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Unlocking the full potential of solar cell materials: parameter sensitivity analysis and optimization using response surface modelling†

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This study introduces a novel approach for predicting solar cell efficiency and conducting sensitivity analysis of key parameters and their interactions, leveraging response surface modeling to optimize interacting solar cell structure parameters for the best performance. Integrating response surface modeling with solar cell simulation software enhances the efficiency prediction process that enables the solar cell capacitance simulator (SCAPS)-1D software to unlock the true potential of a material. Through the utilization of central composite design (CCD) and response surface modeling (RSM), this research minimizes material waste during synthesis, saves time, and conserves energy. The methodology involves selecting five input parameters within specific ranges, modeling them using the least square method to create a polynomial regression model, and validating the model through efficiency predictions compared to SCAPS-1D simulations. The parameter sensitivity analysis is validated using analysis of variance (ANOVA) test results, demonstrating the precision of the RSM in predicting solar cell efficiency with a maximum error of 1.93%.

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Introduction

Simulation is a powerful tool to predict the actual potential of a device under ideal conditions. There are so many solar cell simulation Software packages, including SCAPS-1D,^{1,2} Silvaco,³ Sentaurus,⁴ *etc.*, to predict the solar cell performance of a device. Generally, it is very hard to predict the best performance with multiple optimized parameters/variables in solar cell simulation software like SCAPS-1D.^{5,6} Mamta *et al.*² simulated Sb₂Se₃ and Sb₂S₃ solar cell devices and chose the optimized set of parameters like the thickness of absorber layers (1 μm for both), 10¹² and 10¹⁶ cm⁻³ of valence band density of states in Sb₂S₃ and Sb₂Se₃, respectively, and so on (at which efficiency was maximum). Similarly, Bhowmik *et al.*⁷ selected the parameters near the maximum efficiency value. The general approach

is to select the optimal parameters at which the device showed the largest efficiency. Also, the steps taken in parameter changes lead to discrete parameters, and the step length depends on the author's choice. Generally, the authors of previous literature simulated the efficiency of solar cell structures using existing simulation software like Sentaurus, SCAPS-1D, *etc.* They chose the desired range of steps for varying individual parameters well in the practical range of the parameters. They collected the value of individual physical parameters at which the device had the largest efficiency. So, it was assumed that individual sole optimal physical parameters for the largest efficiency can be combined to obtain the maximum efficiency of the device if the physical parameters do not couple with one another or are independent of one another. However, these parameters were indeed interconnected and not independent of one another, therefore, their combination will not be able to produce the maximum efficiency of the device. By applying our proposed method, one can easily locate the maximum efficiency among the many coupled parameters within their range. So, after using the simulation software, one should apply our method (again validated by the ANOVA method) to unlock the device's real potential.

The novelty of our method lies in the fact that both the SCAPS-1D and RSM are applied to identify an optimal combination of interconnecting physical parameters of the SnSe-based solar device for producing maximum efficiency for the first time. Hence, the strategy of applying both simulation and modelling offers a precise target of achieving the optimal

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parameters at which the device offers maximum efficiency. The optimization process by using RSM provides the freedom to look into all possible values within the range of a given parameter offering a continuous parameter value search within the range.

There are many reports on the optimization of device fabrication conditions for the best solar cell performance using RSM.^{8–15} Suliman *et al.* used RSM with CCD to optimize the fabrication conditions of organic solar cells.¹² Mohammed *et al.*¹³ optimized the thickness of the active layer to reduce the series resistance of the tandem solar cell using CCD and RSM. Hunde *et al.*¹³ used the SCAPS-1D software along with the Box–Behnken designs (BBD) and RSM methods for the optimization of perovskite solar cells to achieve their best efficiency.

Besides, there are many applications of RSM in the fields of food science, chemometrics, and biochemistry, introduced by Box *et al.* in 1950.¹⁶ It is a technique based on fitting an experimental model from experimental data based on an experimental design.

The uniqueness of the proposed method is being able to fit a regression polynomial model of the solar cell material properties such as the band gap (eV), shallow uniform acceptor density (cm^{-3}), CBO (eV), work function of back contact (eV), and operating temperature (K) to predict the efficiency output from the solar cell material properties. It can be applied to identify the optimal solar cell material property parameter combination to predict the largest efficiency and unlock the full potential of solar cell materials. The proposed method can be used to determine the sensitivity of the input variables and their interactions according to the magnitude sequence of the coefficients of the variables in the regression polynomial model. The sensitivity analysis and RSM model can be validated by its ANOVA. In the proposed solar cell RSM simulation method using the SCAPS-1D software, input parameters are planned and arranged in CCD where the optimal parameter combination and maximum efficiency can be initially determined. However, CCD is not able to generate the regression polynomial parameter model, and RSM is then applied to generate the model for the prediction, conduct a parameter sensitivity study, and verify and refine the initial CCD optimal results.

