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## Can self-propelled objects escape from compression stimulation?†

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We studied circular papers impregnated with camphor (CPs) and CPs with magnets (MCPs) as self-propelled objects floating on water under the compression of the water surface as an inanimate system for evacuation in an emergency. Two water chambers— $C_{in}$  and  $C_{out}$ —were connected via a plastic gate, and eight CPs or eight MCPs were placed on  $C_{in}$ . We monitored the movement of the CPs or MCPs from  $C_{in}$  to  $C_{out}$  when the gate was opened and the area of  $C_{in}$  ( $A_{in}$ ) was decreased using a barrier. When  $A_{in}$  was large, CPs moved stochastically from  $C_{in}$  to  $C_{out}$  while exhibiting random motion. The escape probability from  $C_{in}$  to  $C_{out}$  ( $P$ ) at time  $t = 20$  s increased with a decrease in  $A_{in}$ , and the rate of increase in  $P$  increased depending on the width of the gate ( $W_g$ ). By contrast, clustering was observed for MCPs. Consequently,  $P$  of MCPs was lower than that of CPs. The difference in the surface tension between  $C_{in}$  and  $C_{out}$  ( $\Delta\gamma$ ) increased with a decrease in  $A_{in}$ .  $P$  is discussed in relation to  $\Delta\gamma$  as the driving force for emergencies and the repulsive forces between CPs or attractive forces between MCPs. These results suggest that the repulsive force enhances the self-propulsion of objects towards the gate, that is, as a result, higher values of  $P$  are obtained.

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## 1. Introduction

The optimization of evacuation patterns of crowds is important to induce safe and rapid evacuation. Many studies have been conducted on the evacuation from closed spaces, such as buildings.<sup>1–7</sup> However, complete evacuation patterns have not yet been established because unpredictable events, such as panic behaviors of crowded people in a complex system, can occur. Experimental and theoretical studies using inanimate systems have become an important strategy not only to virtually examine many types of complex and serious conditions without actually using people but also to overcome such problems while reducing the actual damage.<sup>8–16</sup>

The present experimental system for evacuation using camphor self-propelled objects is very simple and controllable since the size and shape of camphor can be easily changed. In addition, constant velocity motion is maintained for about 10 minutes.

Furthermore, evacuation using self-propelled objects can be investigated both theoretically and experimentally since a mathematical model constructed based on the simple experimental system clarifies the intrinsic mechanism and gives us a novel perspective. In this study, we examined the evacuation of two types of self-propelled objects, namely circular papers impregnated with camphor (CPs) and CPs with magnets (MCPs), from an inner chamber ( $C_{in}$ ) to an outer chamber ( $C_{out}$ ) under a decrease in the surface area of  $C_{in}$  ( $A_{in}$ ). Here,  $C_{in}$  and  $C_{out}$  were connected through a gate, and eight CPs or eight MCPs were placed on  $C_{in}$  initially. The movement number of the CPs or MCPs was measured at different widths of the gate ( $W_g$ ). The surface tensions of  $C_{in}$  and  $C_{out}$  in the presence of the eight CPs in  $C_{in}$  were measured with a decrease in  $A_{in}$  to clarify the driving force of evacuation. The escape probability of the eight CPs was numerically calculated based on the difference in the surface tension between  $C_{in}$  and  $C_{out}$ . The experimental results suggest that self-propelled objects with repulsive force between them are easier to evacuate than those without a repulsive force or with an attractive force. This tendency is owing to a difference in the surface tension between  $C_{in}$  and  $C_{out}$ .

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## 2. Experimental section

(+)-Camphor and methanol were purchased from FUJIFILM Wako Pure Chemical Co. (Osaka, Japan) and Nacalai Tesque,



