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## Pulling on grafted flexible polymers can cause twisted bundles

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Bundles of semiflexible polymers can twist at low temperatures to balance energy gain from attraction and energy cost from bending. This raises the question whether twisting can be also observed for bundles of rather flexible grafted polymers stretched out by pulling force. Here, we address this question using Monte Carlo computer simulations of small bundles. Our data show that for weak forces  $F < F_u$ , intertwined globular conformations are favored, whereas for strong forces  $F > F_u$ , rod-like bundles emerge. In the intermediate force window  $F_l < F < F_u$ , bundles with a helical twist can be clearly identified. Applying a field to all monomers yields qualitatively the same effect. This suggests the conclusion that rather flexible polymers under pulling force or field behave effectively like semiflexible polymers without external pull.

### 1 Introduction

A challenging problem in computational physics is the understanding of the fundamental aspects behind aggregation of proteins and polymers. Its significance stems from relevance for a broad variety of research fields, ranging from medicine which shows how well-ordered, yet misfolded proteins can be key to diseases including Alzheimer's, Huntington's or diabetes type II,<sup>1</sup> as well as materials science where geometry and stiffness of polymer bundles can be precisely tuned<sup>2</sup> to design carbon nanotubes<sup>3</sup> or responsive gels with supramolecular polymers.<sup>4</sup>

Bundles are a motif that can often be found in natural and artificial environments. This prevalence does not emerge randomly, as their strength easily surpasses a mere assortment of rods when inter-connected, *i.e.*, usually cross-linked at proper density.<sup>5</sup> Their properties and location in phase space have been extensively studied.<sup>6</sup> Using Monte Carlo simulations of rather rigid worm-like chains with linker-mediated interactions, bundle formation has been found dependent on a critical concentration of cross-linking agents, whereas unbinding happens in a discontinuous transition.<sup>7,8</sup> Similar models have also been investigated regarding the effect of bundling on bending rigidity.<sup>9–11</sup> It should be kept in mind, however, that bundling

aggregation of polymers is certainly not restricted to explicitly cross-linked systems.<sup>12,13</sup> For rather short semiflexible chains grafted to a surface, the combination of sufficient rigidity and adverse solvent-monomer interaction alone yield tower-like micelles.<sup>14</sup> By further research utilizing coarse-grained bead-spring models which rely solely on short-range attraction,<sup>‡</sup> elastic bonds and bending resistance, it has been demonstrated<sup>13,15,16</sup> that the stiffness of semiflexible theta polymers is a distinguishing parameter for distinct emergent structures.

One interesting emergent structure is that of twisted bundles,<sup>17</sup> *e.g.*, in fibril<sup>18</sup> or collagen<sup>19</sup> bundles. The collective twist serves as a general mechanism to regulate a finite equilibrium diameter<sup>20</sup> and can be a result of both chiral or achiral building blocks.<sup>21</sup> Focusing on achiral building blocks, spontaneous twists were shown in computer simulations of assemblies of axially symmetric discoids due to competing length scales<sup>22</sup> or during aggregation of attractive semiflexible chains due to competing energies.<sup>13,23</sup> For this work, the relevant competition is that between energy gain from newly formed Lennard-Jones contacts compared to energy cost from twisting.

Especially relevant for experimental biophysics are polymer systems grafted to a surface, as they must be fixed locally to study their properties by, *e.g.*, atomic force microscopy,<sup>24</sup> optical tweezers or light scattering.<sup>25</sup> The effect of grafting on aggregation has been investigated by employing similar models as above, demonstrating how it altered the aggregation transition between two polymers from discontinuous to continuous without significantly affecting structural properties.<sup>26</sup> Besides grafting, the aforementioned experimental methods often

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<sup>‡</sup> This can be seen as implicit linkage.



require external forces on probed polymers, whose effect on emerging structures and the phase space in total is yet to gauge. Modeling single polymers as self-avoiding random walks on a regular lattice under external force has shown how a strand unravels under increased tension.<sup>27</sup>

The bundling aggregation of multiple polymers under force, however, cannot be predicted as intuitively since the inter-polymeric interactions introduce a distinct layer of complexity.<sup>28</sup> Still, our approximate analytical estimates suggest<sup>29</sup> that sufficiently strong forces  $F$  may direct the monomers of the stretched polymers to positions where the bundles exhibit a helical twist even if the polymers are relatively flexible. This can happen when the monomer positions are such that the energy gain from inter-polymeric interactions outweighs the energy penalty from twisting. For too large forces, however, the bundles will untwist and rod-like bundles result. We thus expect that twisted bundles can be observed in a certain force window  $F_l < F < F_u$ . This heuristic reasoning neglects entropic contributions and, apart from temperature, also the dependence on bending rigidity, polymer length *etc.* are not easy to assess accurately.

With those motivations in mind, this work aims to fill the gap regarding off-lattice simulations of multi-polymer systems under force. By means of Monte Carlo computer simulations we will analyze under which conditions even rather flexible strands can form bundled structures with helical twist when the necessary stretched “upright” figure cannot be supplied by bending stiffness but external force instead, and draw connections between the emerging motifs with respect to both parameters.

The rest of the paper is organized as follows. In Section 2, we first discuss the utilized coarse-grained model and the interactions it is comprised of, the considered observables, and the employed Monte Carlo simulation techniques. In particular the newly devised multi-force method tailored to the problem at hand is explained in some detail. The results are presented in Section 3, illustrating the requirements for twisted bundle formation and how an external force can subvert them. Finally, in Section 4 we summarize our findings and draw the conclusions.

## 2 Model and method

### 2.1 Model

We consider bundles of  $M$  grafted coarse-grained semiflexible polymers of length  $N$  whose monomers are located at positions  $\vec{r}_i^{(j)}$ ,  $i = 1, \dots, N$ ,  $j = 1, \dots, M$  in three-dimensional space. Their first monomers  $\vec{r}_1^{(j)}$  are grafted on the  $xy$ -plane in a specific geometrical pattern (here square and hexagon) depending on the number of polymers  $M$ . Adopting the conventions of ref. 13, we employed a bead-spring model with a finitely extensible nonlinear elastic (FENE) potential

$$V_{\text{FENE}}(r) = -\frac{K}{2} R^2 \ln \left[ 1 - \left( \frac{r - r_0}{R} \right)^2 \right] \quad (1)$$

where  $r = |\vec{b}_i^{(j)}| \equiv |\vec{r}_{i+1}^{(j)} - \vec{r}_i^{(j)}|$  is the actual bond length of the fluctuating chain, *i.e.*, the distance of two neighboring “bonded” monomers of polymer  $j$ . The parameters are chosen as<sup>30,31</sup>  $K = 40$  (spring constant),  $r_0 = 0.7$  (equilibrium bond length), and  $R = 0.3$  such that the maximal possible spring extension is  $r_0 + R = 1.0$  which we thus use as unit of length.

The non-bonded interactions of the monomers are modeled by a truncated and shifted 12–6 Lennard-Jones (LJ) potential ( $r = |\vec{r}_i^{(j)} - \vec{r}_{i'}^{(j')}|$  with  $i' \notin \{i - 1, i, i + 1\}$  if  $j = j'$ )

$$V'_{\text{LJ}}(r) = \begin{cases} V_{\text{LJ}}(r) - V_{\text{LJ}}(r_{\text{cut}}) & \text{if } r \leq r_{\text{cut}}, \\ 0 & \text{if } r > r_{\text{cut}}, \end{cases} \quad (2)$$

with

$$V_{\text{LJ}}(r) = 4\epsilon \left[ \left( \frac{\sigma}{r} \right)^{12} - \left( \frac{\sigma}{r} \right)^6 \right]. \quad (3)$$

This has a minimum at  $r_{\text{min}} = 2^{1/6}\sigma$  where  $V_{\text{LJ},\text{min}} = -\epsilon$ . We do not differentiate between intrachain ( $j' = j$ ) and interchain ( $j' \neq j$ ) interactions and set  $\epsilon = 1$ , which defines the energy scale. We set the monomer diameter  $\sigma = r_0/2^{1/6}$  and the cut-off radius  $r_{\text{cut}} = 2.5\sigma$ . The choice of  $\sigma$  ensures that  $r_{\text{min}} = r_0$  and the constant shift  $V_{\text{LJ}}(r_{\text{cut}}) = -0.0163$  in (2) affects the depth of the potential minimum by less than 2%.

