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## Critical insights into eutectic molten hydroxide electrolysis for sustainable green hydrogen production

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In addressing global energy demands, the focus on hydrogen gas production from renewable sources intensifies. This research review investigates hydrogen production via steam splitting using eutectic molten hydroxide ( $\text{NaOH}-\text{KOH}\%$ ) electrolysis, a promising solution for escalating energy needs. A pivotal aspect involves developing a novel reference electrode for eutectic molten hydroxide, enveloping  $\text{Ni}/\text{Ni(OH)}_2$  with an alumina or mullite tube ionic membrane. The mullite-covered electrode proves stable and reusable from 225 to 300 °C, showcasing a novel advancement in electrochemical stability. Compared to silver and platinum quasi-reference electrodes, the designed reference electrode demonstrates superior stability and efficacy in controlling the platinum working electrode, marking a significant innovation. Moreover, an intriguing cyclic voltammetry study examines different working electrodes, including Ni, Pt, Ag, Mo, and stainless steel (SS) in eutectic molten hydroxide at different temperature conditions. The observed reduction potential for hydrogen evolution follows the order: Ni > Pt > Ag > SS > Mo, corroborated by chronoamperometry, underscoring the reliability of the findings. In the pursuit of high-temperature eutectic molten hydroxide electrolysis to split steam into hydrogen fuel, cathodes of nickel, platinum, and stainless steel are deployed alongside stainless steel and graphite anodes. Operating within the temperature range of 225 to 300 °C and applying voltages ranging from 1.5 to 2.5 V, stainless steel as an anode yields impressive current efficiencies at 300 °C: 90.5, 80 and 68.6% for nickel, stainless steel, and platinum cathodes, respectively. This study positions steam splitting via molten hydroxides as a promising alternative for hydrogen production, poised for integration with renewable energy sources, marking a transformative step in sustainable energy practices.

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### 1. Introduction

The rapid industrialization of the last century, driven by the widespread use of fossil fuels, has brought about unprecedented development. However, the consequential rise in greenhouse gas pollutants, including  $\text{CO}_2$ ,  $\text{N}_2\text{O}$ , and  $\text{SO}_2$  from burning fossil fuels, has prompted growing environmental concerns.<sup>1</sup> In recent years, the quest for alternatives has intensified, with a particular focus on hydrogen gas production. Hydrogen is acknowledged as a highly efficient and environmentally friendly fuel, offering significant promise for the future. Unlike conventional fossil fuels, hydrogen has the potential to drastically reduce air pollution, making it a vital contender for a variety of purposes like transportation, heating, and generating power.<sup>2</sup> Despite the challenges encountered in hydrogen fuel production, it emerges as a viable solution to address the issue of greenhouse gas emissions detrimental to the environment. Consequently, hydrogen is positioned to significantly impact the future energy sector, addressing the increasing global demand.<sup>3</sup>

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The sources of hydrogen, ranging from non-renewable ones like hydrocarbons to renewables such as hydropower, solar, wind, and biomass, offer diverse options for production.<sup>4</sup> Terlouw *et al.*<sup>5</sup> emphasize the possibility of substantial reductions in harmful emissions by generating hydrogen from renewable sources. The operational measure of the hydrogen production setup is outlined as one kilogram of hydrogen at 80 bar pressure, guaranteeing a purity surpassing 99.9%. This metric is derived from an average reference flow of 10 tons of production and storage of hydrogen per day.<sup>6</sup> Electrolysis, leveraging water as a pristine and environmentally friendly energy source, stands as the foremost method for hydrogen generation, offering exceptional purity in its output, viable for applications ranging from small-scale to large-scale operations. However, challenges arise as electrolysis may contribute to CO<sub>2</sub> emissions if non-renewable energy resources power the necessary electricity generation. Additional advancements are required to enable the commercialization of this clean energy approach for hydrogen gas production as fuel, necessitating materials capable of withstanding challenging operating conditions within electrolysis cells.<sup>7</sup> Addressing the imperative to mitigate global warming necessitates an alternative fuel that is affordable, user-friendly, clean, and emits minimal greenhouse gases. Hydrogen emerges as a promising alternative, aligning with the criteria for an ideal fuel due to its potential benefits.<sup>8</sup>

Hydrogen functions as an energy carrier with high efficiency, emitting minimal to zero emissions during utilization, thus playing a pivotal role in combating global warming. Despite its environmental advantages, challenges persist, particularly in ensuring safety throughout production, storage, and transportation.<sup>9</sup> Understanding key metrics such as the hydrogen concentration (measured at 15% during storage conditions at 20 MPa pressure and room temperature), global warming potential (GWP), nitrogen oxide emissions, and acidification potential is crucial for evaluating its environmental impact. The GWP is equivalent to 0.058 kg CO<sub>2</sub> eq. per kW per h, with nitrogen oxide emissions measured at  $7.04 \times 10^5$  NO<sub>2</sub> eq. per kW per h and acidification potential at  $3.63 \times 10^4$  kg SO<sub>2</sub> eq. per kW per h. These metrics provide valuable insights into hydrogen's broader implications and guide efforts toward sustainable energy practices.<sup>9</sup> In fuel cells, hydrogen reacts with oxygen, yielding energy and producing only water as a by-product. Unlike readily available fuels like coal and hydrocarbons, hydrogen exists as a compound in water, fossil hydrocarbons, and biomass products.<sup>10</sup>

Addressing economic concerns within the hydrogen fuel industry, efficient and affordable storage and distribution remain pivotal.<sup>11</sup> Whether produced in small-scale local plants or large-scale central plants, hydrogen gas can be stored and transported as gaseous hydrogen, liquid hydrogen, or metal hydrides.<sup>12</sup> The transportation of hydrogen involves three main routes. First, pipelines similar to those used for natural gas provide a convenient means of delivery, constructed from materials like low-carbon steel, aluminium, or brass.<sup>13</sup> Second, large-scale storage tanks, akin to those for natural gas, facilitate storage. Gaseous hydrogen can also be stored in cylinders for small-scale operations, often at high pressures ranging from 20 MPa to 80 MPa for

industrial use.<sup>13</sup> Liquid hydrogen (LH<sub>2</sub>), with a low density of 70.8 kg/cm<sup>3</sup> and a boiling point of  $-252.3$  °C, requires extremely low temperatures for storage.<sup>14</sup> Cryostats are employed for this purpose, although the associated conversion and maintenance costs make this method more suitable for aircraft than road vehicles. Finally, certain metal alloys offer an alternative for storing hydrogen.<sup>15</sup> These alloys absorb hydrogen gas reversibly, forming metal hydrides, presenting a unique approach to hydrogen storage.

Embarking on a journey at the intersection of innovation and sustainability, this research review delves into the realm of hydrogen gas production through a lens of unprecedented possibilities. Driven by concerns over environmental impact and the ever-increasing demand for clean energy, the focus shifts towards the electrochemical process of splitting steam for hydrogen production *via* eutectic molten hydroxide electrolysis. This exploration is not merely a scientific pursuit; it is a quest to redefine our energy landscape. Imagine a novel reference electrode, a stable companion crafted from the fusion of Ni/Ni(OH)<sub>2</sub> and an ionic membrane. Picture the efficient working electrodes Ni, Pt, Mo, Ag, and stainless steel each revealing its unique prowess in the intricate process of hydrogen evolution. This review aspires to unravel the mysteries of cyclic voltammetry, chronoamperometry, and two-electrode electrolysis within the dynamic environment of eutectic molten hydroxide, where process variables such as applied voltage, electrode material, and molten salt temperature shape the narrative of clean energy production. From the physical measurement of hydrogen gas using water displacement to the theoretical calculations echoing Dalton's law for gases. Through meticulous exploration and theoretical contemplation, this review sets out to redefine the boundaries of hydrogen gas production, laying the groundwork for a sustainable energy future. This review transcends the ordinary, unlocking the secrets that propel us toward a cleaner, brighter tomorrow.

## 2. Hydrogen production technologies overview

In response to the pressing demand for sustainable energy solutions, the landscape of hydrogen production undergoes a transformative evolution, embracing diverse methodologies each laden with distinct promises and challenges. Anchored in history, Alkaline Electrolysis has evolved into a globally acknowledged technology,<sup>16</sup> employing liquid alkaline electrolytes to yield hydrogen efficiently.<sup>17</sup> Solid oxide electrolysis cells (SOECs), functioning at elevated temperatures,<sup>18</sup> represent a robust approach, marked by recent advancements in hybrid configurations.<sup>19</sup> The emergence of proton exchange membrane electrolysis (PEM) signifies a paradigm shift, leveraging solid polymer electrolytes to elevate performance and efficiency standards.<sup>20</sup> Ambitiously harnessing sunlight for water splitting, photo-electrolysis navigates challenges on the path to viability.<sup>21</sup> Thermochemical Water Splitting strategies, relying on intricate high and low-temperature chemical reactions, set the course for large-scale, sustainable hydrogen production.<sup>22</sup>




**Table 1** Comparative analysis of hydrogen production technologies with operating conditions, efficiency, challenges and environmental impacts

Electrolysis method	Operating conditions	Efficiency	Challenges	Noteworthy advancements	Reference
Alkaline electrolysis	Immerging two electrodes in a liquid alkaline electrolyte (e.g., 20–30% KOH), typically below 100 °C	Up to 70%	Diaphragm limitations, restricted current density, hindered high-pressure operation	Low-temperature electrochemical water splitting with high efficiency even at 100 °C, low-cost nickel alloy electrocatalysts, insights from magnetic properties, shaping the design of highly efficient electrocatalysts	17 and 23
Solid oxide electrolysis cells (SOECs)	Leveraging steam at elevated temperatures (750–1000 °C)	Hybrid-SOEC with a current per unit area of 3.16 A/cm <sup>2</sup> at 750 °C and 1.3 V	Temperature-dependent efficiency, cation removal challenges	The hybrid-SOEC with BaZr <sub>x</sub> Ce <sub>0.7</sub> Yb <sub>0.1</sub> O <sub>3-δ</sub> electrolyte, no performance decline over 60 hours of uninterrupted operation	24 and 25
Proton exchange membrane electrolysis (PEM)	Solid polymer electrolyte (e.g., Nafion), effective proton conductivity at around 80 °C	50–70%	Gas crossover reduction, compact system design	Introduction of solid polymer electrolytes, a significant departure from traditional methods	26
Photo-electrolysis	Harnessing sunlight to separate water into hydrogen and oxygen, typically at 20 °C to 30 °C	Photo-current density of 4.30 mA/cm <sup>2</sup> , stability demonstrated over 70 hours in seawater splitting	Challenges in yield and efficiency, economic viability	A durable photo-electrode layout featuring an ultra-stable PEC cell with a BiVO <sub>4</sub> photo-anode and a MoO <sub>3</sub> barrier layer, ensuring stable and efficient hydrogen production from seawater	27
Thermochemical water splitting	Converting water into hydrogen and oxygen <i>via</i> high-temperature endothermic (500 °C to 1800 °C) and low-temperature exothermic processes	Potential for sustainable, large-scale hydrogen generation	Energy and exergy efficiency variations, design challenges	Favourable assessment of sulfur-iodine and hybrid sulfur cycles, achieving approximately 77% efficiency	28
Eutectic molten salt electrolysis	Voltage range: 1.5–2 V Temperature range: 225–475 °C Electrolyte: titanium cathode, graphite anode	59.30% (molten chloride), 87.70% (molten hydroxide), 99% (molten carbonate)	Variable product rates, CO <sub>2</sub> conversion varies with molten electrolyte type	Longer-chain hydrocarbons are exclusively produced within molten carbonates at 1.5 V. Promising for sustainable hydrocarbon fuel production, providing a foundation for fundamental investigations. Adequate heating values of produced fuels for subsequent applications	29

Within this dynamic landscape, water electrolysis, though not mainstream, emerges as a beacon of simplicity, reliability, and environmental friendliness.

As we embark on an in-depth exploration detailed in Table 1, a critical analysis unfolds, shedding light on nuanced operating conditions, efficiency benchmarks, persistent challenges, and noteworthy advancements. Notably, Eutectic Molten Hydroxide Electrolysis stands out, offering compelling advantages in energy efficiency and cost-effectiveness, presenting a viable option for hydrogen production. Beyond these merits, it showcases the ability to convert  $\text{CO}_2$  into hydrocarbons, presenting a sustainable solution for fuel production. However, this method is not without limitations, involving reduced production rates, specific electrode material demands, increased production expenses, decreased durability, and heightened energy consumption. The ensuing sections delve into a comprehensive study of the novelty and performance of Eutectic Molten Hydroxide in the intricate landscape of hydrogen production methods.

