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## Simulation and machine learning driven optimization of $\text{Rb}_2\text{SnBr}_6$ -based lead-free perovskite solar cells using diverse ETLs for enhanced photovoltaic performance

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In this work, n-i-p planar heterojunction perovskite solar cells (PSCs) were simulated using SCAPS-1D, employing  $\text{Rb}_2\text{SnBr}_6$  as a lead-free, stable, and cost-effective absorber. Fluorine-doped tin oxide (FTO) served as the transparent substrate, with gold (Au) as the rear contact, and three electron transport layers (ETLs) – ZnSe,  $\text{In}_2\text{S}_3$ , and CdZnSe – were evaluated. Device I (ZnSe) achieved the best performance with a PCE of 28.73%,  $V_{\text{OC}}$  of 0.868 V,  $J_{\text{SC}}$  of  $38.09 \text{ mA cm}^{-2}$ , and FF of 86.86%. Device II ( $\text{In}_2\text{S}_3$ ) and device III (CdZnSe) exhibited lower efficiencies of 26.62% and 24.04%, respectively. To further analyze performance, a random forest (RF) machine learning model was applied, with SHAP values identifying the most influential parameters. The RF model demonstrated high accuracy ( $R^2 = 0.8825$ ) and strong agreement between predicted and actual efficiencies. These results highlight the potential of  $\text{Rb}_2\text{SnBr}_6$ , particularly with a ZnSe ETL, for developing high-efficiency, eco-friendly PSCs.

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## 1. Introduction

One of the primary areas of research in energy harvesting (EH) focuses on capturing ambient energy from the surroundings and converting it into electrical energy. This accumulated energy can be used to charge batteries or directly power electronic devices. Power generation in the nanowatt (nW) to milliwatt (mW) range is made possible by harnessing various

external energy sources, including solar radiation, thermal gradients, radio frequency (RF) signals, mechanical motion, and environmental vibrations.<sup>1</sup> The rising global demand for electricity is compelling scientists to explore alternatives to traditional energy sources. Meanwhile, the enhancing need for eco-friendly energy solutions has become more urgent, driven by the limited availability of non-renewable resources and their harmful environmental impacts, high costs, and significant logistical challenges.<sup>2</sup> Among various sustainable energy sources, sun-derived power is widely regarded as one of the most efficient and practical alternatives. Silicon (Si) has become the material of choice for the commercialization of photovoltaic cells due to its numerous advantages, including high power conversion efficiency (PCE), durability, and strong resistance to radiation.<sup>3</sup> The development of traditional photo-cells, incorporating silicon (Si), has been obstructed by inherent limitations like silicon's indirect and suboptimal energy gap, as well as the high costs associated with its production.<sup>4</sup> Since 2009, certain hybrid inorganic-organic lead halide perovskite (OILHP) components have emerged as promising substances for solar cells.<sup>5-8</sup> Their notable features have garnered significant interest for potential use in solar energy applications. These features include high power conversion efficiency (PCE), an optimal bandgap, a strong absorption coefficient, exceptional mobility of charge carriers, and excellent resistance to defects.<sup>4,9</sup> The PCE of absorber photocells has seen

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remarkable growth in recent years. Starting at 3.8% in 2009, the PCE has made significant advancements, reaching an impressive 26% by 2021.<sup>10,11</sup> F. Rahman *et al.* replicated  $\text{Rb}_2\text{SnBr}_6$  in 2025 using the one-dimensional solar cell capacitance simulator (SCAPS-1D), achieving a conceptual peak PCE of 27.25%.<sup>12</sup> These remarkable advancements underscore the rapid progress in perovskite solar cell technology and its exceptional energy conversion efficiency. However, the limited stability and the harmful effects associated with the presence of lead (Pb) pose significant challenges to the widespread adoption and further development of perovskite solar cells.<sup>13–15</sup> Despite ongoing researches to develop lead-free perovskite materials, it is still exceedingly challenging to obtain the identical layers of surroundings durability and PCE as lead-based solar cells.<sup>12</sup> Therefore, research into PV components that are both greatly effective and lead-free and appropriate for commercial use is immensely needed in the photocell sector.<sup>16,17</sup>  $\text{X}_2\text{SnBr}_6$  (where X represents elements such as Cs, Rb, K, and Na) is a member of the  $\text{X}_2\text{BA}_6$  family of compounds. In this family, X denotes cations like  $\text{Cs}^+$ ,  $\text{Rb}^+$ ,  $\text{K}^+$ , and  $\text{Na}^+$ , B represents cations such as  $\text{Si}^{2+}$ ,  $\text{Ge}^{2+}$ ,  $\text{Sn}^{2+}$ , and  $\text{Pb}^{2+}$ ,<sup>18</sup> and A signifies anions, for example, F, Cl, Br, and I. Within the  $Fm\bar{3}m$  space group,  $\text{X}_2\text{SnBr}_6$  exhibits a high-symmetry structure akin to that of a cubic halide solar cell.<sup>19,20</sup> The authorized transitions in band-edge conditions, facilitated by parity, observed in  $\text{X}_2\text{SnBr}_6$  materials suggest their promising potential for next-generation solar cell utilization.<sup>21</sup> The energy gap of a substance plays an essential role in calculating the PCE of photo-cells, as it immediately impacts generation and solar absorption. Therefore, optimizing the bandgap is essential for improving photocell efficiency. According to the Shockley–Queisser limit, perovskite photocells could gain a maximum PCE of up to 33% if the material's energy gap is carefully tuned between 1.2 and 1.4 eV.<sup>22</sup> ZnSe,  $\text{In}_2\text{S}_3$ , CdZnSe, and  $\text{Rb}_2\text{SnS}_3$  have garnered significant attention for their potential functions in photocells and optoelectronics. ZnSe, with its hexagonal crystal structure and wide bandgap of 1.8 eV, holds promise for photovoltaic applications. However, its relatively low carrier mobility limits its overall efficiency, presenting a challenge for further optimization.<sup>23</sup> Research is ongoing to enhance its performance using doping and hybridization techniques.  $\text{In}_2\text{S}_3$ , with an energy gap limit from 2.0 to 2.4 eV, is known for its high optical transparency and conductivity, making it ideal for use in thin-film solar cells and transparent electronics.<sup>24,25</sup> ZnSe,  $\text{In}_2\text{S}_3$ , and CdZnSe are promising components for electron transport layers (ETLs) in photocells and optoelectronics. ZnSe, with an energy gap of 1.8 eV, offers high electron mobility and transparency, making it suitable for thin-film and perovskite solar cells, though it can face adhesion issues.  $\text{In}_2\text{S}_3$ , with a 2.1 eV bandgap, provides good transparency and moderate electron mobility but suffers from low carrier mobility, limiting efficiency. CdZnSe, a ternary compound with an energy gap of 2.7–2.8 eV, offers elevated electron mobility and transparency, ideal for transparent and adaptable electronics, but faces obstacles related to long-term stability and expandability for large-area applications.<sup>26</sup>  $\text{Rb}_2\text{SnBr}_6$  is selected as the absorber layer due to its lead-free

composition, making it an eco-friendly and non-toxic replacement for traditional lead-based perovskites. As an all-inorganic, vacancy-ordered double perovskite, it offers superior thermal and moisture stability, enhancing device longevity and reliability compared to organic-inorganic hybrids. With a suitable band gap (1.0–1.3 eV), strong light absorption, good charge transport properties, and intrinsic defect tolerance,  $\text{Rb}_2\text{SnBr}_6$  is well-suited for high-performance photovoltaic applications. It is also compatible with inorganic electron transport layers like ZnSe, further improving efficiency and stability. Recent studies have shown promising efficiencies and operational stability of  $\text{Rb}_2\text{SnBr}_6$ -based devices, supporting their potential for scalable, eco-friendly solar technologies. Ongoing research continues to advance its charge transport and interface properties, bringing it closer to commercial viability as a robust absorber material.<sup>12,27,28</sup> However, its low carrier mobility is a major limitation in its use for high-performance solar cells. All these materials share common challenges, primarily related to low carrier mobility, which affects their efficiency in photovoltaic devices. Ongoing research aims to overcome these challenges through doping, hybridization, and advanced deposition techniques. While ZnSe and  $\text{Rb}_2\text{SnBr}_6$  show promise as absorber layers in thin-film solar cells,  $\text{In}_2\text{S}_3$  and CdZnSe are more commonly used as buffer or transparent conducting oxide layers.<sup>29</sup> Each material offers unique advantages, but further optimization is required to improve their performance and stability. The integration of these materials into tandem solar cells could potentially enhance their efficiency.<sup>30</sup> Au (gold) and Al (aluminum) are used as metal contacts due to their suitable electrical properties and energy level alignment with adjacent layers. Gold, with its high work function (5.47 eV), forms an efficient ohmic contact with the valence band of  $\text{Rb}_2\text{SnBr}_6$ , facilitating effective hole extraction. Additionally, Au is chemically stable and resistant to oxidation, ensuring long-term interface stability. On the other hand, aluminum has a lower work function (4.2 eV), making it well-suited for forming an ohmic contact with the conduction band of ZnSe, thereby enabling efficient electron extraction. Al is also cost-effective and highly conductive, which supports scalable and efficient device fabrication. Altogether, these metal contacts are carefully chosen to refine charge collection, reduce recombination losses, and boost overall model performance.<sup>31,32</sup> Continued research and development are necessary to fully exploit their potential in next-generation solar cells and optoelectronic devices. By addressing their limitations, these materials could become key components in sustainable, high-efficiency solar technology. The future of solar cell technology depends largely on the development of materials that offer a combination of high efficiency, long-term stability, and ease of fabrication. Materials such as ZnSe,  $\text{In}_2\text{S}_3$ , CdZnSe, and  $\text{Rb}_2\text{SnBr}_6$  each present unique merits in terms of optical attributes, charge carrier mobility, and material stability. However, to fully understand their capability in solar energy applications, these materials must overcome significant challenges related to performance, scalability, and integration with other components. Ongoing research into doping strategies, material hybridization,



and advanced fabrication techniques will be essential in advancing these materials toward commercial viability and widespread adoption in next-generation solar cells and optoelectronic devices.

This study investigates the potential of  $\text{Rb}_2\text{SnBr}_6$ -based perovskite solar cells by evaluating various electron transport layers (ETLs) to propose an optimized device configuration. The novelty of this work lies in the integrated simulation and machine learning approach: multiple ETLs ( $\text{ZnSe}$ ,  $\text{In}_2\text{S}_3$ , and  $\text{CdZnSe}$ ) were systematically assessed, identifying  $\text{ZnSe}$  as the optimal candidate with a superior simulated PCE of 28.73%. A random forest model with SHAP analysis was employed to quantify the relative impact of key device parameters, providing interpretable insights and predictive guidance, an approach not previously applied to  $\text{Rb}_2\text{SnBr}_6$ -based PSCs. While prior SCAPS-based studies have reported efficiency estimates, a systematic ETL comparison combined with ML-driven analysis has not been explored. This study addresses that gap by offering both optimized device design and actionable design insights for future experimental development.

Building on previous research, this study analyzed key factors affecting performance, including operating temperature, metal contact work function, series and shunt resistances, electron surface recombination, charge carrier density, and layer thickness and defect density in both the absorber and ETL. Device performance was evaluated using current–voltage ( $J$ – $V$ ) characteristics and quantum efficiency (QE), and the results were compared with prior studies to highlight technological improvements. These analyses provide comprehensive guidance for designing high-efficiency, stable, and scalable  $\text{Rb}_2\text{SnBr}_6$ -based perovskite solar cells.

## 2. In simulation techniques, models are employed and band structures are aligned

### 2.1 Computation using SCAPS-1D

The numerical structure of PSCs can be replicated using a single-dimensional simulator called SCAPS-1D, which was produced at the University of Gent in Belgium.<sup>33</sup> Key parameters such as layer depth, bandgap, defect density, and doping concentration are critically tuned to elevate the efficiency of photocell systems.<sup>34,35</sup> This mathematical analysis depends on two basic equations: the Poisson equation (eqn (1)) and the continuity equations (eqn (2) and (3)). The Poisson equation relates the electrostatic field  $E(x)$ , the material's permittivity, and the total charge concentration. Meanwhile, the continuity equations describe the transport and behavior of charge carriers within the device: eqn (2) for electrons and eqn (3) for holes, capturing their generation, recombination, and flow under varying conditions.<sup>36</sup>

$$\frac{d}{dx} \left( -\epsilon(x) \frac{d\psi}{dx} \right) = q \left[ \{p(x) + N_D^+(x)\} - \{n(x) + N_A^-(x)\} \right] \quad (1)$$

Here the symbols  $\epsilon$ ,  $N_A^-(x)$ ,  $q$ ,  $n(x)$ ,  $p(x)$ , and  $N_D^+(x)$  represent the dielectric constant, ionized acceptor concentration, charge,

electron concentration, hole concentration and ionized donor concentration, respectively.

$$\frac{\partial j_p}{\partial x} = -q \left( R_p + \frac{\partial p}{\partial t} - G \right) \quad (2)$$

$$\frac{\partial j_n}{\partial x} = q \left( R_n - G + \frac{\partial n}{\partial t} \right) \quad (3)$$

The density of electron pair recombination, density of hole pair recombination, and density of generation are denoted by the symbols  $R_n$ ,  $R_p$ , and  $G$ , respectively. The formula  $J = j_p + j_n$  presents the overall density of current. On the other hand, the symbols  $j_p$  and  $j_n$ , respectively, represent the current concentrations for charge carriers (holes and electrons). Eqn (4) and (5) illustrate the development of a drift-diffusion formula for determining the electron and hole flow densities.

$$J_p = q \left( \mu_p n E + D_p \frac{d_n}{d x} \right) \quad (4)$$

$$J_n = q \left( \mu_n n E + D_n \frac{d_n}{d x} \right) \quad (5)$$

where the symbols  $\mu_n$  and  $\mu_p$  represent electron and hole flexibility, respectively, and  $D_n$  and  $D_p$  represent the densities of electron and hole diffusion. Eqn (6) illustrates the strong relationship between the penetration depth, diffusivity, and conduction particle lifetime.

$$L(n, p) = \sqrt{T(n, p) D(n, p)} \quad (6)$$

The mass diffusivity, diffusion length, and minority carrier lifetime are denoted by the icons  $D(n, p)$ ,  $L(n, p)$ , and  $T(n, p)$ , respectively. SCAPS-1D computes the coefficient of absorption, which characterizes the connection between photons and the perovskite layer, in accordance with what are known as the “Tauc laws,” using eqn (7).

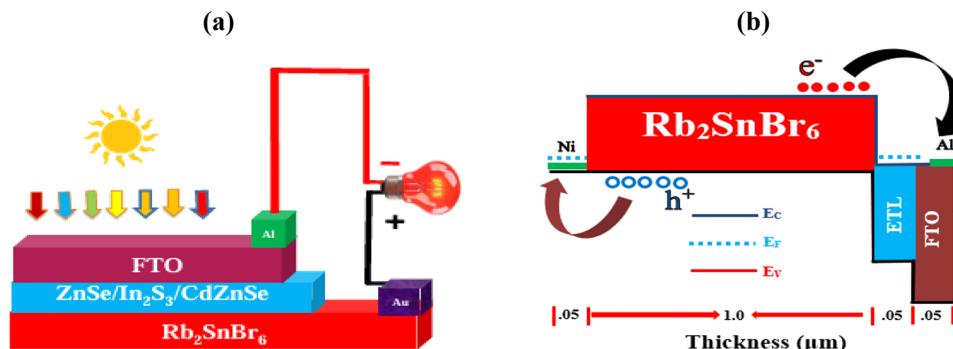
$$\alpha(\lambda) = \left( A + \frac{B}{h\nu} \right) \sqrt{h\nu - E_g} \quad (7)$$

where  $A$  and  $B$  are the constants of the device and the symbols  $E_g$  and  $h\nu$  stand for the energy gap and photon energy, respectively.