The energies  $E_{\text{FENE}}$  and  $E_{\text{LJ}}'$  result from summing over all  $M(N-1)$  springs and over all possible non-bonded intra- and interchain interaction terms,<sup>§</sup> respectively.

Semiflexibility is introduced for each polymer through the bending potential

$$V_{\text{bend}}(\vartheta) = \kappa \sum_{i=1}^{N-2} (1 - \cos \vartheta_i) \quad (4)$$

where  $\kappa$  is the bending stiffness parameter (measured in units of  $\epsilon$ ) and  $\vartheta_i$  is the angle between consecutive bonds. Suppressing the polymer superscript ( $j$ ) and denoting the bond vector from  $\vec{r}_i$  to  $\vec{r}_{i+1}$  by  $\vec{b}_i = \vec{r}_{i+1} - \vec{r}_i$ ,  $\vartheta_i$  is given by  $\cos \vartheta = \vec{b}_i \cdot \vec{b}_{i+1}$ . Note that in the worm-like chain model where only this energy term is present,  $\kappa$  is directly related to the persistence length  $\ell_p$  which in this case can be defined from the exponential decay of the bond–bond correlations,  $\langle \vec{b}_i \cdot \vec{b}_j \rangle \propto \exp(-|j - i|/\ell_p)$  where  $|j - i|$  is the (intrinsic) distance between two bonds. In the continuum limit of the worm-like chain model ( $\ell_p \gg |\vec{b}_i| \equiv 1$ ), it is well known that  $\ell_p = \frac{\kappa}{k_B T d - 1} = \frac{\kappa}{k_B T}$  in  $d = 3$  dimensions where  $T$  denotes the temperature. With hard-core repulsion as implemented here through the repulsive  $r^{-12}$  term of the LJ potential, however, the bond–bond correlations decay algebraically<sup>32–34</sup> and the relation between  $\kappa$  and  $\ell_p$  provides only an effective guideline.

Finally, we also apply a pulling force  $F$ . Without loss of generality, we graft the polymers on a steric wall in the  $xy$ -plane and apply a perpendicular force in the  $z$ -direction on the last

<sup>§</sup> Due to the employed cutoff at  $r_{\text{cut}} = 2.5\sigma$  their precise number depends on the actual polymer conformations. An obvious upper bound is  $\approx M^2 N^2$ .



monomers of each of the  $M$  polymers. This translates into a potential energy per polymer of

$$V_F = -F(z_N^{(j)} - z_1^{(j)}) \quad (5)$$

where  $z_N^{(j)}$  is the  $z$ -coordinate of the last monomer and  $z_1^{(j)} (= 0)$  the  $z$ -coordinate of the first monomer that is grafted on the  $xy$ -plane of the  $j$ th chain.

Similarly, if a field is exerting a force  $F_i$  on each monomer, the field potential for each polymer is given by

$$V_{\text{field}} = -\sum_{i=2}^N F_i(z_i^{(j)} - z_1^{(j)}) \quad (6)$$

The corresponding energies  $E_{\text{bend}}$ ,  $E_F$ , and  $E_{\text{field}}$  result by summing over all  $M$  polymer chains. Specifically we mainly consider bundles of  $M = 4$  polymers with grafting points on a square with side lengths  $r_0$  and bundles of  $M = 7$  polymers grafted on a hexagonal pattern including the center composed of equilateral triangles with side lengths  $r_0$ .

## 2.2 Observables

The simplest caloric observable is the total energy  $E = E_{\text{int}} + E_{\text{ext}}$  (and its derivatives with respect to force or field and temperature) where

$$E_{\text{int}} = E_{\text{FENE}} + E_{\text{LJ}}' + E_{\text{bend}} \quad (7)$$

is the sum of internal interactions and  $E_{\text{ext}} = 0$  (no force or field),  $E_{\text{ext}} = E_F$  (with pulling force), or  $E_{\text{ext}} = E_{\text{field}}$  (in external field).

To characterize the geometrical properties of the bundles we recorded the end-to-end distances of all polymers  $j = 1, \dots, M$ ,

$$R_{\text{ee}}^{(j)} = |\vec{r}_N^{(j)} - \vec{r}_1^{(j)}|, \quad (8)$$

the average height of their last monomers above the  $xy$ -plane,

$$\bar{z}_N = \frac{1}{M} \sum_{j=1}^M z_N^{(j)}, \quad (9)$$

and the phase-separation parameter,<sup>12</sup>

$$\Gamma^2 = \frac{1}{2M^2} \sum_{j=1}^M \sum_{j' \neq j}^M \left( \vec{r}_{\text{cm}}^{(j)} - \vec{r}_{\text{cm}}^{(j')} \right)^2 \quad (10)$$

where  $\vec{r}_{\text{cm}}^{(j)} = (1/N) \sum_{i=1}^N \vec{r}_i^{(j)}$  is the center of mass of the  $j$ th polymer. We also recorded the average bond length  $\bar{b}$  defined as

$$\bar{b} = \frac{1}{M(N-1)} \sum_{j=1}^M \sum_{i=1}^{N-1} |\vec{b}_i^{(j)}| \quad (11)$$

with the bond vectors  $\vec{b}_i^{(j)} = \vec{r}_{i+1}^{(j)} - \vec{r}_i^{(j)}$  pointing from the  $i$ th to the  $(i+1)$ th monomer of the  $j$ th polymer.

Finally, in order to identify the conjectured helical twist of the bundles quantitatively, it is helpful to include an observable that tracks the angular component directly, *i.e.*, not only by inference *via* extension or spaciousness. From the study of  $\alpha$ -helices (see, *e.g.*, ref. 35–39) it seems convenient to utilize the dihedral angle, which yields the twist of the fourth

monomer with respect to the first around the axis defined by monomers 2 and 3.<sup>40</sup> For our multi-polymer system, we first sum up all  $N-3$  dihedral angles of an individual polymer and then average over all  $M$  polymers yielding the helical twist parameter

$$\phi = \frac{1}{M} \sum_{j=1}^M \sum_{i=1}^{N-3} \text{atan2} \left( \left| \vec{b}_{i+1}^{(j)} \right| \vec{b}_i^{(j)} \cdot \left( \vec{b}_{i+1}^{(j)} \times \vec{b}_{i+2}^{(j)} \right), \right. \\ \left. \times \left( \vec{b}_i^{(j)} \times \vec{b}_{i+1}^{(j)} \right) \cdot \left( \vec{b}_{i+1}^{(j)} \times \vec{b}_{i+2}^{(j)} \right) \right). \quad (12)$$

Here  $\text{atan2}(y, x)$  is a two-argument generalization of the standard trigonometric arctan function that is implemented in many programming languages.<sup>41</sup> It automatically takes care of the possible cases when inverting the tan function.

The sign of  $\phi$  indicates the helical sense of the bundle with + and – representing right- and left-handed twists, respectively. To acquire a sensible equilibrium value of  $\phi$ , we average its absolute value over the available measurements, *i.e.*, consider  $\langle |\phi| \rangle$  which is not influenced by flips of the helical sense. Even though such flips are rare they can occur (see Section 3.2). The magnitude of  $\langle |\phi| \rangle / 2\pi$  corresponds to the average number of turns in each of the  $M$  polymers.

## 2.3 Simulation techniques

To estimate these observables numerically, we performed Monte Carlo computer simulations in the canonical ensemble.<sup>42,43</sup> Here each conformation (microstate) of the  $M$  polymers parameterized by the state-space vector  $\mathbf{x}$  is weighted by the Boltzmann factor  $\exp(-E(\mathbf{x})/k_B T)$  according to the usual expression

$$\langle O \rangle = \frac{1}{Z} \int d\mathbf{x} O(\mathbf{x}) \exp(-E(\mathbf{x})/k_B T) \quad (13)$$

where  $E(\mathbf{x})$  is the corresponding energy of the conformation,  $\beta = 1/k_B T$  is the inverse temperature (or inverse thermal energy), the integral goes over all possible conformations, and  $Z = \int d\mathbf{x} \exp(-E(\mathbf{x})/k_B T)$  denotes the canonical partition function. In the following we use units in which  $k_B = 1$ , corresponding to measuring  $T$  in units of  $\varepsilon/k_B$ .