## 2.1. Advancements in small organic molecule electrolysis

In addition to water electrolysis, small organic molecule electrolysis, such as methanol electrolysis and urea electrolysis, has shown significant advancements. Recent studies have demonstrated remarkable progress in green hydrogen fuel production using these methods. The research on MoP-NC nanosphere-supported Pt nanoparticles showcases significant improvements in methanol electrolysis,<sup>30</sup> with the Pt/MoP-NC catalyst achieving a peak current density of  $90.7 \text{ mA/cm}^2$  for methanol oxidation, 3.2 times higher than commercial Pt/C catalysts. It also exhibits excellent hydrogen evolution reaction (HER) performance with a low overpotential of 30 mV to achieve  $10 \text{ mA/cm}^2$ , reducing energy consumption by about 60%. Similarly, the Pt-CoTe/NC catalyst shows a peak current density of  $102.2 \text{ mA/cm}^2$  for methanol oxidation and a small overpotential of 28 mV for HER,<sup>31</sup> significantly lowering the cell potential required for methanol electrolysis compared to water electrolysis. The integration of Pt and CoSe<sub>2</sub> in another study further enhances catalytic activity and durability for methanol and ethanol electro-reforming, with peak current densities reaching  $87.61 \text{ mA/cm}^2$  for methanol and  $48.27 \text{ mA/cm}^2$  for ethanol, demonstrating high stability and efficiency.<sup>32</sup>

Additionally, the NiS<sub>2</sub>-MoS<sub>2</sub> hetero-nanorods catalyst, leveraging high valence state Ni and Mo synergism, exhibits a current density of  $103.41 \text{ mA/cm}^2$  at 1.54 V for urea-assisted water electrolysis, reducing the cell potential by 224 mV compared to general water electrolysis.<sup>33</sup> Another promising catalyst, the 15% Ni/ZrO<sub>2</sub> synthesized *via* the wetness impregnation method, shows high conversion rates of methane (62.9%) and carbon dioxide (64.9%) in the dry methane reforming (DRM) process at 750 °C with a gas hourly space velocity (GHSV) of  $72\,000 \text{ mL h}^{-1} \text{ g}_{\text{cat}}^{-1}$ , indicating its potential for efficient hydrogen production with enhanced stability.<sup>34</sup> The NiSe<sub>2</sub>/MoSe<sub>2</sub> heterostructured catalyst demonstrated optimized interfacial electron redistribution and enhanced urea adsorption energies,<sup>35</sup> achieving a current density of  $10 \text{ mA/cm}^2$  at

a potential of 1.33 V for urea oxidation, and requiring a cell voltage of only 1.47 V for the urea–water electrolyzer to drive  $10 \text{ mA/cm}^2$ , highlighting significant energy savings.

In line with these advancements, the conversion of formaldehyde (HCHO) using a direct formaldehyde fuel cell achieved remarkable results, with a selectivity greater than 99% and a faradaic efficiency of 200%. Similarly, methanol (CH<sub>3</sub>OH) co-electrolysis with water demonstrated a promising reaction potential of approximately 1.3 V *vs.* RHE, producing hydrogen and formate with a faradaic efficiency exceeding 95%. The co-electrolysis of urea (CO(NH<sub>2</sub>)<sub>2</sub>) and water also showed significant potential, resulting in the production of hydrogen and carbon monoxide with a reaction potential of around 1.3 V *vs.* RHE. Moreover, the use of nickel-based catalysts, such as Ni(OH)<sub>2</sub>, significantly enhanced the electro-oxidation of methanol, achieving a current density increase of 8.2 times when modified with platinum (Pt).<sup>36</sup> These results collectively underscore the potential for efficient and sustainable hydrogen and value-added chemical production using small organic molecules, while maintaining high selectivity and energy efficiency.

## 2.2. Electrolysis mechanism and catalyst material evolution

The water electrolysis process, fundamental for hydrogen production, involves splitting water molecules into hydrogen and oxygen using an electric current, with the primary reactions being the oxygen evolution reaction (OER) at the anode and the hydrogen evolution reaction (HER) at the cathode. Efficient electrolysis necessitates the use of catalysts to lower the overpotentials of these reactions, with Pt commonly used for HER and IrO<sub>2</sub> or RuO<sub>2</sub> for OER.<sup>37</sup> However, research is actively exploring cost-effective alternatives such as transition metal oxides, phosphides, and sulfides. For instance, Ni-based catalysts, which form surface hydroxides or oxyhydroxides acting as active sites for OER, can dissolve over time, impacting catalytic activity. Fe-doped Ni<sub>2</sub>P catalysts exhibit enhanced stability and activity due to the formation of a FeNiOOH layer during operation.<sup>38</sup> Similarly, advanced catalysts like NiCo@C/MXene/CF electrodes show superior stability and efficiency, achieving a hydrogen production rate of  $18.66 \text{ mmol/cm}^2/\text{h}$  at a current density of  $1.0 \text{ A/cm}^2$ , attributed to the mesoporous array of NiCo-decorated carbon nanosheets facilitating rapid gas bubble release during electrolysis. In contrast, the absence of MXene results in irregular microstructures and decreased hydrogen production efficiency of  $7.46 \text{ mmol/cm}^2/\text{h}$  at the same current density.<sup>38</sup>

Further, FeCoMoS@NG catalysts, used in zinc–air batteries and water splitting, demonstrate excellent stability and low cell voltages, requiring only 1.58 V to achieve a current density of  $10 \text{ mA/cm}^2$  and maintaining stability over 100 hours of operation. Rh/RhOx catalysts achieve remarkable turnover frequencies of  $2.19 \text{ s}^{-1}$  at 1.53 V and  $20.30 \text{ s}^{-1}$  at 1.63 V, reflecting a significant increase in activity compared to standard Rh catalysts and exhibiting exceptional stability over 20 hours at a current density of  $50 \text{ mA/cm}^2$ .<sup>39</sup> Additionally, a recent study developed a highly efficient water electrolysis system powered by a cellulose sponge-based hydrovoltaic power generator (CHPG)



optimized for long-term stability and high performance. A single CHPG achieved an open-circuit voltage ( $V_{oc}$ ) of approximately 0.47 V and a short-circuit current ( $I_{sc}$ ) of approximately 477  $\mu$ A under relative humidity of 45–50% at 25 °C.<sup>40</sup> By connecting six CHPG modules in parallel, the system produced a  $V_{oc}$  of 2.09 V and an  $I_{sc}$  of 3.11 mA, sufficient to drive water electrolysis for hydrogen production. The HER was facilitated by a cobalt phosphide/nickel foam (PCO/NF) electrode, which showed a significantly lower overpotential and a Tafel slope of 85 mV/dec compared to other electrodes. For OER, the  $\text{Co}_5\text{O}_4/\text{NiFe-LDH}/\text{NF}$  electrode demonstrated an overpotential of 1.5 V to achieve 1 mA and a Tafel slope of 74 mV/dec. These optimized electrodes exhibited excellent long-term stability, maintaining performance over 24 hours at a current density of 100 mA/cm<sup>2</sup>. The integrated system achieved a hydrogen production rate of 81.0  $\mu\text{mol}/\text{h}$ , highlighting its potential for sustainable and efficient hydrogen generation.<sup>40</sup>

Building on recent advancements, several studies have demonstrated significant improvements in hydrogen yield and production efficiency through innovative catalyst designs. For instance, Chai *et al.*<sup>41</sup> reported a 71% increase in hydrogen yield using Fe nanoparticles and a 35.2% increase with NiO nanoparticles in wastewater treatments. Furthermore, they observed a 623% enhancement in hydrogenase activity with 20 mg/L Ec-NiO-NP synthesized from *Eichhornia crassipes*, significantly boosting hydrogen production. Similarly, Liu *et al.*<sup>42</sup> showed that dual-doped  $\text{Co}_3\text{N}$  electrodes achieved high current densities at low overpotentials, retaining 92.3% of their current density after 10 hours of operation. Additionally, Qian *et al.*<sup>43</sup> developed  $\text{Ni}_3\text{N}-\text{Co}_3\text{N}$  heterointerfaces on Ni foam, achieving an overpotential of 43 mV for HER at 10 mA/cm<sup>2</sup> and an ultralow working potential of  $-88$  mV for HzOR, maintaining 25 mA/cm<sup>2</sup> for 40 hours without significant decay. Moreover, Zhu *et al.*<sup>44</sup> demonstrated that Ru/NiFe-LDH catalysts achieved an industrial-scale current density of 1 A/cm<sup>2</sup> at 0.43 V, resulting in an energy saving of 3.94 kW h m<sup>3</sup> of  $\text{H}_2$ , while maintaining performance over 120 hours at 5 A/cm<sup>2</sup>. Zhu *et al.*<sup>45</sup> showcased  $\text{Ni}_3\text{N}/\text{Co}_3\text{N}$  nanowires, achieving a 94.6% faradaic efficiency for formate production at 1.35 V, producing 11 mmol/cm<sup>2</sup>/h of formate and 21.4 mmol/cm<sup>2</sup>/h of hydrogen, and maintaining stability for over 200 hours at 1 A/cm<sup>2</sup>. Collectively, these insights underscore the potential of advanced catalysts to significantly enhance hydrogen production efficiency. *In situ* and *ex situ* characterizations, along with advanced techniques like Density Functional Theory (DFT), provide a deeper understanding of catalyst evolution and reaction mechanisms, essential for optimizing performance and ensuring long-term stability. Comprehensive testing and analysis are crucial for addressing overpotential, efficiency, and durability in water electrolysis systems.

### 3. Steam electrolysis using eutectic molten hydroxides

Molten hydroxide electrolysis for water splitting presents numerous advantages. One notable advantage is that

a substantial portion of the necessary energy for the electrolysis process is provided in the form of heat, proving to be a more economical option compared to using electricity.<sup>46</sup> The exceptional high-temperature conductivity of hydroxide electrolytes improves as temperatures increase. Molten hydroxides demonstrate superior conductivity, even at lower temperatures when compared to other molten salts such as chlorides and carbonates.

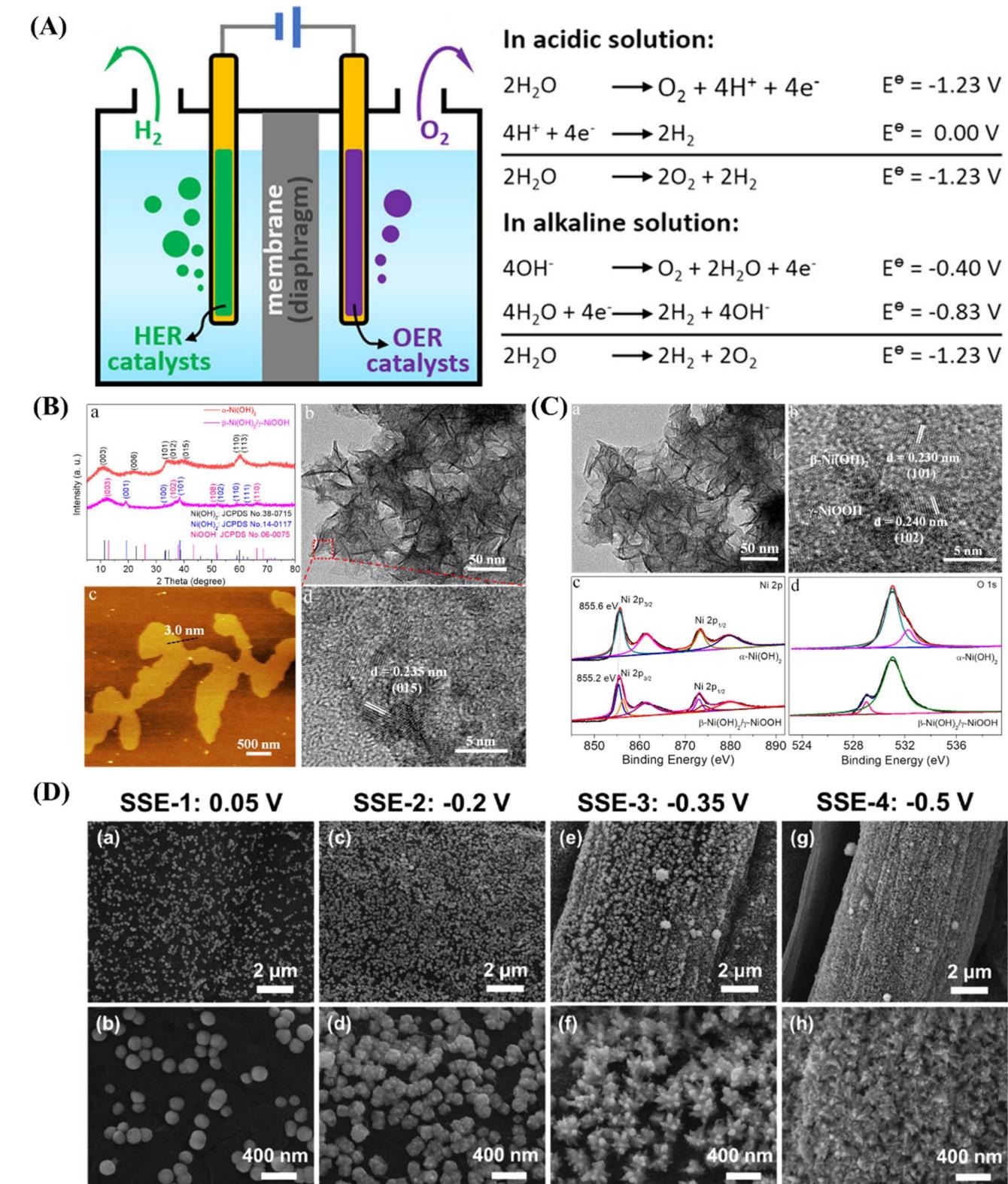
For instance, at a temperature of 427 °C, the conductivity of NaOH is twice that of NaNO<sub>3</sub> at the equivalent temperature. This heightened conductivity facilitates faster reaction kinetics and minimizes energy loss resulting from electrode overpotential. Consequently, it proves advantageous for high-temperature fuel cell systems and water-splitting procedures.<sup>47</sup>

Consequently, there is a general improvement in system efficiency. Moreover, this technology eliminates the necessity for valuable catalytic metals by employing base metals to generate hydrogen gas, with the molten hydroxide acting as a catalyst instead.<sup>48</sup> The increased operational temperature of molten salt reduces the decomposition potential of water, thereby enhancing efficiency even further. By effectively isolating the electrolysis system, sustained energy savings can be consistently attained for prolonged usage.<sup>49</sup> Moreover, molten salt, without the need for extra heating, sustains the required temperature through the passage of current during electrolysis, provided that the system is properly insulated.<sup>50</sup> The process can also leverage waste heat from other systems. However, the primary drawback limiting its industrial application is the requirement for a working temperature of less than 300 °C.<sup>51</sup> According to the Carnot cycle for thermodynamic efficiency, this leads to heat wastage, preventing widespread industrial utilization.

