPAD (Fig. S5†) shows that not only the characteristic absorption peaks of DAC (at 1164  $\text{cm}^{-1}$ , 1479  $\text{cm}^{-1}$  and 1740  $\text{cm}^{-1}$  corresponding to the stretching vibration of C–O,  $-\text{CH}_2-\text{N}^+$  and C=O, respectively)<sup>40</sup> but also those of AM (at 1667  $\text{cm}^{-1}$  corresponding to the stretching vibration of  $-\text{NH}_2$ ) appear,<sup>41</sup> confirming the formation of the copolymerized crosslinked microspheres CPAD. In the FT-IR spectrum of  $\text{SiW}_{12}/\text{CPAD}$ , in addition to peaks of CPAD, the characteristic absorption peaks of  $\text{SiW}_{12}$  are found at 1017, 973, 920, 881 and 796  $\text{cm}^{-1}$  ascribed to the stretching vibration of Si–O<sub>a</sub>, W–O<sub>d</sub>, W–O<sub>b</sub>–W, O–O and W–O<sub>c</sub>–W bonds, respectively,<sup>42,43</sup> verifying the successful combination of  $\text{SiW}_{12}$  onto CPAD.

Fig. 4a illustrates the FT-IR spectra of the calcination products of  $\text{SiW}_{12}/\text{CPAD}$  at different temperatures. When calcinating at 300 °C, the peaks of  $\text{SiW}_{12}$  remain basically unchanged, but the peak of AM in CPAD at 1667  $\text{cm}^{-1}$  is greatly reduced, suggesting that the structure of CPAD has changed. After calcinating  $\text{SiW}_{12}/\text{CPAD}$  at 400 °C, the peaks assigned to AM and DAC in CPAD have almost gone, and the peaks of  $\text{SiW}_{12}$  at 1017, 973, 920, and 796  $\text{cm}^{-1}$  remain basically the same except for the peak at 880  $\text{cm}^{-1}$  corresponding to the O–O bond that almost disappears, indicating that not only the structure of CPAD is destroyed owing to carbonization (see the blackened product shown in Fig. S4†), but also that of  $\text{SiW}_{12}$  is damaged to some extent owing to the formation of oxygen vacancies, which is further supported by the presented symmetric peak at  $g = 2.003$  in the electron paramagnetic resonance (EPR) spectrum compared with the  $\text{SiW}_{12}/\text{CPAD}$  precursor and its calcined product at 300 °C (Fig. S6†). As the calcination temperature exceeds 500 °C, the peaks of both CPAD and  $\text{SiW}_{12}$  disappear completely, and only a large, wide peak appears at about 790  $\text{cm}^{-1}$  corresponding to the W–O–W bond.<sup>27</sup> This significant structural change is also disclosed by XRD patterns. As shown in Fig. 4b, the calcination products at 400 and 300 °C exhibit XRD patterns similar to that of the  $\text{SiW}_{12}/\text{CPAD}$  precursor, with almost no diffraction peaks, indicating the uniform dispersion of  $\text{SiW}_{12}$  in the CPAD matrix or its derived carbon materials<sup>39,44,45</sup> and the preservation of the basic  $\text{SiW}_{12}$  structure even after calcination at 300 or 400 °C in air, which agrees with the literature.<sup>5,27</sup> However, as the calcination temperature exceeds 500 °C, the XRD patterns of the calcination products are distinctly different, and some clear diffraction peaks appear, corresponding to the monochromatic  $\text{WO}_3$  phase (PDF # 71-0131), which comes from the oxidation and decomposition of  $\text{SiW}_{12}$ . The XRD results are in good agreement with those of the FT-IR spectra. To sum up, the calcination temperature of 400 °C is indispensable for ensuring the basic structure of  $\text{SiW}_{12}$  while creating partial oxygen vacancy defects.

Furthermore, X-ray photoelectron spectroscopy (XPS) was performed to evaluate the chemical environment and composition of  $\text{O}_\text{v}-\text{SiW}_{12}/\text{SNC}$ , as shown in Fig. 4c and S7.† The XPS survey spectrum (Fig. S7a†) shows the presence of C, O, N, W,

