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## Conductive carbon embedded beneath cathode active material for longevity of solid-state batteries†

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A composite structure was developed for use in all-solid-state batteries that consists of a conductive 3D reduced graphene oxide framework embedded beneath cathode active material particles. This unique structure offers significant advantages when combined with a sulfide solid electrolyte as the heterogeneous distribution of the conductive carbon in the composite cathode ensures good contact between the carbon and cathode particles for facile electron transfer while a direct contact between the carbon and sulfide solid electrolyte is avoided or minimized. This approach assists in preventing or reducing unwanted irreversible faradaic reactions. As a result, the newly developed composite of cathode particles decorated on a 3D reduced graphene oxide framework delivers higher specific capacity with improved cycling stability compared with a typical composite cathode consisting of a homogenous mixture of the cathode active material, carbon nanofibers, and sulfide solid electrolyte.

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property relationship. He has published more than 95 peer-reviewed articles and 6 patents until now. He was selected as a Clarivate's 'Highly Cited Researcher (HCR)', and won several awards, including 2023 ACS Materials Au Rising Star, Young Scientist Award from the International Society for Solid-State Ionics, ECS Battery Division Postdoctoral Associate Research Award.

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## 1. Introduction

All-solid-state batteries (ASSBs) hold great promise, including improved safety and higher energy density, compared with conventional lithium-ion batteries (LIBs) as the non-flammable solid electrolyte (SE) can be combined with an energy-dense lithium-metal anode.<sup>1–3</sup> Given these technical advantages, various types of SEs have been studied and developed, including sulfides, halides, and oxides as well as their polymer composites.<sup>4–7</sup> Among these materials, sulfide-based SEs exhibit superior ionic conductivity of  $10^{-3}$  to  $10^{-4}$  S cm<sup>-1</sup> at room temperature, which is even comparable to that of liquid organic electrolytes.<sup>4,8</sup> However, sulfide-based SEs have a narrow electrochemical stability window<sup>9</sup> and poor chemical/electrochemical compatibility with electrodes,<sup>3,10–14</sup> which remain grand challenges.

Argyrodite ( $\text{Li}_x\text{PS}_5\text{X}$ , X = Cl, Br) SEs possess both high ionic conductivity and relatively good interfacial compatibility against a lithium-metal anode compared with other sulfide SEs such as  $\text{Li}_{10}\text{GeP}_2\text{S}_{12}$  and  $\text{Li}_3\text{PS}_4$  electrolytes.<sup>15,16</sup> However, in the composite cathode, both the cathode active material (CAM)/argyrodite SE and carbon/argyrodite SE interfaces are not thermodynamically stable.<sup>10,17,18</sup> Recent studies have demonstrated

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that inorganic coating layers such as  $\text{LiNbO}_3$  (LNO),<sup>19</sup>  $\text{Li}_2\text{O}-\text{ZrO}_2$  (LZO),<sup>20</sup> and  $\text{Li}_{1.175}\text{Nb}_{0.645}\text{Ti}_{0.4}\text{O}_3$  (LNTO)<sup>21</sup> can suppress the degradation at the CAM/argyrodite SE interface. Whereas cation substitutions barely affect their intrinsic oxidative electrochemical stability when sulfur remains a major part of the chemical composition,<sup>22</sup> partial substitution of oxygen with sulfur has been suggested to increase the oxidation limit.<sup>23,24</sup> Coating of halide SEs with higher oxidative stability on the CAM also results in improved cycling stability as the formation of a detrimental interface between the CAM and argyrodite SE can be avoided, and the halide SE functions as a Li-conducting buffer layer in this composite cathode design.<sup>25</sup>

The use of an electronically conductive carbon additive in the composite cathode is necessary to provide facile electron transfers to the CAMs and create uniform current distributions. However, sulfide SEs, including argyrodites, are readily decomposed when they form an interface with the conductive carbon, and the decomposition is even accelerated when the composite cathode is charged to high voltage.<sup>26</sup> Recent studies show that the morphology and quality (*i.e.*, defects and functional groups) of carbon significantly affect the electrochemical performance of ASSBs.<sup>18,27–29</sup> For example, Darren *et al.* showed that the low-surface-area carbon (vapor-grown carbon fiber) delivered a lower irreversible capacity in the composite cathode than high-surface-area carbon (carbon black).<sup>18</sup> Park *et al.* demonstrated that the use of graphitized carbon with fewer functional groups in the composite cathode improved the reversible capacity and cycling stability.<sup>29</sup>

Although conductive carbon coating on the CAM surface is frequently used in conventional LIBs to improve the electronic conductivity of the cathode,<sup>30,31</sup> this approach is not suitable for ASSBs using sulfide SEs because the coated carbon must contact the SEs, which would lead to detrimental decomposition reactions (Fig. 1a). Therefore, low-surface-area carbon nanofibers (CNFs) or carbon nanotubes (CNTs) are widely used in the composite cathode of ASSBs.<sup>17,18,20,32</sup> These low-surface-area carbon additives can reduce the interfacial area between carbon and SEs.<sup>18</sup> However, the homogeneously mixed CNFs with CAM and SE cannot prevent direct contact between the carbon additive and SEs, and we cannot control these interfaces (Fig. 1b). In a very recent study, Lee and colleagues developed zinc oxide (ZnO)-coated CNF to reduce the contact area between the carbon additive and SEs.<sup>17</sup>

In the current study, an unconventional CAM–carbon structure was designed where an electronically conductive carbon framework is embedded beneath CAM particles, as illustrated in Fig. 1c. In this unique structure, electron transfers to CAM particles can be facilitated through the carbon framework while the detrimental interface between the carbon additive and SE can be avoided or at least minimized when this CAM–carbon structure is mixed with a SE. Herein, we applied this strategy to  $\text{LiNbO}_3$  (LNO)-coated polycrystalline  $\text{LiNi}_{0.8}\text{-Mn}_{0.1}\text{Co}_{0.1}\text{O}_2$  (pc-NMC) and LNO-coated single-crystalline  $\text{LiNi}_{0.6}\text{Mn}_{0.2}\text{Co}_{0.2}\text{O}_2$  (sc-NMC622), and these materials demonstrated improved cycling performance.