#### 3.1. Thermoelectric analysis of alkaline water electrolysis

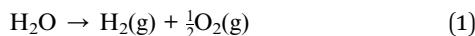
In alkaline water electrolysis, a direct current is applied to water, splitting it into hydrogen and oxygen gas molecules (Fig. 1(A)). The process involves two metal electrodes and an electrolyte to facilitate separation, with the electrolyte enhancing ionic conductivity.<sup>55</sup> Electrodes must resist corrosion, exhibit efficient electric conductivity, and possess good catalytic properties while maintaining structural integrity. A membrane is used to prevent the synthesis of hydrogen and oxygen gas into water.<sup>56</sup> The electrochemical cell comprises electrodes, a membrane, and an electrolyte. The overall water electrolysis reaction is expressed as eqn (1).<sup>57</sup> During electrolysis, reduction occurs at the cathode, generating hydrogen, while oxidation occurs at the anode, generating oxygen.<sup>58</sup> The process of water electrolysis transforms electrical and thermal energy into chemical energy, which is stored as hydrogen fuel. The energy needs are in line with thermodynamic principles, with the required energy dictated by the enthalpy change ( $\Delta H$ ) of the process (eqn (2)).<sup>59</sup> A portion of electric energy is utilized, as indicated by the Gibbs free energy change ( $\Delta G$ ), while the remaining energy is in the form of thermal energy ( $Q_E$ ). The minimum cell voltage ( $E_{cell}^\circ$ ) for electrolysis under specific pressure and temperature conditions can be expressed as eqn (3).<sup>59</sup>





**Fig. 1** (A) Traditional electrocatalytic water splitting in alkaline environments. (B) (a) X-ray powder diffraction (PXRD) patterns of  $\alpha\text{-Ni(OH)}_2$  obtained from the nonwoven fabric (NF) before (above) and after (below) oxygen evolution reaction (OER). (b) Transmission electron microscopy (TEM), (c) atomic force microscopy (AFM), and (d) high-resolution TEM images of  $\alpha\text{-Ni(OH)}_2$ . (C) (a) TEM and (b) HRTEM images of  $\alpha\text{-Ni(OH)}_2$  after OER. High-resolution X-ray photoelectron spectroscopy (XPS) spectra for (c) Ni 2p and (d) O 1s of  $\alpha\text{-Ni(OH)}_2$  before (above) and after (below) OER. The original data is represented by the black curves in panels (c) and (d). (D) Scanning electron microscopy (SEM) images at different magnifications of platinum nanoparticles (Pt NPs) electrodeposited on self-supporting electrodes manufactured at various electrolyte levels (EL): (a and b) 0.05 V, (c and d) -0.2 V, (e and f) -0.35 V, and (g and h) -0.5 V. Edited with permission from ref. 52–54. Copyright ACS ©2018, ©2021 and Elsevier ©2022.





$$\Delta G = \Delta H - Q_E = \Delta H - T\Delta S \quad (2)$$

$$\Delta E_{\text{cell}}^{\circ} = \frac{-\Delta G^{\circ}}{zF} \quad (3)$$

$$\Delta E_{\Delta H} = \Delta E_{\text{cell}} = \frac{\Delta H}{zF} \quad (4)$$

Here,  $z$  represents the number of electrons transferred in the electrochemical reaction, and  $F$  (Faraday's constant) is the charge of one mole of electrons, approximately 96 485 C/mol. In an ideal electrolysis process, the minimum voltage, known as the thermo-neutral voltage ( $\Delta E^{\circ}$ ), is equivalent to the enthalpy change potential  $\Delta E_{\Delta H}$  as highlighted in eqn (4). For an actual electrolysis process, must be greater than  $\Delta E_{\Delta H}$ , representing additional energy caused by thermodynamic irreversibility, primarily associated with water vapour in the hydrogen and oxygen streams.<sup>60</sup> Thermodynamic properties under standard conditions (1 atm and 25 °C) provide insights into the feasibility of the process, including enthalpy change ( $\Delta H^{\circ}$ ), Gibbs free energy change ( $\Delta G^{\circ}$ ), entropy change ( $\Delta S^{\circ}$ ), and cell voltage ( $E_{\text{cell}}^{\circ}$ ).<sup>61</sup> These insights shed light on the energy transformations involved in generating hydrogen and oxygen gases.

### 3.2. Alkaline water electrolysis and efficiency analysis

The functioning mechanism of an alkaline water electrolysis cell is characterized by a straightforward configuration consisting of a cathode, anode, electrolyte, and power supply. The application of direct current (DC) maintains electron flow from the negative compartment to the cathode, where hydrogen gas is produced by consuming electrons from hydrogen ions.<sup>62</sup> Simultaneously, hydroxide ions migrate towards the anode within the electrolyte, ensuring charge balance.<sup>63</sup> Commonly used electrolytes, such as potassium hydroxide, enhance solution conductivity and prevent corrosion loss. Nickel, recognized for its cost-effectiveness and high efficiency, is commonly used as electrode material.<sup>64</sup> In their investigation, Cao *et al.*<sup>52</sup> delved into the electrocatalytic properties of  $\alpha\text{-Ni(OH)}_2$  on a self-supporting electrode for the oxygen evolution reaction (OER), aiming to optimize preparation conditions for heightened electrocatalytic activity and stability. The study employed various measurements and characterizations to assess the catalyst's performance, revealing structural and morphological changes pre- and post-OER. For instance, Fig. 1(B) illustrates PXRD patterns and images of  $\alpha\text{-Ni(OH)}_2$  from different electrochemical conditions, indicating similar crystalline  $\alpha\text{-Ni(OH)}_2$  generation.<sup>52</sup> Furthermore, Fig. 1(B) also displayed TEM, AFM, and HRTEM images, providing visual evidence of the material's morphology and structure. Additionally, high-resolution XPS spectra indicated the conversion of  $\alpha\text{-Ni(OH)}_2$  to  $\beta\text{-Ni(OH)}_2$  during OER, with a portion converting into NiOOH, the active OER species.<sup>52</sup> Similarly, Fig. 1(C) presented TEM and HRTEM images post-OER, along with XPS spectra, clarified the post-reaction composition and phase transition. The observed phase transition, marked by the emergence of NiOOH,

substantiated the catalyst's heightened catalytic activity after OER.<sup>52</sup>

In a related study, Zhang *et al.*<sup>65</sup> aimed to create self-supporting electrodes (SSEs) for use in direct methanol fuel cells (DMFC) and direct alcohol fuel cells (DAFC) by utilizing a simple square-wave potential (SWP) method to electrodeposit platinum nanoparticles (Pt NPs) onto carbon paper.<sup>65</sup> The study targeted an enhancement in the utilization rate and catalytic durability of Pt in these fuel cells. Specifically, Fig. 1(D) showcased SEM images of the electrodeposited Pt NPs on SSEs prepared at different lower potentials, revealing morphological changes in Pt NPs with varying potentials ( $E$ ). For example, At  $E = 0.05$  V, smooth sphere-like Pt NPs were observed. However, as the potential negatively shifted to  $-0.2$  V, the PtNPs surface became rough, presenting a cauliflower-like morphology.<sup>65</sup> At  $E = -0.35$  V, observations revealed platinum nanoparticles (Pt NPs) resembling coral formations, with surface protrusions. Finally, at  $E = -0.5$  V, thorn-like Pt NPs were formed.<sup>65</sup> These outcomes suggest that managing the potential had a notable effect on the quantity, distribution, and structure of the electrodeposited Pt NPs on carbon paper, potentially influencing the catalytic activity and endurance of the Pt catalysts in fuel cells.

In the process of water electrolysis, hydrogen ions are drawn towards the cathode, while hydroxide ions are directed towards the anode. Meanwhile, gas receivers gather hydrogen and oxygen generated at the cathode and anode, respectively, with a membrane separating them.  $T$  notably, the combined potential of the reactions is  $-1.23$  V, indicating the theoretical cell voltage for the procedure. However, various barriers must be overcome, including electrode surface boundary layers, electrode and electrolyte phases, separator, electrical resistance, and activation energies, analyzed in thermodynamic, kinetic, and transport process principles contexts.<sup>64</sup> Specifically, resistance in a water electrolysis system includes external electrical circuit resistance ( $R_1$ ), anode overpotential ( $R_{\text{anode}}$ ), resistance due to oxygen bubbles ( $R_{\text{bubble of O}_2}$ ), electrolyte resistance ( $R_{\text{ions}}$ ), membrane resistance ( $R_{\text{membrane}}$ ), resistance due to hydrogen bubbles ( $R_{\text{bubble of H}_2}$ ), cathode overpotential ( $R_{\text{cathode}}$ ), and electrical resistance at the cathode ( $R'_1$ ). Therefore, the total resistance is expressed in eqn (5).<sup>66</sup>

$$R_{\text{total}} = R_1 + R_{\text{anode}} + R_{\text{bubble, O}_2} + R_{\text{ions}} + R_{\text{membrane}} + R_{\text{bubble, H}_2} + R_{\text{cathode}} + R'_1 \quad (5)$$

$$R = \frac{E}{i} \quad (6)$$

$$R = \frac{L}{kA} \quad (7)$$

where  $E$  is the potential (voltage) across the electrodes,  $i$  is the current flowing through the system,  $L$  is the distance between the electrodes,  $k$  is the conductivity of the electrolyte, and  $A$  is the cross-sectional area through which the current flows. Electrolysis resistances are categorized into electrical, reaction, and transport resistances. Electrical resistance is calculated using



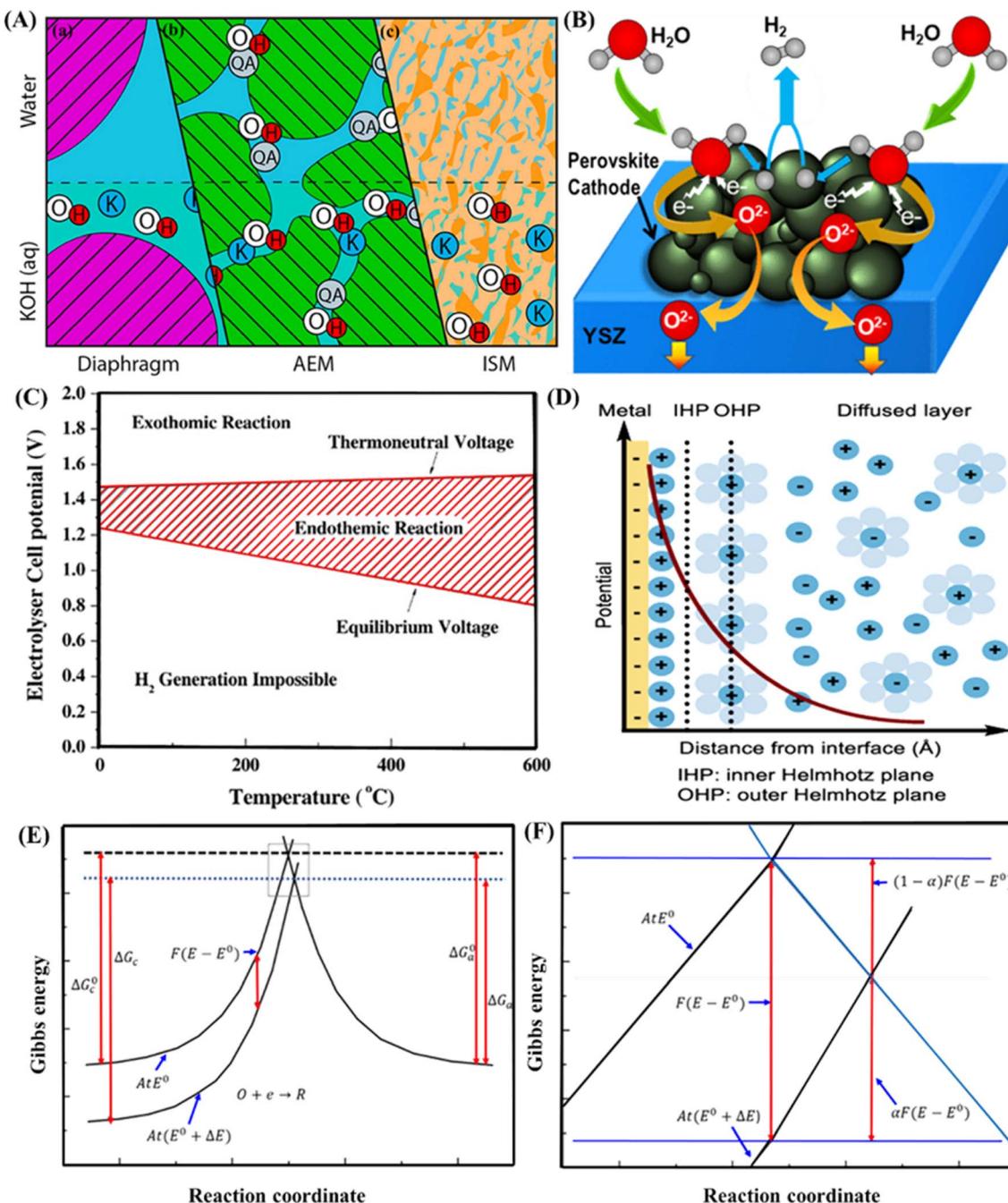


Fig. 2 (A) Illustration demonstrating various electrolyte concepts in distilled water and in combination with aqueous KOH, including (a) porous diaphragms, (b) anion-exchange membranes (AEM), and (c) ion-solvating membranes. (B) Visual representation outlining the sequential steps of high-temperature water electrolysis. (C) Representation of cell potential for hydrogen gas production through the water electrolysis process as a function of temperature. (D) Schematic depicting the electrical double layer near a negatively charged electrode surface. (E) Depiction of the effect of potential change on Gibbs energy: the overall relationship between energy change and reaction state. (F) Enlarged view of the highlighted section in (E). Reproduced with permission from ref. 69–73. Copyright ACS ©2023 and 2019, Elsevier ©2022, 2015, ACS ©2020 and Springer ©2023.