### 2.2 The form of the $\text{Rb}_2\text{SnBr}_6$ photocell

Fig. 1(a) illustrates the n-i-p junction model of the  $\text{Rb}_2\text{SnBr}_6$ -based photocell, which forms the core focus of this study. The n, i, and p regions represent the ETL, the intrinsic absorber layer, and the HTL, respectively. In the numerical model, the device architecture includes three ETLs, an absorber layer, a front contact, and a rear (back) contact. Within this configuration, when excitons are generated in the perovskite layer, the ETL plays a crucial role by facilitating the transport of electrons while acting as a barrier to hole movement. This selective charge transport enhances carrier separation and minimizes recombination, contributing to improved device efficiency. The band alignments for the (Au/ $\text{Rb}_2\text{SnBr}_6$ /ETLs/FTO/Al) configurations are shown in Fig. 1(b). Notably, gold (Au), which has been



Fig. 1 Al/FTO/ETL/Rb<sub>2</sub>SnBr<sub>6</sub>/Au diagram illustration (a) and band sketch (b).

the subject of several previous studies, exhibits the highest work function, exceeding 5.47 eV.<sup>37,38</sup> Due to the high work function of gold (Au), constructing a solar cell with this material effectively forms a Schottky barrier that facilitates electron collection. Its optimal alignment with the ZnSe electron band ensures efficient hole transit, thereby minimizing recombination losses. This model increases the overall conductivity, stability, and efficiency of the solar cell. Similarly, with Al also exhibiting a high work function, constructing an (Au/Rb<sub>2</sub>SnBr<sub>6</sub>/ETL (ZnSe, In<sub>2</sub>S<sub>3</sub>, CdZnSe)/FTO/Al) solar cell creates a Schottky barrier to effectively collect electrons.

The excellent alignment between Al and the ZnSe electron band further contributes to improved cell performance and stability.<sup>39</sup> A well-known application of the quarter-wavelength ( $\lambda/4$ ) principle is in enhancing solar cell performance by optimizing layer thickness to the highest optical surface and minimizing reflection. When a level has a thickness equal to an odd factor of  $\lambda/4$ , where  $\lambda$  is the shortest wavelength of light within the material, harmful obstruction is reduced, thereby decreasing reflection and enhancing light propagation and absorption. Specifically, adjusting the thickness of the FTO (fluorine-doped tin oxide) layer to approximately  $\lambda/4$  improves sunlight penetration and optical clarity, particularly within the critical 500–700 nm wavelength range, where solar irradiance is most intense. To maximize light absorption and minimize reflection, similar quarter-wavelength ( $\lambda/4$ ) thickness adjustments should be applied to the ZnSe, In<sub>2</sub>S<sub>3</sub>, CdZnSe, and Rb<sub>2</sub>SnBr<sub>6</sub> layers. This study investigates three distinct device configurations without an HTL, aiming to identify the optimal

ETL for enhanced performance. Each setup is analyzed in detail, and the configuration yielding the best efficiency is selected. Throughout the investigation, the composition of the absorber layer, Rb<sub>2</sub>SnBr<sub>6</sub>, remains constant to ensure consistency and isolate the effects of ETL variation. After optimizing the model, the roles of temperature, density of defects ( $N_t$ ), series-shunt resistance, and other key parameters are analyzed. These include characteristics such as thickness ( $t$ ) and (donor ( $N_D$ ) and acceptor ( $N_A$ )) density. The initial components, including the effective density of the conduction band ( $N_C$ ), energy gap ( $E_g$ ), mobility of electrons ( $\mu_n$ ), insulator permittivity ( $\epsilon_r$ ), effective density of the valence band ( $N_V$ ), electron affinity ( $\chi$ ), hole mobility ( $\mu_p$ ), and various ETLs, FTO, and absorber materials, are listed in Table 1. The SCAPS-1D simulation is performed under AM1.5 solar spectrum conditions with an illumination intensity of 100 mW cm<sup>-2</sup> to evaluate the performance of the device.

The increase in efficiency may be readily seen by calculating the lattice mismatch between the perovskite and ETL layers using eqn (8).

$$\delta = \frac{2|a_s - a_e|}{(a_s + a_e)} \quad (8)$$

The lattice constants for the substrate, lattice misfit, and epitaxial thin film are  $a_s$ ,  $a_e$ , and  $\delta$ , respectively. The lattice properties are an additional important consideration in the development and design of heterojunction models. Table 2 presents the lattice parameters and percentage of lattice mismatch for devices based on Rb<sub>2</sub>SnBr<sub>6</sub> with various reported

Table 1 Parameters for the ETL, perovskite layer, and FTO

Factors	Rb <sub>2</sub> SnBr <sub>6</sub> <sup>12</sup>	ZnSe <sup>40</sup>	In <sub>2</sub> S <sub>3</sub> <sup>41</sup>	CdZnSe <sup>42</sup>	FTO <sup>43</sup>
$t$ (nm)	1000	50	50	50	50
$E_g$ (eV)	1.208	1.8	2.1	2.8	3.6
$\chi$ (eV)	4.25	4.55	4.65	3.8	4.5
$\epsilon_r$	4.208	5.54	13.5	10	10
$N_C$ (cm <sup>-3</sup> )	$1.842 \times 10^{18}$	$1 \times 10^{18}$	$1.8 \times 10^{19}$	$1 \times 10^{18}$	$2 \times 10^{18}$
$N_V$ (cm <sup>-3</sup> )	$1.273 \times 10^{19}$	$1 \times 10^{18}$	$4 \times 10^{13}$	$1 \times 10^{18}$	$1.8 \times 10^{19}$
$\mu_n$ (cm <sup>2</sup> V <sup>-1</sup> s <sup>-1</sup> )	100	100	400	100	100
$\mu_h$ (cm <sup>2</sup> V <sup>-1</sup> s <sup>-1</sup> )	250	50	210	25	20
$N_D$ (cm <sup>-3</sup> )	0	$1 \times 10^{19}$	$1 \times 10^{19}$	$1 \times 10^{19}$	$1 \times 10^{18}$
$N_t$ (cm <sup>-3</sup> )	$1 \times 10^{13}$	$1 \times 10^{13}$	$1 \times 10^{13}$	$1 \times 10^{13}$	$1 \times 10^{14}$
$N_A$ (cm <sup>-3</sup> )	$1 \times 10^{17}$	0	0	0	0



Table 2 Lattice mismatch of the ETL layer with the  $\text{Rb}_2\text{SnBr}_6$  absorber

Layers	Lattice parameters			Lattice mismatch (%)
	<i>a</i> (Å)	<i>b</i> (Å)	<i>c</i> (Å)	
$\text{Rb}_2\text{SnBr}_6$	11.01	11.01	11.01	—
ZnSe	3.98	3.98	6.53	51.08
$\text{In}_2\text{S}_3$	7.621	7.621	32.053	97.73
CdZnSe	5.858	—	—	61.08

Table 3 The performance parameter values for Al/FTO/ETL/Rb<sub>2</sub>SnBr<sub>6</sub>/Au models with several ETLs

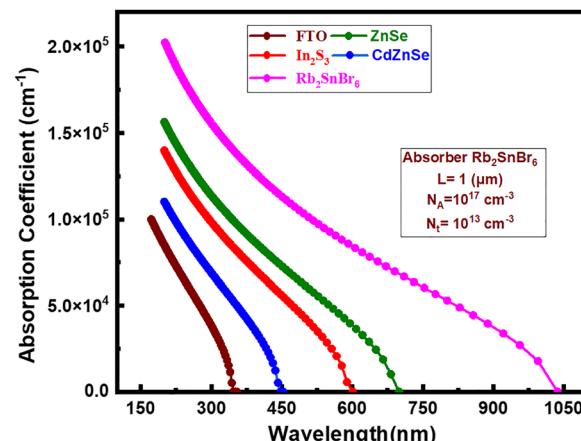
Model	<i>V<sub>OC</sub></i> (V)	<i>J<sub>SC</sub></i> (mA cm <sup>-2</sup> )	FF (%)	PCE (%)
Al/FTO/ZnSe/Rb <sub>2</sub> SnBr <sub>6</sub> /Au	0.868	38.094	86.86	28.73
Al/FTO/In <sub>2</sub> S <sub>3</sub> /Rb <sub>2</sub> SnBr <sub>6</sub> /Au	0.843	38.087	82.93	26.62
Al/FTO/CdZnSe/Rb <sub>2</sub> SnBr <sub>6</sub> /Au	0.869	38.093	72.60	24.04

ETLs. The lattice mismatch between  $\text{Rb}_2\text{SnBr}_6$  and ZnSe was the lowest at 51.08%, while mismatches with other ETLs were substantially higher. Although these values are relatively large (>50%), the simulations assume ideal, defect-free interfaces. This allows the model to predict theoretical upper-limit performance, which explains the excellent PCE observed for device I in Table 3. In practical devices, such high mismatches would likely introduce interface defects and degrade performance. Therefore, interface engineering, passivation layers, or alternative ETLs with better lattice compatibility would be essential to achieve comparable efficiencies experimentally. This clarification emphasizes that the simulation results should be interpreted as performance trends and design guidance rather than direct fabrication predictions. Table 3 summarizes the simulated performance parameters for the Al/FTO/ETL/Rb<sub>2</sub>SnBr<sub>6</sub>/Au structures using the three ETL components.

### 3. Results and discussion

#### 3.1 The factor of absorption for each single layer

The absorption coefficient of each material layer, as determined using the SCAPS-1D simulator, plays a vital role in defining the amount of photoenergy absorbed. This, in turn, meaningfully influences the PCE of the solar cell. High absorption in the first layers of photocells is essential since it shows which light wavelengths the components can absorb.<sup>30,44</sup> The solar cell (SC) architecture used in all three device configurations consists of multiple material layers, including ZnSe, In<sub>2</sub>S<sub>3</sub>, CdZnSe, and Rb<sub>2</sub>SnBr<sub>6</sub>, each selected for their favorable optical and electronic properties. FTO (fluorine-doped tin oxide) serves as the transparent front contact, while the remaining layers function as buffer or absorber materials. Fig. 2 illustrates the wavelength-dependent absorption coefficients for FTO, ZnSe, In<sub>2</sub>S<sub>3</sub>, CdZnSe, and Rb<sub>2</sub>SnBr<sub>6</sub>. FTO shows its zenith absorption at 172.21 nm, primarily within the deep ultraviolet (UV) region. In comparison, ZnSe, In<sub>2</sub>S<sub>3</sub>, CdZnSe, and Rb<sub>2</sub>SnBr<sub>6</sub> demonstrate significant absorption peaks around 200 nm, indicating their effectiveness in the UV-visible spectrum. The maximum absorption coefficients (in  $\text{cm}^{-1}$ ) for these materials are as

Fig. 2 Absorption coefficients ( $\text{cm}^{-1}$ ) for all materials.

follows: Rb<sub>2</sub>SnBr<sub>6</sub> (202 260.602), ZnSe (156 345.149), In<sub>2</sub>S<sub>3</sub> (139 725.667), CdZnSe (110 192.769), and FTO (100 000). These high absorption values are critical for efficient photon harvesting, directly impacting the PCE of the photocells. Among the studied components, Rb<sub>2</sub>SnBr<sub>6</sub> shows the highest absorption, making it a strong candidate for the active perovskite layer. The combination of these materials supports broad-spectrum light absorption, effective charge carrier generation, and optimized solar cell performance.

#### 3.2 Correlation between the work function and solar cell efficiency

For solar panels to function and be effective overall, the left contact is crucial for solar energy.<sup>45</sup> The back contact, an essential part of the electrical structure from which resources show origination, should have the lowest ohmic losses possible in order to improve solar cell performance. A poor contact model could result in elevated opposition in series, which reduces charge movement.

To provide endurance, the back contact can also offer strong adhesion and limited combined communication with the semiconductor. A tiny active zone, less photon absorption, and obscuring can all be consequences of suboptimal contact designs. Well-designed left contacts boost charge carrier buildup and reduce recombination losses, increasing the photo module's overall efficiency and dependability. The reason for choosing ideal metals for the right and left contacts, respectively, is their work functions being restricted to 4.20 eV to 4.95 eV and 5.0 eV to 5.47 eV. Fig. 3(a)–(d) displays the PV properties of structures I, II, and III with various left vs. right connections. We have observed that devices I, II, and III function optimally when gold (Au) is utilized as the back contact. However, the same value is observed for all materials with the appropriate contacts (Al, Fe, Ru, and Tc).

Although it may create an oxide layer, aluminum (Al) is the most economical option among those suitable connections because of its high conductivity and low cost. Al is frequently used in solar cells because it offers a good balance between cost and performance, making it the most practical option for



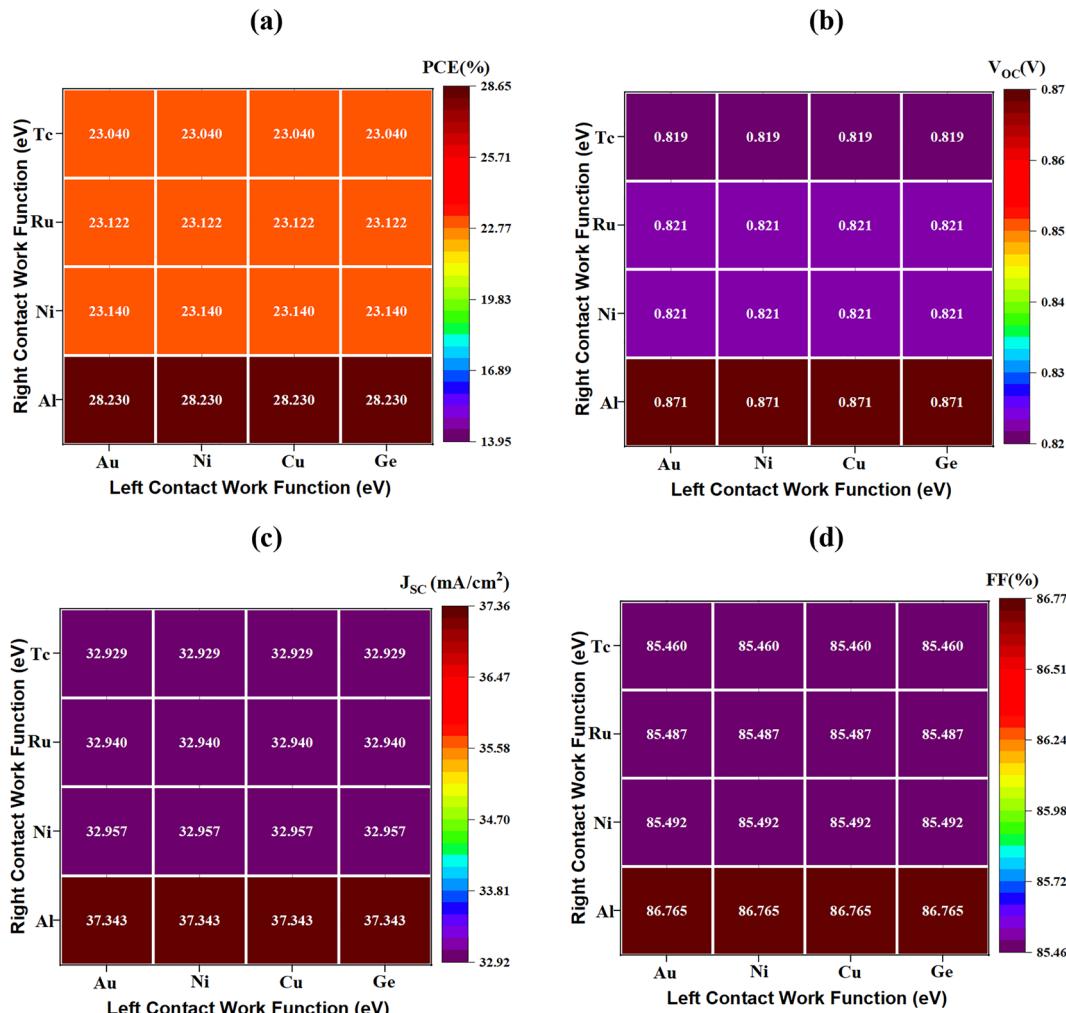


Fig. 3 Effects of left vs. right metal contacts on (a) efficiency, (b)  $V_{OC}$ , (c)  $J_{SC}$ , and (d) FF.

contacts in this application. Although different left contacts provide similar results to Al, Au is employed in  $\text{Rb}_2\text{SnBr}_6$  perovskites due to its high work function, which aligns well with the valence band, and its chemical inertness that ensures stable hole extraction. Unlike Ni, Cu, and Ge, Au does not oxidize or react with halides, thereby providing superior long-term stability and reproducibility. With Au and Al used as the back and front contacts, respectively, the devices achieved the highest performance, with a PCE of 28.23%, FF of 86.765%,  $J_{SC}$  of 37.343 mA cm<sup>-2</sup>, and  $V_{OC}$  of 0.871 V when ZnSe was employed as the ETL.

