


 Cite this: *RSC Adv.*, 2025, 15, 15397

Preparation and characterization of HfOC/SiOC composite powders and fiber mats *via* the polymer pyrolysis route†

 Arijit Roy,  ‡ Paul Owiredu  ‡ and Gurpreet Singh  *

We report on the synthesis and characterization of HfOC/SiOC ceramic composite powders and electrospun fiber mats, which integrate the high-temperature resilience of HfOC with the oxidation resistance of silicon oxycarbide (SiOC). The composites were fabricated through a polymer-pyrolysis route by integrating 1,3,5,7-tetramethyl, 1,3,5,7-tetravinyl cyclotetrasiloxane (4-TTCS), a precursor source for SiOC, and a commercial HfC precursor in a 1 : 1 ratio by mass. First, the HfC precursor was heated to 70 °C to drive off water molecules, followed by its blending with the liquid phase 4-TTCS and cross-linking at a moderate temperature (160–400 °C). This was followed by pyrolysis at three different temperatures – 800, 1000, and 1200 °C in an inert argon atmosphere. The composite ceramic was comprehensively characterized by the use of electron microscopy for particle and fiber morphology, X-ray diffraction for the evolution of various ceramic phases, and a range of spectroscopies to document the change in molecular vibrations or the evolution of the functional groups and molecular bonding in preceramic polymer during cross-linking and ceramization. The crosslinked polymer-to-ceramic yield for powder samples was observed to be as high as approximately 78 wt% when pyrolyzed at 800 °C, and 74 wt% when pyrolyzed at 1200 °C. The oxidation test performed at 800 °C in stagnant air for the fiber mat pyrolyzed at 1000 °C indicated a linear shrinkage of 6% for the HfOC/SiOC composite. This represents an improvement over the carbon rich-SiOC fiber mat which exhibited a mass loss of 71 wt% and a linear shrinkage of nearly 19%, while the neat carbon fiber mat was completely burned off under similar conditions.

 Received 22nd March 2025
 Accepted 2nd May 2025

DOI: 10.1039/d5ra02006a

rsc.li/rsc-advances

Introduction

Ultra-high-temperature ceramics (UHTCs) possess remarkable durability in high-temperature applications, attributed to their elevated melting points, low coefficients of thermal expansion, and exceptional hardness.^{1–3} Typically, UHTCs consist of transition metal carbides, borides, and nitrides, such as hafnium carbide (HfC), zirconium diboride (ZrB₂), and titanium nitride (TiN) among others.^{4–6} In particular, researchers have shown considerable interest in hafnium monocarbide, which exhibits one of the highest melting points at 3928 °C, as well as exceptional hardness (22–25 GPa) and Young's modulus (300–500 GPa).^{7–9} However, the low-fracture toughness (1.73–3.40 MPa √m) of HfC and its susceptibility to oxidation at high temperatures limits its applications.^{10,11} To address such issues, silicon carbide (SiC), silicon dioxide (SiO₂), and silicon carbonitrides (SiCN) are typically incorporated into metal carbides to create

composite ceramic matrices, which enhances mechanical properties compared to single-phase ceramic materials.^{10,12–15} This silicon-based framework improves intermolecular bonding interactions, thus increasing the oxidation resistance of the ceramic composite, rendering it suitable for aerospace applications.¹⁶

The ceramic composites are conventionally synthesized through solid-state sintering of metal carbide and silicon carbide powders, while sintering is challenging because the coarse particle size necessitates high temperatures, significant pressure, and extended production time.^{17,18} In contrast, a polymer-derived ceramic (PDC) offers an easier and more effective solution for dual-phase ceramic composites preparation with tailored phase composition and microstructures, leading to enhanced properties.^{19,20} Silicon oxycarbide (SiOC) is one of the earliest silicon-based PDCs, extensively studied for its available source of raw materials, cost-effectiveness, scalability in production, and significant design flexibility, which is conferred by the molecular structure of its precursors.^{21–25} Previous studies have demonstrated that the incorporation of SiOC with Hf to form a SiOC/HfO₂ composite significantly enhances oxidation resistance at temperatures of up to 1600 °C, and this enhancement is attributed to the formation of HfSiO₄

Mechanical and Nuclear Engineering Department, Kansas State University, Manhattan, KS 66506, USA. E-mail: arijit@ksu.edu; gurpreet@ksu.edu

† Electronic supplementary information (ESI) available. See DOI: <https://doi.org/10.1039/d5ra02006a>

‡ Equal contribution.



at elevated temperatures, which acts as a protective layer.^{16,26} This incorporation of hafnia (HfO₂) within SiOC ceramic composites enhances thermal stability by inhibiting phase separation and decomposition while also improving creep resistance under stress at elevated temperatures compared to neat SiOC.^{26–28}

Thus, a synergistic interaction between the protective properties of SiOC ceramics and the high-temperature stability of HfC ceramics could position HfOC/SiOC ceramics as ideal candidates for advanced high-temperature applications that require material stability in oxidative environments. In this study, liquid preceramic precursors of HfC and SiOC were employed to synthesize a HfOC/SiOC ceramic composite matrix. The pyrolyzed ceramic composite matrices at three different temperatures, in both particulate and fibrous forms, were analyzed to confirm the presence of HfC and SiOC ceramics, as well as HfO₂ and excess carbon. The conversion of polymers to ceramics and the subsequent structural evolution of the customized nanofoms suggest that this method could be utilized for the development of a range of dual-phase ceramics, especially those with a silicon-based skeleton. Additionally, the oxidation analysis of the HfOC/SiOC fibers at 800 °C shows that incorporating Hf into the SiOC ceramic composite improves yields, while preserving the fiber structure.

Material characterization

The morphology and microstructure of the HfOC/SiOC ceramics were characterized by utilizing a scanning electron microscope (SEM, SU8010, Hitachi). This microscope was also equipped with an X-ray fluorescence (XRF) analyzer for the determination of the elemental composition of the specimens. The presence and alteration in the chemical functional groups of polymer precursors and ceramic composite powder were assessed with Fourier-transform infrared spectroscopy (FTIR) conducted on a Thermo Scientific Nicolet iS5 (iD7 ATR) spectrometer. Surface chemical composition analysis was conducted *via* X-ray photoelectron spectroscopy (XPS) with a Thermo Scientific Al K α source (beam energy = 1486.6 eV, spot size = 400 μ m). A confocal Raman microscope (Renishaw inVia, wavelength 532 nm) was employed to determine the carbon vibrational modes in HfOC/SiOC ceramics. The crystallography of the material was analyzed through X-ray diffraction (XRD) utilizing a PANalytical Empyrean instrument set to 45 kV and 40 mA power, with a step size of 0.02°.

Materials and methods

Materials

The preceramic silicon oligomer 1,3,5,7-tetramethyl 1,3,5,7-tetra-vinyl cyclotetrasiloxane (denoted as 4TTCS) was purchased from Gelest (Morrisville, PA, USA). The crosslinking agent, [C₆H₅C(CH₃)₂]₂O₂ or bis(1-methyl-1-phenylethyl) peroxide or dicumyl peroxide (denoted as DCP), was purchased from Sigma-Aldrich (St. Louis, MO, USA).²⁹ The spinning agent polyvinylpyrrolidone (PVP) with an average molecular mass of 1 300 000 g mol⁻¹ was purchased from Sigma-Aldrich (St. Louis,

MO, USA). The HfC precursor, SPH-199 HfC (Starfire Systems), was supplied by Spirit AeroSystems Inc. The ultra-high-purity argon (Ar) gas in the glove box and tube furnace was purchased from Matheson (Manhattan, KS, USA). The isopropyl alcohol or IPA was purchased from Thermo Fisher Scientific (Waltham, MA, USA).

Methods

Preparation of ceramic particles. The synthesis of HfOC/SiOC ceramic particles was conducted in two stages. Initially, 5 mL of water-based HfC precursor was dried at 70 °C to get rid of excess water. Subsequently, it was added to 5 mL of the SiOC precursor, or 4TTCS, along with 1 wt% of DCP, and was subjected to magnetic stirring. Drying of HfC precursor was necessary because the HfC liquid precursor was found to be immiscible in liquid 4TTCS directly. The solution obtained was crosslinked at a temperature of 160 °C overnight on a hot plate inside a glove box filled with ultra-high-purity argon gas. The resulting brownish material is referred to as crosslinked or HfC/4TTCS XL particles. During this crosslinking process, in the presence of a crosslinking agent, the 4TTCS was immobilized, and a possible polymeric network of 4TTCS and HfC was formed.

