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## Facile synthesis of magnetic core–shell structures for tunable microwave absorption†

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The rapid development of electronic communication and radar technologies in the 5G era has exacerbated electromagnetic pollution, thereby driving the urgent need for cutting-edge microwave absorption materials. In this study, a novel SnCo/C@MoS<sub>2</sub> composite was proposed, and the core–shell structure was synthesized *via* electrospinning and hydrothermal methods. This composite uniquely integrated the high conductivity and magnetic properties of Sn and Co while capitalizing on the superior dielectric performance of MoS<sub>2</sub> nanosheets, which are uniformly grown on carbon nanofibers. This design capitalized on the synergistic effects of a one-dimensional (1D) carbon fiber (CF) framework and two-dimensional (2D) MoS<sub>2</sub> nanostructures, enhancing interfacial polarization and multi-loss mechanisms. SnCo/C@MoS<sub>2</sub> exhibited remarkable microwave absorption properties, achieving a minimum reflection loss (RL<sub>min</sub>) of −64.27 dB at a thickness of 1.52 mm and an effective absorption bandwidth (EAB) of 5.20 GHz. Moreover, computer simulation technology (CST) demonstrated that SnCo/CNF@MoS<sub>2</sub> simulated radar cross-section (RCS) values fell below −20 dB m<sup>2</sup>. These results demonstrated a substantial improvement in absorption performance compared to the individual SnCo/CNF and MoS<sub>2</sub> components. This work underscored the effectiveness of combining 1D and 2D materials to obtain core–shell structures for superior electromagnetic wave (EMW) attenuation.

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### 1. Introduction

With the advent of the 5G era, electronic communication and radar detection technologies are widely used in both civilian and military fields, significantly improving quality of life.<sup>1</sup> However, the widespread use of high-frequency electronic equipment generates EMWs that may pose a serious threat to human health and communication security, leading to a new form of pollution. This issue has attracted widespread societal attention. Air pollution, water pollution, noise pollution, and electromagnetic radiation are now defined as the four major sources of pollution. Consequently, the demand for electromagnetic shielding and microwave absorption materials is increasing. Currently, there are two primary methods to address electromagnetic pollution: electromagnetic shielding

and electromagnetic absorption, with the latter being the most effective.<sup>2–4</sup> Therefore, extensive research on EMW-absorbing materials is urgently needed.

Carbon materials, such as carbon nanofibers (CNFs),<sup>5</sup> carbon nanotubes (CNTs)<sup>6</sup> and graphene,<sup>7</sup> are typical dielectric loss absorbers. In particular, CNFs offer unique advantages in 1D wave absorption due to their high specific surface area, low density, high aspect ratio, and stable chemical properties.<sup>8</sup> A simple and efficient electrospinning technique is typically employed to produce stable magnetic CF. While CNF materials loaded with a single magnetic metal have been extensively studied, their loss mechanism remains relatively simple, leading to suboptimal impedance matching and inadequate EMW attenuation. Consequently, combining lightweight carbon-based materials with various magnetic absorbers can diversify loss mechanisms and improve impedance matching to some extent. Common magnetic absorbing materials include magnetic metal powders, metal oxides, and ferrites. Zhang *et al.* prepared multi-phase carbon-coated FeSn<sub>2</sub>/Sn nanocomposites by an *in situ* arc discharge method and achieved effective absorption across the 9–18 GHz range.<sup>9</sup> Hu *et al.* prepared CoNi/C nanofibers with excellent absorption properties by adjusting the ratio of Co and Ni. When the Co/Ni ratio was 1/3, the matching thickness was 2.4 mm and the RL<sub>min</sub> was −71.2 dB. In addition, the maximum EAB (EAB<sub>max</sub>)

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reached 5.9 GHz, covering the entire Ku band.<sup>10</sup> Shen *et al.* showed that NiFe<sub>2</sub>O<sub>4</sub>/NiO/CNF exhibited an EAB of 8 GHz when the load in paraffin was 50%, and the content of FeNi/NiFe<sub>2</sub>O<sub>4</sub>/NiO/CNF in paraffin was only 5%, with an RL<sub>min</sub> of -37.4 dB at 12.8 GHz. However, the EAB of 4.3 GHz was narrowed.<sup>11</sup> Therefore, the combined use of CF and a variety of magnetic absorbing materials is insufficient to further improve the EMW absorption performance and broaden the effective absorption bandwidth.

2D layered nanostructured materials (TDMs) like graphene,<sup>12</sup> black phosphorus,<sup>13</sup> MoS<sub>2</sub>,<sup>14</sup> WS<sub>2</sub>,<sup>15</sup> and MXene<sup>16</sup> have gained significant attention as potential next-generation microwave absorbers due to their lightweight, strong absorption coefficients, and thin structures. Among these, MoS<sub>2</sub> stands out due to its low cost, high specific surface area, and unique electrical and optical properties, making it particularly promising for electromagnetic attenuation in electronic and optoelectronic devices.<sup>17,18</sup> Its exceptional photoelectric properties enhance conductive and polarization losses, leading to superior attenuation performance and impedance matching compared to traditional carbon-based dielectric materials. Sun *et al.* regulated the microwave absorption performance of MoS<sub>2</sub> by constructing various microscopic interface structures, finding that different van der Waals heterogeneous structures yielded distinct absorption characteristics. Notably, 2D MoS<sub>2</sub>/3D carbon layers achieved an RL<sub>min</sub> of -69.2 dB with an EAB of 4.88 GHz.<sup>19</sup> Similarly, Xu *et al.* enhanced absorption by coating hollow carbon spheres (MHCSs) with a MoS<sub>2</sub> layer, forming core-shell nanospheres (MHCS@MoS<sub>2</sub>) that provided an EAB of 6.21 GHz at a matching thickness of 2.1 mm.<sup>20</sup> Zhao *et al.* spun Mil88 A into CNFs by electrospinning and grew MoS<sub>2</sub> on the surface of CF, which formed a nanorod heterostructure with a magnetic flower shape (CF-Mil88 A@MoS<sub>2</sub>) with an RL of -70 dB at a thickness of 2.5 mm and an EAB of 4.68 GHz.<sup>21</sup> Although previous studies have investigated composites of magnetic and dielectric materials for EMW absorption, achieving strong absorption, broad bandwidth, and lightweight structures simultaneously remains challenging. This study addresses these limitations by designing a core-shell SnCo/C@MoS<sub>2</sub> composite that exploits the synergistic effects of 1D/2D hybrid structures to enhance EMW attenuation.

Based on the favorable magnetic properties of Sn and Co and the excellent electrical conductivity of MoS<sub>2</sub>, this paper employs highly conductive CF as the base of Sn and Co and wraps a layer of MoS<sub>2</sub> on the fiber surface, thereby combining the morphological advantages of 1D CNFs with the unique nanostructure of the 2D material MoS<sub>2</sub>. SnCo/C@MoS<sub>2</sub> is prepared, its microstructure and electromagnetic properties are studied, and the mechanism of synergistic enhancement of the absorbing properties of Sn, Co and MoS<sub>2</sub> composites is discussed.

## 2. Experimental section

### 2.1 Materials

Stannous chloride dihydrate (SnCl<sub>2</sub>·2H<sub>2</sub>O, 99%, Sinopharm Chemical Reagent Co., Ltd (SCRC)), cobalt nitrate hexahydrate

(Co(NO<sub>3</sub>)<sub>2</sub>·6H<sub>2</sub>O, 99%, SCRC), *N,N*-dimethylformamide (DMF, 99.5%, SCRC), sodium molybdate dihydrate (Na<sub>2</sub>MoO<sub>4</sub>·2H<sub>2</sub>O, 99%, SCRC), thioacetamide (C<sub>2</sub>H<sub>5</sub>NS, 99%, SCRC) and polyacrylonitrile (PAN, *M*<sub>w</sub> = 150 000, Shanghai Aladdin Bio-Chem. Technology Co., Ltd).

