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Integrated photonics has emerged as a pivotal technology in the advancement of next-generation computing and communication devices. Thermal optical phase shifters (OPSS) have been widely used to realize a tunable Mach–Zehnder interferometer (MZI) and a micro-ring resonator (MRR), which are the building bricks for the LSI/VLSI photonic integrated circuits. Due to the thermal crosstalk and the low modulation efficiency, thermal OPSSs have large-scale size and high power consumption. In this work, we embed a Mie resonant metasurface into a waveguide and use the liquid crystal to tune the phase of the propagated light, which could realize a novel integrated phase shifter based on LC meta-waveguides. We use nanofabrication to prepare the meta-waveguide integrated MZI and MRR. By applying voltage, the output of the waveguide's intensity can be changed. Compared with thermo OPSSs, this new modulator has the advantages of small size ($20\text{ }\mu\text{m} \times 0.35\text{ }\mu\text{m}$), no thermal crosstalk, low power consumption ($<10\text{ nW}$), and easy large-scale integration. Additionally, we apply it to the convolutional architecture and verify that it has the potential to accelerate neural network computation.

An ultra-compact integrated phase shifter via electrically tunable meta-waveguides[†]

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New concepts

Our study presents a major advance in the field of very large-scale integration (VLSI) of photonic integrated circuits (PICs), addressing longstanding challenges associated with the large form factors and high power consumption of on-chip components. Shrinking the area and reducing the power consumption of functional on-chip components will help photonic integrated circuits (PICs) to advance from medium-scale integration (MSI) to VLSI, driving progress in fields ranging from communication and computation to sensing. In this work, we present an ultra-compact, electrically tunable phase shifter with low power consumption, enabled by leveraging phase shifts arising from Mie-type resonances and the electrical tunability endowed by liquid crystals. Compared to current thermal optical phase shifters, the active length required for a 2π phase shift is reduced by ~ 50 -fold, from a few millimeters to tens of microns, and the power consumption is lowered by ~ 10 -fold, from hundreds of nanowatts to tens of nanowatts. Free from thermal crosstalk, we have achieved an ultra-compact Mach–Zehnder interferometer (MZI) and a micro-ring resonator (MRR), which are the two basic building bricks for photonic VLSIs. Using the proposed phase shifter, we have also demonstrated a photonic neural network for classification computing with accelerated optical convolution.

Introduction

Integrated optical phase shifters^{1–3} which can control the phase of light have been widely used in various applications, including optical communication systems, quantum information processing,⁴ light detection and ranging (LIDAR),^{5,6} and sensing. Although integrated phase shifters based on the thermo-optic^{7,8} effects are already generally available in foundry platforms,⁹ their large-scale integration is limited by high power consumption and

thermal crosstalk. To further enable large-scale optical phased arrays¹⁰ and optical computing architectures,¹¹ the development of integrated optics phase shifters is progressing towards smaller size, lower power consumption, and higher efficiency.¹²

Recently, researchers have been working on developing novel phase shifters¹³ based on new materials and new modulation mechanisms. One of them is based on MEMS, which tune the refractive index by moving the waveguide mechanically.¹⁴ Hermetic sealing is difficult to use in practical applications. Another promising way is using phase change materials (PCMs) as active materials.¹⁵ Normally, they consume too much energy during the phase change process. Additionally, phase shifters based on the Pockels electro-optic effect have attracted attention due to their ultrafast response and low power consumption. Materials such as lithium niobate (LN),¹⁶ barium titanate,¹⁷ and electro-optic polymers provide direct phase modulation through an external electric field without requiring mechanical

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movement or thermal effects. However, challenges such as material integration and fabrication complexity remain key considerations for practical implementation.

Tunable metasurfaces^{18–20} have shown great potential in various applications, ranging from imaging,^{21–23} sensing,^{24–26} and optical communication^{27–30} to LIDAR.^{31–33} Recently, there has been growing interest in developing dynamic metasurfaces based on phase-change materials (PCMs),^{34–36} which can modulate phase, amplitude, and polarization by thermal or optical stimulation. Another promising approach is to use graphene metasurfaces,^{37–39} which can dynamically control the polarization and phase of light by tuning the Fermi level of graphene through the electro-optic effect. Additionally, tuning free-carriers in transparent conducting oxides and semiconductors has been demonstrated to be a convincing way to dynamically tune the metasurfaces.⁴⁰ Beyond these approaches, lithium niobate metasurfaces⁴¹ based on the Pockels effect have also emerged as an effective method for dynamic optical control, which enable fast, low-power modulation not only of the phase but also of the intensity and wavelength of light. These dynamic tuning methods provide real-time and broadband tuning capabilities, making them promising candidates for ultrafast optical switches, spatial light modulators, and adaptive optics.

Liquid crystal metasurfaces⁴² employ anisotropic liquid crystals to dynamically modulate the phase, polarization, and amplitude of light. This allows for the creation of ultra-thin, tunable optical elements that can be integrated into a wide range of applications, including displays, imaging systems, and optical communications. Furthermore, the use of liquid crystals allows for dynamic control of these optical responses, enabling real-time reconfiguration of the metasurface properties.

