


Cite this: *RSC Adv.*, 2024, 14, 39937

# Effect of catholyte in a single step electrochemical hydroiodic acid decomposition for hydrogen production using the iodine–sulfur thermochemical cycle

Ashwin Yashawanth Hegde,<sup>a</sup> Saroj Chaudhary,<sup>b</sup> Parvatalu Damaraju<sup>b</sup> and Pradeep Kumar Sow<sup>ib</sup>\*<sup>a</sup>

This study identifies the most suitable catholyte for the electrochemical HI decomposition process, an emerging single-step alternative to the conventional multistep HI section of the I–S thermochemical cycle for hydrogen production. Four catholytes, H<sub>2</sub>O, H<sub>3</sub>PO<sub>4</sub>, H<sub>2</sub>SO<sub>4</sub>, and HI, were shortlisted based on compatibility with the I–S cycle and ability to support the hydrogen evolution. Polarization studies in a two-compartment electrochemical cell revealed a similar order of onset potentials for the electrochemical HI decomposition across all four catholyte electrolytes. However, the performance at higher overpotentials following the onset of the electrochemical HI decomposition followed the order H<sub>2</sub>SO<sub>4</sub> > HI > H<sub>3</sub>PO<sub>4</sub> > H<sub>2</sub>O. The polarization behavior was not found to vary significantly with the catholyte concentration. Model fitting revealed that the invariance in polarization behavior with the catholyte concentration arose from the compensation between the changes in activation overpotentials with the open-circuit voltage. The onset potential was predominantly influenced by the I<sub>2</sub>/HI ratio in the anolyte, with higher ratios resulting in an increase in the onset potentials for electrochemical HI decomposition. Polarization studies identified H<sub>2</sub>SO<sub>4</sub> and HI as the most promising catholytes for further investigation. Consequently, continuous electrochemical HI decomposition and hydrogen production was demonstrated with H<sub>2</sub>SO<sub>4</sub> and HI as the catholyte for three I<sub>2</sub>/HI ratios of 0.25, 0.5, and 1 at two different current densities, with an average current efficiency of ~97%. Among the two acids, H<sub>2</sub>SO<sub>4</sub> showed higher current efficiency and lower energy consumption per mole of hydrogen compared to HI under the similar anolyte configuration and current density.

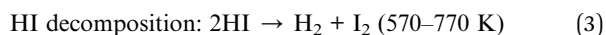
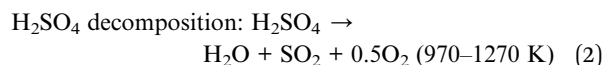
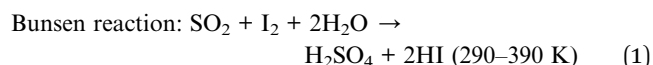
Received 21st October 2024  
Accepted 13th December 2024

DOI: 10.1039/d4ra07522f

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## 1. Introduction

Hydrogen is an efficient energy carrier and, when derived from renewable energy sources such as solar, wind, or nuclear, has the potential to be a carbon-neutral fuel and thereby reduce greenhouse gas emissions. In addition to the direct water electrolysis, the thermochemical cycles, especially the iodine–sulfur (I–S) thermochemical cycle, has been considered a promising approach suitable for large-scale hydrogen production.<sup>1</sup> The I–S thermochemical cycle is a promising green hydrogen production strategy that can integrate renewable energy sources like solar, wind, or nuclear power.<sup>2</sup> Overall, the I–S thermochemical cycle comprises three primary reactions, namely the Bunsen reaction, the hydroiodic acid (HI) decomposition reaction, and the sulfuric acid (H<sub>2</sub>SO<sub>4</sub>) decomposition reaction, as given below:



Various studies and reports on the thermochemical cycles have consistently listed the I–S thermochemical cycle as one of the promising thermochemical cycle for large-scale hydrogen production.<sup>1,3–5</sup> Studies have shown that the I–S thermochemical cycle can attain thermal efficiencies greater than 50%.<sup>6,7</sup> The open-loop variant of the I–S thermochemical cycle offers a significant simplification by omitting the H<sub>2</sub>SO<sub>4</sub> decomposition step. This elimination of the H<sub>2</sub>SO<sub>4</sub> decomposition step not only simplifies the process but also yields H<sub>2</sub>SO<sub>4</sub> as a valuable byproduct, which has considerable commercial significance.<sup>8</sup> Sulfuric acid is in high demand across various sectors of the chemical industry, particularly in producing fertilizers, where it is required in substantial quantities. Additionally, this

<sup>a</sup>Department of Chemical Engineering, BITS Pilani, K K Birla Goa Campus, Zuarinagar, Goa 403726, India. E-mail: pradeeps@goa.bits-pilani.ac.in

<sup>b</sup>Oil and Natural Gas Corporation (ONGC) Energy Centre, India



modification enhances the overall thermal efficiency of the open-loop I-S cycle, achieving values exceeding 81%.<sup>6</sup> Nevertheless, the above process does involve multiple challenges, such as the need for high temperatures, holdup of materials, excess amount of iodine and water requirement, which increases the energy consumption in the HI section, high iodine ( $I_2$ ) losses, and the highly corrosive nature of the chemicals used.<sup>9,10</sup> In addition to the above, the precipitation of iodine and the associated clogging of pipes also present significant challenges for the I-S cycle.<sup>11</sup> Various recent studies have elaborated on the system modelling-based assessment of the thermochemical I-S cycle.<sup>12,13</sup> Many of the I-S thermochemical cycle challenges are associated with the HI section, originating with the Bunsen reaction. The Bunsen reaction produces an  $HI-I_2-H_2O$  mixture, referred to as the  $HI_x$  solution. The phase separation of the two acids phases, HI and  $H_2SO_4$ , produced in the Bunsen reaction is achieved when  $I_2$  is in excess.<sup>14</sup> Furthermore, excess water is required to make the reaction thermodynamically favorable.<sup>15</sup> The excess reactants are further required to reduce the side reactions associated with the Bunsen reaction.<sup>16</sup> A significantly high amount of energy is required to process the excess water and iodine in the stream, resulting in a high energy demand for the HI section.<sup>17,18</sup> It is to be noted that both the acids produced in the Bunsen reaction are required to be concentrated before the decomposition process. However, the concentration process for the HI produced in the Bunsen reaction is complicated by the formation of azeotrope, which renders the conventional distillation-based separation redundant. Consequently, alternative concentration strategies are employed, including electro-electrodialysis,<sup>8,9</sup> extractive distillation,<sup>10</sup> *etc.* Recently, pressure-swing distillation method has also been reported for the purification of HI from the  $HI_x$  ( $HI-I_2-H_2O$ ) mixture.<sup>19</sup> In addition to the significant energy requirement of the HI section, the  $HI_x$  solution is highly corrosive, requiring unique corrosion resistance materials, significantly increasing the associated capital costs.<sup>20</sup> Specifically, it has been observed that the  $HI_x$  present in the HI section is far more corrosive than HI alone.<sup>21</sup> The need for multiple processing steps further exacerbates the high capital requirement for fabricating corrosion-resistant materials. The conventional thermal HI decomposition also suffers from low conversion efficiency, where most of the reported studies found the HI decomposition conversion to be within 20–30%.<sup>22</sup> Advanced designs such as the use of U-shaped decomposer for the HI decomposition reaction have also been developed, where the HI conversion has been found up to ~22%.<sup>23</sup> For the scale up designs of the continuous HI decomposer using a Pt-Ir/C catalyst with the  $H_2$  production rate of  $100\text{ L h}^{-1}$ , the HI decomposition rate was approximately 22%.<sup>24</sup> The lower conversion increases the quantity of recycled chemicals, thereby increasing the cycle energy demand.

As an alternative to the pre-concentration step followed by thermal HI decomposition, an electrochemical HI decomposition strategy can realize hydrogen production at lower temperatures without needing the above azeotropic composition of HI. The generalized scheme of electrochemical HI decomposition cell involves a two-compartment electrochemical cell, separated

by an ion exchange membrane, with each compartment housing the cathode and the anode.<sup>25–30</sup> The hydrogen evolution reaction (HER) occurs at the cathode through the proton reduction, while iodide and tri-iodide ion oxidation occurs at the anode.<sup>26,30</sup> The output  $HI_x$  from the Bunsen reaction serves as the anolyte. The effect of the  $HI_x$  concentration in the anolyte on the performance of the electrochemical HI decomposition has been reported.<sup>27,30</sup> Cation exchange membranes, including commercial Nafion membrane,<sup>26</sup> and sulfonated (PVDF-co-HFP)-graphene oxide composite polymer electrolyte membrane,<sup>25</sup> have been studied for their effectiveness in the process. In most of the reported studies, a constant hydrogen production rate has been demonstrated.<sup>26,27</sup> Flowsheet development for the integrated electrochemical HI decomposition demonstrated thermal efficiencies ranging from 25–42%, depending on waste heat utilization, and 33.3% considering internal heat exchange.<sup>27</sup> Additional simulation studies showed the energy and exergy efficiencies estimated to be 15.3–31.0% and 32.8%, respectively. Most exergy destruction occurred in the  $H_2SO_4$  decomposer and condenser, accounting for 93.0% and 63.4%, respectively. The electrochemical HI decomposition has been shown to have a high exergy efficiency of 92.4% when integrated with I-S cycle.<sup>28</sup> In most previously reported studies, water has been widely employed as the catholyte.<sup>25–29</sup> In addition, HI and  $H_2SO_4$  have also been reported as the catholytes for realizing electrochemical HI decomposition.<sup>30–32</sup> However, the choice of catholyte and the impact of the catholyte concentration on the performance of electrochemical HI decomposition has not been reported. Since the catholyte contributes significantly towards the overpotential losses, it is crucial to investigate the influence of the catholyte on system performance.<sup>30</sup>

Here, we have shortlisted four potential electrolytes and have conducted a detailed analysis of the effect of catholyte and their concentration on the electrochemical interactions and the performance of the electrochemical HI decomposition system. The impact of electrolytes on HER was initially studied using a three-electrode setup, and the electrochemical HI decomposition system's performance was assessed through polarization ( $I$ - $V$ ) curves. Experimental data were modelled to identify overpotential components and understand variations in behavior. Additionally, we analyzed the emergent effects of  $I_2$ /HI ratio changes in the anolyte for each catholyte. Based on these findings, we selected HI and  $H_2SO_4$  for further continuous flow studies, where hydrogen production was successfully demonstrated, and performance parameters, including current efficiency and energy consumption, were evaluated. Among the studied catholytes,  $H_2SO_4$  offers the best performance with the lowest energy requirement and highest current efficiency. The crucial insights gained from this research can assist in further scaleup studies and the operation of the new scheme for the I-S cycle with integrated electrochemical HI decomposition.