In the second stage, the crosslinked polymer was pyrolyzed (py) at three different temperatures (800, 1000, and 1200 °C) in a tube furnace with a continuous flow of Ar gas. The cross-linked samples were initially heated to 400 °C for 10 minutes at a rate of 2 °C per minute. Subsequently, the temperature was raised to 800 °C, 1000 °C, and 1200 °C at a rate of 5 °C per minute, and maintained for 1 hour to synthesize three different pyrolyzed samples. These obtained dark samples were denoted as HfOC/SiOC ceramic composite particles. The precision of the temperature controller in the tube furnace is ± 1 °C. This high-temperature carbonization of the crosslinked polymers possibly transformed into HfOC/SiOC ceramic network along with excess carbon, originated from 4TTCS. The schematic in Fig. 1 demonstrates the synthesis process of the HfOC/SiOC ceramic particles.

Preparation of ceramic fibermats. The HfOC/SiOC ceramic fibermats were synthesized in three stages, beginning with the electrospinning stage. At first, 90 mg of crosslinked HfC/4TTCS was dispersed into 6 mL of IPA and sonicated (bath) for 30 minutes. Then 600 mg of PVP (with a PVP:IPA ratio of 100:1 mg mL⁻¹) was added to the solution and magnetically stirred. After an hour, 1800 mg of 4TTCS (maintaining an XL-HfC/4TTCS:4TTCS ratio of 1:20) and 18 mg of DCP (1 wt% of 4TTCS) were added, and the stirring continued overnight to confirm a homogeneous mixture. The resulting solution was loaded into a 10 mL syringe with a metallic needle for electrospinning. A 15 cm distance was kept between the needle tip of the syringe and the cylindrical-shaped roller collector, while maintaining a high applied voltage (~ 15 kV) and slow feed rate (~ 5 mL h⁻¹). The as-spun fiber mat (15 \times 15 cm²) was dried in the open air at room temperature overnight and denoted as as-spun HfOC/SiOC FM. All mass measurements in this study were conducted utilizing a precision scale with a readability of 0.1 mg and a linearity of ± 0.2 mg.



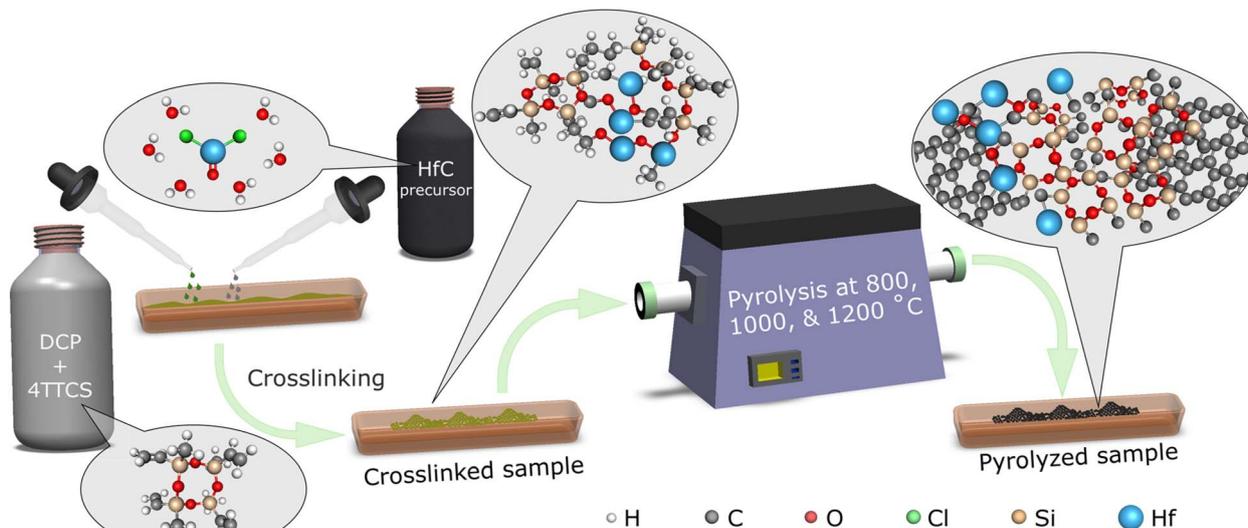


Fig. 1 Schematic representation of the synthesis process for HfOC/SiOC ceramic particles. The HfC precursor and 4TCS were first crosslinked and then pyrolyzed at three different temperatures to obtain HfOC/SiOC ceramic particles.

In the second stage, the fiber mat was crosslinked at 160 °C for 6 hours in air, and in the final stage, the XL fiber mats were cut into smaller pieces ($\sim 5.5 \times 3.5 \text{ cm}^2$) and pyrolyzed at three different temperatures (800, 1000, and 1200 °C) in an inert atmosphere. This two-step annealing process started with increasing the temperature up to 400 °C at a heating rate of 2 °C min^{-1} and maintaining that for an hour. Then, similar to the particle samples, the temperature was raised to 800, 1000, and 1200 °C with a rate of 2 °C min^{-1} , maintaining that for 1 hour for synthesizing three different HfOC/SiOC fiber mats. The presence of PVP in this high-temperature treatment contributes to a higher quantity of free carbon in the fiber mat samples compared to the particle form. All the crosslinking to pyrolysis yields for both the particle and fiber mat samples are tabulated in Table S1.†

Sample preparation for oxidation of the fiber mats. Along with HfOC/SiOC fiber mats, PVP-derived carbonized and SiOC fiber mats were prepared. These fiber mats were prepared using similar conditions as the HfOC/SiOC fiber mats, with the only difference in the solution for electrospinning. In the case of PVP-derived carbonized fiber mat, there was no HfC or 4TCS precursor (or XL material) present, and for SiOC fiber mat, 4TCS with DCP was added to the solution without any HfC precursor. The PVP-derived carbonized fiber mat was synthesized *via* electrospinning on three occasions, yielding an average mass of about 300 mg ($\pm 15 \text{ mg}$), indicating minimal influence of repeated electrospinning processes on final characteristics of the fiber mats under the same conditions. Then, circular-shaped fiber mats with an area of 1.6 cm^2 were punched out for the oxidation tests.

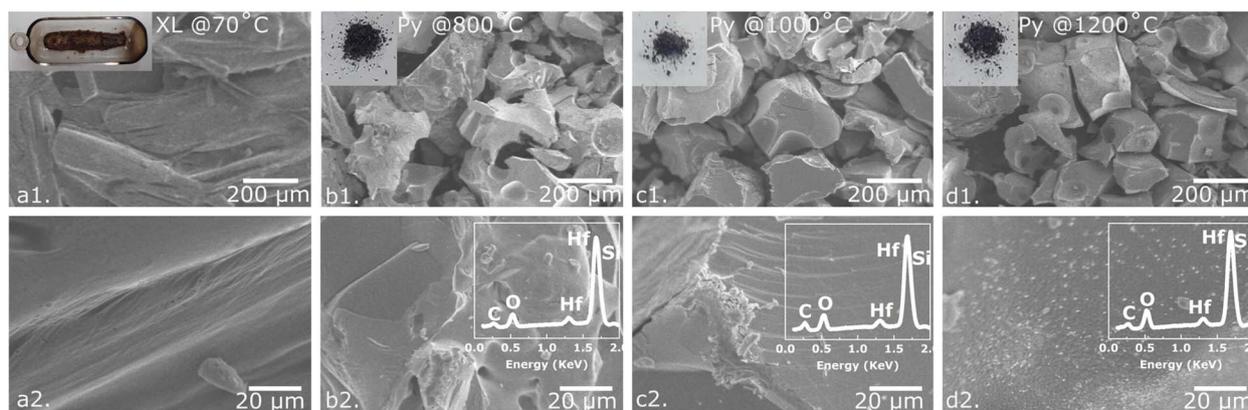


Fig. 2 SEM images of (a1) low magnification crosslinked, (a2) high magnification crosslinked, (b1) low magnification pyrolyzed at 800 °C, (b2) high magnification pyrolyzed at 800 °C, (c1) low magnification pyrolyzed at 1000 °C, (c2) high magnification pyrolyzed at 1000 °C, (d1) low magnification pyrolyzed at 1200 °C, (d2) high magnification pyrolyzed at 1200 °C HfOC/SiOC ceramic particles and their corresponding camera images as inset of (a1–d1) and XRF data as inset of (b2–d2). The SEM images depict the particulate form and the change in average particle size of the HfOC/SiOC ceramic, while the XRF data confirms the presence of Hf and Si.



