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Single and combined treatment processes for rhodamine B removal by coagulation–flocculation and adsorption

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In this paper, two physico-chemical methods were adopted for the removal of rhodamine B from aqueous solutions. The first one is the adsorption process using biochar derived from olive stones (OSB). Results demonstrated that the removal efficiency reached 97.79% within an equilibrium time of one hour. It was observed that the pH had no significant effect on the degradation of rhodamine B by OSB. The adsorption process was characterized by the endothermic nature, spontaneity, favorability, and disorder at the solid–liquid interface. Langmuir isotherm analysis revealed a maximum adsorption capacity of 11.82 mg g⁻¹, and the prepared biochar could be reused for up to four cycles. For the second method, coagulation–flocculation using FeCl₃ as a coagulant was investigated. The findings displayed that an increase in the dosage of FeCl₃ enhanced the degradation process, with the best performance registered at a dose of 2000 mg L⁻¹ of FeCl₃. The optimum pH for this process was found to be 2. A combination approach by these two methods, starting with coagulation–flocculation and followed by adsorption, was also investigated. The results showed that the combined approach improved the removal performance compared to each process alone, with minimal doses of both coagulant and adsorbent. Thus, the combination of these two physico-chemical processes allows benefits from the advantages and reduces the disadvantages of each individual method.

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1. Introduction

Synthetic dyes are frequently used in industries, which are producing large quantities of wastewater.^{1,2} These dyes are characterized by an intricate composition and large molecular size, tenacious and resistant characteristics, and poisonous, oncogenic, and gene-altering properties.^{3,4} Thus, the discharged effluents contain these types of pollutants that have the potential to cause substantial ecological damage by increasing wastewater turbidity, obstructing sunlight penetration at deeper levels, altering the photosynthetic activity of aquatic environments, and deteriorating the water quality, consequently leading to ecosystem imbalances.⁵ The presence of dyes in different water samples have been studied by different research works (ref. 6). The study presented by (ref. 7) demonstrated the presence of nine selected dyes including disperse dyes with

concentration ranging from 0.01 to 6.81 µg L⁻¹ in the upstream and downstream discharges of Piracicaba River and the effluent of a wastewater treatment plant (WWTP) in Americana, Brazil. Another work of (ref. 8) pointed that the malachite green is present in the laundry effluent, paper effluent, printing effluent and textile effluent with dose levels of 1320, 620, 790 and 1680 µg L⁻¹. Among these dyes is rhodamine B, an organic dye used in tinted glass and dyeing industries,⁹ which can present a high toxicity to the ecosystem.^{10,11} The presence of rhodamine B in water bodies was determined by (ref. 12), revealing its wide presence in wastewater effluent (62 and 37 ng L⁻¹) and surface water (4.8 ng L⁻¹) in Taiwan. The report of (ref. 13) stated the contamination of Zalew Biskupice Brzozki dam in Poland with a concentration of 0.0594 µg L⁻¹. The harmful effects of long-term rhodamine B accumulation in water include negative impacts on the metabolic and physiological processes of aquatic plants,¹¹ the hindrance of aquatic photosynthesis by limiting sunlight exposure,¹⁴ which results in reduced dissolved oxygen levels, increased bacterial and viral growth, and a steady deterioration of water quality.⁹ Rhodamine B also poses significant hazards to human health, microbial diversity, and other organisms. It not only causes irritation to the eyes, skin, and respiratory tract but is also characterized by its high mutagenic, neurotoxic, and carcinogenic potential in humans.¹⁵ Thus, a key priority is to implement sustainable methods for

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treating these dyes before they enter the environment, thereby securing clean water for future generations.¹⁴ Biological,^{16,17} physico-chemical,^{18,19} and membrane processes^{20,21} have been applied for dye removal in water samples. However, some of these techniques have drawbacks, such as high costs, sludge generation, and the need for extensive maintenance.²² Additionally, the use of strong oxidizing agents can produce undesirable by-products.^{23,24} Furthermore, some dyes are resistant to chemical agents and require higher dosages, indicating that the excessive use of chemicals could cause secondary pollution.^{22,23}