## 2. Experimental section

### 2.1 Materials

HI (57%; Loba Chemicals, India) and  $I_2$  (99.8%; Loba Chemicals, India) were utilized to prepare the anolyte solutions in



deionized water with three different I<sub>2</sub>/HI ratios of 0.25, 0.5, and 1. Sulfuric acid (H<sub>2</sub>SO<sub>4</sub>) (98% extra pure; Loba Chemicals), phosphoric acid (H<sub>3</sub>PO<sub>4</sub>) (85% extra pure; Loba Chemicals), and hydroiodic acid (57%; Loba Chemicals, India) and deionized (DI) water were used for the preparation of the catholyte. The chemicals were used without any further processing or refinement procedures. Platinum electrodes (99.9%) procured from Fisher Scientific Pvt Ltd, measuring 25 mm × 25 mm and with a thickness of 0.25 mm, were utilized as electrodes for the two-compartment cell investigations. Nafion-117, procured from Fisher Scientific Pvt Ltd, was used as the proton exchange membrane (PEM) separator.

## 2.2 Catholyte selection for electrochemical HI decomposition

In principle, any proton source can facilitate the HER and thus function as a catholyte. Consequently, there exists a multitude of potential candidates for catholyte, presenting a challenge in terms of selection and performance evaluation. To address this, we have first streamlined this extensive list by prioritizing electrolytes compatible with the I–S cycle, capable of HER drawing inferences from the previously reported studies. The rationale guiding the selection of these electrolytes is elaborated below. In addition to being the most widely reported catholyte for the electrochemical HI decomposition, water is present throughout the I–S cycle and thus possesses the least potential for contamination and impacting associated processes.<sup>25–29</sup> The earlier studies on the electrochemical HI decomposition with water as a catholyte establish the feasibility of HER with water. Water has the lowest cost among all the catholytes considered here, thus amplifying its appeal as a catholyte for electrochemical HI decomposition.

H<sub>3</sub>PO<sub>4</sub> is a proton source and has been utilized as an electrolyte for the HER.<sup>33</sup> The use of H<sub>3</sub>PO<sub>4</sub> has been demonstrated in earlier schemes of the I–S cycle in the HI section.<sup>34,35</sup> Furthermore, H<sub>3</sub>PO<sub>4</sub> being extremely hygroscopic, has been used to purify the HI<sub>x</sub> solution from the Bunsen reaction by breaking an azeotropic mixture comprising HI and H<sub>2</sub>O. H<sub>3</sub>PO<sub>4</sub> has also been used in the precipitating agent-based approach for conducting Bunsen reactions.<sup>36</sup> Based on the established compatibility with the I–S cycle, we have shortlisted H<sub>3</sub>PO<sub>4</sub> as a potential candidate for the catholyte section of the electrochemical HI decomposition.

H<sub>2</sub>SO<sub>4</sub> is the most commonly reported electrolyte for HER studies and electrolysis experiments. Furthermore, H<sub>2</sub>SO<sub>4</sub> is one of the existing chemical components within the traditional and current scheme of the I–S thermochemical cycle as a part of the sulfur section. During the Bunsen reaction, H<sub>2</sub>SO<sub>4</sub> interacts with the HI<sub>x</sub> phase directly, as in the traditional Bunsen reaction scheme, or indirectly, as in the membrane-based Bunsen reaction strategy.<sup>37,38</sup> Cross-contamination was also observed during the HI<sub>x</sub> and H<sub>2</sub>SO<sub>4</sub> phase interactions across a Nafion 117 ion exchange membrane.<sup>39</sup> However, the presence of H<sub>2</sub>SO<sub>4</sub> in HI solution has not been found to affect the iodide electro-oxidation occurring in the anodic section.<sup>31</sup> Furthermore, the electrochemical HI decomposition has been demonstrated with

H<sub>2</sub>SO<sub>4</sub> as the catholyte.<sup>31,32</sup> Based on the established compatibility and minimal effect on the iodine–iodide redox reactions, we have shortlisted H<sub>2</sub>SO<sub>4</sub> as a potential catholyte for the electrochemical HI decomposition.

HI is the common component with the anolyte section of the electrochemical HI decomposition cell system and, therefore, has the least potential for foreign component contamination compared to all the above-discussed acids. Our earlier work demonstrated the potential for hydrogen production using HI as the catholyte in an electrochemical HI decomposition system, supporting the use of HI as the potential catholyte.<sup>30</sup> Based on the above discussion the four potential catholytes selected for the electrochemical HI decomposition are: H<sub>2</sub>O, H<sub>3</sub>PO<sub>4</sub>, H<sub>2</sub>SO<sub>4</sub> and HI.

## 2.3 Three-electrode studies

A standard three-electrode glass cell (ALS Co. Ltd) was used for the cyclic voltammetry (CV) studies. The three-electrode studies were conducted with a platinum disk (0.5 mm diameter) as the working electrode, Ag/AgCl as reference electrode, and platinum coil as a counter electrode, respectively. The platinum working electrode was cleaned by polishing on a polishing pad before each experiment using alumina powder (0.05 micron). The studies were conducted for four electrolytes: H<sub>2</sub>SO<sub>4</sub>, H<sub>3</sub>PO<sub>4</sub>, HI, and water. The concentration of the three acids used in this study was maintained at a constant 0.5 M.

## 2.4 Electrochemical studies with small-volume two-compartment cell

A small size batch scale two-compartment cell was used for the polarization studies with the cell design described in our previous work.<sup>30</sup> Reduced electrolyte requirements with the miniaturized cell significantly lowered both testing costs and the generation of waste electrolytes. Overall, the cell body coming in contact with the electrolyte was fabricated with Teflon. The two compartments were separated by Nafion 117 membrane, and each of the two compartments housed a platinum plate electrode with exposed circular area of 10 mm diameter. The volume of each compartment was 0.785 ml. Programmed chronoamperometry was used to evaluate the polarization data, where the current was evaluated at varying voltage values. The electrochemical studies for the two-compartment cell and the three-electrode system were conducted utilizing BioLogic SAS VSP electrochemical workstation.

## 2.5 Model for the polarization curve studies

The total voltage (*V*) in the electrochemical system comprises the contribution from the open circuit voltage (OCV), voltage loss to realize the charge transfer, referred to as the activation overpotential ( $\Delta V_{\text{act}}$ ), ohmic overpotential ( $\Delta V_{\text{ohmic}}$ ) and the mass transfer overpotential ( $\Delta V_{\text{MT}}$ ) represented mathematically as:<sup>40,41</sup>

$$V = \text{OCV} + \Delta V_{\text{act}} + \Delta V_{\text{ohmic}} + \Delta V_{\text{MT}} \quad (4)$$



Asymmetric electrolyte composition in the anolyte and the catholyte section and the resulting difference in the activity of the electrochemical species give rise to the OCV. The OCV corresponds to the measured voltage when no current flows through the external circuit. The reaction kinetics corresponding to the anodic and cathodic section of the electrochemical cell results in the activation overpotential represented as  $\Delta V_{\text{act}}$ . The activation overpotential ( $\Delta V_{\text{act}}$ ) is represented as the sum of anodic and cathodic activation overpotentials using a simplified Tafel equation:

$$\Delta V_{\text{act}} = \Delta V_{\text{act}} (\text{anode}) + \Delta V_{\text{act}} (\text{cathode}) = b \log(i)/(i_o) \quad (5)$$

here,  $i_o$  represents the equivalent exchange current density,  $b$  is the equivalent Tafel slope given as  $b = 2.303 \frac{RT}{\alpha F}$ . Here,  $R$  is the ideal gas constant,  $T$  is the temperature,  $F$  is Faraday's constant, and  $\alpha$  is the transfer coefficient. The ohmic overpotential loss can be described with a linear relationship between the current density and the voltage, given as:

$$\Delta V_{\text{ohmic}} = R_{\Omega} \times i \quad (6)$$

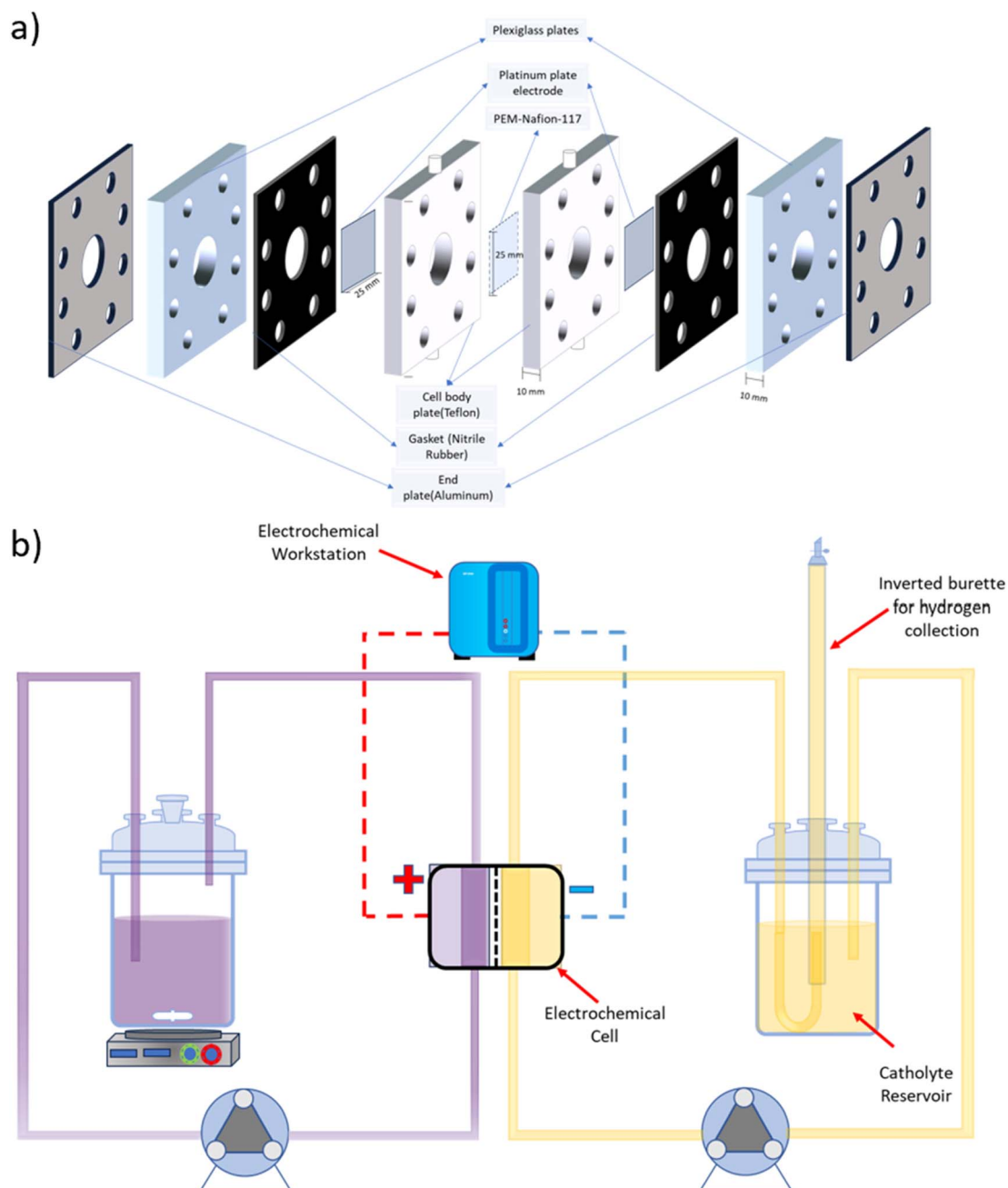


Fig. 1 Schematic representation of (a) the two-compartment electrochemical HI decomposition cell and (b) the continuous flow system for electrochemical HI decomposition.





here,  $R_{\Omega}$  is the total ohmic resistance in the cell system & comprises of the resistance contribution from electrolyte, membrane, and the electrical connections. The present studies have been conducted at low current densities, where the mass transport losses are not dominant, and the mass transfer overpotential can be considered linearly varying with the current density as:<sup>42–44</sup>

$$\Delta V_{MT} = R_{MT} \times i \quad (7)$$

Considering the activation overpotential losses, ohmic overpotential losses, and mass transfer overpotential losses, the total voltage  $V$  can be represented as

$$V = OCV - b \log(i_o) + b \log(i) + R_{\Omega} \times i + R_{MT} \times i \\ = V_o + b \log(i) + R_T \times i \quad (8)$$

here,  $V_o = OCV - b \log(i_o)$ , where  $V_o$  represents the current independent component.  $R_T$  is referred to as the equivalent resistance corresponding to the resistive overpotential losses as ( $R_T \times i$ ) and is the sum of the mass transfer and ohmic resistance given as  $R_T = R_{\Omega} + R_{MT}$ .<sup>44</sup> The polarization curve providing current density ( $i$ ) and the voltage ( $V$ ) was fitted with the above equation using the non-linear least square method in MATLAB with the fitting parameters  $V_o$ ,  $b$ , and  $R_T$ . Post-fitting the experimentally obtained OCV was subtracted from the term  $V_o$ , and the evolution of the overall activation overpotential losses ( $V_o - OCV + b \log(i)$ ) were evaluated as a function of current density.

## 2.6 Continuous electrochemical HI decomposition

A symmetrical two-compartment electrochemical cell for HI decomposition was fabricated in-house, as shown in Fig. 1(a). Each of the two compartments of the electrochemical cell had a volume of 3.14 ml and was fabricated with Teflon considering its chemical resistance against  $HI_x$  and other acids used in this study. Nafion 117 PEM divided the two compartments while providing an exposed circular area measuring 20 mm in diameter that allowed selective permeation of  $H^+$ . Platinum electrodes were housed within each Teflon cell section at a distance of 10 mm from the membrane with a circular exposed area of 20 mm diameter. The overall design is similar to that used for the batch cell but with a higher electroactive area. All electrolysis experiments were conducted using a BioLogic SAS SP 200 electrochemical workstation.

A schematic representation of the experimental arrangement used for the continuous electrochemical HI decomposition is shown in Fig. 1(b). The setup comprised of the anolyte reservoir and the catholyte reservoir fitted with an inverted graduated burette as a gas collector with a U-type tube junction at the bottom of the burette to collect and simultaneously measure the gas volume by volume displacement method. The anolyte reservoir was placed on a magnetic stirrer to ensure the dissolution of iodine and homogenous concentration within the anolyte. Two peristaltic pumps, each for the anolyte and the catholyte section, were used to recirculate the electrolytes with the flow rates of  $120 \text{ ml min}^{-1}$ . The electrochemical HI decomposition was conducted under constant current mode,

and the volume of the hydrogen collected was quantified as a function of time.

The current efficiency was evaluated as the ratio of the experimentally observed hydrogen produced to the theoretical hydrogen production based on Faraday's law as:

$$E_I (\%) = \frac{n_{\text{exp}}}{n_{\text{calc}}} \times 100\% \quad (9)$$

here,  $n_{\text{exp}}$  represents the experimentally obtained change in moles of hydrogen based on the gas volume collected, and  $n_{\text{calc}}$  is the corresponding theoretically calculated value. The volume of hydrogen collected ( $V$ ) for the experiment was converted to the moles of hydrogen produced ( $n$ ), using the ideal gas law  $PV = nRT$ . Here,  $R$  is the gas constant,  $T$  is the absolute temperature, and  $P$  corresponds to the pressure within the gas collection chamber. The theoretically calculated change in the moles was evaluated as follows:

$$n_{\text{calc}} = \frac{It}{nF} \quad (10)$$

where  $I$  (A) is the current in amperes,  $n$  is the number of electrons participating in the reaction,  $F$  is the Faraday constant, and  $t$  (s) is the total time for which the current has been supplied in seconds.

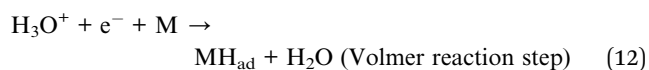
## 3. Results and discussion

### 3.1 Electrochemical behavior of catholyte in three-electrode system

The electrochemical behavior of four shortlisted catholytes has been studied using CV at varying scan rates, shown in Fig. 2. Here, the concentration of all the acids, HI,  $H_2SO_4$ , and  $H_3PO_4$ , were kept at 0.5 M. The CV analysis reveals similar features for  $H_2SO_4$  and  $H_3PO_4$  (Fig. 2(c) and (b)), whereas notable differences are observed in the CV profiles of  $H_2O$  and HI. For  $H_2SO_4$  and  $H_3PO_4$ , the positive potential region of the CV curves shows the presence of the platinum surface oxide formation–reduction reaction along with oxygen evolution. The middle zone of the CV corresponds to the double-layer effects on the platinum electrode. Since these electrolytes are to be used as the catholyte, the reduction potential regions become particularly important for the electrochemical HI decomposition process. In the negative potential CV region, features of hydrogen underpotential deposition and HER are observed in the forward scan, while desorption and hydrogen oxidation are seen in the reverse scan. Overall, the HER can be represented as:



For all the acidic electrolytes  $H_2SO_4$ ,  $H_3PO_4$ , and HI, the HER proceeds through the hydronium ion interactions. In particular, the HER is a multistep reaction that proceeds with either the Volmer–Heyrovsky or Volmer–Tafel pathway, where the elementary steps are given as:<sup>45–47</sup>



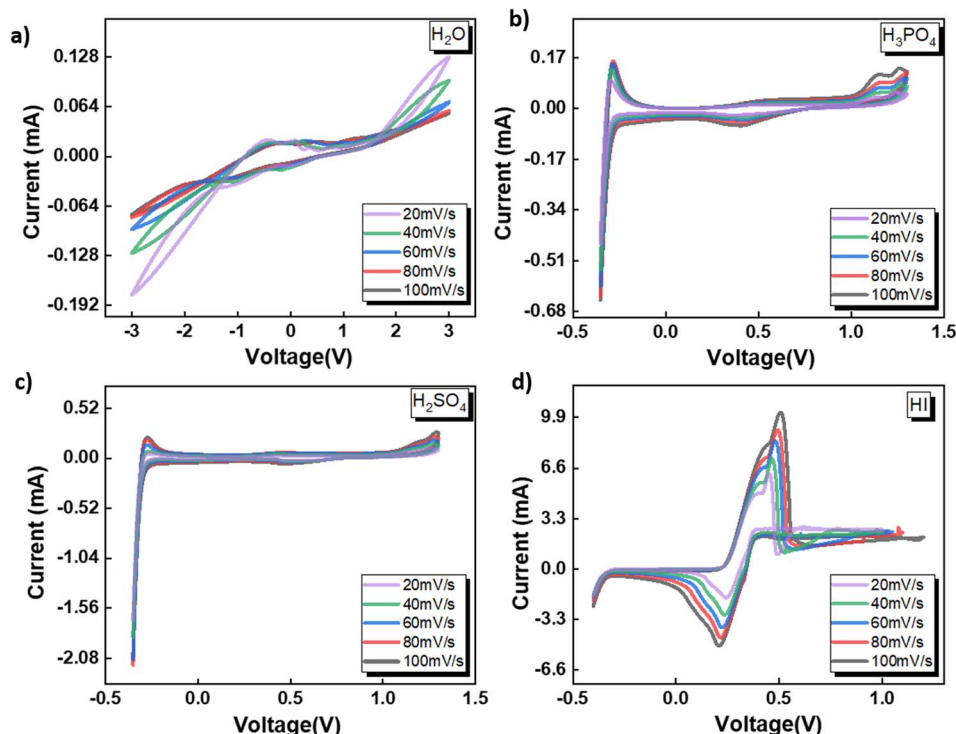
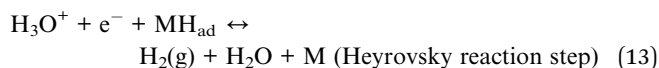


Fig. 2 CV data obtained for the three-electrode system with Ag/AgCl reference at the scan rates of 20, 40, 60, 80, and 100  $\text{mV s}^{-1}$  with the electrolytes (a)  $\text{H}_2\text{O}$  (b)  $\text{H}_3\text{PO}_4$  (c)  $\text{H}_2\text{SO}_4$  and (d) HI.



