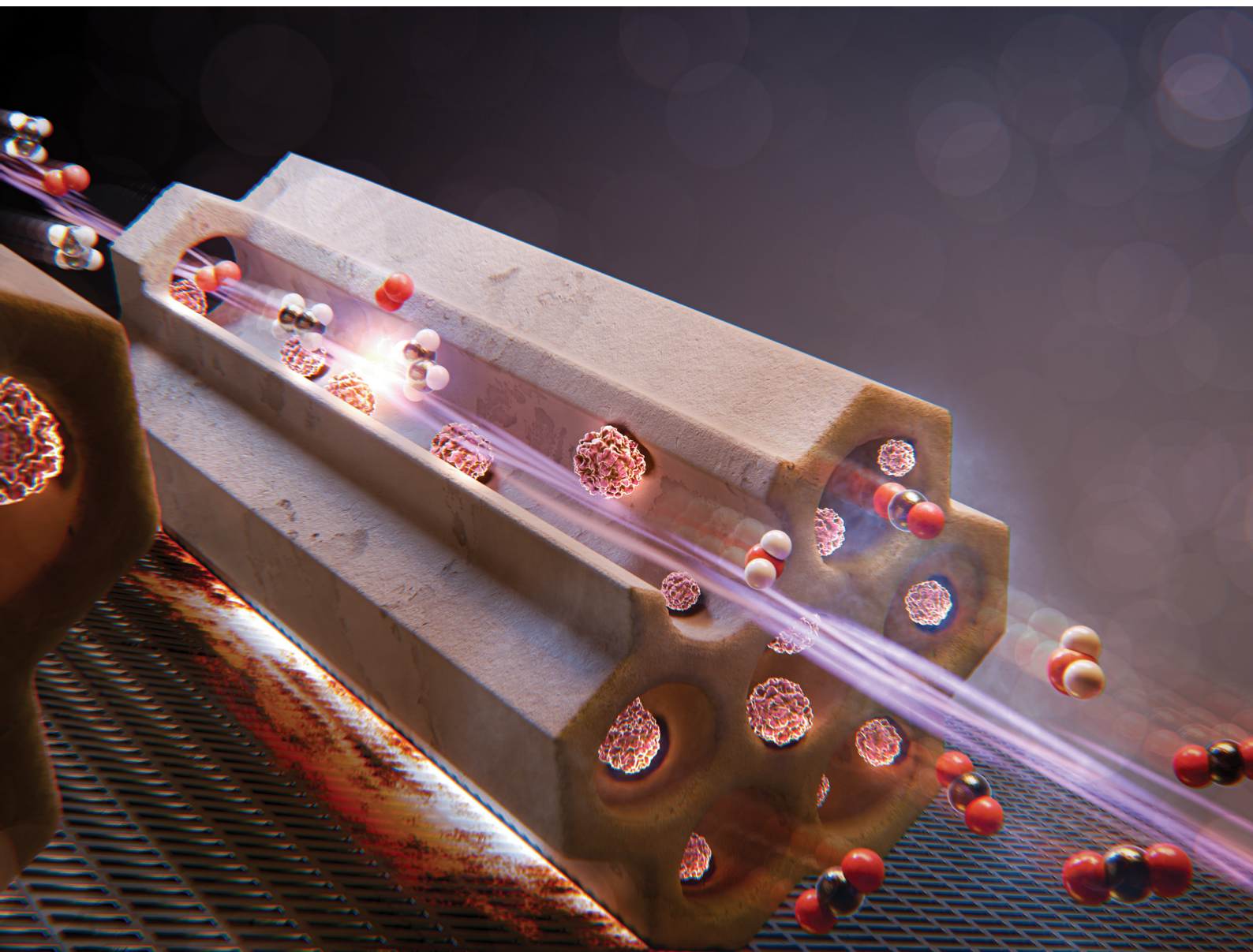


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**PAPER**

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# Nano-confined manganese oxide on SBA-15 for ethylene catalytic oxidation†

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This study investigates the synthesis and catalytic performance of nano-confined manganese oxide (MnO<sub>x</sub>) on SBA-15 for ethylene oxidation. A “med-synthesis” approach, involving dry impregnation of manganese nitrate on as-synthesized SBA-15 *via* grinding, was employed to achieve high MnO<sub>x</sub> loading and controlled dispersion within the mesoporous channels. The resulting catalysts (xMn/SBA-15<sub>d</sub>) were characterized by XRD, SAXS, TEM, TGA, and XPS to understand the impact of MnO<sub>x</sub> content on structural properties and catalytic activity. The results demonstrate that the dry impregnation method leads to well-dispersed MnO<sub>x</sub> nanoparticles within the SBA-15 framework, even at high loadings (up to 30 wt%). In contrast, wet impregnation resulted in larger MnO<sub>x</sub> particles and a loss of the ordered mesoporous structure. The nano-confined MnO<sub>x</sub> particles exhibited excellent thermal stability, resisting sintering even after prolonged exposure to high temperatures (550 °C) under reaction conditions. Catalytic testing revealed that the 20 wt% Mn loaded on SBA-15 *via* the med-synthesis approach displayed superior activity for ethylene oxidation compared to the wet-impregnated counterpart, achieving complete conversion at lower temperatures. *In situ* TEM studies further confirmed the stability of the nano-confined MnO<sub>x</sub> particles, highlighting the potential of this med-synthesis approach for developing highly active and durable catalysts for volatile organic compound oxidation.

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## 1. Introduction

Volatile organic compounds (VOCs) are hazardous air pollutants emitted from both natural and anthropogenic sources. VOCs encompass various families of hydrocarbons, such as alkanes, alkenes, and aromatics.<sup>1,2</sup> Exposure to VOCs is a human health hazard because they are carcinogenic, teratogenic, toxic, and mutagenic.<sup>3</sup> Moreover, VOCs are also recognized as one of the primary drivers of photochemical smog, tropospheric ozone formation, and stratospheric ozone depletion.<sup>4</sup> Ethylene is one of the most studied VOCs in literature due to its harmful effects on humans and the environment. Numerous approaches have been explored and implemented to remove ethylene from industrial sources, including adsorption, incineration, and catalytic combustion.<sup>4,5</sup> This study selected ethylene as a model compound

to represent the diverse range of hydrocarbons present in vehicle exhaust gases. As noted by Impens *et al.*,<sup>6</sup> the four most prevalent hydrocarbons in vehicle exhaust are typically ethylene (constituting 25 mol% of the total hydrocarbons), acetylene and methane (each accounting for 20 mol%), and aromatic compounds such as toluene (15 mol%) and benzene (5 mol%). Prior research demonstrates that ethylene exhibits reaction behavior comparable to that of toluene and benzene.<sup>7,8</sup> The key elimination methods to reduce VOC emissions at low concentrations and temperatures is the implementation of catalytic oxidation, which allows for the combustion of those hazardous compounds at lower temperatures compared to those required in gas phase reactions. The design of the catalytic material is the key step in guaranteeing efficient VOC removal.<sup>1,2,9,10</sup> The catalytic active material can consist of two main classes: noble and non-noble metal-based catalysts. Non-noble metals are characterised by their good activity in VOC oxidation due to their high stability, poison resistance, wider availability and lower cost compared to noble metals.<sup>11,12</sup>

Transition metal oxides are widely studied in the literature for hydrocarbon oxidation.<sup>12</sup> Among these, manganese oxide-based catalysts are reported to be among the most efficient transition metal compounds for oxidation catalysis, and they are environmentally friendly as well.<sup>13</sup> However, the catalytic performance of MnO<sub>x</sub> nanoparticles as oxidation catalysts has not been fully recognized. In particular, little attention has