These features of the proposed method combining RSM with CCD differentiate it from the others in the existing literature, providing an unusual potential for simulation prediction and material property parameter optimization for the best performance. Also, the study suggests the best parameters for the device where the SnSe-based single junction cell offers the maximum efficiency so far.

Methodology

The efficiency of a solar cell depends on many factors like the active layer, fabrication technique, *etc.* In this paper, optimization is carried out for maximum efficiency by taking into account parameters like band gap, shallow uniform acceptor

Table 1 Variation range of the input parameters/variables (called z_i) of the solar cell

Parameters (z_i)	Varied range of parameter (z_{\min} – z_{\max})
Band gap (eV)	1–1.5
Shallow uniform acceptor density (cm^{-3})	9×10^{15} – 4×10^{16}
CBO (eV)	–0.1 to 0.3
The work function of back contact (eV)	4.8–5.4
Operating temperature (K)	275–320

z_{\min} and z_{\max} denote the minimum and maximum range of the chosen parameter z_i for simulations.

density of states, conduction band offset (CBO), the work function of the back contact, and operating temperature. In contrast, other parameters like valence band density of states (VB DOS), conduction band density of states (CB DOS), radiative recombination coefficient (RRC), dielectric constant of the material, mobilities of electrons and holes, *etc.* are taken fixed as per reported values. The variation range of these parameters is shown in Table 1 below. First, the CCD matrix is formed based on the number of variable parameters. The CCD and RSM are applied to model the input parameters and the output efficiency obtained by the SCAPS-1D simulation to get a regression prediction model. RSM is validated by the ANOVA test. Finally, optimization for the input parameters is carried out for maximum efficiency to determine the optimal input variable combination.

The values in Table 1 are chosen well in the practical range of the parameters. The variation in the band gap of the SnSe can be seen in the literature from 0.95–1.76 eV.^{17,18} The band gap is an easily tunable parameter and can be tuned by varying the thickness of the film,^{18–20} deposition method, the crystallinity of film, post-annealing, *etc.*^{21,22} We chose the band gap value of SnSe that lies well in the practical range of the parameters.^{23,24}

Generally, shallow energy states are near the valence band maxima and conduction band minima. Dopant energy levels near the valence band maxima form the shallow acceptor density of states, and this density of states is proportional to the dopant concentration. The shallow acceptor density of SnSe can be easily varied by the doping in the SnSe. SnSe is intrinsically p-type due to the vacancy of Sn,^{23,25} so dopants like Na, Mg, K, Ag, *etc.* led to the increased shallow acceptor density after substitution at the Sn site.^{25–28} The shallow uniform acceptor density in the SnSe ranges from 9×10^{15} to $4 \times 10^{16} \text{ cm}^{-3}$. The value of shallow acceptor density of states is within the range reported by Yadav *et al.*²⁹ Elementary calculations for the dopant concentration indicate that the shallow acceptor density of states in the range of 9×10^{15} – $4 \times 10^{16} \text{ cm}^{-3}$ is roughly equal to the substitution of the one Sn atom by dopants per 4.97×10^7 – 2.19×10^6 atoms of Sn in the crystal (taking the unit cell volume as 219.19 \AA^3). During the synthesis of the SnSe (by a physical route), one can easily select the number of the Sn atoms available for the Se to react to form SnSe (following the required number of Sn vacancies). Additionally, the same number of atoms are replaced with the



dopants, and under the controlled conditions of the reaction, dopant atoms can be substituted at the place of Sn.³⁰ After getting the desired stoichiometric ratio of Sn and dopant in SnSe, close sublimation and thermal evaporation of the same powder can be carried out to obtain the desired state of SnSe. Also, thermal co-evaporation of Sn and Se can be optimized for the desired range of Sn vacancy, and then dopants can be added *via* thermal evaporation followed by thermal diffusion processes.³¹ Technically, such precise doping is impossible to achieve, but one may reach nearby values that do not change the device's efficiency significantly. The work function of the back contacts is selected in the range 4.8–5.4 eV. Generally, metals like Au, Pt, Pd, Ni, Ge, and Co have their work function in this range.³²

VBDOS and CBDOS are calculated with the help of the equations below.³³

$$N_C = 2 \left(\frac{2\pi m_n^* K_B T}{h^2} \right)^{3/2} \quad (1)$$

$$N_V = 2 \left(\frac{2\pi m_p^* K_B T}{h^2} \right)^{3/2} \quad (2)$$

where m_n^* is the effective mass of electrons, m_p^* is the effective mass of holes, K_B is the Boltzmann constant, T is temperature, h is Planck's constant, π is 3.1416, N_C is the density of states in the conduction band, and N_V is the density of states in the valence band.

The values of the effective mass of electrons and holes are taken as 0.15 and 0.16 m_0 (ref. 34) (here the direction of transport is taken along the c axis for the vertical solar device; m_0 is the mass of a free electron). From eqn (1) and (2), VBDOS and CBDOS are calculated to be 1.6×10^{18} and $1.45 \times 10^{18} \text{ cm}^{-3}$, respectively.