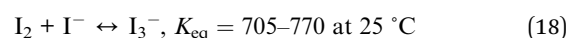
here, M denotes the catalytic active site,  $\text{MH}_{\text{ad}}$  is the hydrogen adsorbed on the catalytic site, and  $\text{H}_2$  is the hydrogen gas. Specifically, the first step (Volmer step) involves the reduction of hydronium on an active site on the catalyst surface. Following the reduction of hydronium, the following steps can either follow the Heyrovsky step involving a second hydronium ion or through the Tafel step involving a combination of two adsorbed protons on the catalyst surface.

Anions play a crucial role in various near-surface phenomena occurring within the electrode–electrolyte interface, affecting the electrochemical process through blocking of the active site, changes in the adsorption energy of the active sites neighbouring the adsorbed anions, potential drop redistribution, surface restructuring.<sup>48</sup> The anions have been shown to affect the platinum–hydrogen bonding and, consequently, the HER.<sup>49</sup> The ability of the anion to affect the platinum–hydrogen surface bonding depends on the degree of solvation for the anion.<sup>48</sup> Generally, a strongly solvated anion bonds weakly to the electrode surface, while a weakly solvated anion bonds strongly, with the possibility of direct chemical bonds.<sup>48</sup> Furthermore, the anion in the electrolyte upon adsorbing on the platinum electrode surface can decrease the amount of adsorbed hydrogen or affect the energy distribution of adsorbed hydrogen and the consequent HER process.<sup>49</sup> For  $\text{H}_2\text{SO}_4$  and  $\text{H}_3\text{PO}_4$ , the difference in the CV peak features indicates that the anionic

species  $\text{SO}_4^{2-}$  and  $\text{PO}_4^{3-}$  affect the hydrogen adsorption process. Compared to the  $\text{H}_2\text{SO}_4$  and  $\text{H}_3\text{PO}_4$ , iodide ions have been shown to adsorb strongly on the platinum surface, reducing the hydrogen–platinum bond energy and the amount of adsorbed hydrogen.<sup>49</sup> In contrast to the  $\text{SO}_4^{2-}$  and  $\text{PO}_4^{3-}$  ions, the iodide ion contributed by the HI is electroactive within the electrochemical analysis window. Consequently, for the HI as the electrolyte, prominent anodic and cathodic peaks can be observed in Fig. 2(d) with significantly higher current values than the current values observed for all the other electrolytes. As the potential is scanned in the positive direction, the iodide ions present in the electrolyte get oxidized to tri-iodide and iodine as per the following reaction:



Furthermore, the iodine produced as a result of the electrochemical reaction reacts homogeneously with the iodide ions to form tri-iodide ions given by the following equation:<sup>50</sup>

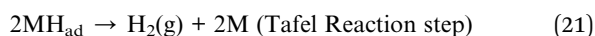
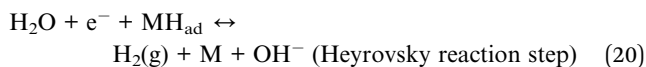


Upon reversing the potential scan, distinct electro-reduction peaks emerge, corresponding to the formation of iodide ions through the electro-reduction of the iodine and tri-iodide ions produced through the electrooxidation reaction during the forward cycle. After the iodide formation peak, the current



increases again, corresponding to the HER process. It is to be noted that the typical underpotential hydrogen adsorption peaks are not prominently visible in the CV for HI, which are otherwise observable for the  $\text{H}_2\text{SO}_4$  and  $\text{H}_3\text{PO}_4$ . This can be attributed to the reduced amount of adsorbed hydrogen due to the strongly adsorbed  $\text{I}^-$  ions on the platinum surface.<sup>49</sup> Additionally, the higher magnitude of current associated with the iodine–iodide redox reaction also contributes to masking any CV features related to hydrogen adsorption–desorption. Nevertheless, the HER can be observed for all three acidic solutions studied here with varying anions.

Fig. 2(a) shows the CV for water as the electrolyte. The potential sweep in the positive direction shows the presence of oxygen evolution. Current peaks associated with the hydrogen adsorption–desorption can be observed for the negative potential scan. A similar two-step pathway comprising of Volmer–Heyrovsky or Volmer–Tafel pathway as that observed for the acidic system is expected for water. However, as a neutral electrolyte, water results in a lower number of available  $\text{H}^+$  ions than the acidic electrolyte. Consequently, the HER in the neutral solution proceeds through the water reduction process:<sup>47</sup>



It is generally accepted that liberating a proton from water by dissociating  $\text{H}_2\text{O}$  is kinetically difficult compared to acidic conditions where the proton is present as a hydronium ion.<sup>46,51</sup> Furthermore, water dissociation introduces an additional energy barrier, contributing to the total energy barrier in the overall hydrogen evolution process from water.<sup>51</sup> In contrast to the acidic electrolytes studied before, for neutral electrolytes such as water, the critical step that governs the rate of the HER involving the reduction of hydronium ions switches from being the Volmer–Tafel or Volmer–Heyrovsky step to the Volmer step, *i.e.*, single-electron transfer to reduce  $\text{H}_2\text{O}$ . The above results indicate that the pH and the anion present in the acid significantly affect the redox reaction mechanism and, therefore, are expected to affect the HER process for the electrochemical decomposition of HI. Overall, based on the CV studies, all four electrolytes selected for the studies can induce HER and, hence, can serve as the catholyte for the electrochemical HI decomposition process.

### 3.2 Polarization studies in two electrode cell system

The CV studies emphasize the influence of anionic species in the electrolyte toward the HER occurring at the cathode. Here, we extend our analysis and derive a comprehensive system-level understanding of the electrochemical decomposition through polarization studies conducted in a two-compartment electrochemical cell. The investigations on the two-compartment cell targeted two specific aspects: (a) the effect of the catholyte type

( $\text{H}_2\text{O}$ ,  $\text{H}_3\text{PO}_4$ ,  $\text{H}_2\text{SO}_4$ , and HI) and its concentration and (b) the emergent effect arising from the variation in the  $\text{I}_2/\text{HI}$  ratio in the anolyte section. Fig. 3 shows the polarization curve obtained for varying catholytes ( $\text{H}_2\text{O}$ ,  $\text{H}_3\text{PO}_4$ ,  $\text{H}_2\text{SO}_4$ , and HI) and their concentration as a function of the  $\text{I}_2/\text{HI}$  ratio in the anolyte. The polarization curve for all the electrolyte variations obtained for the cell system shows a similar shape. The current density remains negligibly low at lower voltages and gradually starts increasing non-linearly with increasing voltage, representing the onset of the electrochemical HI decomposition and hydrogen production.

The onset potential increased with the  $\text{I}_2/\text{HI}$  ratio, as observed in Fig. 3(a), with water as the catholyte. Similar behavior was observed for the other electrolytes used in this study. It is to be noted that the onset potential was found to be in the range of 0.3 to 0.4 V for all the cases. This increase in the onset potential aligns with the earlier reported studies, which can be attributed to the increase in the OCV for the cell with an increasing  $\text{I}_2/\text{HI}$  ratio.<sup>30</sup> Furthermore, it can be observed that at any given current density after the onset potential, the total voltage is lower for the lower  $\text{I}_2/\text{HI}$  ratio, indicative of better performance. Interestingly, it can be observed that the polarization curve curves are nearly identical for the variation in the acid/ $\text{H}_2\text{O}$  ratio in the catholyte at any given  $\text{I}_2/\text{HI}$  ratio in the anolyte, featuring similar onset potentials in Fig. 3(b)–(j) for all the acids,  $\text{H}_2\text{SO}_4$ ,  $\text{H}_3\text{PO}_4$ , and HI used in this study. The experimental data were fitted with the mathematical model outlined in Section 2.5 to deconvolute the overpotential contributions in the polarization behavior. The model equation described in eqn (8) was found to show a good fit for all the experimental polarization curve data, as shown in Fig. 3, with  $R^2$  values  $\sim 0.99$ .

The OCV was evaluated experimentally before the experiment, and the data is shown in Fig. 4(a), (c), (e) and (g). For all the catholytes studied here, it was observed that the OCV became relatively more positive with an increase in the  $\text{I}_2/\text{HI}$  ratios in the anolyte. Additionally, for the catholyte section, an increase in the acid/ $\text{H}_2\text{O}$  ratio for all three acids resulted in the OCV attaining relatively more positive values. Positive OCV values were observed for HI as the catholyte, except for the HI/ $\text{H}_2\text{O}$  ratio of 0.076 in the catholyte with an  $\text{I}_2/\text{HI}$  ratio of 1 in the anolyte. This starkly contrasts the other acids studied here, where the OCV was found to have negative values. The OCV results from the asymmetric composition of the anolyte and catholyte sections.<sup>41</sup> In a two-compartment PEM-separated cell system, the OCV is the combination of the electrode potentials for the anode and the cathode, the Donnan potential for the membrane, and the diffusion potential through the membrane.<sup>52</sup> Consequently, changing the composition on either side of the membrane results in a variation of the OCV.