### 3.3 Electronic band diagram of $\text{Rb}_2\text{SnBr}_6$

The refined energy band gaps for PSCs incorporating  $\text{Rb}_2\text{SnBr}_6$  as the perovskite layer are presented in Fig. 4(a)–(c). The selection of the ETL plays an important role in finding the conduction and valence band offsets, which represent the power rank mismatches between the absorber and bordering transport layers. In this configuration, zinc selenide (ZnSe) is employed as the ETL in conjunction with  $\text{Rb}_2\text{SnBr}_6$  as the light-absorbing material. The arrangement of power levels at the

interfaces, particularly between the ETL and absorber, is essential for efficient carrier separation, minimized recombination reduction, and enhanced total device performance. Proper band alignment facilitates the smooth transfer of photogenerated charge carriers, reducing potential energy barriers that hinder charge flow. In this structure, photogenerated electrons are extracted through the right contact (Al), where holes are collected at the left metallic electrode (Au), enabling efficient carrier separation and current flow. This optimized energy band configuration demonstrates the importance of interfacial engineering in PSCs, highlighting how careful selection and alignment of materials significantly influence power conversion efficiency. Device performance can be greatly influenced by improper energy band alignment at the interface between the ETL and  $\text{Rb}_2\text{SnBr}_6$  absorber. Such misalignment could lead to increased interfacial recombination, which is primarily determined by the surface properties of the contacting layers. Fine-tuning the electrical characteristics of the ETL is crucial for efficient electron extraction in  $\text{Rb}_2\text{SnBr}_6$ -based devices. The ETL must possess a higher ionization energy than the absorber to ensure proper energy-level alignment, which promotes

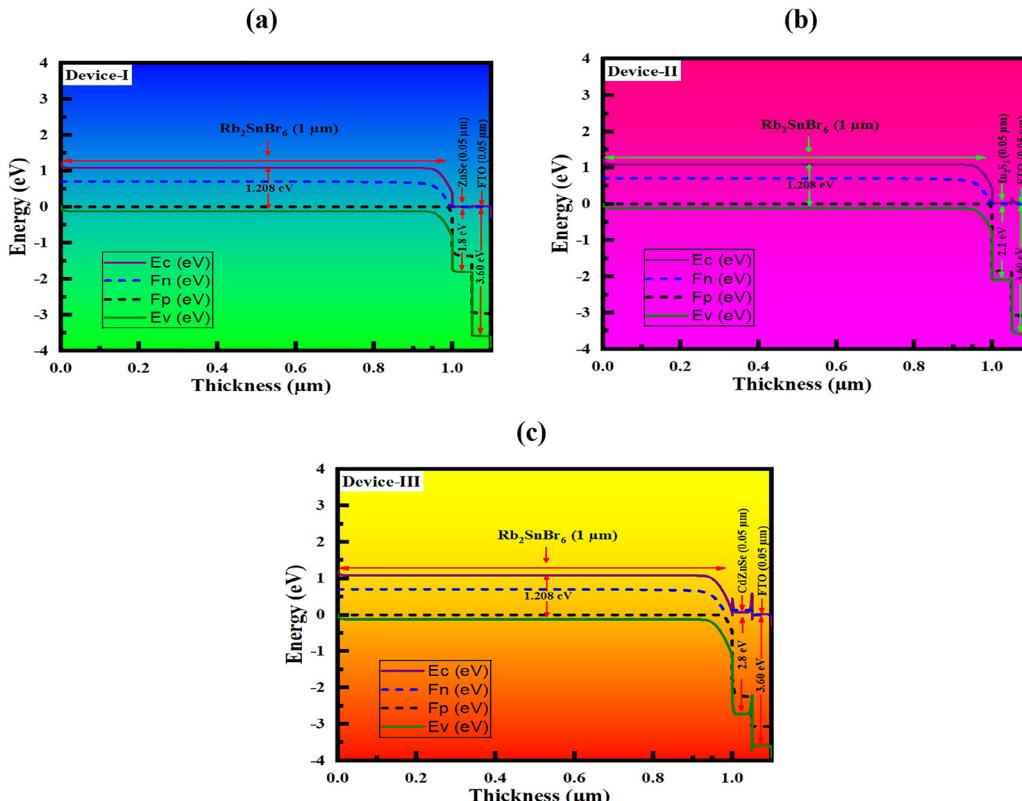


Fig. 4 Band diagrams for (a) ZnSe, (b)  $\text{In}_2\text{S}_3$ , and (c) CdZnSe.

smooth electron transfer, suppresses recombination, and improves device efficiency.

In ideal models, the Fermi level lies near the band of conduction, as shown in Fig. 4(a), with ZnSe as the ETL. Similar performance is also observed with  $\text{In}_2\text{S}_3$  and CdZnSe (Fig. 4(b) and (c)), confirming that effective alignment can be achieved with multiple ETLs. The corresponding device architectures are: device-I (Al/FTO/ZnSe/Rb<sub>2</sub>SnBr<sub>6</sub>/Au), device-II (Al/FTO/ $\text{In}_2\text{S}_3$ /Rb<sub>2</sub>SnBr<sub>6</sub>/Au), and device-III (Al/FTO/CdZnSe/Rb<sub>2</sub>SnBr<sub>6</sub>/Au), as illustrated in Fig. 4(a)–(c).

Cell performance largely depends on the conduction band offset (CBO) and valence band offset (VBO). A spike-like CBO (0–0.2 eV) is typically ideal, as it forms a small barrier at the ETL/absorber interface that suppresses electron backflow while maintaining efficient electron transport, thereby reducing interfacial recombination and enhancing  $V_{\text{OC}}$ . A large positive CBO (>0.4 eV) hinders current flow, while a negative (cliff-like) CBO can increase recombination. Similarly, a spike-like VBO—where the absorber's valence band maximum (VBM) lies slightly below the HTL—improves hole transport and  $V_{\text{OC}}$ , whereas a cliff-like VBO reduces performance.

In our devices, ZnSe,  $\text{In}_2\text{S}_3$ , and CdZnSe act as n-type ETLs with strong electron affinity, while Rb<sub>2</sub>SnBr<sub>6</sub>, being intrinsic or slightly p-type, provides efficient light absorption, charge generation, and hole transport. The small CBM difference (~0.2 eV) between ZnSe (1.8 eV) and Rb<sub>2</sub>SnBr<sub>6</sub> (1.208 eV) forms

a shallow barrier that blocks hole back-transfer without impeding electron flow, ensuring effective charge separation and minimal recombination losses. Although the calculated CBOs for ZnSe (−0.3 eV) and  $\text{In}_2\text{S}_3$  (−0.4 eV) are slightly cliff-like, the cliffs are shallow, and the ETLs' high electron affinity and conductivity enable rapid electron extraction. The favorable VBO further ensures efficient hole transport toward the HTL. Altogether, these factors minimize interfacial recombination and allow high FF and PCE, demonstrating that device performance is determined not solely by the CBO magnitude but by the combined effect of electron and hole transport at the interfaces.

Fig. 4 illustrates the various cliff and spike shapes that have a direct effect on this photocell's efficiency. We're aware that

$$\text{VBO} = \{\chi_{(\text{ETL/HTL})} - E_g(\text{Absorber}) + E_g(\text{ETL/HTL}) - \chi_{(\text{Absorber})}\} \quad (9)$$

$$\text{CBO} = \chi_{\text{Absorber}} - \chi_{(\text{ETL/HTL})} \quad (10)$$

Eqn (9) and (10) were used to find out the CBO and VBO.<sup>46</sup> For the absorber and ETLs, the CBO and VBO is:

For the ZnSe ETL

$$\text{CBO} = \chi_{\text{Absorber}} - \chi_{\text{ETL}} = 4.25 - 4.55 = -0.3 \text{ eV}$$

$$\begin{aligned} \text{VBO} = \chi_{\text{ETL}} - \chi_{\text{Absorber}} + E_g(\text{ETL}) - E_g(\text{Absorber}) &= 4.55 - 4.25 \\ &+ 1.8 - 1.208 = 0.892 \text{ eV} \end{aligned}$$



For the  $\text{In}_2\text{S}_3$  ETL

$$\text{CBO} = \chi_{\text{Absorber}} - \chi_{\text{ETL}} = 4.25 - 4.65 = -0.4 \text{ eV}$$

$$\begin{aligned} \text{VBO} &= \chi_{\text{ETL}} - \chi_{\text{Absorber}} + E_g(\text{ETL}) - E_g(\text{Absorber}) \\ &= 4.65 - 4.25 + 2.1 - 1.208 = 1.292 \text{ eV} \end{aligned}$$

For the  $\text{CdZnSe}$  ETL

$$\text{CBO} = \chi_{\text{Absorber}} - \chi_{\text{ETL}} = 4.25 - 3.8 = 0.45 \text{ eV}$$

$$\begin{aligned} \text{VBO} &= \chi_{\text{ETL}} - \chi_{\text{Absorber}} + E_g(\text{ETL}) - E_g(\text{Absorber}) \\ &= 3.8 - 4.25 + 2.8 - 1.208 = 1.142 \text{ eV} \end{aligned}$$

### 3.4 Impact of thickness of both the ETL and absorber layer

The thickness of the ETL plays a vital role in the overall efficiency of PSCs by affecting carrier mobility and facilitating effective electron extraction from the perovskite layer. As illustrated in Fig. 5(a), the effect of varying ETL thickness from 25 nm to 400 nm was analyzed for  $\text{ZnSe}$ ,  $\text{In}_2\text{S}_3$ , and  $\text{CdZnSe}$ -based devices. The results indicate that changes in ETL thickness within this limit have a minimal role in the PCE of the devices, demonstrating that performance remains relatively stable regardless of the ETL used. However, in devices utilizing  $\text{CdZnSe}$ , reducing the ETL thickness from 50 nm to 25 nm caused a notable drop in  $V_{\text{OC}}$  from 0.93 V to 0.872 V, even though slight improvements in PCE,  $J_{\text{SC}}$ , and FF were observed when increasing the thickness from 25 nm to 50 nm. For devices incorporating  $\text{ZnSe}$  and  $\text{In}_2\text{S}_3$  as ETLs, all photovoltaic parameters remained nearly constant, except for  $\text{ZnSe}$ , which

showed a slight increase in  $J_{\text{SC}}$  with increasing thickness. Although similar performance was recorded at both 25 nm and 50 nm during simulation, a thickness of 50 nm was selected as optimal, as very thin layers (e.g., 25 nm) may introduce challenges in experimental reproducibility and device fabrication. At the optimized ETL thickness of 50 nm, the devices demonstrated the following performance metrics: device-I  $\text{ZnSe}$  achieved an efficiency of 28.40%, a  $V_{\text{OC}}$  of 0.898 V, a FF of 87.86%, and a  $J_{\text{SC}}$  of  $37.08 \text{ mA cm}^{-2}$ ; device-II ( $\text{In}_2\text{S}_3$ ) showed an efficiency of 26.40%, a  $V_{\text{OC}}$  of 0.848 V, an FF of 82.86%, and a  $J_{\text{SC}}$  of  $38.08 \text{ mA cm}^{-2}$ ; and device-III ( $\text{CdZnSe}$ ) showed an efficiency of 24.04%, a  $V_{\text{OC}}$  of 0.898 V, an FF of 87.86%, and a  $J_{\text{SC}}$  of  $37.08 \text{ mA cm}^{-2}$ .

These findings confirm that a 50 nm ETL thickness offers optimal performance while maintaining practical feasibility for further investigations.

Fig. 5(b) demonstrates the effect of varying perovskite layer thickness from 200 nm to 2000 nm on the performance of the reported devices, keeping all other factors from Table 1 stable. Enhancing the thickness of the perovskite absorber layer is crucial to achieving high device efficiency, as it directly influences photon absorption, charge generation, and recombination dynamics. The goal is to determine an optimal thickness that maximizes performance while minimizing material usage, thereby reducing production costs. The simulation results show that increasing the absorber thickness from 200 nm to 1000 nm significantly improves device performance across all configurations. Specifically, for device-I, the efficiency,  $V_{\text{OC}}$ , and short circuit current increased from 22.59% to 28.73%, 0.842 V to 0.868 V, and  $29.52$  to  $38.094 \text{ mA cm}^{-2}$ , respectively. Similarly, device-II exhibited improvements from 19.25% to 26.62% in

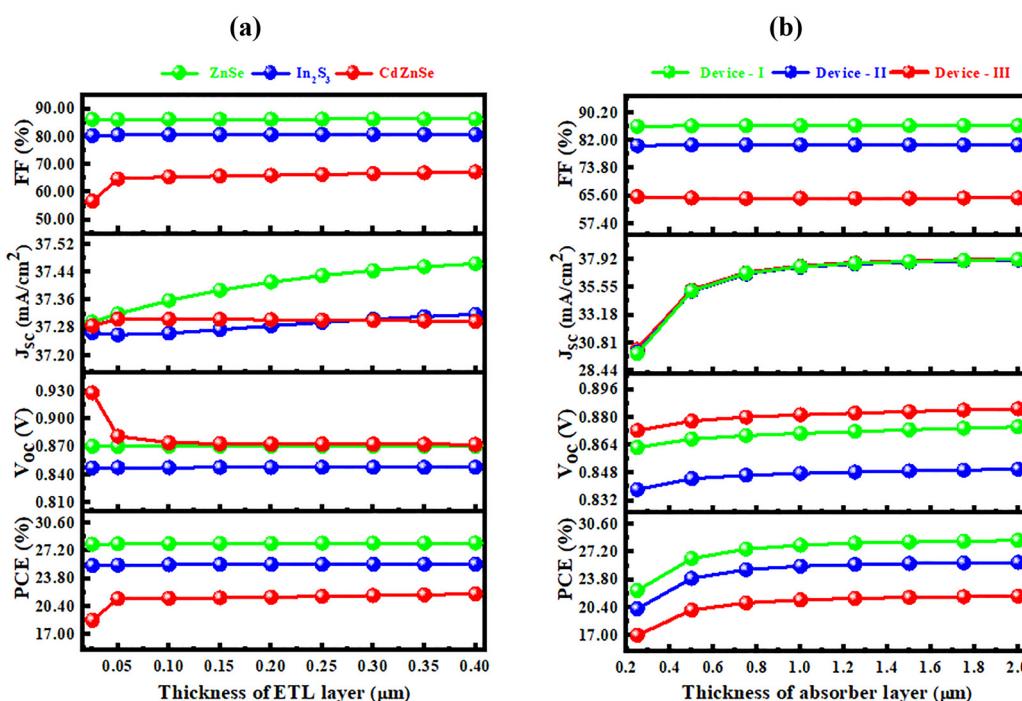


Fig. 5 Effect of PV factors considering the variation in the thickness of the (a) ETL layer and (b) absorber layer on efficiency,  $V_{\text{OC}}$ ,  $J_{\text{SC}}$ , and FF.