As usual in Monte Carlo simulations, expectation values  $\langle O \rangle$  are estimated by averages  $O_{\text{av}}$  over many equilibrium conformations,  $\langle O \rangle \approx O_{\text{av}} = (1/n_{\text{meas}}) \sum_{k=1}^{n_{\text{meas}}} O(\mathbf{x}_k)$ , that are recorded after discarding  $n_{\text{equil}}$  conformations for equilibration. Since  $|\langle O \rangle - O_{\text{av}}| \propto 1/\sqrt{n_{\text{meas}}}$  becomes small in long simulations, in order to ease the notation we mostly suppress the conceptual difference between expectation value and its estimator in the following.

**2.3.1 Metropolis Monte Carlo simulations.** In the first set of simulations we employed the very general standard Metropolis Monte Carlo method<sup>44</sup> for sampling the polymer conformations in the canonical ensemble at a given temperature  $T$  and fixed forces (or fields). To update the polymer conformations we applied quite elaborate move sets comprising besides local monomer displacements also non-local moves such as pivot rotations and tail-shift moves. For pivot rotations, we choose a random monomer  $i$  and rotate all following monomers  $i' > i$  around the pivot point  $\vec{r}_i$  by a random angle  $\alpha$ ; for



tail-shift moves, we again choose a random monomer  $i$  and displace all monomers  $i' \geq i$  by a random vector  $\vec{d}$ . Their relative frequencies were chosen to be 70:15:15. Since the optimal amplitudes of these update moves depend on the parameters force, bending stiffness, temperature, *etc.*, we adjusted them before the production runs empirically in shorter test simulations by requiring Metropolis acceptance rates around 0.4. For a recent overview with references to the original literature see, *e.g.*, ref. 45 and 46. With this setup we performed for each parameter set  $(F, \kappa, T, M, N)$  typically  $4 \times 10^7$  sweeps during which we took  $n_{\text{meas}} = 9 \times 10^4$  measurements after an initial equilibration period over  $4 \times 10^6$  sweeps. To improve the statistics of the main results for  $\kappa = 3$ , we further averaged for  $M = 4, 7, N = 13$  over 11 and for  $M = 4, N = 26$  over 16 such runs.

**2.3.2 Multi-force simulation technique.** For the second set of Monte Carlo simulations we devised a special generalized ensemble method that is tailored to the problem at hand. Adapting the idea of multicanonical simulations<sup>47–50</sup> (for a recent review of applications to macromolecules, see ref. 51), the goal of multi-force (MuFo) simulations is to obtain estimates  $O_{\text{av}}$  of expectation values  $\langle O \rangle$  for any given observable  $O$ , *i.e.*,  $\langle O \rangle \approx O_{\text{av}}$ , as a smooth function of an externally applied force.

To understand the working principle of MuFo simulations, let us consider our system of  $M$  polymers of length  $N$  grafted to a flat steric surface. The internal interaction energy  $E_{\text{int}}(\mathbf{x})$  is determined by the full  $M \times N$  dimensional state vector  $\mathbf{x}$ . The external pulling force  $F$ , however, acts only on the last monomer of each of the  $M$  polymers. We can decompose the total energy into an interaction part  $E_{\text{int}}(\mathbf{x})$  and a force contribution  $E_{\text{F}}(\mathbf{x})$  that only depends on the  $z$ -components of the  $M$  end monomers,

$$E_{\text{F}}(\mathbf{x}) = E_{\text{F}}(z_N^{(1)}, z_N^{(2)}, \dots, z_N^{(M)}) = -F \sum_{j=1}^M z_N^{(j)} = -F z_N \quad (14)$$

where  $z_N \equiv \sum_{j=1}^M z_N^{(j)} = M \bar{z}_N$ . This likewise applies also to an external field (that acts on all monomers of each polymer chain), for which one simply needs to replace  $E_{\text{F}}$  with the corresponding  $E_{\text{field}}$ . We can then write the expectation value as

$$\langle O \rangle = \frac{1}{Z} \int d\mathbf{x} O e^{-\beta E_{\text{int}} + \beta F z_N} = \frac{1}{Z} \int d\mathbf{x} O e^{-\beta E_{\text{int}}} e^{\beta F z_N}, \quad (15)$$

where the first term on the r.h.s. is the Boltzmann weight of the monomer-monomer interactions and the second term is a weight factor that changes depending on the applied force and only depends on the end positions of the polymers (the monomers that the pulling force exerts upon).

The trick we can now apply to sample all applied forces at the same time, is to replace the force-related weight with an *a priori* unknown weight function that only depends on the conformational contributions to the force energy, *i.e.*,  $e^{\beta F z_N} \rightarrow W(z_N)$ . One can start from an unbiased weight,  $W(z_N) = 1$  for all  $z_N$ , and sample the histogram  $H(z_N)$  of the sum of polymer end-positions. As in standard multicanonical simulations, we can

then iteratively adapt the weight function, *e.g.*,  $W^{n+1}(z_N) = W^n(z_N)/H(z_N)$ , to obtain samples over all possible  $z_N$ . Importantly, the observables  $O_k = O(\mathbf{x}_k)$  we sample already take care of the temperature weighting if conformation space is sampled ergodically.

Once this weight iteration has converged, which can be quite tedious and time-consuming, we can reweight our samples, *i.e.*, the tuples  $(O, z_N)_k$ , to any force for which the flat histogram covers the canonical distribution. Specifically, the average over measurements (labeled by subscript  $k$ ) is given by

$$O_{\text{av}}(F) = \frac{\sum_k O_k e^{\beta F z_{N,k}} / W(z_{N,k})}{\sum_k e^{\beta F z_{N,k}} / W(z_{N,k})} \quad (16)$$

where  $z_{N,k} = z_N(\mathbf{x}_k)$ , so that once the multi-force weights are determined, we can get estimates of our expectation values for continuous values of the force  $F$ .

Since the simulation setup is completely analogous to standard multicanonical formulations, we easily applied our parallel implementation<sup>52</sup> and ran the simulations on up to 256 cores in parallel, which in addition to accelerating the wall-clock time of the simulation further improves ergodicity and convergence.<sup>53</sup> Specifically, we worked with 64 cores for the  $M = 4$  system and 256 cores for the  $M = 7$  system. On each core, the iteration steps start with a short equilibration of  $50 \times 10^3$  sweeps, where we define empirically one sweep to consist of  $(NM)^{1.5}$  updates randomly choosing between a single-monomer shift and a pivot rotation. During the weight iteration we performed in the  $n$ th iteration step a total of  $1.28n \times 10^6$  sweeps distributed across the cores. The iterations are stopped once the histograms are sufficiently flat and we observed a minimum number of so-called tunnel events. For a tunnel event, one core has to travel from one end of the histogram to the other. In our application, we choose a minimum of 200 (100) tunnel events for  $M = 4$  ( $M = 7$ ). This took 16 iterations for the  $M = 4$  system and 51 iterations for the  $M = 7$  system which gives an idea of the convergence properties of the weight iteration. In the subsequent production run (with fixed weights) we recorded a total of  $2.56 \times 10^6$  measurements with 50 sweeps between measurements, again distributed across the cores. Similarly, this approach can be generalized to tailored non-flat histograms<sup>54</sup> and also to Wang-Landau-type simulations as described in ref. 55.