The  $R_T$  corresponding to the resistive overpotential losses is a combination of the ohmic and mass transfer resistance and is shown in Fig. 4(b), (d), (f) and (h). While we can assume the resistance contribution from the electronic resistance from electrical connections and electrodes to be low and constant for the system, the ionic resistance and the mass transfer resistance component are expected to depend on the electrolyte



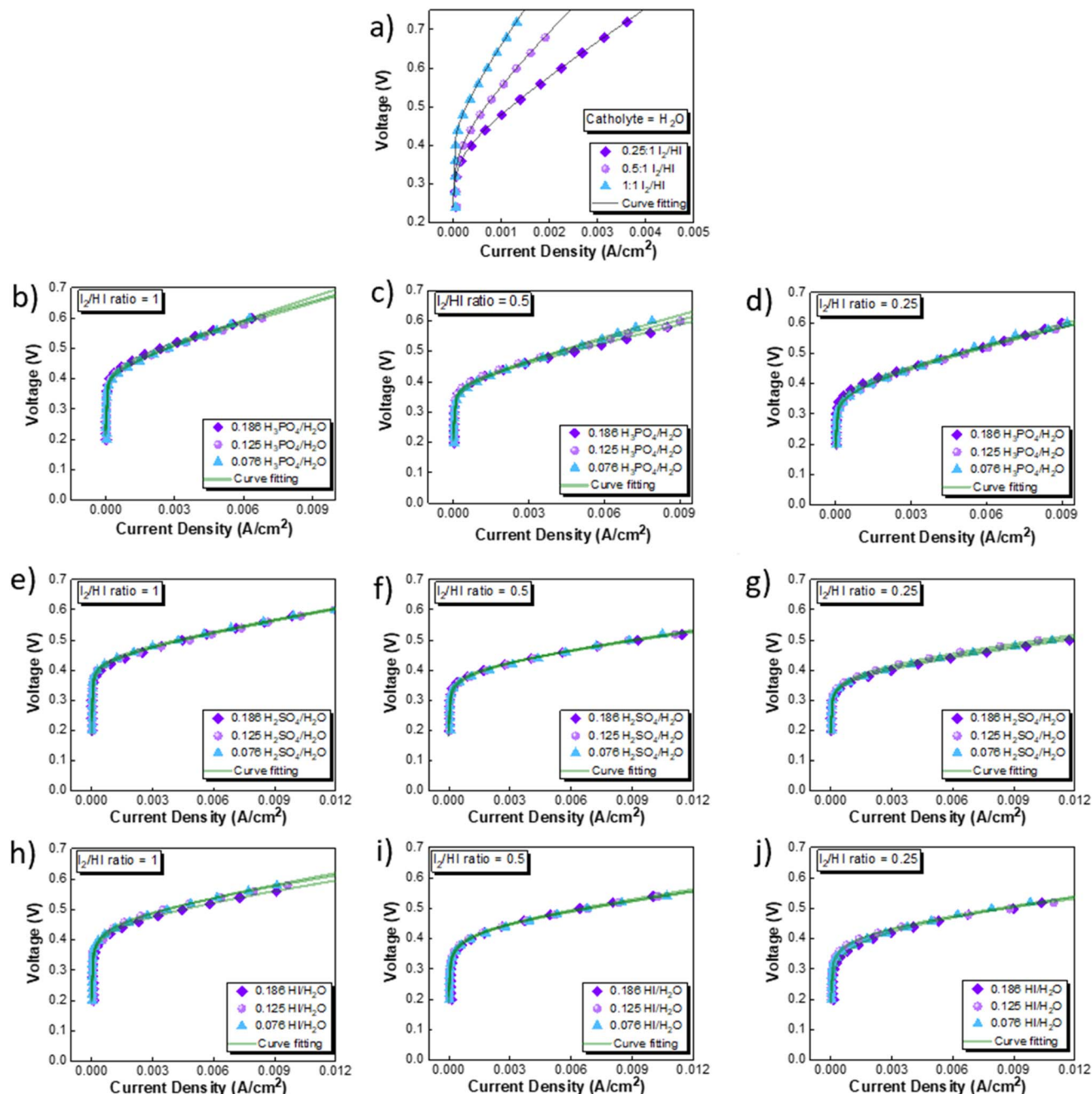


Fig. 3 Two electrode polarisation curve studies corresponding to the three  $I_2/HI$  ratios with respective catholytes, namely (a)  $H_2O$  (b)–(d)  $H_3PO_4$  (e)–(g)  $H_2SO_4$ , and (h)–(j)  $HI$ .

composition. The  $R_T$  of the cell was found to increase with increasing  $I_2/HI$  ratio for fixed catholyte composition. With an increase in the iodine content in the anolyte, the concentration of tri-iodide ions increases. In comparison, the tri-iodide ion exhibits a larger solvated ion size (1.8 nm) compared to the iodide ion (0.39 nm). Consequently, this leads to reduced mobility of tri-iodide ions, resulting in a higher ionic resistance with increasing  $I_2/HI$  ratio.<sup>53,54</sup> This is in line with the earlier reported studies where the solution resistance was found to increase with an increase in the iodine content in the electrolyte solution.<sup>26,53,55,56</sup> For the catholyte variation, the  $R_T$  values for the

four electrolytes follow the order:  $H_2O > H_3PO_4 > H_2SO_4 > HI$ . Therefore, for the same anolyte composition, the difference in the  $R_T$  can be attributed to the difference in the ionic species behavior in the catholyte. In general, increasing the concentration of the charged species reduces the electrolyte resistance. Water's exceptionally high  $R_T$  can be attributed to the lower number of ionic species present and, hence, the lower number of charge carriers. For varying acids in the catholyte, the difference in the property of the anionic species contributes to the difference in the observed values of  $R_T$ . For the three acids studied here, the phosphate ion (0.483 nm)<sup>57</sup> presents with the





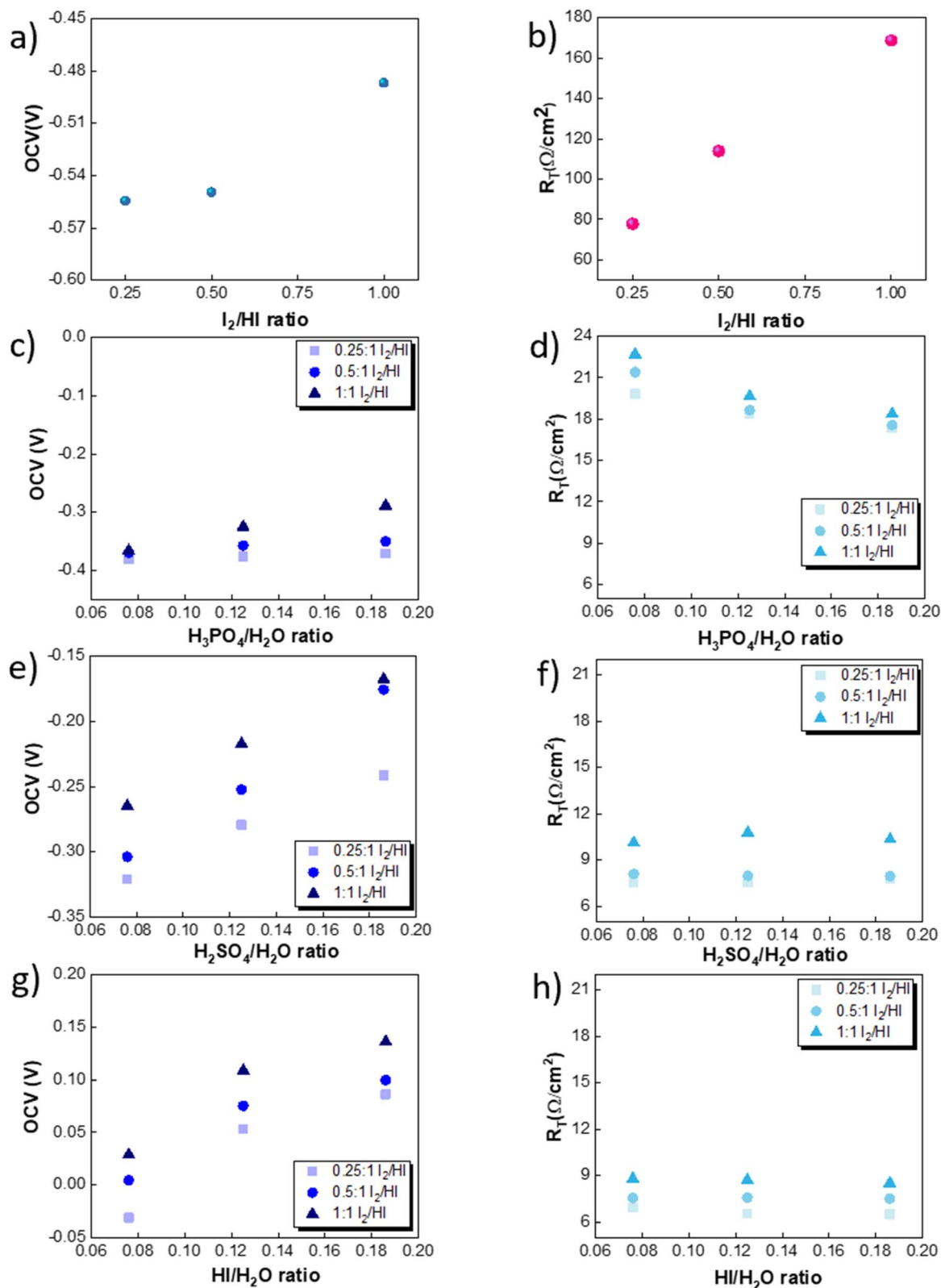


Fig. 4 Variation in the OCV for three  $I_2/HI$  ratios of 0.25, 0.5 and 1 for the catholytes (a)  $H_2O$ , (c)  $H_3PO_4$ , (e)  $H_2SO_4$ , and (g)  $HI$ . Variation in the  $R_T$  for the three  $I_2/HI$  ratios of 0.25, 0.5 and 1 for the catholytes (b)  $H_2O$  (d)  $H_3PO_4$  (f)  $H_2SO_4$  (h)  $HI$ .

largest hydrated ion size, followed by the sulfate ion (0.379 nm) and the iodide ion (0.331 nm).<sup>58</sup> A higher hydrated ion radius reduces the mobility, contributing to the higher  $R_T$  for  $H_3PO_4$

while being the lowest for  $HI$  at similar acid/ $H_2O$  ratios. Furthermore, it is to be noted that  $HI$  and  $H_2SO_4$  are strong acids, while  $H_3PO_4$  is a weak acid. As a result,  $H_3PO_4$  is only

weakly dissociated, producing relatively lower number of ions under equilibrium, which further contributes to the higher  $R_T$  observed in the  $\text{H}_3\text{PO}_4$  catholyte. In addition, when  $\text{H}_3\text{PO}_4$  serves as the catholyte, an increase in the  $\text{H}_3\text{PO}_4/\text{H}_2\text{O}$  ratio results in a reduction of the  $R_T$ . On the other hand, for  $\text{H}_2\text{SO}_4$  and HI, a change in the acid/ $\text{H}_2\text{O}$  ratio does not significantly influence the  $R_T$ . Increasing the number of ionic species in the electrolyte leads to two opposing effects on the solution resistance. Increasing the acid concentration increases the number

of charged species, which can reduce the  $R_T$ . However, the inter-ionic interactions also increase with the increasing number of charged species, which reduces the mobility of ions and hence can increase the  $R_T$ . For HI and  $\text{H}_2\text{SO}_4$ , the relatively similar  $R_T$  values indicate that the above two opposing effects emanating from the increasing acid concentration get balanced. However,  $\text{H}_3\text{PO}_4$  is a weak acid, and the increase in conductivity due to the increased number of charged species dominates the overall effect, reducing the  $R_T$  with an increase in the  $\text{H}_3\text{PO}_4/\text{H}_2\text{O}$  ratio.