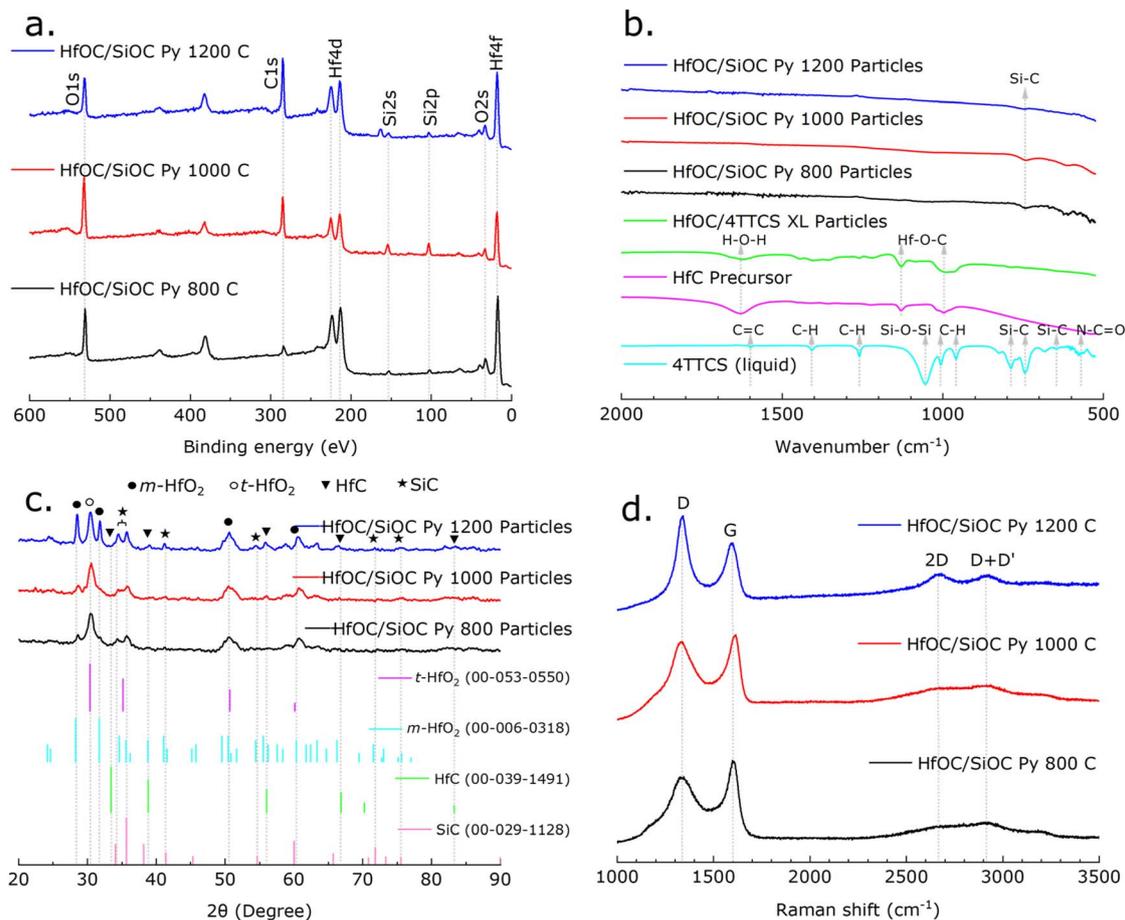


Fig. 3 (a) The XPS survey scan of the HfOC/SiOC ceramic particles pyrolyzed at 800, 1000, and 1200 °C represents the binding energy and possible bonding between Hf, Si, O and C. (b) Their FTIR spectra, including precursors and crosslinked samples, represents the gradual disappearance of H-containing functional groups. (c) Their XRD pattern, including comparable JCPDS card numbers, indicates the increase in crystallinity with the increase in pyrolysis temperature. (d) The Raman spectra of HfOC/SiOC ceramic particles indicate evolution of the carbon phase as function of the pyrolysis temperature.

Result and discussion

The SEM images of the crosslinked and pyrolyzed samples at various temperatures (800, 1000, and 1200 °C) have been shown in Fig. 2, and the insets of Fig. 2(a1–d1) display camera images of the corresponding samples. The SEM and camera pictures of crosslinked polymer samples consist of a compact morphology, whereas the pyrolyzed samples indicate uniform distribution of particles. The average particle size of the sample pyrolyzed at 800 °C was approximately 300 μm , and it decreased as the pyrolysis temperature increased. This morphological change supposedly indicates the radical conversion of HfO_2 to HfC during pyrolysis.^{30,31} Fig. 2(d2) shows that a high pyrolysis temperature of 1200 °C has resulted in increased porosity and a coarse surface for the ceramics. This is potentially caused by the release of volatile gases such as CO, CO₂, and CH₄.³¹ The XRF data of all the pyrolyzed HfOC/SiOC samples are presented in the inset of Fig. 2(b2–d2), which reveals the presence of Hf and Si (overlapped with Hf peak) with O and C. However, the XRF analysis has inherent limitations in detecting lighter elements accurately. In the presence of additional elements, the

measured intensity of the target element may be influenced either through absorption or enhancement of its fluorescent X-rays, and this phenomenon is known as the matrix effect, which can result in inaccurate outcomes in XRF analysis. Hence, the XRF data utilized in this study were employed exclusively for the identification of material composition, rather than for quantification purposes.

The chemical binding states of the HfOC/SiOC were analyzed using XPS survey scan, as shown in Fig. 3(a). The XPS data revealed that the composite sample contains Hf 4f, Si 2p, O 1s, and C 1s peaks. The Hf 4f peak at 18.08 eV binding energy suggests the presence of Hf–O–Si (hafnium silicate), Hf–C, and Hf–O bonds.^{32,33} The Si 2p peak at 103.08 eV reveals the Hf–O–Si, SiCO₃, and SiC₂O₂ bonds.^{10,34} At 285.08 eV binding energy, the C 1s peak corresponds to C–O bond and C–C bond, confirming the presence of free carbon in the ceramic structure.¹⁰ The O 1s peak of the ceramic indicates the Si–O bond of SiO_x and C=O bonds at 532.08 eV.^{32,35} Also, the additional peaks for Hf 4d (214.08 and 225.08 eV) are associated with Hf–O bond of HfO_x, and the presence of Si 2s (154.08 eV) and O 2s (33.08 eV) peaks suggests the formation of SiOC ceramic.^{36,37}



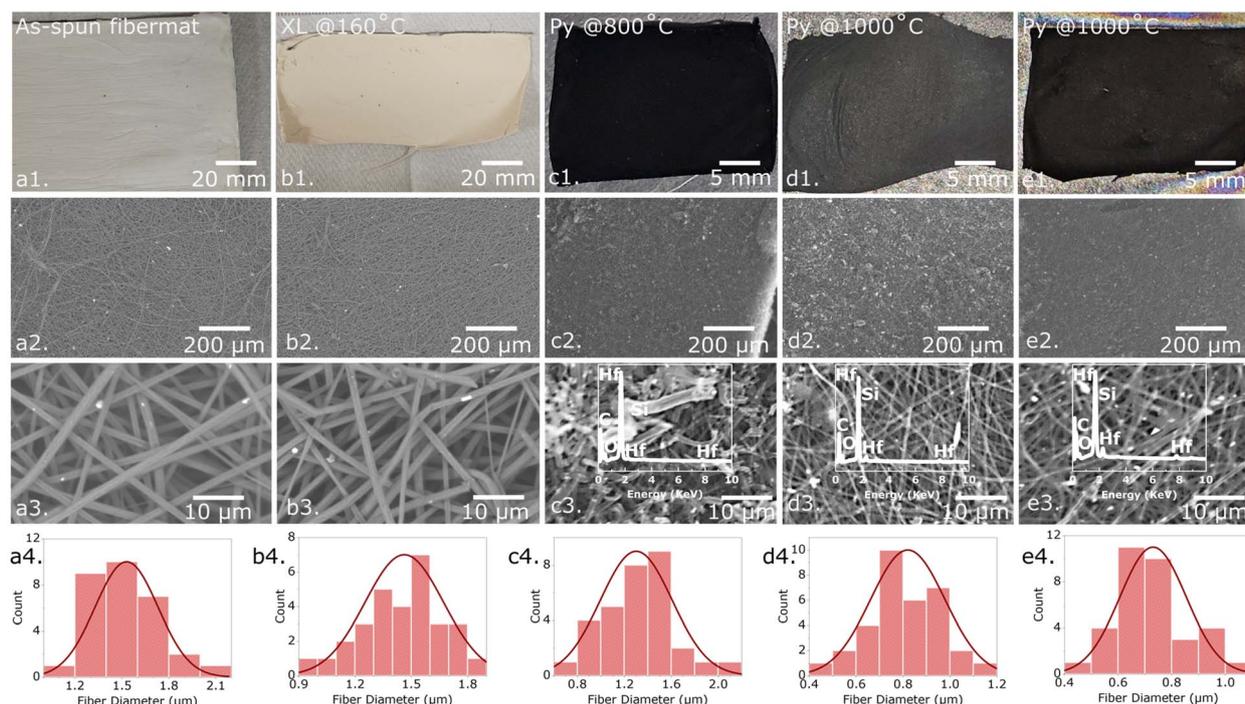


Fig. 4 Camera pictures of (a1) as-spun, (b1) crosslinked, pyrolyzed at (c1) 800 °C, (d1) 1000 °C, and (e1) 1200 °C HfOC/SiOC ceramic fiber mats; (a2) low and (a3) high magnification SEM images of as-spun, (b2) low and (b3) high magnification SEM images of crosslinked, (c2) low and (c3) high magnification SEM images of pyrolyzed at 800 °C, (d2) low and (d3) high magnification SEM images of pyrolyzed at 1000 °C, (e2) low and (e3) high magnification SEM images of pyrolyzed at 1200 °C HfOC/SiOC ceramic fiber mats and their corresponding XRF data as inset of (c3–e3), representing the presence of Hf and Si in the fibers. The diameter distribution curves of (a4) as-spun, (b4) crosslinked, pyrolyzed at (c4) 800 °C, (d4) 1000 °C, and (e4) 1200 °C HfOC/SiOC ceramic fiber mats illustrate a reduction in the average diameter of the fibers as pyrolysis temperature increases.