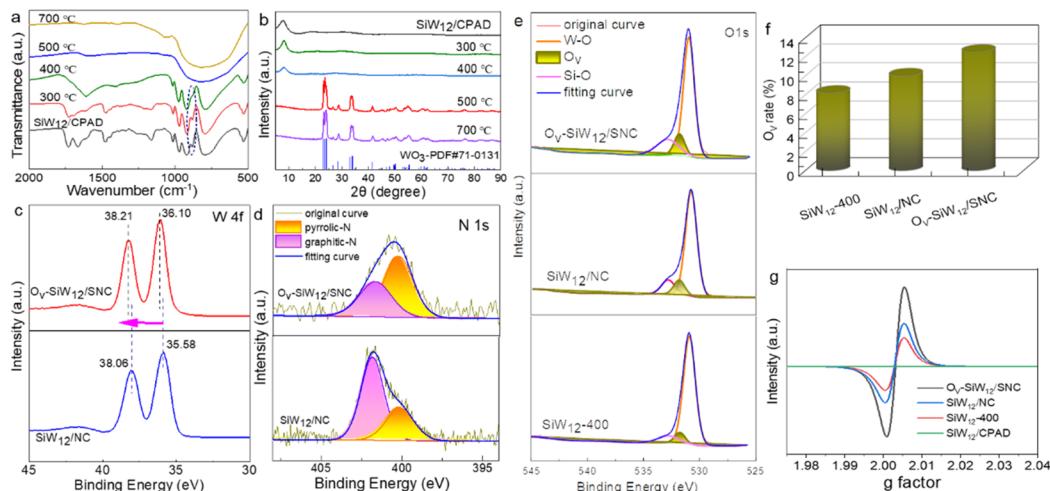


Fig. 4 (a) FT-IR spectra and (b) XRD patterns of SiW<sub>12</sub>/CPAD, and its annealing products at different temperatures. High resolution XPS spectra of (c) W 4f and (d) N 1s. (e) High resolution XPS spectra of O 1s in the specimens. (f) Proportions of O<sub>v</sub> vacancies for three specimens deduced from (e) and (g) EPR spectra of the specimens.

and Si elements in accordance with the EDX element mapping results. In the high resolution W 4f spectrum of O<sub>v</sub>-SiW<sub>12</sub>/SNC (Fig. 4c), two split peaks at 36.10 and 38.21 eV respectively correspond to W<sup>6+</sup> of SiW<sub>12</sub>,<sup>5</sup> and are redshifted compared to SiW<sub>12</sub>/NC, suggesting that the electronic structure of W elements changes. In addition, it is clearly found in the N 1s spectra of O<sub>v</sub>-SiW<sub>12</sub>/SNC and SiW<sub>12</sub>/NC (Fig. 4d) that two peaks at 400.1 and 401.8 eV are ascribed to pyrrolic N and graphitic N, respectively,<sup>46</sup> and the ratio of pyrrolic N to graphitic N for O<sub>v</sub>-SiW<sub>12</sub>/SNC is notably greater than that for SiW<sub>12</sub>/NC. The coordination of pyrrolic N with metal (W) atoms can regulate its electronic structure and thus promote its catalytic activity.<sup>47</sup> Hence, a higher ratio of pyrrolic N to graphitic N for O<sub>v</sub>-SiW<sub>12</sub>/SNC is propitious to facilitate its catalytic activities. The O 1s spectrum (Fig. 4e) can be fitted into three peaks at 530.9 eV, 531.8 eV and 532.8 eV, corresponding to the W–O, O<sub>v</sub>, and Si–O bonds, respectively.<sup>48,49</sup> Importantly, it can be found from Fig. 4e and f that the O<sub>v</sub> contents of various specimens decrease in the order O<sub>v</sub>-SiW<sub>12</sub>/SNC > SiW<sub>12</sub>/NC > SiW<sub>12</sub>-400, which is also verified by changes in the intensity of signal peaks of O<sub>v</sub> defects at *g* = 2.003 observed in the EPR spectrum depicted in Fig. 4g. Therefore, the addition of AM to the precursor facilitates the formation of more O<sub>v</sub> defects, which could modulate the electronic structure of the active W sites in SiW<sub>12</sub>, thus accelerating the decomposition of H<sub>2</sub>O<sub>2</sub> and improving the ODS performance of O<sub>v</sub>-SiW<sub>12</sub>/SNC.