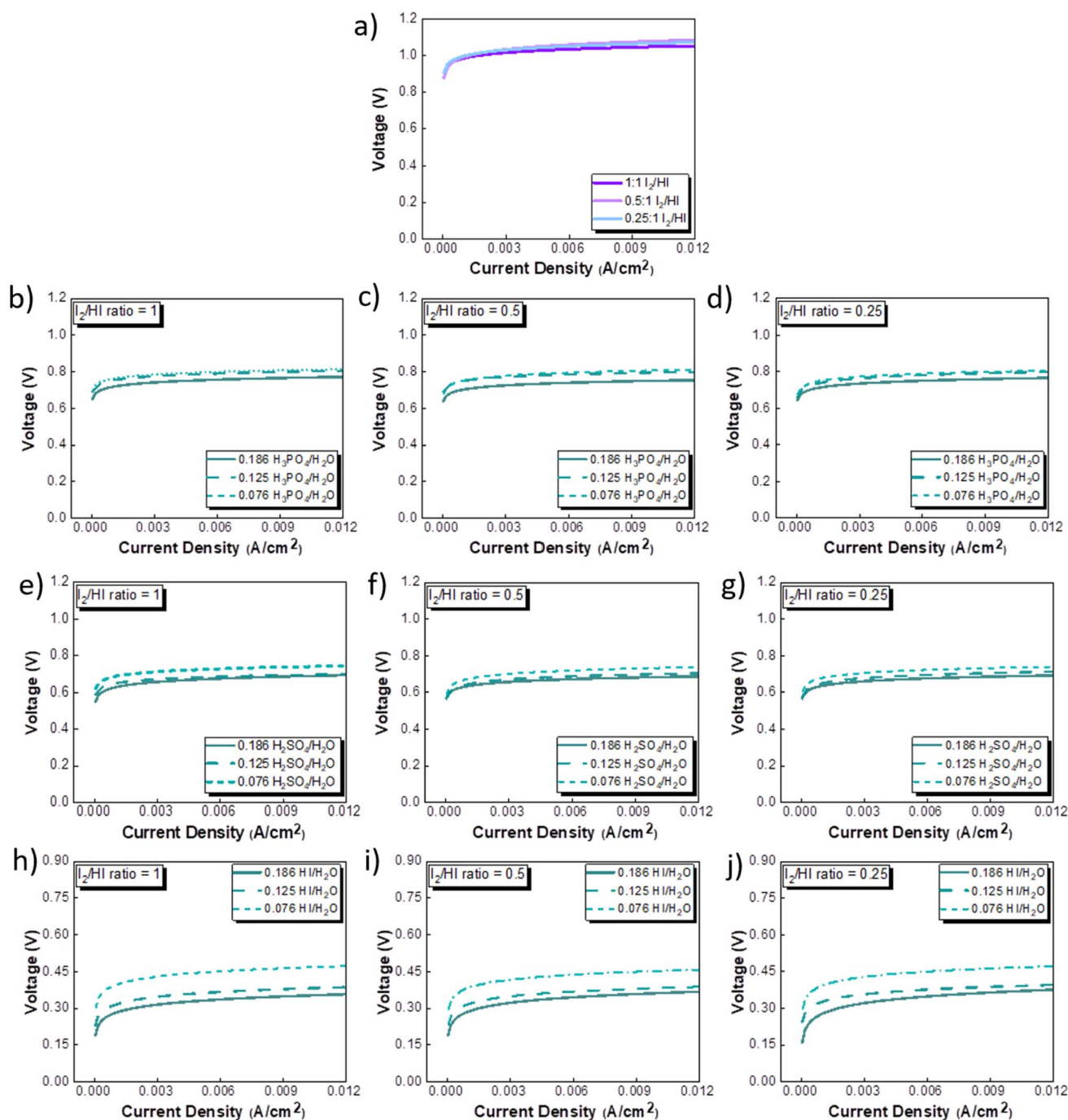


Fig. 5 Activation overpotential losses corresponding to the three  $\text{I}_2/\text{HI}$  ratios of 0.25, 0.5 and 1 with the catholytes (a)  $\text{H}_2\text{O}$  (b)–(d)  $\text{H}_3\text{PO}_4$  (e)–(g)  $\text{H}_2\text{SO}_4$ , and (h)–(j) HI.



The activation overpotential contribution evaluated from the model fitting data is shown in Fig. 5 for all the studies. The activation overpotential losses were found to be of similar order for the same catholyte composition for all three  $I_2$ /HI ratios. This aligns with the earlier studies that the activation overpotential losses in the anolyte section are negligibly low, and the overall activation losses emanate predominantly from the catholyte section.<sup>30</sup> In contrast, the activation overpotential increases with a reducing acid/ $H_2O$  ratio. Here, the activation overpotential components graphs are found to be shifted towards higher values while retaining a similar shape. The activation overpotential component is expressed with the Tafel equation as  $b \log \frac{i}{i_0}$ . A reduction in the acid/ $H_2O$  ratio signifies a reduction in the  $H^+$  ion concentration, which results in the reduction of  $i_0$  values and increase in the cathodic transfer coefficient, causing the above observed increase in the activation overpotential losses.<sup>59</sup> While the activation overpotential varies with the dilution of all acids, the polarization behavior for the cell remains similar for a given catholyte at varying dilutions. Such invariance in the polarization behavior can be attributed to the compensation of the change in the activation overpotential with the OCV change of the cell.

**3.2.1 Performance comparison and catholyte selection.** The performance of the three acids remains nearly similar upon reducing the acid/ $H_2O$  ratio. A lower acid concentration reduces the electrolyte costs associated with the operation. Moreover, excessively high acid concentrations have detrimental effects on the electrode material by promoting platinum dissolution, thereby leading to increased costs.<sup>60</sup> Based on the above rationale, the acid/ $H_2O$  ratio of 0.076 has been considered for further analysis. Fig. 6 shows the performance evaluation of the catholytes with a fixed acid/ $H_2O$  ratio of 0.076 at three  $I_2$ /HI ratios of 0.25, 0.5, and 1. The relative cell performance was found to follow the order  $H_2SO_4 > HI > H_3PO_4 > H_2O$ . Even though  $H_2O$  as the catholyte has been extensively demonstrated in prior studies,<sup>25–29</sup> its usage will lead to higher overpotential losses and, hence, higher energy consumption. While water is a low-cost electrolyte, present throughout the I–S cycle and thus poses no contamination risk, our investigations indicate that water fares the poorest among all the electrolytes examined.

While the earlier schemes of the I–S cycle did utilize  $H_3PO_4$  in the HI section, the currently prevalent schemes of the I–S cycle, such as electro-electrodialysis with distillation, electrochemical HI decomposition, do not involve  $H_3PO_4$  and hence present a potential foreign ion contamination risk. Based on the above, we deduce that the  $H_2O$  and  $H_3PO_4$  are not good candidates for further studies. The results support  $H_2SO_4$  and HI as promising catholyte candidates, with  $H_2SO_4$  exhibiting the highest performance and HI closely following. Also,  $H_2SO_4$  and HI are already present in the current I–S cycle scheme. Thus, selecting them as the catholyte eliminates adding additional chemical components into the process stream. Moreover, any cross contamination of  $H_2SO_4$  and HI from the catholyte section into the anolyte section will have a negligible impact on the iodine–iodide redox reaction occurring in the anolyte section.<sup>31</sup> Therefore, further continuous flow studies have been done with  $H_2SO_4$  and HI as the catholyte with HI/ $H_2O$  and  $H_2SO_4$ / $H_2O$  ratios of 0.076 for hydrogen production.

### 3.3 Continuous electrochemical HI decomposition

The electrochemical HI decomposition for hydrogen production with HI and  $H_2SO_4$  as the catholyte has been carried out in a two-compartment cell system at two different current densities of  $0.025 \text{ A cm}^{-2}$  to  $0.038 \text{ A cm}^{-2}$ .  $HI_x$  solutions with  $I_2$ /HI ratios of 1, 0.5, and 0.25 with a fixed HI/ $H_2O$  ratio of 0.186 were employed in the anolyte section. For the catholyte section, investigations were conducted using HI/ $H_2O$  and  $H_2SO_4$ / $H_2O$  ratios of 0.076. A total of nine continuous flow cell studies with hydrogen production have been presented. Upon the application of voltage, it was observed that hydrogen gas bubbles were transported to the inverted burette gas collector. Furthermore, the volume of collected hydrogen gas increased progressively over time, demonstrating the feasibility of continuous hydrogen production.