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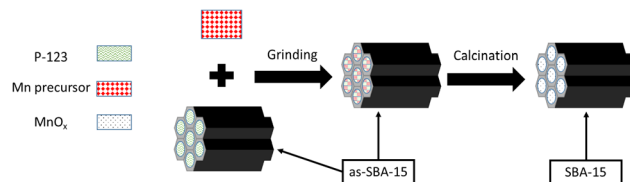
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been paid to the catalytic behaviour of  $\text{MnO}_x$  catalysts in oxidation/combustion reactions at low temperatures (e.g., below 300 °C), which are usually performed with noble metal catalysts.<sup>14–17</sup> Generally, the catalytic activities of transition metal oxide catalysts are lower than those of noble metal catalysts. However, the inherent advantages of metal oxide catalysts, such as low cost, high thermal stability, and high mechanical strength, make them a promising alternative in several catalytic applications.<sup>18,19</sup> Therefore, the controlled synthesis of  $\text{MnO}_x$  nanomaterials has attracted considerable attention from both academia and industry perspective.<sup>20–22</sup> Recently several reports on dry impregnation of metal precursors have achieved high dispersion with well-controlled particle size.<sup>23</sup> Generally, inorganic precursors are first introduced into the channels of host materials, such as mesoporous silica, and then metal precursors are calcined to produce metal nanoparticles with replicas of the confined space.<sup>24,25</sup> Several mesoporous materials like  $\text{CeO}_2$  and  $\text{ZrO}_2$  have been used; however, due to their low surface area, their performance remains less attractive.<sup>26,27</sup>

Since the first synthesis of SBA-15 by Zhao *et al.*<sup>28</sup> with a hexagonal pore network, the tuneable pore size has facilitated the accommodation of larger molecules, mitigating mass transfer limitations compared to other conventional metal oxides. Therefore, the inert nature and inherent hydrophobic properties of  $\text{SiO}_2$  make mesoporous SBA-15 a promising support material for the incorporation of various active compositions.<sup>29,30</sup> Extensive research efforts have gone into the modification of silica-based materials with active nanoparticles, with two main strategies for the synthesis of silica supported materials: the “one-pot” method (or pre-synthesis method) and the “loading” method (or post-synthesis method).<sup>31</sup> With the “one-pot” method, the silicon source and the active metal precursor are mixed, and they subsequently interact with the template to form a porous framework. This method is simple and results in an atomic-level mixture of active sites within the porous material. However, adding extra heteroatoms to the framework could disrupt the ordered mesoporous structure and cause further collapse during calcination.<sup>32–34</sup> The “loading” method mainly involves first preparing a stable mesoporous silica matrix and then adding the active component to it ref. 35–37. Several variations of this strategy have been reported in literature including impregnation,<sup>14</sup> deposition–precipitation,<sup>38</sup> graft hybrid,<sup>39</sup> colloidal immobilization,<sup>40</sup> and vacuum calcination.<sup>41</sup> A notable challenge with this method is the distribution of active species, such as nanoclusters of metals or metal oxides, within the elongated pore channels. This distribution may be susceptible to sintering effects during high-temperature calcination. Moreover, achieving high metal loading inside the channels of SBA-15 remains challenging.<sup>42</sup>

An intriguing alternative is the “med-synthesis” approach, positioned as an intermediate method between pre- and post-synthesis techniques. In this approach, denoted as med-synthesis, the template is retained within the pores. Med-synthesis holds the potential to amalgamate the advantages of both pre- and post-synthesis approaches. This includes achieving a well-distributed active phase and maintaining a defined structure, offering a



Scheme 1 Synthesis process for mesoporous silicate loaded with  $\text{MnO}_x$  via the med-synthesis approach.

promising compromise in the realm of porous material synthesis. In their earlier work, Zhu and Sun's group<sup>43,44</sup> reported the existence of extraordinarily confined spaces between the silica walls in the as-synthesized SBA-15 (as-SBA-15). By efficiently utilizing this space, a high degree of monolayer dispersion of active metal oxides with high loading can be achieved. The nanoconfinement of metals within SBA-15 pores *via* the “med-synthesis approach” is accomplished by dry impregnation of metal precursor over as-SBA-15 *via* grinding. This method employs pluronic P-123 in as-SBA-15 as a surfactant to assist in impregnation and agglomeration prevention<sup>24,31,45,46</sup>

The incorporation of high metal loading opens the door for the utilization of transition metal oxides as an economical alternative to noble metals such as Pt which is considered an optimal catalyst for hydrocarbon oxidation applications.<sup>42,47</sup>

In this study a manganese precursor was directly incorporated into as synthesized SBA-15 by employing the med-synthesis approach using solid state grinding of the precursor (Scheme 1). The subsequent calcination in air was conducted to obtain the resultant material which where denoted as ( $x\text{Mn}/\text{SBA-15}_d$ ). Manganese nitrate was used in the preparation of the supported systems due to the ease of removing nitrates anions during the calcination. The best performing catalyst prepared *via* dry impregnation was benchmarked against manganese oxide catalysts synthesized by the wet impregnation method. The controlled crystal growth has gained significant attention for several oxidation reactions, specifically low temperature CO and hydrocarbon oxidation,<sup>48–50</sup> and in this context, this work investigates synthesis of  $\text{MnO}_x$  on SBA-15 support by controlled dispersion. This study also aims to enhance the understanding of the catalyst structure, dispersity, and catalytic properties of  $\text{MnO}_x$  nanoparticles for ethylene oxidation, which is crucial for mitigating the impact of unburned hydrocarbons on global warming.

## 2. Experiment

### 2.1 Materials

Manganese(II) nitrate hydrate ( $\text{Mn}(\text{NO}_3)_2 \cdot x\text{H}_2\text{O}$ ), tetraethyl orthosilicate (TEOS, 98%), hydrochloric acid (HCl, 37%), and Pluronic P-123 ( $\text{EO}_{20}\text{PO}_{70}\text{EO}_{20}$ ,  $M_n = \sim 5800$ ) were purchased from Sigma-Aldrich.

### 2.2 Catalyst synthesis

**2.2.1 Synthesis of SBA-15.** The well-known synthesis procedure was adopted from the literature.<sup>15,51</sup> Briefly, 4.0 g of P-123 were dispersed overnight in 110 ml of DI water. 20 ml of



HCl are then added over the P-123 solution and left to stir for 20 min. The solution temperature is elevated to 36 °C and then 8 g of TEOS are added dropwise and the mixture is kept stirring for 4 hour. The formed suspension is hydrothermally treated at 130 °C for 16 hour. The precipitated material is collected and dried at 80 °C overnight. The dried precipitate is denoted as as-SBA-15.

**2.2.2 Dry impregnation to synthesize xMn/SBA-15 catalyst.** Manganese(II) nitrate is dry impregnated over as-SBA-15 by grinding both solids well for 30 min as demonstrated in Scheme 1. The manganese precursor weight is adjusted to produce the following weight percentages respectively: 10, 15, 20, 25, and 30 wt%. The solid mixture is then calcined at 550 °C for 6 hour at 1 °C min<sup>-1</sup> and left to cool naturally. The produced catalysts are denoted as 10Mn/SBA-15<sub>d</sub>, 15Mn/SBA-15<sub>d</sub>, 20Mn/SBA-15<sub>d</sub>, 25Mn/SBA-15<sub>d</sub>, and 30Mn/SBA-15<sub>d</sub> respectively.