### 2.2 Synthesis of SnCo/C@MoS<sub>2</sub>

**2.2.1 Synthesis of SnCo/CNF.** A mixture of 1.6 g PAN and 18 mL DMF was magnetically stirred at 70 °C for 12 h, followed by the addition of 1 mmol SnCl<sub>2</sub>·2H<sub>2</sub>O and 1 mmol Co(NO<sub>3</sub>)<sub>2</sub>·6H<sub>2</sub>O and stirring for another 12 h to form the precursor solution. SnCo/PAN fibers were obtained through electrospinning and then collected and dried at 50 °C for 10 h. SnCo/CNF was obtained by pre-carbonizing the dried SnCo/PAN at 280 °C for 2 h to stabilize the fiber structure and carbonizing at 800 °C for 3 h under a nitrogen atmosphere. Sn/CNF and Co/CNF were also prepared as control samples.

**2.2.2 Synthesis of SnCo/C@MoS<sub>2</sub>.** C<sub>2</sub>H<sub>5</sub>NS (0.64 g) and Na<sub>2</sub>MoO<sub>4</sub>·2H<sub>2</sub>O (0.32 g) were dissolved in 80 mL deionized water, stirred magnetically for 1 h, and then 0.2 g SnCo@CNF nanofibers were dispersed in the solution and reacted at 200 °C for 24 h. The mixture was centrifuged and washed with ethanol and deionized water three times each. The resulting precipitate was freeze-dried to obtain SnCo/C@MoS<sub>2</sub>. It should be noted that Sn/CNF, Co/CNF, SnCo/CNF, and SnCo/C@MoS<sub>2</sub> were referred to as SC, CC, SCC, and SCCM, respectively.

### 2.3 Characterization

The surface morphology and micro-composition of the materials were analyzed using a scanning electron microscope (SEM, Sigma 300) coupled with a scanning energy dispersive spectrometer (EDS). The crystal structure was analyzed using an X-ray diffractometer (XRD, Shimadzu XRD-7000). The degree of graphitization was characterized by Raman spectroscopy (Thermo DXR2). Fourier transform infrared spectroscopy (FTIR, Shimadzu IRTracer 100) was used to detect the chemical bonds in the molecules and analyze the molecular structure characteristics of the samples. X-ray photoelectron spectroscopy (XPS, Thermo Scientific Nexsa) was used to characterize the chemical composition and valence state of the material. Static magnetic properties were measured using a vibrating sample magnetometer (VSM, Lake Shore 7307). The electromagnetic parameters of the samples prepared as paraffin rings (2–18 GHz) were analyzed using a vector network analyzer (VNA, Agilent A N5244A).

## 3. Results and discussion

### 3.1 Microstructure and component

The synthesis process of SnCo/C@MoS<sub>2</sub> by electrospinning and hydrothermal techniques is shown in Fig. 1a. Electrospinning produced 1D CNFs as the matrix, which interwove with each other to form a three-dimensional (3D) conductive network with magnetic particles loaded onto the CNF.<sup>22</sup> Hydrothermal growth of 2D nanosheets onto the fiber surface

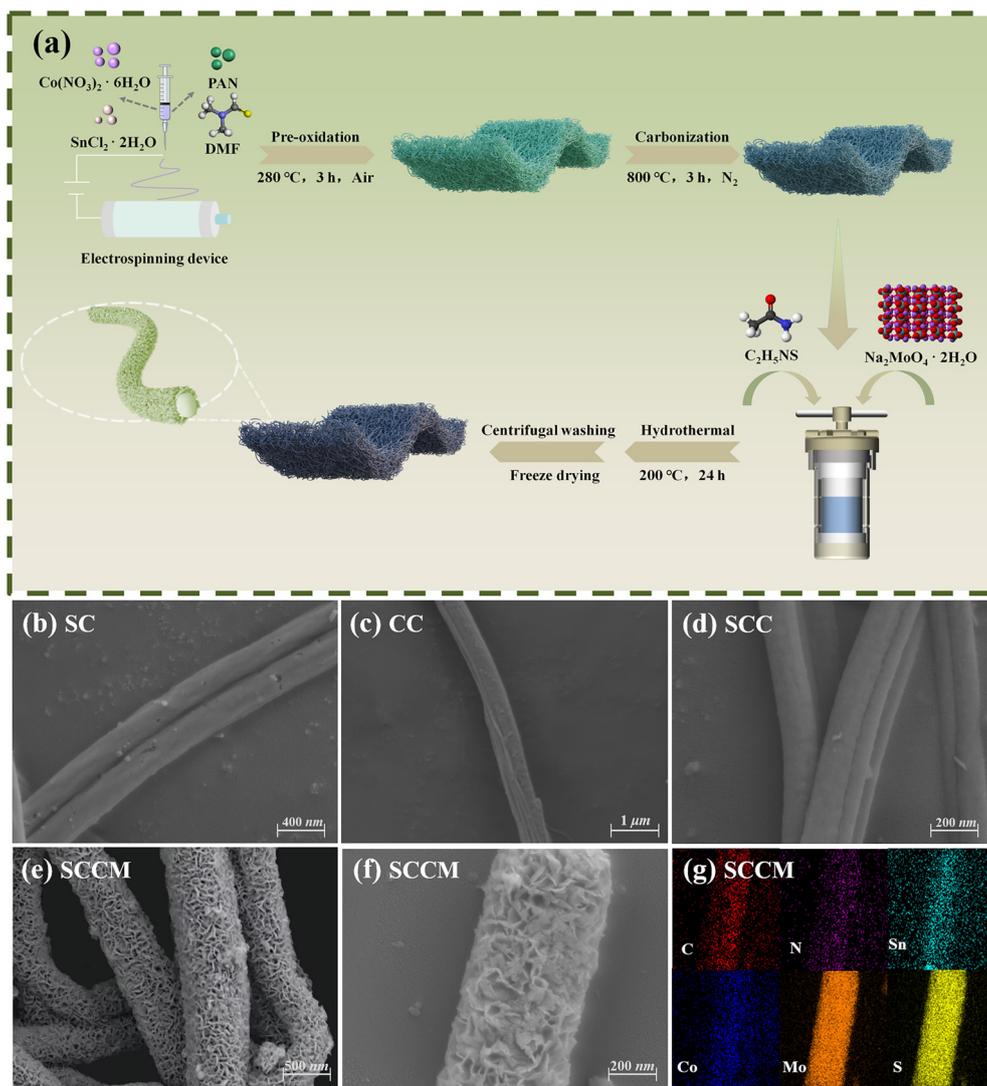


Fig. 1 Schematic of the preparation process of SCCM (a); SEM of SC (b), CC (c), SCC (d) and SCCM (e and f); elemental mapping analysis of SCCM (g).

forming a core-shell structure lengthened the multiple reflection loss paths. In Fig. 1b–g, SEM images of SC, CC, SCC and SCCM and EDS spectra of SCCM are shown. Observation of the morphological features of SC and CC samples (Fig. 1b, c and Fig. S1a†) revealed that Sn and Co particles made the surface of CNF rough. As can be seen from Fig. 1d, small bumps were uniformly distributed on the surface of CNF, a result of the nanoscale SnCo alloy being anchored on the surface of CNF. Fig. S1b† clearly displays the SnCo alloy topography of SCC. Fig. S1c–f† show the distribution of elements C, N, Sn and Co of SCC respectively, where Sn and Co were uniformly distributed, indicating the existence of SnCo alloys. Fig. 1e and f clearly demonstrate the successful growth of MoS<sub>2</sub> nanosheets to form core-shell structures on the SCC fiber surface. The large specific surface area of MoS<sub>2</sub> nanosheets can prolong the reflection path of EMWs, and the high dielectric properties of MoS<sub>2</sub> were conducive to conduc-

tive losses. Fig. 1g shows the EDS diagram of SCCM (Fig. 1f) with a uniform distribution of C, N, Sn, Co, Mo and S elements, proving that SnCo/C@MoS<sub>2</sub> was successfully prepared.<sup>23</sup> Furthermore, the similar distribution patterns of Sn with Co and Mo with S underpin the formation of the SnCo alloy and MoS<sub>2</sub>.