The evolution of molecular structure and the presence of various functional groups were assessed through the analysis of FTIR spectra obtained from the 4TTCS and HfC precursors, along with their crosslinked and pyrolyzed particle samples, as illustrated in Fig. 3(b). For the 4TTCS or SiOC precursor, the peaks at approximately 1598, 1408, 1260, 1054, 1006, 958, 787, 743, 645, and 569 cm^{-1} correspond to the C=C stretching of Si-CH=CH₂, C-H asymmetric bending of Si-CH₃, C-H symmetric bending of Si-CH₃, Si-O-Si asymmetric stretching, CH out-of-plane bending of Si-CH=CH₂, CH out-of-plane bending of Si-

CH=CH₂, Si-C deformation vibration of Si-CH₃, Si-C deformation vibration of Si-CH₃, Si-C stretching of Si-CH₃, and N-C=O bending, respectively.^{34,35,38–40} The FTIR spectra of the HfC liquid precursor show a broad H-O-H adsorption band near 1628 cm^{-1} , indicating the bending vibrational mode of water molecules.¹⁰ The FTIR intensity indicates that following the crosslinking of HfC/4TTCS at 160 °C, there is a decrease in water molecule presence and an increase in Hf-O-C bonds, as evidenced by the intensified absorption peaks located near 1128 and 996 cm^{-1} .^{10,41} Furthermore, minor peaks observed near

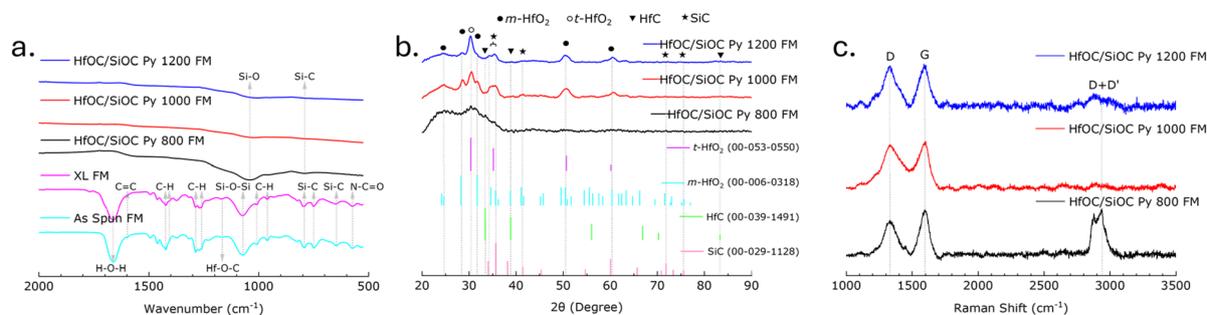


Fig. 5 (a) The FTIR spectra of HfOC/SiOC ceramic fiber mats pyrolyzed at 800, 1000, and 1200 °C, including as-spun and crosslinked fiber mat samples, represent the gradual disappearance of H-containing functional groups. (b) Their XRD pattern, including comparable JCPDS card numbers, represents an increase in crystallinity with the increase of pyrolysis temperature. (c) Their Raman spectra indicate evolution of the free carbon phase as a function of pyrolysis temperature.



Table 1 FTIR spectra of the electrospun and crosslinked HfOC/SiOC fiber mats

Wavenumber (cm ⁻¹)	Chemical group	Reference
1663	H-O-H (vibrational mode of water molecule)	10
1598	Si-CH=CH ₂ (C=C stretching)	34 and 39
1423	CH bending	34 and 38
1406	Si-CH ₃ (C-H asymmetric bending)	34 and 39
1286	CH ₂ wagging	34 and 38
1259	Si-CH ₃ (C-H symmetric bending)	34 and 39
1166	Hf-O-C	10 and 41
1070	Si-O-Si asymmetric stretching	34 and 39
1008	Si-CH=CH ₂ (CH out-of-plane bending)	34 and 39
960	Si-CH=CH ₂ (CH out-of-plane bending)	34 and 39
792	Si-CH ₃ (Si-C deformation vibration)	34 and 40
750	Si-CH ₃ (Si-C deformation vibration)	34 and 40
646	Si-CH ₃ (Si-C stretching)	34 and 39
571	N-C=O bending	34 and 38

1400, 1260, and 780 cm⁻¹ indicate C-H asymmetric bending, C-H symmetric bending, and Si-C deformation, respectively, confirming the presence of 4TTCS. After pyrolysis, only Si-C peaks were observed, while all characteristic bands associated with H-containing functional groups were absent, which suggests a complete transformation into ceramic material.⁴²

The crystallographic characterization of the HfOC/SiOC ceramic samples was performed utilizing XRD, as presented in Fig. 3(c), revealing crystalline characteristics in the pyrolyzed

samples. The XRD data of the synthesized ceramic samples were matched with reference pattern from ICDD database for tetragonal hafnia or t-HfO₂ (JCPDS card no. 00-053-0550), monoclinic hafnia or m-HfO₂ (JCPDS card no. 00-006-0318), HfC (JCPDS card no. 00-039-1491), SiC (JCPDS card no. 00-029-1128), Si (JCPDS card no. 01-089-2955), and C (JCPDS card no. 00-050-1082). Here, the diffraction peaks at 28.4°, 31.7°, 50.5°, and 60.3° on the 2θ scale correspond to (-111), (111), (-220), and (131) planes respectively of m-HfO₂, while the peaks at

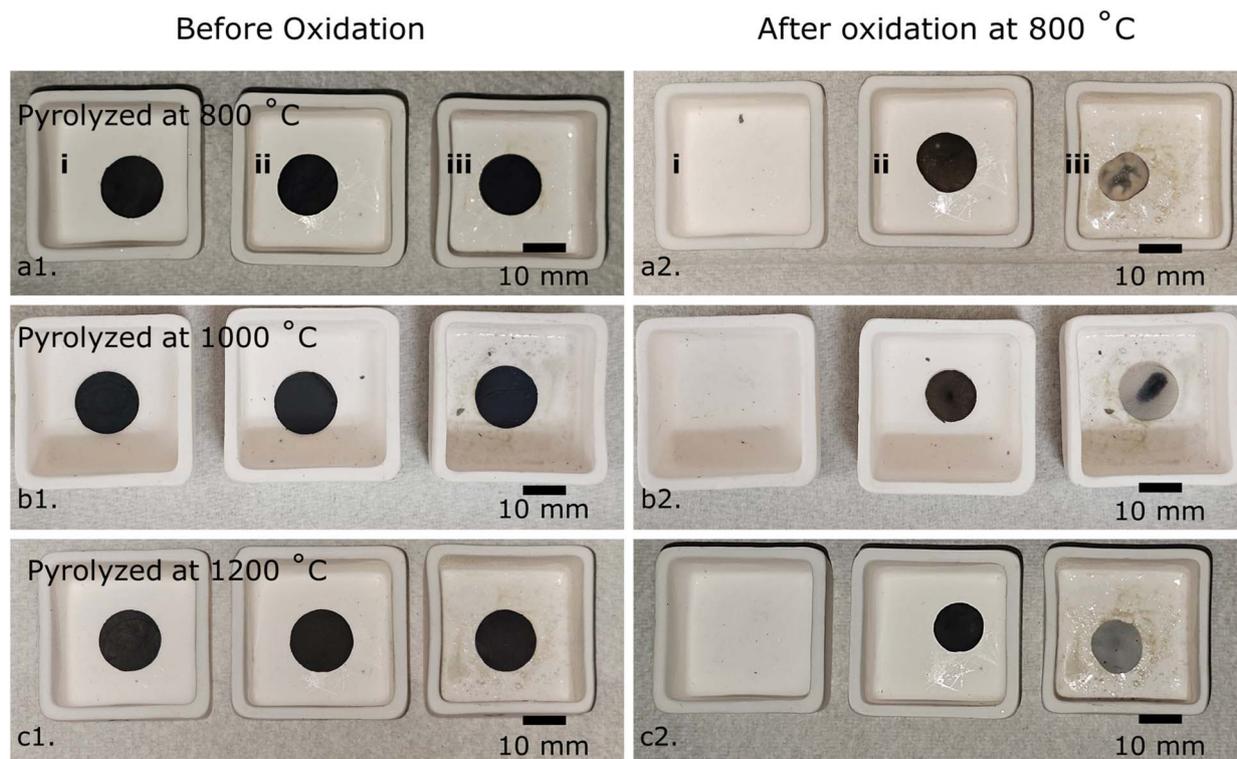


Fig. 6 Camera images of various fiber mat samples (a1–c1) before and (a2–c2) after the oxidation tests: (i) PVP-derived carbonized fiber mats, (ii) carbon rich SiOC fiber mats, and (iii) HfOC/SiOC fiber mats. A summary of linear shrinkage for these samples is presented in the ESI.†