**2.2.3 Wet impregnation to synthesize 20Mn/SBA-15 catalyst.** For the preparation of the wet impregnated catalyst, Mn(NO<sub>3</sub>)<sub>2</sub>·xH<sub>2</sub>O is dissolved in 100 ml of DI water. The precursor corresponding to 20 wt% is mixed well, and SBA-15 support recovered after calcination is added for impregnation. The rotary evaporator was used to desiccate the sample and dry it in vacuum. After the solvent is completely dried, the sample was dried for 12 hour at 80 °C and calcined at 550 °C for 6 hour. Temperature was ramped from room temperature to 550 °C with 1 °C min<sup>-1</sup>. The sample is denoted as 20Mn/SBA-15<sub>w</sub>.

### 2.3 Characterization

Crystal structure of the catalyst was characterized by powder X-ray diffraction (XRD) on a Bruker D8 Advance using Cu k<sub>α</sub> radiation source with a wavelength of 1.5418 Å at 40 kV and 40 mA in the range of 10–90°. The same instrument was used for small-angle X-ray scattering (SAXS).

Analyzer 5500 (TA Instruments, US) was used to analyze thermogravimetric (TGA) properties of the samples. Measurements were conducted under an air atmosphere with a flow rate of 20 ml min<sup>-1</sup>. The samples used had an approximate mass of 4.0 mg.

Textural properties of the catalyst were evaluated by N<sub>2</sub> physisorption in Micromeritics ASAP-2020 equipment. Catalysts (300 mg) were first degassed for 5 h at 150 °C. Specific surface area was calculated in the relative pressure range of 0.01–0.2, assuming the N<sub>2</sub> molecule has a cross-sectional size of 0.162 nm<sup>2</sup>.

Catalyst morphology was probed using a TEM Titan Themis microscope. To record the *in situ* evolution of MnO<sub>x</sub> particles with temperature, K3 direct detection camera was used. Surface compositions and chemical states were analyzed by X-ray photoelectron spectroscopy on a XPS Amicus. High-resolution X-ray photoelectron spectroscopy (HrXPS) using a Kratos Axis Ultra photoelectron spectrometer (Kratos Analytical Ltd) was employed to analyze the chemical bonding states of the FAC anodes. Prior to analysis, the samples underwent Ar<sup>+</sup> ion beam etching for a duration of 30 minutes. The HrXPS measurements were conducted using a Kratos Axis Ultra DLD spectrometer with a monochromatic Al K X-ray source, operating at 150 W

and an energy of  $h\nu = 1486.6$  eV. The spectrometer was equipped with a multichannel plate, delay line detector, and maintained a vacuum level of  $1 \times 10^{-8}$  mbar. The entire survey spectra and high-resolution spectra were acquired at fixed analyzer pass energies of 160 and 20 eV, respectively. The binding energies were calibrated using the C 1s peak set at 284.8 eV. Analysis of the XPS spectra was performed using CasaXPS, a commercially available software. The fitting method described by Biesinger *et al.*<sup>52</sup> was employed for spectrum analysis, and a Shirley background was applied to the Mn 2p<sub>3/2</sub> region.

Mn loading in the prepared catalysts is quantified using a wavelength dispersive XRF spectrometer (Bruker S8 TIGER WD-XRF).

### 2.4 Catalytic testing

Catalytic testing was performed in a U-shaped reactor. For each test 30 mg of pelletized catalyst (45–60 mesh) were loaded into the reactor and sandwiched between two layers of glass wool. The reactor bed was heated by an electric oven and a k-type thermocouple touching the catalyst bed was used for temperature measurement. The inlet feed consists of 850 ppm ethylene, 15% oxygen, and balance nitrogen. The gas hourly space velocity is 64 000 ml g<sub>cat</sub><sup>-1</sup> h<sup>-1</sup>. Agilent gas chromatograph (7890 B) with FID and TCD detectors was used to monitor the reactant concentration. Ethylene conversion is defined as:

$$\text{Conversion\%} = \frac{X_{\text{Ethylene}}(\text{initial}) - X_{\text{Ethylene}}(\text{final})}{X_{\text{Ethylene}}(\text{initial})} \times 100\%$$

To evaluate the apparent rate constant, calculations were performed under the following assumptions:

- (1) The rate expression is assumed to be first order power law that is dependent on ethylene partial pressures, *i.e.*,  $r = kP_{\text{C}_2\text{H}_4}$ .
- (2) The occurring reaction is assumed to be complete combustion.
- (3) Atmospheric pressure, isobaric conditions, throughout the catalyst bed.
- (4) Isothermal conditions throughout the catalyst bed.
- (5) The change in total molar flow rate ( $F_{\text{total}}$ ) is negligible since the ethylene stream is diluted ( $\leq 1\%$  C<sub>2</sub>H<sub>4</sub> in all cases).
- (6) The absence of heat and mass transfer limitations and other parasitic phenomena.

To derive the expression of the rate constant, the change in the molar flow rate of ethylene with respect to catalyst loading is expressed as:

$$\frac{dF_{\text{C}_2\text{H}_4}}{dW} = -kP_{\text{C}_2\text{H}_4}$$

where  $F_{\text{C}_2\text{H}_4} = Q \cdot C_{\text{C}_2\text{H}_4}$ ,  $C_{\text{C}_2\text{H}_4} = \frac{P_{\text{C}_2\text{H}_4}}{RT}$ ,  $Q = Q^0 \frac{T}{273.15}$  (to account for flow expansion with temperature). Thus  $F_{\text{C}_2\text{H}_4} = Q \frac{P_{\text{C}_2\text{H}_4}}{R \cdot T}$  and  $\frac{dF_{\text{C}_2\text{H}_4}}{dW} = \frac{Q}{R \cdot T} \frac{dP_{\text{C}_2\text{H}_4}}{dW} = \frac{1}{R \cdot 273.15} \frac{dP_{\text{C}_2\text{H}_4}}{d\tau}$ , where  $R$  is the gas constant ( $R = 8.2 \times 10^{-5} \frac{\text{m}^3 \text{ atm}}{\text{mol K}}$ )  $\tau$  is the catalyst



weight-to-volumetric flow rate ratio  $\tau = \frac{W}{Q^0} [\text{g s m}^{-3}]$ . The change in molar flow rates of ethylene with respect to conversion ( $X$ ) is expressed as  $F_{\text{C}_2\text{H}_4} = F_{\text{C}_2\text{H}_4}^0 (1 - X)$ . The partial pressure is calculated as  $P_i = \frac{F_i}{F_{\text{total}}} \cdot P^0 = y_i \cdot P^0$ . Thus, the rate constant is calculated by fitting a kinetic integral model over the bed loading *via* the following expression:

$$k = \frac{1}{R \cdot 273 \cdot \tau} \ln\left(\frac{1}{1 - X}\right)$$

To investigate water resistance of the optimum dry impregnated catalyst and its wet-impregnated counterpart, tests were conducted under wet feed conditions. The inlet feed for these tests consisted of 850 ppm ethylene, 15% oxygen, 5% water vapours, and balance nitrogen. The gas hourly space velocity was maintained at  $64\,000 \text{ ml g}_{\text{cat}}^{-1} \text{ h}^{-1}$ .

To investigate the thermal stability, the catalyst was exposed to elevated temperatures for 6 hours under reaction flow conditions. After keeping the catalyst under isothermal conditions for 6 hours, it was cooled down to  $125^\circ\text{C}$  and the catalytic testing was performed by incrementing the temperature gradually until complete conversion was attained. Two tests were performed in the case of 20Mn/SBA-15<sub>d</sub> samples, where their catalytic performance was evaluated after their exposure to reaction flow conditions at  $550^\circ\text{C}$  and  $625^\circ\text{C}$ . For the case of 20Mn/SBA-15<sub>w</sub>, it was exposed to  $550^\circ\text{C}$ . Moreover, time-on-stream stability test for 100 hours was performed for the best performing catalyst (20Mn/SBA-15<sub>d</sub>) at  $225^\circ\text{C}$ .