The radiative recombination coefficient (RRC) is defined as the direct or radiative transitions of excited carriers to the ground states taking place for a defined volume of carriers per second and is calculated using the following formula³⁵

$$t_{\text{rad}} = \frac{1}{B\Delta N} \quad (3)$$

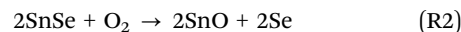
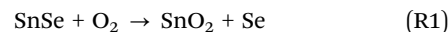
where t_{rad} is the radiative lifetime of excited carriers, B is the radiative recombination rate, and ΔN is an excess number of excited carriers.

SnSe is an indirect band gap material having a band gap value of 1.08 eV.³⁶ The value of radiative recombination coefficients B for the indirect band gap materials is very small and generally lies in the value of $10^{-10} \text{ cm}^{-3} \text{ s}^{-1}$ to $10^{-15} \text{ cm}^{-3} \text{ s}^{-1}$, e.g. Si has $7 \times 10^{-15} \text{ cm}^{-3} \text{ s}^{-1}$,³⁷ GaAs has $10^{-10} \text{ cm}^{-3} \text{ s}^{-1}$.³⁸ For SnSe we have taken radiative recombination coefficient B as a random value of $2.9 \times 10^{-11} \text{ cm}^{-3} \text{ s}^{-1}$. A schematic of the device based on SnSe/TiO₂/SnO₂ is shown in Fig. 1(a) below. Table S1 (ESI[†]) incorporates all the variables chosen for the device.

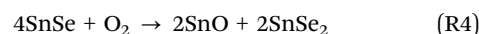
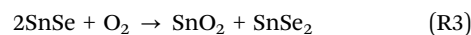
Choosing TiO₂ as a buffer layer has one significant role in the device. Ti can reduce the surface oxidized SnSe to the pure non-oxidized SnSe by converting itself to TiO₂. The SnSe surface can be easily oxidized at room temperature.^{22,39} Ti has the

potential to reduce the surface oxide of all metal chalcogenides.³⁹

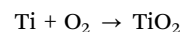
There are four possible reactions for the oxidation of SnSe, with a Gibbs free energy change of $\Delta G = -432.485 \text{ kJ}$ and -328.858 kJ , respectively, for the first and second reactions. The first reaction showed higher possibilities for the formation of a more stable oxide of SnO₂.



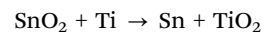
Also, there may form a higher metal oxidation state and anion ratio for SnSe with a Gibbs free energy change³⁹ of $\Delta G = -454.894 \text{ kJ}$, -373.675 kJ , respectively, for the third and fourth reactions.



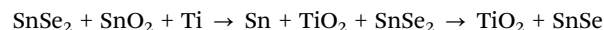
The change in Gibbs free energy for the oxidation of Ti is around -880 kJ (ref. 39)



So, Ti has a greater tendency to react with the oxygen, and even snatch the oxygen atoms from the SnO₂, which has $\Delta G \approx -600 \text{ kJ}$, *via* the following reactions



overall in the presence of Ti, oxidized SnSe again transforms into pure SnSe as³⁹



Details about the algorithm of the SCAPS-1D software can be found in the reports.^{40–42}

Variations in the efficiency of all the above-mentioned parameters are simulated by SCAPS-1D. One can see that the efficiency is maximum at the shallow acceptor density of $4 \times 10^{16} \text{ cm}^{-3}$, the band gap of 1.38 eV, the CBO of 0 eV, temperature of 275 K (but taken more practically to be 300 K for the simulation), and work function of the back contact of 5.4 eV, respectively, as shown in Fig. 1(b). These optimized parameters (Fig. S1(a) and (b), ESI[†]) are applied to simulate for optimal efficiency. The maximum efficiency obtained is 20.74% (Fig. 1(c)).

Generally, it becomes more cumbersome for researchers to search all the possible combinations of variables for maximum efficiency. It is quite easy to apply all the optimized parameters to calculate the maximum efficiency, but one often does not know about the maximum efficiency of the device within these ranges of parameters. Hence one of the ways to find the global maxima of function (efficiency) with 5 input parameters is *via* the CCD and RSM method where the multiple objective optimization genetic algorithm with the following steps is used: (1) the initial population is given by the SCAPS-1D software, or a random initial population is generated by itself. This population will be recorded as population zero. (2) Individuals in