## 3 Results

### 3.1 Grafted bundles of semiflexible polymers

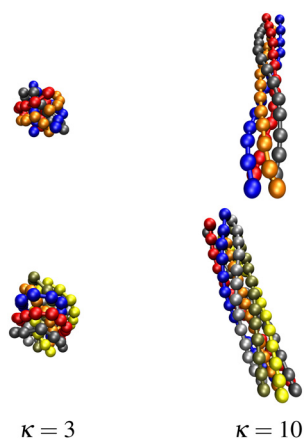
In studies of freely aggregating semiflexible polymer chains that are otherwise unconstrained (*i.e.*, no grafting, no steric surface) we observed for stiffer chains at low temperatures the formation of polymer bundles with a helical twist.<sup>13,15</sup> In another study, we focused specifically on the effects of grafting a single semiflexible polymer (with bending stiffness  $\kappa$ ) to a steric (or attractive) substrate and obtained entire  $\kappa$ - $T$  phase diagrams for different surface attraction strengths.<sup>16</sup>



The additional (persistence) length scale generated by the bending energy of a semiflexible polymer puts rather difficult challenges on the computer simulations and enriches the structural phase diagrams by many new interesting aspects. Lastly, we also investigated the binding transition of two flexible polymers grafted to a steric surface with close-by grafting points.<sup>26</sup> While free polymers show a discontinuous binding transition, grafting to a steric flat surface leads to a continuous transition. A combination of canonical and micro-canonical analyses revealed that the change in transition order can be understood in terms of the reduced translational entropy of the unbound high-temperature phase upon grafting.

Here we extend these considerations by performing systematic Monte Carlo simulations for bundles of  $M$  semiflexible polymers of length  $N = 13$  grafted to a steric flat surface in specific grafting patterns. We mainly concentrated on the cases of  $M = 4$  polymers grafted in a square geometry and  $M = 7$  polymers grafted in a hexagonal (plus the center) geometry, with the grafting points a distance  $r_0 = 0.7$  (the equilibrium spring extension) apart in both cases. As expected we observe a similar behavior as for the freely aggregating polymers studied in ref. 13 and 15. At low temperature ( $T = 0.2$ ) we find for both  $M = 4$  and 7 globular conformations for rather flexible polymers ( $\kappa = 3$ ) whereas for stiffer polymers ( $\kappa = 10$ ) twisted or braided bundles are formed also in the grafted case. For an illustration see the three-dimensional snapshots in Fig. 1.

Note that apart from fixing the overall average distance of the  $M$  polymers due to grafting, we treat the  $xy$ -plane as a steric surface, *i.e.*, the polymers are only allowed to fluctuate in the upper half-space, thus reducing entropic contributions. By varying the bending stiffness and temperature, we find, however, still a very similar  $\kappa$ - $T$  phase diagram as reported in ref. 13 and 15 (as could be anticipated also from our results for a single semiflexible polymer<sup>16</sup>) and therefore refrained from determining the free-energy landscape for the grafted case too.

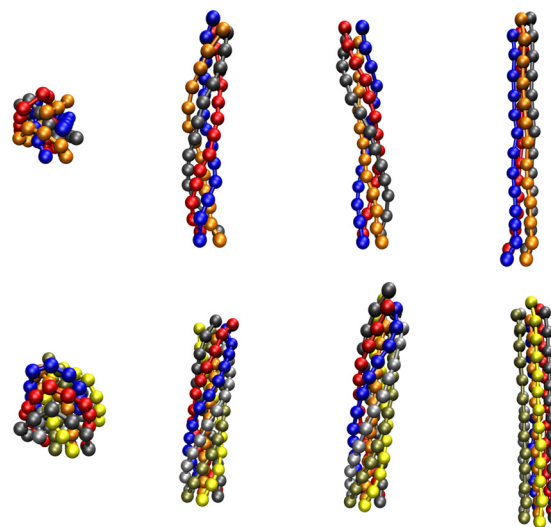


**Fig. 1** Snapshots of bundles of  $M = 4$  (top) respectively 7 (bottom) grafted semiflexible polymers of length  $N = 13$  at temperature  $T = 0.2$  with small bending stiffness  $\kappa = 3$ , forming globules, and strong bending stiffness  $\kappa = 10$ , forming twisted bundles.

### 3.2 Grafted bundles of (almost) flexible polymers under pulling force

While above results for bundles of semiflexible polymers could thus be anticipated to some extent, the next task was much more exploratory: the aim was to test our conjecture that even bundles of rather flexible polymers may exhibit twisted conformations when subject to a pulling force  $F$ . The picture behind this conjecture is that one needs the force to orient the  $M$  polymers on average preferentially along the  $z$ -direction so that the (inter) distances of monomers of different chains are comparable to those in the aggregated phase of rather stiff free polymers or the bundles of rather stiff grafted polymers described above (*cf.* the plots for  $\kappa = 10$  in Fig. 1). Then the interplay of bending and Lennard-Jones energies can be expected to yield twisted bundles as free-energy minimum for rather flexible polymers under pulling force as well. One problem with this picture is that the pulling force  $F$  must be strong enough to achieve a sufficiently well aligned average orientation of the polymers – but must not be too strong to just favor fully stretched parallel rods (“untwisting due to force”). One therefore expects only a certain force window extending from a lower force  $F_l$  to an upper force  $F_u$  within which twisting might be observable, and *a priori* it was not even clear whether this is possible at all (*i.e.*, whether  $F_u > F_l$ ). From an oversimplified linear chain model with monomers connected by harmonic springs with spring constant  $K$ , it is straightforward to calculate the average spring stretching  $\Delta r_{i,i+1} = F/K > 0$  (for each of the springs), from which at least some rough idea of the magnitude of a suitable  $F$  range can be inferred analytically.

While the actual localization required some exploration, we find clear evidence for a force window with twisted bundles of rather flexible polymers ( $\kappa = 3$ ) for low temperatures ( $T = 0.2$ ) where without pulling force one would have found equilibrium



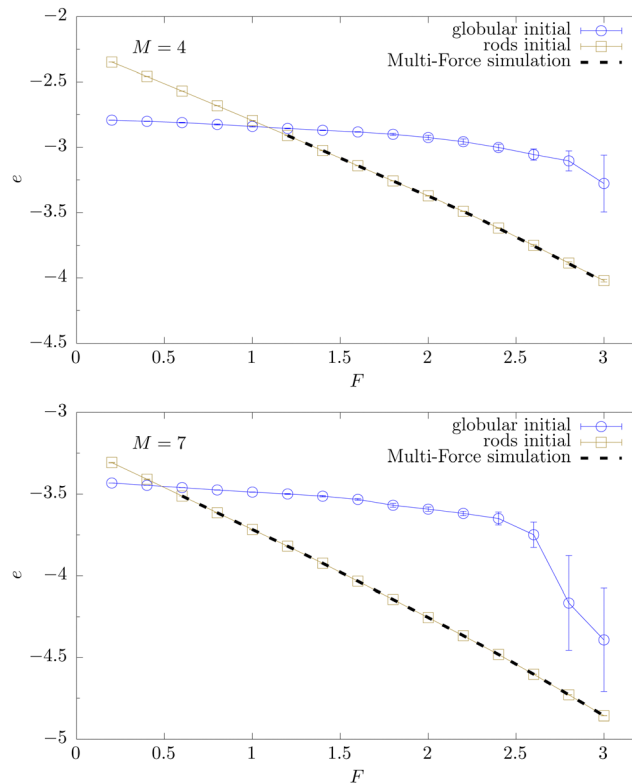
**Fig. 2** Snapshots of grafted bundles of rather flexible polymers with small bending stiffness  $\kappa = 3$  under pulling force  $F$  in  $z$ -direction ( $N = 13$ ,  $T = 0.2$ ). Top: Bundles of 4 polymers for  $F = 0.6$  ( $<F_l \approx 1.1$ ), 1.4, 1.8 ( $<F_u \approx 2.2$ ), 3.0 from left to right. Bottom: Bundles of 7 polymers for  $F = 0.2$  ( $<F_l \approx 0.5$ ), 0.8, 1.8 ( $<F_u \approx 2.3$ ), 3.0.



globular conformations, cf. Fig. 1. This is demonstrated in Fig. 2 where the resulting bundle conformations for both  $M = 4$  and  $7$  are shown. For intermediate forces they clearly exhibit twisted structures reminiscent of the conformations for the case of rather stiff polymers with  $\kappa = 10$  in the grafted case, cf. Fig. 1.