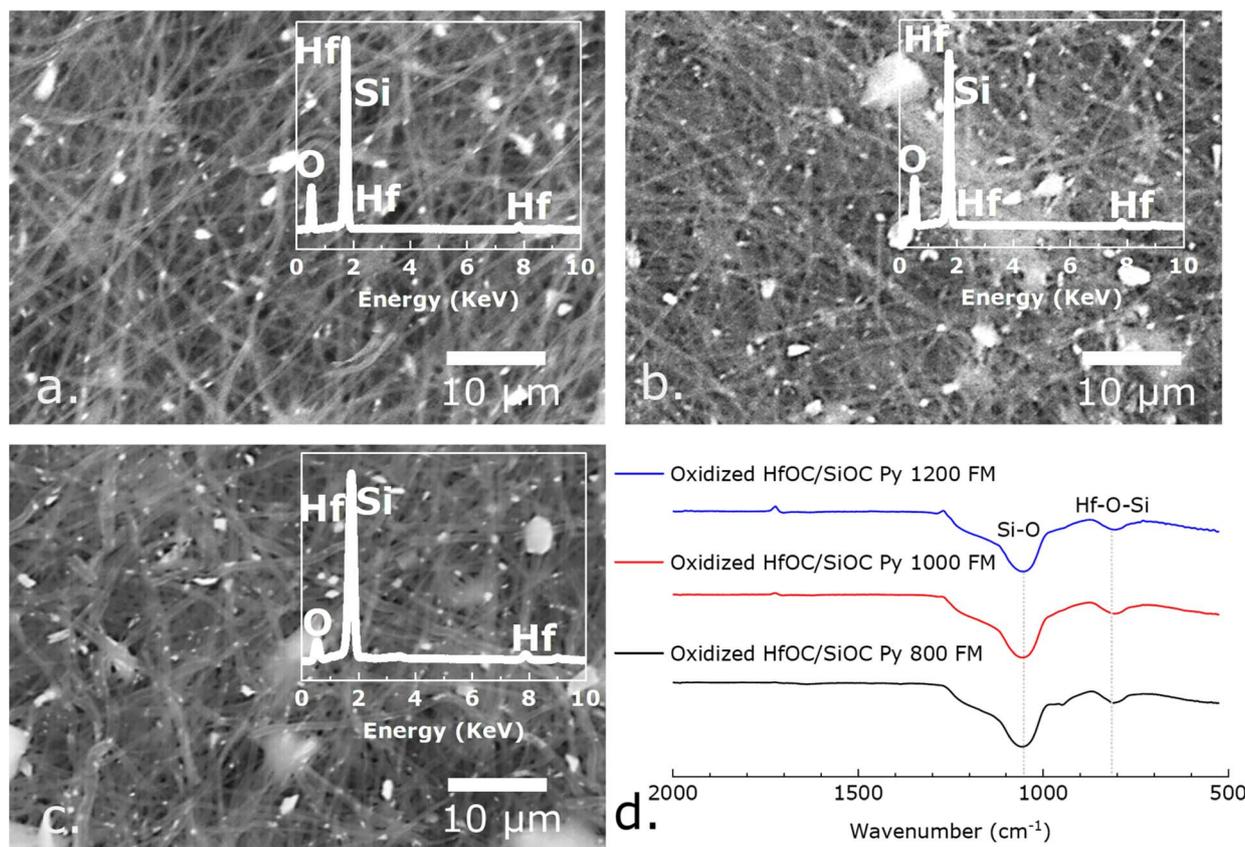


Fig. 7 The SEM images of oxidized HfOC/SiOC ceramic fiber mats at 800 °C for the samples pyrolyzed at (a) 800 °C, (b) 1000 °C, and (c) 1200 °C represent the fiber structure was preserved, while their corresponding XRF data, inset of (a–c), indicates the presence of Hf and Si. (d) The FTIR spectra of oxidized fiber mats, pyrolyzed at 800, 1000, and 1200 °C, reveal the presence of vibrational modes for Si–O and Hf–O–Si.

30.4° correspond to (111) plane of t-HfO₂.⁴³ The peak intensity of t-HfO₂ remains unchanged as the pyrolysis temperature rises, while the intensity of m-HfO₂ increases, indicating the conversion of t-HfO₂ to m-HfO₂.¹⁶ The (111), (200), (220), (311), and (400) planes of HfC were ascribed to the 33.4°, 38.8°, 56.0°, 66.8°, and 83.2°, respectively.⁴⁴ The diffraction peaks at 34.2°, 35.6°, 41.4°, 54.6°, 71.7°, and 75.5° were assigned to the (101), (102), (104), (107), (202), and (204) crystalline planes of SiC, respectively.⁴⁵ The intensity of SiC planes in the synthesized samples shows that higher pyrolysis temperatures lead to greater SiC crystallization.

The carbon vibrational modes of HfOC/SiOC ceramic particles were analyzed through Raman spectroscopy and illustrated in Fig. 3(d). The Raman spectra revealed two distinct peaks corresponding to the D (~1320–1350 cm⁻¹) and G (~1589–1614 cm⁻¹) bands. The D band was correlated with disordered carbon, which was characterized by lattice defects, displaying A_{1g} symmetry, and the G band was assigned to the in-plane stretching of sp² hybridized carbon, exhibiting E_{2g} symmetry.^{10,46} In the ceramic particles pyrolyzed at 800 °C, the G band was observed to be more prominent than the broader D band, indicating a predominance of graphitic carbon in the sample. As the pyrolysis temperature rose, the D band became

more distinct and prominent, while the G band expanded, signifying a rise in disordered carbon.¹⁰ In the second order of Raman spectra, the 2D peak (~2660–2690 cm⁻¹), identified as an overtone of the D peak, has been associated with the stacking of graphene layers in the structural composition, and the disordered graphitic sites correspond to the D + D' band (~2900–2930 cm⁻¹).⁴⁷

In this study, the HfOC/SiOC ceramic was examined both in particulate form and fiber mat configuration. Fig. 4 presents the camera pictures, SEM images, and diameter distribution curves of the as-spun, crosslinked, and three distinct pyrolyzed HfOC/SiOC fiber mat samples subjected to pyrolysis temperatures of 800, 1000, and 1200 °C. The average diameter of the as-spun fiber mats was measured at approximately 1.55 μm, which subsequently reduced to ~1.45 μm following crosslinking. Further reductions were observed, with diameters decreasing to approximately 1.3, 0.85, and 0.75 μm after pyrolysis at temperatures of 800, 1000, and 1200 °C, respectively. In addition, the XRF data for the three pyrolyzed fiber mat samples are illustrated as the insets of Fig. 4(c3–e3), indicating a significant presence of Hf and Si (overlapped with Hf peak) similar to particle samples. However, in the fiber mat form, carbon presence was significantly higher than in the particle form, despite



having a similar intensity of the O peak, thereby confirming the presence of SiOC. The excess carbon in the pyrolyzed samples was primarily generated from the spinning agent of the fiber-mat or PVP.

The FTIR spectra of as-spun, crosslinked, and pyrolyzed fiber-mat (at temperatures of 800, 1000, and 1200 °C) samples, are illustrated in Fig. 5(a). The chemical characteristics of the as-spun and crosslinked fiber-mat samples across various wavenumbers are detailed in Table 1. Notably, the intensity of the C–H bending reduced in the crosslinked samples in comparison to the as-spun samples, thereby confirming that the crosslinking reaction occurred at 160 °C.³⁴ On the other hand, the pyrolyzed samples exhibited a more pronounced peak for the Si–O bond in comparison to the Si–C bond, thereby affirming the existence of SiOC ceramic within the sample. Also, the absence of all H-containing functional groups indicates that the material has entirely transformed into a ceramic state.⁴² However, as the pyrolysis temperature elevated from 800 °C to 1000 °C and 1200 °C, the observed peaks exhibited increased broadening and decreased intensity.