PCE, 0.833 V to 0.843 V in  $V_{OC}$ , and 29.52 to 38.087 mA  $\text{cm}^{-2}$  in  $J_{SC}$ . Device-III showed a PCE increase from 16.94% to 24.04%,  $V_{OC}$  slightly varied from 0.872 to 0.869 V, and  $J_{SC}$  rose from 29.52 to 38.092 mA  $\text{cm}^{-2}$ . Beyond a thickness of 1000 nm, these performance metrics plateaued, indicating no further gains with additional material. Throughout the thickness range, the FF remained constant at 86.86%, 82.93%, and 72.60% for devices-I, -II, and -III, respectively. As the absorber layer becomes thicker, both carrier generation and recombination rates increase; thus, an optimal balance must be achieved. Based on these findings, a thickness of 1000 nm is selected as the optimal value, offering the best trade-off between performance enhancement and material efficiency.

### 3.5 Impact of density of doping of the perovskite layer and ETL layer

Optimizing the acceptor doping concentration ( $N_A$ ) in the perovskite layer is pivotal for enhancing solar cell efficiency. Proper doping improves charge carrier concentration, strengthens the built-in solar field at the p-n junction, and enhances charge separation and extraction, thereby boosting total model performance. However, excessive doping can lead to enhanced recombination rates, altered charge transport mechanisms, and the formation of defects, which reduce the  $V_{OC}$  and efficiency. On the other hand, insufficient doping results in weak electric fields and poor carrier separation. Moreover, achieving the optimal doping level adds complexity to the fabrication process and can affect charge carrier mobility. Therefore, precise control of doping concentration is essential

to balance enhanced performance with manufacturability, less recombination, and secure efficient carrier transport in high-performance solar cells. In our simulations, the  $N_A$  of the absorber layer was systematically varied from  $10^{14}$  to  $10^{21}$   $\text{cm}^{-3}$  to determine the optimal value for device performance. As shown in Fig. 6(a), the  $V_{OC}$  and  $J_{SC}$  remain relatively constant up to a doping level of  $10^{16}$   $\text{cm}^{-3}$ . Beyond this point,  $V_{OC}$  began to increase with higher  $N_A$  values. This upward trend is attributed to a reduction in recombination losses and improved hole collection efficiency resulting from the enhanced doping. The increase in  $N_A$  strengthens the internal electric field, facilitating more efficient charge separation and transport, thereby contributing to the observed rise in  $V_{OC}$ . The  $J_{SC}$  remained largely unaffected by changes in the  $N_A$  until it reached  $10^{18}$   $\text{cm}^{-3}$ , after which a noticeable decline was observed. This reduction in  $J_{SC}$  was particularly significant in devices utilizing  $\text{In}_2\text{S}_3$  and  $\text{ZnSe}$  as electron transport layers, while the decrease was slightly less pronounced in devices employing  $\text{CdZnSe}$ . The drop in  $J_{SC}$  at higher doping levels is primarily attributed to the increased presence of impurities and defects within the absorber layer, which act as non-radiative recombination centers.

These defects shorten the carrier lifetime and reduce the number of photogenerated charge carriers that can be effectively collected, ultimately diminishing the device's current output. The FF exhibited a gradual increase with rising  $N_A$ , peaking at  $10^{16}$   $\text{cm}^{-3}$ , beyond which it remained relatively constant even as  $N_A$  exceeded  $10^{18}$   $\text{cm}^{-3}$ . This behavior reflects the sensitivity of FF to internal recombination dynamics within the device. At higher doping levels, increased defect densities

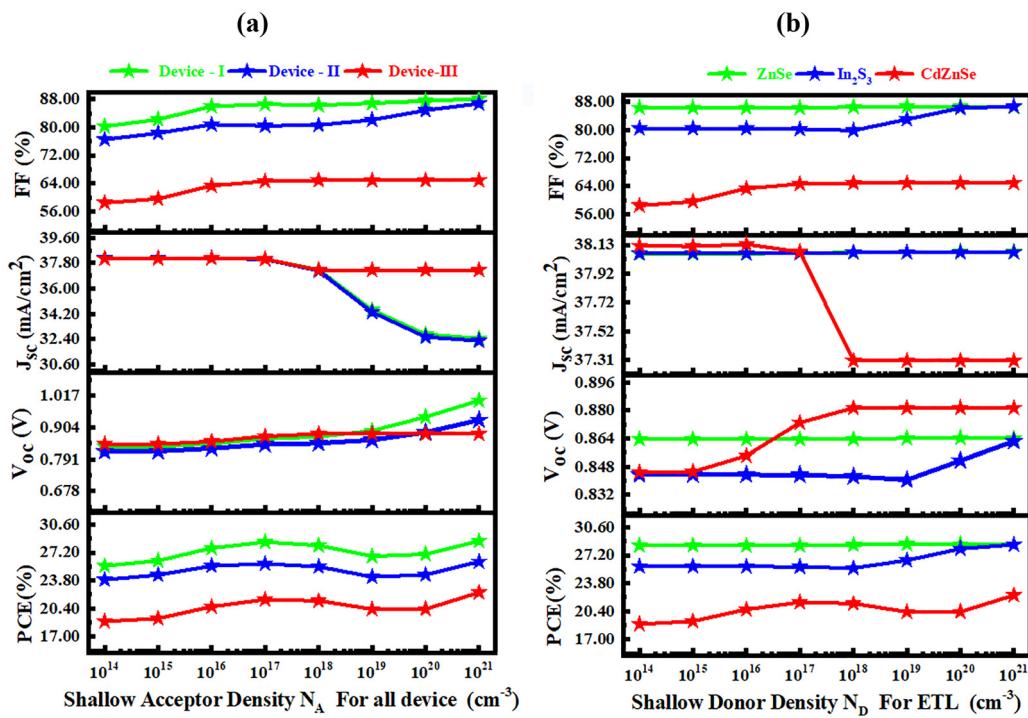


Fig. 6 Effect of PV factors considering the variation in the acceptor density of (a) the perovskite layer and donor density of (b) the ETL layer on PCE,  $V_{OC}$ ,  $J_{SC}$ , and FF.



lead to elevated recombination rates, thereby hindering efficient charge collection at the interfaces. Similarly, the PCE remained stable up to an  $N_A$  of  $10^{16} \text{ cm}^{-3}$  followed by a modest rise before beginning to decline after  $10^{17} \text{ cm}^{-3}$ .<sup>47</sup>

This drop is primarily assigned to the compounded effects of intensified recombination and disrupted charge transport pathways at excessively high doping levels. These simulation results underscore the important impact of  $N_A$  in shaping the performance of perovskite solar cells. Achieving an optimal doping concentration is essential for enhancing carrier density, suppressing recombination losses, and promoting effective charge transport. Based on our findings, an  $N_A$  of  $10^{18} \text{ cm}^{-3}$  represents the optimal value, offering the best balance between efficiency and device stability. Fig. 6(b) further investigates the impact of donor concentration ( $N_D$ ) on the ETL, spanning the limit of  $10^{14} \text{ cm}^{-3}$  to  $10^{21} \text{ cm}^{-3}$ . The findings demonstrate that as the donor concentration rose to  $10^{18} \text{ cm}^{-3}$ , the photovoltaic properties of  $\text{In}_2\text{S}_3$  and  $\text{CdZnSe}$  stabilized. However, a plateau was then achieved, suggesting a minor drop in performance. On the other hand,  $\text{ZnSe}$  stability kept becoming a little better until it reached a donor concentration of  $10^{19} \text{ cm}^{-3}$ . This pattern is consistent with earlier research findings.<sup>47</sup>

This implies that increased donor concentrations improve PCE by facilitating charge carrier extraction and transfer at the ETL/perovskite interface. However, an increase in series resistance happens when the  $N_D$  is too high, which has a detrimental impact on the model's total performance. To enhance device performance, an  $N_D$  of  $10^{17} \text{ cm}^{-3}$  was selected for additional adjustment.

### 3.6 Effects of a $\text{Rb}_2\text{SnBr}_6$ absorber and ETL's defect density $N_t$ fluctuations on the photovoltaic performance of device-I

The effect of defect density ( $N_t$ ) in both the  $\text{Rb}_2\text{SnBr}_6$  perovskite and  $\text{ZnSe}$  ETL on the PV operation of device-I was investigated over a wide range of values, from  $10^{10}$  to  $10^{15} \text{ cm}^{-3}$ . This analysis is crucial, as defect states in these layers play an important role in finding the total efficiency and stability of the model. As presented in Fig. 7(a)–(d), when the density of defects of the  $\text{Rb}_2\text{SnBr}_6$  perovskite increases from  $10^{10}$  to  $10^{16} \text{ cm}^{-3}$ , the performance parameters, namely PCE,  $J_{SC}$ , and FF, exhibit a gradual but consistent decline. The efficiency drops slightly from 28.73% to 28.54%, the short-circuit current decreases from 38.09 to  $38.078 \text{ mA cm}^{-2}$ , and the fill factor falls from 86.86% to 86.75%. These changes, though minimal,

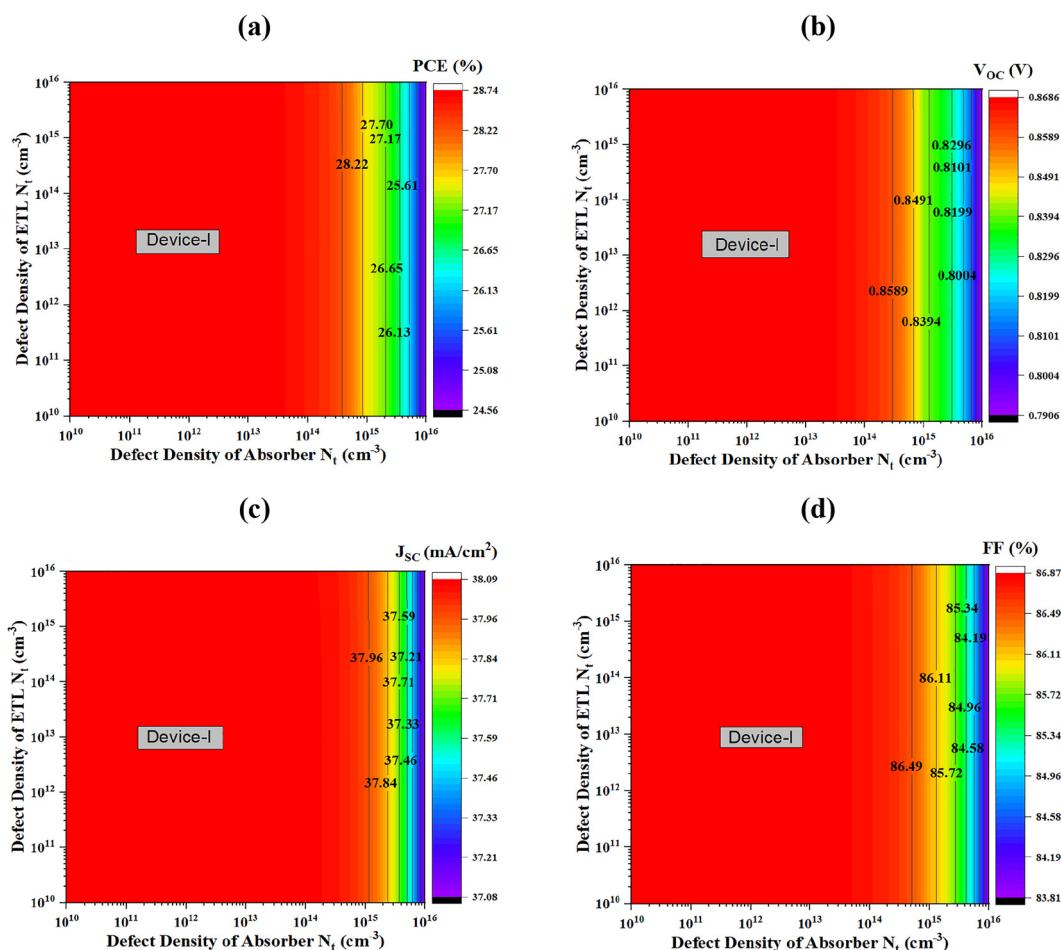


Fig. 7 Role of PV factors considering the modification in the defect density of the ETL vs. the perovskite layer for device-I: (a) efficiency, (b)  $V_{OC}$ , (c)  $J_{SC}$ , and (d) FF.

indicate that up to a density of defects of  $10^{14} \text{ cm}^{-3}$ , the perovskite layer can still support effective charge transport and extraction, with only minor losses due to recombination. Yet, once the absorber defect density surpasses  $10^{14} \text{ cm}^{-3}$  a more pronounced deterioration in device performance is observed. This is attributed to the increase in non-radiative recombination centers, trapping charge carriers and reducing the overall carrier lifetime, leading to substantial losses in both voltage and current generation.<sup>48</sup> Such defect-related losses are particularly detrimental in materials like  $\text{Rb}_2\text{SnBr}_6$ , where the defect tolerance is lower compared to other halide-based semiconductors. In contrast, the variation of defect density in the ZnSe ETL, across the same range from  $10^{10}$  to  $10^{14} \text{ cm}^{-3}$ , shows a negligible impact on all the evaluated photovoltaic parameters.

Throughout this range, the efficiency,  $J_{\text{SC}}$ , and FF remain essentially unchanged, indicating that the device is largely insensitive to the presence of traps or imperfections in the ETL.

This suggests that ZnSe offers favorable energy band alignment and efficient electron transport, which minimizes the impact of intrinsic or extrinsic defects within the layer.

Based on these outcomes, it is evident that the performance of device-I is far more sensitive to defect states in the absorber than in the ETL. Consequently, for optimized device performance and to minimize recombination-related losses, a density of defects of  $10^{13} \text{ cm}^{-3}$  is identified as the optimum for both the  $\text{Rb}_2\text{SnBr}_6$  absorber and the ZnSe ETL. This value offers a balance between realistic material quality and high efficiency, making it a suitable benchmark for further simulation and experimental studies aimed at enhancing device stability and performance.