To locate  $F_l$  and  $F_u$  we recorded several observables as a function of  $F$  (which are not all shown here). The simplest is the total energy per monomer  $e = E/NM$  displayed in Fig. 3. The two branches plotted as data points with error bars connected by interpolating lines (labeled “globular initial” and “rods initial”) crossing at  $F_l \approx 1.1$  ( $M = 4$ ) respectively  $F_l \approx 0.5$  ( $M = 7$ ) result from Metropolis simulations initialized with either a globular or rod-like (bundle) conformation. We thus clearly observe strong hysteresis effects, being typical for a first-order-like transition. For forces  $F > F_l$  the Metropolis data agree very well with the black dashed continuous curve obtained by reweighting the MuFo simulations. Since the temperature is chosen to be low ( $T = 0.2$ ), entropy does not matter much and the energy can be considered as a rough approximation of the free energy. We have checked that this re-interpretation does make sense by computing the derivative  $de/dF$  which, with the free-energy interpretation, should give the average position  $\bar{z}_N = (1/M) \sum_{j=1}^M z_N^{(j)}$  of the last monomers, more precisely  $de/dF \approx -\langle \bar{z}_N \rangle / N$ . Comparing with the direct measurements of  $\langle \bar{z}_N \rangle$  in Fig. 4, we obtain indeed good agreement (not shown here). We notice that  $\langle \bar{z}_N \rangle$  exhibits several jumps: a large jump occurs when the system transitions from the globular phase to a twisted bundle. When further increasing the force, there is one more jump for  $M = 4$  towards an extended bundle and two more jumps for the  $M = 7$  system, well signaled by the peaks in the derivative. These discrete changes in the extension are consistent with the idea that columnar packings of spheres “lock in” to certain commensurate helical geometries.<sup>56</sup> The force where  $\langle \bar{z}_N \rangle$  jumps from  $\approx 1$  to  $\approx 7-8$  (corresponding to jumps from  $\langle \bar{z}_N \rangle / r_0 \approx 1-2$  to  $10-11$  in units of the equilibrium bond length  $r_0 = 0.7$ ; for the actual bond lengths see Fig. 6 below) coincides with the crossing point of the two energy branches in Fig. 3 and hence locates the lower end of the force window  $F_l$ .

As is shown by the black dashed lines in Fig. 3 and 4, the more elaborate multi-force simulations agree perfectly with the usual Metropolis simulations at discrete  $F$  values, at least for  $F > F_l$ . To have a means for overcoming the associated free-energy barrier at  $F_l$  was the primary motivation for setting up the “multi-force” simulations in analogy to multicanonical simulations of a temperature-driven first-order transition (such as, e.g., in the two-dimensional  $q$ -state Potts model with  $q \geq 5$ ). However, for the rather strong first-order phase transition between globules and twisted bundles, we run into an unexpected problem: starting from a rod-like state, the flattening of the small  $z_N$  region involves overcoming an “orthogonal” barrier that is not visible (“hidden”) in  $z_N$ . Being in the bundle state, this barrier most likely results from first untwisting the polymers at almost constant  $z_N$  which involves intermediate states that have higher free energy. Note that this “hidden



**Fig. 3** Average total energy per monomer  $\langle e \rangle = \langle E \rangle / NM$  for  $M = 4$  (top) and  $M = 7$  (bottom) as a function of pulling force  $F$  ( $\kappa = 3$ ,  $T = 0.2$ ,  $N = 13$ ). Here and in the following figures, the Metropolis Monte Carlo simulations are initialized either with a globular or rod-like state (data symbols connected by lines to guide the eye). A clear hysteresis behavior is observed. The crossing point of the two energy branches determines the (first-order-like) transition point  $F_l$  ( $\approx 1.1$  for  $M = 4$  and  $\approx 0.5$  for  $M = 7$ ) from the globular state to twisted bundle conformations. The continuous dashed line for  $F > F_l$  shows the results from multi-force simulations combined with reweighting.

barrier effect” is similar to the problem at the condensation–evaporation (and also droplet–strip) transition encountered in multimagnetical simulations of the Ising model below the critical temperature.<sup>57,58</sup> In the present case, the simulation was able to converge without reaching the low-force globule configurations with small  $z_N$ , because starting from an extended bundle, the target range of small  $z_N$  was also achieved by bending the entire bundle by  $90^\circ$ . While this is not the free-energy minimum when comparing to the Metropolis simulations, it is easier to reach for the selected update moves than overcoming the hidden barrier. Since a direct solution of this problem was not apparent, we decided to restrict our analysis of the multi-force simulations to large-force ranges, where the main qualitative result of our work is clearly verified by the good agreement with the independent Metropolis simulations.

Being in the twisted-bundle phase for  $F > F_l$  (cp. the middle snapshots in Fig. 2), with further increasing force one should encounter  $F_u$  where the twisted bundles untwist due to strong pulling force and eventually for  $F > F_u$  form bundles of parallel rods (cp. the rightmost snapshots in Fig. 2). This upper bound  $F_u \approx 2.2$  for  $M = 4$  and  $F_u \approx 2.3$  for  $M = 7$  is less clearly signaled



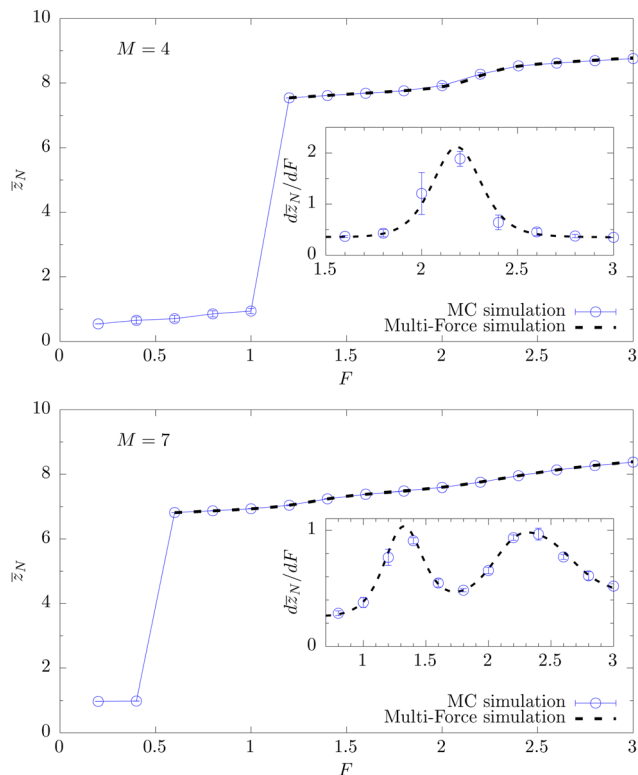


Fig. 4 Average position  $\langle \bar{z}_N \rangle = (1/M) \sum_{j=1}^M \langle z_N^{(j)} \rangle$  of the last monomers for  $M = 4$  (top) and  $M = 7$  (bottom) as a function of pulling force  $F$  ( $\kappa = 3$ ,  $T = 0.2$ ,  $N = 13$ ). The insets show the force derivative  $d\langle \bar{z}_N \rangle/dF$ . To avoid the hysteresis behavior, the Metropolis Monte Carlo runs are initialized below  $F_l$  in a globular state and above  $F_l$  in a rod-like bundle conformation (with  $F_l$  read off from Fig. 3).