Ohm's law (eqn (6)) and expressed in eqn (7). Reaction resistances stem from over potential needed to overcome activation energies at cathode and anode surfaces.<sup>67</sup> Additionally, transport-related resistances include hindrances such as gas bubbles, ionic transfer resistance, and membrane resistance. Consequently, heat generation, resulting from both electrical

and transport resistances, contributes to inefficiency, commonly referred to as ohmic loss. Therefore, understanding and minimizing these resistances are crucial for enhancing energy efficiency in water electrolysis and overall system performance.<sup>68</sup>



## 4. Thermodynamics assessment and integration of alkaline electrolysis

The electrolyte concepts depicted in Fig. 2(A) play an essential role in shaping the thermodynamics of alkaline water electrolysis cells. These concepts, namely porous diaphragms, anion-exchange membranes (AEM), and materials with narrow electrolyte-filled channels, offer diverse approaches to improve the effectiveness and functionality of alkaline electrolysis cells.<sup>69</sup> Porous diaphragms, illustrated in Fig. 2A(a), are crafted from poly(arylene ether sulfone) combined with inorganic hydrophilic particles, creating a highly porous composite structure featuring denser surface layers. These separators aid in establishing ionic conductivity between electrodes while reducing the mixing of product gases.<sup>69</sup> The impact on the thermodynamics of alkaline electrolysis cells is notable, particularly in influencing gas crossover and the efficiency of gas discharge. Anion-exchange membranes (AEM), illustrated in Fig. 2A(b), are composed of polymer chemistries with covalently linked cationic properties, typically employing quaternary ammonium-functionalized groups.<sup>69</sup> AEMs contribute to improved ion conductivity, reduced gas crossover, and enhanced chemical and mechanical stability, thereby influencing the thermodynamics of alkaline electrolysis cells positively. Fig. 2A(c) introduces the concept of highly alkali-resistant materials with narrow electrolyte-filled channels.<sup>69</sup> This involves separators made of such materials, striving to merge superior conductivity with exceptional hydrogen ( $H_2$ ) barrier properties and durability. The potential impact on the thermodynamics of alkaline electrolysis cells includes reduced ohmic losses, suppressed gas crossover, and efficient gas discharge.

Connecting this insight to the broader context of the section discussing equilibrium potential and thermodynamics, it's evident that these electrolyte concepts play a pivotal role in influencing overpotentials, ion conductivity, and overall efficiency in water electrolysis.<sup>69</sup> The interaction among these ideas and the thermodynamic principles deliberated upon provides insights into the complex factors influencing the functionality of alkaline electrolysis cells. The equilibrium potential is derived by deducting the cathode electrode's equilibrium potential from that of the anode electrode, as outlined in eqn (8).<sup>74</sup> The equilibrium cell potential correlates with the Gibbs free energy alteration of the entire cell reaction, as delineated in eqn (9).<sup>74</sup> In the case of a spontaneous cell reaction, the driving force possesses a negative value of  $\Delta G_{cell}$ , articulated as eqn (10).<sup>74</sup>

$$E_{cell}^{\circ} = E_{cathode}^{\circ} - E_{anode}^{\circ} \quad (8)$$

$$\Delta G_{cell} = -nFE_{cell}^{\circ} \quad (9)$$

$$\Delta G_{cell} = \sum \Delta G_{product} - \sum \Delta G_{reactant} = \Delta H_{cell} - T\Delta S_{cell} \quad (10)$$

where  $n$  stands for the quantity of transferred electrons.  $\Delta G_{cell}$  represents the electrochemical cell reaction and is determined by the disparity between the cumulative free energy values of

products and reactants.<sup>75</sup> Where  $\Delta H_{cell}$  and  $\Delta S_{cell}$  represent, correspondingly, the alteration in enthalpy and entropy linked with the cell reaction, while  $T$  signifies the reaction's temperature.<sup>76</sup> It is noteworthy that for spontaneous cell reactions,  $T\Delta S_{cell} > \Delta H_{cell}$ , resulting in  $\Delta G_{cell} < 0.0$ . The equilibrium potential of the cell in water electrolysis stands at  $-1.23$  V, with a Gibbs free energy of  $238$  kJ/mol for hydrogen.<sup>77</sup> Despite the transformation of water into two gases, hydrogen and oxygen, during electrolysis, this process leads to a substantial increase in the system's entropy, accompanied by an extraordinarily high enthalpy value of  $286$  kJ/mol at  $25$  °C.

During high-temperature water electrolysis, several reaction steps occur as highlighted in Fig. 2(B). Initially,  $H_2O$  adheres to the perovskite surface or the three-phase boundary (TPB), leading to the formation of an  $OH^-$  ion by relinquishing a hydrogen atom. Subsequently, the  $OH^-$  ion sheds another hydrogen atom, yielding  $O^{2-}$  ions, while the liberated hydrogen atoms merge to generate hydrogen gas.<sup>78</sup> The generated  $O^{2-}$  ions move towards the YSZ phase and traverse the YSZ electrolyte's interior towards the anode side, where they unite to generate oxygen gas. These steps are influenced by factors such as electrode material properties, TPB nature, and microstructure. It's important to highlight that the conversion of water into hydrogen and oxygen is not thermodynamically favourable, necessitating an external supply of electrical energy to initiate the cell reaction.<sup>79</sup> The cell potential must exceed the applied potential, and reactions can vary in speed, with some requiring overpotential for the necessary current density.<sup>80</sup> The kinetics discussed earlier, reveal an increase in overpotential with rising current density. Additional energy introduces a potential drop influenced by electrolyte properties, electrode shape, and cell design. As expressed in eqn (11), the cell potential consistently ranges between  $1.8$ – $2.0$  V, with a current density value between  $0.001$ – $0.003$  A/cm<sup>2</sup> for an industrial water electrolysis system.<sup>80</sup>

$$E_{cell}^{\circ} = E_{cathode}^{\circ} - E_{anode}^{\circ} - \sum \eta + iR_{cell} \quad (11)$$

where  $\sum \eta$  represents the total overpotentials arising from variations in electrolyte concentration, obstruction at the electrode surface because of bubble formation; and from the bubble formation itself.<sup>81</sup> As both  $\eta$  and  $iR_{cell}$  rise, the current density also increases, resulting in inefficiencies during the electrolysis process.<sup>82</sup> Numerous researchers indicate that the connection between the potential of the electrolytic cell and the operational temperature can be depicted in Fig. 2(C). The correlation between the potential of the cell and the temperature within the electrolysis system, illustrated in Fig. 2(C), is delineated into three segments, delineated by two lines: the line representing the equilibrium voltage and the line indicating the thermoneutral voltage.<sup>82</sup> The equilibrium voltage line denotes the minimum potential required for water dissociation through electrolysis, implying that electrolysis cannot proceed below this threshold. It's worth noting that the equilibrium voltage decreases with rising temperature.<sup>83</sup> The thermoneutral voltage represents the minimum voltage necessary for the electrolysis cell to operate, implying that electrolysis is endothermic below this line. Conversely, electrolysis is exothermic above this





Table 2 Experimental conditions used hydroxide salts and their mixtures at different operating conditions and compositions during the electrochemical process

Composition of electrolyte	Temperature (°C)	Atmosphere	Reference electrode	Working electrode	Crucible material	Anode	Cathode	Applied voltage (V)	Reference
NaOH	550	Ar	Ni rod	Pt wire, Ni wire, and Ni pallet	Ni	—	—	—	94
NaOH-KOH	200	Ar	Pt wire	Pt, Au, Fe rod	Platinum	—	—	—	95
NaOH-KOH (50 : 50)	347	N <sub>2</sub>	Cu plated	Pt	Vitreous carbon crucible	—	—	—	96
LiOH-NaOH, LiOH-KOH,	250–300	—	Platinum sheet	Pt, Pd, Ni, Ag, Al	Nickel crucible	—	—	—	97
NaOH-KOH	110–160	—	Fe	Fe, FeSi, and FeC	PTFE	—	—	—	98
KOH	35–400	Steam	—	—	Ni 400	Ni, Ni400, Co plated Ni	Ni 400	—	99
KOH, NaOH, Ba(OH) <sub>2</sub> , LiOH	200–700	Ar	—	—	Alumina	Ni, Pt and Ni	Ni	1.1–2.3	100
NaOH	25	Air	SCE	Cu rod	—	—	—	—	101
NaOH (8.0 M)	90	Air	Hg/HgO/1 M NaOH	Co–Mo alloy	—	Ni–Cr–Fe alloy	—	—	102
KOH (10 wt%)	20, 40, 60	Air	—	—	Vinyl chloride	Ni–Cr–Fe alloy	—	—	103
NaOH-NaHS (50 : 50)	80	Air	Hg/HgO (1 M NaOH)	—	Glass	Graphite, Ni, graphite	—	—	104
NaOH	320–400	Argon	—	—	—	Ni–Cr alloy	—	—	—
Aqueous, KOH–NaOH, LiOH–NaOH	110–140, 350,	Argon	—	—	—	Ni	Ni	—	—
KOH (1.0 M)	300–400	—	—	—	Activated Ni	Activated Ni	1.55,1.3, 1.45	105	106
NaOH (0.1–5.0 M)	25	Air	Ag/AgCl	C-felt supported Ni, —	—	—	—	—	107
NaOH-KOH (57 : 43)	200–220	Ar or NH <sub>3</sub>	Ag wire	Co, Ni–Co	—	—	—	—	108
NaOH	530	Ar	—	Ni–Mo–Fe coated stainless steel	—	—	—	—	—
KOH (50 wt%)	80, 150, 208, 264	—	(DHE)	—	Ni	—	—	—	109
NaOH-KOH (51 : 49)	200–450	NH <sub>3</sub>	—	Pt plate	Ni-400 (commercial Monel® alloy)	—	—	—	110
NaOH-KOH (50 : 50)	200	N <sub>2</sub> and steam	—	Ni-covered by alumina	Ni	FeO	1.7	—	111
NaOH	550	O <sub>2</sub> + air	—	Ni tube	Ni-400 (commercial Monel® alloy)	—	—	—	112
NaOH-KOH (54 : 46)	400	O <sub>2</sub> + air	Ni alloy	—	Planar Ni	Mesh Ni monel	1.2	—	113
NaOH (8.0 M)	70	Air	Ni alloy	Alumina	—	—	—	—	114
			Hg/HgO	Alumina	—	—	—	—	114
				Plastic	—	—	—	—	115

threshold.<sup>84</sup> The thermoneutral voltage includes the overpotential of the electrodes, which exhibit weak temperature dependence. As a result, the thermoneutral voltage demonstrates a minor elevation in potential as the temperature rises.

The efficiency of electrolysis can be assessed using different parameters. One crucial indicator is voltage efficiency, which signifies the proportion of the actual voltage employed for water splitting compared to the total voltage applied to the cell. This relationship is articulated in eqn (12).<sup>85</sup> Thermal efficiency, as delineated in eqn (13) is grounded in the energy variations of the water electrolysis reaction.<sup>85</sup> It covers the complete thermal equilibrium of the process. Another approach to assessing efficiency involves evaluating the rate of hydrogen gas generation compared to the total electrical energy input to the electrolysis system, as depicted in eqn (14).<sup>85</sup>

$$\text{Voltage efficiency}(\%) = \frac{E_{\text{cell}}^{\circ}}{E_{\text{cell}}} \quad (12)$$

$$\text{Faradaic efficiency}(\%) = \frac{\Delta H_{\text{cell}}}{\Delta G_{\text{cell}}} \quad (13)$$

$$\begin{aligned} \text{Efficiency of H}_2 \text{ production rate}(\%) &= \frac{r_{\text{H}_2} \text{ of production rate}}{\Delta W} \\ &= \frac{-V_{\text{H}_2}}{iE_{\text{cell}}t} \quad (14) \end{aligned}$$

In this context,  $t$  denotes the duration of electrolysis, while  $V_{\text{H}_2}$  represents the rate of hydrogen production per unit volume of the cell. By utilizing the efficiency equations mentioned earlier, enhancements to the electrolytic process can be attained by reducing the energy required for the splitting of water.<sup>86</sup> This reduction can be attained by elevating the temperature or pressure and minimizing energy losses by reducing system resistance.<sup>85</sup> Hence, much of the research focuses on improving both the efficiency of the electrolysis setup and the rate at which hydrogen gas is produced, with a strong emphasis on high-temperature steam electrolysis.<sup>87</sup>

#### 4.1. Electrochemical kinetics of reference electrodes

The electrode reaction rate, determined by current density, relies on the electrode surface nature and pre-treatment. The electrolytic solution composition near the electrodes influences the reaction rate, forming a double layer of ions.<sup>88</sup> For instance, a charge layer near the cathode involves hydroxyl and potassium ions during electrolysis. Moreover, the reaction rate is contingent upon the electrode potential, denoted by the reaction overpotential. Investigating electrode kinetics aims to elucidate the macroscopic relationship between current density, the composition of the electrolytic solution near the electrode and surface overpotential.<sup>89</sup> In Fig. 2(D), the double layer is depicted, characterized by two mobile layers with accumulated ions and solvent molecules.<sup>90</sup> The layer proximal to the electrode, termed the Inner Helmholtz Layer (IHL), exhibits a relatively ordered structure, while the Outer Helmholtz Layer (OHL) is less organized. Ionic countercharges in the vicinity balance the electrical

charges on electrode surfaces. The plot in Fig. 2(D) illustrates the potential distribution with respect to the distance from the electrode surface, revealing an interfacial potential variation resulting from the double layer.<sup>39</sup> This non-faradic mechanism plays a role in the capacitive characteristics of electrode reactions, which is an important aspect of electrode kinetics. The Butler–Volmer equation illustrates the relationship between current density, surface potential, and the electrolytic solution composition near the electrode surface.<sup>91</sup> This equation can be expressed as a one-electron reaction, linking the current to the rate as shown in eqn (15).<sup>91</sup>

$$i = i_{\text{cathodic}} - i_{\text{anodic}} = FAK^{\circ}(C_0(0,t)e^{-\alpha f(E-E^{\circ})} - C_R(0,t)e^{(1-\alpha)f(E-E^{\circ})}) \quad (15)$$