The newly developed liquid crystal metasurfaces^{43–45} are mostly aimed at dynamic phase modulation of free-space optical fields. However, applying an LC metasurface to an integrated phase shifter remains untapped. Here, we propose an on-chip integrated phase shifter based on liquid crystal meta-waveguides. Simulation results demonstrate that the phase modulation under liquid crystal deflection can reach 2π along the meta-waveguide at a 1550 nm wavelength. Based on this, we fabricated an MZI and MRR and experimentally verified the phase shift characteristics by measuring the intensity variation of the output waveguides. Compared with traditional thermal-optic phase shifters, our proposed phase shifter has advantages such as no thermal crosstalk, small size, and ease of large-scale integration. We also applied the proposed phase shifter in convolutional neural networks (CNNs), which can achieve high-speed convolution operation. All 2×2 convolutional kernels in modified VGG16⁴⁶ have been replaced, and the classification performance of the network has not decreased. This proves that the architecture can be used to accelerate the calculation of modified VGG16. The proposed novel on-chip phase shifter is conducive to increasing the scale of integrated optics and promoting the development of optical computing and optical phased arrays.

Results and discussion

Principle

In this work, we put the metasurface integrated waveguide into the arm of the MZI and MRR to dynamically tune the phase delay inside the waveguide using a liquid crystal.

Fig. 1a shows the meta-waveguides integrated with a liquid crystal. The amplitude and phase inside meta-waveguides can be modulated when applying voltage to deflect the orientation of liquid crystals. The LC molecules are influenced by the alignment layer on the surface of ITO, causing their long axes to align in the x -direction. Additionally, the metasurface exerts an orientational effect on the LC molecules, resulting in a parallel alignment of the liquid crystals.³³ If the variation of the amplitude is homogeneous during the phase modulation, it can be used as a phase shifter for integrated optics. Here we design the dimensions of the meta-waveguide: the height of the meta-waveguide is 220 nm, the width of the meta-waveguide is 350 nm, the period is 400 nm, and the fill factor follows a quadratic distribution, with a maximum of 60.75% at the two ends and a minimum of 51.25% in the middle.

The phase and amplitude of the proposed LC meta-waveguide are simulated using FDTD. Fig. 1b shows the spectrum of the meta-waveguide from 1450 nm to 1650 nm under different liquid crystal deflection angles. Meta-waveguides have low transmittance at short wavelengths and high transmittance at long wavelengths. There is a blue shift in the spectrum when voltage is applied. Fig. 1c shows the changes in the amplitude and phase of the light field modulated by the designed meta-waveguide at different liquid crystal deflection angles, respectively. It can be seen that the amplitude of the meta-waveguide in the figure remains homogeneous near the wavelength of 1550 nm, while the amount of phase variation reaches 2π . Fig. 1d shows that the LC waveguide (without a metasurface structure) cannot reach 2π during LC deflection. This also proves that the metasurface structure in the waveguide has a phase enhancement effect. Fig. 1e shows the measured phase modulation of LC meta-waveguides by adding voltage at 1537.0 nm. The method of phase measurement is to use the interference optical path, which is mentioned in the following section. From the optical field diagram shown in Fig. 1f, it can be seen that the mode in the waveguide is similar to that in the meta-waveguide area, thus allowing the mode in the waveguide to evolve into the mode in the meta-waveguide.

In Fig. 2a and b, we simulated the spectral response of a meta-waveguide with a fixed period of 400 nm and varying widths in the wavelength range of 1450 nm to 1650 nm. When the width is greater than 350 nm, the LC modulation causes large amplitude fluctuations at a wavelength of 1550 nm, making it unsuitable for use in phase shifters. As shown in Fig. 1c, when the waveguide width is smaller than 350 nm, the phase modulation at a wavelength of 1550 nm is less than 2π .

In Fig. 2d and e, we also simulated the spectral response of a meta-waveguide with a fixed width of 350 nm and varying periods in the same wavelength range. Similarly, when the period is greater than 400 nm, the amplitude variation during