### 3. Results and discussion

Fig. 1 shows the X-ray diffraction patterns of the SBA-15 support and metal-loaded catalysts with different loading concentrations. The wider peak appearing at  $22.6^\circ$  corresponds to amorphous  $\text{SiO}_2$ . The catalysts loaded up to 15 wt% did not show a well observed crystal structure of  $\text{MnO}_x$ , indicating that the metal oxide is well dispersed. As shown in Fig. 1, the main crystalline structures of Mn in the 10–30 wt% Mn/SBA-15 samples after calcining were  $\text{Mn}_2\text{O}_3$  (89-4836) and  $\text{MnO}_2$  (89-5171). This suggests that the amorphous  $\text{MnO}_x$  crystallize to  $\text{MnO}$ ,  $\text{MnO}_2$  and  $\text{Mn}_2\text{O}_3$  at  $550^\circ\text{C}$ . It is worth noting that the crystal size in the case of wet impregnated catalyst is greater. We hypothesize that in wet impregnation particles grow on the unprotected SBA-15 surface. Consequently, these particles begin to sinter when calcined at higher temperatures ( $550^\circ\text{C}$ ). However, in dry impregnation,  $\text{MnO}_x$  crystals are nanoconfined within SBA-15 pores.

The SAXS patterns displayed in Fig. 2 illustrate the distinctive features of the dry impregnated and pristine SBA-15 samples. The appearance of three diffraction peaks within the range of  $2\theta = 0.4^\circ\text{--}3^\circ$  provides evidence for the development of neatly arranged hexagonal pores. Specifically, these peaks correspond to the (100), (110), and (200) planes, which are indicative of the well-defined hexagonal ( $p6mm$ ) pores found in

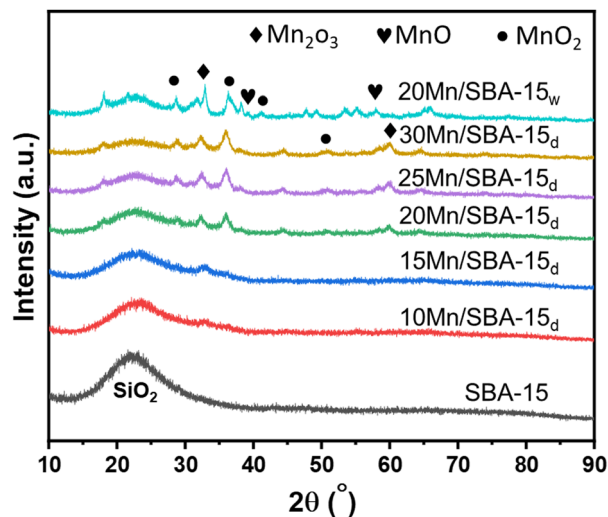


Fig. 1 X-ray diffraction patterns of all the  $\text{MnO}_x/\text{SBA-15}$  prepared catalysts.

SBA-15.<sup>53,54</sup> These distinctive features of ordered pores are absent in the case of the wet-impregnated sample.

Fig. 3 shows thermogravimetric analysis (TGA) curves of the polymers P-123 which is used as a template for SBA-15. In the TGA curve for P-123, weight loss started sharply at around  $50^\circ\text{C}$  and was complete at  $250^\circ\text{C}$ . The observed thermal decomposition of bare as-made SBA-15 shows a single weight loss of 47 wt% at about  $120^\circ\text{C}$ , which is associated with the decomposition of the triblock copolymer P-123 slightly embedded in the siliceous pore walls. We identified  $221^\circ\text{C}$  as a critical temperature point, attributed to the onset of manganese nitrate decomposition. Weight losses observed below  $221^\circ\text{C}$  are assigned to the release of surface and structural water, while at temperatures above  $221^\circ\text{C}$  the decomposition of nitrate resulted in the release of  $\text{NO}_x$  gas and a further substantial

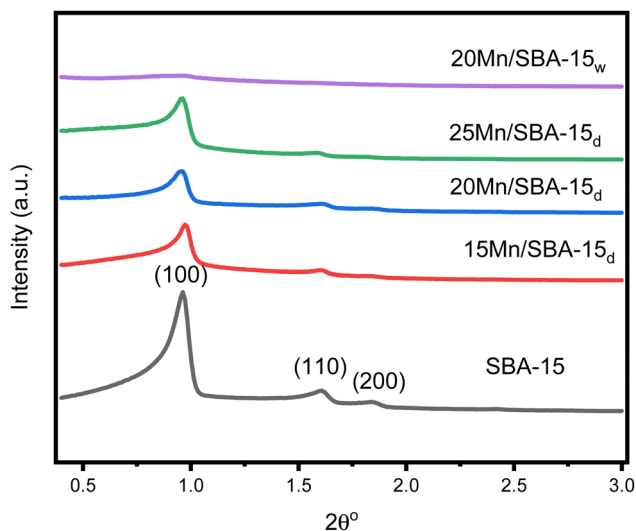


Fig. 2 SAXS patterns depicting the structural features of pristine SBA-15 and Mn-loaded SBA-15 samples at various manganese loading levels.



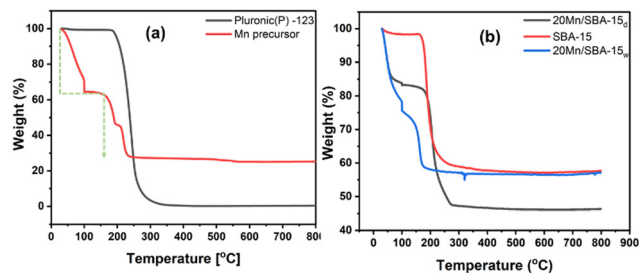


Fig. 3 TGA curves of (a) P-123 template and  $\text{Mn}(\text{NO}_3)_2 \cdot x\text{H}_2\text{O}$  and (b) TEOS condensed on P-123, and 20 wt% Mn loaded on SBA-15 at a heating rate of  $10\text{ }^\circ\text{C min}^{-1}$ .

weight loss of 35 wt%. Sample 20Mn/SBA-15<sub>w</sub> calcined in air shows a substantial decrease in weight below  $200\text{ }^\circ\text{C}$  due to lower onset temperatures for the release of water and manganese nitrate decomposition compared to bare manganese nitrate.

$\text{N}_2$  adsorption and desorption isotherms were measured on all samples to evaluate the surface and structural properties. The  $\text{N}_2$  adsorption curves are presented in Fig. 4, and the data are summarized in Table 1.

Both pure SBA-15 and  $x\text{Mn}/\text{SBA-15}_d$  samples exhibited adsorption isotherms of type IV with hysteresis loops, which are characteristic of nanostructured materials with uniform mesopores. The adsorption and desorption isotherms showed a large increase in the relative pressure ( $P/P_0$ ) ranging from 0.6 to 0.8 for SBA-15 and from 0.5 to 0.7 for  $\text{MnO}_x$  on SBA-15, which is caused by capillary condensation into the mesopores.  $\text{N}_2$  adsorption data presented in Fig. 4(a).