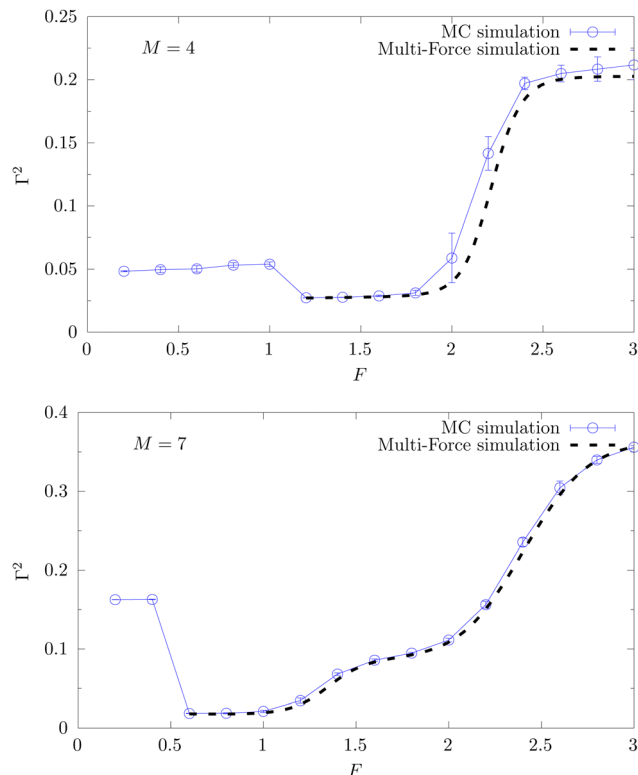


Fig. 5 Average phase-separation parameter  $\langle \Gamma^2 \rangle$  being sensitive to the horizontal distance of the polymers for  $M = 4$  (top) and  $M = 7$  (bottom) as a function of pulling force  $F$  ( $\kappa = 3$ ,  $T = 0.2$ ,  $N = 13$ ). As in Fig. 4 the runs are initialized below  $F_l$  in a globular state and above  $F_l$  in a rod-like bundle conformation.

in  $e$  and  $\langle \bar{z}_N \rangle$  and hence more difficult to locate precisely. Still, there are (weak) signals visible also in these two observables which for  $\langle \bar{z}_N \rangle$  are more clearly reflected by the peaks of the derivative  $d\langle \bar{z}_N \rangle/dF$  shown in the insets of Fig. 4 (peaks at about the same positions are also visible in  $de/dF$ ). This is supported by the phase-separation parameter  $\Gamma^2$ , cf. eqn (10), displayed in Fig. 5. Note that this observable is sensitive to the horizontal distance of the polymers whereas  $d\langle \bar{z}_N \rangle/dF$  reflects their vertical extension. Further related observables (not shown here) confirm this picture. A particularly interesting observation is the weak crossover signal for  $M = 7$  between  $F_l$  and  $F_u$  at around  $F_x \approx 1.3$  corresponding to the first peak of  $d\langle \bar{z}_N \rangle/dF$  in the inset of Fig. 4 (bottom) (and to the related peak in  $de/dF$ ). From the snapshots in Fig. 2 (bottom) we identify this as crossover from a tightly to a loosely twisted state which is what is reflected by the phase-separation parameter  $\Gamma^2$  in Fig. 5 (bottom). On closer inspection of Fig. 3 in our ref. 13 this seems to correspond to the difference of the bundle conformations in the phases  $F_{21}$  and  $F_{22}$  for  $M = 8$  (aggregated semiflexible polymers with  $\kappa \approx 6$ ) which then we did not identify. Note that in ref. 15 such an intermediate crossover as a function of bending stiffness was not observed for  $M = 4$  – and analogously we here as well do not observe such a crossover for  $M = 4$  as a function of force. These observations support our initial conjecture that bundles of

rather flexible polymers subject to pulling force should behave effectively as bundles of rather stiff polymers without force, *i.e.*, force applied to flexible polymers effectively plays a similar role as bending stiffness for semiflexible polymers.

Another interesting, at first sight somewhat counter-intuitive observation is that the average bond length of the chains turns out to be smaller than the equilibrium bond length  $r_0$  for small and intermediate forces, *i.e.*, they are slightly compressed (but less so than for vanishing force), see Fig. 6. Qualitatively this can be explained by the attractive Lennard-Jones potential. For large pulling forces the polymers are stretched into rod-like conformations and the average bond length exceeds  $r_0$ .

We have checked that even for entirely flexible polymers (*i.e.*, vanishing bending stiffness  $\kappa = 0$ ) under external force, the bundling and twisting effect can be observed (one should keep in mind, however, that due to the excluded-volume constraint, *i.e.*, the  $1/r^{12}$  repulsion of the LJ potential, a small effective stiffness is generated). Here we had to choose, however, a lower temperature  $T = 0.1$  for which representative conformation snapshots are displayed in Fig. 7. One clearly observes a helical twist, but for  $\kappa = 0$  the twist is less pronounced and the force window  $[F_l, F_u]$  where twisting happens is much smaller than for  $\kappa = 3: 2.7 \lesssim F \lesssim 2.9$  for bundles of  $M = 4$  polymers and a slightly wider range of  $2.4 \lesssim F \lesssim 2.8$  for  $M = 7$ .



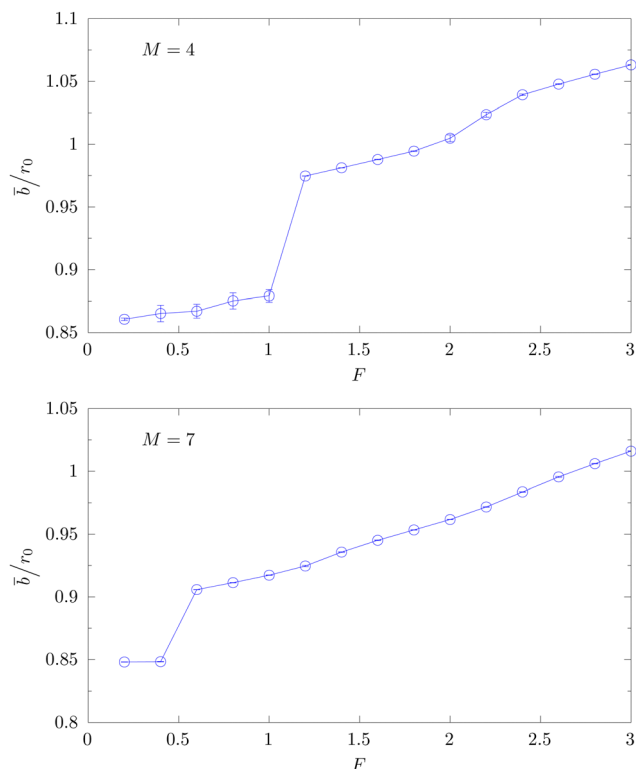


Fig. 6 Average bond length for  $M = 4$  (top) and  $M = 7$  (bottom) as a function of pulling force  $F$  ( $\kappa = 3$ ,  $T = 0.2$ ,  $N = 13$ ), where  $r_0 = 0.7$  is the equilibrium bond length. As in Fig. 4 the runs are initialized below  $F_1$  in a globular state and above  $F_1$  in a rod-like bundle conformation.

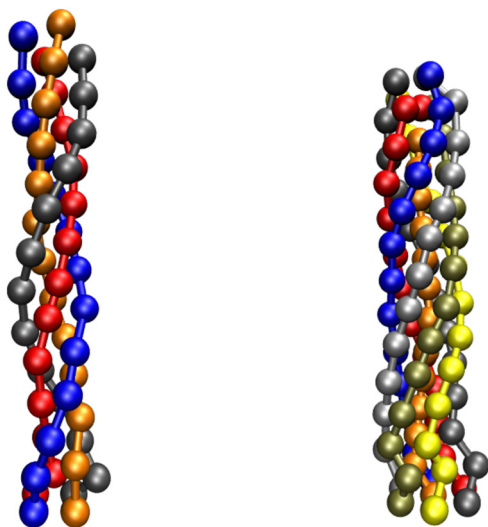


Fig. 7 Snapshots of grafted bundles of flexible polymers with vanishing bending stiffness  $\kappa = 0$  under pulling force  $F$  in  $z$ -direction ( $N = 13$ ,  $T = 0.1$ ). Left: Bundle of 4 polymers for  $F = 2.8$  featuring a helical twist in the rather small force window  $F_1 < F < F_u$  with  $F_1 \approx 2.7$ ,  $F_u \approx 2.9$ . Right: Bundle of 7 polymers for  $F = 2.6$ . Here the force window for twisting is slightly wider with  $F_1 \approx 2.4$ ,  $F_u \approx 2.8$ .