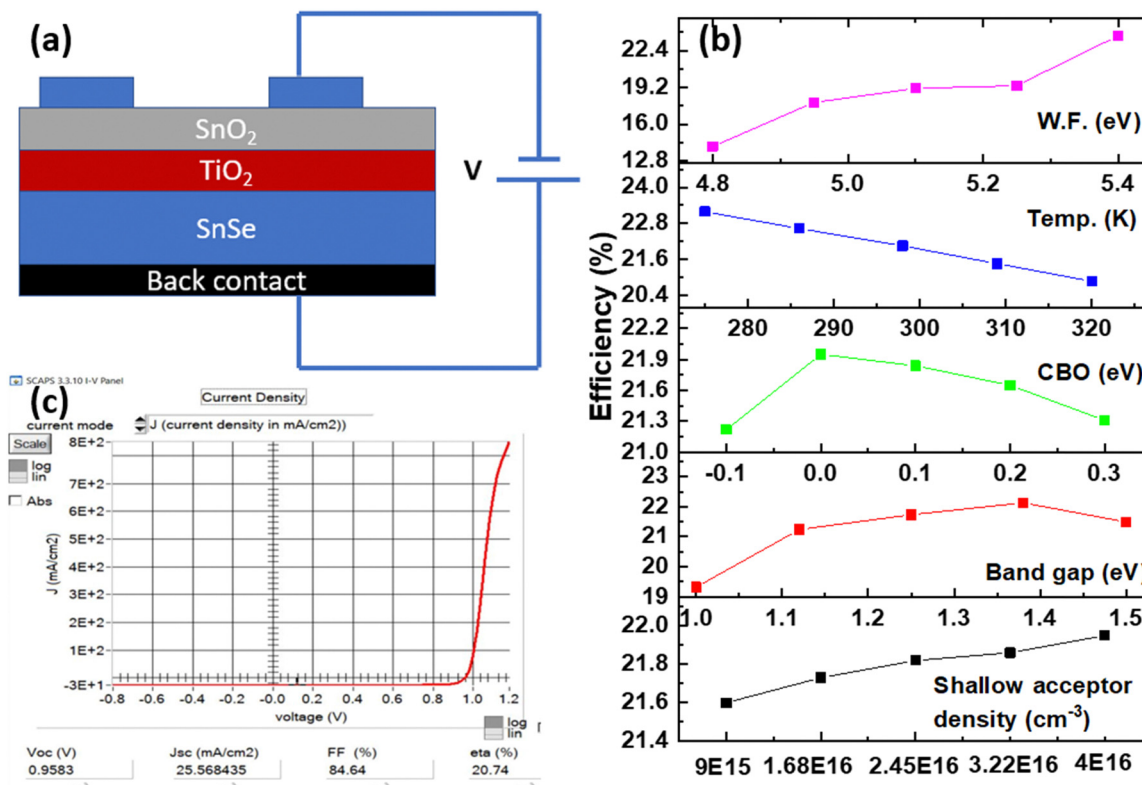


Fig. 1 (a) Schematic of the device, (b) efficiency of the cell for different variables, and (c) efficiency at optimized parameters in (b).

population zero will be assessed and the individuals with high fitness will be selected and combined into the parent population. (3) A child population is then generated by the program using selection, crossover, and mutation. (4) The parent population (the last generation) and child population will be combined by the program to generate a new population. (5) The new non-dominated population will be sorted by the program and the new front is generated. (6) The optimal population will be picked up by the program based on the crowded distance sorting to calculate new generation.

If the present tolerance of the fitness function is less than the preset tolerance of the fitness function of the optimal population, the output result should be produced. Otherwise, repeat steps 3 to 5.

At last, this optimization could potentially suggest the particular values of the parameters at which the device showed its largest efficiency, but practically using the combination of individual sole optimal parameters make it difficult to achieve the targeted maximum efficiency. This is because these parameters are interconnected. For example, the band gap is a function of the doping concentration and the type of dopant, their concentration, thickness, absorption coefficient, *etc.* are not independent and interact with one another. So, controlling the device parameter to the desired value of thickness, shallow acceptor density of states, type of dopant, absorption coefficient, and band gap value may not be possible to achieve simultaneously. In this report, we have taken care in selecting the parameter values in the practical range of the parameters which were either reported

in the literature or can be achieved by a simple strategy or taking the externally controlled parameters in the simulation to be more achievable (like the work function of the back contact, operating temperature, and conduction band offset). Hence the optimal parameters of the device for the maximum efficiency define the efficiency cap of the device, and one can achieve nearby values by targeting the optimized parameters.

CCD modelling and design of experiments

The central composite design table's size depends on the number of parameters, *e.g.* for 5 variables, 50 entries are obtained. There are 8 center points and 42 non-center points in Table S2 (ESI[†]). Centre points are referred to as the middle points of the variable inputs (points in the run of 43 to 50 in Table S3, ESI[†]). For complete details of the CCD and RSM, please refer to ref. 43. The number of runs can be derived from the following equation

$$\text{Total runs} = 2^k + 2k + N$$

where k is the number of independent variables, and N is the number of centre points.