### 3.2. ODS performance evaluation

**3.2.1 ODS performances of different catalytic systems.** The ODS performance of the different reaction systems is shown in Fig. 5a. It can be observed from Fig. 5a that the catalyst and H<sub>2</sub>O<sub>2</sub> are essential in the extraction–oxidation desulfurization model. Concurrently, in the absence of H<sub>2</sub>O<sub>2</sub>, O<sub>v</sub>-SiW<sub>12</sub>/SNC shows an adsorption capacity of about 8.96 mg g<sup>-1</sup> towards DBT. Notably, it is still found that in the presence of H<sub>2</sub>O<sub>2</sub>, the ODS performance of catalysts follows the order O<sub>v</sub>-SiW<sub>12</sub>/SNC >

SiW<sub>12</sub>-400 > pure SiW<sub>12</sub>. According to Fig. S8a,<sup>†</sup> SiW<sub>12</sub>-400 possesses an XRD pattern similar to that of pure SiW<sub>12</sub>, indicating that they have almost the same structure. Moreover, SiW<sub>12</sub>-400 exhibits O<sub>v</sub> defects owing to calcination, but there are no O<sub>v</sub> defects in pure SiW<sub>12</sub> (Fig. S8b<sup>†</sup>), demonstrating that SiW<sub>12</sub>-400 has a higher desulfurization rate than pure SiW<sub>12</sub>. Thus, O<sub>v</sub>-SiW<sub>12</sub>/SNC presents better ODS performance than SiW<sub>12</sub>-400, which is related not only to the excellent dispersion of SiW<sub>12</sub> in the N-doped carbon matrix and the uniform suspension of O<sub>v</sub>-SiW<sub>12</sub>/SNC in the acetonitrile phase (Fig. S9<sup>†</sup>) but also to more O<sub>v</sub> defects of O<sub>v</sub>-SiW<sub>12</sub>/SNC than that of SiW<sub>12</sub>-400 (Fig. 4g).

Furthermore, it is surprising to find that with the feed DAC/AM ratio in the range of 4:0–4:3 during the preparation of precursors, not only the morphology of the corresponding calcined products varies from bowl shape to spherical structure (as shown in Fig. S3<sup>†</sup>), but also the O<sub>v</sub> defects of calcined products increase until the precursor with the feed DAC/AM ratio of 4:2 produces the almost same number of O<sub>v</sub> defects as that with 4:3 (Fig. 5b). Accordingly, with the addition of AM, fuel oil achieves ultra-deep desulfurization in a short time with a lower O/S ratio (3:1). Moreover, with the increased feed amount of AM, the feed DAC/AM ratio was stretched up in the range of 4:0–4:3, and the ODS performance of the corresponding calcined products becomes better and better owing to the fast mass transfer process supported by the spherical morphology, more O<sub>v</sub> defects induced by the introduction of AM, and the modulated electronic structure of W active sites by O<sub>v</sub> defects (Fig. 4c). In view of almost the same desulfurization ratio of the sample with a feed DAC/AM ratio of 4:2 as that with 4:3, the feed DAC/AM ratio is optimized as 4:2.

In addition, the ODS performances of the calcinated products of the precursor SiW<sub>12</sub>/CPAD with a DAC/AM feed molar ratio of 4:2 at different temperatures are explored to uncover the particularity of the calcination temperature of 400 °C, as shown in Fig. 5d. It is clear that too high or too low a calcination