In addition we have also checked that the twisting effect remains stable for longer polymers by doubling the number of

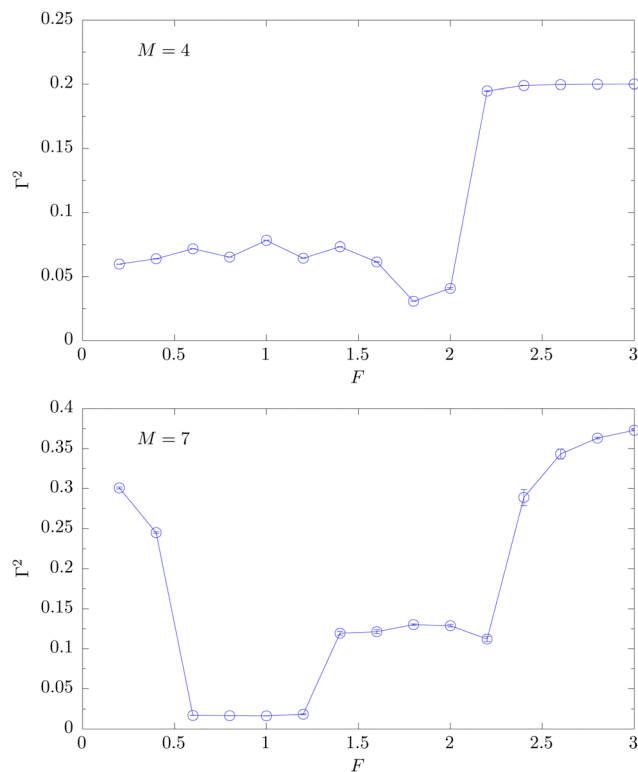
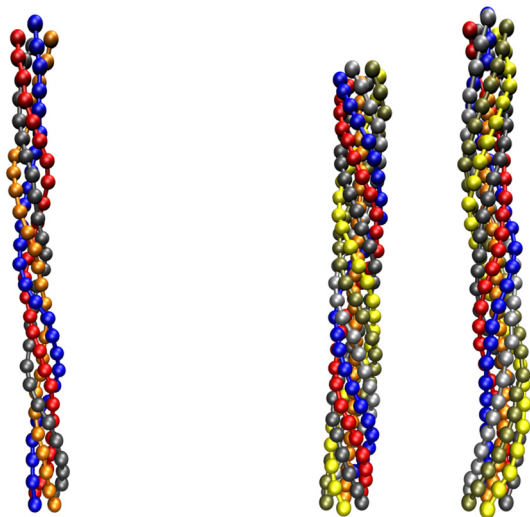


Fig. 8 Average phase-separation parameter  $\langle \Gamma^2 \rangle$  for bundles of  $M = 4$  (top) and  $M = 7$  (bottom) rather flexible polymers of length  $N = 26$  as a function of pulling force  $F$  ( $\kappa = 3$ ,  $T = 0.2$ ). As for  $N = 13$  the runs are initialized below  $F_1$  in a globular state and above  $F_1$  in a rod-like bundle conformation.

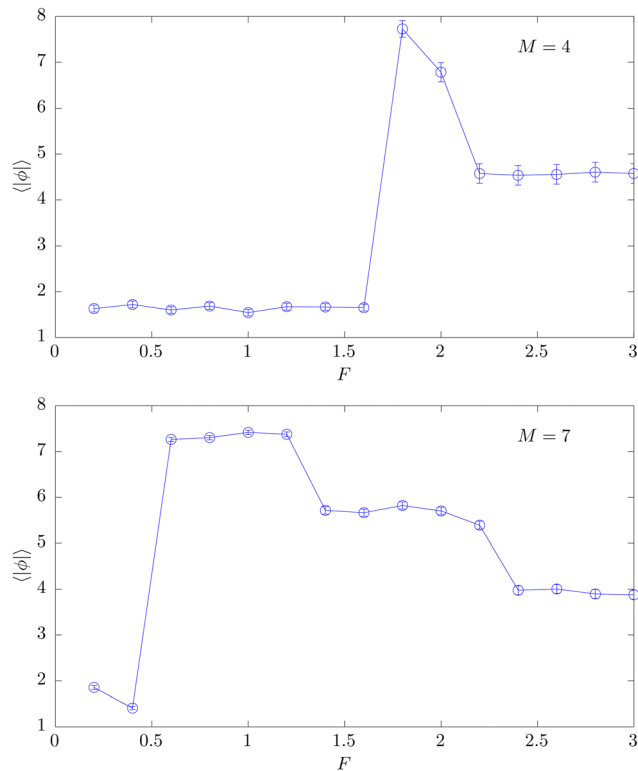
monomers to  $N = 26$ . From the phase-separation parameter shown in Fig. 8 for temperature  $T = 0.2$  one reads off that for bundles of  $M = 4$  rather flexible polymers with  $\kappa = 3$  the transition from globular conformations for small forces to twisted bundles happens much later than for  $N = 13$  at around  $F_1 \approx 1.7$ – $1.8$  while the transition to rod-like bundles for large forces still happens at  $F_u \approx 2.2$  as for  $N = 13$ , cf. Fig. 5. This yields a smaller but still sizeable force window for observing twisted bundles. That bundles with helical twist are indeed the predominant conformations in this force window is demonstrated by the snapshot displayed in Fig. 9. Bundles of  $M = 7$  polymers of length  $N = 26$  behave very similar to those of length  $N = 13$ . As for  $N = 13$ , here the force window for twisted bundles (with  $\kappa = 3$ ,  $T = 0.2$ ) also extends from about  $F_1 \approx 0.5$  to  $F_u \approx 2.2$ , albeit with sharper transition signals, cp. again with Fig. 5. In particular the signal for the crossover from tightly twisted to loosely twisted bundles at about  $F_x \approx 1.3$  is much more pronounced. This crossover is also clearly reflected in the snapshot configurations shown in Fig. 9 which also reveal that for  $N = 26$  one observes about one-and-a-half helical twists instead of only about one for  $N = 13$ . As a final comment we remark that within the worm-like chain approximation, one would estimate a persistence length of  $\ell_p = \kappa/k_B T = 3/0.2 = 15$ . A plausible explanation is thus that for rather flexible polymers, e.g., with small bending stiffness  $\kappa = 3$ , about one helical twist occurs over one persistence length.





**Fig. 9** Snapshots of grafted bundles of rather flexible polymers of length  $N = 26$  with small bending stiffness  $\kappa = 3$  under pulling force  $F$  in  $z$ -direction at temperature  $T = 0.2$ . Shown are from left to right a bundle of 4 polymers for  $F = 1.8$  at the left margin of the force window for twisting from  $F_l \approx 1.7$ – $1.8$  to  $F_u \approx 2.2$  and two bundles of 7 polymers for  $F = 0.8$  (tightly twisted) and  $F = 1.6$  (loosely twisted). Here the force window for twisting extends over a wider range from  $F_l \approx 0.5$  to  $F_u \approx 2.2$  with a crossover from tightly to loosely twisted bundles at  $F_x \approx 1.3$ .

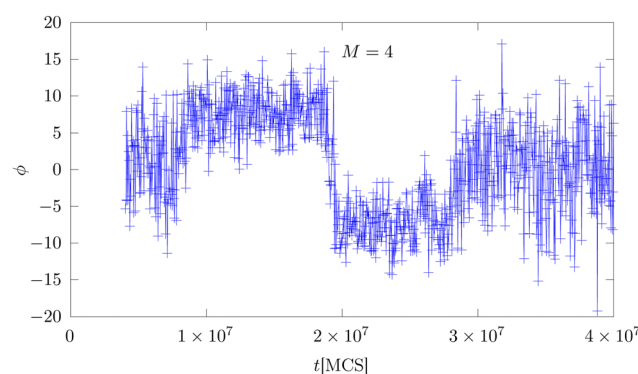
After these qualitative checks of the persistence of the observed effects for longer chains, we have also performed a more quantitative analysis of several aspects regarding the helical twist by employing the average sum of dihedrals  $\phi$  defined in eqn (12), which is sensitive to both its magnitude and sense. In Fig. 10 we present the absolute value of  $\phi$  averaged over the time evolution of the measurements. Overall the two curves for  $M = 4$  and  $M = 7$  nicely reflect the different conformations with respect to both the position and type of phases already signaled by the phase-separation parameter  $\Gamma^2$  shown in Fig. 8. Particularly for four polymers, it demonstrates the usefulness of this observable for the conformational analysis of our model. Here the peak around  $F \approx 1.5$ – $2$  features a strong signal of the twisted bundle motif. Also in the globular and rod-like phases some remaining weaker twist is reflected, but the signals are much less pronounced. The corresponding signals given by  $\Gamma^2$  are less clearly distinguished, albeit still discernible. For  $M = 7$ , the change in the bundle structure at  $F_x \approx 1.3$  from tightly to loosely twisted bundles is reflected with a comparatively high signature as these two phases are not only distinguished by their density, as suggested by the phase-separation parameter, but also by a larger angular sum of dihedrals for the tightly twisted bundles around their primary axis given by the vertical force. This step-wise change in the helical twist is consistent with the previously noted step-wise increase in the extension (*cf.* Fig. 4) and further supports the intuitive picture that the helical twist is a result of optimized packing<sup>29</sup> that results from distinct combinations of bundle diameter and extension.<sup>56</sup> It can be expected that with infinite force, *i.e.*, absolutely vertical polymers, the value of  $\langle |\phi| \rangle$