The Butler–Volmer equation describes the connection between current density, surface potential, and the composition of the electrolyte near the electrode surface. Expressed as a one-electron reaction, it involves parameters such as  $A$  (electrode surface area),  $K^{\circ}$  (typical rate constant),  $\alpha$  (transfer coefficient ranging from 0 to 1 for a single-electron reaction), and  $f$  (the  $\frac{F}{RT}$  ratio). The variables “ $t$ ” and “0” within the brackets represent the particular time and distance from the electrode, respectively.<sup>91</sup>

The Butler–Volmer equation, derived through the transition-state theory, utilizes curvilinear coordinates along reaction pathways (Fig. 2(E)), where potential energy varies as a function of independent coordinates within the system. An increase in potential ( $\Delta E$ ) results in a reduction in the electron's relative energy by  $F(E - E^{\circ})$  (as shown in Fig. 2(F)), subsequently influencing the Gibbs free energy of hydrogen ions and hydrogen in the reaction as highlighted in Fig. 2(F).<sup>92</sup> This behaviour does not impose any restrictions on mass transfer. The Butler–Volmer equation (eqn (16)) can be simplified as follows.<sup>92</sup> Where  $i_0$  represents the current density of exchange, which is defined as the current related to the reversible process of water cleavage. The overpotential at each electrode is derived from this simplified equation.<sup>92</sup> Neglecting one term in the total resistance equation is permissible in the absence of mass transfer influence and at large over-potentials ( $>118$  mV at 25 °C), *i.e.*, when  $e^{-\alpha f\eta} > e^{-(1-\alpha)f\eta}$ . The relation between  $i$  and  $\eta(E - E^{\circ})$  is represented by the Tafel eqn (17).<sup>92</sup>

$$i = i_0(e^{-\alpha f\eta} - e^{-(1-\alpha)f\eta}) \quad (16)$$

$$\eta = a + b \log i \quad (17)$$

where  $a = \frac{2.3RT}{\alpha F} \log i_0$  and  $b = \frac{-2.3RT}{\alpha F}$ . The linear relationship between overpotential and the logarithm of current density is defined by slope ( $b$ ), where  $\alpha$  represents the exchange current density  $i_0$ , also recognized as the Tafel slope. In conclusion, the electrolysis rate is directly determined by current or current density, which, in turn, depends on various factors, including overpotential influenced by activation energy (EA).<sup>93</sup> The electrode material plays a crucial role in minimizing activation energy, making it a primary focus in research alongside optimizing electrode materials and surface configurations.



## 4.2. Enhancing molten hydroxide electrolysis under diverse conditions

In this section, the intricacies of anodic and cathodic reactions within a molten hydroxide electrolysis cell are investigated,

aiming to unravel the nuanced interplay under diverse process conditions. Influencing these orchestrated reactions are critical factors such as salt compositions, temperature, atmosphere, pressure, and electrode materials, each leaving a distinctive imprint. The consequential variable, hydrogen gas production,

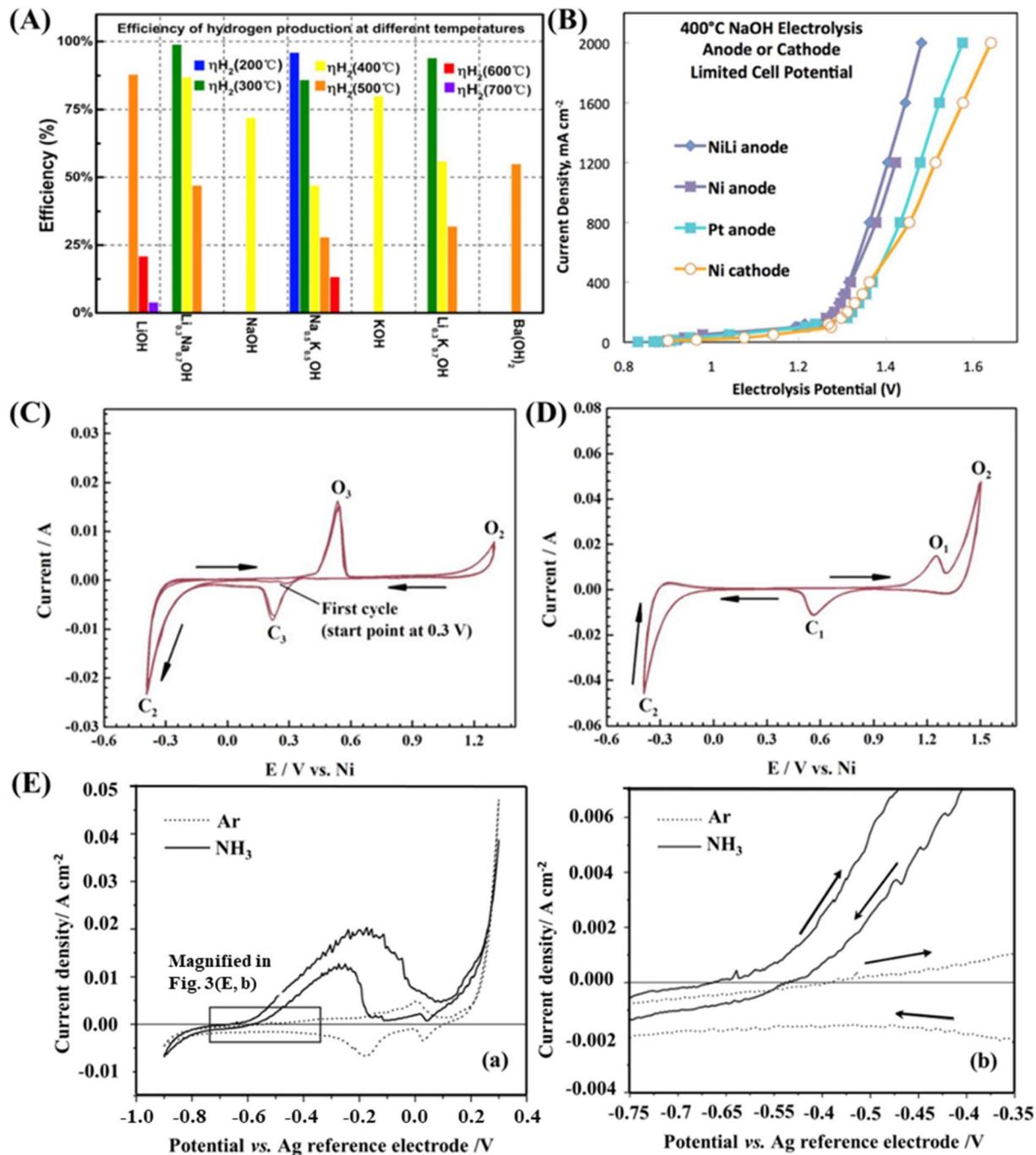


Fig. 3 (A) The efficiency of hydrogen production as a function of temperature and the selected hydroxide electrolyte under atmospheric pressure was assessed at 1 A between two flat nickel electrodes. (B) A cyclic voltammogram of a nickel wire electrode in the NaOH melt at 550 °C was conducted at a scan rate of 100 mV/s. The reference electrode was a nickel wire, with the potential limited between -0.4 V and 1.3 V. (C) A cyclic voltammogram of a platinum wire electrode in the NaOH melt at 550 °C was conducted at a scan rate of 100 mV/s. The reference electrode was a nickel wire, with the potential limited between -0.4 V and 1.3 V. (D) Cyclic voltammograms of a platinum electrode in NaOH-KOH at 200 °C were performed at a scan rate of 20 mV/s, using argon gas or ammonia as the atmosphere, and with Ag reference electrode. (E) (a) Cyclic voltammograms of a Pt plate electrode under Ar or  $\text{NH}_3$  at 200 °C (sweep rate: 20 mV/s); (b) an enlarged view of the profiles between -0.75 and -0.35 V from (a). Edited with permission from ref. 100, 109 and 135. Copyright IOPscience ©2016, 2015 and Elsevier ©2014.



showcases considerable variability under these conditions, providing a rich terrain for exploration. Choices span from room temperature to high-temperature scenarios, and from aqueous to molten hydroxide salt environments. Meticulously documented in Table 2, the conditions narrate the stories of low-temperature processes in ambient air and high-temperature counterparts immersed in argon, ammonia, or nitrogen atmospheres, capturing developments from the past until the present.

In 1976, Miles *et al.*<sup>116</sup> demonstrated a temperature-dependent influence on electrode kinetics, influencing the oxygen evolution reaction to a greater extent compared to the hydrogen evolution. Subsequently, Divisek *et al.*<sup>117</sup> expanded this inquiry to molten NaOH, achieving an efficiency of approximately 38–39% in water electrolysis at elevated temperatures. Furthermore, in a further study, Divisek *et al.*<sup>118</sup> broadened their scope to the electrolytic splitting of water in aqueous KOH and molten hydroxides (NaOH, LiOH–NaOH) at different temperature ranges. This research achieved a notable current efficiency of 90% in a NaOH melt at 350 °C, revealing a unique side reaction of peroxide production, which was notably diminished within a LiOH–NaOH melt. Moreover, Anani *et al.*<sup>119</sup> demonstrated the potential for hydrogen production by electrolyzing sulfur hydrogen at 80 °C in an equimolar aqueous solution of NaOH. A novel approach was taken by Abouatallah *et al.*<sup>120</sup> investigating the addition of soluble V<sub>2</sub>O<sub>5</sub> to an 8 M KOH aqueous solution at 70 °C to reactivate a nickel cathode during hydrogen evolution. While the V<sub>2</sub>O<sub>5</sub> additive proved effective, the electro-catalytic activity of vanadium-modified nickel did not surpass that of a fresh nickel electrode.

Additionally, Miles *et al.*<sup>121</sup> explored various eutectic molten hydroxides (NaOH–KOH, LiOH–KOH, LiOH–NaOH) with different working electrodes. Proposing Ag/AgCl as a reference electrode due to its swifter reaction kinetics, the study emphasized the applicability of molten hydroxides in thermal battery applications, underscoring the need to minimize H<sub>2</sub>O and O<sub>2</sub> for the effective use of lithium or sodium anodes. Nagai *et al.*<sup>122</sup> investigated the effect of bubble formation between electrodes on water electrolysis efficiency. Using a 10 wt% KOH aqueous solution and Ni–Cr–Mo alloy electrodes, they found that adjusting the space between electrodes influenced the void fraction, impacting electrolysis efficiency. Similarly, Zabinski *et al.*<sup>123</sup> investigated augmenting hydrogen evolution by incorporating carbon into the Co–Mo alloy cathode. They conducted experiments in an 8 M NaOH solution at a temperature of 90 °C. Despite increased hydrogen evolution activity, preventing molybdenum dissolution proved elusive. Híveš *et al.*<sup>124</sup> pioneered the electrochemical production of ferrate(vi) in eutectic molten hydroxide NaOH–KOH at 200 °C. Ferrate(vi) formation was detected at the inert electrode in contact with ferrate(III) ions and an iron electrode.

Simultaneously, Jayalakshmi *et al.*<sup>125</sup> explored the electrochemical catalytic activity of a stainless steel substrate coated with a composite film of Ni–Mo–Fe in alkali solutions, showcasing improved hydrogen evolution activity. The potential for ferrate(vi) production was further explored by Híveš *et al.*<sup>126</sup> using

a NaOH–KOH eutectic hydroxide at temperatures between 170–200 °C with a stationary iron electrode. The formation of ferrate(vi) at the anodic oxidation of the iron electrode was confirmed, achieving a current efficiency of Fe(vi) formation of up to 72%. In a different domain, Ganley *et al.*<sup>127</sup> pioneered a direct ammonia fuel cell using eutectic molten hydroxides (NaOH–KOH) at temperatures from 200 to 450 °C, achieving a maximum power density of 40 mW/cm<sup>2</sup> at 450 °C. On a separate note, Cox and Fray<sup>128</sup> effectively converted iron(III) oxide to iron in molten sodium hydroxide at 530 °C, accomplishing a current efficiency of around 90%. In addition, Ganley<sup>129</sup> extended the investigation, examining the impacts of elevated temperature and pressure on alkaline electrolysis, employing concentrated KOH at 400 °C across different pressure conditions. The research utilized nickel Monel as a cathode and evaluated different anode materials. It determined that the most optimal cell performance was achieved when employing a cobalt-plated nickel anode at 400 °C and under a steam partial pressure of 8.7 MPa.