### 3.7 Effects of a $\text{Rb}_2\text{SnBr}_6$ absorber and ETL's defect density $N_t$ fluctuations on the photovoltaic performance of device-II

The effect of density of defect ( $N_t$ ) fluctuations in the  $\text{Rb}_2\text{SnBr}_6$  absorber and  $\text{In}_2\text{S}_3$  ETL on the photovoltaic performance of device-II was evaluated by varying  $N_t$  from  $10^{10}$  to  $10^{16} \text{ cm}^{-3}$  for both layers. As drawn in Fig. 8(a)–(d), when the density of defects in the absorber increases across this entire range, the key performance parameters remain remarkably stable. Specifically, the device maintains a PCE of 26.62%, a  $V_{\text{OC}}$  of 0.843 V, a  $J_{\text{SC}}$  of  $38.089 \text{ mA cm}^{-2}$ , and an FF of 82.91%. This consistency

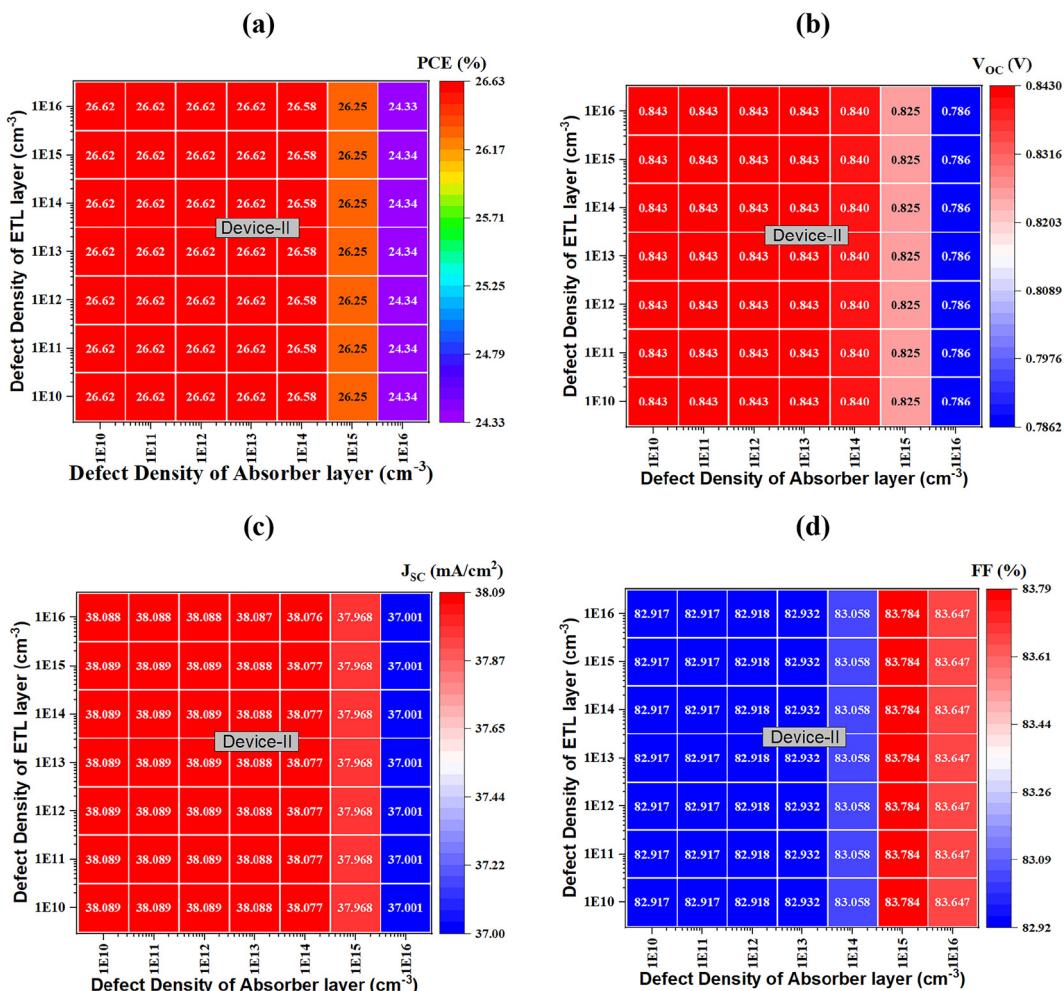


Fig. 8 Role of PV factors considering the modification in the defect density of the ETL vs. absorber layer for device-II: (a) efficiency, (b)  $V_{\text{OC}}$ , (c)  $J_{\text{SC}}$ , and (d) FF.



indicates a high degree of defect tolerance in the absorber layer of device-II, with a negligible impact on charge transport and recombination even at high defect concentrations. However, a different trend is observed when increasing the defect density in the  $\text{In}_2\text{S}_3$  ETL. While performance remains largely unaffected up to a density of defects of  $10^{16} \text{ cm}^{-3}$ , beyond this threshold, slight but noticeable declines in several parameters are observed. As displayed in Fig. 8(a), PCE decreases modestly from 26.62% to 26.25%. Similarly, in Fig. 8(b),  $V_{\text{OC}}$  drops from 0.843 V to 0.825 V, and in Fig. 8(c),  $J_{\text{SC}}$  falls from 38.089 to 37.968  $\text{mA cm}^{-2}$ . Interestingly, as seen in Fig. 8(d), FF exhibits a slight increase, rising from 82.91% to 83.78%, potentially due to improved charge extraction dynamics compensating for minor losses in current and voltage. These findings suggest that device-II exhibits stable and efficient operation across a wide limit of absorber defect densities, with only minimal sensitivity to ETL defect fluctuations, particularly beyond  $10^{14} \text{ cm}^{-3}$ . Based on these results, a defect density of  $10^{13} \text{ cm}^{-3}$  is identified as the optimal value for both the absorber and the ETL. This choice ensures a favorable balance between performance and material quality and is selected for further optimization and device development.

### 3.8 Effects of a $\text{Rb}_2\text{SnBr}_6$ absorber and ETL's defect density $N_t$ fluctuations on the photovoltaic performance of device-III

The influence of defect density ( $N_t$ ) in the  $\text{Rb}_2\text{SnBr}_6$  absorber and  $\text{CdZnSe}$  ETL on the efficiency of device-III was analyzed over a range from  $10^{10}$  to  $10^{16} \text{ cm}^{-3}$ . As displayed in Fig. 9(a)–(d), increasing the absorber's density of defects up to  $10^{14} \text{ cm}^{-3}$  causes only slight reduction in power conversion efficiency (24.06% to 24.04%), short-circuit current (38.09 to  $38.082 \text{ mA cm}^{-2}$ ), and fill factor (72.63% to 70.92%). The observed relationship between absorber layer defect density and  $V_{\text{OC}}$  suggests that as defect density increases, performance tends to decline due to enhanced non-radiative recombination. However, when defect levels are low, the absorber layer exhibits higher efficiency and improved  $V_{\text{OC}}$ , primarily because reduced defect states minimize recombination losses and facilitate better charge carrier lifetimes<sup>49</sup>.

However, beyond  $10^{13} \text{ cm}^{-3}$ , a more significant decline occurs due to enhanced non-radiative recombination. In contrast, variations in  $\text{CdZnSe}$  ETL defect density show a minimal effect on performance, indicating strong defect tolerance and efficient charge transport. Based on these findings, an optimal density of defects of  $10^{13} \text{ cm}^{-3}$  is suggested for both layers,

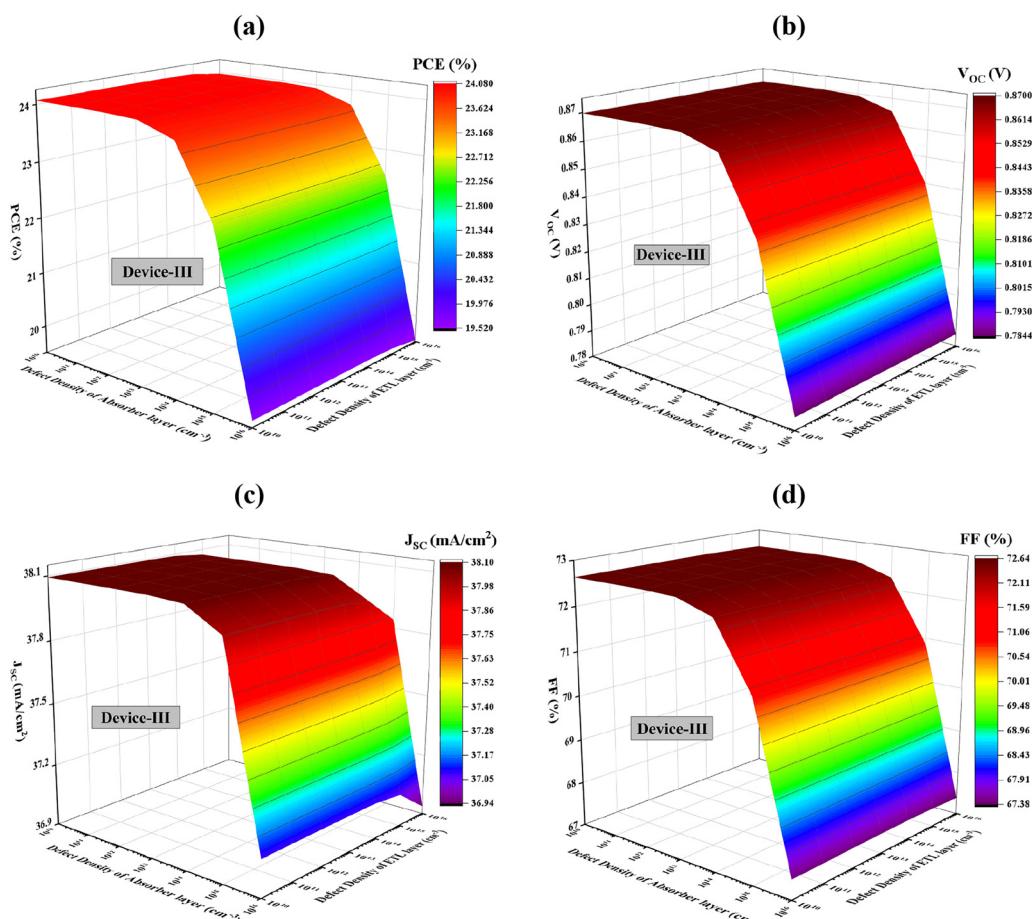


Fig. 9 Role of PV considering the variation in the defect density of the ETL vs. absorber layer for device-III: (a) PCE, (b)  $V_{\text{OC}}$ , (c)  $J_{\text{SC}}$ , and (d) FF.



offering a balance between device efficiency and material quality for further development.

### 3.9 Evaluation of JV and QE features in $\text{Rb}_2\text{SnBr}_6$

Understanding the density of current, representing the electric current generated area density, is pivotal for evaluating the efficiency of photocells, as it directly reflects their efficiency.

The  $J$ - $V$  properties of a structure with the configuration Al/FTO/ETLs/ $\text{Rb}_2\text{SnBr}_6$ /Au, incorporating three different ETLs and measured across a voltage limit of 0 to 0.90 V, are presented in Fig. 10(a). All three configurations exhibit similar photocurrent responses, demonstrating consistent behavior and stable current output throughout the entire voltage limit, from 0.0 to 0.90 V. Yet, a noticeable diminution in photocurrent takes place in all PSCs in the 0.70–0.90 V operating voltage range. In the initial optimization stage, the ETLs based on ZnSe,  $\text{In}_2\text{S}_3$ , and CdZnSe showed increased  $J$ - $V$  efficiency, especially under conditions of  $J_{\text{SC}}$  and  $V_{\text{OC}}$ , relative to those based on ZnSe and  $\text{In}_2\text{S}_3$ . Particularly, the PSCs using devices I, II, and III attained a  $J_{\text{SC}}$  of roughly  $38.09 \text{ mA cm}^{-2}$ . Furthermore, when the input voltage increased, the electricity of light in all models considerably diminished. Fig. 10(b) demonstrates the connection between quantum efficiency (QE) and formula wave interval for PSCs that utilize models I, II, and III, including the wave interval limit of 300–1000 nm. The QE ranges matching each configuration are illustrated in Fig. 10(b). At a spectrum wave interval of 300 nm, PSCs using ZnSe,  $\text{In}_2\text{S}_3$ , and CdZnSe ETLs gained a maximum QE of 100% and less at 1000 nm. The decline in QE observed in most solar cells is primarily attributed to recombination processes that hinder carriers from reaching the external outer circuit. Various factors, including modifications to the front surface that affect carrier collection probability, also play a role in influencing QE. Moreover, for longer wavelengths, a further decrease in QE may result from the absorption of free carriers in strongly doped front surface layers.<sup>50</sup> After achieving their maximum values, the quantum efficiency (QE) of all device designs showed a progressive decrease with increasing wavelength. The decreased absorption of longer-wavelength photons is the cause of this trend. QE is often improved by thickening the absorber layer because a

fatter absorber can capture more incident photons, which increases carrier production.<sup>51</sup>

### 3.10 Examining how interface flaws and temperature affect PV efficiency

The efficiency of PSCs is significantly swayed by recombination losses at the interfaces between  $\text{Rb}_2\text{SnBr}_6$  and the ETL. The main cause of these losses is defects that trap charge carriers, decreasing their mobility and raising the chance of recombination. We changed the defect density ( $N_t$ ) in Fig. 11(a) from  $10^9$  to  $10^{15} \text{ cm}^{-2}$  in order to evaluate its effect at the  $\text{Rb}_2\text{SnBr}_6$ /ETL interface. The findings demonstrate that the PCE of the  $\text{Rb}_2\text{SnBr}_6$ /ZnSe and  $\text{Rb}_2\text{SnBr}_6$ / $\text{In}_2\text{S}_3$  interfaces stayed relatively stable up to an  $N_t$  of  $10^{12} \text{ cm}^{-2}$ . However, it decreased for the  $\text{Rb}_2\text{SnBr}_6$ /CdZnSe interface. Beyond this point, though, the PCE dramatically dropped for every device configuration. The ZnSe-based structure maintained the maximum PCE of 28.75% as  $N_t$  rose, whereas the CdZnSe-based structure showed the lowest PCE of 24.06%. Additionally, a PCE value of 26.62% is assigned to the  $\text{In}_2\text{S}_3$ -based structure. Up to an  $N_t$  of  $10^{12} \text{ cm}^{-2}$ , the  $V_{\text{OC}}$  and FF of the ZnSe- and  $\text{In}_2\text{S}_3$ -based structures stayed constant. However, as  $N_t$  was above this cutoff, both metrics saw notable decline. The decline in PCE was mirrored by a decreased trend in both  $V_{\text{OC}}$  and FF for the CdZnSe-based structure as  $N_t$  increased. However, up to an  $N_t$  of  $10^{15} \text{ cm}^{-2}$ , the  $J_{\text{SC}}$  of the ZnSe,  $\text{In}_2\text{S}_3$ , and CdZnSe-based structures stayed stable. The buildup of trap states and recombination, obstructing the flow and collection of carriers and reducing the solar cells' total performance, is the cause of the performance decline at higher  $N_t$  values.<sup>52</sup> This phenomenon is measured by the higher rate of transport production and recombination on the device's front side, where light enters through the ETL. Finding the optimal  $N_t$  at the  $\text{Rb}_2\text{SnBr}_6$ /ETL interface at  $10^{10} \text{ cm}^{-2}$  reduced recombination losses and improved the model's total performance.<sup>53</sup>

Temperature has a crucial role in the efficiency of photocells, primarily leading to a reduction in total performance. As temperature increases, the band gap of the absorber material slightly decreases, which may cause a minor increase in  $J_{\text{SC}}$ . However, this is usually outweighed by a more substantial reduction in  $V_{\text{OC}}$ , as higher temperatures increase carrier recombination and the reverse saturation current. This leads

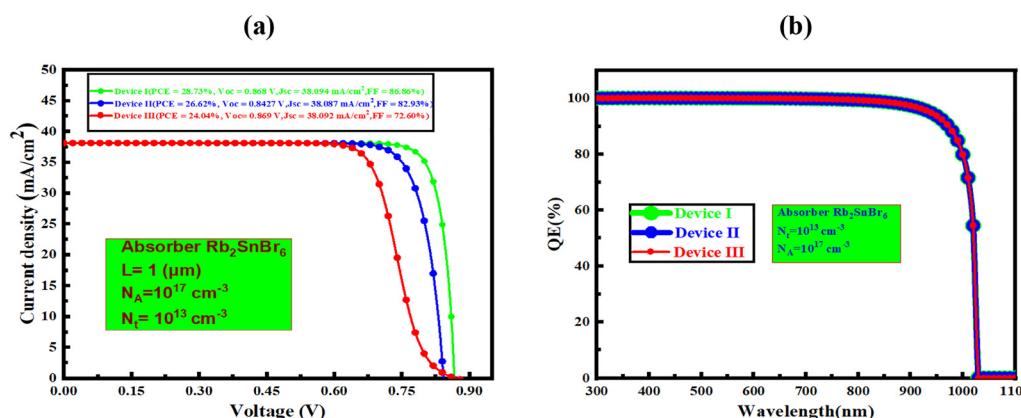


Fig. 10 The (a)  $J$ - $V$  curve and (b) QE diagram of  $\text{Rb}_2\text{SnBr}_6$ .