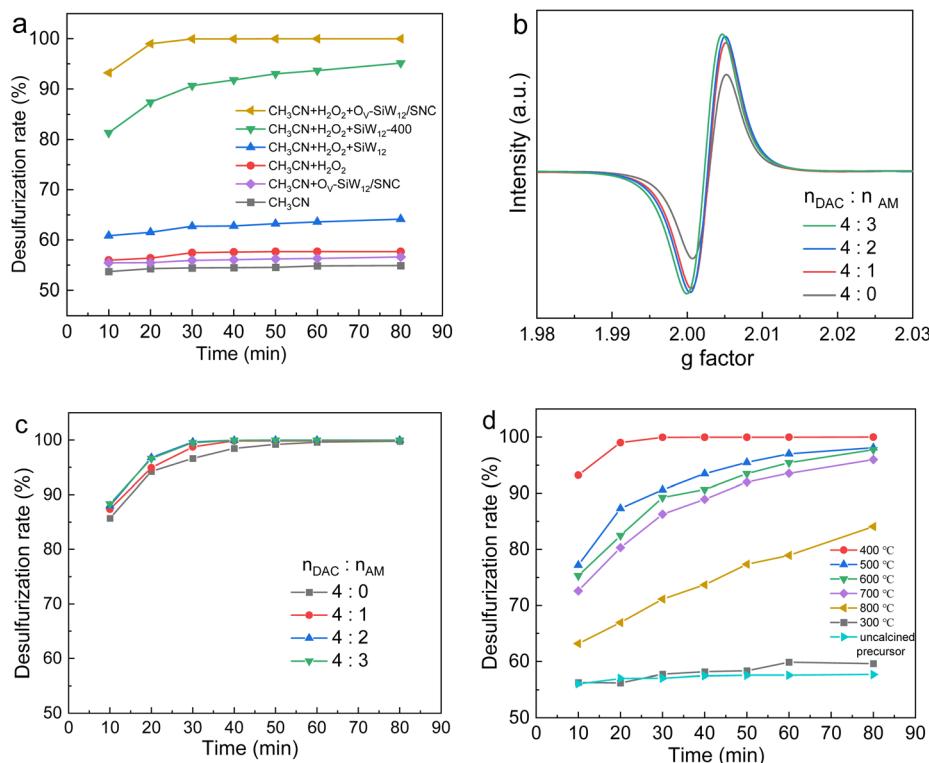


Fig. 5 ODS performances of (a) different reaction systems, (b) EPR tests and ODS performances for the calcined products (c) with different ratios of DAC to AM (calcination condition: 400 °C), and (d) at different temperatures (ODS conditions: DBT content: 500 ppm; catalysts: 0.1 g;  $n(\text{H}_2\text{O}_2) : n(\text{S}) = 3 : 1$ ;  $T = 60$  °C).

temperature is not conducive to the ODS performance of the calcinated products. Combined with FT-IR, XRD, and EPR results (Fig. 4a, b, and S6†), the structure of  $\text{SiW}_{12}$  in the calcined product at 300 °C is the same as that in the precursor, with no  $\text{O}_\text{V}$  defects, thus demonstrating a lower ODS activity. Although the Keggin structure of  $\text{SiW}_{12}$  in the calcined product at 400 °C is maintained, more  $\text{O}_\text{V}$  defects appear (Fig. S6†), resulting in excellent ODS activity. As the calcination temperature increases beyond 400 °C, the desulfurization rate decreases instead, which is related to the structural transformation of  $\text{SiW}_{12}$  into  $\text{WO}_3$  (Fig. 4b). The reduction of exposed active sites

led to the aggregation of  $\text{WO}_3$  species owing to the loss of carbon layers as a barrier during high temperature calcination (as shown in the TG result in Fig. 3a).

**3.2.2 Effects of various factors on ODS performance.** It is well known that the catalyst dosage, the molar ratio of  $\text{H}_2\text{O}_2$  to sulfur compounds (O/S), and the reaction temperature are usually the key parameters for the ODS reaction. Therefore, they were investigated to optimize the ODS reaction. As illustrated in Fig. S10† and elucidated by the corresponding discussion, the optimal catalyst dosage and the molar ratio of  $n(\text{H}_2\text{O}_2)$  to  $n(\text{S})$  are determined to be 0.2 g and 4:1, respectively.

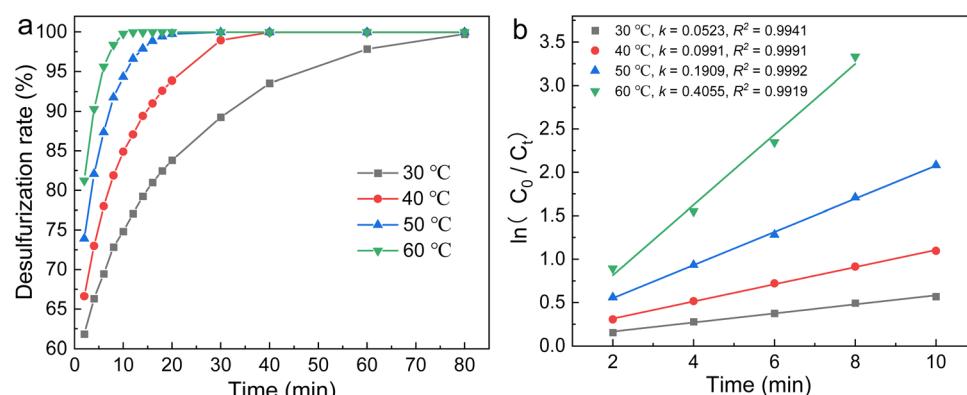


Fig. 6 (a) ODS efficiencies at different reaction temperatures and (b) pseudo-first-order kinetic curves (DBT content: 2000 ppm; catalysts: 0.2 g;  $n(\text{H}_2\text{O}_2) : n(\text{S}) = 4 : 1$ ).