The coagulation–flocculation approach is extensively implemented in wastewater treatment due to its well-documented methodology, operational simplicity, cost-effectiveness, and exceptional efficiency.^{18,24} Coagulants facilitate the aggregation of colloids and suspended particles and form larger flocs, which settle easily.²⁵ Ferric chloride (FeCl₃) is one of the coagulants that has revealed good removal efficiencies for dyes.^{26,27} Adsorption technology widely uses low-cost materials, such as those based on agricultural wastes for dye removal from wastewater, namely, biochar, which are carbon-rich materials obtained from the pyrolysis of biomass waste under limited oxygen conditions.²⁸

Algeria boasts a longstanding tradition in olive cultivation. Data from the International Olive Council indicate that the country's olive oil production surged from 6000 tons in 1990 to 82 500 tons in 2017.²⁹ The significant production of oils is accompanied by substantial amounts of wastes as olive stones, which should be valorized. It has been demonstrated that olive stones have good adsorption properties for contaminants reported by (ref. 2 and 30). Olive biomass waste presents a viable option for adsorbing dyes, including rhodamine B, from wastewater.^{4,31} This finding was also supported by the ecological and economic feasibility of the adsorbents based on olive stones³² as well as the dyes' high adsorption and desorption removal capacities by such adsorbents.^{32–34}

Accordingly, the aim of this research is to apply a combination of two physico-chemical processes, coagulation–flocculation (using FeCl₃), which is a process currently used in water treatment systems, followed by adsorption (using olive stones biochar), which is an eco-friendly and effective process, as an efficient technique for rhodamine B removal from aqueous solutions. This approach is designed to ensure optimal performance and effectively uses the advantages of each process while minimizing the requirement of coagulant and adsorbent dosages.

In this context and before applying a combination technique, a study of both single adsorption treatment and single coagulation–flocculation treatment of rhodamine B removal was done and is described herein. For each process, the effects of reaction parameters were thoroughly examined. Additionally, the study identified the optimal conditions and the mechanism by which olive stones biochar (OSB) and FeCl₃ remove rhodamine B during the adsorption and coagulation–flocculation treatment, respectively. Finally, the study analyzed the combined coagulation–flocculation/adsorption process to provide the best performance under optimum conditions.

2. Materials and methods

2.1. Dye solutions and measuring techniques

A 100 mg L⁻¹ stock solution of rhodamine B dye was prepared. The physico-chemical properties of rhodamine B are as follows: chemical formula: C₂₈H₃₁ClN₂O₃, class: cationic dye, molar mass (g mol⁻¹): 479.02, solubility in water (20 °C) (g L⁻¹): 50, λ_{max} (nm): 554.

A series of rhodamine B solutions with well-defined concentrations for standard solutions (0 to 12 mg L⁻¹) and for adsorption and coagulation–flocculation tests was prepared in distilled water by dilution from the 100 mg L⁻¹ stock solution. The absorbance of each solution sample was read on a UV spectrophotometer (Optizen 2120 UV) at a wavelength of 554 nm, and the corresponding rhodamine B contents (mg L⁻¹) were determined according to Beer–Lambert's relation.

2.2. Preparation of coagulant solution

Iron chloride solution was prepared using FeCl₃ (iron(III) chloride, reagent grade 97%). The substance identified is available as a black powder. Due to its rapid reactivity with air, FeCl₃ was handled with extreme caution. Consequently, the FeCl₃ coagulant was quickly removed from its container, which was immediately sealed to preserve its contents. The stock solution of iron chloride was prepared by dissolving 10 g of FeCl₃ in 1 L of distilled water and saved for coagulation–flocculation tests.

2.3. Biochar preparation

A sample of olive stones from Ghoufi town, Batna, Algeria was washed with tap water until the washing water became clear and then dipped in distilled water, followed by air-drying. After crushing, the pits were oven-dried for 24 hours at 105–110 °C and sieved to retain particles between 1 and 2 mm in size. The mixture was carbonized under limiting oxygen condition for 2 hours at 700 °C, then soaked in 0.1 N HCl to remove the resulting mineral matters from pyrolysis and washing with distilled water until the pH of the washing water was in the range of 6 to 7. The produced biochar was dried at 105–110 °C for 24 hours. Therefore, olive stones biochar (OSB) was ready for adsorption tests.