**Fig. 10** Average of the absolute helical twist parameter for  $M = 4$  (top) and  $M = 7$  (bottom) for  $N = 26$  as a function of pulling force  $F$  ( $\kappa = 3$ ,  $T = 0.2$ ).

converges to zero. Similarly, owing to their undirected nature, the sum of dihedral angles of globular structures should equally settle at zero in the limit of infinite polymer length  $N$ .

Besides the quantification of the magnitudes of the helical twist, it is also interesting to study the twist orientation, *i.e.*, the handedness, as well as its preparation and bias dependences. This can be accomplished by regarding the time series of  $\phi$  while conserving its sign. In Fig. 11 one sees that the twist direction can be subject to stark variation if the force is in the vicinity of the transition to untwisting.



**Fig. 11** Time series of the helical twist parameter  $\phi$  for  $M = 4$ ,  $N = 26$  at  $F = 2.0$  ( $\kappa = 3$ ,  $T = 0.2$ ).



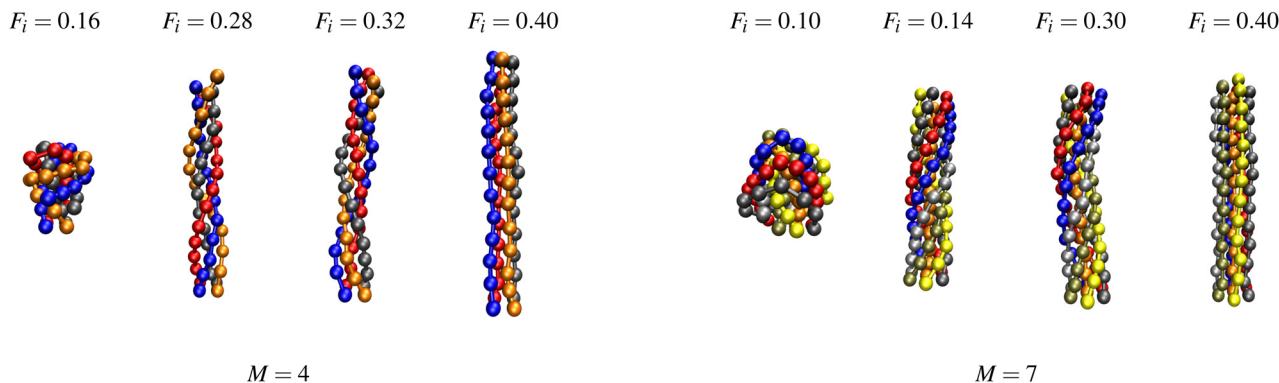


Fig. 12 Snapshots of bundles of rather flexible grafted polymers with small bending stiffness  $\kappa = 3$  in an external field  $F_i$  in  $z$ -direction ( $N = 13$ ,  $T = 0.2$ ).

In fact, 14 of 16 initializations of  $M = 4$  at  $F = 2.0$ , *i.e.*, the far right end of the bundle's force window for twisting, have exhibited such changes over the course of the simulation. This also demonstrates that the energy barrier separating bundles from rods is far lower than between bundles and globules, which is quite intuitive given the hidden barrier discussed earlier, while the untwisting of bundles into rods can be accomplished geometrically easier with growing  $F$ . And if the force is not yet strong enough to keep the polymers at a firmly stretched conformation, they will occasionally recede into helices with arbitrary sense, as visualized in Fig. 11 for  $M = 4$  at  $F = 2.0$ , where the system changes from right-handedness ( $\phi > 0$ ) *via* rods ( $\phi = 0$ ) to left-handedness ( $\phi < 0$ ) until settling for rods again. With seven polymers, a similar behavior has not been observed, as the system exhibits bundles until  $F = 2.2$  and yields rods thereafter. Our numerical measurements suggest that inside the twisted bundle phase the chirality is stable. If one were to manipulate the system to set it up for a certain helical sense, this should be feasible with rather little effort, although the precise extent of the necessary bias has yet to be investigated.

### 3.3 Grafted bundles of (almost) flexible polymers in external field

As a final step we also briefly explored the case of an external field where a constant force  $F_i = \text{const}$  acts on each monomer  $i = 2, \dots, N$  ( $i = 1$  labels the grafted monomers). From the harmonic chain model one readily concludes that in this case the spring stretching is given by  $\Delta r_{i,i+1} = \sum_{k=i}^N F_k / K$ , so that the magnitude of  $F_i$  should be roughly in the range  $F/N$ , *i.e.*, the  $F_i$  relevant for the "twisting window" should be considerably smaller than the corresponding values  $F$  of the pulling force acting only on the last monomers of each chain labeled with  $i = N$ . This is indeed the case as illustrated by the snapshots in Fig. 12.

## 4 Conclusion

Studying grafted polymer bundles consisting of 4 respectively 7 polymers grafted in a square respectively hexagonal (including

the center) pattern on a flat steric surface in the  $xy$ -plane, the main outcome of our Monte Carlo simulations is two-fold. First, by considering semiflexible polymers we find in both cases basically the same behavior as for the aggregation of free semiflexible polymers studied earlier:<sup>13</sup> For low temperature and small bending stiffness, intertwined globular states form, whereas for sufficiently large bending stiffness, we again observe bundles with a helical twist. Second, we confirmed our theoretical conjecture that even rather flexible grafted polymers may be driven into twisted bundles by applying to the last monomer a pulling force orthogonal to the grafting plane. This indeed happens for both considered grafting patterns in an intermediate force regime. If the force is too weak, the polymers are not sufficiently stretched to gain from the attractive Lennard-Jones contacts and upon lowering the temperature globular states form. On the other hand, if the force is too strong, the polymers are so strongly stretched that they simply form bundles of parallel rods at low temperature. This behavior of rather flexible grafted polymer bundles under pulling force is most clearly reflected by the helical twist parameter  $\langle |\phi| \rangle$  which directly signals the helical twist of the polymer bundles by a pronounced increase of the sum of dihedral angles in the intermediate force region.

Besides performing standard Metropolis Monte Carlo simulations at discrete values of the force, we also devised a multi-force approach, a generalization of multicanonical simulations that is tailored to generating a flat distribution of the  $z$ -coordinates of the last monomers (for polymers grafted in the  $xy$ -plane). This allows one to compute any observable as a continuous function of force. While this aspect works well, another goal of multi-force sampling, namely overcoming the free-energy barrier at the transition from a twisted bundle to a globular state, was not achieved with our current implementation. The probable reason is that this "twisted/untwisted" barrier is parameterized in an "orthogonal" direction not encoded in the multi-force approach. Possible work-arounds are conceivable but would require extensive developments that are left for future work.

Finally, we also checked that with an external field in  $z$ -direction interacting with all monomers of rather flexible grafted polymers, the same twisting effect can be achieved as



for a pulling force applied to their last monomers. The emerging qualitative picture is that grafted bundles of rather flexible polymers subject to pulling force or field behave with increasing pulling strength like bundles of grafted or free semiflexible polymers (without force or field) with increasing bending stiffness. This supports our initial conjecture and we conclude that, as far as the twisting effect is concerned, force or field applied to flexible polymers effectively plays a similar role as bending stiffness for semiflexible polymers.

## Conflicts of interest

There are no conflicts to declare.

## Acknowledgements

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