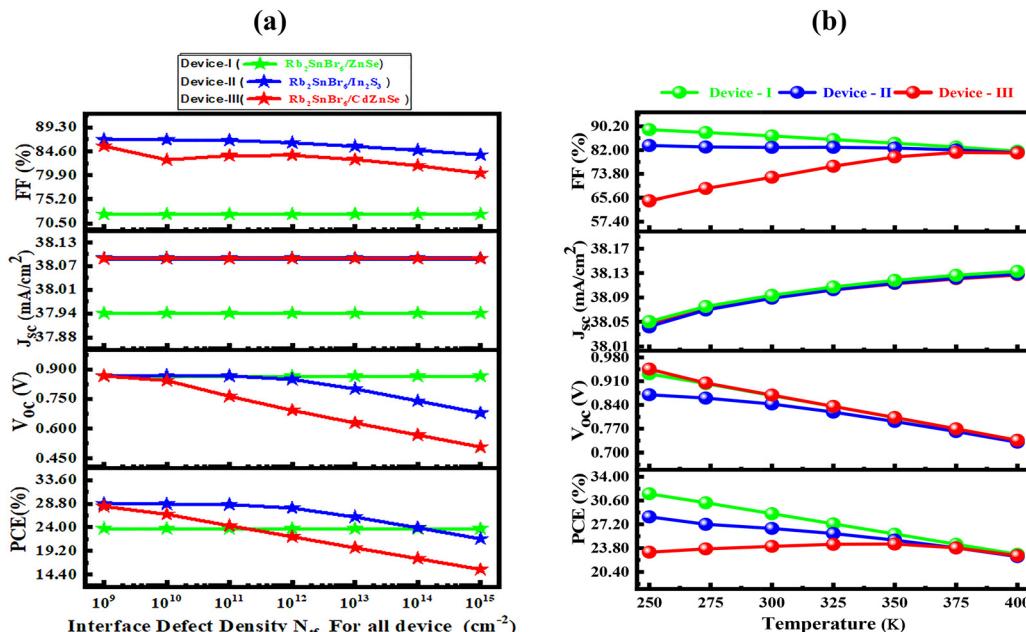


Fig. 11 The role of (a) interface defects and (b) working temperature.

to a decline in  $V_{OC}$  and, consequently, a drop in power conversion efficiency. Additionally, elevated temperatures can increase recombination losses and negatively affect the fill factor. In materials like perovskites, high temperatures can also accelerate degradation processes such as ion migration, thermal decomposition, and interface instability, further reducing device performance and long-term stability. Therefore, effective thermal management is crucial to maintain the efficiency and durability of photovoltaic devices. Within a moderate temperature range, a slight increase can lead to a small rise in current due to bandgap narrowing, but this is usually outweighed by a reduction in open-circuit voltage ( $V_{OC}$ ), resulting in decreased overall efficiency. Typically, efficiency drops by 0.3% to 0.5% per  $^{\circ}\text{C}$  for many solar cell types. Under extreme temperature conditions, the device may experience severe performance degradation due to increased carrier recombination, thermal instability, and material degradation, especially in perovskite-based devices. High temperatures can accelerate ion migration, phase changes, and interfacial breakdown, leading to permanent efficiency loss and reduced lifespan. Therefore, thermal stability is a key factor in reliable PV device design and material selection.

As illustrated in Fig. 11(b), increasing the temperature from 250 K to 400 K leads to a decline in  $V_{OC}$ , PCE, and FF, while  $J_{SC}$  shows a slight increase. Temperature variations have different impacts on the carrier layers, helping transit charge carriers. This fluctuation is attributed to distinctions in conductivity, particular temperature, and density within the components used.<sup>54</sup> Similar patterns are shown for FF,  $J_{SC}$ , and PCE, and the decrease in  $V_{OC}$  becomes more pronounced as the temperature rises.

Eqn (8) is given to help clarify how temperature affects solar cell performance.<sup>55</sup> This behavior is explained by eqn (11):

$$V_{OC} = \frac{E_A}{q} - \frac{nKT}{q} \ln \left( \frac{J_{00}}{J_{SC}} \right). \quad (11)$$

Here  $E_A$  is the activation energy,  $q$  is the elementary charge,  $n$  is the diode ideality factor,  $K$  is the Boltzmann constant,  $T$  is the temperature,  $J_{00}$  is the reverse saturation current, and  $J_{SC}$  is the short-circuit current. As temperature rises,  $J_{00}$  increases exponentially, enhancing the  $\ln(J_{00}/J_{SC})$  term and thereby reducing  $V_{OC}$ . This accounts for the observed drop in  $V_{OC}$  from 0.931 to 0.71 V (device I), 0.945 to 0.71 V (device II), and 0.85 to 0.72 V (device III). PCE declines from 31.65% to 22.14% (device I) and 28.46% to 22.14% (device II), while FF decreases slightly from 90.20% to 81.90% (device I) and 82.00% to 81.90% (device II). In contrast,  $J_{SC}$  increases marginally from 38.04 to 38.10  $\text{mA cm}^{-2}$  across all devices. Overall, device performance improves at lower temperatures, with peak efficiency observed at 250–275 K. However, 300 K is chosen as the optimal operating temperature, as it represents standard test conditions.

### 3.11 The function of carrier concentration and generation-recombination rates

As illustrated in Fig. 12, the area of the solar cell in the apparatus impacts the pace of recombination and production of the charge carrier combination, determining cell efficiency. When a solar cell is triggered, excitons are generated inside. When electrons shift from the valence band to the conduction band, electron-hole pairs are made. SCAPS-1D uses incident photon flux to calculate the generation of charge carriers. Eqn (12) contains  $N_{\text{phot}}(\lambda, \chi)$ , which is applied to calculate the production of the  $G(x)$ , which is known as an electron-hole pair.

$$G(\lambda, \chi) = \alpha(\lambda, \chi) \cdot N_{\text{phot}}(\lambda, \chi) \quad (12)$$

Fig. 12(a) and (b) depict the generation and recombination rates for all construction diagrams of large sites.  $\text{Rb}_2\text{SnBr}_6$

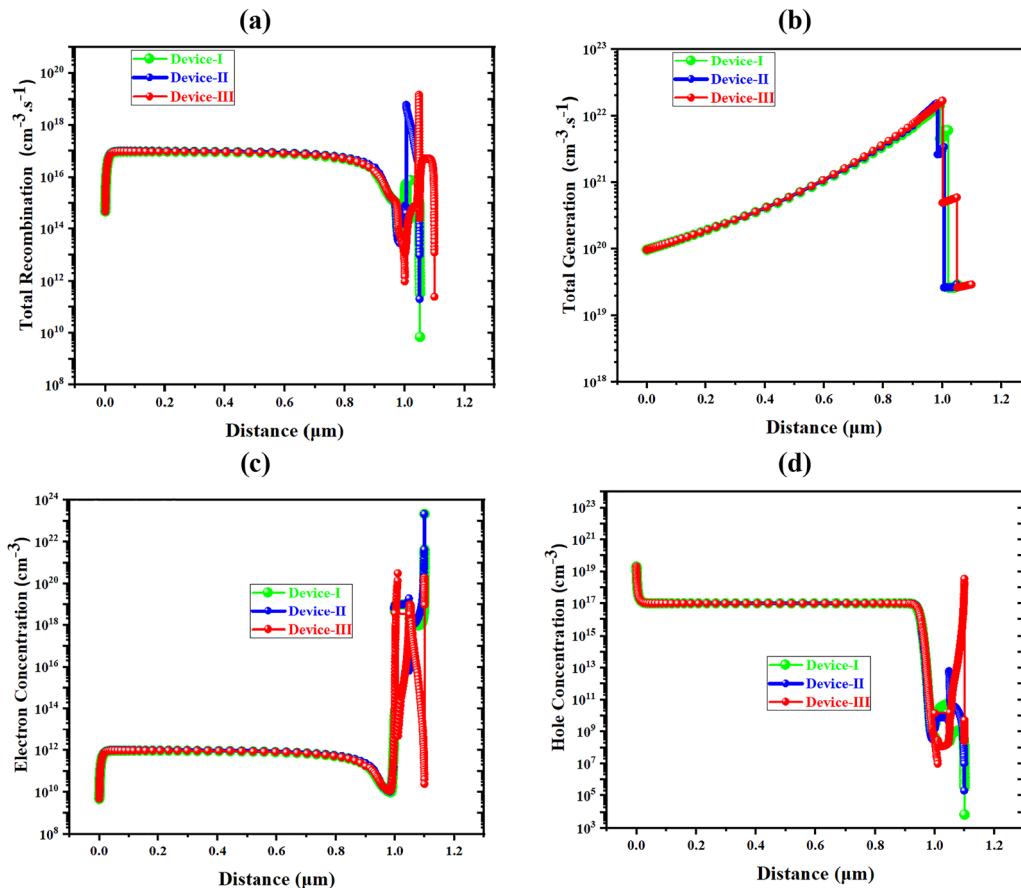


Fig. 12 The effect of the absorber layer's depth on (a) total generation and (b) recombination rates, (c) density of electrons, and (d) density of holes.

emits electrons and holes through carrier formation. When an electron shifts from the hole in the valence band (VB) to the conduction band (CB), it forms couples of electrons and holes. Significantly, this transportation results in an increase in carriers for all devices, with devices I, II, and III producing an inferior value at approximately  $0 \mu\text{m}$  and the largest at approximately  $1.05 \mu\text{m}$ , respectively.

Recombination rate values for every component range from  $0 \mu\text{m}$  at the lowest to  $1.05 \mu\text{m}$  at the highest. Changes in hole and electron configurations occur in the photosystem's energy band. In strong and enhanced SCs, the recombination rates are mostly calculated using the density and endurance of these negatively charged fragments. The defect states present in each stratum are a significant factor affecting SC recombination. When the energy barrier is breached, further electrons from the conduction spectrum make contact with holes in the valence band. The power values linked to this shift also affect the rates of electron and hole recombination.

Fig. 12(c) and (d) exemplify the transitions in the ZnSe,  $\text{In}_2\text{S}_3$ , and  $\text{CdZnSe}$  ETLs and how they affect the electron and hole carrier concentrations. These indicate how deep the  $\text{Rb}_2\text{SnBr}_6$  perovskite layer is. These changes in perovskite depth affect the hole concentration in the  $\text{Rb}_2\text{SnBr}_6$  perovskite because of the influence of various densities of states (DOS) inside the valence electron bands.<sup>56</sup> Greater concentrations of carriers are more significant,

notably when they align with parallel densities of electrons and holes. According to this work, the performance of the absorber substances may be enhanced by employing ZnSe as the ETL in conjunction with  $\text{Rb}_2\text{SnBr}_6$  to reduce hole-electron recombination and increase carrier generation. This technology could potentially enable the creation of highly profitable SCs.

### 3.12 Effects of series and shunt resistances on photocell performance

The use of series resistance ( $R_s$ ) and shunt resistance ( $R_{sh}$ ) in the solar cell device is investigated in Fig. 13. The resistance of the front and back conductive interfaces, the circuit resistance, and the incremental resistance work together to determine a photocell's  $R_s$ . Higher  $R_{sh}$  and minimum  $R_s$  are crucial for the SC to run more optimally.<sup>57,58</sup> The outcomes of these impedances also change the  $J_{SC}$  and  $V_{OC}$ .  $R_s$  is assessed between 0 and  $5 \Omega \text{ cm}^2$ , while  $R_{sh}$  is assessed between 10 and  $10^7 \Omega \text{ cm}^2$ , and the efficacy of the recommended and traditional SCs is observed using SCAPS-1D.  $V_{OC}$  is significantly impacted by  $R_{sh}$ . With an increase in  $R_{sh}$  from 10 to  $10^3 \Omega \text{ cm}^2$ , the value of  $V_{OC}$  rises from 0.38 to 0.87 V. Raising the  $R_s$  by itself remains constant at the  $V_{OC}$  from 0 to  $5 \Omega \text{ cm}^2$  when  $R_{sh}$  is  $0 \Omega \text{ cm}^2$  as displayed in Fig. 13(b). Fig. 13(c) depicts the highest  $J_{SC}$  at  $0 \Omega \text{ cm}^2 R_s$  and  $0-10^7 \Omega \text{ cm}^2 R_{sh}$ . This  $R_s$  mainly reduces the FF and stops it from increasing. As depicted in Fig. 13, when  $R_s$



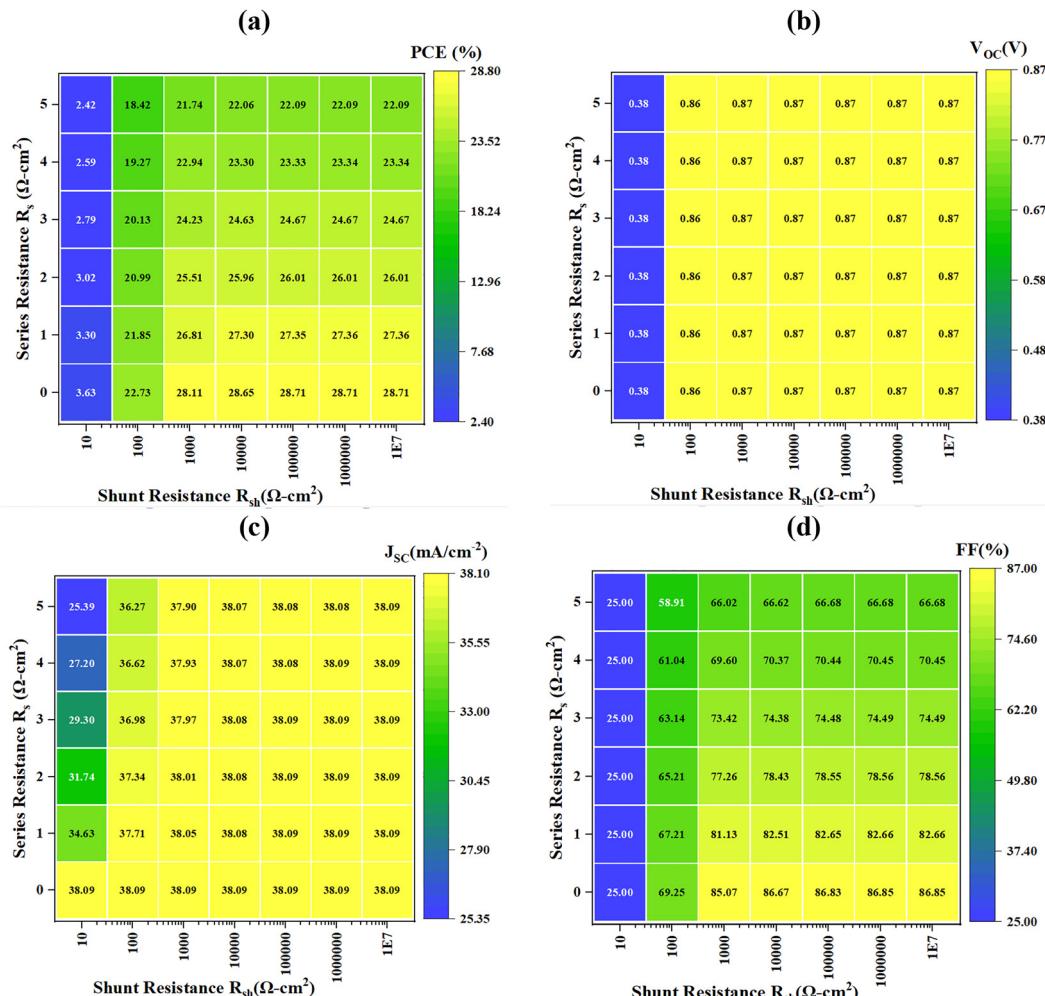


Fig. 13 Impact of the change in series vs. shunt impedance on PV parameters: optimum device-I values for (a) efficiency, (b)  $V_{OC}$ , (c)  $J_{SC}$ , and (d) FF.

rises from 0 to  $6 \Omega \text{ cm}^2$  and  $R_{sh}$  varies from 10 to  $10^7 \Omega \text{ cm}^2$ , the  $V_{OC}$ ,  $J_{SC}$ , FF (Fig. 13(d)), and PCE (Fig. 13(a)) shift from 0.38 V to 0.87 V, 25.79 to 38.09  $\text{mA cm}^{-2}$ , 25.00 to 86.67% and 2.42 to 28.71%, respectively. According to the study, to increase  $R_{sh}$  and decrease  $R_s$ , ideal outputs should be gained.