Input variables (shown in Table S3, ESI[†]) can be calculated using eqn (4)–(6) below and output variable R1 (efficiency) using the SCAPS-1D simulation for the RSM.

$$z_0 = \frac{z_{\max} + z_{\min}}{2} \quad (4)$$



$$\Delta z = \frac{z_{\max} - z_{\min}}{2} \quad (5)$$

where z_0 is the mean value of the uncoded (dimensional) input variables z_i ($i = 1-5$); z_{\max} is the maximum value of the uncoded input variables z_i ; z_{\min} is the minimum value of the uncoded input variables z_i ; and the varied range of the uncoded input

variables (*i.e.* minimum and maximum) are taken as z_{\min} and z_{\max} , respectively. The coded (dimensionless) input variables x_i ($i = 1-5$) can be converted from the uncoded input variables z_i ($i = 1-5$) by the following equation:

$$x_{ij} = \frac{z_{ij} - z_0}{\Delta z} \quad (6)$$

Table 2 Analysis of variable (ANOVA) results of the fitted cubic model

Source	Sum of squares	df	Mean square	F-value	p-value	
Model	1676.40	13	128.95	213.28	<0.0001	Significant
$x_1 - x_1$	507.36	1	507.36	839.13	<0.0001	
$x_2 - x_2$	7.87	1	7.87	13.01	0.0009	
$x_3 - x_3$	1.80	1	1.80	2.98	0.0929	
$x_4 - x_4$	1098.70	1	1098.70	1817.15	<0.0001	
$x_5 - x_5$	15.58	1	15.58	25.77	<0.0001	
$x_1 \cdot x_3$	3.13	1	3.13	5.17	0.0291	
$x_1 \cdot x_4$	7.20	1	7.20	11.91	0.0014	
$x_1 \cdot x_5$	1.75	1	1.75	2.89	0.0977	
$x_2 \cdot x_4$	2.29	1	2.29	3.79	0.0595	
$x_3 \cdot x_5$	2.02	1	2.02	3.34	0.0759	
x_1^2	3.21	1	3.21	5.31	0.0271	
x_2^2	3.15	1	3.15	5.22	0.0284	
x_3^2	10.38	1	10.38	17.17	0.0002	
Residual	21.77	36	0.6046			
Lack of fit	21.77	29	0.7506			
Pure error	0.0000	7	0.0000			
Cor total	1698.17	49				

p -values less than 0.0500 indicate the model terms are significant. In this case there are significant model terms. Values greater than 0.1000 indicate the model terms are not significant. If there are many insignificant model terms (not counting those required to support hierarchy), model reduction may improve your model. The model F -value of 213.28 implies the model is significant. There is only a 0.01% chance that an F -value this large could occur due to noise.

where z_{ij} is the table element of the i th row and j th column in Table S2 (ESI[†]), and x_{ij} are the i th row and j th column elements of Table S3 (ESI[†]). In Table S3 (ESI[†]), the uncoded parameters are defined by $x_{i1}, x_{i2}, \dots, x_{i5}$ or compactly to x_1, x_2, \dots, x_5 as the band gap, shallow uniform acceptor density, CBO, work function of the back contact, and operating temperature, respectively.

After the simulation of all these row runs and getting their corresponding efficiency using SCAPS-1D, the input parameters and the calculated efficiency results are co-related in the mathematical polynomial formula with the best fit. The magnitude sequence of the coefficients of the polynomial formula of the RSM reflects the sensitivity of the corresponding variables and interactions like least sensitive, sensitive, and highly sensitive variables/parameters. One can find an optimal combination of these parameters/variables in the range of parameters to achieve maximum efficiency. From the utilization of the CCD and RSM, one can easily find more detailed information about the effects of the variables/parameters on efficiency.

In this paper, we run the 5 variables of the SnSe/TiO₂/SnO₂-based solar cell: band gap, shallow uniform acceptor density, CBO, the device's operating temperature and work function of the back contact. Using the CCD design arrangement (alpha = face-centred, centre point 8, 5 variables), 50 simulation runs are listed in Table S2 (ESI[†]). All 50 simulation runs are simulated in

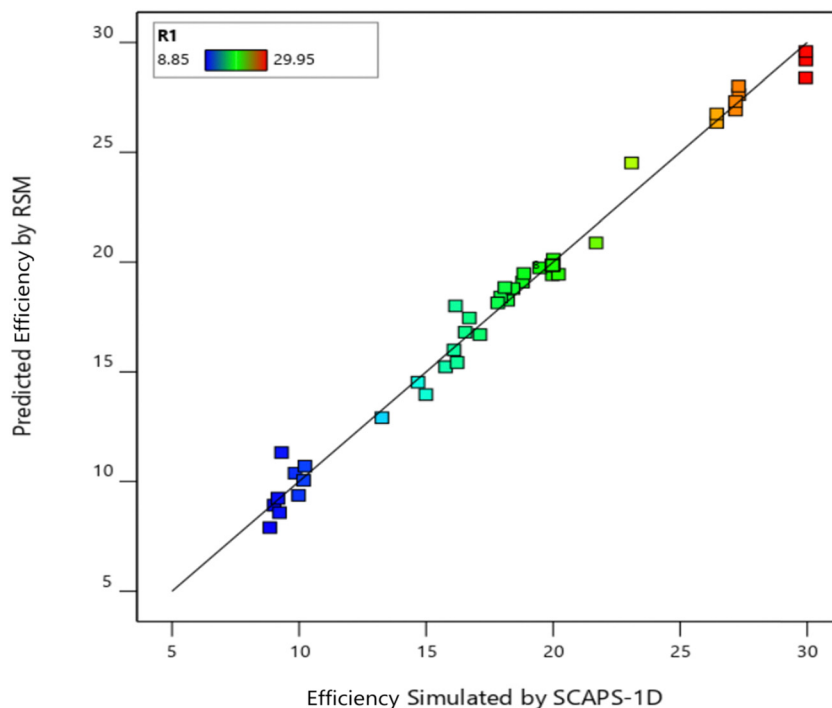


Fig. 2 The efficiencies of the solar cell predicted by the RSM and simulated by SCAPS-1D software.