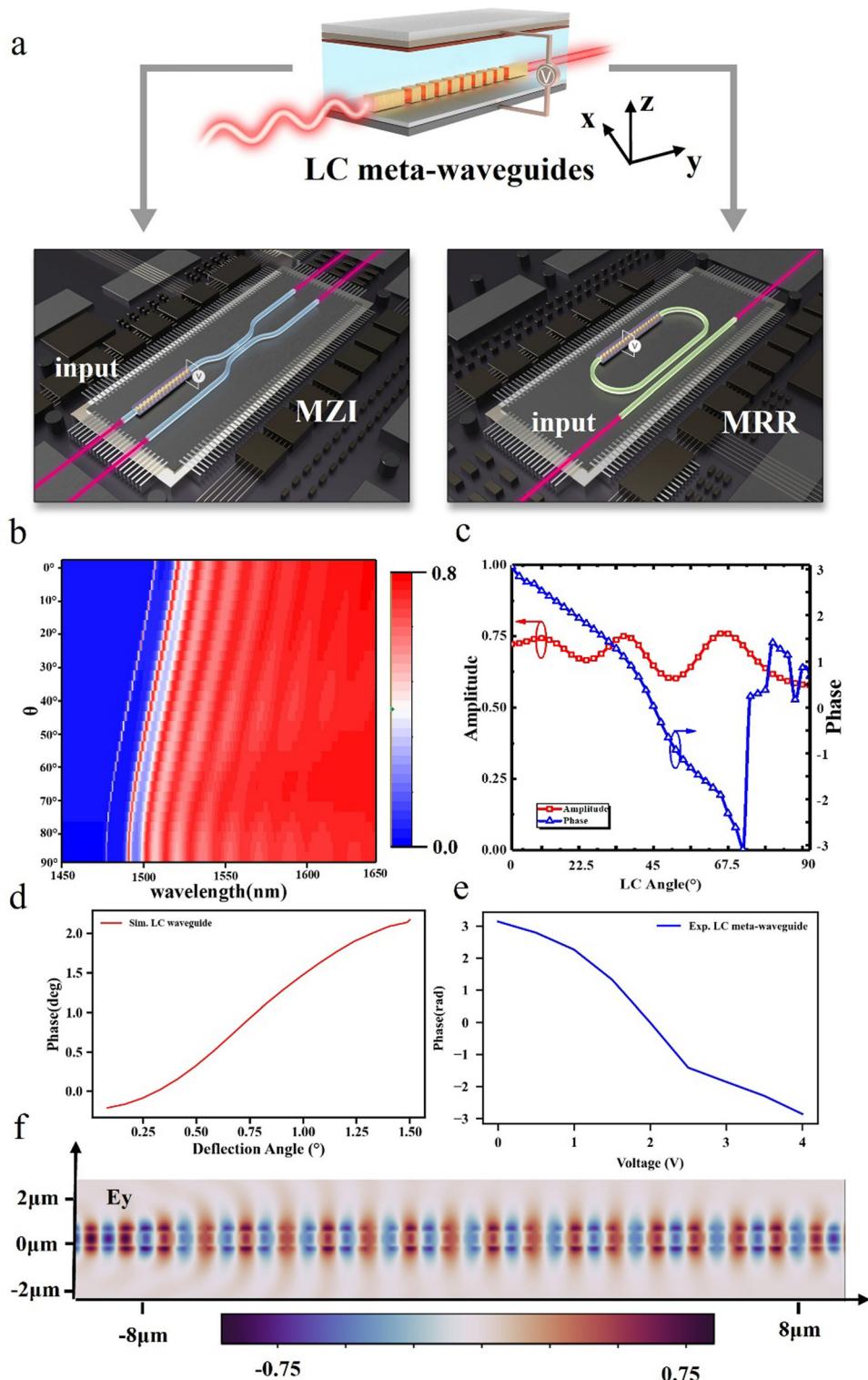


Fig. 1 Device geometry and general concept. (a) Schematic of the LC meta-waveguide for MZI and MRR. (b) Spectral response of LC meta-waveguides in the range of 1450 nm–1650 nm, with liquid crystal deflection angles ranging from 0° to 90°. (c) At 1550 nm wavelength, the amplitude and phase of LC meta-waveguides vary at different liquid crystal deflection angles. (d) Simulated phase modulation varying at different liquid crystal deflection angles in LC waveguides. (e) Measured phase modulation of LC meta-waveguides as a function of voltage. (f) Optical field diagram for LC meta-waveguides.

the liquid crystal deflection process is large; as shown in Fig. 1f, when the period is smaller than 350 nm, the phase modulation

is less than 2π . Therefore, to minimize amplitude variation and achieve a phase change of 2π during liquid crystal deflection at

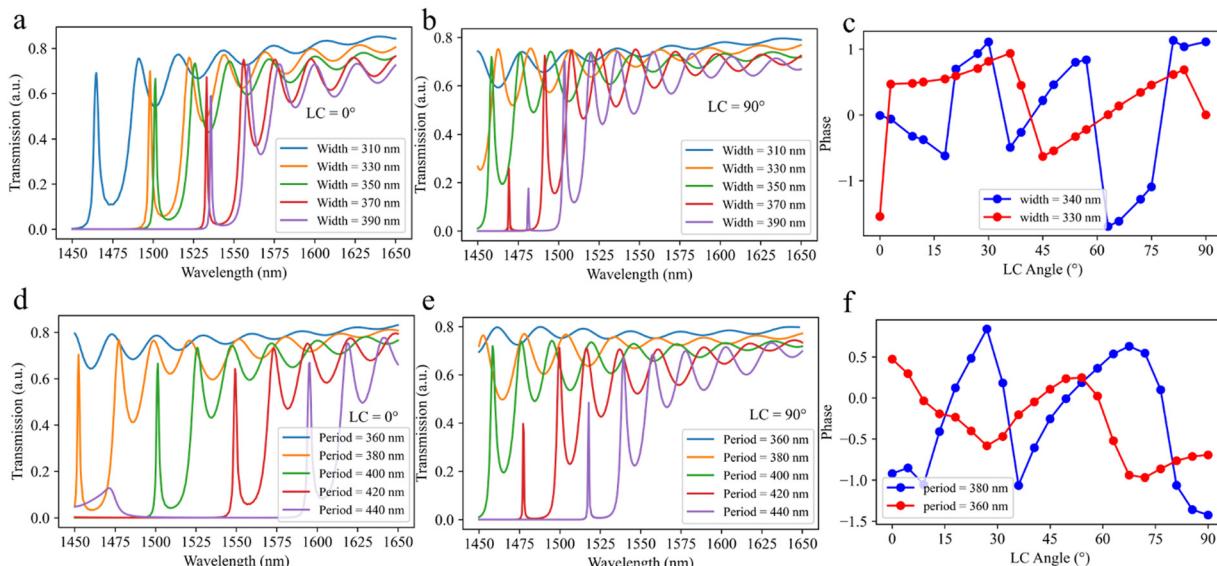


Fig. 2 Spectral response in the wavelength range of 1450 nm to 1650 nm for meta-waveguides with a fixed period of 400 nm and different widths: (a) LC deflection angle of 0° and (b) LC deflection angle of 90°. (c) Phase variation as the LC rotates from 0° to 90° for widths of 330 nm and 340 nm. For a width of 350 nm and different periods, the spectral response in the wavelength range of 1450 nm to 1650 nm: (d) LC deflection angle of 0° and (e) LC deflection angle of 90°. (f) Phase variation as the LC rotates from 0° to 90° for periods of 360 nm and 380 nm.

the 1550 nm wavelength, we choose a meta-waveguide period of 400 nm and a width of 350 nm. Therefore, to minimize amplitude variation and achieve a phase change of 2π during liquid crystal deflection at 1550 nm, we choose a meta-waveguide with a period of 400 nm and a width of 350 nm.