XRD patterns of SC, CC, SCC, and SCCM samples and PDF cards of SnCo alloys and MoS<sub>2</sub> are shown in Fig. 2a. The SC sample had obvious peaks at  $2\theta$  of  $30.64^\circ$ ,  $32.02^\circ$  and  $44.90^\circ$ , corresponding to the (200), (101) and (211) crystal faces of Sn, respectively. The CC sample had obvious peaks at  $44.22^\circ$ ,  $51.52^\circ$ , and  $75.85^\circ$ , corresponding to the (111), (200), and (220) crystal faces of Co, respectively. In addition, SC and CC had gentle peaks at  $2\theta$  of  $25^\circ$ , indicating that PAN fibers were directly transformed into amorphous carbon during carbonization.<sup>24</sup> The SCC sample had peaks at  $2\theta$  of  $28.49^\circ$ ,  $33.93^\circ$ ,  $45.07^\circ$ ,  $55.66^\circ$ ,  $57.56^\circ$ , and  $71.40^\circ$ , representing the (101),

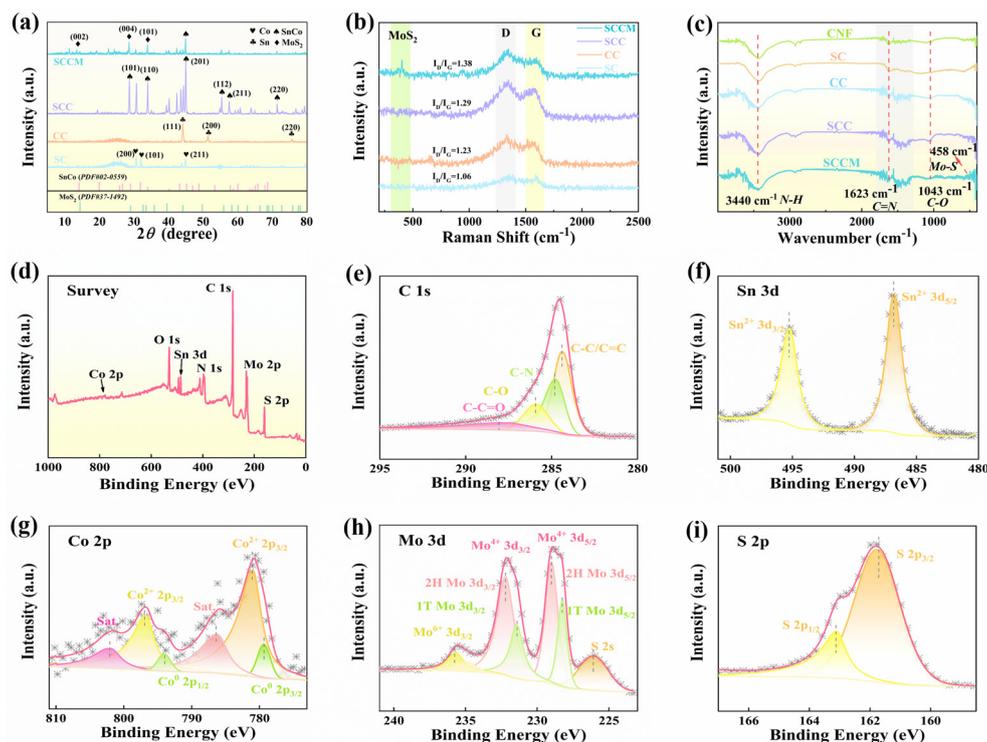


Fig. 2 XRD pattern (a); Raman spectrum (b); FTIR spectra of SC; CC, SCC and SCCM (c); XPS survey spectra (d), C 1s (e), Sn 3d (f), Co 2p (g), Mo 3d (h) and S 2p (i) of SCCM.

(110), (201), (112), (211), and (220) crystal faces of the SnCo alloy (PDF#02-0559), respectively. SCCM corresponded to the (002), (004) and (101) crystal faces of MoS<sub>2</sub> (PDF#37-1492) at  $2\theta$  of  $14.37^\circ$ ,  $29.02^\circ$  and  $33.51^\circ$ , respectively.<sup>25</sup> As a result, a portion of Sn and Co formed an SnCo alloy, and a (002) crystal face appeared in the SCCM at  $14.37^\circ$ , which meant that MoS<sub>2</sub> was successfully coated on the SCC surface, in contrast to the SCC.

The degree of graphitization in carbon materials affected their electromagnetic parameters and microwave absorption properties.<sup>26</sup> Thus, analyzing graphitization through Raman spectroscopy was necessary.<sup>27</sup> Fig. 2b displays the Raman spectra of the samples, all of which exhibited strong vibration peaks at the D band ( $1349\text{ cm}^{-1}$ ) and G band ( $1587\text{ cm}^{-1}$ ), corresponding to lattice defects in graphite carbon atoms and the tensile vibration of  $\text{sp}^2$  hybridized carbon, respectively.<sup>28</sup> The  $I_D/I_G$  ratio reflected the degree of graphitization, with a higher  $I_G$  peak indicating greater graphitization. In Fig. 2b, the  $I_D/I_G$  ratios for SC, CC, SCC, and SCCM were 1.06, 1.23, 1.29, and 1.38, respectively. Obviously, the degree of graphitization decreased successively, and it is worth mentioning that the degree of graphitization was the lowest in the SCCM sample, which was attributed to the large number of defects brought about by the introduction of MoS<sub>2</sub>. In addition, SCCM exhibited two small peaks at  $370\text{ cm}^{-1}$  and  $400\text{ cm}^{-1}$  that are characteristic peaks of MoS<sub>2</sub>, which are attributed to the first-order Raman vibration mode of S.<sup>29</sup> The edge termination structure at  $400\text{ cm}^{-1}$  was dominant, which was conducive to electron transition and increased conductive loss.<sup>30</sup>

The bonding mode was interpreted using infrared spectroscopy. The characteristic absorption peaks of CNF, SC, CC, SCC and SCCM are shown in Fig. 2c. A prominent absorption peak at  $3340\text{ cm}^{-1}$  corresponded to the stretching vibrations of O–H, N–H, or C–H bonds, confirming the presence of hydrogen bonds within the material. A subtle peak around  $1623\text{ cm}^{-1}$  was attributed to C=N stretching, originating from the vibrations of C–N and C=C bonds within the benzene ring. The absorption peak at  $1043\text{ cm}^{-1}$  was associated with the single bond vibration of C–O. In addition, the peak at  $458\text{ cm}^{-1}$  in SCCM, attributed to Mo–S vibrations, confirmed the successful growth of MoS<sub>2</sub> on the SCC surface.<sup>31</sup>