Inc. (Kyoto, Japan), respectively. Water was purified by filtering through active carbon, ion-exchange resin, and Millipore Milli-Q filtering system (Merck Direct-Q 3UV, Germany; resistance:  $18 \text{ M}\Omega \text{ cm}$ ). Two types of self-propelled objects were prepared (Fig. 1a). For one of the objects, a circular paper (diameter: 4 mm, thickness: 0.2 mm) as a self-propelled body was prepared from filter paper (WHATMAN, 5307-090, USA) using a brass punch and soaked in a saturated camphor-in-methanol solution ( $1.1 \text{ g mL}^{-1}$ ) for several seconds.<sup>17,18</sup> The circular paper was then dried in air on a glass plate for 5 min to evaporate methanol. We call this circular paper with camphor CP (see the upper part of Fig. 1a). As for the other object, a circular paper with magnetic force was prepared with a CP and a double-sided magnetic sheet (thickness: 0.1 mm, Uinkit, Japan) shaped like a circle (diameter: 3 mm) using a brass punch. The magnet sheet was glued to the top and center of the CP. We call this circular paper with the magnet MCP (see the lower part of Fig. 1a). A trough for measuring the  $\Pi$ -A isotherm (Kyowa Interface Science Co. Ltd, HMB, Saitama, Japan) was used as the water chamber, as shown in Fig. 1b. The water chamber (width: 49 mm, water phase depth: 6 mm) was divided into two chambers,  $C_{\text{in}}$  and  $C_{\text{out}}$ , using an acrylic bar (length: 4 mm, height: 5 mm, width: 80 mm); however, the two chambers were connected through a gate (width:  $W_g$  mm, height: 4 mm) in the bar. The volume of water in the chamber was 105 mL. The gate was blocked using another plastic plate (width: 49 mm, length: 5 mm, height: 15 mm) to maintain the initial number of CPs or MCPs at eight before starting the examination. After blocking the gate using a plate, eight CPs or eight MCPs were floated on the  $C_{\text{in}}$ . The examination started when the gate was opened by removing the plate, followed by a reduction in  $A_{\text{in}}$  using the barrier, which was linearly moved using a stepping motor X stage (the minimum precision:  $0.2 \mu\text{m}$ ; COMS Co., PM80B-100X, Hyogo, Japan). The barrier was scanned from  $x = 100$  to 28 mm along the  $x$ -axis at  $3.6 \text{ mm s}^{-1}$  (Fig. 1b), that is, the scan time was 20 s. During this scan,  $A_{\text{in}}$  was changed from  $4900 \text{ mm}^2$  to  $1372 \text{ mm}^2$  at  $176.4 \text{ mm}^2 \text{ s}^{-1}$ . The location of the gate on the  $x$ -axis was  $x = 0$ . In addition, during the scan of the barrier,  $A_{\text{in}}$  was smaller than the area of  $C_{\text{out}}$  ( $A_{\text{out}} = 3920 \text{ mm}^2$ ) at  $t \geq 5.6 \text{ s}$ . At least five examinations were performed under each experimental condition to confirm the reproducibility of the results. The motion of CPs was monitored with a digital video

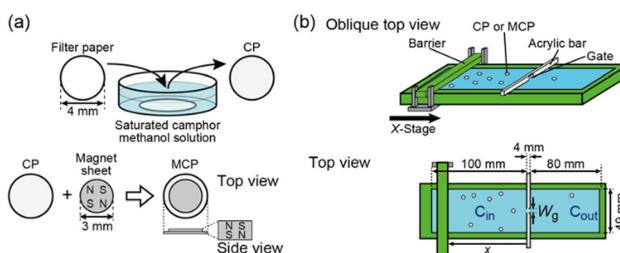


Fig. 1 Schematic illustration of (a) preparation of CPs and MCPs, and (b) the experimental apparatus with escape of eight self-propelled objects from  $C_{\text{in}}$  to  $C_{\text{out}}$  under the compression.  $x = 100 \text{ mm}$  was the initial position of the barrier on the  $x$ -axis.

camera (HDR-CX560V, Sony, Tokyo, Japan; minimum time resolution:  $1/30 \text{ s}$ ) in an air-conditioned room at  $298 \pm 2 \text{ K}$  and then analyzed using an image-processing system (ImageJ, National Institutes of Health, MD, USA). The surface tension at the air/aqueous interface was measured using a surface tensiometer (CBVP-A3, Kyowa Interface Science Co. Ltd, Saitama, Japan) based on the Wilhelmy method *in situ*.