Table 1 show that the pore diameter and surface area comparison of the prepared catalysts. The specific surface area of SBA-15 was found to be  $518\text{ m}^2\text{ g}^{-1}$ . The surface of catalyst

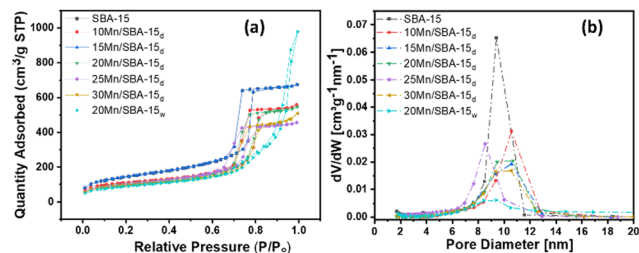


Fig. 4 (a)  $\text{N}_2$  adsorption-desorption isotherm (b) BJH pore size distribution of prepared catalysts.

Table 1 BET surface area and pore size calculated from BJH pore size distribution

Catalyst	Surface area [ $\text{m}^2\text{ g}^{-1}$ ]	Pore size [nm]
SBA-15	518	8.5
10Mn/SBA-15 <sub>d</sub>	397	10.2
15Mn/SBA-15 <sub>d</sub>	358	9.8
20Mn/SBA-15 <sub>d</sub>	361	9.7
25Mn/SBA-15 <sub>d</sub>	354	9.9
30Mn/SBA-15 <sub>d</sub>	340	10.3
20Mn/SBA-15 <sub>w</sub>	320	20.4

( $x\text{Mn}/\text{SBA-15}_d$ ) after calcination decreased up to  $340\text{ m}^2\text{ g}^{-1}$  for 30Mn/SBA-15<sub>d</sub> which is the highest loading in dry impregnation method. The highest decrease in area is noted for catalyst prepared by wet impregnation, indicating that the pores were progressively blocked by  $\text{MnO}_x$  nanoparticles. In contrary to dry impregnated samples wet impregnated one exhibited adsorption isotherms of type type III, which indicates the loss of ordered mesoporosity, which is in accordance with SAXS results the BJH pore size distribution (Fig. 4b) reveals a monomodal distribution for both SBA-15 and the dry-impregnated catalyst. In contrast, the wet-impregnated sample exhibits a bimodal distribution, indicating the presence of pores both on the surface and within the silica support.<sup>55</sup>

TEM observation results and EDS mapping of  $x\text{Mn}/\text{SBA-15}$  under vacuum conditions are shown in Fig. 5. It is remarkable that  $\text{MnO}_x$  up to 20% did not grow significantly in size due to the nanoconfinement inside the porous walls of SBA-15. In the wet impregnation method, the particles are mostly on the surface and are not strongly encapsulated by thick walls. EDX mapping analysis was used to test the elemental dispersion of  $x\text{Mn}/\text{SBA-15}_d$  composites (see Fig. 5). The mapping images of 15–25Mn/SBA-15<sub>d</sub> demonstrated that Mn element was uniformly distributed on  $\text{SiO}_2$  after calcination. The  $x\text{Mn}/\text{SBA-15}_d$  composites have a stable structure under  $550\text{ }^\circ\text{C}$ . The effect was attributed to the interaction between SBA-15 and  $\text{MnO}_x$  as well as the channel limiting effect.

The comparison for the manganese oxide particle size distribution of dry impregnated 20Mn/SBA-15<sub>d</sub> and wet impregnated catalyst 20Mn/SBA-15<sub>w</sub> is given in Fig. 6 with average particle size of 7.3 nm and 48 nm, respectively. The growth of particle in wet impregnation implies that the particles are already sintered when calcined at high temperature ( $550\text{ }^\circ\text{C}$ ) for the activation of the catalyst. In case of dry impregnation, the particles are not sintered, rather they remained intact.

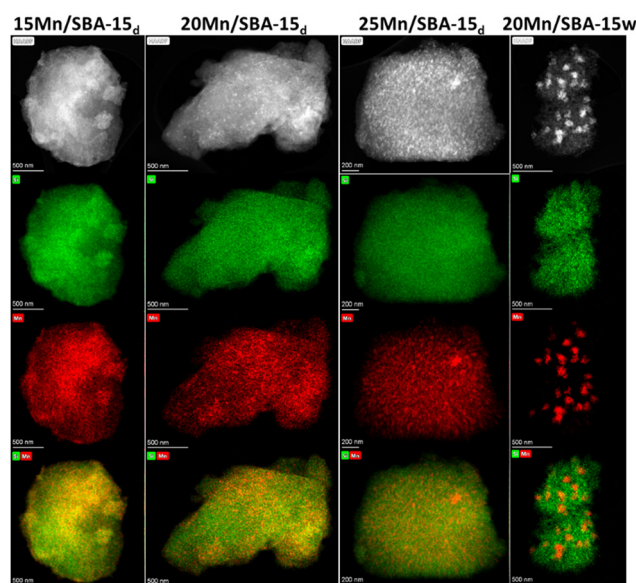


Fig. 5 TEM and EDX color mapping of catalysts prepared with dry and wet impregnation methods.



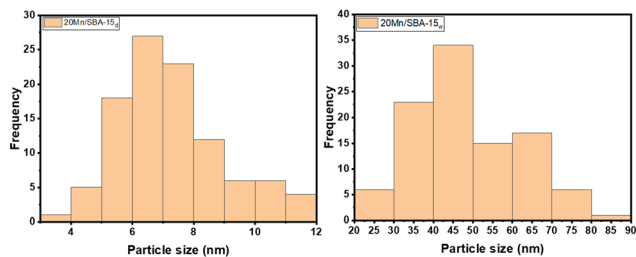


Fig. 6 Average particle size distribution calculated for 20Mn/SBA-15<sub>d</sub> and 20Mn/SBA-15<sub>w</sub>.

To investigate sample stability under reaction conditions, TEM results for spent catalysts are reported in Fig. 7. The spent catalyst 20Mn/SBA-15<sub>d</sub> in Run-1 shows a slight increase in particle size after 6 hours at 550 °C as the average particle size is 10 nm. However, after exposure to reaction conditions in Run-2 at 625 °C for 6 hours, the average particle size of 20Mn/SBA-15<sub>d</sub> increased to 16.7 nm, which gives an indication on the thermal stability limit of this catalyst. In the case of wet impregnated sample, the average particle size increased after Run-1 from 48 nm to 54.1 nm. The average particle size distribution for the spent catalysts is reported in Fig. S1 (ESI<sup>†</sup>).

Since atomic movement is easily influenced by temperature and partial pressure of gas surrounding the sample, adjusting the reaction temperature can change atomic dispersion and modify catalyst surface defects, thereby affecting reactivity. We utilized *in situ* TEM to investigate the behavior of MnO<sub>x</sub> particles under controlled gas conditions and temperature variations. The dynamic evolution process of uncalcined 20Mn/SBA-15<sub>d</sub> catalyst under increasing temperature and switching oxygen/nitrogen conditions was monitored with TEM measurements. In Fig. 8, TEM measurements are taken at conditions closely resembling air conditions: 80% N<sub>2</sub> with 20% O<sub>2</sub> at a total flow rate of 1 ml min<sup>-1</sup>. Pressure was maintained at 1 atm, and temperature was ramped from 175 to 625 °C with a ramping rate of 1 °C min<sup>-1</sup> and intermediate temperature intervals of 350, 450, and 550 °C.