### 3.13 Enhanced apparatus when contrasted to earlier studies

According to scientists studying  $\text{Rb}_2\text{SnBr}_6$ -based solar cells today, using  $\text{ZnSe}$  as the ETL at first led to subpar performance. Nevertheless, further investigation has generated a necessary discovery: at the beginning of this year, a peak efficiency of 27.25% was seen.<sup>12</sup> This value suggests that photo-systems based on  $\text{Rb}_2\text{SnBr}_6$  have been functioning more productively each year. This work on the optimum device model, as displayed in Fig. 14, unexpectedly discovered an amazing 28.73% largest PCE for  $\text{Rb}_2\text{SnBr}_6$ -based solar cells, with an FF of 86.86%, a  $J_{SC}$  of  $38.094 \text{ mA cm}^{-2}$ , and a  $V_{OC}$  of 0.868 V. A correlation between the output metrics from this research and those from previous research is shown in Table 4.

To improve the reliability and validity of simulation outcomes, as summarized in Table 4, future experimental

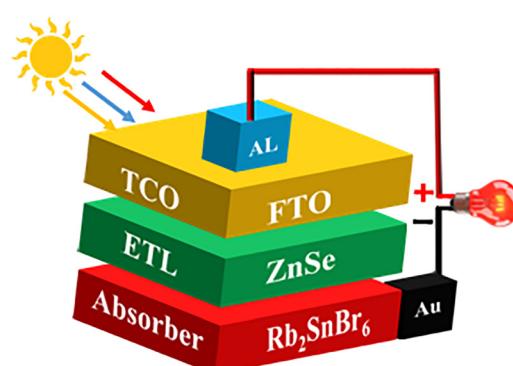


Fig. 14 The optimum structure Al/FTO/ZnSe/Rb<sub>2</sub>SnBr<sub>6</sub>/Au.

investigations should adopt a comprehensive approach that encompasses material combination, depiction, device manufacturing, performance evaluation, and durability testing.

Although experimental reports on  $\text{Rb}_2\text{SnBr}_6$ -based PSCs are limited, our simulations show that device I (Au/Rb<sub>2</sub>SnBr<sub>6</sub>/ZnSe/FTO/Al) achieves a PCE of 28.73%, slightly higher than the

**Table 4** Evaluation and comparison of the PV performance indicators found in this study with those found for previous double absorber designs that have been published in the literature

Structure	$V_{OC}$ (V)	$J_{SC}$ (mA cm $^{-2}$ )	FF (%)	PCE (%)	Ref.
Device-I	0.8682	38.094	86.86	28.73	This work
Device-II	0.8427	38.087	82.93	26.62	This work
Device-III	0.8693	38.093	72.60	24.04	This work
FTO/TiO <sub>2</sub> /Rb <sub>2</sub> SnBr <sub>6</sub>	0.87	36.72	85.18	27.25	12
TiO <sub>2</sub> /CsPbI <sub>3</sub> /CBTS	0.99	21.07	85.21	17.9%	59
CuSCN/CsGeI <sub>3</sub> /C <sub>60</sub>	1.0169	19.653	88.13	17.61	60
ZnO/CsSnI <sub>3</sub> /NiO <sub>x</sub>	1.05	28.02	81.22	23.84	61
CuSCN/FASnI <sub>3</sub> /Zn	1.0859	28.12	84.96	25.94	62
CuI/KSnI <sub>3</sub> /ZnO/FTO	1.44	17.06	85.24	20.99	63
WS <sub>2</sub> /Cs <sub>4</sub> CuSb <sub>2</sub> Cl <sub>12</sub> /CuSbS <sub>2</sub>	1.16	29.27	83.33	23.10	48
ZnMgO/CsSnI <sub>3</sub> /GO	0.62	35.61	78.21	17.37	64
FTO/SnS <sub>2</sub> /RbSnI <sub>3</sub>	0.83	51.83	81.44	26.38	65

27.25% reported for FTO/TiO<sub>2</sub>/Rb<sub>2</sub>SnBr<sub>6</sub> devices.<sup>12</sup> This improvement can be attributed to optimized ETL selection, which enhances charge transport and reduces recombination losses. Device II (In<sub>2</sub>S<sub>3</sub>) and device III (CdZnSe) exhibit lower PCEs (26.62% and 24.04%, respectively), highlighting the critical role of ETL choice. As summarized in Table 4, device I not only outperforms previous Rb<sub>2</sub>SnBr<sub>6</sub>-based PSCs, but also demonstrates superior PCE compared with other lead-free perovskites, such as CsSnI<sub>3</sub><sup>-</sup>, FASnI<sub>3</sub><sup>-</sup>, and Cs<sub>4</sub>CuSb<sub>2</sub>Cl<sub>12</sub>-based devices, indicating its competitive efficiency and favorable optoelectronic properties. Moreover, the random forest model with SHAP analysis identifies layer thickness, defect density, and doping concentration as the most influential parameters, providing interpretable guidance for experimental optimization and interface engineering. These insights bridge the gap between theoretical predictions and practical device design, highlighting the effectiveness of optimized ETL selection and the predictive value of the simulation-ML framework in guiding high-performance, lead-free PSC development.

## 4. Employing machine learning to forecast and improve PSC performance

The incorporation of artificial intelligence (AI) in renewable energy has facilitated significant advancements in materials discovery, device optimization, and performance prediction. In this context, machine learning (ML) has demonstrated significant efficacy in PSC research, as the complex interactions between materials and devices complicate performance optimization *via* traditional experimental and simulation methods.<sup>66,67</sup> Utilizing machine learning models allows for the capture of complex relationships among physical parameters, facilitating precise predictions of photovoltaic behavior and markedly decreasing both computational and experimental expenses. This study constructed a dataset from 1000 SCAPS-1D simulations, systematically varying the properties of the absorber, ETL, and HTL within practical ranges of interest. Key variables included absorber thickness, defect density,

doping concentration, and material parameters, all of which influence photovoltaic performance. The simulations generated output parameters, including  $V_{OC}$ ,  $J_{SC}$ , FF, and PCE, which formed a structured dataset appropriate for supervised learning. The large dataset provided adequate variability for the ML model to effectively capture nonlinear dependencies between material properties and device output. The dataset was randomly divided into an 80:20 split, allocating 800 samples for training and 200 for independent testing to ensure thorough model evaluation. This method is commonly employed to evaluate generalization ability, mitigating the risk of overfitting to the training dataset. A 10-fold cross-validation procedure was conducted solely on the training subset to further assess the model's robustness beyond the initial partitioning. In this procedure, the training data were systematically partitioned into ten folds, utilizing nine folds for training and one-fold for validation in each iteration, thereby ensuring that each data point contributed to both model training and validation. This strategy reduced the likelihood of random bias in train-test partitioning and yielded a dependable estimate of predictive accuracy.

The random forest (RF) algorithm was chosen for predictive modeling due to its ability to manage nonlinearities, intricate feature interactions, and diverse data distributions without requiring extensive preprocessing.<sup>68</sup> In contrast to deep neural networks, which can add unnecessary complexity when data are limited, random forests maintain a balance among accuracy, interpretability, and computational efficiency.<sup>69,70</sup> Additionally, the ensemble-based learning approach mitigates the risk of overfitting by averaging the outputs of several decorrelated decision trees. The random forest was configured with 1000 estimators, each trained on bootstrap samples of the training dataset, which ensured diversity among the trees and enhanced generalization. Hyperparameters were optimized using a comprehensive grid search process, evaluating various candidate values for maximum depth, minimum samples per split, and the number of features considered at each split. The optimized configuration comprised a maximum tree depth of 25 nodes, a minimum of two samples per split, and square-root feature selection at each branching step. This configuration achieved an ideal equilibrium between capturing intricate interactions and avoiding excessive complexity in individual trees. Validation results demonstrated consistent predictive performance across folds, with root mean square error (RMSE) values under 0.02 for normalized outputs and coefficients of determination ( $R^2 > 0.8825$ ) for all photovoltaic parameters. Scatter plots analysis indicated a swift convergence of training and validation errors, with no divergence observed, thereby confirming the lack of high-variance overfitting. Parity plots provided additional support, demonstrating that predicted and actual values closely aligned along the diagonal, highlighting the reliability of the RF model. In addition to prediction accuracy, interpretability improved *via* feature importance analysis, which measured the relative contribution of each input parameter to the model's decision-making process. This interpretability validated the physical soundness of the machine



learning predictions and provided actionable insights into the relationships between material properties and performance, thereby guiding future experimental optimization.

#### 4.1 Synopsis of the RF algorithm

This study utilized the RF algorithm due to its exceptional capacity for producing precise forecasts while ensuring interpretability and robustness. As an ensemble learning method, RF produces several regression trees, each constructed from casually appointed subsets of data and features. The ultimate output is obtained by consolidating the findings of these several trees either *via* majority vote for classification jobs or averaging for regression issues. This collaborative decision-making process improves the model's stability and generalization capabilities, rendering it suitable for intricate scientific applications like PV performance prediction. A primary benefit of RF is its ability to identify complex, non-linear correlations between material properties and PV operational variable relationships that frequently elude simpler statistical methods.<sup>71,72</sup> By amalgamating numerous decision trees, RF circumvents dependence on a solitary model and attains equilibrium between predictive efficacy and robustness.

The primary advantages of the RF method in this situation can be listed as follows:

Modeling complex interactions: RF adeptly captures non-linear relationships between component features and PV metrics, facilitating a more accurate simulation of real-world behavior.

Overfitting mitigation: by averaging predictions from many decision trees, the model's variance is diminished, hence reducing the likelihood of overfitting, a prevalent drawback of singular decision trees.

Feature significance evaluation: RF delivers significance scores for each input variable, thereby determining which features have the most significant impact on PSC efficiency. This facilitates both scientific analysis and the prioritization of experiments.

Hyperparameter tuning: various parameters were meticulously tuned to enhance performance. These encompass:

- Quantity of trees (T): set at 100 to optimize operational efficiency and prediction precision.
- Tree depth: limited to avoid undue complexity and overfitting.
- Minimum samples per leaf node: established at two, guaranteeing generalizable forecasts devoid of bias from excessively minor splits.
- Bootstrap sampling: utilized to provide varied training subsets, enhancing robustness.
- Feature subsampling: randomly picking features at each split mitigates the dominance of variables and guarantees equitable representation of all input parameters.

A feature selection technique was applied to improve model accuracy and interpretability. This investigation indicated that only a limited number of variables significantly influenced PV characteristics. Fig. 15 demonstrates that among the eleven most significant features, bandgap, left contact, and temperature

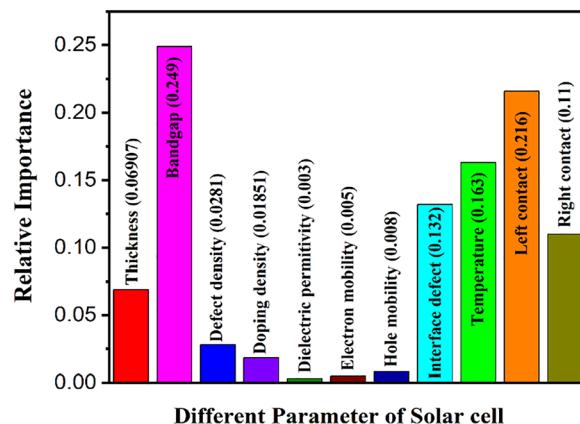


Fig. 15 The integration of ML enables the identification of critical design parameters that significantly influence and enhance the PCE of Au/Rb<sub>2</sub>SnBr<sub>6</sub>/ZnSe/FTO/Al solar cells.

exhibited the greatest influence on PSC efficiency. Secondary considerations encompassed interface defect density, contact integrity, layer thickness, doping concentration, carrier mobilities (both electron and hole), and dielectric permittivity, all of which exhibited comparatively minor impact. A refined RF model was created by concentrating solely on the most crucial parameters. This streamlined version attained roughly equivalent prediction performance to the full-feature model while substantially decreasing processing requirements. The integration of ensemble learning with systematic feature selection enhanced prediction reliability and offered deeper scientific understanding of the critical aspects influencing PSC performance.

#### 4.2 Disclosing feature importance in predictive models through SHAP values

This study addresses a significant challenge in applying machine learning to photovoltaic research: achieving high predictive accuracy while ensuring transparent reasoning for model outputs. This was accomplished through the integration of Shapley additive explanations (SHAP). SHAP, based on cooperative game theory, provides a robust and model-agnostic framework for interpretability that quantifies the contribution of each feature to the predictive outcome. This approach ensures fairness, transparency, and reproducibility, offering both global and local perspectives.<sup>73</sup> The SHAP summary plot (Fig. 16) indicated that contact layers (left and right) and hole mobility had the most significant positive impact on PCE, with increased values consistently improving device performance. Conversely, increased defect density, interface defects, and the dielectric constant negatively impacted performance, aligning with their contribution to recombination losses and diminished carrier lifetime. The bandgap and doping density demonstrated nonlinear effects, with both excessively high and low values leading to reduced efficiency. This underscores the necessity of maintaining optimal ranges for band alignment and charge balance. Electron mobility, absorber thickness, and operating temperature exhibited moderate, context-dependent effects, with their advantages reliant on the concurrent regulation



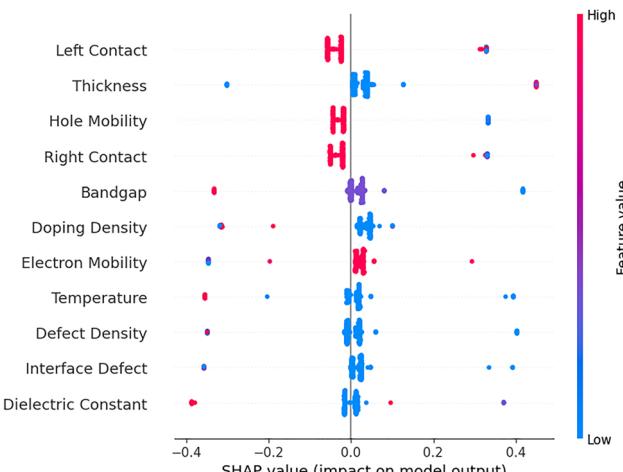


Fig. 16 The impact of individual variables on PCE was systematically evaluated using SHAP values, with rankings derived from their importance in the RF regression model.

of additional parameters, including the reduction of defect density and the optimization of hole mobility. The distribution of SHAP values revealed that certain parameters, like contact quality, exerted consistently strong effects across the majority of samples, while others, such as bandgap, exhibited varied and occasionally opposing influences based on their magnitude and interactions with other features. This analysis highlights that the efficiency of PSC is determined by the complex and nonlinear interactions among various material and structural variables, rather than by a

single dominant factor. This study integrates SHAP into the modeling framework, illustrating how explainable AI can both validate predictive reliability and generate physically meaningful insights. This approach offers a scientifically grounded method for directing material design, defect engineering, and optimization strategies in next-generation perovskite solar cells.