### 3. Results

#### 3.1. Escape probability of eight CPs or MCPs from $C_{\text{in}}$ to $C_{\text{out}}$ with the decreasing water surface area of $C_{\text{in}}$

First, we examined the eight CPs and MCPs at different values of  $W_g$  with a decrease in the water surface of  $C_{\text{in}}$ . Fig. 2 shows the behavior of (a) eight CPs and (b) eight MCPs with a linear decrease in  $A_{\text{in}}$  by scanning the barrier. At high values of  $A_{\text{in}}$  ( $3489$ – $4900 \text{ mm}^2$ ), CPs individually and randomly exhibited self-propulsion only on  $C_{\text{in}}$  ( $t = 0, 4$ , and  $8 \text{ s}$ ). Several seconds after reaching  $A_{\text{in}} = 2783 \text{ mm}^2$ , CP moved from  $C_{\text{in}}$  to  $C_{\text{out}}$  at  $t = 11 \text{ s}$  (see Fig. S1, ESI†), and the number of CPs in  $C_{\text{out}}$  ( $N_{\text{out}}$ ) increased with time at  $t = 12$ – $16 \text{ s}$ , with  $N_{\text{out}} = 4$  maintained at  $t = 16$  and  $20 \text{ s}$ . However, self-propulsion with two MCPs stuck together was partly observed at the largest value of  $A_{\text{in}}$  ( $4900 \text{ mm}^2$ ) at  $t = 0 \text{ s}$ . During compression, the stuck number increased with decreasing  $A_{\text{in}}$  at  $t = 4$ – $20 \text{ s}$ . Although two MCPs stuck together moved from  $C_{\text{in}}$  to  $C_{\text{out}}$  (see Fig. S1, ESI†), six MCPs stuck together in  $C_{\text{in}}$  did not move to  $C_{\text{out}}$  at  $t = 20 \text{ s}$ .

Fig. 3 shows (a) the time-variation of  $N_{\text{out}}$  and (b)  $N_{\text{out}}$  as a function of  $A_{\text{in}}$  for (1) eight CPs and (2) eight MCPs at different values of  $W_g$  (5, 25, and  $40 \text{ mm}$ ). CPs at  $W_g = 5 \text{ mm}$  did not

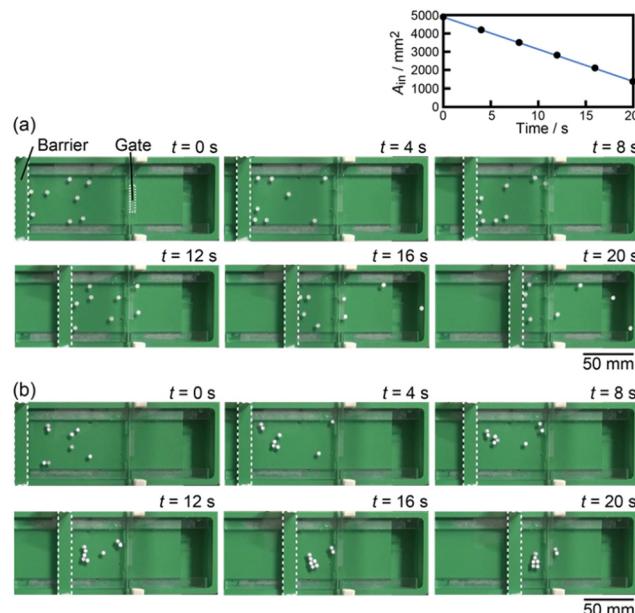


Fig. 2 Snapshots of (a) eight CPs and (b) eight MCPs with a decrease in the surface area of  $C_{\text{in}}$  at  $W_g = 25 \text{ mm}$  (top view, time interval: 4 s). The time variation of  $A_{\text{in}}$  is shown above (a). The pertinent movies (Movies S1 and S2, ESI†) which correspond to figures (a) and (b), respectively, are shown in the ESI.†