The XPS analysis of the chemical states of C, Sn, Co, Mo, and S in SCCM samples is presented in Fig. 2d–i. The full spectrum of the SCCM sample is shown in Fig. 2d. Fig. 2e depicts four fitting peaks of C 1s, corresponding to distinct bonding states including C–C/C=C ( $284.8\text{ eV}$ ), C–N ( $285.0\text{ eV}$ ), C–O ( $285.9\text{ eV}$ ), and C–C=O ( $288.1\text{ eV}$ ).<sup>32,33</sup> The presence of the C–C=O bond indicated oxygen involvement during PAN pyrolysis to form carbon. In Fig. 2f, the Sn 3d spectrum exhibited two symmetric peaks, assigned to  $\text{Sn}^{2+} 3d_{5/2}$  ( $486.8\text{ eV}$ ) and  $\text{Sn}^{2+} 3d_{3/2}$  ( $495.3\text{ eV}$ ) states.<sup>34</sup> Fig. 2g shows that the Co 2p spectrum comprises six peaks, indicating the presence of Co in two oxidation states, Co<sup>0</sup> and Co<sup>2+</sup>. Co<sup>0</sup>  $2p_{3/2}$  and Co<sup>0</sup>  $2p_{1/2}$  peaks appeared at binding energies of  $779.4\text{ eV}$  and  $794.1\text{ eV}$ , respectively, while Co<sup>2+</sup>  $2p_{3/2}$  and Co<sup>2+</sup>  $2p_{1/2}$  were observed at  $781.1\text{ eV}$  and  $796.9\text{ eV}$ . Additionally, satellite peaks (Sat.) were located at  $785.4\text{ eV}$  and  $802.1\text{ eV}$ .<sup>35,36</sup> In Fig. 2h, the deconvoluted Mo 3d

spectrum confirmed the presence of Mo in multiple valence states ( $\text{Mo}^0$ ,  $\text{Mo}^{4+}$ , and  $\text{Mo}^{6+}$ ) and the coexistence of 1T and 2H phases in SCCM. Peaks at 228.3 eV ( $\text{Mo } 3d_{5/2}$ ) and 231.4 eV ( $\text{Mo } 3d_{3/2}$ ) corresponded to the metallic 1T phase of  $\text{MoS}_2$ ,<sup>37</sup> while those at 228.9 eV ( $\text{Mo } 3d_{5/2}$ ) and 232.2 eV ( $\text{Mo } 3d_{3/2}$ ) represented the semiconducting 2H phase.<sup>38,39</sup> In Fig. 2i, binding energies at 226.1 eV (S 2s) and 235.8 eV ( $\text{Mo}^{6+} 3d_{3/2}$ ) indicated the formation of Mo–S bonds and partial oxidation of  $\text{MoS}_2$  to  $\text{Mo}^{6+}$ .<sup>40</sup> The S 2p spectrum was deconvoluted into two peaks, S 2p<sub>3/2</sub> (161.7 eV) and S 2p<sub>1/2</sub> (163.1 eV), confirming that  $\text{MoS}_2$  grew on the CNF surface.<sup>41</sup>

### 3.2. Magnetic performance

Magnetostatic analysis (VSM) was performed on SC, CC, SCC and SCCM samples in order to understand the magnetic properties of the samples in depth, as shown in Fig. 3 and Table 1. Under external magnetic fields of  $-30\,000$  to  $30\,000$  Oe, the hysteresis loops of SC, CC, SCC and SCCM samples exhibit a typical S-shape (Fig. 3a), indicating that the magnetization reached a saturation state, which led to favorable magnetic losses.<sup>42</sup> It can be seen from Table 1 that the saturation magnetization ( $M_s$ ) values of CC, SCC and SCCM samples were 25.06, 9.08 and 6.20  $\text{emu g}^{-1}$ , respectively (where SC was not magnetic). The  $M_s$  values of SCC and SCCM decreased in turn, due to the non-magnetic Sn loading on the CNF and the non-magnetic  $\text{MoS}_2$  coating on the SCC fiber surface.<sup>43,44</sup> In Fig. 3b, the remanent magnetization ( $M_r$ ) values of CC, SCC and SCCM samples were 6.22, 2.35 and 1.57  $\text{emu g}^{-1}$ , respectively. High coercivity ( $H_c$ ) meant high magnetic anisotropy. The  $H_c$  of the SCCM sample was 190.90 Oe, higher than those of CC and SCC (114.56 and 167.89 Oe), indicating that SCCM had prominent magnetic anisotropy, which increased the demagnetization energy and prevented the reversal of magnetic domains.

### 3.3. Microwave property analysis

**3.3.1 Microwave absorption performance.** Based on transmission line theory,<sup>45</sup> the EMW absorption properties of materials can be assessed through impedance ( $Z_{\text{in}}$ ) and RL,

**Table 1**  $M_s$ ,  $M_r$  and  $H_c$  of SC, CC, SCC and SCCM

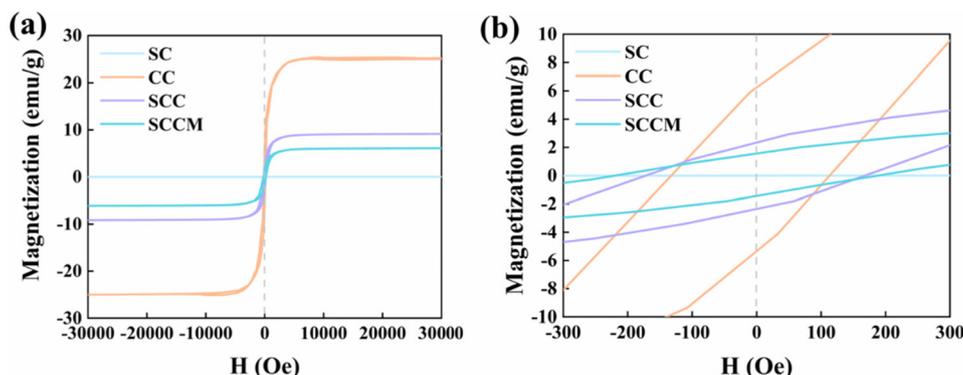
Samples	$M_s$ ( $\text{emu g}^{-1}$ )	$M_r$ ( $\text{emu g}^{-1}$ )	$H_c$ (Oe)
SC	—	—	—
CC	25.06	6.22	114.56
SCC	9.08	2.35	167.89
SCCM	6.20	1.57	190.90

both in the medium and in free space, as shown in eqn (1) and (2):

$$Z_{\text{in}} = Z_0 \sqrt{\frac{\mu_r}{\epsilon_r}} \tanh \left[ j \frac{2\pi f d}{c} \sqrt{\mu_r \epsilon_r} \right] \quad (1)$$

$$\text{RL} = 20 \lg \left| \frac{Z_{\text{in}} - Z_0}{Z_{\text{in}} + Z_0} \right| \quad (2)$$