2.4. Adsorbent feature analysis

A PerkinElmer Spectrum Two instrument was used to identify the chemical groups in the prepared adsorbent (OSB) using Fourier transform infrared (FTIR) spectroscopy. A Tescan Vega3 instrument was employed for scanning electron microscopy (SEM) imaging and energy dispersive X-ray (EDX) spectroscopy. The analysis of adsorption/desorption isotherms of nitrogen gas (N₂) provided the textural properties of the prepared biochar OSB using ASAP 2010 V5.00E. For the determination of the point of zero charge (pH_{pzc}), which refers to the pH at which the net charge on the surface of an adsorbent material is zero, the procedure outlined by (ref. 35) was followed. In short description, a set of NaCl (0.1 M) solutions with initial pH values ranging from 2 to 12 was prepared, after which the adsorbent



with a concentration of 4 g L^{-1} was added in the NaCl solutions. The final pH of each solution was determined after 12 hours of stirring. The pH_{PZC} is determined by plotting the pH of the final solution against the initial pH. The point when initial and final pH are equal is the pH_{PZC} of OSB.

2.5. Description of dye removal tests

Rhodamine B removal was tested by one step of treatment, adsorption treatment and coagulation–flocculation treatment, and by coupling of the two processes, namely, coagulation–flocculation, followed by an adsorption step.

The adsorption tests were performed by magnetic mixing, after introducing a pre-measured quantity of biochar to rhodamine B solutions (volume of 50 mL). The samples taken after adsorption tests were vacuum-filtered through a $0.45 \mu\text{m}$ pore size membrane. Several factors that impact the process were investigated.

- Adsorption kinetics: the kinetics study was monitored from 2 minutes to 6 hours for 10 mg L^{-1} initial rhodamine B and 4 g L^{-1} of the prepared biochar at $20 \text{ }^\circ\text{C}$ of temperature.

- Impact of adsorbent dosage: to ascertain the optimal amount of OSB, a range of OSB dose ($1\text{--}10 \text{ g L}^{-1}$) was added to 10 mg L^{-1} of rhodamine B solution at $20 \text{ }^\circ\text{C}$ temperature.

- The impact of the initial pH: the range of pH studied was from 2 to 12, and in order to set the initial pH of the solutions to the designated value, 0.1 M HCl and 0.1 M NaOH solutions were used. The concentration of biochar adopted is 4 g L^{-1} and that of rhodamine B is 10 mg L^{-1} .

- The influence of the initial pollutant content: the study on the adsorption isotherms of biochar was investigated using different concentrations of rhodamine B solutions from 1 mg L^{-1} to 100 mg L^{-1} at $20 \text{ }^\circ\text{C}$ temperature in a period corresponding to the equilibrium time, established from the kinetics testing.

- The effect of adsorbent dose: in this test, rhodamine B concentrations were fixed at 10 mg L^{-1} and the adsorbent content (OSB) was altered from 1 to 10 g L^{-1} at $20 \text{ }^\circ\text{C}$.

- The impact of solution temperature: the study of temperature impact on the adsorption process was implemented for

a series of rhodamine B solutions with concentrations from 1 to 100 mg L^{-1} at temperatures of 20, 30, 40 and $50 \text{ }^\circ\text{C}$ with a fixed adsorbent content of 4 g L^{-1} .

- Reuse and regeneration: the reuse step involves using the recovered adsorbent from the first adsorption test (cycle 1) for the subsequent adsorption test (cycle 2) with the same concentrations of rhodamine B (10 mg L^{-1}) and OSB adsorbent (4 g L^{-1}). The regeneration step involves rinsing the adsorbent using NaOH solution (0.1 M) and successive washing with distilled water up to the moment where the filtrate is neutralized.

The coagulation–flocculation tests were done using a flocculator, adding a set amount of FeCl_3 to 300 mL of pre-set rhodamine B solution concentrations. The samples were mixed with high-speed stirring for 3 min and then at slow speed of stirring for 17 min, and then the time was completed in one hour for the sedimentation stage and filtered using a $0.45 \mu\text{m}$ pore size membrane under vacuum. The initial content of rhodamine B and FeCl_3 were tested.

- The effect of coagulant dose: the JAR TEST were carried out for coagulant concentration range from 10 mg L^{-1} to 2000 mg L^{-1} with a fixed rhodamine B concentration of 10 mg L^{-1} .

- Influence of rhodamine B concentration: The range of rhodamine B concentration studied was from 1 mg L^{-1} to 100 mg L^{-1} , with a fixed coagulant dose of 80 mg L^{-1} .