Table 1 Comparison of different ODS systems in the presence of  $\text{H}_2\text{O}_2$ 

Catalyst	Reaction conditions	Time	Desulfurization rate	Ref.
HPW@UiO-66	800 ppm, 0.08 g catalysts, 20 mL mode oil, O/S = 7, $T = 60^\circ\text{C}$	90 min	100%	50
WOx@mSnO <sub>2</sub>	500 ppm, 0.1 g catalysts, 20 mL mode oil, O/S = 5, $T = 60^\circ\text{C}$	120 min	100%	51
[mim(CH <sub>2</sub> ) <sub>3</sub> COO] <sub>3</sub> PW@UiO-66	1000 ppm, 0.16 g catalysts, 20 mL mode oil, O/S = 5, $T = 70^\circ\text{C}$	60 min	100%	44
30HPW/ZrO <sub>2</sub>	500 ppm, 0.1 g catalysts, 20 mL mode oil, O/S = 4, $T = 60^\circ\text{C}$	120 min	100%	52
HPW-vim	500 ppm, 0.20 g catalysts, 20 mL mode oil, O/S = 5, $T = 50^\circ\text{C}$	30 min	100%	53
CeO <sub>2</sub> -WO <sub>x</sub> -TiO <sub>2</sub>	1154 ppm, 0.20 g catalysts, 100 mL mode oil, $T = 60^\circ\text{C}$	30 min	98%	54
O <sub>v</sub> -SiW <sub>12</sub> /SNC	<b>2000 ppm, 0.2 g catalysts, 20 mL mode oil, O/S = 4, <math>T = 60^\circ\text{C}</math></b>	<b>12 min</b>	<b>100%</b>	<b>This work</b>

Generally, the reaction temperature plays a dominant role in improving ODS efficiency. As illustrated in Fig. 6a, the desulfurization efficiency of O<sub>v</sub>-SiW<sub>12</sub>/SNC is substantially improved with an increased temperature, which is ascribed to the facilitated probability of collision between the reactants, oxidants, and catalysts, and hence the promoted reaction rate. Optimally, it reaches 100% of DBT removal from the 2000 ppm of model fuel within 12 minutes at 60 °C, better than most reports (Table 1). Surprisingly, even at lower temperatures, the DBT removal rate was still up to 100% within 40 min (at 40 °C) and 99.7% within 80 min (at 30 °C), indicating the outstanding ODS activity of O<sub>v</sub>-SiW<sub>12</sub>/SNC. Furthermore, the kinetic plots for ODS reactions over the catalyst are performed, as shown in Fig. 6b (see Section 4 of ESI† for the fitting method). These results demonstrate that all of them follow the pseudo-first-order kinetic model, as confirmed by the high correlation factor ( $R^2 > 0.99$ ). When the reaction temperature is 60 °C, the rate constant is as high as 0.4055 min<sup>-1</sup>.

Additionally, the O<sub>v</sub>-SiW<sub>12</sub>/SNC catalyst achieves a turnover frequency (TOF) value of 10.65 h<sup>-1</sup> at 60 °C by utilizing the W atom as the active site based on a W content of 2.93 mmol g<sup>-1</sup> calculated by the ICP-OES test according to Formula (S2) in the ESI.† Notably, the TOF value of the spherical O<sub>v</sub>-SiW<sub>12</sub>/SNC catalyst with more O<sub>v</sub> defects is about 10 times that (1.39 h<sup>-1</sup>) of the bowl SiW<sub>12</sub>/NC catalyst with less O<sub>v</sub> defects obtained by the corresponding precursor with no addition of AM,<sup>5</sup> verifying the

great advantage of introducing AM components into the precursor once again.

**3.2.3 Investigation on the desulfurization adaptability of O<sub>v</sub>-SiW<sub>12</sub>/SNC.** To evaluate the industrial adaptability of the as-prepared O<sub>v</sub>-SiW<sub>12</sub>/SNC catalyst, ODS performances of various fuel oils with different S contents (500~4000 ppm) and different sulfur compounds (DBT, 4,6-DMDBT, and BT) are studied. As shown in Fig. 7a, the desulfurization efficiency of fuel oils containing different sulfur compounds follows the order DBT>4,6-dmdbt > BT depending on the electron density of the sulfur (S) atom and the steric hindrance, which is consistent with the literature.<sup>1,27,55,56</sup> Among them, a higher electron density of the sulfur (S) atom of DBT (5.758) than that of BT (5.739) makes the former more vulnerable to electrophilic attack by reactive oxygen species, thus expediting the oxidation of DBT.<sup>57</sup> However, 4,6-DMDBT with the highest electron density (5.760) of the S atom presents slightly weaker ODS performance than DBT, attributed to the synergistic effect of greater steric hindrance caused by two methyl groups on the benzene ring and the greatest electron density of the S atom. Fig. 7b presents the desulfurization efficiency of fuel oils with S contents in the range of 500–2000 ppm. It is distinctly observed that the O<sub>v</sub>-SiW<sub>12</sub>/SNC catalyst could eliminate DBT from model oils with a wide range of S contents (500–4000 ppm) within 10–30 min, suggesting again that the O<sub>v</sub>-SiW<sub>12</sub>/SNC catalyst can be a promising potential catalyst for the ODS reaction of fuel oil.