When the temperature was systematically increased from 175 to 625 °C, MnO<sub>x</sub> particles remained elusive until the temperature reached 625 °C. This observation indicates a temperature threshold for the appearance of MnO<sub>x</sub> particles in the given conditions (shown in the inset of Fig. 8). Further investigation involved continuous heating at 550 °C for 60 minutes, during which TEM images were captured. Surprisingly, despite the

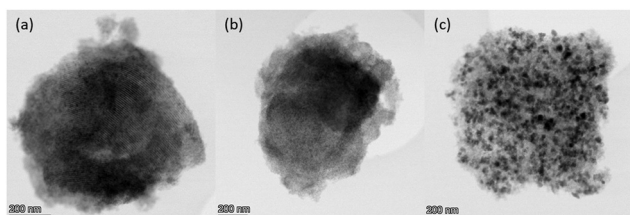


Fig. 7 TEM images of spent catalysts after thermal stability catalytic testing: (a) 20Mn/SBA-15<sub>d</sub> at 550 °C, (b) and 625 °C, (c) 20Mn/SBA-15<sub>w</sub> at 550 °C.

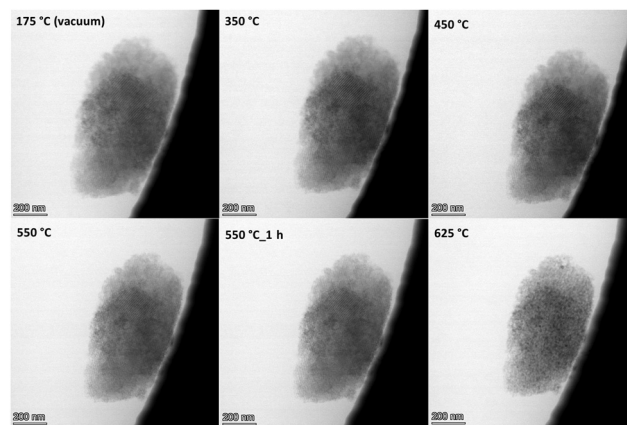


Fig. 8 Growth of MnO<sub>x</sub> nano particles in a TEM (200 kV). Temperature from the start of the irradiation is displayed on each image. Diffusion of MnO<sub>x</sub> on the surface is seen. Beam current density: 200 A cm<sup>-2</sup>. Each image represents an area of 9.2 × 9.2 nm<sup>2</sup>.

prolonged heating, there was no discernible evolution of particles from the MnO<sub>x</sub> material.

To validate and understand the particle growth phenomenon, we elevated the temperature to 625 °C. This additional temperature increment was chosen to confirm and observe any subsequent changes in MnO<sub>x</sub> particles.

In Fig. S2 (ESI<sup>†</sup>), we examined the particle growth under a specific temperature condition of 550 °C. To capture the potential evolution of MnO<sub>x</sub> crystals, we conducted a series of sequential imaging experiments at a slightly higher temperature, namely 625 °C. The imaging sessions were performed at specific intervals of 15 minutes, 45 minutes, 1 hour and 45 minutes, 2 hours and 45 minutes, and finally, 3 hours and 15 minutes. This approach aimed to assess whether MnO<sub>x</sub> crystals exhibit growth at 550 °C over an extended duration.

Across all TEM image frames obtained from sequential imaging sessions, a consistent observation emerges: there is no discernible evidence of particle growth at 550 °C even when subjected to prolonged durations. This absence of observable growth underlines the stability and resistance of MnO<sub>x</sub> crystals to significant changes in size or morphology under the specified temperature conditions.

Fig. S3 (ESI<sup>†</sup>) presents *in situ* validation of the growth and sintering behavior of MnO<sub>x</sub> particles. TEM images were captured at a temperature of 625 °C for varying durations (5, 30, and 60 minutes) to observe the sintering behavior of the particles. Upon analysis of both STEM and TEM images (top and bottom, respectively), MnO<sub>x</sub> nanoclusters are apparent on the SBA-15 surface. The particle size increased with time from 6 nm at 5 min to 14.5 nm at 60 min (see Fig. S4, ESI<sup>†</sup>). This result is consistent with the *ex situ* results of spent catalyst at 625 °C, where in both cases the average particle size increases with temperature. It is worth noting that due to the limited resolution of STEM imaging in *in situ* gas conditions, the clear identification of MnO<sub>x</sub> particles is very difficult. Moreover, due to the sample thickness and complex morphology, even small changes in focus/astigmatism can disrupt the image of small



Mn oxide particles or it may highlight some defects in the SBA-15 structure that could be mistakenly identified as highly contrasted Mn oxide particles.

The resistance to sintering, as evidenced by the images, provides valuable insights into the robust nature of MnO<sub>x</sub> particles within the SBA-15 framework. These observations contribute to our understanding of the thermal stability and behavior of MnO<sub>x</sub> particles under the specific conditions explored in this study.

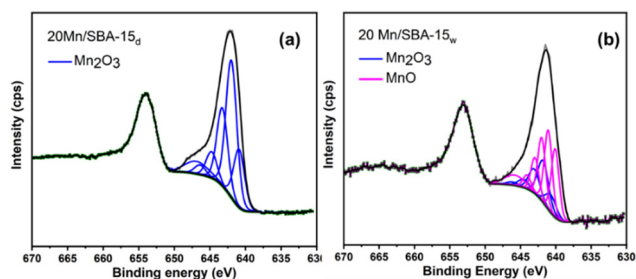
From Fig. 8 and Fig. S2 and S3 (ESI<sup>†</sup>) it is evident that there is diffusion of MnO<sub>x</sub> particles emerging on the surface and migrating from the edges to the center. This observation is consistent with the recorded video Video S1 (ESI<sup>†</sup>) showing Mn migration across the surface with temperature elevation from 350 to 650 °C. We postulate that the facilitated Mn migration is due to the presence of P-123 in accordance with its proposed role in enhancing metal dispersion.<sup>31,45,46</sup>

X-ray photoelectron spectroscopy (XPS) was conducted to elucidate the surface chemical state of manganese (Mn). The atomic concentration of elements on the surfaces of 20Mn/SBA-15<sub>d</sub> and 20Mn/SBA-15<sub>w</sub> samples obtained by XPS are given in Table 2.

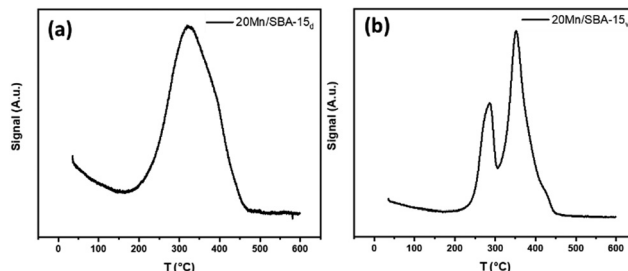
As shown in Fig. 9, high-resolution XPS spectra of Mn 2p core level was acquired for both samples. Subsequently, spectral deconvolution was employed to fit Mn 2p<sub>3/2</sub> spectrum, using a combination of the standard references, namely MnO<sub>2</sub>, Mn<sub>2</sub>O<sub>3</sub>, and MnO.<sup>52</sup> Notably, the results revealed the absence of MnO<sub>2</sub> in both samples. In the case of 20Mn/SBA-15<sub>d</sub> catalyst, the presence of manganese was determined to be primarily in the form of Mn<sup>3+</sup> oxides, whereas in the 20Mn/SBA-15<sub>w</sub> sample, manganese was found to exist in a combination of Mn<sup>3+</sup> and Mn<sup>2+</sup> oxidation states. The utilization of the wet impregnation method thus resulted in a significant reduction in the concentration of Mn<sub>2</sub>O<sub>3</sub> to 69%.