move from  $C_{in}$  to  $C_{out}$  at  $0 \leq t \leq 16.0$  s, which corresponded to  $4900 \geq A_{in} \geq 2078 \text{ mm}^2$  (see Fig. 3a1). For the CPs at  $W_g = 25$  and 40 mm,  $N_{out}$  increased with time under compression, and the rate of increase of  $N_{out}$  increased with an increase in  $W_g$  (see Fig. 3a1). However, the increase rate of  $N_{out}$  of eight MCPs was individually lower than those for eight CPs at the examined values of  $W_g$  (see Fig. 3a2). Particularly, MCPs at  $W_g = 5 \text{ mm}$  did not move from  $C_{in}$  to  $C_{out}$  during compression (see Fig. 3a2). In addition, two or more MCPs that stuck together did not move from  $C_{in}$  to  $C_{out}$  at  $W_g = 5 \text{ mm}$ . By contrast, two MCPs stuck together moved from  $C_{in}$  to  $C_{out}$  but three or more MCPs stuck together did not move from  $C_{in}$  to  $C_{out}$  at  $W_g = 25$  and 40 mm.

Fig. 4 shows the escape probability from  $C_{in}$  to  $C_{out}$  ( $P$ ) for CPs, MCPs, and Ps depending on  $W_g$ . Here, Ps are 8 filter papers without camphor and  $P = N_{out-f}/N_{in-i}$  ( $N_{out-f}$ : the final value of  $N_{out}$  and  $N_{in-i}$ : the initial value of  $N_{in}$  ( $= 8$ ) at  $t = 20$  s.  $P$  for CPs clearly increased with an increase in  $W_g$  and reached  $\sim 65\%$  at  $W_g = 40 \text{ mm}$ . However,  $P$  for MCPs increased slightly with an increase in  $W_g$  and reached  $\sim 45\%$  at  $W_g = 40 \text{ mm}$ . Additionally,  $P$  for MCPs was lower than those for the CPs at all  $W_g$ . Approximately 2 Ps escaped to  $C_{out}$  for every  $W_g$ .

### 3.2. Measurement of the surface tension for $C_{in}$ and $C_{out}$ with the decrease in $A_{in}$ in the presence of eight CPs in $C_{in}$

The measurement of the surface tension of the water phase is important to clarify the mechanism of the escape phenomenon because the decrease in the surface tension due to the existence of CPs or MCPs in  $C_{in}$  induces a difference in the surface tension between  $C_{in}$  and  $C_{out}$ . Fig. 5 shows the surface tension ( $\gamma$ ) of  $C_{in}$  and  $C_{out}$  with a decrease in  $A_{in}$  owing to the movement of the barrier and the presence of eight CPs in  $C_{in}$ .  $\gamma$  of  $C_{out}$  was higher than that of  $C_{in}$  under the present conditions. The difference in  $\gamma$  between  $C_{in}$  and  $C_{out}$ ,  $\Delta\gamma = \gamma_{out} - \gamma_{in}$ , was the smallest at the largest value of  $A_{in}$  ( $4900 \text{ mm}^2$ ) but increased with the decrease in  $A_{in}$ .

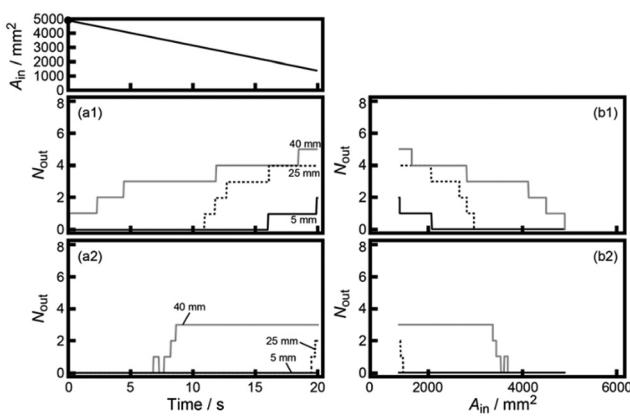


Fig. 3 (a) Time variation of  $N_{out}$  and (b) the relationship between  $N_{out}$  and  $A_{in}$  for (1) CPs and (2) MCPs at different values of  $W_g$  (5 (black line), 25 (black dotted line), and 40 (gray line)). The relationship between  $A_{in}$  and time is shown above (a1). The data for  $W_g = 25 \text{ mm}$  correspond to those in Fig. 2.