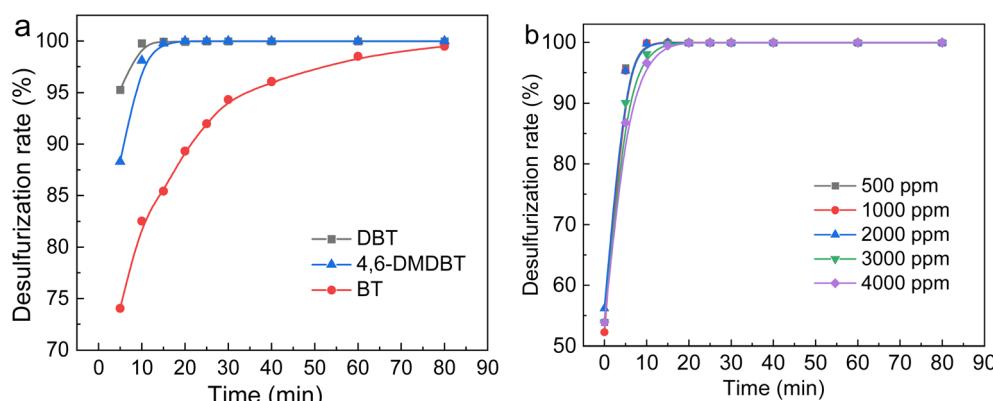


Fig. 7 ODS performances of model oil with different sulfur compounds (DBT, 4,6-DMDBT, and BT) (a) and different sulfur contents (500–4000 ppm) (b) (catalyst: 0.2 g;  $n(\text{H}_2\text{O}_2) : n(\text{S}) = 4 : 1$ ;  $T = 60^\circ\text{C}$ ).



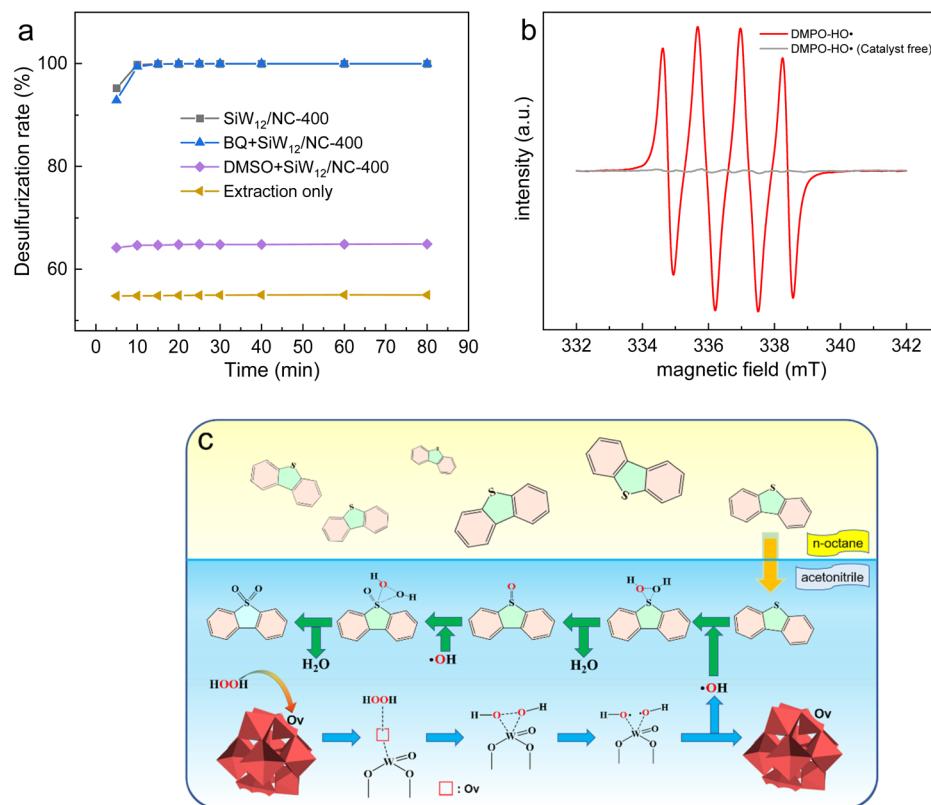


Fig. 8 (a) Removal efficiency of DBT in the presence of scavengers. (b) EPR spectrum of the reaction system. (c) Mechanism diagram of the ODS reaction over  $\text{O}_v\text{-SiW}_{12}/\text{SNC}$  (catalyst: 0.2 g;  $n(\text{H}_2\text{O}_2) : n(\text{S}) = 4 : 1$ ;  $T = 60$  °C).