**Table 2** Atomic concentration of elements on the surfaces of 20Mn/SBA-15<sub>d</sub> and 20Mn/SBA-15<sub>w</sub> samples obtained by XPS

Catalyst (s)	C 1s	O 1s	Si 2p	Mn 2p
20Mn/SBA-15 <sub>w</sub>	10.67	57.37	30.82	1.14
20Mn/SBA-15 <sub>d</sub>	7.48	59.55	29.56	3.41



**Fig. 9** XPS spectra of Mn 2p of (a) 20Mn/SBA-15<sub>d</sub> and (b) 20Mn/SBA-15<sub>w</sub> catalysts.



**Fig. 10** H<sub>2</sub>-TPR profile of 20Mn/SBA-15 catalyst prepared by (a) dry impregnation, and (b) wet impregnation.

To investigate bulk redox properties, H<sub>2</sub>-TPR profiles of 20Mn/SBA-15<sub>d</sub> and 20Mn/SBA-15<sub>w</sub> were recorded (see Fig. 10). The reduction process of MnO<sub>x</sub> into MnO by H<sub>2</sub> is reported over the temperature range of 200–550 °C.<sup>56,57</sup> This reduction pattern is observed in both cases of 20Mn/SBA-15<sub>d</sub> and 20Mn/SBA-15<sub>w</sub>. The 20Mn/SBA-15<sub>d</sub> H<sub>2</sub> evolution showed a broad peak centered at 336 °C, which can be assigned to the highly dispersed MnO<sub>x</sub> (as shown in XRD and TEM results).<sup>58</sup> The 20Mn/SBA-15<sub>w</sub> catalysts showed two consecutive reduction peaks at 285 °C and 352 °C and a narrow peak shoulder at 412 °C. Jacob *et al.*<sup>59</sup> discovered that Mn<sub>3</sub>O<sub>4</sub> is the main intermediate reduction product, the lower-temperature peak was ascribed to the reduction of MnO<sub>2</sub>/Mn<sub>2</sub>O<sub>3</sub> to Mn<sub>3</sub>O<sub>4</sub>, and the higher-temperature peak is attributed to the further reduction of Mn<sub>3</sub>O<sub>4</sub> to MnO. The two-stage reduction pattern in the case of wet impregnated sample indicates more heterogeneity in the manganese species compared to the dry method.

The bulk average oxidation state from H<sub>2</sub>-TPR is calculated based on the metal loading and hydrogen consumption assuming the reduction of all Mn species into MnO with Mn<sub>2</sub>O<sub>3</sub>.<sup>56,57,60</sup> Hydrogen consumption and average oxidation state for each sample are reported in Table 3. These findings align with our observations in the context of XPS measurements, suggesting coherence between surface and bulk properties of the MnO<sub>x</sub> in the synthesized samples. The higher oxidation state in the case of dry impregnated sample is attributed to the enhanced oxygen uptake by smaller nanocrystals, as the oxidation rate is proportional to the surface to volume ratio.<sup>61–63</sup>

Fig. 11 shows the conversion profiles of ethylene using SBA-15 with different manganese loadings. By increasing the metallic loading from 10 to 20 wt%, the light-off temperature is shifted to lower temperatures by ~100 °C. Catalyst activity decreases with further increase of metal content as observed with 25 and 30 wt% Mn/SBA-15 in dry impregnation. This trend

**Table 3** Mn average oxidation state of 20Mn/SBA-15<sub>d</sub> and 20Mn/SBA-15<sub>w</sub> samples obtained by XPS and H<sub>2</sub>-TPR

Catalyst (s)	Mn <sub>2</sub> O <sub>3</sub> (%)	MnO (%)	Average oxidation state XPS	H <sub>2</sub> consumption (mmol g <sup>-1</sup> )	Average oxidation state H <sub>2</sub> -TPR
20Mn/SBA-15 <sub>w</sub>	31	69	2.31	2.64	2.45
20Mn/SBA-15 <sub>d</sub>	98	2	2.98	3.53	2.94



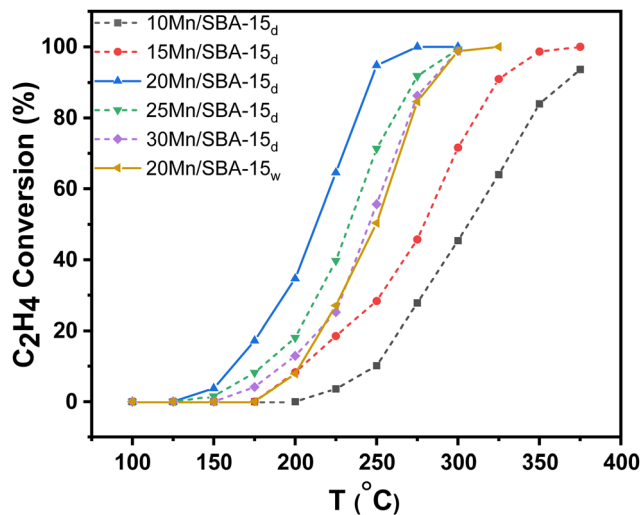


Fig. 11 Temperature screening of  $C_2H_4$  oxidation on supported  $MnO_x/SBA-15$  catalysts at a space velocity of  $64\,000\text{ ml g}_{\text{cat}}^{-1}\text{ h}^{-1}$ .

suggests the onset of metal agglomeration, resulting in a reduction in the number of available active sites. The normalized conversion per Mn loading is shown in Fig. S5 (ESI<sup>†</sup>). The observed trend of increased activity with particle size growth in the 5–10 nm range aligns with the enhanced catalytic performance typically seen in transition metal oxide-based catalysts during redox reactions. Beyond this particle size range, the reduction in surface-to-volume ratio becomes dominant, leading to a decline in activity.<sup>64,65</sup> In this study,  $MnO_x$  did not exhibit well defined crystalline peaks in XRD patterns for Mn loadings below 20%, and TEM images did not reveal any observable surface nano particles at these loadings. However, at 20% Mn loading,  $MnO_x$  nanoparticles within the postulated optimum size range (5–10 nm) were observed in XRD patterns corresponding to crystalline  $MnO_x$  phases. Turn over frequency (TOF) values as a function of temperature are reported in Fig. S6 (ESI<sup>†</sup>); the results confirm the observed activity trends in Fig. S5 (ESI<sup>†</sup>) below 250 °C. The  $T_{90}$  value of 20Mn/SBA-15<sub>d</sub> is 250 °C while that of 20Mn/SBA-15<sub>w</sub> is 300 °C. This difference in performance could be attributed to the enhanced dispersion in the case of dry impregnated catalyst along with the higher average oxidation state. Shaheen *et al.*<sup>66</sup> reported decrease in activity with increased crystallinity, which is in accordance with our observation where wet impregnated sample has more pronounced XRD peaks due to the agglomeration of  $MnO_x$  nanoparticles. Another factor that explains the enhanced catalytic

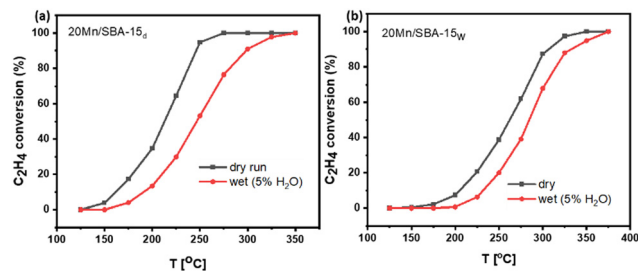


Fig. 12 Catalytic activity tests of  $MnO_x$  catalysts at GHSV of  $64\,000\text{ ml g}_{\text{cat}}^{-1}\text{ h}^{-1}$  in dry and wet conditions; (a) 20Mn/SBA-15<sub>d</sub> and (b) 20Mn/SBA-15<sub>w</sub>. Test conducted with 850 ppm ethylene, 15%  $O_2$ , 5%  $H_2O$  (wet conditions) and balance  $N_2$  at 250 °C.