## 2. Experimental section

### 2.1. Materials synthesis

**Polyethylenimine (PEI)-coated NMC.** In a typical process, 1000 mg of polyethylenimine (PEI) and 800 mg of polyvinylpyrrolidone (PVP) were dissolved in 20 mL of an EtOH/MeOH (1 : 1) solution. Then, 1000 mg of pc-NMC811 (or sc-NMC622) particles were dispersed in that solution at a concentration of 50 mg mL<sup>-1</sup>. The dispersion was ultrasonically treated for 1 h and then stirred at 600 rpm at RT for 24 h. The products were obtained and washed with MeOH and acetone. LNO-coated pc-NMC811 and sc-NMC622 are purchased from MSE supplies LLC.

**Acid treatment for porous carbon.** Porous carbon was treated with 4 M  $\text{HNO}_3$  and  $\text{H}_2\text{SO}_4$  for 1 day, centrifuged, and washed with  $\text{H}_2\text{O}$  and MeOH sequentially.

**Reduced graphene oxide (RGO)-carbon composite (conductive carbon).** After treating with  $\text{H}_2\text{SO}_4/\text{HNO}_3$ , the porous carbon was mixed with single-layer graphene oxide (10 : 1 ratio) in  $\text{H}_2\text{O}$  and sonicated for 1 h. Then, 57% hydrogen iodide (HI) was added to the dispersion and stirred for 2 h at 90 °C. After cooling down to RT, the composite was washed with water and MeOH to obtain the desired RGO–carbon composite.

**Conductive carbon–CAM.** PEI-coated NMC and RGO–carbon composites in different ratios were sonicated in MeOH for 2 h and stirred at RT for 24 h. The composite was then centrifuged and washed with acetone and dried in an oven to obtain the final product.

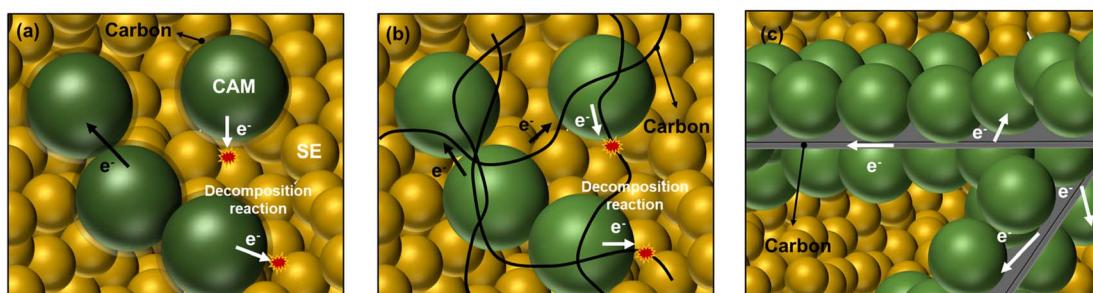


Fig. 1 Schematics of carbon–CAM composite with SEs. (a) Carbon-coated CAM mixture with SEs. (b) Mixture of CAM, CNF, and SE. (c) Carbon embedded beneath CAM and its mixture with SE.



## 2.2. Characterization

X-ray diffraction (XRD) analysis was conducted using a Rigaku Miniflex 600 equipped with a Cu K $\alpha$  radiation source. The surface morphology and microstructure of the samples were examined using scanning electron microscopy (SEM; PHENOM PW-100-017 or FEI Quanta FEG-250). Energy-dispersive X-ray spectroscopy (EDS) elemental mappings were obtained using transmission electron microscopy (TEM; FEI Titan X 60-300). The K $\alpha$  X-ray edges were used to construct a map of each element (C, N, O, Si, Mn, Co, Ni, Cu, and Nb) to avoid energy overlaps between certain elements in the samples.

Thermogravimetric analysis (TGA) was performed with a TGA5500 (TA instruments) using an aluminum pan. The measurements were conducted at a heating rate of 5 °C min $^{-1}$  from 40 °C to 650 °C after drying at 120 °C for 1 h before measurement to remove absorbed moisture on the sample surface. Fourier-transform infrared (FTIR) spectra were recorded on a Nicolet iS50 FT-IR system (Thermo Fisher, USA). Raman measurements were performed using a Renishaw Invia Raman spectrometer equipped with a laser of 514.5 nm excitation wavelength. Raman mapping measurements were conducted on a confocal Raman spectrometer (Horiba, Xplorer 405 nm edge laser, long working distance objective = 50 $\times$ , grating with 2400 grooves per mm, numerical aperture (N.A.) = 0.42, local power < 500  $\mu$ W). The laser spot diameter was estimated to be 1  $\mu$ m. The scan region was set to 80  $\times$  40  $\mu$ m $^2$ , with a 1  $\mu$ m $^2$  per pixel step size. The integration time was set to 2 s for each point. Autofocus mode was applied at each XY point to ensure consistent focus on the sample surface. All the Raman mappings were analyzed using Horiba LabSpec 6 imaging and spectroscopy software, and the K-means clustering algorithm was integrated into the Scikit-learn platform using a previously reported similar method.<sup>33,34</sup> The SEM images of the composite cathodes were obtained from the cross-sectioned particles using a Scios Dual Beam focused-ion beam (FIB)/SEM (FEI/ Thermo Fisher) at the QB3 facility at the University of California, Berkeley. The composite cathode pellets were first cross-sectioned using the Ga $^+$  ion beam for material. The composite cathode pellets were milled with a beam current of 0.9–6.5 nA and then polished with a beam current of 93 pA to 0.46 nA. SEM/EDX analysis was conducted on the milled samples.