**3.2.4 ODS reaction mechanism.** Usually, *p*-benzoquinone (BQ) and dimethyl sulfoxide (DMSO) are used as quenchers for superoxide anion radical ( $\text{O}_2^{\cdot-}$ ) and hydroxyl radical ( $\text{HO}^{\cdot}$ ), respectively,<sup>23</sup> to elucidate the ODS mechanism of  $\text{O}_v\text{-SiW}_{12}/\text{SNC}$ . As shown in Fig. 8a, BQ slightly affects ODS efficiency, demonstrating the absence of  $\text{O}_2^{\cdot-}$  radical in the ODS reaction. However, the addition of DMSO can greatly inhibit the desulfurization efficiency, indicating that the  $\text{HO}^{\cdot}$  radical plays an essential role in the ODS reaction. In addition, the electron paramagnetic resonance (EPR) spectrum (Fig. 8b) using 5, 5-dimethylpyrroline-oxide (DMPO) as a radical scavenger shows a fourfold peak with a peak area ratio of 1 : 2.2 : 1, confirming the presence of the  $\text{HO}^{\cdot}$  radical and thus a free radical reaction mechanism for the ODS reaction, which is similar to the results in the literature.<sup>5,29</sup>

Furthermore, Fig. S11<sup>†</sup> shows HPLC chromatograms of the *n*-octane and acetonitrile phases during the ODS reaction. As the ODS reaction proceeds, DBT in the acetonitrile phase is initially oxidized into DBTO and eventually into DBTO<sub>2</sub>. Combined with the aforementioned results, the possible reaction mechanism (Fig. 8c) is inferred as follows. DBT is first transferred from the *n*-octane phase to the acetonitrile phase. Simultaneously, in the acetonitrile phase,  $\text{H}_2\text{O}_2$  is activated by  $\text{O}_v\text{-SiW}_{12}/\text{SNC}$  to generate  $\text{HO}^{\cdot}$ ; then, DBT is oxidized by  $\text{HO}^{\cdot}$  into DBTO and further into DBTO<sub>2</sub>. During the key process, not only the W active sites with high electron density triggered by  $\text{O}_v$  defects boost the cleavage of O-O bonds of  $\text{H}_2\text{O}_2$  and thus the

generation of a substantial quantity of electrophilic  $\text{HO}^{\cdot}$  species,<sup>58</sup> but also the spherical structure of  $\text{O}_v\text{-SiW}_{12}/\text{SNC}$  is conducive to the exposure of W active sites and the diffusion of DBT and  $\text{H}_2\text{O}_2$ , thereby providing opportunities for excellent interaction with active species and reactants, which thus facilitates the ODS reaction. With the transformation of DBT in the acetonitrile phase into DBTO and DBTO<sub>2</sub>, the extraction equilibrium is disturbed, and the residual DBT in the *n*-octane phase is further extracted into the acetonitrile phase for the subsequent oxidation reaction. In this way, extraction and oxidation are carried out alternately until all DBTs are completely transferred from the *n*-octane phase into the acetonitrile phase and converted into DBTO<sub>2</sub> in the acetonitrile phase, thereby obtaining the final complete removal of DBT from the *n*-octane phase.

**3.2.5 Reusability of  $\text{O}_v\text{-SiW}_{12}/\text{SNC}$ .** The reusability of  $\text{O}_v\text{-SiW}_{12}/\text{SNC}$  is evaluated, as shown in Fig. 9a. It is clear that after 6 cycles, the desulfurization rate can still reach 100%, and only the complete desulfurization time is slightly extended. In addition, it can be observed from the filtration experiment depicted in Fig. S12<sup>†</sup> that DBT is no longer removed after  $\text{O}_v\text{-SiW}_{12}/\text{SNC}$  is filtered out, indicating its good stability. The structural stability of  $\text{O}_v\text{-SiW}_{12}/\text{SNC}$  can also be verified by comparing the XRD patterns (Fig. 9b) and FT-IR spectra (Fig. 9c) of fresh and recovered catalysts. As illustrated in Fig. 9b and c, the structure of the recovered catalyst does not show significant changes compared to that of the fresh one, and only two weak