- The effect of pH: the pH was studied in the range from 2 to 12 under the same operational condition of coagulant dose (80 mg L^{-1}) and 10 mg L^{-1} of rhodamine B concentration.

The treatment test for the combination of two processes was started by the coagulation–flocculation step using 80 mg L^{-1} , followed by the adsorption step. The amount of the adsorbent was varied within the range from 0.5 g L^{-1} to 5 g L^{-1} (Fig. 1).

The adsorption capacities of rhodamine B on OSB (q_t (mg g^{-1})) at time t , equilibrium (q_e (mg g^{-1})), and the efficiencies of dye removal (%) were assessed according to eqn (1)–(3).

$$q_t = \frac{(C_0 - C_t)}{m} \times V \quad (1)$$

$$q_t = \frac{(C_0 - C_e)}{m} \times V \quad (2)$$

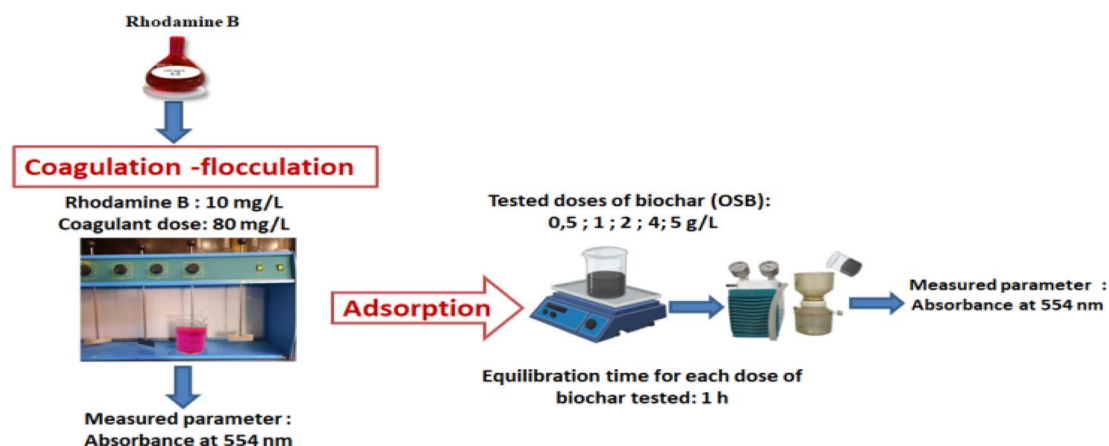


Fig. 1 Schematic of the combined coagulation–flocculation/adsorption tests (rhodamine B).



$$\text{Efficiency}(\%) = \frac{(C_0 - C_e)}{C_0} \times 100 \quad (3)$$

where C_0 (mg L^{-1}), C_e (mg L^{-1}), and C_t (mg L^{-1}) are the rhodamine B content at initial, equilibrium, and time t , respectively, m (g) is the OSB mass introduced and V (L) denotes the sample volume tested.

2.6. Statistic tests

Chi-square (χ^2) and R -square (R^2) are both statistical measures used to assess the fit between the predicted data obtained by fitting the adsorption models $q_{e,\text{cal}}$ and experimental data obtained by experience $q_{e,\text{exp}}$, the (R^2) statistic coefficient (eqn (4)) should converge towards 1, and the (χ^2) test statistic (eqn (5)) should be close to zero.^{36,37}

$$\text{Coefficient of determination: } R^2 = 1 - \frac{\sum (q_{e,\text{exp}} - q_{e,\text{cal}})^2}{\sum (q_{e,\text{exp}} - q_{e,\text{mean}})^2} \quad (4)$$

$$\text{Chi-square: } \chi^2 = \sum_{i=1}^N \frac{(q_{e,\text{exp}} - q_{e,\text{cal}})^2}{q_{e,\text{cal}}} \quad (5)$$

where both $q_{e,\text{exp}}$ and $q_{e,\text{cal}}$ represent the capacity of adsorption at equilibrium, $q_{e,\text{mean}}$ denotes the average of $q_{e,\text{exp}}$ values and N presents the number of trials conducted.

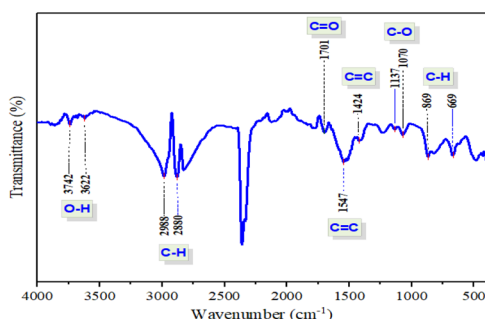


Fig. 2 Analysis of chemical functionalities on the ATR-FTIR spectrum of OSB.