the SCAPS-1D software to get the corresponding efficiency values listed in the last column of Table S3 (ESI[†]) as the response (R1). The input and response values of the 50 simulation runs shown in Table S3 (ESI[†]) below are fitted with a quadratic polynomial formula model that provides a prediction equation of the response (R1 here efficiency) from the various input parameters of the solar cell, which is given by

$$\eta = 19.86 - 3.71x_1 + 0.4618x_2 + 0.2210x_3 + 5.46x_4 - 0.6498x_5 - 0.3125x_1x_3 - 0.4744x_1x_4 + 0.2338x_1x_5 - 0.2675x_2x_4 - 0.2513x_3x_5 - 0.4679x_1x_1 - 0.4639x_2x_2 - 0.8615x_3x_3 \quad (7)$$

where x_1 , x_2 , x_3 , x_4 , and x_5 are the coded (dimensionless) band gap, shallow uniform acceptor density, conduction band offset, work function of the back contact, and operating temperature of the device, respectively, which are calculated using eqn (6) and Table S2 (ESI[†]).

From eqn (7), it can be seen that the work function of the back contact (z_4/x_4) has the largest effect on the efficiency, while

Table 3 Optimized input parameter combination for the maximum efficiency of the solar cell obtained using the response surface model (eqn (7))

(A) Band gap (eV)	1
(B) Shallow uniform acceptor density of the absorber (cm^{-3})	2.89×10^{16}
(C) CBO (eV)	0.164
(D) Work function of the back contact (eV)	5.399
(E) Temperature (K)	300
(R1) Optimized efficiency by RSM (%)	29.01

the band gap (z_1/x_1), operating temperature (z_5/x_5), shallow acceptor density of states (z_2/x_2), and conduction band offset (z_3/x_3), are the second, third, fourth, and fifth largest impacting parameters to the efficiency of solar cell. Also, when the band gap (z_1/x_1) and operating temperature of the device (z_5/x_5) increase, the efficiency will increase, while increasing the other two parameters (*i.e.* $x_1 \cdot x_3$, $x_1 \cdot x_4$, $x_2 \cdot x_4$, and $x_3 \cdot x_5$) results in decreasing efficiency. Linear coupling terms such as coupling ($x_1 \cdot x_4$) of the band gap of the absorber material (z_1/x_1) and work function of the back contact (z_4/x_4), and coupling ($x_1 \cdot x_5$) of the band gap (z_1/x_1) and operating temperature of the device (z_5/x_5) have the most impact and least impact on the efficiency, respectively.

ANOVA analysis of the RSM

To validate the RSM, the analysis of variance (ANOVA) test can be applied.⁴⁴ The F -value and p -value are the test indicators of the regression model and its terms. The F -value should be as large as possible, and the p value should be as small as possible (< 0.05 at least), respectively, for the RSM and its terms to be valid. The ANOVA analysis results are listed in Table 2.

A scattering of the values around the mean is indicated by the R^2 value 0.9872 (which should be close to 1). The difference between adjusted R^2 (=0.9826) and predicted R^2 (=0.9726) should be reasonable if the difference value is less than 0.2. All statistical values show a good fit for the model. From Table 2, it can also be inferred that the individual terms/variables having high F -values and low p -values have a larger influence on efficiency than the other terms/variables. So, from Table 2, the F -value of the work function of the back contact (z_4/x_4) has the highest value of