In the formula,  $Z_0$  represents the air impedance,  $\mu_r$  denotes the relative permeability,  $\epsilon_r$  signifies the relative dielectric constant,  $f$  indicates the incident EMW frequency (Hz),  $d$  refers to the sample thickness (mm), and  $c$  stands for the speed of light in a vacuum.<sup>46</sup> When evaluating the performance of EMW absorbing materials, the primary index used was RL. The RL of  $-10$  dB indicated that 90% of the EMW was absorbed, while  $\text{RL} < -10$  dB corresponded to the EAB of the material.<sup>47</sup> As shown in Fig. 4a–d, the  $\text{RL}_{\text{min}}$  of SC was  $-28.85$  dB (10.94 GHz,  $d = 2.13$  mm), and the  $\text{EAB}_{\text{max}}$  was 4.73 GHz (13.28–18 GHz,  $d = 1.5$  mm). As shown in Fig. 4e–h, the  $\text{RL}_{\text{min}}$  of CC was  $-20.61$  dB (7.42 GHz,  $d = 2.79$  mm), and the  $\text{EAB}_{\text{max}}$  was 5.04 GHz (12.96–18 GHz,  $d = 1.58$  mm). Sample SC primarily absorbed X and Ku-band EMWs, while CC absorbed C, X, and Ku-band waves, offering broader coverage and a larger EAB than SC, mainly due to the presence of cobalt as a magnetic element. However, despite its wave-absorbing properties, CC exhibited unsatisfactory thickness and RL values. By preparing bimetallic CF SnCo/C, we aimed to address the issues of excessive thickness and low RL values. As illustrated in Fig. 4i–l, SCC exhibited an  $\text{RL}_{\text{min}}$  of  $-59.49$  dB (4.74 GHz,  $d = 5.67$  mm) and an  $\text{EAB}_{\text{max}}$  of 4.94 GHz (7.02–11.96 GHz,  $d = 3.1$  mm). While the RL of SCC required significant enhancement, it



**Fig. 3** Hysteresis loops (a) of SC, CC, SCC, and SCCM and enlarged view of hysteresis loops (b).

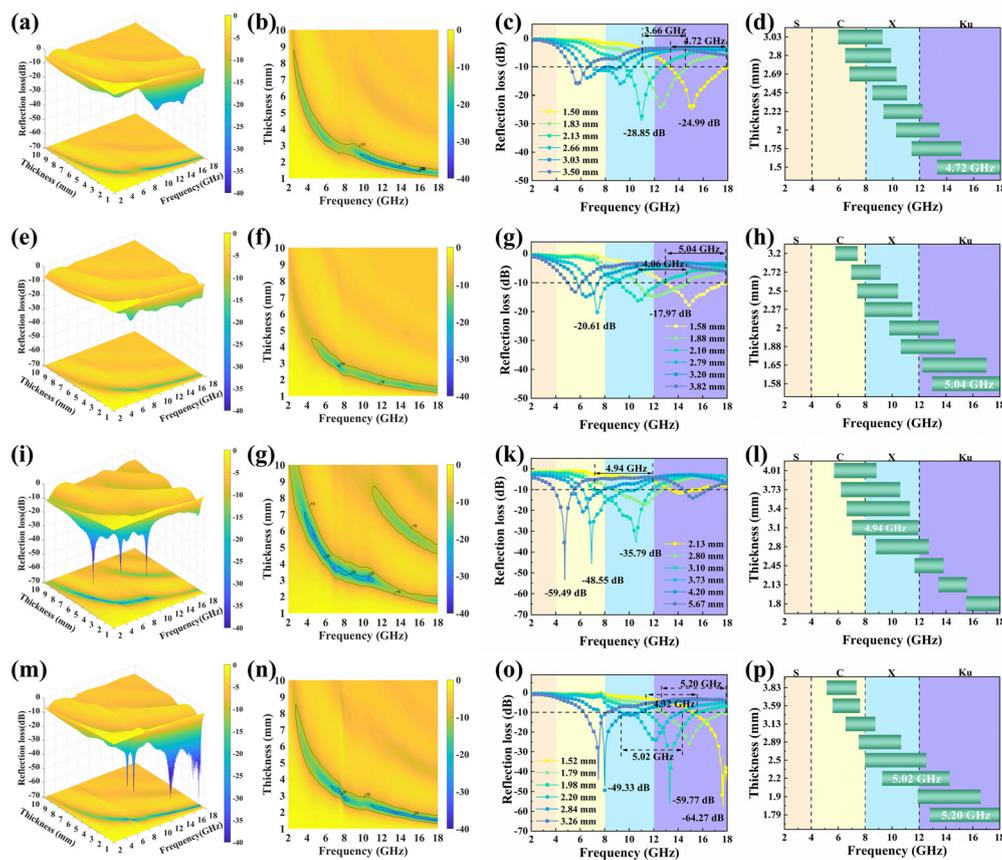


Fig. 4 3D and 2D RL and EAB curves of SC (a–d), CC (e–h), SCC (i–l) and SCCM (m–p).

paradoxically resulted in increased thickness. Remarkably, incorporating high-conductivity MoS<sub>2</sub> onto the SnCo/CNF surface enabled the attainment of reduced thickness alongside heightened attenuation.<sup>48</sup> Fig. 4m–p illustrates the presence of three prominent absorption peaks at thicknesses of 1.52 mm, 1.98 mm, and 2.84 mm, corresponding to RL values of –64.27 dB (17.68 GHz), –59.77 dB (13.32 GHz), and –49.33 dB (8.00 GHz), respectively, with EAB surpassing 3.2 GHz. Notably, Fig. 4p indicates that the absorption band of SCCM spanned the entire 2–18 GHz range. A longitudinal comparison of the EAB between SCC and SCCM, as demonstrated in Fig. 4l and p, revealed that while the EAB of SCC was primarily centered around the X-band, the EAB of SCCM extended significantly into higher frequency regions, encompassing the entire X and Ku bands and exceeding 5 GHz in this spectrum, attributed to the elevated conductivity of magnetic metals Co and MoS<sub>2</sub>. Table 2 displays RL<sub>min</sub>, corresponding thickness at RL<sub>min</sub> (dRL<sub>min</sub>), and EAB values. Through comparison, it was evident that the SCC coated with a MoS<sub>2</sub> layer in this study achieved commendable RL<sub>min</sub>, thickness, and EAB, with the SCCM fiber demonstrating outstanding EMW absorption capabilities. As indicated in Table 2, the fabricated SCCM nanofibers exhibited minimal thickness (1.52 mm), excellent RL<sub>min</sub> (–64.27 dB), and relatively high EAB (5.20 GHz). In accordance

Table 2 Recent research on MoS<sub>2</sub> composites and their EMW absorption performance

Sample	RL <sub>min</sub> (dB)	dRL <sub>min</sub> (mm)	EAB (GHz)	Ref.
MoS <sub>2</sub> /Ni	–44.70	2.60	2.8	50
CNT@MoS <sub>2</sub>	–66.80	1.60	4.8	51
Co/CoS <sub>2</sub> @NC@MoS <sub>2</sub>	–43.90	3.50	4.40	52
CoZn/C@MoS <sub>2</sub>	–41.50	4.50	4.58	53
MoS <sub>2</sub> @C@CoFe <sub>2</sub> O <sub>4</sub>	–47.70	2.40	3.50	54
CoFe <sub>2</sub> O <sub>4</sub> @1T/2H-MoS <sub>2</sub>	–68.5	1.81	4.56	55
MoS <sub>2</sub> /CoNi	–41.44	2.00	5.60	56
Co <sub>3</sub> SnC <sub>0.7</sub> /CNF	–21.7	2.00	5.92	57
SCCM	–64.27	1.52	5.20	This work

with the current trends in microwave absorption materials, key attributes included “thin thickness, light weight, broad bandwidth, and high loss”.<sup>49</sup>

**3.3.2. Electromagnetic parameters and absorption mechanism.** Analyzing the electromagnetic characteristic parameters enabled the evaluation of a material’s response capability and absorption performance under EMWs.<sup>58</sup> The two fundamental parameters characterizing the electromagnetic properties of materials—complex permittivity ( $\epsilon_r$ ) and complex permeability