## 2.3. Electrochemical testing

The all-solid-state Li-metal batteries were constructed using a commercial battery cell enclosure system (model WCBR-SLD-S, Wellcos Inc.). Firstly, 50 mg of LPSCl powder ( $D_{50} \sim 1 \mu$ m, Ampcera Inc.) was pressed using two stainless-steel rods at a pressure of 100 MPa to fabricate a thin LPSCl pellet. To fabricate the composite cathodes, the synthesized NMC/RGO composite (78 wt%) was homogeneously mixed with LPSCl powder (22 wt%) and then uniformly applied on the LPSCl solid-electrolyte layer. For the reference NMC/CNF composite, NMC and CNF were initially mixed to achieve homogeneity, followed by the subsequent addition of LPSCl powder to make the composite. The composite cathode and LPSCl SE layer were pressed under 250 MPa to secure contact between the

composite cathode and SE layers. To add the anode layer, an In metal disk was first placed onto the other side of the LPSCl pellet, followed by placing a Li-metal disk onto the indium (In) disk (composition: Li<sub>0.22</sub>In<sub>0.78</sub>). In our experiments, we used 7.0–7.3 mg of CAM for each cell, which corresponds to the CAM loading density of 9.1–9.5 mg cm $^{-2}$ . The assembled ASSB cell was then pressed under 30 MPa during the galvanostatic cycling performed in a voltage window of 2.5–4.3 V (vs. Li/Li $^+$ ). All electrochemical testing was conducted using a Maccor Model 2200 cycler at 50 °C.

## 3. Results

### 3.1. Polycrystalline LiNi<sub>0.8</sub>Mn<sub>0.1</sub>Co<sub>0.1</sub>O<sub>2</sub>/reduced graphene oxide framework composite

Fig. 2 illustrates the fabrication process for the CAM-3D reduced graphene oxide (RGO) framework composite. First, a porous 3D RGO framework was prepared by dispersing acid-treated porous carbon and single-layer graphene oxide (GO) in H<sub>2</sub>O. The objective of the acid treatment of the porous carbon was to improve its dispersion ability in H<sub>2</sub>O, which aids the hybridization with single-layer GO. After that, the porous 3D RGO framework was reduced by HI aqueous solution. The porous 3D RGO framework exhibits graphitic features, as confirmed by XRD (see ESI Fig. S1a $\dagger$ ). Typical D- and G-bands of RGO are confirmed at  $\sim$ 1340 and  $\sim$ 1580 cm $^{-1}$ , respectively, by Raman spectroscopy (ESI Fig. S1b $\dagger$ ). The  $I_D/I_G$  ratio of the RGO framework is estimated to be 0.59. ESI Fig. S1c $\dagger$  presents SEM images of the 3D RGO framework where graphene flakes are attached on the porous carbon framework. In this structure, porous carbon is the framework and RGO is added to increase the electrical conductivity. After the reduction, the obtained 3D RGO framework was mixed with PEI-modified NMC in MeOH. To synthesize PEI-modified NMC particles, we used PVP and PEI polymers in which PVP was used to prevent NMC particle agglomeration and PEI was used to create a positively charged surface layer on NMC particles. The resulting mixture of PEI-modified NMC and 3D RGO framework was sonicated for 2 h and stirred overnight to produce the desired CAM–carbon composite. In this process, the PEI-coated NMC particles, which have positive surface charges attracts the 3D RGO framework with the negatively charged surface. The presence of the PEI coating on pc-NMC811 was confirmed by the N–H stretching and bending peaks in the IR analysis, as illustrated in ESI Fig. S2a $\dagger$  and the EDS mapping in ESI Fig. S2b. $\dagger$  We also confirm that the pc-NMC811 particles and their morphologies were not damaged by the PEI coating process, as shown in the SEM images in ESI Fig. S2c and d. $\dagger$

Following the synthesis process described above, we developed LiNbO<sub>3</sub> (LNO)-coated polycrystalline LiNi<sub>0.8</sub>Mn<sub>0.1</sub>Co<sub>0.1</sub>O<sub>2</sub>/RGO composites (hereafter, pc-NMC811/RGO) with varied carbon contents. The target carbon contents were 0.5 wt%, 1.0 wt%, 2.0 wt%, and 4.0 wt%. The carbon contents in the pc-NMC811/RGO composites were estimated using TGA as shown in Fig. 3a. The weight loss from 100 °C to 650 °C of the pc-NMC811/RGO is attributable to the decomposition of any carbon in the composite, which includes RGO and porous



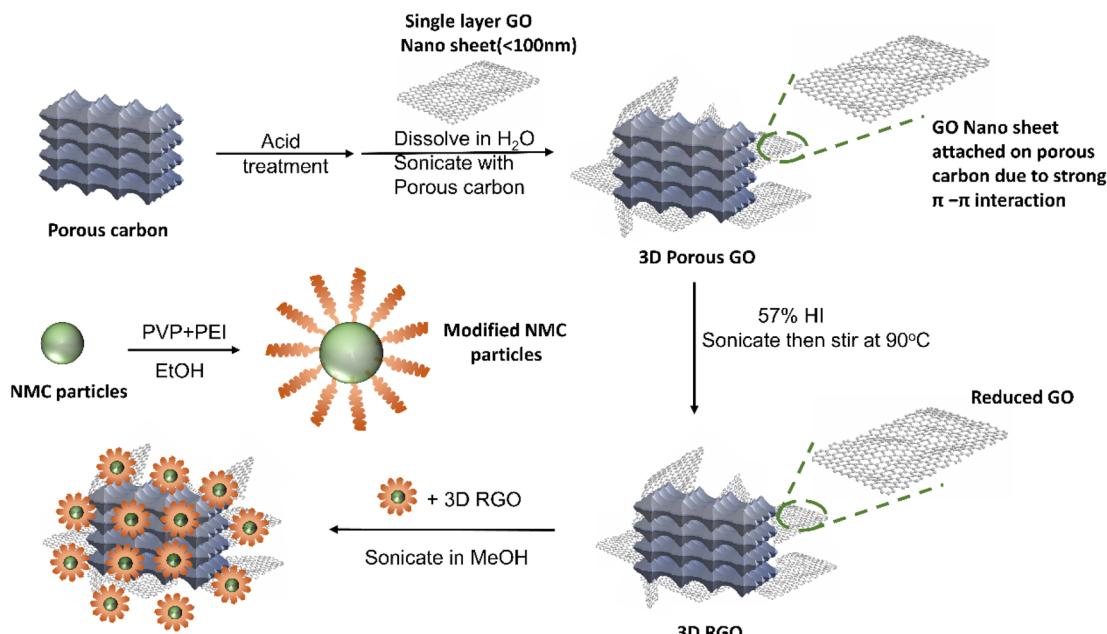


Fig. 2 Schematic of the fabrication of the CAM-RGO framework composite.