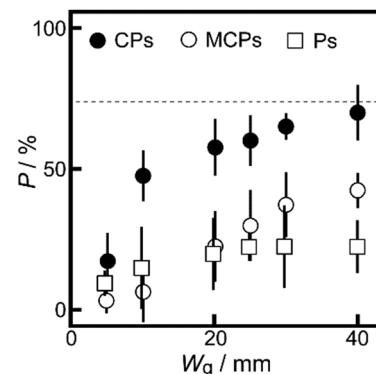


Fig. 4 Escape probability from  $C_{in}$  to  $C_{out}$  ( $P$ ) as a function of  $W_g$  for CPs (filled circles), MCPs (empty circles), and Ps (empty squares) at  $t = 20$  s. The gray horizontal dotted line denotes  $P = 74.07\%$ , which is equal to  $A_{out}/(A_{in-f} + A_{out}) \times 100\%$ , where  $A_{in-f}$  is the final value of  $A_{in}$  ( $1372 \text{ mm}^2$ ) at  $t = 20$  s. Error bars represent the standard deviation from four examinations.

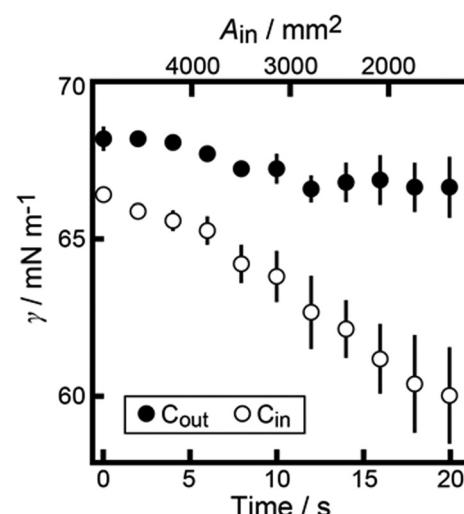


Fig. 5 Time variation of the surface tension ( $\gamma$ ) for  $C_{in}$  (empty marks) and  $C_{out}$  (filled marks) when  $A_{in}$  was decreased from  $4900$  to  $1372 \text{ mm}^2$  along the x-axis at  $3.6 \text{ mm s}^{-1}$ .  $W_g$  was selected as  $2 \text{ mm}$  to prevent eight CPs from going out from  $C_{in}$  to  $C_{out}$ . Error bars represent the standard deviation from four examinations.

## 4. Discussion

Based on the experimental results and related reports,<sup>19–32</sup> we discuss the mechanism of escape from  $C_{in}$  to  $C_{out}$  for two types of self-propelled objects: CPs and MCPs. Here, the time required for  $N_{out}$  to reach 4 as the equilibrium condition is defined as the relaxation time,  $t_e$ . If  $t_e$  is equal to or shorter than the observation time ( $t_0 = 20 \text{ s}$ ),  $P$  is determined as  $A_{out}/(A_{in-f} + A_{out})$ , that is, 74.07%. Table S1 (ESI†) shows the time ( $t_1$ ) when the first CP or MCP escaped to  $C_{out}$ . Values of  $P$  lower than 74.07% for CPs suggest that  $t_e$  is longer than  $t_0$ , and the convergence of  $P$  to 74.07% for CPs with an increase in  $W_g$  suggests that  $t_e$  decreases to  $t_0$  depending on  $W_g$  (see Fig. 2–4). By contrast, the fact that  $P$  of MCPs is lower than that of CPs for the individual values of  $W_g$ , suggests that MCPs crowded by the



attractive force reduce  $P$  owing to the increase in their sizes. Alternatively, the repulsive force between CPs makes them difficult to crowd together.<sup>20,23,26,32</sup> Fig. 4 and 5 suggest that the difference in surface tension between  $C_{in}$  and  $C_{out}$  enhances the escape of CPs from  $C_{in}$  to  $C_{out}$  because CPs move in the direction of higher surface tension.<sup>23,26,30-32</sup>

We assume that the time variation of  $N_{out}$  is expressed by eqn (1). Here, we ignored the repulsive and attractive forces between self-propelled objects and their volume.

$$\frac{dN_{out}}{dt} = a \left( \frac{N_{in}(t)}{A_{in}(t)} - \frac{N_{out}(t)}{A_{out}} \right), \quad (1)$$

where  $a$  is a positive constant. As  $N_{in} = N_{total} - N_{out}$  ( $N_{total}$ : the total number of self-propelled disks (= 8)), eqn (1) is rewritten as eqn (2).