( $\mu_r$ )—were employed to assess the attenuation capacity of EMWs, as shown below (eqn. (3)–(6)):

$$\epsilon_r = \epsilon' - j\epsilon'' \quad (3)$$

$$\mu_r = \mu' - j\mu'' \quad (4)$$

$$\tan \delta_\epsilon = \frac{\epsilon''}{\epsilon'} \quad (5)$$

$$\tan \delta_\mu = \frac{\mu''}{\mu'} \quad (6)$$

In electromagnetism, the real component of the dielectric constant ( $\epsilon'$ ) reflected a material's ability to store electromagnetic energy, whereas the imaginary component ( $\epsilon''$ ) denoted its ability to absorb and dissipate energy. The real and imaginary components of magnetic permeability ( $\mu$ ) corresponded to the material's energy storage density and its magnetic dissipation capability, respectively. The dielectric loss angle tangent ( $\tan \delta_\epsilon$ ) and magnetic loss angle tangent ( $\tan \delta_\mu$ ) were

employed to assess the material's dissipative properties.<sup>59</sup> Fig. 5 depicts the changes in electromagnetic parameters ( $\epsilon'$ ,  $\epsilon''$ ,  $\mu'$ , and  $\mu''$ ) and the corresponding tangents of electromagnetic loss for both SCCM and SCC. As seen in Fig. 5a and c,  $\epsilon'$  exhibited a declining trend as frequency increased. For example, the  $\epsilon'$  of SCC decreased from 8.68 GHz to 6.13 GHz, and SCCM decreased from 12.97 GHz to 7.27 GHz. This can be attributed to the dispersion effect, where the displacement current in an alternating electric field failed to keep pace with the accumulated potential.<sup>60</sup> The permeability ( $\mu$ ) of SCCM was comparatively lower than that of SCC, as MoS<sub>2</sub> nanosheets were non-magnetic, and their incorporation dilutes the magnetic properties of SCC. A comparison of Fig. 5b and d showed that the  $\tan \delta_\epsilon$  for SCC fluctuated around 0.3, while SCCM fluctuated around 0.5, indicating that SCCM had superior electrical conductivity, which was attributed to the unique structure of MoS<sub>2</sub> inducing electrons to move along the 3D network of CNF. This resulted in conductive loss.<sup>61</sup> The SCCM sample exhibited a peak at 10 GHz, which was attributed to interfacial

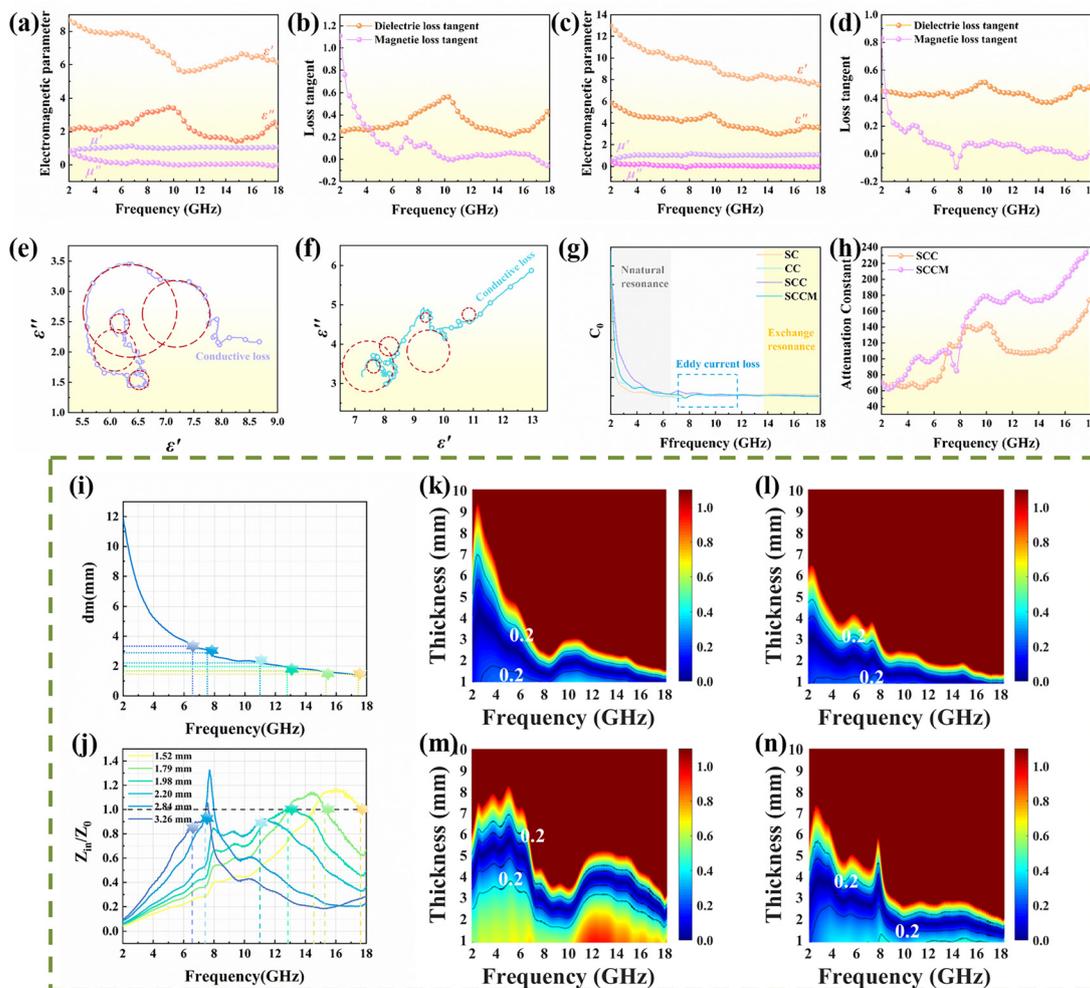


Fig. 5 Electromagnetic parameters of SCC (a) and SCCM (c) and the loss tangent of SCC (b) and SCCM (d); Cole–Cole of SCC (e) and SCCM (f);  $C_0$  curve diagram (g); attenuation constant (h); 1/4 wavelength matching (i) and 2D Z curves of SCCM (j); colorful contour maps of  $|\Delta|$  for SC (k), CC (l), SCC (m) and SCCM (n).

polarization arising from the differing conductive properties of MoS<sub>2</sub> and SnCo/CNF. As shown in Fig. 5b, 4 GHz marked the turning point: below this frequency, the tangent of tan δ<sub>μ</sub> exceeded that of tan δ<sub>ε</sub>, indicating magnetic loss as the dominant mechanism. Above 4 GHz, the electrical loss became dominant. As depicted in Fig. 5d, the SCCM sample consistently showed a higher tan δ<sub>ε</sub> compared to the tan δ<sub>μ</sub> across the 2–8 GHz frequency range, suggesting that electrical loss was the dominant mechanism throughout the microwave phase. This was attributed to the incorporation of high-dielectric MoS<sub>2</sub>.