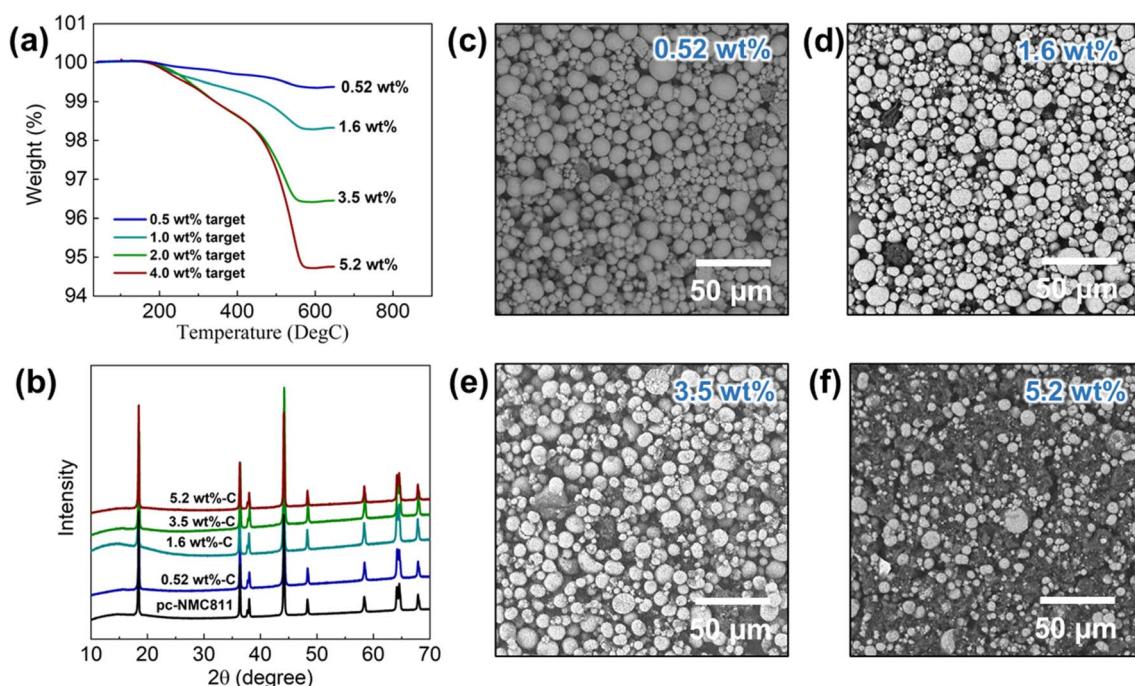


Fig. 3 Materials characterization of pc-NMC811/RGO composites. (a) TGA results, (b) XRD patterns, and (c)–(f) SEM images of pc-NMC811/RGO composites.

carbon.<sup>35</sup> Hereafter, we used the RGO content to refer to the carbon content in the composite structure for simplicity. The RGO contents of the composites are 0.52 wt%, 1.6 wt%, 3.5 wt%, and 5.2 wt%, respectively. The RGO contents calculated from the TGA results are used in the following sections. Fig. 3b presents XRD patterns of pc-NMC811 and its RGO composites, without any noticeable impurity phases or structure changes of

pc-NMC811 after the synthesis. Fig. 3c–f presents SEM images of the pc-NMC811/RGO composites with varied carbon contents. We found that the 3D RGO framework is well covered by pc-NMC811 cathode particles (secondary particle size: 5–20  $\mu\text{m}$ ), and only a limited surface of the RGO framework remained uncovered by pc-NMC811 when the RGO content is below 5.2 wt%, as confirmed by the SEM images. In contrast, 3D-RGO



is not fully covered by pc-NMC811 particles when a relatively high RGO content of 5.2 wt% is used (Fig. 3f). To demonstrate that pc-NMC811 particles are selectively attached on the 3D-RGO framework in our synthesis process, we synthesized the control group where pc-NMC811 without PEI coating was mixed with 3D-RGO. In this control group, we found that pc-NMC811 particles are randomly distributed and that some of the pc-NMC811 particles are not attached on the 3D-RGO framework (ESI Fig. S3a†). In contrast, all the PEI-coated pc-NMC811 particles are covered on the 3D-RGO framework (ESI Fig. S3b†), which is clear evidence that the PEI coating on pc-NMC811 particles plays a key role in creating good contact between the pc-NMC811 particles and 3D-RGO framework.

To evaluate our hypothesis that using conductive carbon embedded beneath cathode particles can reduce the interfacial area between the conductive carbon and SEs in the composite cathode, we mixed the pc-NMC811/RGO composite with LPSCl SE, pelletized the mixture, and then conducted Raman mapping as shown in Fig. 4a. All Raman mapping frames were analyzed using the *K*-means clustering algorithm, which has been proven effective in extracting heterogeneous chemical and structural information in several previous studies.<sup>36,37</sup> The Raman peak intensities were normalized by the highest peak intensity from LPSCl or its decomposed products at 400–600 cm<sup>-1</sup>.<sup>38</sup> The lower

part of the mapping area consists solely of LPSCl SE. In Fig. 4a, the carbon-rich areas with a relatively high intensity of Raman peaks at 1200–1800 cm<sup>-1</sup>, which are typical Raman peaks from carbon (*i.e.*, D-band at 1377 cm<sup>-1</sup> and G-band at 1584 cm<sup>-1</sup>), are colored red.<sup>39,40</sup> The average domain size of the carbon-rich area is 10–20 μm, which is consistent with the pc-NMC811 particle size. Since pc-NMC811 particles are decorated on the RGO framework, as confirmed by the SEM images in Fig. 3, we expect pc-NMC811 particles to be present in the carbon-rich areas. The green areas, showing a reduced intensity of the typical Raman carbon peaks, correspond to LPSCl-rich domains. Due to overlapping Raman peaks of pc-NMC811 and LPSCl, distinguishing pc-NMC811 particles from LPSCl in the composite cathode is not feasible.<sup>38,41</sup> Nevertheless, our results confirm that the distribution of the carbon framework is highly heterogeneous in the composite cathode, which suggests a reduced contact area between the RGO framework and LPSCl SE. We expect that the contact area (if any) between RGO and LPSCl SE will still lead to unwanted side reactions because we did not control the functionalities of the carbon. The gray, brown, and orange colors in Fig. 4 indicate LPSCl only areas from the LPSCl SE. Each color has a slightly different peak shape at Raman shift below 700 cm<sup>-1</sup>, which is attributable to the distinct local structural environments. In contrast, Fig. 4b displays