$$\frac{dN_{out}}{dt} = \left( \frac{a}{A_{in}(t)} \right) \left\{ N_{total} - N_{out}(t) \frac{(A_{in}(t) + A_{out})}{A_{out}} \right\}. \quad (2)$$

If  $A_{in}$  is constant and  $A_{in} = A_{out}$ , eqn (2) can be rewritten as eqn (3).

$$\frac{dN_{out}}{dt} = \left( \frac{a}{A_{in}(t)} \right) (N_{total} - 2N_{out}(t)). \quad (3)$$

Assuming that  $A_{in}(t)$  is constant  $A_{in}$ , eqn (3) is solved as follows:

$$-\left( \frac{A_{in}}{2} \right) \ln \left( 1 - \frac{2N_{out}(t)}{N_{total}} \right) = at, \quad (4)$$

where  $N_{out}(0) = 0$ . Because  $a$  is changed depending on  $W_g$  (see Fig. S2, ESI†),  $a$  is approximately expressed as a function of  $W_g$ , as shown in eqn (5).

$$a = a_0 W_g, \quad (5)$$

where  $a_0$  ( $\text{mm s}^{-1}$ ) is a positive constant. In order to obtain  $a_0$ , experiments were performed at  $A_{in} = A_{out} = 3920 \text{ mm}^2$  and different values of  $W_g$ . The value of  $a_0$  was obtained as  $2.05 \pm 0.19$  ( $R^2 = 0.85$ ) from the relationship between  $-(A_{in}/2)\ln(1 - 2N_{out}(t)/N_{total})$  and  $t$  based on the least squares method for the experimental results of  $N_{out}$  of CPs (see Fig. S2, ESI†).

Furthermore,  $P$  depending on  $W_g$  was calculated using eqn (2) and (5) when  $A_{in}$  was changed from 4900 to  $1372 \text{ mm}^2$  due to the decrease of  $dA_{in}/dt = -176.4 \text{ mm}^2 \text{ s}^{-1}$  (Calculation 1). The calculation had no effect on the difference in surface tension between  $C_{in}$  and  $C_{out}$ .

In addition, the effect of the difference between the surface tension of  $C_{in}$  ( $\gamma_{in}$ ) and that of  $C_{out}$  ( $\gamma_{out}$ ), that is,  $\Delta\gamma = \gamma_{out} - \gamma_{in}$  ( $\text{mN mm}^{-1}$ ), was introduced in eqn (2). Based on the experimental results shown in Fig. 5,  $\Delta\gamma$  is described by eqn (6).

$$\Delta\gamma = b_0 + b_1 (A_{in-i} - A_{in}), \quad (6)$$

where  $b_0$  ( $\text{mN mm}^{-1}$ ) and  $b_1$  ( $\text{mN mm}^{-3}$ ) are positive constants and  $A_{in-i}$  is the initial value of  $A_{in}$  (=  $4900 \text{ mm}^2$ ). In fact,  $\Delta\gamma$  was almost linearly dependent on  $A_{in-i} - A_{in}$ , as shown in Fig. S3 (ESI†). The  $b_0$  and  $b_1$  values were obtained from Fig. S3 (ESI†) as  $(1.38 \pm 0.23) \times 10^{-3}$  and  $(1.41 \pm 0.11) \times 10^{-6}$ , respectively.

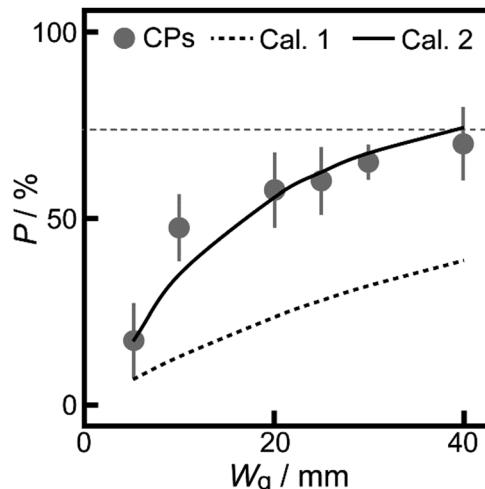


Fig. 6 Numerical (dotted line: Calculation 1, solid line: Calculation 2) and experimental results (gray circles) for CPs on  $P$  depending on  $W_g$  which corresponds to those in Fig. 4. The gray horizontal dotted line denotes  $P = 74.07\%$ , which is obtained from  $A_{out}/(A_{in-i} + A_{out}) \times 100\%$ .