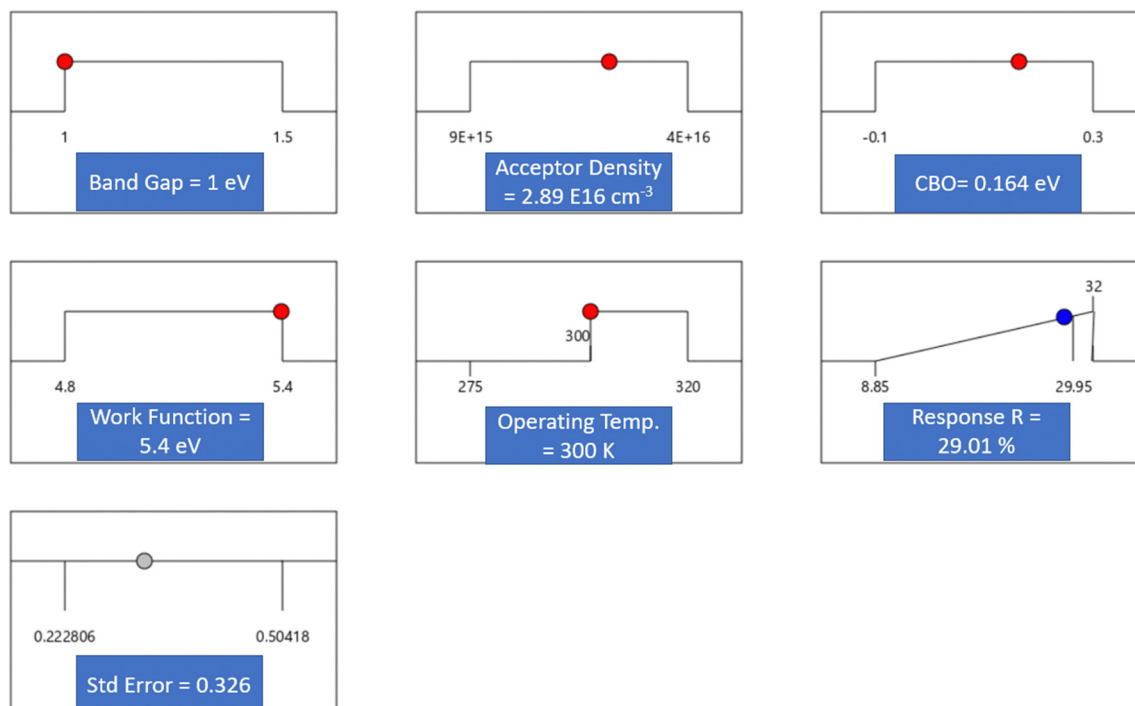


Fig. 3 Optimal input parameters using RSM (design expert panel) for the maximum efficiency of 29.01%.



1817.15 and $p < 0.0001$, followed by that of the band gap (z_1/x_1) with F -value = 839.13, $p < 0.0001$, then that of the operating temperature of the device (z_5/x_5) with F -value = 25.77, $p < 0.0001$.

The coupling term (x_1x_4) of the band gap of the absorber material (x_1) and work function of the back contact (x_4) with an F -value of 11.19 is the interaction term with the largest impact on the efficiency, followed by that (x_1x_3) of the band gap (x_1) and CBO (x_3) with F -value = 5.17, $p = 0.029$, then that (x_2x_4) of the shallow acceptor density of states (x_2) and work function of the back contact (x_4) with F -value = 3.79, $p = 0.0595$. All inferences from the ANOVA test results are in agreement with those from the RSM equation. The ANOVA test results validated the RSM in eqn (7), and the sensitivity analysis was based on the magnitude sequence of the coefficients of the individual terms in eqn (7).

The efficiencies obtained by the RSM and the simulation by SCAPS-1D are compared, and their residuals are shown in Fig. 2 below. The scattered data in Fig. 2 show the simulated or actual efficiencies obtained by SCAPS-1D in the x -axis and the predicted efficiencies by the RSM in the y -axis, showing a good correlation of both.

Parameter optimization for the maximum efficiency and validation

Eqn (7) is used to find the optimal input parameter combination for the maximum R1 using the Design Expert software. The results are listed in Table 3. The optimal input parameter combination gives an efficiency (R) value of 29.01%, as shown in Fig. 3 and listed in Table 3.