Continuing the journey to enhance hydrogen evolution, Döner *et al.*<sup>130</sup> employed a 1.0 M KOH water solution at ambient temperature. They supported cathodes made from various materials (Ni, Co, and Ni–Co alloy) with C-felt coating, resulting in significant increases in current densities, particularly with the C-felt/Ni–Co combination recording the highest current density. Extending the versatility of molten hydroxide, Guo *et al.*<sup>131</sup> demonstrated a direct carbon fuel cell with enhanced performance up to 400 °C by employing the eutectic mixture as an electrolyte. Moreover, Hrnčiariková *et al.*<sup>132</sup> contributed to this area by examining how the composition of the anode affects the electrochemical production of ferrate(vi) using molten KOH. They analyzed three distinct anode materials in molten KOH: pure iron (Fe), white cast iron (FeC), and silicon-rich steel (FeSi) electrodes. The research unveiled the concurrent existence of ferrate(vi) formation alongside significant oxygen evolution. Recent advancements include Yang *et al.*'s platinum electrode, achieving a maximum power of approximately 16 mW/cm<sup>2</sup>.<sup>133</sup> Licht *et al.*<sup>100,134</sup> in their studies demonstrated ammonia production feasibility while observing a decrease in hydrogen gas evolution efficiency at high temperatures. The hydrogen gas evolution efficiency of the mixed hydroxide electrolyte (NaOH–KOH; 50–50 mol%) dropped from 96% to 13.4% with increasing temperature from 200 to 600 °C, as illustrated in Fig. 3(A). Ultimately, the evolving narrative illustrates the interconnected nature of these studies, providing insights into the intricate world of molten hydroxide electrochemistry.

## 5. Electrochemical stability of eutectic molten hydroxide electrodes

### 5.1. Voltammetric investigation of nickel electrode

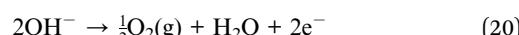
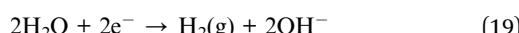
Many reactions in molten salt electrolytes have been elucidated through cyclic voltammetry, the recognized as a powerful tool for comprehending electrochemical processes at electrode interface. Cyclic voltammetry plays a pivotal role in shedding light on the fundamental aspects of reactions and contributing to the



comprehensive exploration of electrolytic systems.<sup>136</sup> In an insightful investigation led by Wang *et al.*,<sup>137</sup> the behaviour of an in-use nickel electrode immersed in molten NaOH–KOH at 280 °C was examined in depth. The outcomes, revealed through cyclic voltammetry, showcased a visually striking result a distinctive black film materialized on the nickel electrode's surface. This captivating phenomenon was attributed to the oxidation process, converting NiO to NiO<sub>2</sub>, as succinctly expressed in eqn (18).



Litch *et al.*<sup>138</sup> explore alternative molten electrolytes for water splitting to generate hydrogen fuel. Their study demonstrates that the electrolysis potential needed for water splitting at 400 °C in molten NaOH is remarkably low, measuring below 1.4 V (Fig. 3(B)). Under these circumstances, elevated current densities, potentially reaching A/cm<sup>2</sup>, are readily attainable. Anticipations suggest that utilizing reticulated or textured electrodes with enhanced microscopic or nanoscopic surface areas may further decrease electrolysis overpotentials. Anodes composed of Ni, Pt, monel, and Ir, paired with Ni cathodes, demonstrate notable stability, maintaining effective current densities of 1 A/cm<sup>2</sup> under conditions where both anode and cathode limitations are present.<sup>138</sup> Notably, at low current density, the electrolysis potential notably drops to less than 1 V in 700 °C LiOH, even yielding some hydrogen gas. In a parallel study, Ge *et al.*<sup>57</sup> delved into the oxidation of nickel-to-nickel oxide in a one-step reaction within molten NaOH, albeit at a higher temperature of 550 °C. This transformative process was succeeded by a secondary reaction involving hydrogen evolution. Fig. 3(C) vividly depicts the cyclic voltammogram of a nickel wire working electrode in molten NaOH at 550 °C, revealing clear redox peaks. The oxidation peak O<sub>3</sub> indicates the oxidation of the Ni wire in NaOH, leading to the creation of a thin oxide film on the Ni surface. Concurrently, peak C<sub>3</sub> captures the reduction of the oxide C<sub>3</sub>. Noteworthy is the intensified current observed at the cathode in C<sub>2</sub> and at the anode in O<sub>2</sub>, corresponding to the evolution of hydrogen and oxygen gas, respectively, as articulated in eqn (19) and (20).



Transitioning to another facet of research, Sayed *et al.*<sup>139</sup> conducted an extensive investigation on an independent nickel-layered double hydroxide characterized by a hierarchical nanosheet architecture. This unique structure, synthesized efficiently on nickel foam *via* hydrothermal treatment and later transformed into NiO at 500 °C, demonstrated impressive activity in methanol oxidation.<sup>139</sup> The synthesized electrodes displayed an onset potential of 0.35 V in a 1 M KOH solution, with the nanosheet structure enhancing charge and mass transfers, resulting in superior overall activity. Notably, these electrodes demonstrated prolonged stability during extended oxidation activity, maintaining a discharge current at 0.5 V for more than 1 hour without any decline in performance represents a noteworthy improvement compared to bare nickel

foam.<sup>139</sup> These findings emphasize the effectiveness of nickel-layered double hydroxide and nickel oxide electrodes as anodes in alkaline direct methanol fuel cells, suggesting substantial promise for energy conversion systems.

Additionally, Al-Shara *et al.*<sup>140</sup> made a valuable contribution to the field by developing a novel reference electrode, Ni/Ni(OH)<sub>2</sub>, specifically designed for electrolysis in eutectic molten hydroxides. This electrode was manufactured by employing a eutectic molten hydroxide (NaOH–KOH; 49–51 mol%) at a temperature of 300 °C.<sup>140</sup> Cyclic voltammetry tests were conducted to evaluate its performance, revealing exceptional stability and reusability. In a comparative analysis with platinum and silver quasi-reference electrodes, the Ni/Ni(OH)<sub>2</sub> electrode emerged as a promising candidate, demonstrating suitability, stability, reproducibility, and reusability as a reference electrode in a molten hydroxide electrolyte. In summary, these crucial findings underscore the potential of the Ni/Ni(OH)<sub>2</sub> electrode as a stable and efficient reference electrode for electrolysis in eutectic molten hydroxides.<sup>140</sup>

## 5.2. Electrochemical capability platinum electrode in molten hydroxide

In the captivating domain of electrochemical exploration, the platinum electrode assumes the spotlight. A meticulous cyclic voltammetry analysis at 550 °C, immersed in molten NaOH, unveils the nuanced interplay of redox peaks, symbolic of the reduction of a delicate oxide film enveloping the platinum wire's surface.<sup>135</sup> Fig. 3(D) presents the cyclic voltammograms from Ge *et al.*'s study<sup>135</sup> employing platinum as the working electrode. Each peak narrates a unique story: the cathodic current peak C<sub>1</sub> signifies the poetic reduction of the oxide film; the captivating surge in cathodic current at C<sub>2</sub> (−0.4 V) unfolds a ballet of hydrogen gas evolution; the anodic current peak O<sub>1</sub> depicts the stoic oxidation of the oxide film, and the enchanting O<sub>2</sub> serves as a crescendo harmonizing with the birth of oxygen gas. The saga continues beyond platinum, venturing into the realm of noble nickel. Its cyclic voltammetry narrative in molten NaOH reveals a tapestry of redox peaks akin to its platinum counterpart. The cathodic sonnet at C<sub>3</sub> serenades the reduction of a wispy oxide film caressing the nickel surface. Meanwhile, the anodic peak O<sub>3</sub> resonates with the bold oxidation of the nickel wire in the molten embrace. However, a twist in potential scan limits between 0.3 V and 1.3 V dims the presence of O<sub>3</sub>, creating an interlude where the generated nickel oxide films seek refuge from reduction in the first cycle.<sup>135</sup> Both platinum and nickel trace redox peaks in molten NaOH, a testament to the oxide tales etched on their surfaces. Yet, nuances emerge, with platinum showcasing distinctive choreography of reduction and oxidation peaks, while nickel pirouettes with reduction peaks for the oxide film and an ode to oxidation for the nickel wire. Specific potential ranges embellish each peak with uniqueness.

Enter Ge *et al.*,<sup>135</sup> pioneers in this symphony. Cyclic voltammetry, the maestro's baton, gracefully wielded on a platinum electrode basking in molten NaOH at 550 °C. A material chosen for its chemical steadfastness, platinum graced the stage with cyclic voltammograms. The cathodic reverie, C<sub>1</sub>, whispers the



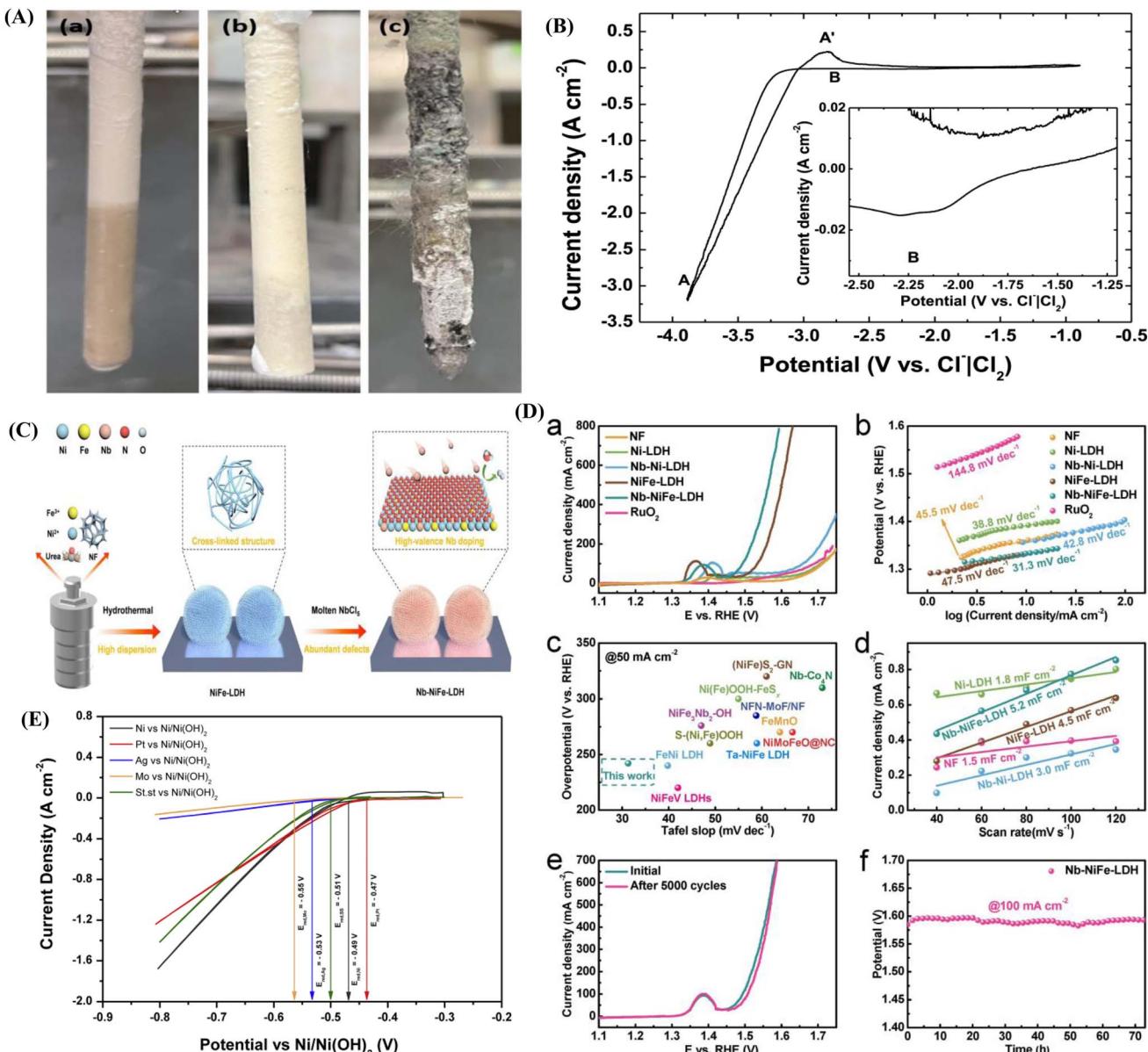


Fig. 4 (A) Depictions of (a) mullite tube reference electrode (RE), (b) MgO tube RE, and (c) Mg working electrode (WE) following a 31 days testing period. (B) Cyclic voltammograms recorded for a Pt plate electrode under Ar or NH<sub>3</sub> at 200 °C with a sweep rate of 20 mV/s. (C) Illustration of the synthesis process of Nb-doped Nb-NiFe-LDH via molten salt. (D) Electrochemical evaluations conducted in 1.0 M KOH, comprising (a) linear sweep voltammetry (LSV) curves for Nb-NiFe-LDH, NiFe-LDH, Nb-Ni-LDH, Ni-LDH, NF, and RuO<sub>2</sub> on NF, accompanied by (b) corresponding Tafel plots; (c) comparative assessment of overpotential at 10 mA/cm<sup>2</sup> and Tafel slopes compared to other catalysts; (d) calculation of the double-layer capacitance (C<sub>dl</sub>) value from cyclic voltammetry (CV) curves at 1.30 V vs. reversible hydrogen electrode (RHE); (e) polarization curves before and after 5000 CV scans; and (f) chronopotentiometric testing at 100 mA/cm<sup>2</sup>. (E) Comparison of cyclic voltammograms for Ni, Pt, Ag, Mo, and stainless steel working electrodes in molten hydroxide at 300 °C with a scan rate of 100 mV/s, utilizing a 0.5 mm Ni/Ni(OH)<sub>2</sub> reference electrode and a 5 mm stainless steel counter electrode with an immersion depth of 14 mm, under Ar gas at a flow rate of 40 cm<sup>3</sup>/min. Edited with permission from ref. 143–145. Copyright IOPscience ©2023, Elsevier ©2013, ©2022, and ©2020.