Mach-Zehnder interferometer using LC meta-waveguides

The MZI and MRR are significant integrated optical components that can be used to form optical computing arrays and optical routing networks. We applied the proposed LC meta-waveguides into them and prepared the MZI and MRR using microfabrication processes such as EBL, PECVD, *etc.* (see Methods). The direction of the LC alignment layer is perpendicular to the waveguide direction and is located on the upper ITO surface. The LC at the bottom, due to the anchoring effect of the meta-atomic gaps, will also be oriented perpendicular to the waveguide, so the LC molecules are considered to be parallel to both the top and bottom.

Based on this, the meta-waveguide is integrated into a Mach-Zehnder interferometer to manifest the amount of phase change. The schematic is shown in Fig. 1a, where the novel MZI input part includes two waveguides, in one of which a meta-waveguide is present for realizing the phase change. There is a 3 dB directional coupler after the modulation region for interference of light on the two arms.⁴⁷

$$T_1 = \frac{1 - \cos(\Delta\varphi)}{2} \quad (1)$$

$$T_2 = \frac{1 + \cos(\Delta\varphi)}{2} \quad (2)$$

where $\Delta\varphi$ is the phase difference of light propagating in the two input waveguides and T_1 and T_2 represent the optical power of the output waveguides of the MZI.⁴⁸

It can be seen from eqn (1) and (2) that the intensity changes at the two output ports are in opposite phases. That is, as the phase difference increases, its transmission intensity shows an opposite trend. When the output of one port reaches the maximum value, the output of the other port is the minimum. Therefore, when the external electric field changes the liquid crystal director and thereby changes the phase modulation amount of the meta-waveguide, the intensity of the two output ports will change accordingly.

In order to eliminate the influence of liquid crystal on couplers and other waveguide structures, liquid crystal is only placed around the meta-waveguide, and the cladding material of other parts of the device is still SiO₂.

The simulation is carried out when the angle between the liquid crystal director and the z-axis changes from 0° to 90°. Fig. 3(a) and (b) show the mode field diagrams when light is output from the lower waveguide and upper waveguide, respectively. The transmittance of the output ends of both arms at 1550 nm is shown in Fig. 3(c). Maximum transmittance of the output waveguide is greater than 70% during modulation.

In addition, in order to further reduce the loss in the meta-waveguide area, we added a taper to guide the light from the waveguide to the meta-atom structure.⁴⁹ Fig. 3(d) and (e) show the light field distribution of the designed MZI with a taper. It can be observed that the leakage of the optical field from the waveguide region to the meta-waveguide region is reduced with the assistance of taper guidance. Fig. 3(f) shows the transmittance of the output ends of both arms at 1550 nm with a taper.⁵⁰

First, the light in the optical fiber is coupled into the input waveguide using a coupling grating. Then the optical power in