3. Results and discussion

3.1. Adsorbent feature analysis

The examination of the ATR-FTIR spectrum of the prepared biochar (Fig. 2) reveals that OSB possesses a variety of chemical groups, which may contribute to bond formation with that of rhodamine B present in the solution. The main groups that may participate in hydrogen bond formation are OH and NH, which are present in the biochar prepared in this work, confirmed by the presence of 3742, 3622 cm^{-1} (ref. 38) and 1547 cm^{-1} (ref. 39) peaks, respectively. According to (ref. 40), the vibration at wavenumbers of 1547 cm^{-1} can also indicate the C-C ring elongation of aromatics. The broad band located at the wavenumber of 1701 cm^{-1} may be attributed to C=C bonds.⁴¹ The C-H stretching vibration of the symmetric or asymmetric of aliphatic acid was verified by the peaks presented at 2880 and 2988 cm^{-1} .^{42,43} The peaks centered at 1424 cm^{-1} characterized the C=O stretching vibration or the N-H in-plane bending.³⁹ The set wavenumbers in the range of 1000–1200 cm^{-1} (the peaks verified are 1070 and 1137 cm^{-1}) corresponding to the vibration of C-O bonds (ref. 44) indicated that the vibration of the C-H moiety in the pyridine ring and that of the out-of-plane deformation are obtained at wavenumbers of 669 and 869 cm^{-1} .

Fig. 3 exhibits the SEM images of the synthesized biochar. The image shows the porous structure of OSB, which is irregular in size and shape, indicating relatively high surface areas. On the other hand, EDX analysis of the biochar clearly indicated that the elementary composition contains atomic percentages of 94.32% and 5.26% for carbon and oxygen, respectively.

BET analysis revealed that OSB has a highly developed pore structure and S_{BET} (specific surface area) of 475.05 $\text{m}^2 \text{g}^{-1}$ with an average pore diameter of 15.74 Å (1.57 nm).

3.2. Single adsorption treatment results

3.2.1. Adsorption kinetics. The examination of kinetics behavior enabled to follow the evolution of the treatment efficiency, estimation of time required for equilibrium, and identification of the predominant mechanisms in the adsorption process by analyzing the experimental results modeling *via* the pseudo-first order kinetic model⁴⁵ (eqn (6)) and the pseudo-

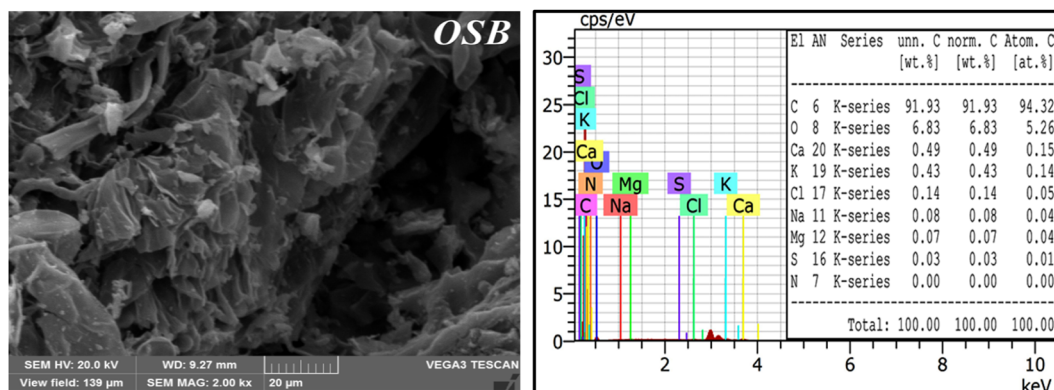


Fig. 3 Morphological and elemental characteristics of the prepared biochar (OSB).



second order kinetic model⁴⁶ (eqn (7)) and to control the diffusion of adsorbent molecules on the surface and inside the adsorbent particles using the intraparticle diffusion kinetic model⁴⁷ (eqn (8)).

$$q_t = q_c(1 - e^{-K_1 t}) \quad (6)$$

$$q_t = \frac{q_c^2 K_2 t}{1 + q_c K_2 t} \quad (7)$$

$$q_t = K_{int} t^{1/2} + C \quad (8)$$

The corresponding parameters are K_1 , K_2 , C and K_{int} ; PFO speed constant in (min^{-1}), PSO speed constant in ($\text{g min}^{-1} \text{mg}^{-1}$), boundary layer depth constant (mg g^{-1}) and Weber-Morris rating constant in ($\text{mg g}^{-1} \text{min}^{-1/2}$).