reduction of a platinum-clad oxide film; O<sub>1</sub>, anodic in nature, resounds oxidation. C<sub>2</sub>'s crescendo echoes the hydrogen evolution reaction, while O<sub>2</sub>, a sonnet, harmonizes with the oxygen evolution reaction. The saga extends as Ge *et al.*<sup>135</sup> venture into the realms of platinum wire, a virtuoso in three molten hydroxides NaOH-KOH at 280 °C, LiOH-NaOH, and LiOH-KOH at 270 °C. In NaOH-KOH's embrace, a cathodic crescendo at −0.32 V, a ballet of superoxide ions (O<sup>−2</sup>)

reduction, unravelled. Cyclic voltammetry gracefully revealed the nuances of a platinum (Pt) electrode in a molten hydroxide electrolyte, a narrative skillfully crafted by Yang *et al.*<sup>109</sup> Reduction and oxidation peaks pirouetted elegantly at distinctive potentials, with reduction currents exhibiting their dance below −0.55 V. The stage was then seized by a commanding oxidation peak between −0.55 V and 0.1 V, rising dramatically above 0.17 V, where the evolution of oxygen took center stage.<sup>109</sup>

In the presence of ammonia ( $\text{NH}_3$ ), an ethereal onset potential of approximately  $-0.67$  V marked the beginning of anodic currents, with a crescendo leading to a maximum of around  $-0.2$  V. However, the drama unfolded swiftly above  $0.15$  V as oxygen evolution claimed the spotlight. The forward scan from  $-0.2$  to  $0.15$  V witnessed a diminishing oxidation current, a subtle interplay involving Pt oxidation and the reduction of the active surface for ammonia oxidation. In a seamless transition, Yang *et al.*<sup>109</sup> continued their electrochemical tale, this time exploring the ammonia-driven drama on a platinum stage immersed in molten  $\text{NaOH-KOH}$  at  $200$  °C. Fig. 3(E) gracefully presented cyclic voltammograms, a visual symphony offering choices of argon and ammonia, while Ag stood as the stoic ref. 109. The dashed line served as a blank canvas, encapsulating platinum's narrative in the hydroxide embrace, while the solid line painted the enchanting transformation of ammonia to  $\text{N}_2$ , all harmonized by the eutectic molten hydroxides. The platinum electrode, a versatile protagonist, showcased its prowess in every experiment, contributing a lyrical stanza to the grand saga of electrochemistry.

### 5.3. Voltammetry of diverse metals in molten hydroxides

Embarking on a comprehensive exploration of electrode materials in molten hydroxides, the utilization of Cyclic Voltammetry (CV), a robust electrochemical method, revealed the complexities of reduction and oxidation processes of molecular species, offering insights into chemical reactions and catalysis initiated by electron transfer.<sup>141</sup> In Choi *et al.*'s investigation,<sup>142</sup> the study explores the durability of  $\text{Ag}/\text{Ag}^+$  reference electrodes in  $\text{MgCl}_2-\text{KCl-NaCl}$  molten chloride salts, providing crucial insights into their stability. Using open circuit potential (OCP) and cyclic voltammetry (CV) measurements, the research establishes the working electrode potential, ensuring the precision of cyclic voltammetry experiments. The evaluation of reference electrode materials, specifically comparing mullite and  $\text{MgO}$  in molten chloride salts, reveals in Fig. 4(A) that the pair of reference electrode tubes appear identical before and after the test, while the Mg rod undergoes dissolution/reaction, resulting in a rough surface and a tapered tip. This observation supports the assumption that the Mg rod dissolves and buffers the redox potential of the salt. Furthermore, the mullite-based reference electrode exhibits a drift rate of  $-1.34$  mV per day, emphasizing the importance of appropriate material selection to minimize potential drift.<sup>142</sup> Although the focus is on molten chloride salts, these findings hold valuable implications for optimizing cyclic voltammetry experiments on Ag metals in molten hydroxides.

In a separate study by Choi *et al.*,<sup>146</sup> the exploration of CV in molten hydroxides, particularly with Mg metals, takes center stage. The cyclic voltammetry (CV) technique allows for the qualitative and quantitative determination of various species in the electrolyte, surpassing open circuit potentiometry. The introduction of hydroxide ions and dissolved magnesium metal to the  $\text{MgCl}_2-\text{KCl-NaCl}$  salt mixture induces effects on redox potential and electrochemical behaviour. While presenting a solubility measurement of approximately  $0.0205$  wt% at  $500$  °C (Fig. 4(B)), the study acknowledges a high associated error,

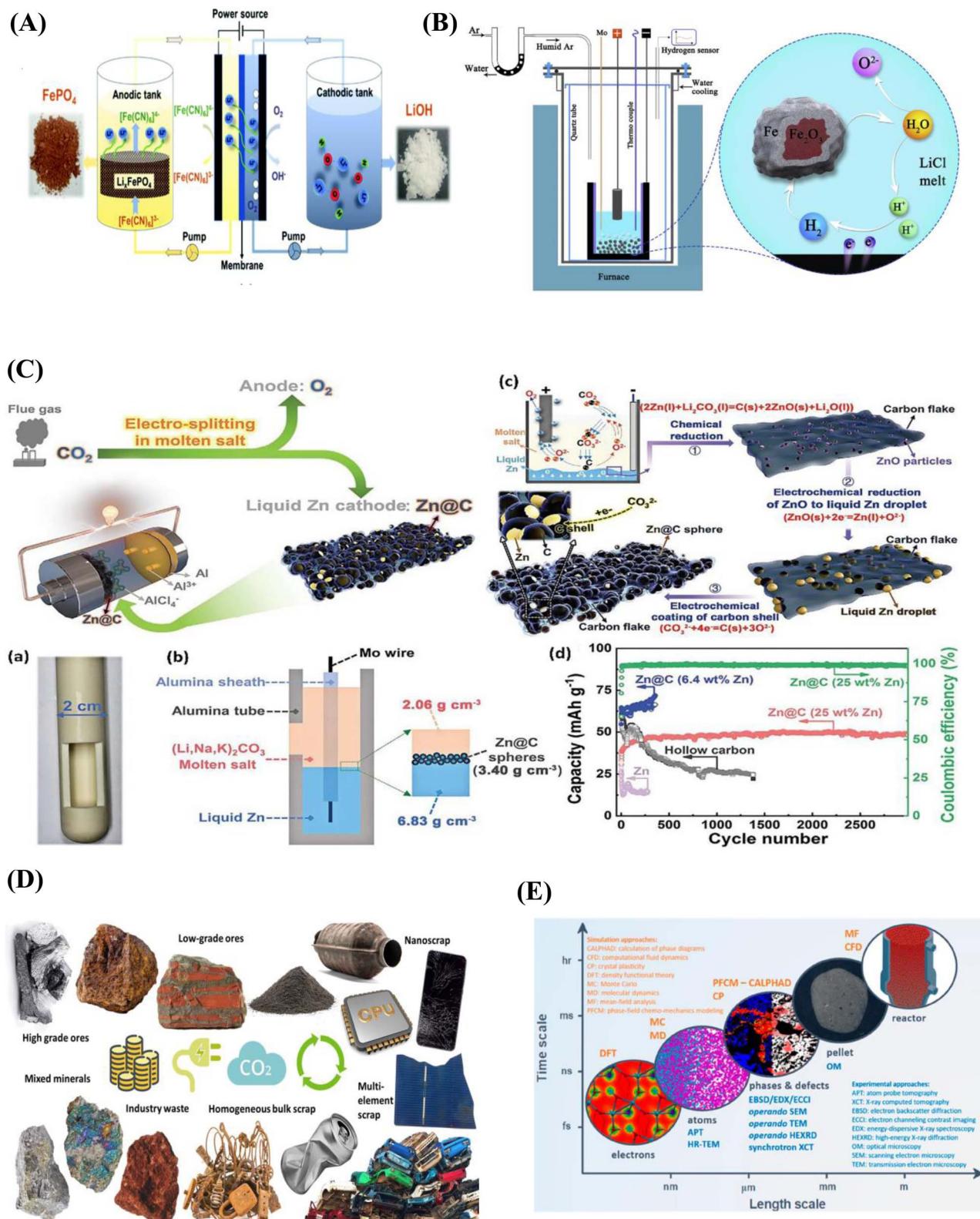
necessitating further understanding in future studies.<sup>143</sup> This study significantly enhances the understanding of the electrochemical behaviour of Mg metals in molten hydroxides. Turning attention to Zhou *et al.*'s<sup>147</sup> investigations, they delve into the synthesis process of Nb-doped Nb-NiFe-LDH *via* molten salt (Fig. 4(C)) and examine the effect of high-valence Nb doping in NiFe hydroxides on improving the oxygen evolution reaction (OER) in water splitting. The findings depicted in Fig. 4(D) underscore the remarkable electrochemical efficacy of Nb-NiFe-LDH, as demonstrated by a notable decrease in overpotential at  $50$  mA/cm $^2$  from  $280$  mV (for NiFe-LDH) to  $242$  mV with Nb doping, signifying considerable advantages for the oxygen evolution reaction. This observation finds further reinforcement in the overpotential values recorded for Ni-LDH (428 mV) and Nb-Ni-LDH (342 mV). Tafel slopes reveal that Nb-NiFe-LDH (31.3 mV/dec) exhibits enhanced electron transport compared to NiFe-LDH (47.5 mV/dec), NbNi-LDH (42.8 mV/dec), and Ni-LDH (38.8 mV/dec), thus accelerating OER kinetics. Electrochemical Impedance Spectroscopy (EIS) at  $1.37$  V *vs.* RHE illustrates the commendable electrode conductivity and electron transfer rate of Nb-NiFe-LDH, as indicated by the smallest fitted semicircle diameter.<sup>147</sup>

Calculations of double-layer capacitance ( $C_{dl}$ ) from cyclic voltammetry curves highlight Nb-NiFe-LDH's larger  $C_{dl}$  value ( $5.2$  mF/cm $^2$ ) compared to NiFe-LDH ( $4.5$  mF/cm $^2$ ), Nb-Ni-LDH ( $3.0$  mF/cm $^2$ ), and Ni-LDH ( $1.8$  mF/cm $^2$ ), indicating a higher exposure of effective active sites through Nb integration.<sup>147</sup> These comprehensive findings significantly advance our understanding of electrochemical processes, providing valuable insights for optimizing cyclic voltammetry experiments in both chloride and hydroxide systems. Comparing various working electrodes (Ni, Pt, Ag, Mo, and St. st) in eutectic molten hydroxide at  $300$  °C using a potential scan rate of  $100$  mV/s, each electrode displayed a unique reduction potential value.<sup>145</sup> Platinum had the most positive reduction potential value, followed by nickel and then stainless steel (Fig. 4(E)). Silver and molybdenum electrodes demonstrated lower reduction potential values. The obtained reduction potential values are consistent with previous literature findings, highlighting the uniqueness of each working electrode. The values, ranging from approximately  $-0.47$  V for platinum (Pt) to  $-0.56$  V for molybdenum (Mo), underscore the diverse electrochemical characteristics of these materials.<sup>145</sup> In conclusion, this collective exploration sheds light on crucial aspects of electrode stability, material selection, and electrochemical behaviour in molten hydroxides, providing valuable insights for optimizing future cyclic voltammetry experiments.

## 6. Emerging techniques for hydrogen evolution from eutectic hydroxide molten salts

Molten salt electrolysis is recognized as a "clean technology" for extracting metals from waste materials, concurrently generating pure  $\text{O}_2$  gas. Its adaptability, particularly in noble metal recovery, capitalizes on a broad operating temperature range





**Fig. 5** (A) Illustrated depiction outlining the regenerative redox targeting-based recycling process for spent  $\text{LiFePO}_4$  material. (B) Schematic representation of hydrogen production through molten salt and its subsequent application in the direct reduction of suspended  $\text{Fe}_2\text{O}_3$  powders within the melt. (C) Diagrammatic representation of electrochemical  $\text{CO}_2$  fixation in molten salts utilizing a liquid Zn cathode. (a) The alumina tube sealed at one end, (b) configuration of the liquid Zn cathode, and (c) formation of  $\text{Zn@C}$  spheres with a core–shell structure within a carbon flake. (D) Overview emphasizing key aspects of the direct sustainability of metallic materials. (E) Illustration showcasing various scales concerning kinetic and thermodynamic simulations and experiments, focusing on the solid-state direct reduction of iron oxides using hydrogen. Edited with permission from ref. 152–155. Copyright ACS ©2020, Elsevier ©2023, ©2019 and ACS ©2023.



and an expansive electrochemical window.<sup>148</sup> Despite its potential, widespread implementation for metal recovery faces hurdles related to cost-effectiveness. The elucidation of metal recovery methods reveals a reliance on electrodeposition, which deposits metal in pores as small as 10 nm, enabling the characterization of microscopic pore-throat systems. Additionally, electrodeposition allows for the examination of features that cannot be directly observed due to its large observation area.<sup>149</sup> Additionally, electrorefining supplements purification, offering advantages like a wider operating temperature range, effective digestion of refractory borides and carbides, and favourable coating formation. This process enhances the purity of crude metals from approximately 99 to over 99.9%.<sup>150</sup>