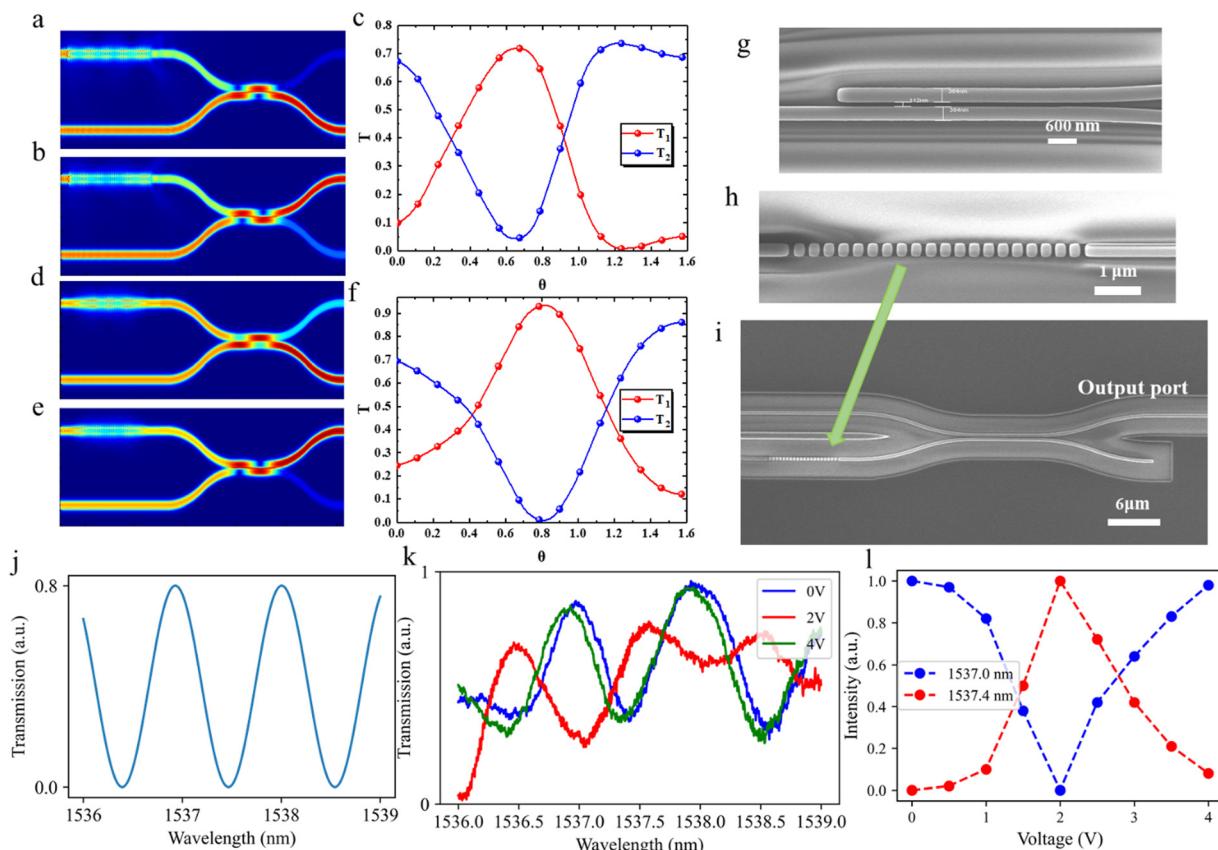


Fig. 3 LC meta-waveguide phase shifter in an MZI. The liquid crystal deflection angle is rotated so that (a) the input light field is output from the lower port. (b) The input light field is output from the higher port. (c) The intensity changes of the two output ports of the MZI under different liquid crystal deflection angles. After adding a taper, (d) the input optical field is output from the lower port. (e) The input optical field is output from the lower port. (f) The intensity changes of the two output ports of the MZI under different liquid crystal deflection angles ((a)–(f) obtained from simulation). (g)–(i) The SEM images of the coupler, meta-waveguides and MZI. (j) Calculated spectrum of MZI from 1536 nm to 1539 nm. (k) The spectrum of the MZI at wavelengths ranging from 1536 nm to 1539 nm under 0 V, 2 V, and 4 V applied voltages. (l) The transmission variation of the MZI at wavelengths of 1537 nm and 1537.4 nm as the voltage is applied from 0 V to 4 V.

the input waveguide is split into two using a directional coupler and fed into the MZI dual arms. The light in one of the arms passes through the meta-waveguide where it can be phase modulated. The voltage is applied to deflect the liquid crystal molecules and thus modulate the light (more details can be seen in Fig. S3 and S4, ESI[†]).

The light output from the waveguide is extracted at one end of the Mach–Zehnder interferometer and a coupling grating is used at the end of the waveguide to couple the light in the waveguide into the output fiber. A spectrometer is used to detect the signal at the output waveguide.

The spectral shift of the device can indicate the phase change in the region of the meta-waveguide. Fig. 3(g–i) show the SEM image of the coupler, the SEM image of the meta-waveguide, and the SEM image of the entire MZI, respectively. Fig. 3(j) shows the calculated spectrum of one arm of the proposed MZI output. The FSR of the proposed MZI is given by:

$$\text{FSR} = \frac{\lambda^2}{n_{g1}L_1 - n_{g2}L_1} \quad (3)$$

Here, λ is the operation wavelength, L_1 and L_1 are the lengths of two waveguides, and n_{g1} and n_{g2} are group indices of the waveguides, which are obtained from simulation in COMSOL. In the calculations, we took into account the insertion loss caused by the meta-waveguides, the initial phase difference, and the coupling loss introduced by the coupling structure. We found that the calculated FSR is approximately 1.12 nm for wavelengths ranging from 1536 nm to 1539 nm.

Fig. 3(k) shows the measured spectral response from 1536 nm to 1539 nm at voltages of 0 V, 2 V, and 4 V. The spectrum exhibits a periodic response, with the peak spacing determined by the FSR, which results from the interference in the MZI. After applying voltage, the spectrum shifted, proving a phase change in the meta-waveguide. As shown in the figure, a peak appears around 1537 nm at 0 V, a trough appears at 2 V, and another peak reappears at 4 V, from which we can infer that the half-wave voltage is 2 V. Fig. 3(l) depicts the variation of light intensity in the output waveguide of the device at different voltages for 1537.0 nm and 1537.4 nm. From the significant light intensity changes in the output waveguide, it can be seen that the phase of the LC meta-waveguide is modulated. According to the change of light intensity at 1537 nm and formula (1),