The XRD analysis of pyrolyzed HfOC/SiOC ceramic samples indicates that crystallization peaks become sharp when the pyrolysis temperature exceeds 800 °C, as shown in Fig. 5(b). In contrast, the sample pyrolyzed at 800 °C exhibited broader low-intensity peaks in XRD, signifying its amorphous nature. This characteristic appeared in the fiber-mat form only and was absent in the particulate form of HfOC/SiOC ceramics. The XRD data were analyzed in comparison with the established reference database, as previously conducted with particle forms. The observed peaks at 24.6°, 28.4°, 31.7°, 50.5°, and 60.3° on the 2θ scale correspond to the (–110), (–111), (111), (–220), and (131) crystallographic planes of m-HfO₂, respectively, and the peak at 30.4° corresponds to the (111) plane of t-HfO₂.⁴³ In alignment with the XRD data pertaining to the particulate form, the peaks observed at 33.4°, 38.8°, and 83.2° correspond to the (111), (200), and (400) crystallographic planes of HfC, respectively.⁴⁴ Additionally, the peaks identified at 34.2°, 35.6°, 41.4°, 54.6°, 71.7°, and 75.5° are associated with the (101), (102), (104), (202), and (204) crystallographic planes of SiC, respectively.⁴⁵

The Raman spectra for the pyrolyzed fiber-mat samples are depicted in Fig. 5(c). These spectra exhibit peaks in the range of ~1330–1340 cm^{–1} and ~1589–1602 cm^{–1}, corresponding to the D and G bands, respectively. Consistent with the particle form, the D band is associated with A_{1g} symmetry, indicating the presence of disordered carbon or out-of-plane vibrations, while the G band is linked to E_{2g} symmetry, which confirms the existence of C–C bonds associated with sp² hybridization or in-plane stretching.^{10,46} In the fiber-mat samples also, the intensity of the D band increased with higher pyrolysis temperatures, suggesting an increase in disordered carbon.¹⁰ However, in the second-order Raman spectra, the 2D peak was minimized in all samples, while a distinct peak at ~2938 cm^{–1} representing the D + D' band was observed exclusively in the fiber-mat sample pyrolyzed at 800 °C.⁴⁷

Oxidation resistance behavior of the HfOC/SiOC ceramic fiber-mats along with PVP-derived carbonized and SiOC fiber-mats, for comparative analysis, were investigated by heating the

circular-shaped samples (pyrolyzed fiber-mat at 800, 1000, and 1200 °C) in stagnant air at 800 °C for a duration of 5 minutes, employing a heating rate of 10 °C min^{–1}. The camera pictures of the oxidized fiber-mats are presented in Fig. 6(a1–c2), with the SEM images of the oxidized HfOC/SiOC samples displayed in Fig. 7(a–c). The results indicate that, despite undergoing oxidation at 800 °C, the fiber structures remain intact in the cases of HfOC/SiOC and SiOC fiber-mats, whereas the PVP-derived carbonized fiber-mat did not survive. The carbonized samples produced little or no residue following the oxidation test, which aligns with the TGA analysis of previously reported studies.^{48,49} The mass losses due to oxidation of the fiber-mat samples are presented in Table S2.† The enhanced oxidation yield observed in the HfOC/SiOC fiber-mat (pyrolyzed at temperatures exceeding 800 °C) compared to that of the bare SiOC fiber-mat under similar conditions signifies a superior endurance attributed to the incorporation of Hf. Additionally, the linear shrinkage analysis (Fig. S1†) from the camera images (Fig. 6) shows that after the oxidation test, although the HfOC/SiOC fiber-mats show a slight tendency to curl, the shrinkage of the disk diameter is significantly lower than that of the SiOC fiber-mat when subjected to pyrolysis at temperatures above 800 °C. The reduction in thickness observed in the pre- and post-oxidation tests of the HfOC/SiOC fiber-mat samples is presented in Table S3.† The data reveal that when the fiber-mat sample undergoes pyrolysis at higher temperatures, such as 1200 °C, the reduction in thickness is limited to around 20%, in contrast to the ~67% reduction observed when the pyrolysis temperature is 800 °C. The XRF data for the oxidized HfOC/SiOC ceramic fiber-mat samples were also analyzed and are presented in the inset of Fig. 7(a–c). As anticipated, the XRF data reveal no C peaks and a more pronounced O peak following oxidation across all samples. Nonetheless, the detection of Hf, Si, and O peaks demonstrates the endurance of the ceramic fiber forms for high temperature applications.

FTIR analysis was also used to identify the chemical characteristics of the oxidized fiber-mat samples, as illustrated in Fig. 7(d). In the wavenumber scale, two prominent peaks at approximately 1040–1060 cm^{–1} and 810–820 cm^{–1} signify the vibrational modes of Si–O and Hf–O–Si in the oxidized samples, respectively.^{34,50} This indicates that in the oxidation test, the Hf–C and Si–C bonds were disrupted, resulting in the formation of Hf–O and Hf–O–Si bonds while preserving the fiber structure.

The studies previously reported regarding Hf-induced polysilazane-based PDCs demonstrate a crosslink-to-pyrolysis mass loss of approximately 20% for particulate samples, which is consistent with the findings of the current research.⁵¹ In case of fiber-mat samples, the observed post-pyrolysis reduction of approximately 30–40% in the average fiber diameter further corroborates the data from earlier studies.⁵² The mass loss during oxidation tests typically ranges from approximately 20% to 57% for similar electrospun PDC nanofibers.⁵³ Additionally, previous studies have demonstrated that Si/O/C type ceramics exhibit relatively low fracture toughness, such as PDC SiOC (0.88–0.99 MPa √m), SiO₂ (0.52–1.02 MPa √m), SiC (1.4–1.9 MPa √m), compared to HfC incorporated silicon-based ceramic composite matrix (0.8–3 MPa √m); which would be the



expected range of fracture toughness for the HfOC/SiOC samples of this study.^{54–58} Also, low thermal expansivity ($3.5 \times 10^{-6} \text{ K}^{-1}$), moderate stiffness (1–8 GPa), and high strength (1.5–13 MPa) of SiOC offer better thermal shock resistance and fatigue resistance compared to similar PDCs.^{59,60} Previous studies indicate that the incorporation of HfC into silicon-based ceramics has been shown to effectively diminish the ablation rate of the composite material.^{61–64} Consequently, this study anticipates enhanced overall thermophysical properties of the HfOC/SiOC ceramic composite.

Conclusion

This study presents a simple methodology for synthesizing HfOC/SiOC ceramic composites, in both particulate and fiber forms, by blending and pyrolysis of liquid 4TTCS and HfC precursors. The ceramics were synthesized from crosslinked polymers at three different temperatures: 800, 1000, and 1200 °C. The SEM images and XRF data demonstrate that the produced ceramic samples contain elements of Hf, Si, O, and C, confirming the successful formation of HfOC/SiOC ceramics, along with the excess or the free carbon phase in both particle and fiber configurations. The XPS analysis further validated these findings, while FTIR confirmed the organic to inorganic transformation of the polymer precursor into ceramic matrices. Further, the XRD analysis confirmed the evolution of HfC, monoclinic-HfO₂, and SiC crystalline phases in specimen processed beyond 800 °C. Although the particle form exhibited X-ray crystallinity when subjected to pyrolysis at 800 °C, the fiber form remained largely X-ray amorphous and only started to crystallize at 1000 °C. Furthermore, oxidation tests conducted on the fiber form samples indicate that HfOC/SiOC ceramic fiberforms exhibit improved thermal endurance for high-temperature applications. Post-oxidation analysis at 800 °C showed the retention of fiber forms, demonstrating superior performance (mass retention and shrinkage) due to the presence of Hf in the composite ceramic fiberforms compared to bare PVP-derived carbonized and/or TTCS derived SiOC ceramic fiberforms. This study does not concentrate on other mechanical and thermophysical properties; however, future research may encompass such investigations on this material. Furthermore, by varying the ratio of HfC to TTCS precursors, subsequent studies could focus on identifying the optimal material characteristics for specific high-temperature applications. This synthesis approach for the preparation of hybrid ceramics from the blending of precursors may have applications in the processing of other multi-elemental and high-performance ceramic composites.

Data availability

Data for this article, including plots, are available at the Ondrive of Kansas State University at [URL – https://ksuemailprod-my.sharepoint.com/:f/g/person/arjit_ksu_edu/Ejy5zVytaQpIi8P0rAdcIgBQcNCMgLfugeCICrVf_lpg?e=4fMPye].

Author contributions

Conceptualization: G. S.; methodology: G. S., P. O., and A. R.; HfOC/SiOC particle synthesis, SEM, XRF, XPS, FTIR, XRD, and Raman: A. R. and P. O.; HfOC/SiOC fiberform synthesis, oxidation test, SEM, XRF, FTIR, XRD, and Raman analysis: A. R.; resources: G. S.; data curation: P. O. and A. R.; writing – original draft preparation: A. R. and P. O.; writing – review and editing: G. S.; visualization: A. R.; supervision: G. S.; funding acquisition: G. S. All authors have read and agreed to the published version of the manuscript.

Conflicts of interest

There are no conflicts to declare.

Acknowledgements

This work is supported by the National Science Foundation grants #1743701 and 2025298. The research was performed in part in the Nebraska Nanoscale Facility: National Nanotechnology Coordinated Infrastructure and the Nebraska Center for Materials and Nanoscience (and/or NERCF), which are supported by the National Science Foundation under Award ECCS: 2025298, and the Nebraska Research Initiative. The partial funding by Spirit Aerosystems Inc. award number PO 4400005266 is gratefully acknowledged.