In the microwave phase, the primary polarization types were interface and dipole polarization, with the Cole–Cole curve employed to elucidate the polarization mechanism in detail (eqn (7) and (8)). Each semicircle represented a Debye polarization relaxation, with more complex semicircles indicating a greater number of relaxation types within the material,<sup>62,63</sup> resulting in stronger polarization loss. There were long linear tails indicating conductive losses.

$$\left(\epsilon' - \frac{\epsilon_s - \epsilon_\infty}{2}\right)^2 + (\epsilon'')^2 = \left(\frac{\epsilon_s - \epsilon_\infty}{2}\right)^2 \quad (7)$$

$$\epsilon' = \epsilon_\infty + \frac{1}{\tau} \left(\frac{\epsilon''}{\omega}\right) \quad (8)$$

The parameters ε<sub>s</sub>, ε<sub>∞</sub>, τ, and ω in the above formula corresponded to the low-frequency electrostatic permittivity, high-frequency relative permittivity, relaxation time, and angular frequency, respectively. The Cole–Cole curves for SC, CC, SCC, and SCCM are shown in Fig. S2a and b† and Fig. 5e and f. It was evident that dual loss mechanisms, namely polarization relaxation and conduction loss, were present. With the addition of Co, Sn, and MoS<sub>2</sub> to CNF, the number of semicircles increased, among which SCCM had the most semicircles compared with other samples, indicating that SCCM samples had more diverse relaxation types and stronger loss capacity to EMWs, which was attributed to the formation of new heterostructures after the introduction of high-dielectric MoS<sub>2</sub> (MoS<sub>2</sub>-CNF). Interfacial polarization and dipole polarization can occur in many locations, including Co–Sn, Co–CNF, Sn–CNF, MoS<sub>2</sub>-CNF, *etc.*<sup>64</sup> In addition, SCCM had an obvious long tail, suggesting that the sample not only had excellent polarization relaxation loss but also had strong conductive loss. The CNF, MoS<sub>2</sub>, and SnCo metal particles generated induced currents when exposed to alternating electromagnetic fields, thereby transforming electromagnetic energy into heat and contributing to conductive loss. This dual-loss mechanism served as the basis for improving the EMW absorption capability of SCCM. The C<sub>0</sub> curve in Fig. 5g depicts the magnetic loss mechanisms including natural resonance, eddy current loss, and exchange resonance observed in SC, CC, SCC, and SCCM samples across the 2–18 GHz range.<sup>65,66</sup> Based on Aharoni's theory,<sup>67</sup> natural resonance primarily occurred at low frequencies, eddy current loss was observed in the mid-frequency range, and exchange resonance dominated at high frequencies. During the initial segment of the C<sub>0</sub> curve (2–6 GHz), all samples exhibited a dis-

tinct decline and fluctuation, suggesting the presence of natural resonance at low frequencies, attributed to the anisotropy induced by the small size of Sn and Co nanoparticles loaded onto the CNF.<sup>68</sup> In the mid- to high-frequency range of the C<sub>0</sub> curve (6–18 GHz), the C<sub>0</sub> value remained stable, indicating that eddy current loss and exchange resonance were the predominant mechanisms. Consequently, it can be inferred that the magnetic loss mechanism varies across frequency ranges, with all mechanisms contributing to the overall magnetic loss.

To better understand the EMW attenuation mechanism, the attenuation constant (α) was a critical evaluation parameter. The ability of the absorber to attenuate EMWs depended on the α, calculated as follows (eqn (9)):

$$\alpha = \frac{\sqrt{2\pi}f}{c} \times \sqrt{(\mu''\epsilon'' - \mu'\epsilon') + \sqrt{(\mu''\epsilon'' - \mu'\epsilon')^2 + (\mu'\epsilon'' - \mu''\epsilon')^2}} \quad (9)$$

The α values of SCC and SCCM are shown in Fig. 5h. It was evident that the α of SCCM exceeds that of SCC, indicating that EMWs underwent rapid attenuation upon entering the SCCM sample. In addition to the magnetic loss attributed to MoS<sub>2</sub>, the introduction of MoS<sub>2</sub> enhanced interfacial polarization sites. In general, when ε<sub>r</sub> was sufficiently large, an increase in μ<sub>r</sub> led to a higher α, enhancing the material's attenuation capacity. However, an excessively high α could lead to impedance mismatch, as attenuation and impedance matching were inherently conflicting factors. Therefore, the real and imaginary components of ε<sub>r</sub> and μ<sub>r</sub> do not necessarily need to be maximized. Minimizing reflection was essential for achieving strong microwave absorption, which necessitated that the impedance ratio (Z) between the absorber and free space approached “1”.<sup>69</sup> For materials incorporating both magnetic and dielectric components, the impedance matching design principle can be derived from the following equations (eqn (10)–(13)):

$$Z = \left| \frac{Z_{in}}{Z_0} \right| = \sqrt{\left| \frac{\mu_r}{\epsilon_r} \right|} = \sqrt{\frac{\sqrt{\mu''^2 + \mu'^2}}{\sqrt{\epsilon''^2 + \epsilon'^2}}} \quad (10)$$

$$|\Delta| = |\sinh^2(Kfd) - M| \quad (11)$$

$$K = \frac{4\pi\sqrt{\epsilon_r\mu_r} \sin\left(\frac{\delta_\epsilon + \delta_\mu}{2}\right)}{c \cdot \cos \delta_\epsilon \cos \delta_\mu} \quad (12)$$

$$M = \frac{4\mu' \cos \delta_\epsilon \epsilon' \cos \delta_\mu}{(\mu' \cos \delta_\epsilon - \epsilon' \cos \delta_\mu)^2 + \left[ \tan \frac{\delta_\mu - \delta_\epsilon}{2} (\mu' \cos \delta_\epsilon + \epsilon' \cos \delta_\mu) \right]^2} \quad (13)$$

According to quarter-wavelength theory, the matching thickness (d<sub>m</sub>) decreases as frequency increases. The relationship between SCCM matching thickness and frequency is shown in Fig. 5i. In conjunction with Fig. 5j, the Z values of SCCM at matching thicknesses of 1.52 mm (17.78 GHz), 1.79 mm (15.26 GHz), 1.98 mm (12.85 GHz), and 2.84 mm (7.40 GHz) were 1, indicating good impedance matching.

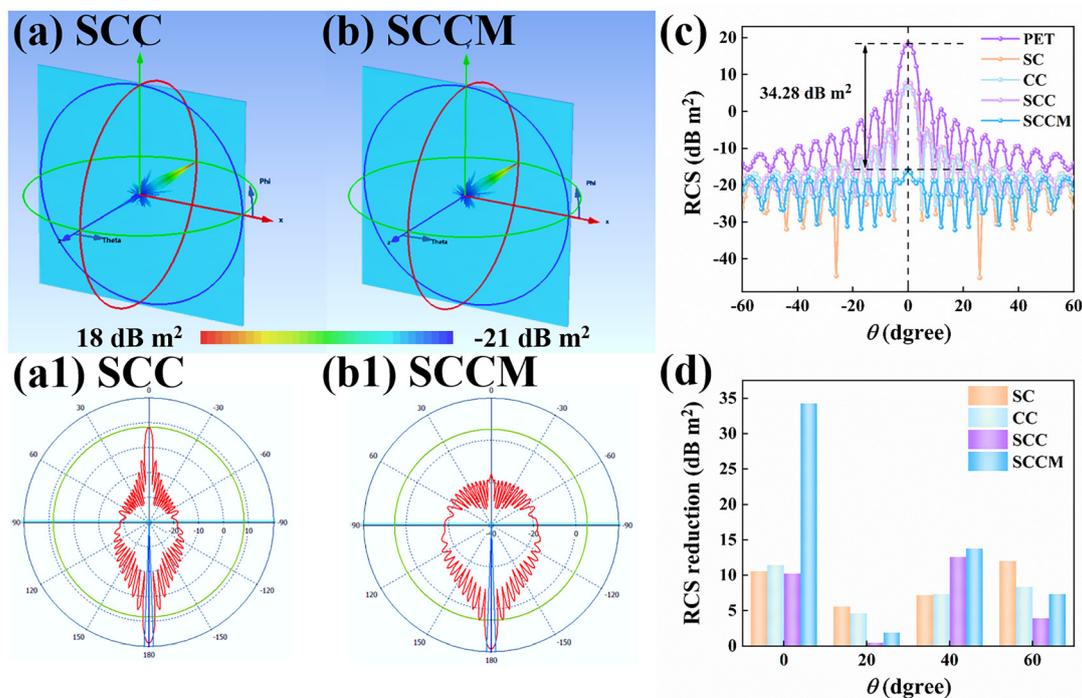
Besides  $Z$ , the value of  $|\Delta|$  can also be used to assess impedance matching. A smaller  $|\Delta|$  signified improved impedance matching, with  $|\Delta| < 0.2$  deemed excellent and adequate for meeting EMW absorption criteria. As illustrated in Fig. 5, a larger blue region indicated better impedance matching, with the SC, CC, and SCCM samples showing a larger blue area. Both SC and CC demonstrated good impedance matching within the 1.5–4.0 mm range, as well as  $RL < -20$  dB within this thickness range. In Fig. 5m, the narrow blue area of SCC was prominent, with a larger thickness (3.5–4.5 mm), indicating that most EMWs were reflected at small thicknesses due to unmatched input impedance. Therefore, adding  $\text{MoS}_2$  to adjust impedance matching was expected to create a synergistic effect between impedance matching and electromagnetic loss at a small matching thickness. Fig. 5n clearly shows that the blue area in SCCM spanned the entire microwave range, indicating excellent impedance matching. Additionally, SCCM exhibited good impedance matching in the thin range of 1–3.8 mm, with multiple strong absorption peaks ( $RL < -40$  dB) within this range in Fig. 4o and an EAB around 5 GHz in Fig. 4p.