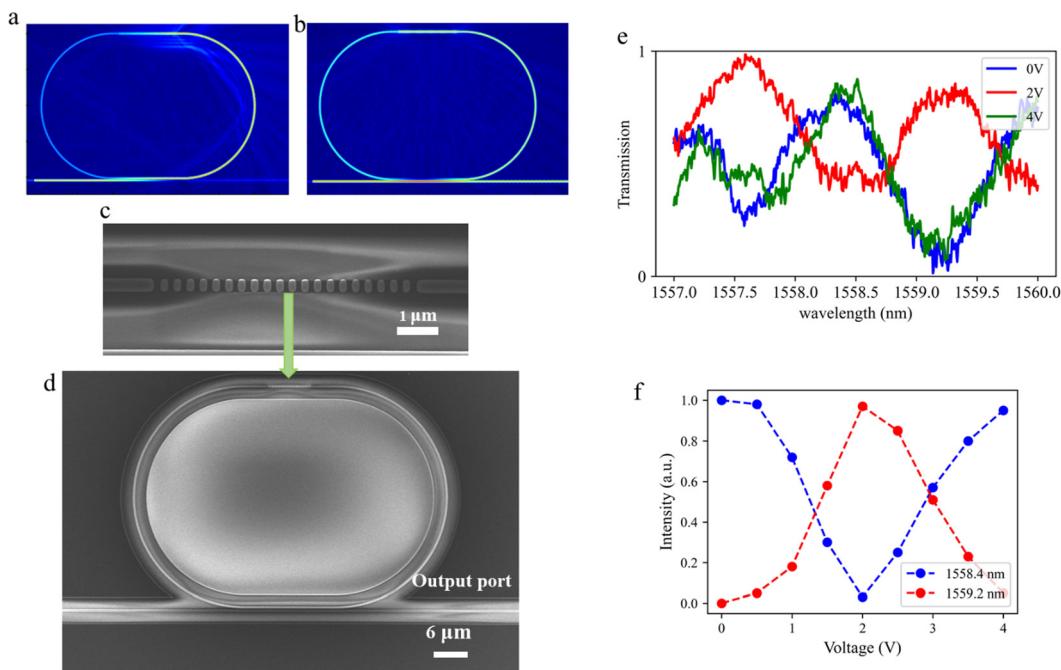


Fig. 4 LC meta-waveguide phase shifter in an MRR. (a) and (b) Two switching states of the MRR in simulation. (c) and (d) SEM images of the metawaveguide and MRR. (e) The spectrum of the MRR at wavelengths ranging from 1557 nm to 1560 nm under 0 V, 2 V, and 4 V applied voltages. (f) The transmission variation of the MRR at wavelengths of 1558.4 nm and 1559.2 nm as the voltage is applied from 0 V to 4 V.

we get the relationship between phase and voltage change, as shown in Fig. 1(d).

Micro-ring resonator using LC metawaveguides

In order to further illustrate the phase modulation of the metawaveguides, it was applied to MRR to create a tunable micro-ring resonator. We place the meta-waveguide in a symmetrical region in the ring waveguide, as shown in Fig. 4(d).

Fig. 4(a) and (b) show two photonic switching states of the MRR under different LC deflection angles. The preparation and electrical testing methods of the MRR are the same as those of MZI. Fig. 4(c) and (d) show the SEM image of the meta-waveguide and MRR before liquid crystal encapsulation and the spectral changes after electrical stimulation.

As shown in Fig. 4(e), without applying any voltage, a peak appears at 1558.4 nm. When a voltage of 2 V is applied, the peak shifts to 1557.5 nm. From Fig. 4(e), the FSR of the device can also be determined to be approximately 1.8 nm, with a half-wave voltage of 2 V. Fig. 4(f) shows the output intensities at 1558.4 nm and 1559.2 nm, with the intensity variations showing opposite trends.

Phase shifters based on the thermo-optic effect⁵¹ consume a significant amount of power, resulting in thermal crosstalk that restricts the scaling of LSI/VLSI. Compared with traditional thermo-optic phase shifters, LC meta-waveguide phase shifters have no thermal crosstalk and ultra-compact size, making them suitable for large-scale integration. It can be seen from Table 1 that the energy consumption of LC meta-waveguide is 10 nW and the active area length is 10 μm , which has significant advantages over thermo-optical phase shifters.

LC meta-waveguides offer a compact design compared to MEMS, phase-change materials, and graphene phase shifters. MEMS phase shifters rely on mechanical movement, requiring larger components and more complex driving systems. PCM-based modulation depends on phase transitions, involving significant material structure changes over a large area. While graphene is small, it requires large planar electrodes for modulation. In contrast, LC meta-waveguides achieve phase modulation through metasurface resonances, enabling smaller device volumes. Additionally, vertical electrode structures drive the liquid crystal, further reducing the device size.

Table 1 Comparison of the performance between LC meta-waveguide phase shifters and other phase shifters

	Thermo-optic effect ¹²	LC waveguide ⁵²	BTO ⁵³	PCM ⁵⁴	LN ⁵⁵	LC meta-waveguide
Power consumption	0.4 mW ⁵⁶	Low			6.24 mW	10 nW (ESI)
Thermal crosstalk	Large	Little			Little	Little
Length of active area	$\sim 1000 \mu\text{m}$	50 μm			400 μm	20 μm
Response time	60 ms	20 ms		0.1 ms (when the pulse voltage is 3 V)	$< 0.1 \mu\text{s}$	2–3 ms
Easy to integrate	N	Y			N	Y