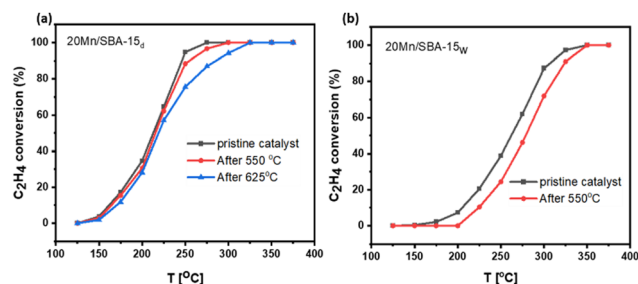


Fig. 13 Thermal stability evaluation of catalyst: (a) 20Mn/SBA-15<sub>d</sub> (b) 20Mn/SBA-15<sub>w</sub>.

performance of dry impregnated catalysts is related to the abundance of  $Mn_2O_3$  phases as quantified from XPS surface species.  $Mn_2O_3$  phase in  $MnO_x$  is considered to be a highly desirable phase in oxidation reactions.<sup>67,68</sup>

The best performing catalyst activity in this work exhibits superior catalytic activity to several manganese-based catalyst for ethylene catalytic combustion. The activity is compared with literature results in Table 4 on the basis of the apparent rate constant ( $k$  [ $\text{atm}^{-2}\text{ s}^{-1}\text{ g}^{-1}$ ]) at 150 °C.

To evaluate the performance of synthesized catalyst under wet conditions (which represent more realistic scenarios for VOC catalytic combustion),<sup>15,51</sup> conversion profiles are presented in Fig. 12. These profiles show that the catalytic activity of the dry impregnated catalyst surpasses that of its wet impregnated counterpart, with  $T_{90}$  values of 300 °C and 333 °C for dry and wet impregnated catalysts, respectively.

Thermal stability catalytic testing (Fig. 13) shows that the dry impregnated catalyst activity is maintained at 550 °C, while that

Table 4 Rate constant values at 150 °C for various Mn-based catalysts

Catalyst	Conditions	$k$ [ $\text{mol atm}^{-1}\text{ s}^{-1}\text{ g}^{-1}$ ]	Ref.
$Mn_2O_3$	500 ppm $C_2H_4$ , 10% $O_2$ , GHSV = $22\,000\text{ ml g}^{-1}\text{ h}^{-1}$	$1.4 \times 10^{-5}$	4 <sup>a</sup>
$Fe_3Mn_1Cu_1O_x$	165 ppm $C_2H_4$ , 10% $O_2$ , GHSV = $60\,000\text{ ml g}^{-1}\text{ h}^{-1}$	No conversion reported	69
$Mn_3O_4$	1000 ppm $C_2H_4$ , 10% $O_2$ , GHSV = $30\,000\text{ ml g}^{-1}\text{ h}^{-1}$	$1.13 \times 10^{-5}$	70
$MnCu_{7.5}Fe_{7.5}$	500 ppm $C_2H_4$ , 10% $O_2$ , GHSV = $20\,000\text{ ml g}^{-1}\text{ h}^{-1}$	$1.93 \times 10^{-5}$	71
$Mn_2O_3$ -SG550	500 ppm $C_2H_4$ , 10% $O_2$ , GHSV = $22\,730\text{ ml g}^{-1}\text{ h}^{-1}$	$2.2 \times 10^{-5}$	72
$Ce_{55}Mn_{45}SiC$	500 ppm $C_2H_4$ , 10% $O_2$ , GHSV = $15\,400\text{ ml g}^{-1}\text{ h}^{-1}$	$9.8 \times 10^{-6}$	3
20Mn/SBA-15 <sub>d</sub>	850 ppm $C_2H_4$ , 15% $O_2$ , GHSV = $64\,000\text{ ml g}^{-1}\text{ h}^{-1}$	$3.04 \times 10^{-5}$	This work

<sup>a</sup> Conversion values were reported at 160 °C instead of 150 °C.



of wet impregnated catalyst drops after the exposure to the same condition. This shows the higher thermal stability of dry impregnated sample. However, at 625 °C the activity of the dry impregnated sample drops significantly. These results are in accordance with the TEM findings where the catalyst deactivation is correlated to particle growth. The dry impregnated catalyst exhibited a stable catalytic performance at 225 °C, as shown in Fig. S7 (ESI<sup>†</sup>). These results are consistent with the recyclability assessments, where the light-on run showed no significant difference compared to the light-off conversion profiles, as shown in Fig. S8 (ESI<sup>†</sup>).

## 4. Conclusions

This study investigated the utilization of nanoconfinement effects facilitated by as-synthesized SBA-15 to disperse MnO<sub>x</sub> nanoparticles within its channels. The controlled synthesis resulted in highly dispersed MnO<sub>x</sub> nanoparticles with a size of ~7.3 nm and a loading content of up to 30 wt%. With the med-synthesis approach, nanoconfinement in dry impregnation allowed particles to disperse on the inner surface of SBA-15, while maintaining an undecorated surface of SBA-15 surrounding each nanoparticle. MnO<sub>x</sub> nanoparticles served as active sites for the oxidation of ethylene.

The choice between dry and wet impregnation methods for preparing Mn/SBA-15 catalyst significantly influences its catalytic performance and thermal stability in ethylene combustion. The observed variations in ethylene conversion rates and temperature dependencies highlight the importance of the preparation method in tailoring catalyst properties for specific applications. In comparison to MnO<sub>x</sub> deposited through conventional wet impregnation, the nanoconfined catalyst exhibited superior performance. *In situ* TEM studies provided insights into the growth behavior of the nanoparticles, highlighting their stability and uniform distribution within the SBA-15 channels. Furthermore, our investigation revealed significant advantages of the nanoconfinement approach in terms of catalytic activity. Specifically, the oxidation of C<sub>2</sub>H<sub>4</sub> exhibited a lower *T*<sub>90</sub> temperature (250 °C) with the nanoconfinement catalyst compared to the catalyst synthesized using wet impregnation (*T*<sub>90</sub> = 300 °C). The temperature investigation, along with EDX color mapping, provided valuable information on the dispersion and growth behavior of MnO<sub>x</sub> nanoparticles at elevated temperatures. These findings demonstrate the potential of the nanoconfinement approach using SBA-15 for the development of efficient catalytic systems based on MnO<sub>x</sub> nanoparticles.

Our study highlights the successful synthesis and characterization of nanoconfined MnO<sub>x</sub> nanoparticles within SBA-15. The results emphasize the advantages of the nanoconfinement approach in terms of particle size control, dispersion, and catalytic performance. Further research and optimization of the nanoconfinement strategy could unlock new opportunities for the design and development of advanced catalysts for various applications.

## Author contributions

Mohamad Abou-Daher: conceptualization, formal analysis, investigation, data curation, writing – original draft. Hassnain Abbas Khan: methodology, investigation, data curation, writing – original draft. Georgian Melinte: characterization and post reaction processing. Sarah Komaty: formal analysis, investigation, data curation.: formal analysis. Javier Ruiz-Martinez: supervision, writing – review & editing. Aamir Farooq: supervision, writing – review & editing, funding.

## Data availability

The data supporting this article have been included as part of the ESI.<sup>†</sup>

## Conflicts of interest

The authors declare no conflicts of interest.

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