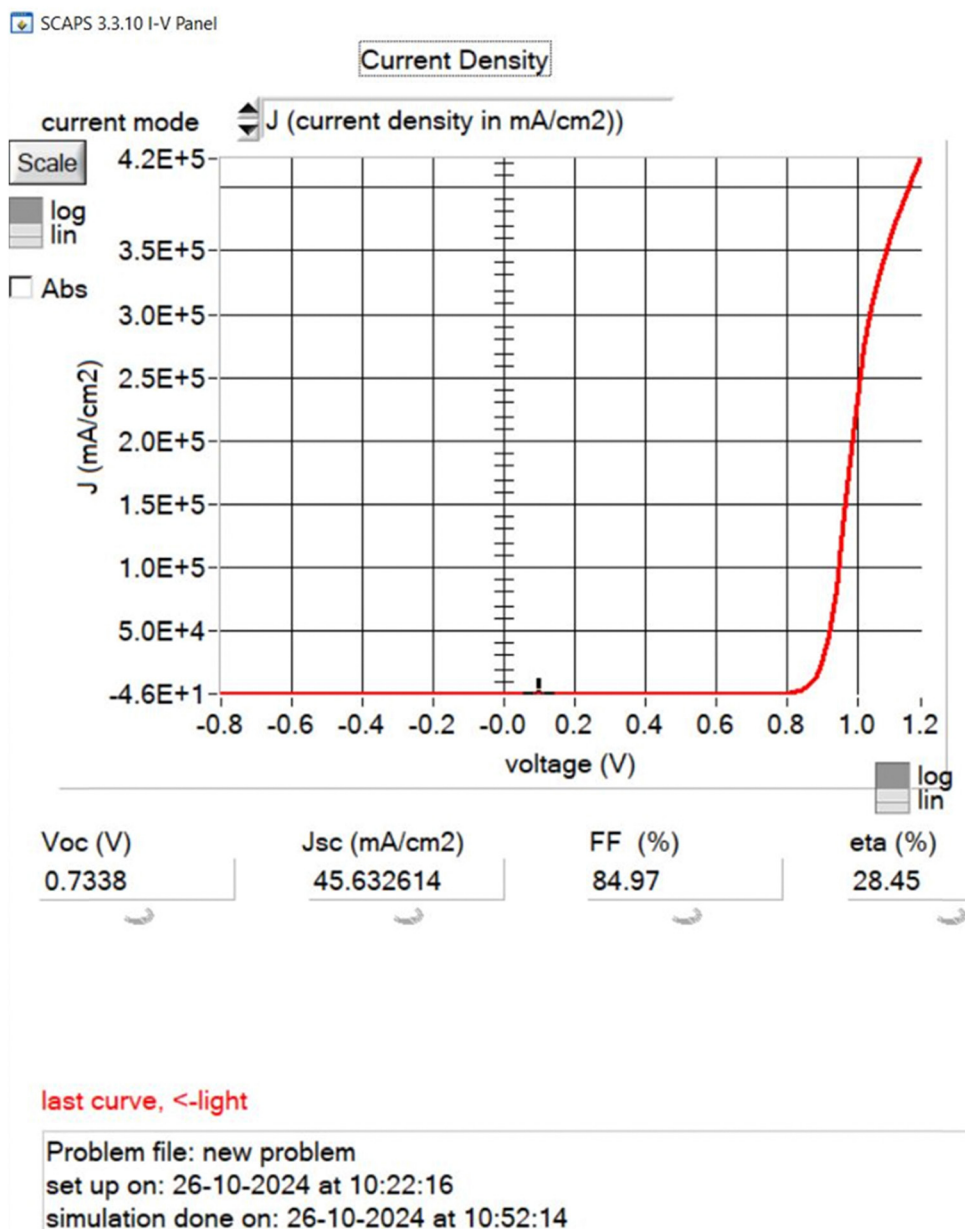


Fig. 4 The output panel of the SCAPS-1D showing the open circuit voltage, short circuit current, fill factor, and efficiency.



The same optimal input parameter values are used as input of the SCAPS-1D software, and a simulation is run in the software; an efficiency of 28.45% is obtained for the input parameters, as shown in Fig. 4.

Input values of the SnSe and TiO₂ are shown in Fig. S2 (ESI†). Both the efficiency values predicted by the RSM (eqn (7)) and the SCAPS-1D software are very close (within 1.93% error), and hence the optimization result of the RSM has been verified by the SCAPS-1D software simulation. A formal intuition into the simple variation and chosen optimum values of the variables led to the maximum value efficiency of 20.74%, while the RSM enabled through CCD runs provides the global maxima of the efficiency function *i.e.* 29.01%. Hence, the proposed CCD and RSM modelling approach enables the SCAPS-1D software to find the real potential of the material.

Conclusions

In conclusion, this study introduces a comprehensive approach to optimizing solar cell performance through parameter sensitivity analysis and response surface modeling. By integrating central composite design (CCD) and response surface methodology (RSM), the research identifies optimal parameter combinations and validates the efficiency predictions using SCAPS-1D simulations. The close agreement between the efficiency values predicted by the RSM and those obtained from SCAPS-1D software demonstrates the effectiveness of the proposed methodology in predicting solar cell efficiency with a high degree of accuracy.

Furthermore, the proposed method enables the SCAPS-1D software to unlock the true potential of solar cell materials by systematically arranging input parameters and refining optimization results through RSM. This approach streamlines the optimization process and minimizes material wastage during synthesis, saving valuable time and energy resources. The sensitivity analysis conducted through RSM provides valuable insights into parameter interactions, enhancing the understanding of factors influencing solar cell efficiency.

By validating the RSM through ANOVA tests, this research underscores the precision and reliability of the proposed methodology in optimizing solar cell structures for maximum performance. The findings of this study contribute to advancing the field of solar cell simulation by offering a systematic and efficient approach to predicting and enhancing solar cell efficiency. Overall, integrating CCD, RSM, and SCAPS-1D software presents a promising avenue for future research in optimizing solar cell performance and realizing the full potential of solar cell materials.

Contributions

Manoj Kumar was involved in conceptualization, investigation, methodology, writing – original draft, and writing – reviewing and editing. Sanju Rani was responsible for conceptualization, formal analysis, investigation, software, writing – original draft, and writing – reviewing and editing. Vidya Nand Singh

contributed to funding acquisition, supervision, reviewing, and editing. Xu Wang took part in conceptualization, formal analysis, investigation, supervision, reviewing, and editing.

Data availability

Data will be made available on request.

Conflicts of interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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