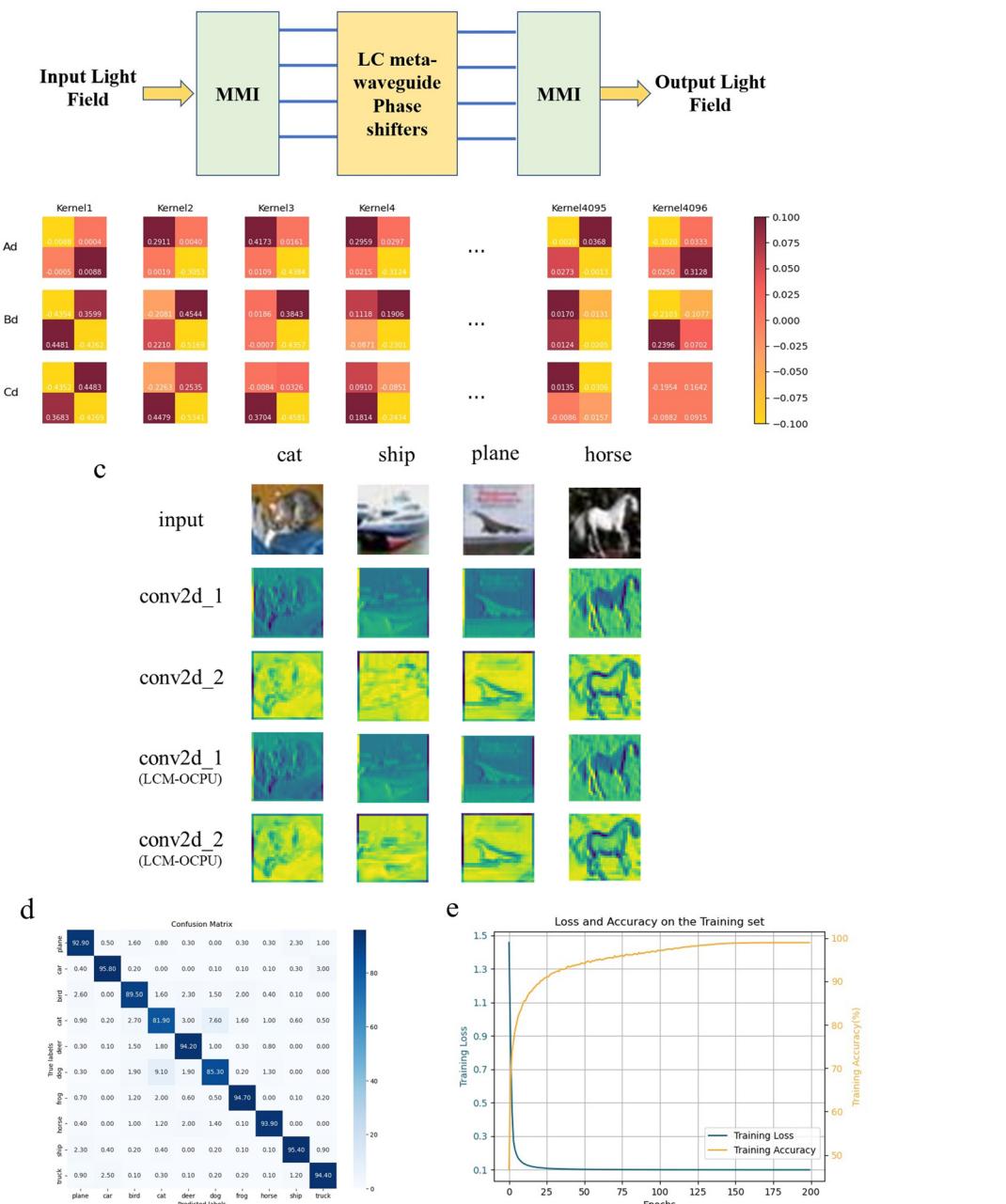


Fig. 5 (a) Architecture diagram for an LC meta-waveguide optical convolution accelerator. (b) Partial values and pseudocolor maps of different kernels. Each column of kernels was obtained under the same phase condition. The parameter value range of the kernels is $(-1, 1)$. (c) The input image and the feature images outputted by two 2×2 convolution layers. The first row is the input image, followed by two rows of images outputted by the proposed network's convolution layers, and then two rows of images outputted by the replaced convolution layers. (d) The confusion matrix of the model on the test set after replacing the parameters in the first two convolution layers with a 2×2 kernel provided by OCPU. The vertical axis represents the true labels and the horizontal axis represents the predicted labels. (e) The cross-entropy loss and classification accuracy curves of our proposed network on the training set are shown as a function of training iterations.

In terms of power consumption, compared to driving micro-mechanical structures, material phase transitions, or applying strong electric fields to change the conductivity or surface states of graphene, the power required to drive LC is much lower.⁵⁷

The LC meta-waveguide arrays' driving method can be compatible with existing large-scale pixel LCOS chips. Additionally,

the individual LC meta-waveguide phase shifters have low power consumption and a small area, making them well-suited for VLSI integration.

Convolution operation

To further validate the ability of the proposed phase shifter applied to optical computing,⁵⁸ we apply the LC meta-waveguide phase

Table 2 Performance of CNNs on the test dataset

CIFAR-10		GoogleNet ⁶¹ (%)	ResNet50 ⁶² (%)	Our model (%)	After replacement (%)
Image category	Airplane	51.10	90.80	92.90	92.90
	Automobile	62.10	69.10	95.50	95.50
	Bird	56.70	72.60	88.90	89.50
	Cat	78.80	61.90	81.80	81.90
	Deer	49.50	75.40	94.50	94.20
	Dog	57.50	82.10	86.20	85.30
	Frog	90.20	76.60	94.60	94.70
	Horse	78.20	84.70	93.70	93.90
	Ship	95.50	83.20	95.40	95.40
	Truck	97.10	84.60	94.70	94.40

shifter to the proposed convolutional architecture and use it in a network based on modified VGG16, as shown in Fig. 5(a). All 2×2 convolution operations in the modified network are performed using the LC meta-waveguide optical convolution accelerator (LCM-OCA).