Fig. 7(a)–(c) illustrates the evolution of the voltage over time during the electrochemical HI decomposition experiment for the electrolyte configurations discussed above at two different current densities. As expected, the voltage values are higher when operated at a higher current density for the same electrolyte composition. Furthermore, the voltage values recorded for the  $H_2SO_4$  are consistently lower than those obtained for the

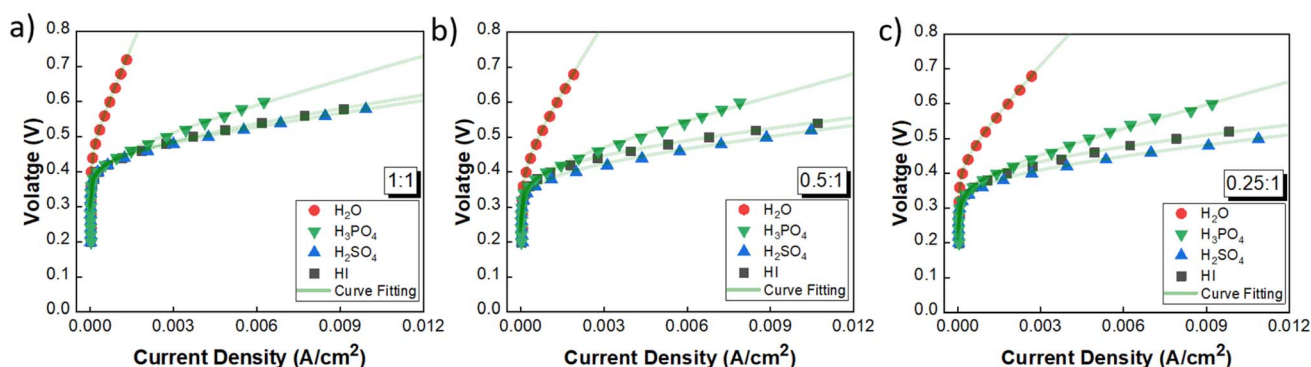


Fig. 6 Performance evaluation of the catholytes with fixed acid/ $H_2O$  ratio of 0.076 and at three  $I_2$ /HI ratios: (a) 1, (b) 0.5, (c) 0.25.

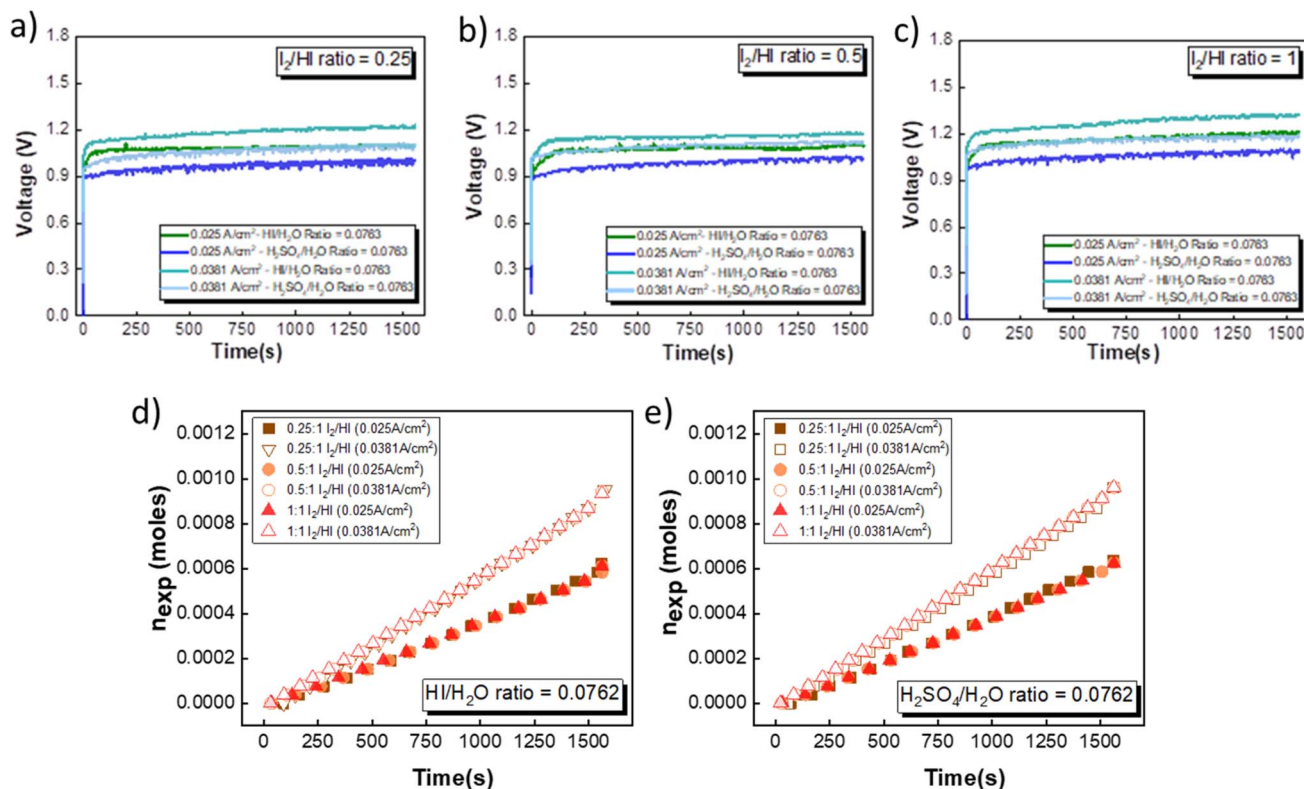


Fig. 7 Voltage evolution over time in an electrochemical HI decomposition experiment for three  $I_2/HI$  ratios is shown for (a) 1, (b) 0.5, and (c) 0.25 with HI and  $H_2SO_4$  as the catholyte. The hydrogen moles collected over time are shown for the two current densities for (d) HI and (e)  $H_2SO_4$ , respectively.

HI for the same current density. This is in line with the polarization studies, where the performance of  $H_2SO_4$  was slightly better than that of HI as the catholyte. The temporal evolution of the voltage exhibits noise-like fluctuations that can be attributed to the hydrogen bubble formation and detachment and the resulting changes in the electroactive area and hydrodynamic disturbances in the electrolyte during the bubble detachment and movement. The transient voltage is seen to show a gradual increase with time. As the electrochemical HI decomposition progresses, the iodide ion converts to iodine in the anolyte section, increasing the  $I_2/HI$  ratio. The increase in the  $I_2/HI$  ratio causes an increase in the OCV and the  $R_T$ , which can be attributed to the gradual increase in the voltage with time during the electrochemical HI decomposition. The moles of hydrogen collected in the reservoir increased almost linearly with time for all the electrolyte combinations, as shown in Fig. 7(d) and (e). The above indicates that the hydrogen production rate remains nearly constant for the duration of the experiment. Furthermore, the hydrogen production rate is a function of the operating current density and remains unaffected by variations in the electrolyte composition, including the  $I_2/HI$  ratio in the anolyte and variations in the catholyte.

As expected, the hydrogen production rate is higher when the system operates at a higher current density, per Faraday's law. The hydrogen production rate was found to be  $\sim 0.4 \mu\text{moles s}^{-1}$  and  $\sim 0.6 \mu\text{moles s}^{-1}$  for the operating current density of

$0.025 \text{ A cm}^{-2}$  and  $0.038 \text{ A cm}^{-2}$ , respectively. An initial lag between the start of the electrolysis and the collection of the first hydrogen bubble was observed due to the time required for the bubble to travel through the connecting pipelines. Therefore, after stopping the voltage supply, the pumps were run until all the bubbles within the pipeline were transferred to the gas collector to express the total hydrogen collected for the operation. The final data points in Fig. 7(d) and (e) correspond to the total volume of hydrogen collected after running the pumps for additional time. Based on the pressure within the inverted burette gas collection chamber, the corresponding moles of the hydrogen gas were evaluated. The final amount of the collected hydrogen gas was used to evaluate the overall current efficiency using eqn (9), as shown in Fig. 8(a), along with the normal distribution in Fig. 8(b). The recorded current efficiency values were above 94% across all experimental runs. Using  $H_2SO_4$  as the catholyte yielded slightly higher current efficiency values than HI at similar anolyte composition and operating current density. An average current efficiency of approximately 97% was observed across all experimental runs. A current efficiency lower than 100% indicates side reactions other than HER. Specifically, the anolyte side is rich in iodine, while the catholyte is devoid of iodine. Consequently, the iodine from the anolyte side can permeate to the catholyte side during the electrochemical HI decomposition.<sup>26</sup> In addition, the negatively charged iodide/tri-iodide ions can also permeate through the membrane, resulting





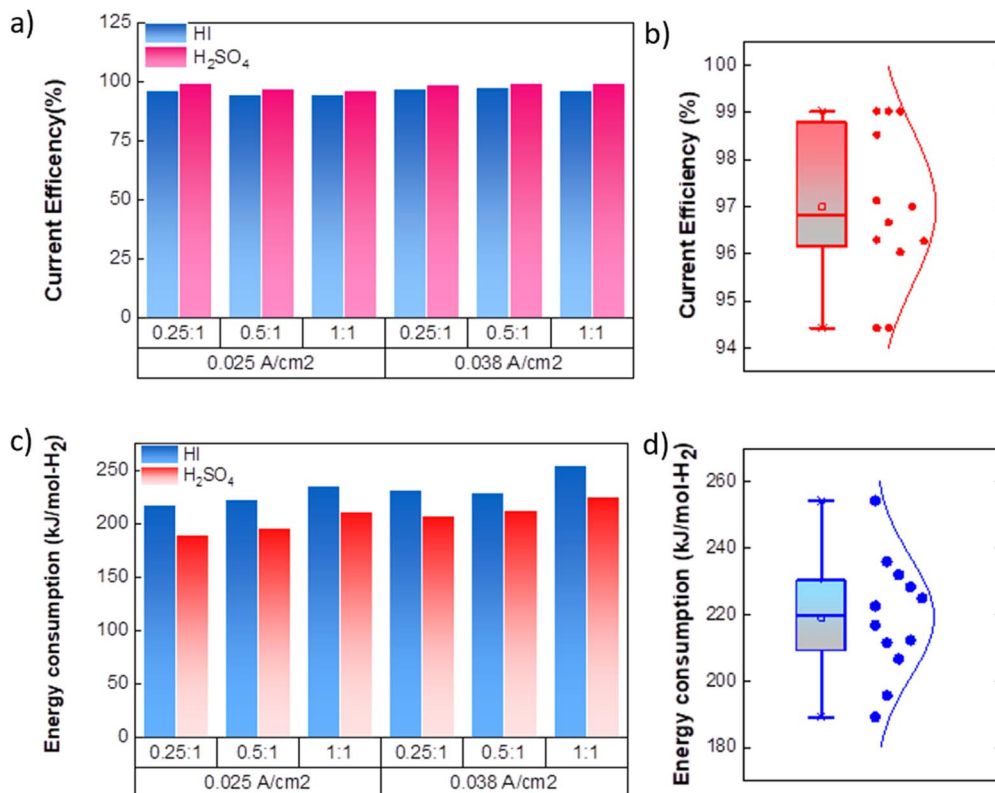


Fig. 8 (a) Current efficiency for continuous electrochemical HI decomposition (b) normal distribution of the current efficiencies. (c) Energy consumed per mole of hydrogen ( $\text{kJ mol}^{-1}\text{H}_2$ ) production for the continuous electrochemical HI decomposition (d) normal distribution plot for the energy consumption.