It is assumed that the time variation of  $N_{out}$  depends on  $\Delta\gamma$  and  $W_g$ , and is expressed by eqn (7).

$$\frac{dN_{out}}{dt} = \left\{ (a_0 + c_0 \Delta\gamma) \left( \frac{N_{in}(t)}{A_{in}(t)} \right) - a_0 \left( \frac{N_{out}(t)}{A_{out}} \right) \right\} W_g \quad (7)$$

where  $c_0$  ( $\text{mm}^2 \text{ s}^{-1} \text{ mN}^{-1}$ ) is a positive constant. The  $c_0$  value was individually estimated using eqn (7) at  $t = 20 \text{ s}$  (see Fig. S4, ESI†). The average value of  $c_0$  was  $844 \pm 287$ . Furthermore, the  $P$  value at each  $W_g$  was numerically calculated using eqn (5)–(7) when  $A_{in}$  was changed from  $4900$  to  $1372 \text{ mm}^2$  at the scan rate of  $dA_{in}/dt = -176.4 \text{ mm}^2 \text{ s}^{-1}$  (Calculation 2).

Fig. 6 shows the numerical results of  $P$  depending on  $W_g$ . The numerical values of  $P$  obtained using eqn (3)–(5) were lower than the experimental values for the CPs (see the dotted line). By contrast, the experimental results for  $P$  of CPs were reproduced well by numerical calculations based on eqn (6) and (7) (see the solid line).  $P$  value obtained using the numerical calculations was higher than that obtained using the experimental results at higher values of  $W_g$  (Fig. 6). Therefore,  $\Delta\gamma$  in eqn (7) was actually lower than that in eqn (6), because  $b_0$  and  $b_1$  were approximately obtained when  $N_{in}$  was constant at eight. However,  $N_{in}$  was actually decreased by scanning the barrier, that is,  $\Delta\gamma$  in eqn (7) had smaller values. These results suggest that the difference in surface tension between  $C_{in}$  and  $C_{out}$  enhances  $P$ . In other words,  $P$  is enhanced by the self-propulsion of CPs in the direction of the higher surface tension. In the present study, no escape panic was observed for CPs because they did not crowd near the gate owing to the repulsive force between them. By contrast, escape panic was observed for MCPs because they crowded near the gate owing to the attractive forces between them.

## 5 Conclusions

In this study, we proposed a novel inanimate evacuation system using self-propelled objects. Self-propelled camphor papers can



escape from  $C_{in}$  to  $C_{out}$  because of the difference in the surface tension between  $C_{in}$  and  $C_{out}$ . Self-propulsion is enhanced to occur in the direction of higher surface tension. As a result, the self-propelled objects move toward the evacuation direction to pass through the gate to  $C_{out}$ . In other words, the difference in the surface tension plays a role of a guidepost in the evacuation. The value of  $P$  as a function of  $W_g$  was determined from the difference in surface tension between  $C_{in}$  and  $C_{out}$ . CPs escaped easily from  $C_{in}$  to  $C_{out}$  because of the repulsive forces among them. By contrast,  $P$  of MCPs was reduced by sticking among MCPs owing to their attractive forces. The present system suggests that self-propelled objects can escape while maintaining an appropriate distance between them. The effects of the attractive and repulsive forces between the objects may be considered in terms of  $c_0$ . These effects will be discussed in the future work.

## Author contributions

Masaki Yoshikai: experiments and analysis, writing and draft preparation; Muneyuki Matsuo: reviewing and editing; Nobuhiko J. Suematsu: reviewing and editing; Hiraku Nishimori: reviewing and editing; and Satoshi Nakata: planning, writing, draft preparation, reviewing and editing.

## Conflicts of interest

There are no conflicts to declare.

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