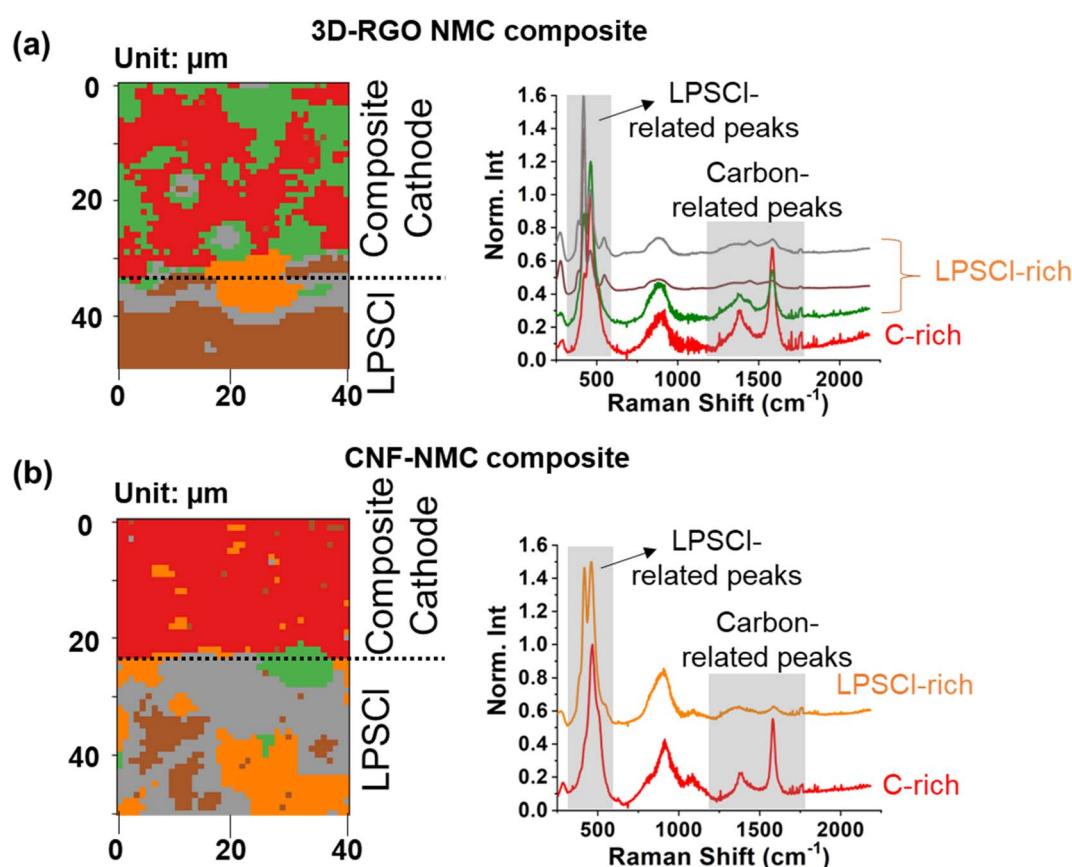


Fig. 4 Raman mapping based on *K*-means clustering analysis for (a) composite cathode consisting of pc-NMC811/RGO and LPSCl SE and (b) composite cathode consisting of pc-NMC811, CNF, and LPSCl SE. The black dotted line indicates the location of the composite cathode|LPSCl interface.



a composite cathode where CNFs were randomly mixed with LPSCl SE and pc-NMC811 particles using a mortar and pestle. In this control group, a homogeneous carbon-rich Raman response (red color) is observed throughout the mapping, indicating an even distribution of CNFs in the composite cathode. We expect that the homogeneous distribution of carbon in the composite cathode may facilitate uniform electron transfer throughout the composite cathode; however, it does not prevent detrimental contact between carbon and the LPSCl SE. These findings indicate that our composite cathode design, featuring conductive carbon embedded beneath the cathode active material, can effectively reduce the interfacial area between carbon and the LPSCl SE. We anticipate that carbon embedded beneath the cathode particles can still provide facile electron transport pathways to the cathode particles.

Fig. 5a presents charge–discharge profiles of the pc-NMC811/RGO composite cathodes with varied RGO contents, a CNF composite cathode, and a cathode without carbon additive. The composite cathodes were prepared by mixing RGO composites (78 wt%) and LPSCl SEs (22 wt%). We used Li–In (composition:  $\text{Li}_{0.22}\text{In}_{0.78}$ ) alloy anodes, and the voltage was converted to *vs.*  $\text{Li}/\text{Li}^+$ . All the solid-state battery cells were tested at 50 °C under 30 MPa. The composite cathode with CNF shows a relatively large charge capacity in the low-voltage regions below 3.5 V (*vs.*  $\text{Li}/\text{Li}^+$ ), whereas the control group without carbon additive shows no capacity in the low-voltage regions (indicated by the green box in Fig. 5a). These results confirm that the capacity obtained from the low-voltage regions <3.5 V (*vs.*  $\text{Li}/\text{Li}^+$ ) originates from the decomposition of LPSCl at LPSCl/carbon interfaces. Interestingly, unwanted side reactions at <3.5 V (*vs.*  $\text{Li}/\text{Li}^+$ ) are greatly suppressed in the RGO composite cathode, as indicated in the highlighted area in Fig. 5a. Fig. 5b summarizes the charge and discharge capacities in the first cycle. The charge and discharge capacities gradually increase as the RGO content increases from 0.52 wt% to 3.5 wt% from 163 to 232 mA h g<sup>-1</sup> for charging and from 104 to 164 mA h g<sup>-1</sup> for discharging at C/10 (1C = 200 mA g<sup>-1</sup>). The charge and discharge capacities decrease when the RGO content increases to 5.2 wt%. In addition, the composite cathode with 5.2 wt% RGO has lower coulombic efficiency (59.4%) than the composite cathodes with lower RGO contents