We change the addressing voltage to control the LC meta-waveguide to produce different additional phases. For each phase shifter, we can generate eight gray levels according to the experiment that can be mapped to drive voltages. The proposed convolutional architecture with the LC meta-waveguide phase shifter is based on simulations that are grounded in experimental test results. Specifically, we measured 8 discrete phase values experimentally to derive the transmission matrix R used in the convolutional architecture. The subsequent work, including system performance analysis, was performed through simulations. By modulating the additional phase of the phase shifter, we are able to change the transmission matrix R of LCM-OCA.⁵⁹

$$R = \begin{bmatrix} |r_{11}|^2 & |r_{12}|^2 & |r_{13}|^2 & |r_{14}|^2 \\ |r_{21}|^2 & |r_{22}|^2 & |r_{23}|^2 & |r_{24}|^2 \\ |r_{31}|^2 & |r_{32}|^2 & |r_{33}|^2 & |r_{34}|^2 \\ |r_{41}|^2 & |r_{42}|^2 & |r_{43}|^2 & |r_{44}|^2 \end{bmatrix} \quad (4)$$

where $|r_{ij}|^2$ ($i, j = 1, 2, 3, 4$) are determined by the transfer matrix of the MMI unit and the additional phase of the LC meta-waveguide. Next, 2×2 convolution kernels can be obtained. The specific values of some convolution kernels are shown in the following Fig. 5(b) and are visualized as a color map.

To validate the effectiveness of the LCM-OCA in convolutional neural networks, we used the modified VGG16 for recognizing simple colored objects and performing classification tasks (for neural network details and datasets, see ESI†).

The output obtained by processing the input vector through LCM-OCA can be considered as the result of convolution with these 2×2 kernels. Therefore, we replace the 2×2 convolution kernels in the model with these kernels, and the convolution layers that use 2×2 convolution kernels in the original model can be computed on LCM-OCA. We evaluate the similarity between two convolution kernels using the root mean square error (RMSE)⁶⁰ between matrices. The RMSE is defined as

follows:

$$\text{RMSE} = \sqrt{\frac{1}{n \times n} \sum_{j=1}^n \sum_{i=1}^n (y_{i,j} - y'_{i,j})^2} \quad (5)$$

Here, the 2×2 convolution kernel $n = 2$, $y_{i,j}$ represents the parameters of the convolution kernel in the saved model, and $y'_{i,j}$ represents the parameters in the kernel used for replacement.

The confusion matrix is shown in Fig. 5(d). The variation curves of cross-entropy loss and classification accuracy of our network on the training set with training rounds are shown in Fig. 5(e). On the test set, our model achieved an accuracy of 91.82% in top-1 probability classification prediction (Table 2).

Our simulation demonstrated that our proposed network using 2×2 convolutional kernels achieved excellent performance in the classification task on the CIFAR10 dataset. This suggests that we can use the replacement method to load the convolutional neural network⁶³ onto an LCM-OCA to accelerate convolutional calculations.

Conclusions

In conclusion, we have proposed and demonstrated an ultra-compact on-chip phase shifter based on electrically tunable meta-waveguides. Simulations demonstrate that the phase modulation of the liquid crystal meta-waveguide phase shifter can reach up to 2π and keep the amplitude homogeneity. We have prepared MZIs and MRRs based on liquid crystal meta-waveguides and verified the role of phase modulation by measuring changes in the light intensity of the output waveguide. We also apply the liquid crystal meta-waveguide phase shifter to the convolutional architecture and apply this architecture to accelerate the operation of the modified VGG16 network. Based on our measured results, we simulated the overall neural network, which proves that it is possible to realize complex operations.

Methods

First, EBL is used to prepare waveguide and meta-waveguide structures on silicon-on-insulator (SOI) substrates. The top layer of single crystal silicon is then etched using dry etching. The plasma enhanced chemical vapor deposition (PECVD) is



then used to deposit silicon oxide, and finally, EBL is used to window the meta-waveguide area. How to remove the silicon oxide above the meta-waveguide area is a challenge. If only dry etching is used, the bottom silicon oxide may be over-etched. Therefore, here we use a combination of dry etching and wet etching to better remove the top silicon oxide. Then the liquid crystal was packaged, using a process similar to the LCOS packaging process.⁶⁴

The device is powered as follows: the ground of the electrode is connected to the silicon substrate, and the high level is applied to ITO.⁶⁵ During the test, a square wave signal with a frequency of 1 kHz and a voltage from 0–4 V was applied. Subsequently, the packaging of LC is compatible with the packaging process of LCOS. Due to the removal of the silicon dioxide above the meta-waveguide area, the LC can make direct contact with the meta-waveguides.⁶⁶

Author contributions

C. D. fabricated the initial meta-waveguide device, performed simulation and optical characterization, and wrote the first draft of the manuscript. X. G. conducted the nanofabrication of the device. Y. H. proposed a modified neural network architecture and performed simulation. Z. Z. performed liquid crystal cell fabrication. J. W. Z. W. and W. W. performed electro-optical characterization. T. C., J. W. and T. Q. provided comments on the revision of the manuscript. J. X. conceived the idea and supervised the work. All authors contributed to the manuscript preparation.

Data availability

The data that support the findings of this study are available from the corresponding authors upon request. Source data are provided in this paper.

Conflicts of interest

The authors declare no conflict of interest.

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