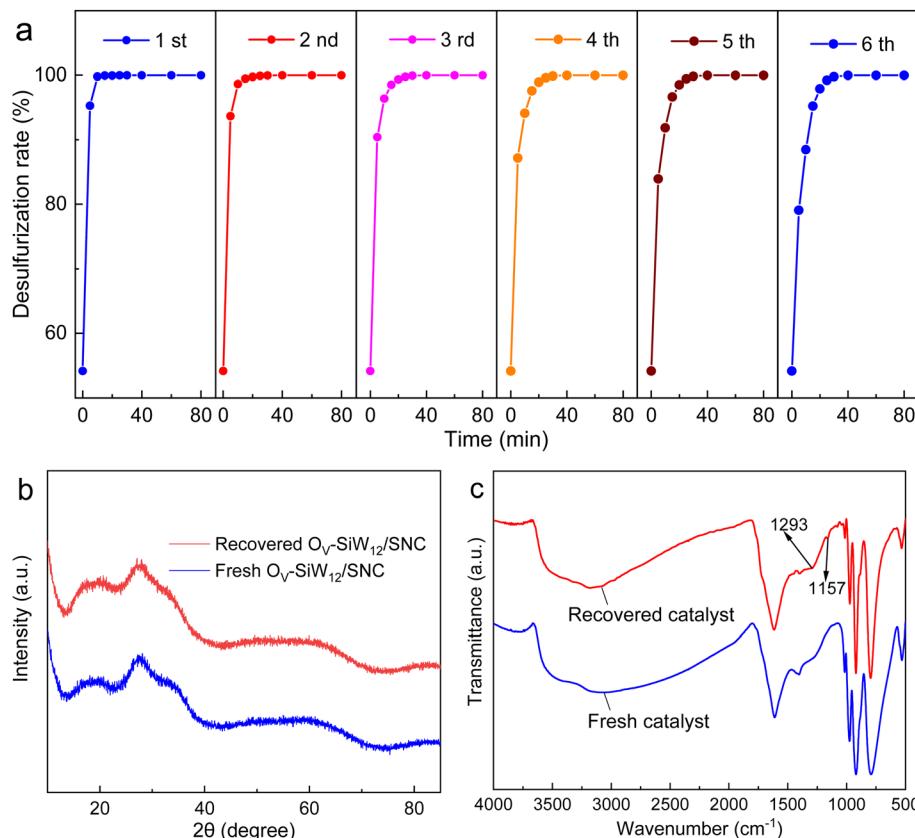


Fig. 9 (a) Reusability of the catalyst. (b) XRD patterns and (c) FT-IR spectra of fresh and recovered catalysts.

absorption peaks appear at  $1293\text{ cm}^{-1}$  and  $1157\text{ cm}^{-1}$  in the FT-IR spectrum of the recovered catalyst, which can be attributed to the asymmetric and symmetrical tensile vibrations of the  $\text{O}=\text{S}=\text{O}$  bond of  $\text{DBTO}_2$ .<sup>5,58</sup>

#### 4. Conclusion

In conclusion, the spherical  $O_V$ -SiW<sub>12</sub>/SNC catalyst with abundant  $O_V$  defects was successfully synthesized through *in situ* low-temperature calcination of the copolymer of AM and DAC as a precursor in air for deep ODS of fuel oil. It is depicted that during the preparation, the introduction of AM in the precursor could facilitate the formation of more  $O_V$  defects and the evolution of the morphology from bowl to sphere. The as-prepared  $O_V$ -SiW<sub>12</sub>/SNC catalyst exhibits an excellent ODS activity and outstanding reusability. It could effectively eliminate DBT from fuel oil with a sulfur content of 2000 ppm within 12 minutes at  $60\text{ }^\circ\text{C}$  and maintain a desulfurization rate of 100% after 6 cycles despite a slightly extended time. Notably, it can still efficiently remove DBT derivatives (such as BT and 4,6-DMDBT) in the same way that DBT is removed from fuel oil. This may be attributed to the W active sites with high electron density induced by abundant  $O_V$  defects, the good dispersion and high exposure of the W sites, and the easy diffusion and contact between the substrate and active sites led by the spherical structure. The ODS reaction follows the  $\text{HO}^\cdot$  radical mechanism. Overall,

this research presents a controllable method for constructing heterogeneous SiW<sub>12</sub> with abundant  $O_V$  defects, which could potentially expand its application in the deep ODS of fuel oils.

#### Data availability

Data for this article, including raw graphical data and ESI files, are available at Science Date Bank at <https://doi.org/10.57760/scencedb.22886>.

#### Conflicts of interest

The authors report no declarations of interest.

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