(71.2% for 1.6 wt% RGO and 70.6% for 3.5 wt% RGO). Low coulombic efficiency in 5.2 wt% RGO sample could be related to the RGO framework surfaces which are not covered by pc-NMC811 particles that led to the decomposition of LPSCl at the interface during the charge process. The 3.5 wt% RGO and 1.6 wt% RGO composites exhibit improved reversible discharge capacities and coulombic efficiency compared with the composite cathode containing CNF (2 wt%), as shown in Fig. 5b. We also found that the 3.5 wt% RGO and 1.6 wt% RGO composites show lower polarization than the composite cathode containing CNF in Fig. 5a. The improved capacities and coulombic efficiencies can be attributed to the electronically conductive carbon being embedded beneath the pc-NMC811 particles and less carbon surface forming interfaces with LPSCl in the RGO composite system. Fig. 5c shows the cycling stability of the pc-NMC811/RGO composites and control groups. All the RGO composites deliver improved cycling stability compared with the composite cathode with CNF. More specifically, the 3.5 wt% RGO and 1.6 wt% RGO composites maintain 94.7 and 106 mA h g<sup>-1</sup>, respectively, after 15 cycles. The 0.52 wt% RGO composite exhibits lower discharge capacity in the first cycle than the other RGO composites but it retains the highest capacity of 114.6 mA h g<sup>-1</sup> after 15 cycles and 70 mA h g<sup>-1</sup> after 30 cycles. Nevertheless, capacity decay was still observed as cycling progressed in the RGO composites. ESI Fig. S4† confirms that some primary NMC811 particles were detached from the secondary particle. In these RGO composites, the detached particles could not be connected to electronically conductive carbon, and their surfaces were not protected by a LNO coating layer, which may have led to capacity degradation upon repeated charge–discharge cycling. Therefore, we extended our study to single-crystal NMC particles, as discussed in the next section.

### 3.2. Single-crystalline $\text{LiNi}_{0.6}\text{Mn}_{0.2}\text{Co}_{0.2}\text{O}_2$ /RGO framework composite

We used LNO-coated single-crystal NMC622 (sc-NMC622) cathode particles (particle size: 1–5  $\mu\text{m}$ ) to create the RGO composite to avoid the issue of particle detachment from the secondary particle agglomerates that occurred in pc-NMC811/RGO composites. The same synthesis procedures that were applied to the pc-NMC811/RGO composites were used for the

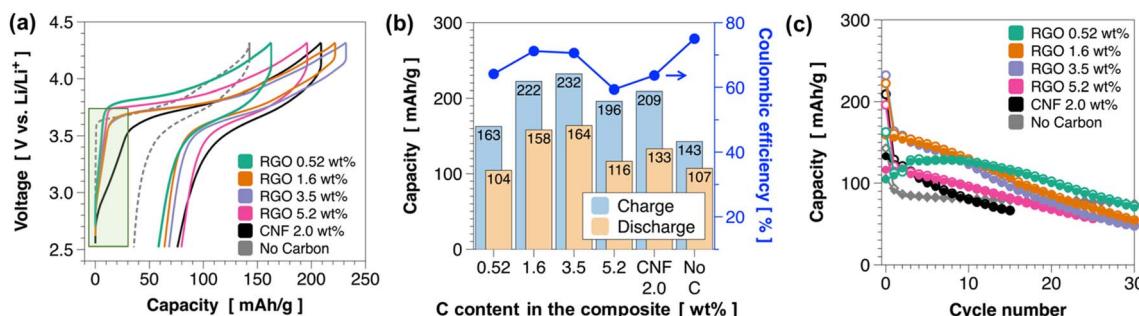


Fig. 5 Electrochemical properties of pc-NMC811/RGO composites. (a) The first charge–discharge profiles of pc-NMC811/RGO composites with varied RGO contents. Composite cathodes with CNF and no carbon are used as control groups. (b) Initial charge and discharge capacities of pc-NMC811/RGO composites and control groups. The right y-axis indicates the coulombic efficiency at the first cycle. (c) Cycling stability of pc-NMC811/RGO composites and control groups.



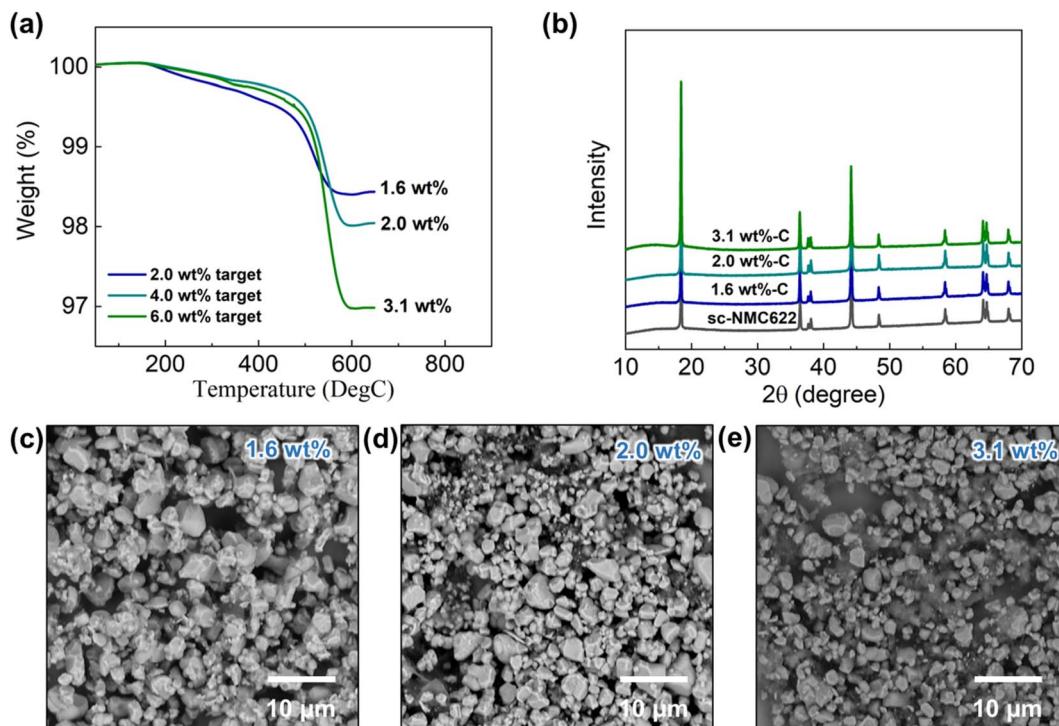


Fig. 6 Materials characterization of sc-NMC622/RGO composites at varied RGO contents. (a) TGA results, (b) XRD patterns, and (c)–(e) SEM images of sc-NMC622/RGO composites.