in cross-contamination.<sup>39</sup> For the HI as the catholyte, the iodine permeating through the membrane can further react homogeneously with the iodide ion to form tri-iodide ions. As seen in Fig. 2(d), the reduction of iodine and tri-iodide ions occurs at lower overpotentials as compared to the HER. Therefore, under reduction potentials, the iodine and tri-iodide ions, if present in the catholyte section, can undergo electro-reduction to form iodide ions preferentially over HER, thereby lowering the current efficiency. Additionally, a consistently higher current efficiency for H<sub>2</sub>SO<sub>4</sub> compared to HI indicates that the iodine and tri-iodide permeation is relatively lower when H<sub>2</sub>SO<sub>4</sub> is in the catholyte compared to HI. One of the possible reasons which can cause a higher permeation with HI as catholyte can be the higher solubility of the iodine in the electrolyte containing iodide ion through homogenous tri-iodide ion formation (eqn (18)). It is to be noted that the gradual contamination for the H<sub>2</sub>SO<sub>4</sub> catholyte will occur during prolonged operations, which will essentially add ionic species in the electrolyte system.

The energy consumed per mole of hydrogen production ( $\text{kJ mol}^{-1}\text{H}_2$ ) based on the total energy consumed over the duration of the experiment and the total moles of hydrogen produced has been evaluated as:  $\frac{E}{n_{\text{exp}}}$  and is shown in Fig. 8(c). In the equation,  $n_{\text{exp}}$  represents the experimentally quantified moles of hydrogen produced from the HI electrochemical decomposition. The net energy consumed ( $E$ ) has been evaluated as the product of the

area under the chronopotentiometry curve and the applied current, expressed as  $E = I \times \int_0^{t_f} V dt$ . The  $t_f$  in the above case is the duration of the experiments in seconds, and  $I$  is the current in amperes, and  $V$  is in volt. The distribution of the energy consumption is shown in Fig. 8(d), and the mean energy consumption is  $\sim 220 \text{ kJ mol}^{-1}\text{H}_2$ . For H<sub>2</sub>SO<sub>4</sub>, as the catholyte with the same current density and I<sub>2</sub>/HI ratio, the energy consumption is lower, which can be attributed to the lower overpotential losses coupled with higher current efficiencies. Additionally, H<sub>2</sub>SO<sub>4</sub> also has a lower cost as compared to HI acid. Overall, H<sub>2</sub>SO<sub>4</sub> results in higher performance, lower energy consumption, and lower cost than HI. Consequently, evaluating factors of performance, energy consumption, and cost, it becomes evident that H<sub>2</sub>SO<sub>4</sub> emerges as a better choice for catholyte in electrochemical HI decomposition. A comparative assessment of the previously reported studies and the present study is shown in Table 1.

The electrochemical decomposition of hydroiodic acid in the I-S thermochemical cycle is designed to operate in an integrated mode, either with the Bunsen reaction in an open-loop scheme or with both the Bunsen reaction and the sulfuric acid decomposition sections in a closed-loop scheme. In the standalone operation conducted in this study, an increase in the I<sub>2</sub>/HI ratio within the anolyte section leads to a rise in operating voltage. In contrast, an integrated system operating under steady-state conditions is expected to maintain a near-



Table 1 Comparison with the previously reported studies for electrochemical HI decomposition with the current work

References	Electrode material	Membrane	Anolyte	Catholyte	Performance parameter	Ref.
Xu <i>et al.</i> (2018)	Carbon papers	Nafion 117 and Nafion 115	HI-I <sub>2</sub> -H <sub>2</sub> O	Deionized water	Current efficiency 93–87% Hydrogen production rate: 6–12.5 ml min <sup>-1</sup>	26
Ying <i>et al.</i> (2020)	Graphite electrodes	Nafion 117	HI-I <sub>2</sub> -H <sub>2</sub> O	Deionized water	Hydrogen production rate: ~4.5 ml min <sup>-1</sup>	29
Ying <i>et al.</i> (2020)	Graphite electrodes	Nafion 117	HI-I <sub>2</sub> -H <sub>2</sub> O	Deionized water	Hydrogen production rate: ~4.5 ml min <sup>-1</sup>	27
Shahi <i>et al.</i> (2021)	TriO <sub>2</sub> expanded sheets coated with triple precious metal oxide (titanium–ruthenium–platinum)	Sulfonated copolymer of PVDF-co-HFP (SCP) and graphene oxide (SGO) Nafion® 117	HI-H <sub>2</sub> O	Water	Current efficiency 93.4–81.3% Energy required: 0.043–0.054 kW h mol-H <sub>2</sub> <sup>-1</sup> (154.8–194.4 kJ mol-H <sub>2</sub> <sup>-1</sup> )	25
Zhang <i>et al.</i> (2022)	Platinum-coated titanium mesh as the anode and stainless-steel mesh as the cathode	Nafion 117	HI + H <sub>2</sub> SO <sub>4</sub> + H <sub>2</sub> O + toluene	H <sub>2</sub> SO <sub>4</sub> + H <sub>2</sub> O	Current efficiency 89.7% Energy required: 0.047 kW h mol-H <sub>2</sub> <sup>-1</sup> (169.2 kJ mol-H <sub>2</sub> <sup>-1</sup> ) Current efficiency ~100% Hydrogen production rate: 6.78 × 10 <sup>-5</sup> to 44.1 × 10 <sup>-5</sup> mol l <sup>-1</sup> s <sup>-1</sup>	32
Current study	Platinum plate electrode for both anode and cathode	Nafion 117	HI-I <sub>2</sub> -H <sub>2</sub> O	HI + H <sub>2</sub> O and H <sub>2</sub> SO <sub>4</sub> + H <sub>2</sub> O	Current efficiency: 94–99% Hydrogen production rate: ~0.4–0.6 μmoles s <sup>-1</sup> Energy required: 189–255 kJ mol-H <sub>2</sub> <sup>-1</sup>	

constant anolyte composition, resulting in stable and nearly constant voltage. Long-term stability evaluations in an integrated system are required, where the coupling of all process steps allows for a realistic assessment of potential component degradation and electrolyte stability under continuous operation. While this study provides insights into the short-term effects of varying the I<sub>2</sub>/HI ratio, further studies are required on exploring long-term performance and durability in such integrated setups.

## 4. Conclusions

In summary, we have presented a detailed study on the effect of the catholyte type and its concentration on the electrochemical HI decomposition process. From the CV behavior it is deduced that there were no parallel reactions in the catholyte when H<sub>2</sub>SO<sub>4</sub>, H<sub>3</sub>PO<sub>4</sub>, and H<sub>2</sub>O were used as an electrolyte. However, for HI as an electrolyte, a parallel reaction of reduction of iodine and tri-iodide ions occurs when iodine is present. The above can be eliminated by ensuring the catholyte is devoid of iodine. Polarization studies revealed that the onset potential for electrochemical HI decomposition remained comparable within the range of 0.3 to 0.4 V across various catholytes and their concentrations. However, a slight increase in the onset potential was observed with an increase in the I<sub>2</sub>/HI ratio from 0.25 to 1. The catholyte concentration was found to have minimal effect on the overall polarization behavior. Among all the electrolytes studied as catholytes, H<sub>2</sub>SO<sub>4</sub> exhibited the highest performance, while H<sub>2</sub>O demonstrated the lowest performance. The nearly invariant polarization behavior for changing the catholyte concentration is attributed to the compensation of the activation overpotential with the changes in the OCV. Furthermore, the activation overpotential was similar for all three I<sub>2</sub>/HI ratios in the anolyte when catholyte composition was constant. Based on polarization curve analysis, HI and H<sub>2</sub>SO<sub>4</sub> with the lowest acid/H<sub>2</sub>O ratio were chosen as catholytes for continuous flow hydrogen production studies. Hydrogen generation was achieved at current densities of 0.025 A cm<sup>-2</sup> and 0.038 A cm<sup>-2</sup> across three I<sub>2</sub>/HI ratios in the anolyte. Current efficiency remained high (~97%), with an average energy requirement of ~220 kJ mol-H<sub>2</sub><sup>-1</sup>. Among the catholytes, H<sub>2</sub>SO<sub>4</sub> exhibited the lowest energy requirement and higher current efficiency, making it the most promising choice for efficient electrochemical HI decomposition.

## Data availability

All the relevant data generated during this study have been included in the main article. Any additional data will be provided on request.

## Author contributions

Ashwin Y.: methodology, validation, formal analysis, investigation, writing – original draft, visualization, Saroj Chaudhary: resources, project administration, Parvatalu Damaraju: resources, project administration, Pradeep Kumar Sow:



conceptualization, methodology, writing – review & editing, visualization, supervision, project administration, funding acquisition.

## Conflicts of interest

There are no conflicts to declare.

## Acknowledgements

The authors thank ONGC Energy Centre Trust (OECT, Agreement signing date: 2nd November 2021) for the financial support for conducting the research work. The authors would also like to thank Dr Richa Singhal for her support during this work. The authors acknowledge the assistance from the Mechanical Engineering workshop for their help with the fabrication of the cell components.

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