References

- 1 Y. Arai, R. Inoue, K. Goto and Y. Kogo, Carbon fiber reinforced ultra-high temperature ceramic matrix composites: A review, *Ceram. Int.*, 2019, **45**(12), 14481–14489.
- 2 J. Binner, M. Porter, B. Baker, J. Zou, V. Venkatachalam, V. R. Diaz, A. D'Angio, P. Ramanujam, T. Zhang and T. S. R. C. Murthy, Selection, processing, properties and applications of ultra-high temperature ceramic matrix composites, UHTCMCs – a review, *Int. Mater. Rev.*, 2020, **65**(7), 389–444.
- 3 E. Castle, T. Csanádi, S. Grasso, J. Dusza and M. Reece, Processing and Properties of High-Entropy Ultra-High Temperature Carbides, *Sci. Rep.*, 2018, **8**(1), 8609.
- 4 H. Kuwahara, N. Mazaki, M. Takahashi, T. Watanabe, X. Yang and T. Aizawa, Mechanical properties of bulk sintered titanium nitride ceramics, *Mater. Sci. Eng., A*, 2001, **319–321**, 687–691.
- 5 F. Monteverde, A. Bellosi and S. Guicciardi, Processing and properties of zirconium diboride-based composites, *J. Eur. Ceram. Soc.*, 2002, **22**(3), 279–288.
- 6 A. B. Peters, C. Wang, D. Zhang, A. Hernandez, D. C. Nagle, T. Mueller and J. B. Spicer, Reactive laser synthesis of ultra-high-temperature ceramics HfC, ZrC, TiC, HfN, ZrN, and TiN for additive manufacturing, *Ceram. Int.*, 2023, **49**(7), 11204–11229.
- 7 E. Wuchina, E. Opila, M. Opeka, B. Fahrenholtz and I. Talmy, UHTCs: Ultra-High Temperature Ceramic Materials for



- Extreme Environment Applications, *Electrochem. Soc. Interface*, 2007, **16**(4), 30.
- 8 E. Wuchina, M. Opeka, S. Causey, K. Buesking, J. Spain, A. Cull, J. Routbort and F. Guitierrez-Mora, Designing for ultrahigh-temperature applications: The mechanical and thermal properties of HfB₂, HfC_x, HfN_x and α Hf(N), *J. Mater. Sci.*, 2004, **39**(19), 5939–5949.
- 9 M. D. Sacks, C.-A. Wang, Z. Yang and A. Jain, Carbothermal reduction synthesis of nanocrystalline zirconium carbide and hafnium carbide powders using solution-derived precursors, *J. Mater. Sci.*, 2004, **39**(19), 6057–6066.
- 10 S. B. Mujib, M. Rasheed, S. R. Arunachalam and G. Singh, Hybrid HfC-SiCN matrix for improved oxidation resistance of carbon fiber-reinforced mini-composites, *Int. J. Ceram. Eng. Sci.*, 2024, **6**(2), e10209.
- 11 S. Shimada, A thermoanalytical study on the oxidation of ZrC and HfC powders with formation of carbon, *Solid State Ionics*, 2002, **149**(3), 319–326.
- 12 Z. Liu, Y. Jia, J. Hou, R. Zhang, S. Zhang, J. Zhang and q. Fu, C/C-HfC-SiC composites with simultaneous the resistance to ultra-high temperature airflow erosion and high temperature oxidation, *J. Materiomics.*, 2025, **11**(1), 100846.
- 13 P. Sarin, P. E. Driemeyer, R. P. Haggerty, D. K. Kim, J. L. Bell, Z. D. Apostolov and W. M. Kriven, In situ studies of oxidation of ZrB₂ and ZrB₂-SiC composites at high temperatures, *J. Eur. Ceram. Soc.*, 2010, **30**(11), 2375–2386.
- 14 C. Yan, F. Liu, W. Wang and R. Liu, Mechanical, thermophysical, and ablation properties of C/HfC-SiC composites with various SiC/HfC ratios, *Int. J. Appl. Ceram. Technol.*, 2025, **22**(1), e14878.
- 15 S. J. Wang, P. C. Lim, A. C. H. Huan, C. L. Liu, J. W. Chai, S. Y. Chow, J. S. Pan, Q. Li and C. K. Ong, Reaction of SiO₂ with hafnium oxide in low oxygen pressure, *Appl. Phys. Lett.*, 2003, **82**(13), 2047–2049.
- 16 Y. Lyu, H. Tang and G. Zhao, Effect of Hf and B incorporation on the SiOC precursor architecture and high-temperature oxidation behavior of SiHfBOC ceramics, *J. Eur. Ceram. Soc.*, 2020, **40**(2), 324–332.
- 17 J.-X. Liu, X. Huang and G.-J. Zhang, Pressureless Sintering of Hafnium Carbide-Silicon Carbide Ceramics, *J. Am. Ceram. Soc.*, 2013, **96**(6), 1751–1756.
- 18 R. Licheri, R. Orrù, C. Musa, A. M. Locci and G. Cao, Consolidation *via* spark plasma sintering of HfB₂/SiC and HfB₂/HfC/SiC composite powders obtained by self-propagating high-temperature synthesis, *J. Alloys Compd.*, 2009, **478**(1), 572–578.
- 19 E. Ionescu, H.-J. Kleebe and R. Riedel, Silicon-containing polymer-derived ceramic nanocomposites (PDC-NCs): preparative approaches and properties, *Chem. Soc. Rev.*, 2012, **41**(15), 5032–5052.
- 20 A. Sawaguchi, K. Toda and K. Niihara, Mechanical and Electrical Properties of Silicon Nitride-Silicon Carbide Nanocomposite Material, *J. Am. Ceram. Soc.*, 1991, **74**(5), 1142–1144.
- 21 S. Kaur, G. Mera, R. Riedel and E. Ionescu, Effect of boron incorporation on the phase composition and high-temperature behavior of polymer-derived silicon carbide, *J. Eur. Ceram. Soc.*, 2016, **36**(4), 967–977.
- 22 A. Gencer and B. S. Oksal, Synthesis and characterization of novel SiBOC ceramics: comparison of microwave and ultrasonic application on gelation time, *J. Sol-Gel Sci. Technol.*, 2015, **73**(1), 171–180.
- 23 H.-J. Kleebe and Y. D. Blum, SiOC ceramic with high excess free carbon, *J. Eur. Ceram. Soc.*, 2008, **28**(5), 1037–1042.
- 24 Z. Ren, S. B. Mujib and G. Singh, High-Temperature Properties and Applications of Si-Based Polymer-Derived Ceramics: A Review, *Materials*, 2021, **14**(3), 614.
- 25 G. Mera, A. Navrotsky, S. Sen, H.-J. Kleebe and R. Riedel, Polymer-derived SiCN and SiOC ceramics – structure and energetics at the nanoscale, *J. Mater. Chem. A*, 2013, **1**(12), 3826–3836.
- 26 E. Ionescu, B. Papendorf, H.-J. Kleebe and R. Riedel, Polymer-Derived Silicon Oxycarbide/Hafnia Ceramic Nanocomposites. Part II: Stability Toward Decomposition and Microstructure Evolution at T ≫ 1000 °C, *J. Am. Ceram. Soc.*, 2010, **93**(6), 1783–1789.
- 27 B. Papendorf, E. Ionescu, H.-J. Kleebe, C. Linck, O. Guillon, K. Nonnenmacher and R. Riedel, High-Temperature Creep Behavior of Dense -Based Ceramic Nanocomposites: Microstructural and Phase Composition Effects, *J. Am. Ceram. Soc.*, 2013, **96**(1), 272–280.
- 28 H.-J. Kleebe, K. Nonnenmacher, E. Ionescu and R. Riedel, Decomposition-Coarsening Model of/2 Ceramic Nanocomposites Upon Isothermal Anneal at 1300 °C, *J. Am. Ceram. Soc.*, 2012, **95**(7), 2290–2297.
- 29 E. I. Ricohermoso, F. Klug, H. Schlaak, R. Riedel and E. Ionescu, Electrically conductive silicon oxycarbide thin films prepared from preceramic polymers, *Int. J. Appl. Ceram. Technol.*, 2022, **19**(1), 149–164.
- 30 B. Matović, B. Babić, D. Bučevac, M. Čebela, V. Maksimović, J. Pantić and M. Miljković, Synthesis and characterization of hafnium carbide fine powders, *Ceram. Int.*, 2013, **39**(1), 719–723.
- 31 S. B. Mujib, S. R. Arunachalam and G. Singh, Low-temperature synthesis of HfC/HfO₂ nanocomposites from a commercial single-source precursor, *Int. J. Ceram. Eng. Sci.*, 2023, **5**(5), e10187.
- 32 S. Lee, D.-J. Yun, S.-W. Rhee and K. Yong, Atomic layer deposition of hafnium silicate film for high mobility pentacene thin film transistor applications, *J. Mater. Chem.*, 2009, **19**(37), 6857–6864.
- 33 J. Cheng, J. Wang, X. Wang and H. Wang, Preparation and high-temperature performance of HfC-based nanocomposites derived from precursor with Hf-(O,N) bonds, *Ceram. Int.*, 2017, **43**(9), 7159–7165.
- 34 A. Roy, S. B. Mujib and G. Singh, C60 Fullerene-Reinforced Silicon Oxycarbide Composite Fiber Mats: Performance as Li-Ion Battery Electrodes, *ACS Omega*, 2024, **9**(33), 35757–35768.
- 35 Z. Ren, C. Gervais and G. Singh, Fabrication and characterization of silicon oxycarbide fibre-mats *via* electrospinning for high temperature applications, *RSC Adv.*, 2020, **10**(63), 38446–38455.