synthesis of sc-NMC622/RGO composites. Fig. 6a presents the TGA results of the sc-NMC622/RGO composites. The target RGO contents in the synthesis process were 2 wt%, 4 wt%, and 6 wt%. The weight loss from 100 °C to 650 °C of the sc-NMC622/RGO in TGA is attributable to the decomposition of any carbon in the composite, which includes RGO and porous carbon.<sup>35</sup> Hereafter, we used the RGO content to refer to the carbon content in the composite structure for simplicity. The RGO contents were estimated to be 1.6 wt%, 2.0 wt%, and 3.1 wt%, respectively, in the composites. Hereafter, the estimated RGO contents will be used to refer to the samples. No changes in the XRD patterns of sc-NMC622 were observed after the RGO composite synthesis, as shown in Fig. 6b, indicating that the synthesis process does not affect the crystal structure of the sc-NMC622 particles and that decomposition of sc-NMC622 did not occur. Fig. 6c–e display SEM images of sc-NMC622/RGO composites at varied RGO contents. In the 1.6 wt% RGO sample, the RGO surface is fully decorated with sc-NMC622 particles, and it is difficult to observe the RGO surface in Fig. 6c. This structure can reduce the contact area between carbon framework and LPSCl SE in the composite cathode structure. However, we suspect that some sc-NMC622 particles may not be directly connected to the electronically conductive RGO framework due to a high sc-NMC622 loading on the RGO framework, which can increase the polarization in the electrochemical test. When the RGO content increased to 2.0 wt%, some of the RGO was detected under the sc-NMC622 particles in the SEM image (Fig. 6d). When the RGO content increased up to 3.1 wt%, more RGO surfaces were exposed and

not covered by sc-NMC622 particles. These uncovered surfaces likely react with the LPSCl SE in the composite cathode.

The three sc-NMC622/RGO composites were tested in ASSB cells using LPSCl as the SE and a Li-In (composition:  $\text{Li}_{0.22}\text{In}_{0.78}$ ) alloy as the counter electrode. Electrochemical tests were conducted at 50 °C under 30 MPa. Fig. 7a presents charge–discharge profiles of the sc-NMC622/RGO composites with varied RGO contents of 1.6 wt%, 2.0 wt%, and 3.1 wt%. The first charge and discharge capacities are 138.6  $\text{mA h g}^{-1}$  (charge) and 104.4  $\text{mA h g}^{-1}$  (discharge), 183.5  $\text{mA h g}^{-1}$  (charge) and 155.4  $\text{mA h g}^{-1}$  (discharge), and 201.4  $\text{mA h g}^{-1}$  (charge) and 171.0  $\text{mA h g}^{-1}$  (discharge) for the 1.6 wt%, 2.0 wt%, and 3.1 wt% RGO composites, respectively, at C/20 (1C = 170  $\text{mA g}^{-1}$ ). The first cycle coulombic efficiency of the 1.6 wt%, 2.0 wt%, and 3.1 wt% RGO composites are 75.3%, 84.7%, and 84.9%, respectively. The inset in Fig. 7a shows that the capacity obtained in a relatively low-voltage region (<3.5 V vs. Li/Li<sup>+</sup>) decreases when the RGO content decreases. This result indicates that the RGO composite with lower RGO content has a lower interfacial area between the RGO framework and LPSCl SE in the composite cathode. However, the RGO composite with low RGO content (1.6 wt%) exhibits a larger polarization than the RGO composites with higher RGO contents (2.0 wt% and 3.1 wt%). These results may indicate that some of the sc-NMC622 particles are not connected to the electronically conductive RGO framework in the 1.6 wt% RGO composite because of the low RGO content. Notably, much lower charge capacity at <3.5 V vs. Li/Li<sup>+</sup> was observed in the sc-NMC622/RGO composites compared with the pc-NMC811/RGO composites.