The versatility of molten salt electrorefining is evident in the recovery of metals such as tungsten, cobalt, manganese, zirconium, lead, uranium, silicon, and ruthenium.<sup>151</sup> Tailored techniques like selective electrodeposition and electrorefining for specific metals such as Te, Cu, U, and actinides enhance efficiency and reduce radioactive sludge formation, contributing to overall process sustainability. Additionally, Fig. 5(A) illustrates a schematic diagram delineating the recycling process based on regenerative redox targeting for used LiFePO<sub>4</sub> material, facilitating comprehension of the steps and compartments involved in recycling LiFePO<sub>4</sub> material using the regenerative redox targeting method.<sup>151</sup> Shen *et al.*<sup>156</sup> explore the diverse applications of hydrogen generated in molten salts, showcasing its potential for large-scale production of advanced carbon nanostructures. The molten salt-assisted electrolysis strategy emerges as an innovative pathway for reducing CO<sub>2</sub> and H<sub>2</sub>O into syngas and hydrocarbon fuels. Operating in molten salts as a reaction solvent, this process benefits from high thermal stability and outstanding CO<sub>2</sub> dissolving capacity, further amplified by the integration of renewable solar energy.<sup>156</sup> This green and efficient electrolysis process converts CO<sub>2</sub> into valuable carbon nanostructures, leveraging rapid ion migration and diffusion, high thermal stability, and superior CO<sub>2</sub> dissolving capacity offered by molten salts. Moreover, the method shows promise for large-scale production of advanced carbon nanostructures, capitalizing on the hydrogen generated in molten salts. Notably, the glassy carbon retains its initial characteristics post-electrolysis.<sup>156</sup> At 650 °C, thick carbon sheets assemble from quasi-spheres, while at 750 °C, fiber-like nanostructures of hollow multi-walled CNTs measuring 20 nm in diameter and having a wall thickness ranging from 5 to 10 nm appear.<sup>156</sup>

Moreover, carbon materials originating from chitosan *via* a single-step carbonization process using LiCl-ZnCl<sub>2</sub> molten salt exhibit a substantial specific surface area of 2025 m<sup>2</sup>/g and a significant nitrogen content of 5.1 wt%. These materials demonstrate noteworthy CO<sub>2</sub> uptake under various temperatures and pressures.<sup>157</sup> The conversion of PET into nitrogen-doped porous carbon using melamine and ZnCl<sub>2</sub>/NaCl eutectic salts at 550 °C yields a considerable specific surface area of 1173 m<sup>2</sup>/g and abundant nitrogen dopants. Additionally, porous biochar derived from wood waste with eutectic molten salts shows enhanced CO<sub>2</sub> sorption, with the most efficient biochar displaying the highest CO<sub>2</sub> uptake and selectivity.<sup>157</sup> Furthermore, N-doped microporous carbons synthesized from

melamine and sucrose using molten LiCl/KCl salts show significant CO<sub>2</sub> uptake under specific conditions. Fig. 5(B) elucidates the specific steps and conditions integral to the borate-enhanced molten salt electrolysis process, directing the mass production of sophisticated carbon nanostructures of high worth using hydrogen produced within molten salts.<sup>152</sup> Additionally, Fig. 5(C) illustrates a schematic representation of the process where hydrogen produced in molten salt is employed for the direct reduction of suspended Fe<sub>2</sub>O<sub>3</sub> powders in the melt.<sup>155</sup> This sustainable method involves the electrochemical decomposition of water in molten salt, generating hydrogen gas that reduces Fe<sub>2</sub>O<sub>3</sub> particles to metallic iron.

Furthermore, the remarkable faradaic efficiency of approximately 94.5% in the one-pot generation of syngas through CO<sub>2</sub> electrolysis at a low temperature of 450 °C is achieved by utilizing renewable solar energy for electricity generation and concentrated solar light for eutectic melting.<sup>152</sup> The research also highlights achievements in the electrolysis of CO<sub>2</sub> to produce a range of hydrocarbon fuels utilizing eutectic molten salts. Raabe *et al.*<sup>153</sup> further explore the potential of electrochemical hydrogen generation in high-temperature molten salts as a versatile method for producing metals and alloys. The electrolysis procedure entails conducting an electrical current through a molten salt electrolyte containing metal ions, resulting in the deposition of metals and alloys on the cathode. During the electrochemical fabrication of graphene in molten LiCl, the procedure produced interconnected graphene nanosheets/nanoscrolls. The reduced graphene exhibited a specific surface area of 565 m<sup>2</sup>/g and a specific capacitance of 255 F/g. Even after 5000 charge/discharge cycles in 6 M KOH, it retained 95% of its capacitance.<sup>158</sup> Additionally, the electrochemical etching process using molten salt to produce carbide-derived carbon (CDC) demonstrated encouraging outcomes. For example, employing a molten salt (CaCl<sub>2</sub>) electrochemical etching method on silicon carbide led to the creation of porous nanospheres, exhibiting a specific capacitance of 176 F/g at 1 A/g in a 6 M KOH electrolyte.<sup>159</sup> Notably, this electrochemical method excels in producing exceptionally pure metals, utilizing sustainable electrical energy sources like wind or hydropower directly.<sup>160</sup> This makes it an attractive alternative to conventional reduction methods reliant on fossil reductants. Moreover, integrating renewable electrical energy in electrolytic cells contributes to higher overall efficiency.

Challenges accompany this technology as the high operating temperatures required for electrolysis can induce aggressive interactions with electrodes and insulation materials. The development of carbon-free electrode materials becomes crucial to minimize CO<sub>2</sub> emissions.<sup>161</sup> Additionally, the variability in sustainable electrical power supply, particularly from sources such as solar or wind energy, underscores the need to design electrolysis cells capable of adapting to variable power supply and interruptions. Fraction of Renewable Energy System values exhibit variation across different scenarios and months, with a fluctuation range of 30–35%. The fluctuations mainly stem from seasonal shifts in renewable resources and changes in demand.<sup>162</sup> Fig. 5(D) provides a comprehensive summary of the crucial aspects of direct sustainability in metallic materials



production, including various ores, such as low-grade and high-grade, used for synthesizing metals from mineral raw materials, as well as the utilization of scrap and waste as alternative feedstock sources.<sup>153</sup> Additionally, Fig. 5(E) illustrates the intricate multi-scale nature of simulations and experiments related to kinetics and thermodynamics involved in the hydrogen-driven solid-state reduction of iron oxides, providing a visual representation of the process's complexity.<sup>153</sup> In conclusion, electrochemical hydrogen generation in high-temperature molten salts offers a promising approach to the sustainable production of metals and alloys. This method utilizes renewable electrical energy sources and has different conversion efficiencies depending on the energy source used. For example, solar PV + electrolysis has a conversion efficiency of 10.5%, while wind + electrolysis, hydroelectric + electrolysis, and tidal + electrolysis has a conversion efficiency of 70%.<sup>163</sup> These technologies are at different stages of development, as indicated by their technology maturity level (TML) ratings. Ongoing research and development efforts are essential to address challenges related.<sup>163</sup>

## 7. Challenges and prospects of molten hydroxide electrolysis

Molten hydroxide electrolysis, which operates at high temperatures, presents both significant challenges and promising prospects. One primary challenge is the need for materials that can withstand the highly corrosive environment created by molten hydroxides, often exceeding 200 °C.<sup>164</sup> For example, 316 L stainless steel exhibits a corrosion rate of up to 18 mm per year in aerated 50 wt% NaOH at 90 °C, highlighting the difficulty in maintaining long-term material stability.<sup>165</sup> Recent studies have shown that catalysts such as Ag-nanowires/NiFeCrAl foam and certain cobalt oxides can remain stable for several hundred hours at temperatures up to 200 °C, achieving impressive current densities up to 3.75 A/cm<sup>2</sup> at 1.75 V.<sup>166</sup> Another significant challenge is the efficiency losses due to heat dissipation, which impacts the effective conversion of energy into hydrogen. The Faraday efficiency for mixed NaOH and KOH at 500 °C is only 28%, although using LiOH at higher pressure can improve this efficiency to 88%. Additionally, the high operating temperatures can lead to increased operational costs. For example, operating at 450 °C can increase energy costs by approximately 20–30% compared to lower temperature processes.

Scaling up from laboratory to industrial-scale operations also poses difficulties, particularly in maintaining efficiency and managing costs. Laboratory setups achieving high efficiencies often do not translate directly to industrial applications, with efficiency drops of around 5–10%.<sup>167</sup> Furthermore, the safe handling of molten salts at high temperatures is critical to prevent accidents, as any spillage or leak can cause severe burns and equipment damage. Managing these materials in large-scale operations introduces additional safety and regulatory concerns. Despite these challenges, the prospects for molten hydroxide electrolysis are compelling. The high

operating temperatures significantly enhance reaction kinetics, reducing overvoltages and improving overall efficiency. Studies have reported a reduction in cell voltage by 3.4 to 4 mV/K between 100 °C and 200 °C, substantially higher than the thermodynamic reduction of 0.8 mV/K for liquid water in the same range. Additionally, the conductivity of the electrolyte, particularly KOH solutions, increases with temperature, further boosting efficiency. Ongoing research into more efficient and durable catalysts is critical for advancing molten hydroxide electrolysis. For instance, NiFeO<sub>x</sub>H<sub>y</sub> nanosheets have demonstrated impressive performance characteristics, with a low overpotential of 216 mV in freshwater electrolytes and 232 mV in saline solutions.<sup>168</sup> These nanosheets show exceptional stability, maintaining functionality for 1000 hours at a current density of 0.1 A/cm<sup>2</sup> in freshwater electrolytes and for 550 hours at 1 A/cm<sup>2</sup> in saline solutions. The Tafel slope of these nanosheets is as low as 51 mV/dec, indicating efficient kinetics and a rapid increase in current density with increasing overpotential. Their robust nanosheet structure provides abundant electroactive sites, reduces charge transfer resistance ( $R_{ct}$  of 1.54 Ω), and enhances mechanical stability, allowing for efficient mass and charge transfer.<sup>168</sup>

The development of new materials that can better withstand harsh conditions could reduce maintenance costs and improve system longevity. Ni-based alloys, for example, show promise due to their durability in molten hydroxide environments. Integrating advanced materials and nanostructures in these catalysts could significantly enhance the lifespan and efficiency of molten hydroxide electrolysis systems, reducing the need for frequent catalyst replacement and lowering overall operational costs. Furthermore, integrating renewable energy sources, such as solar or wind power, with molten hydroxide electrolysis could significantly lower operational costs, potentially reducing the overall cost of hydrogen production by 15–20%.<sup>169</sup> Process optimization techniques, such as advanced thermal management and automated control systems, can improve efficiency by 10–12%, making operations more cost-effective. For instance, an ET-PEMFC system using concentrated solar power and thermal energy storage showed improved overall efficiency and operational flexibility. As technology advances and production scales up, the cost of hydrogen production through molten hydroxide electrolysis could become competitive with traditional methods. With technological advancements and increased production scales, the cost of hydrogen production could potentially lower to below \$2 per kilogram of hydrogen, making it a viable option for large-scale hydrogen production.<sup>169</sup> For example, a PtM system utilizing a LSGM-based tubular SOEC stack achieved a CO<sub>2</sub>-to-CH<sub>4</sub> conversion ratio of 98.7% and a PtG efficiency of 94.5%, demonstrating the potential for economic feasibility and large-scale application.<sup>170</sup>

## 8. Conclusions

In conclusion, this review has provided a comprehensive exploration of hydrogen gas production from steam through eutectic molten hydroxide electrolysis. The investigations incorporated cyclic voltammetry and amperometry techniques



to predict electrolysis reactions, establishing correlations between process efficiency and various experimental parameters. The direct electrolysis of steam through eutectic molten hydroxide was examined using different analysis techniques, including hydrogen gas tube detection and hydrogen gas sensors, with quantification performed through the water displacement technique. A significant breakthrough is the study of ionic membranes for the nickel reference electrode. The mullite membrane exhibits superior stability compared to alumina within the eutectic molten hydroxide, extending the reference electrode's lifespan to 9 days. Mullite-covered electrodes effectively control the potential of platinum working electrodes, yielding high cathodic products (hydrogen gas). Cyclic voltammetry results for various working electrodes unveil a distinct order in hydrogen evolution reaction reduction potential: Pt > Ni > SS > Ag > Mo. The nickel reference electrode crafted shows efficiency in molten hydroxide environments, a novel achievement. Direct electrolysis with nickel, platinum, and stainless-steel cathodes shows increased current with higher temperatures and voltages. At 300 °C, current efficiencies are 90.5, 68.6 and 80% for nickel, platinum, and stainless-steel cathodes, respectively. Utilizing a graphite anode doesn't enhance hydrogen production; instead, efficiency decreases. Nickel emerges as the most efficient cathode in eutectic molten hydroxide. The study also discusses various aspects of hydrogen evolution from molten salts, emphasizing its applications in renewable development. Looking forward, future work is essential for process optimization. Integrating the electrochemical cell with renewable sources, exploring diverse molten hydroxide mixtures, investigating electro-catalytic cathodic metals, studying cathode-anode distance impact, and exploring additives to reduce bubble formation are key. These recommendations pave the way for enhancing efficiency and sustainability in hydrogen gas production through eutectic molten hydroxide electrolysis.

## Nomenclature

HER	Hydrogen evolution reaction
OER	Oxygen evolution reaction
PTFE	Polytetrafluoroethylene
$\Delta E$	Potential difference
$\Delta G$	Gibbs free energy
$\Delta H$	Enthalpy change
$\Delta S$	Entropy change
$A_0$	Frequency factor
$C_0$	Concentration of the reactant
$C_R$	Concentration of the product
$E$	Potential
$E_A$	Activation energy
$E_{\text{cell}}^{\circ}$	Equilibrium potential
$E_{\text{pa}}$	Anodic peak potential
$K_{\text{eq}}$	Reversible constant
$K_0$	Standard rate constant
$Q_E$	Thermal energy
$R$	Gas constant

$R'_1$	External electric resistance at cathode
$R_{\text{anode}}, R_{\text{cathode}}$	Resistance of the electrodes
$R_{\text{bubble}, \text{H}_2}$	Resistance of hydrogen bubbles
$R_{\text{bubble}, \text{O}_2}$	Resistance of oxygen bubbles
$R_{\text{ions}}$	Resistance of electrolyte
$R_{\text{membrane}}$	Resistance of membrane
$H$	Overpotential of the reaction
$K$	Electrical conductivity

## Data availability

Data will be made available on request.

## Conflicts of interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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