- 36 D. Barreca, A. Milanov, R. A. Fischer, A. Devi and E. Tondello, Hafnium oxide thin film grown by ALD: An XPS study, *Surf. Sci. Spectra*, 2009, **14**(1), 34–40.
- 37 L. David, R. Bhandavat, U. Barrera and G. Singh, Silicon oxycarbide glass-graphene composite paper electrode for long-cycle lithium-ion batteries, *Nat. Commun.*, 2016, **7**(1), 10998.
- 38 A. Rahma, M. M. Munir, A. Prasetyo, V. Suendo and H. Rachmawati, Intermolecular interactions and the release pattern of electrospun curcumin-polyvinyl (pyrrolidone) fiber, *Biol. Pharm. Bull.*, 2016, **39**(2), 163–173.
- 39 A. Nyczyk, C. Paluszkiwicz, A. Pyda and M. Hasik, Preceramic polysiloxane networks obtained by hydrosilylation of 1, 3, 5, 7-tetravinyl-1, 3, 5, 7-tetramethylcyclotetrasiloxane, *Spectrochim. Acta, Part A*, 2011, **79**(4), 801–808.
- 40 Y. Zhang, Y. Li, J. Shao and C. Zou, Fabrication of superhydrophobic fluorine-free films on cotton fabrics through plasma-induced grafting polymerization of 1, 3, 5, 7-tetravinyl-1, 3, 5, 7-tetramethylcyclotetrasiloxane, *Surf. Coat. Technol.*, 2015, **276**, 16–22.
- 41 R. Ghelich, H. Abdizadeh, M. R. Jahannama, F. S. Torknik and M. R. Vaezi, A different chemical route to prepare hafnium diboride-based nanofibers: Effect of chemical composition, *Int. J. Appl. Ceram. Technol.*, 2020, **17**(5), 2123–2136.
- 42 S. B. Mujib, M. Rasheed and G. Singh, Evaluating Use of Boron- and Hafnium-Modified Polysilazanes for Ceramic Matrix Minicomposites, *ACS Omega*, 2022, **7**(49), 45325–45335.
- 43 Y. Wan and X. Zhou, Formation mechanism of hafnium oxide nanoparticles by a hydrothermal route, *RSC Adv.*, 2017, **7**(13), 7763–7773.
- 44 Y. Cheng, H. Tang, G. Fang, Y. Yu, L. Wang, Y. Zhang and Z. Qiao, Microstructure and Mechanical Properties of HfC-SiC Ceramics Influenced by WC Addition, *Materials*, 2023, **16**(9), 3337.
- 45 L. Li, Y. Chu, H. Li, L. Qi and Q. Fu, Periodically twinned 6H-SiC nanowires with fluctuating stems, *Ceram. Int.*, 2014, **40**(3), 4455–4460.
- 46 Z. Li, L. Deng, I. A. Kinloch and R. J. Young, Raman spectroscopy of carbon materials and their composites: Graphene, nanotubes and fibres, *Prog. Mater. Sci.*, 2023, **135**, 101089.
- 47 M. Peña-Álvarez, E. d. Corro, F. Langa, V. G. Baonza and M. Taravillo, Morphological changes in carbon nanohorns under stress: a combined Raman spectroscopy and TEM study, *RSC Adv.*, 2016, **6**(55), 49543–49550.
- 48 D. Sharma, N. Patel, S. Panjabi and V. Patel, Structural, morphological, optical, and thermal properties of electrospun PbS/PVP-PEO nanofibers, *Ceram. Int.*, 2023, **49**(6), 8839–8846.
- 49 O. Elishav, V. Beilin, O. Rozent, G. E. Shter and G. S. Grader, Thermal shrinkage of electrospun PVP nanofibers, *J. Polym. Sci., Part B: Polym. Phys.*, 2018, **56**(3), 248–254.
- 50 T. C. Chen, C. Y. Peng, C. H. Tseng, M. H. Liao, M. H. Chen, C. I. Wu, M. Y. Chern, P. J. Tzeng and C. W. Liu, Characterization of the Ultrathin HfO_2 and Hf-Silicate Films Grown by Atomic Layer Deposition, *IEEE Trans. Electron Devices*, 2007, **54**(4), 759–766.
- 51 E. Ionescu, B. Papendorf, H.-J. Kleebe, H. Breitzke, K. Nonnenmacher, G. Buntkowsky and R. Riedel, Phase separation of a hafnium alkoxide-modified polysilazane upon polymer-to-ceramic transformation—A case study, *J. Eur. Ceram. Soc.*, 2012, **32**(9), 1873–1881.
- 52 S. B. Mujib, R. Cuccato, S. Mukherjee, G. Franchin, P. Colombo and G. Singh, Electrospun SiOC ceramic fiber mats as freestanding electrodes for electrochemical energy storage applications, *Ceram. Int.*, 2020, **46**(3), 3565–3573.
- 53 H. Ramlow, L. F. B. Ribeiro, S. Schafföner, G. Motz and R. A. F. Machado, Thermo-oxidative resistance of C-rich SiCN(O) nonwovens influenced by the pretreatment of the silazane, *J. Eur. Ceram. Soc.*, 2024, **44**(9), 5308–5318.
- 54 J. Liu, E. Ricohermoso, W. Li, X. Liu, Z. Qiao, E. Ionescu and R. Riedel, Phase composition, microstructure, and mechanical properties of polymer-derived SiOC glass-ceramics reinforced by WC particles, *J. Eur. Ceram. Soc.*, 2022, **42**(5), 1955–1962.
- 55 T. To, C. Stabler, E. Ionescu, R. Riedel, F. Célerié and T. Rouxel, Elastic properties and fracture toughness of SiOC-based glass-ceramic nanocomposites, *J. Am. Ceram. Soc.*, 2020, **103**(1), 491–499.
- 56 R. Sujith, A. Zimmermann and R. Kumar, Crack Evolution and Estimation of Fracture Toughness of HfO₂/SiCN(O) Polymer Derived Ceramic Nanocomposites, *Adv. Eng. Mater.*, 2015, **17**(9), 1265–1269.
- 57 V. Hatty, H. Kahn and A. H. Heuer, Fracture Toughness, Fracture Strength, and Stress Corrosion Cracking of Silicon Dioxide Thin Films, *J. Microelectromech. Syst.*, 2008, **17**(4), 943–947.
- 58 C. Kunka, A. Trachet and G. Subhash, Interaction of Indentation-Induced Cracks on Single-Crystal Silicon Carbide, *J. Am. Ceram. Soc.*, 2015, **98**(6), 1891–1897.
- 59 P. Colombo, J. R. Hellmann and D. L. Shelleman, Thermal Shock Behavior of Silicon Oxycarbide Foams, *J. Am. Ceram. Soc.*, 2002, **85**(9), 2306–2312.
- 60 P. Colombo, J. R. Hellmann and D. L. Shelleman, Mechanical Properties of Silicon Oxycarbide Ceramic Foams, *J. Am. Ceram. Soc.*, 2001, **84**(10), 2245–2251.
- 61 Y. Wei, Y. Yang, M. Liu, Q. Li, J. Yin and Z. Huang, Effect of HfC addition on ablation behavior of SiBCN ceramics, *Ceram. Int.*, 2020, **46**(3), 3927–3934.
- 62 K.-S. Kim, S.-H. Lee, V. Q. Nguyen, Y. Yun and S. Kwon, Ablation characteristics of rocket nozzle using HfC-SiC refractory ceramic composite, *Acta Astronaut.*, 2020, **173**, 31–44.
- 63 J. Ren, Y. Zhang, H. Hu, T. Fei and H. Li, Oxidation resistance and mechanical properties of HfC nanowire-toughened ultra-high temperature ceramic coating for SiC-coated C/C composites, *Appl. Surf. Sci.*, 2016, **360**, 970–978.
- 64 Y. Chen, W. Sun, X. Xiong, Y. Chang, Y. Xu, Z. Peng, T. Tian and Y. Zeng, Microstructure, thermophysical properties, and ablation resistance of C/HfC-ZrC-SiC composites, *Ceram. Int.*, 2019, **45**(4), 4685–4691.