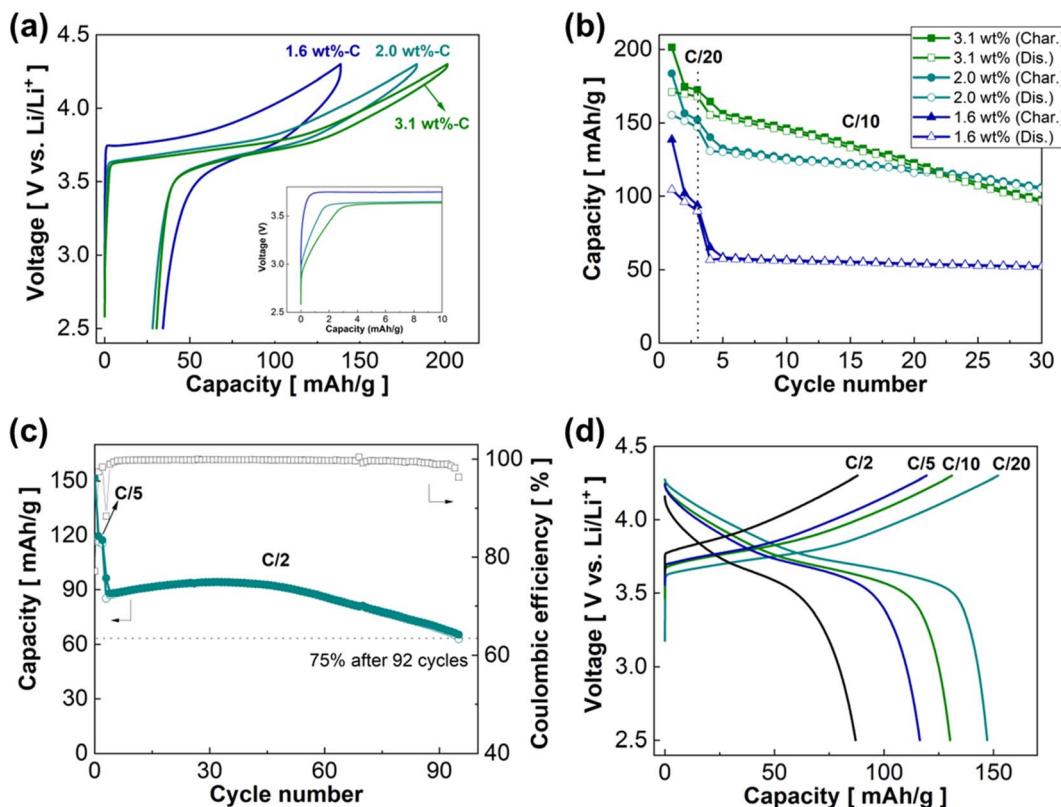


Fig. 7 Electrochemical properties of sc-NMC622/RGO composites. (a) Charge–discharge profiles of sc-NMC622/RGO composites with varied RGO contents. Inset: magnified area of the initial charging process up to  $10 \text{ mA h g}^{-1}$ . (b) Cycling stability of sc-NMC622/RGO composites. (c) Cycling stability of 2.0 wt% RGO composite at C/5 and C/10. (d) Rate capability of 2.0 wt% RGO composite.

This is attributable to the sc-NMC622 particles being well connected to the RGO framework without breaking.

Fig. 7b shows the cycling stability of the sc-NMC622/RGO composites. The initial three cycles were performed at C/20, and the current rate increased to C/10 for the following cycles. After 30 cycles, the 3.1 wt% RGO composite maintains a capacity of  $96.2 \text{ mA h g}^{-1}$ , corresponding to 62% retention at C/10. The 2.0 wt% RGO and 1.6 wt% RGO composites retain capacities of 105.0 and  $52.0 \text{ mA h g}^{-1}$ , which correspond to capacity retention of 80% and 91.5%, respectively, after 30 cycles at C/10. We found a trade-off in the RGO content of the composite. A high RGO content delivers higher first discharge capacity but shows faster capacity decay over cycles than lower RGO content. Fig. 7c shows the cycling stability of the 2.0 wt% RGO composite at C/2 after the initial three cycles at C/5. The 2.0 wt% RGO composite maintains 75% ( $63.0 \text{ mA h g}^{-1}$ ) of the capacity at C/2 after 92 cycles. The first-cycle coulombic efficiency is 77.1% and increases gradually upon cycling up to 99.7–99.96%, which might indicate the formation of passivating cathode–electrolyte interphase (CEI). After 60 cycles, the coulombic efficiency and capacity begins to decrease. Fig. 7d displays the charge–discharge profiles of the 2.0 wt% RGO composite at varied current rates of C/20, C/10, C/5, and C/2. The 2.0 wt% RGO composite delivers capacities of 147.1, 130.2, 116.4, and  $87.0 \text{ mA g}^{-1}$  at C/20, C/10, C/5, and C/2, respectively.

## 4. Discussion

In this work, we developed a new composite structure consisting of an electronically conductive RGO framework embedded beneath CAM particles using both polycrystalline (pc) and single-crystalline (sc) NMC particles. Although both the pc-NMC811/RGO and sc-NMC622/RGO composites delivered reasonably good electrochemical performance, the sc-NMC622/RGO composite exhibited improved cycling stability (Fig. 5 and 7). The different compositions of pc-NMC811 and sc-NMC622 may have affected the electrochemical performance. However, we suspect that the improved cycling stability in the sc-NMC622/RGO composite is mainly attributable to all the sc-NMC622 particles being well attached on the RGO framework and sc-NMC622 not breaking down during the mixing process with LPSCl SE particles. In the pc-NMC811/RGO composite, we observed that some pc-NMC811 particles were broken and that small primary particles were detached from the polycrystalline composite, as shown in ESI Fig. S4,† after mixing with LPSCl SE particles. Because the outer surface of the secondary particles was covered by a LNO coating layer, the primary particles were not protected by LNO after the primary particles were detached from the secondary particles. These unprotected surfaces led to unwanted side reactions with LPSCl SE particles both chemically and electrochemically. In addition, these detached



primary particles could not be effectively connected to the RGO framework.

Our RGO framework had negatively charged oxygen-containing functional groups at the surface, which were used to attract the positively charged PEI-coated NMC particles (either pc-NMC811 or sc-NMC622). These attractions created a unique structure where an electronically conductive RGO framework was embedded beneath NMC particles. However, it is known that the functional groups and defects in the carbon additive can form a functional-group-induced insulating layer at the SE interface.<sup>29</sup> Although most of the surface of the RGO framework was covered by NMC particles, it is expected that some of the surface may form an interface with LPSCl. In this case, the functional groups at the surface of the RGO framework can accelerate decomposition of LPSCl.

## 5. Conclusion

In this study, we developed a conductive 3D RGO framework embedded beneath the CAM (pc-NMC811 and sc-NMC622). In the composite cathode for the solid-state battery, the newly developed composite of NMC particles decorated on the 3D RGO framework exhibited higher specific capacity and improved cycling stability compared with a typical composite cathode, where the CAM, CNF, and LPSCl SE are homogeneously mixed. In our composite cathode where the NMC/RGO composite and LPSCl SE were mixed, the heterogeneous distribution of the electronically conductive RGO framework, which preferably contacted with NMC particles, prevented the formation of a detrimental interface between RGO framework and LPSCl SE. This study demonstrates the importance of designing carbon–CAM composite structures where the electronically conductive carbon is embedded beneath the CAM to provide facilitated electron pathways while preventing direct contact between the carbon and SE in the composite cathode of solid-state batteries.

## Author contributions

Y. W. B.: investigation, data curation, visualization, writing-original draft. S. Y.: investigation, data curation, visualization, writing-original draft. G. Y.: investigation, data curation, visualization. D. M. K.: investigation, data curation. V. S. A.: investigation, data curation. T. O.: investigation, data curation. M. S.: supervision. B. H.: supervision. J. U.: funding acquisition, supervision. H. K.: conceptualization, funding acquisition, data curation, investigation, visualization, supervision, writing-original draft. All: writing-review & editing.

## Conflicts of interest

There are no conflicts to declare.

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