### 3.4. RCS simulation results

To evaluate the EMW absorption performance of SCCM in practical applications, CST, professional electromagnetic simulation software, was used to measure the RCS.<sup>70–72</sup> The loss mechanism was further analyzed using SC, CC, SCC, and SCCM as the absorption layer, with a perfect electric conductor (PEC) as the reflector (Fig. 6 and Fig. S4†). RCS represented a

physical measurement of the intensity of the echo generated by a target under radar irradiation.<sup>73</sup> Therefore, the RCS value was small, and the absorption performance of the material was excellent. As shown in Fig. S4a,† pure PEC produced the largest electromagnetic scattering signal at  $0^\circ$ . As shown in Fig. 6c, when PEC was coated with the four different samples, the RCS value significantly decreased, demonstrating effective EMW dissipation. The PEC coated with the SCCM absorber demonstrated the lowest RCS value (below  $-20$  dB  $\text{m}^2$ ), reflecting superior EMW absorption, which aligned with the transmission line theoretical calculations. Fig. 6d presents a bar chart comparing RCS reductions across the four different materials at different angles. The RCS reductions for SCCM were 34.28 dB  $\text{m}^2$  at  $0^\circ$  and 13.77 dB  $\text{m}^2$  at  $40^\circ$ , confirming its excellent absorption properties and practical feasibility for microwave absorption applications. Overall, the superior RCS reduction and alignment with theoretical predictions confirm SCCM's practical feasibility as a high-performance microwave absorber, making it a promising candidate for advanced electromagnetic shielding and stealth applications in both military and civilian fields.

The absorbing performance and electromagnetic parameters of SCCM were thoroughly analyzed above. The potential electromagnetic loss mechanisms of SCCM are shown in Fig. 7. The introduction of high-dielectric  $\text{MoS}_2$  and magnetic Co particles worked synergistically to balance the dielectric constant, achieving excellent impedance matching. First, interfacial polarization arose between metal particles (Sn–Co), between metal particles and CNF (Sn–CNF and Co–CNF), and



**Fig. 6** RCS simulation images of SCC (a) and SCCM (b); RCS values of SCC (a1) and SCCM (b1) from  $-60^\circ$  to  $60^\circ$ ; RCS values of PEC and PEC coated with four different samples, respectively (c); comparison of RCS reduction values of PEC coated with four different samples (d).

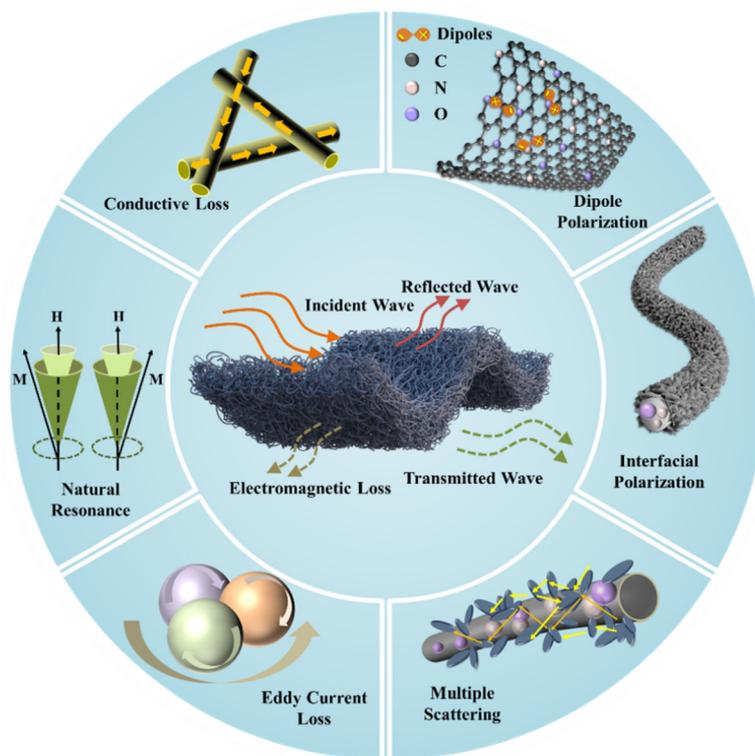


Fig. 7 Schematic diagram of potential electromagnetic loss mechanisms of SCCM.

between core and shell layers ( $\text{MoS}_2\text{-CNF}$ ). Due to differences in electrical conductivity among these components, charge accumulated at the heterogeneous interfaces, resulting in significant interfacial polarization. Additionally, defects in the CNF (vacancies and N atom doping) and the  $\text{MoS}_2$  nanosheets (Mo and S vacancies) increased dipole polarization sites, enriching relaxation losses. Second, the combined effect of  $\text{MoS}_2$  slices with a high specific surface area and interwoven CNF forming 3D structures extended the microwave transmission path, enabling multiple reflection losses and promoting conductive losses. Finally, magnetic Co particles contributed to magnetic losses *via* natural resonance, exchange resonance, and eddy current loss, thereby improving the magnetic loss capacity of materials.

## 4. Conclusion

In conclusion, the  $\text{SnCo/C@MoS}_2$  core-shell composite developed in this study demonstrated significant advancements in microwave absorption performance, driven by the synergy between 1D CNF and 2D  $\text{MoS}_2$  nanosheets. By integrating the magnetic and conductive properties of SnCo with the dielectric properties of  $\text{MoS}_2$ , the composite achieved impressive RL ( $-64.27$  dB), EAB (5.20 GHz) and RCS (below  $-20$  dB  $\text{m}^2$ ). The enhanced performance was attributed to a combination of interfacial polarization, dipole relaxation, conductive and magnetic losses, and the unique core-shell structure. This work

underscores the potential of rationally designed 1D/2D hybrid architectures in developing lightweight, high-performance, and broadband microwave absorbers for practical EMW attenuation applications. Future work will explore scalability, long-term environmental stability, and integration into real-world EMW shielding systems.

## Data availability

The authors confirm that the data supporting the findings of this study are available within the article and its ESI.†

## Conflicts of interest

There are no conflicts to declare.

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