#### 4.3 Analysis of the correlation heatmap

Fig. 17 illustrates the correlation heatmap for the eleven input features utilized in the ML-assisted solar cell design: thickness, dielectric constant, defect density, doping density, bandgap, electron mobility, hole mobility, interface defect, temperature, left contact, and right contact. The diagonal value of 1.00 indicates self-correlation, whereas the off-diagonal entries demonstrate the extent of pairwise linear correlations, varying from  $-1$  (strong negative correlation) to  $+1$  (strong positive correlation).<sup>74</sup> Most correlation coefficients are near 0, signifying that the bulk of variables exhibit weak correlations and are mostly independent. This benefits the ML framework by reducing multicollinearity and ensuring that each parameter provides distinct information to the predictive model. Minor correlations were noted, including a slight negative association between electron mobility and hole mobility ( $-0.08$ ), indicating a subtle trade-off in charge transport properties. Electron mobility and dielectric constant ( $0.07$ ) demonstrated a slight positive correlation, indicating a possible relationship between dielectric characteristics and carrier mobility. All other feature pairings, including thickness, bandgap, and defect-related characteristics, exhibited minimal

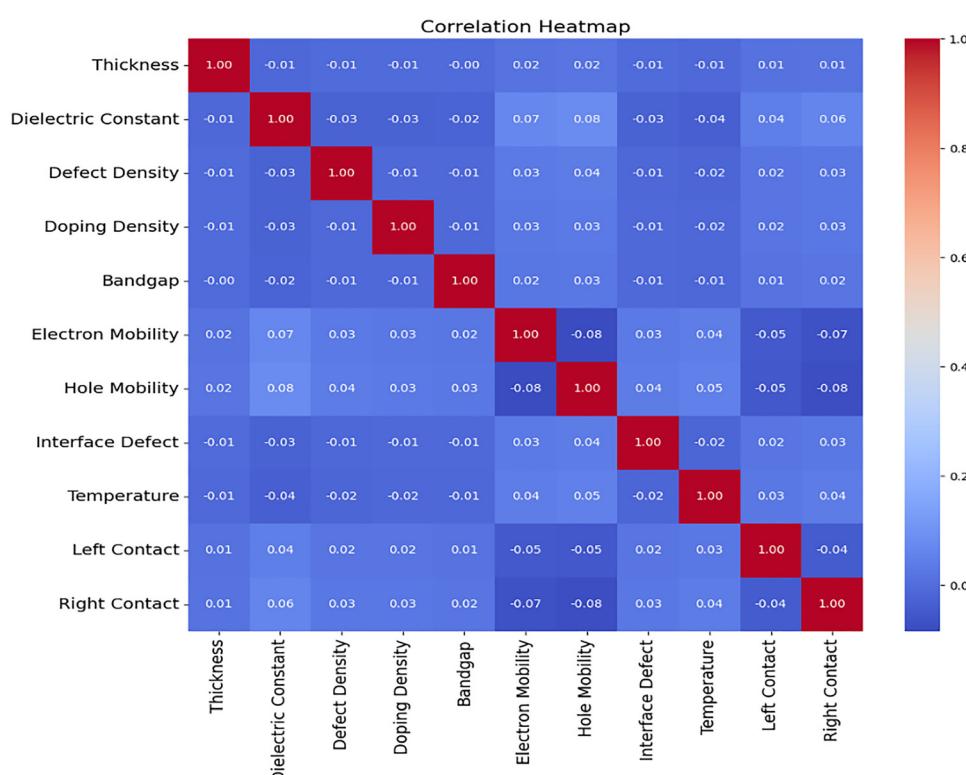


Fig. 17 Correlation heatmap of the proposed solar cell structure showing relationships among different variable parameters.



correlation values. The comprehensive dispersion of correlations validates the appropriateness of the chosen variables for ML research, as they jointly offer varied and independent descriptions of the solar cell system. This improves the interpretability and robustness of the RF model in assessing feature significance and optimizing PV performance.

#### 4.4 Metrics and outcomes of performance assessment

A thorough evaluation framework was built to examine the predictive capabilities of the RF model in forecasting key performance characteristics of PV systems. The structure was experimented with 1100 estimators, ensuring that the ensemble accurately represented the intricate interactions between material attributes and PV efficiency measures. Upon completion of training, the structure generated predictions for several PV components, which were later matched to simulation data to assess performance reliability. The precision of predictions was illustrated using scatter plots (Fig. 18), in which the expected outcomes were compared to actual values. These plots offer a clear assessment of model accuracy, with a closer alignment of dots along the reference line ( $y = x$ ) signifying enhanced prediction performance.

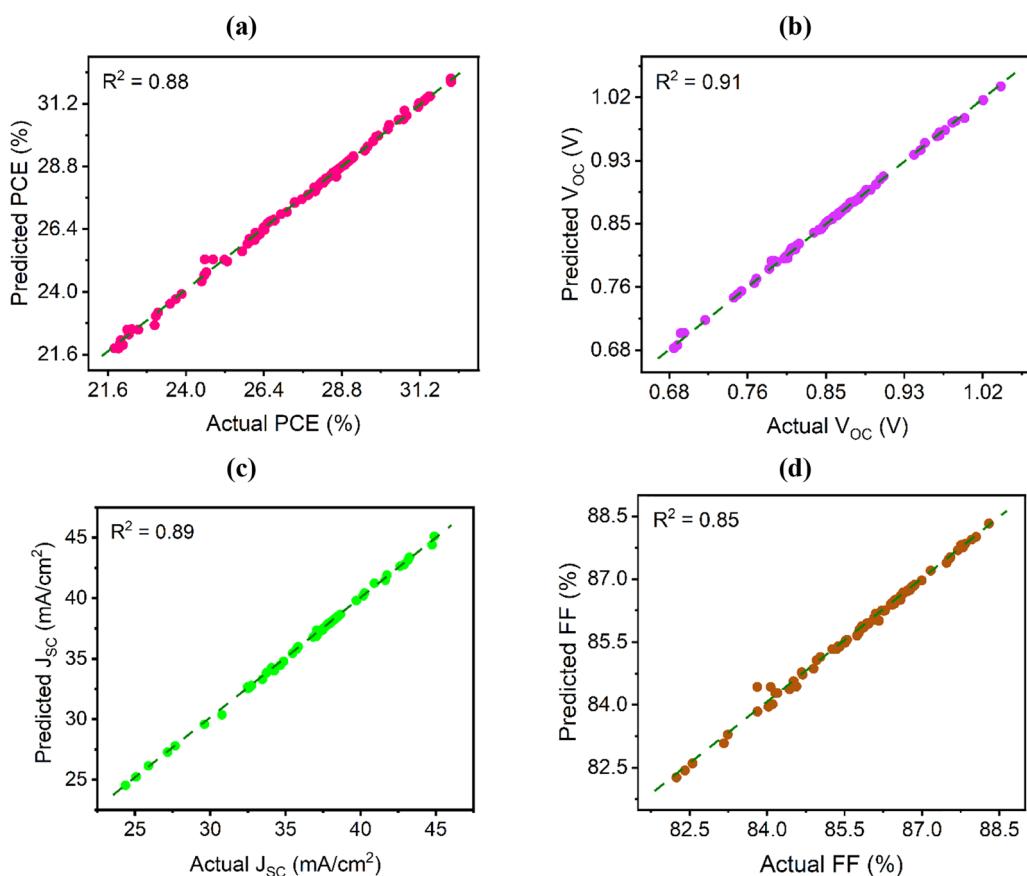
The predictive accuracy of the RF model was further assessed using established statistical metrics:

**Coefficient of determination ( $R^2$ ):** this statistic assesses the extent of concordance between expected and actual values. Elevated  $R^2$  values indicate superior model fit. In this analysis, the RF model attained significant results:  $V_{OC} = 0.91$ ,  $PCE = 0.88$ ,  $J_{SC} = 0.89$ , and  $FF = 0.85$ , all indicating robust predictive concordance.

**Root mean square error (RMSE):** calculated the size of squared prediction errors, assigning higher significance to larger discrepancies and emphasizing cases of model underperformance.

**Mean absolute error (MAE):** quantifies the average absolute deviation between predictions and actual values, providing a clear indication of overall accuracy.

The results collectively demonstrated a prediction accuracy of 88.25%, affirming the efficacy of the RF algorithm in correlating material properties with PV performance outcomes. The incorporation of feature selection optimized the model by diminishing dimensionality, therefore enhancing computational efficiency while maintaining accuracy. Fig. 18(a)–(d) illustrates that the dense aggregation of data points along the optimal fit line visually substantiates the model's reliability. These findings highlight the RF model's capacity to provide dependable predictions while facilitating a more profound comprehension of the complex interdependencies that influence PV device performance. Fig. 19(a) displays regression graphs



**Fig. 18** Assessment of model prediction accuracy through comparison of ML-predicted and simulation-derived parameters for  $\text{Au/Rb}_2\text{SnBr}_6/\text{ZnSe}/\text{FTO/Al}$  solar cells: (a) PCE, (b)  $V_{OC}$ , (c)  $J_{SC}$ , and (d) FF.



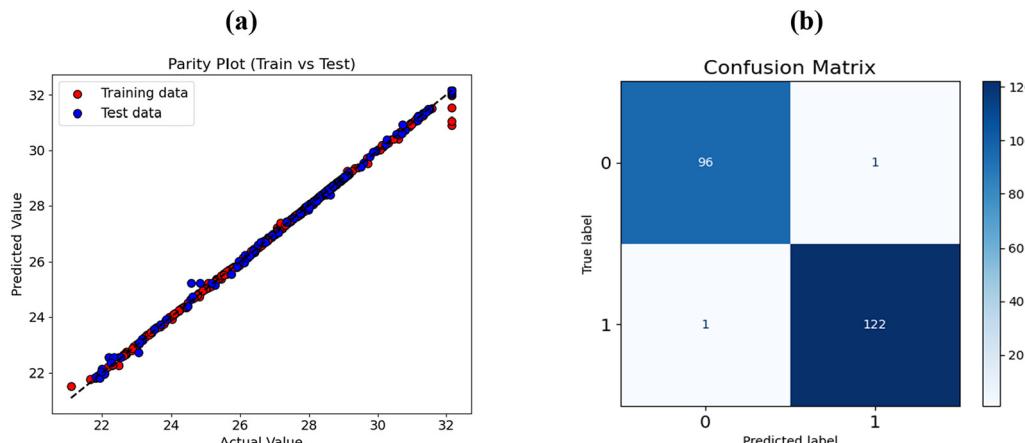


Fig. 19 Performance evaluation of the proposed solar cell structure illustrated through (a) the parity plot and (b) the confusion matrix.

juxtaposing projected values with actual data, providing compelling proof of the model's robust generalization capability. The strong correlation between predicted and observed values in both training and testing datasets indicates that the RF model attains an accurate fit while preventing overfitting, thereby maintaining high performance on unseen samples.<sup>75</sup> In accordance with statistical principles, as the  $R^2$  nears 1, the reliability and validity of the model's predictions increase.

In addition to regression performance, the model's classification abilities were evaluated using the confusion matrix depicted in Fig. 19(b). Of 220 data points, the RF model accurately identified 96 instances as class 0 and 122 as class 1, with only one mistake in each group. This exceptional outcome achieved an overall accuracy of 99.09%, further corroborated by robust precision and recall metrics. Collectively, these results underscore the RF algorithm's exceptional reliability and versatility. It not only reduces prediction errors but also exhibits remarkable efficacy in class distinction, positioning it as a robust instrument for both regression and classification tasks in solar system analysis. Although the methodology outlined in this paper exhibits considerable prediction accuracy, there is significant potential for enhancement. Future research may concentrate on amalgamating larger and more heterogeneous datasets, enhancing model generalizability across various device architectures and operational situations. Moreover, integrating ML with experimental validation could produce hybrid methodologies that connect computational predictions with practical applications.

This paper establishes a robust basis for integrating ML into solar cell research and design. By facilitating more efficient, stable, and economically viable PV solutions, ML serves as a revolutionary instrument for the forthcoming generation of sustainable energy technology.

## 5. Conclusion

This study demonstrates the potential of  $\text{Rb}_2\text{SnBr}_6$  as a lead-free, stable, and high-performance absorber material for perovskite solar cells. Among the three simulated device structures

with different electron transport layers (ETLs), device I ( $\text{Au}/\text{Rb}_2\text{SnBr}_6/\text{ZnSe}/\text{FTO}/\text{Al}$ ) exhibited the highest performance, achieving a PCE of 28.73%,  $V_{\text{OC}}$  of 0.8682 V,  $J_{\text{SC}}$  of  $38.094 \text{ mA cm}^{-2}$ , and FF of 86.86%. Device II ( $\text{In}_2\text{S}_3$ ) and device III ( $\text{CdZnSe}$ ) showed lower efficiencies of 26.62% and 24.04%, respectively, highlighting the critical role of ETL selection in enhancing charge transport and minimizing recombination losses. In addition to SCAPS-based simulations, a random forest model with SHAP analysis was applied to quantify the relative impact of device parameters. The analysis identified layer thickness, defect density, and doping concentration as the most influential factors affecting PCE, providing interpretable design insights that extend beyond conventional simulation optimization. It should be noted that the reported PCE of 28.73% represents a theoretical upper limit under idealized SCAPS simulation conditions. When assessing the performance metrics of these cells with ML, the model's accuracy was 88.25%. In practical devices, interface defects, material non-uniformity, and environmental degradation are likely to reduce efficiency. Therefore, these results should be interpreted as guidance for optimized device design rather than guaranteed experimental performance. Overall, this work delivers a dual contribution: an optimized  $\text{Rb}_2\text{SnBr}_6$ -based device structure (device I) and a predictive, interpretable machine learning framework to guide future experimental design, highlighting pathways toward high-efficiency, scalable, and sustainable perovskite photovoltaics. Future studies should focus on experimental validation, interface engineering, and operational stability to translate these findings into practical devices.

## Ethical approval

All the authors declare that the manuscript does not have studies on human subjects, human data or tissue, or animals.

## Author contributions

Md. Selim Reza and Avijit Ghosh: conceptualization, methodology, software, validation, formal analysis, visualization,



investigation, data curation, supervision, writing – original draft, and review and editing; Asadul Islam Shimul, Manjuara Akter, Saeed Hasan Nabil, Ajaz Rasool Chaudhry, Dipongkar Ray Sobuj, Yedluri Anil Kumar, Shaikat Biswas, Khorshed Alam, and Maida Maqsood: software, validation, formal analysis, writing – original draft, and review and editing.

## Conflicts of interest

The authors have no conflicts of interest.

## Abbreviations

$Rb_2SnBr_6$	Rubidium tin hexabromide
PCE	Power conversion efficiency
FF	Fill factor
PV cell	Photo-voltaic cell
$J_{SC}$	Short circuit voltage
VBO	Valence band offset
SC	Solar cell
HPSCs	Hybrid perovskite solar cells
ETL	Electron transport layer
Pb	Lead
PSCs	Perovskite solar cells
$V_{OC}$	Open circuit voltage
HTL	Hole transport layer
CBO	Conduction band offset
QE	Quantum efficiency
DOS	Density of states

## Data availability

Data will be made available upon reasonable request.

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