The evolution of adsorption capacity of OSB had a positive correlation with the progression of contact duration prior to achieving the equilibrium (Fig. 4a). Optimal removal conditions were determined to have an equilibrium time of 1 hour, a removal efficiency of 97.79%, and a capacity of adsorption of 2.445 mg g^{-1} , as shown in Fig. 4a.

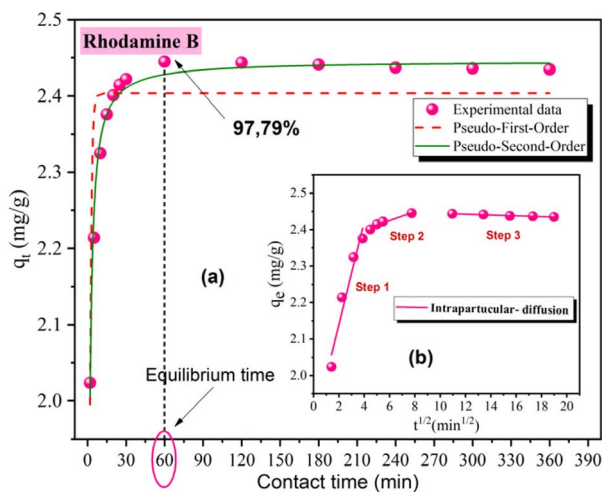


Fig. 4 Experimental data for rhodamine B adsorption on OSB (a) non-linear fit of PFO, PSO models. (b) Intra-particle diffusion model ([rhodamine B] = 10 mg L^{-1} ; OSB = 4 g L^{-1} ; $T = 20 \text{ }^\circ\text{C}$).

To elucidate the adsorption mechanism of rhodamine B on OSB, data obtained from the experiment were well fitted by three models of adsorption kinetics: PFO, PSO and intraparticle diffusion kinetic model. As shown in Fig. 4a and Table 1, the adjustment results of the non-linear models for PFO and PSO are very satisfactory. This is evidenced by the values of the statistic coefficient (R^2), which is close to 1, and the chi-square (χ^2), which is close to 0.

To select the most suitable fitting model, comparison between the estimated adsorption capacity through model fitting to the experimental points ($q_{e,cal}$) with the maximum adsorption capacity obtained experimentally ($q_{e,exp}$) was done, which corresponds to the equilibrium time for rhodamine B adsorption (1 h). According to the results obtained and presented in Table 1, it seems then that the PSO kinetic model is more appropriate than the PFO model for modeling rhodamine B adsorption kinetics since $q_{e2,cal}$ is closer to that obtained experimentally ($q_{e,exp}$). This implies that rhodamine B adsorption on OSB is largely chemical than a physical process.

As illustrated in Fig. 4b, the intra-particle diffusion plots show three lines, and it was also clear that the first line does not intersect the origin, implying that the adsorption behavior was not solely governed by the intra-particle diffusion mechanism but also by multiple mechanisms, which can take place during the adsorption of the pollutant onto the adsorbent.^{48,49} The values obtained for the intra-particle diffusion rate (Table 1) could be ranked in the prescribed arrangement: $K_{int,1} > K_{int,2} > K_{int,3}$ (Table 1). This result leads to the inference that the transfer of rhodamine B molecules from the solution to OSB external surfaces occurs rapidly at the first time of adsorption. The lower slopes in the last linear parts suggest that the intra-particle diffusion rates of the pollutant decline as equilibrium is progressively achieved. The contact between the surface internal and the rhodamine B molecules were translated by the internal diffusion or what is called the pore filling mechanism, which depends on the scale of the adsorbate and that of the adsorbent pore.⁵⁰ Therefore, OSB is a highly porous material (average pore diameter of 1.57 nm) with key factors of surface area ($475.05 \text{ m}^2 \text{ g}^{-1}$), which can enhance the adsorption capacity. As stated by (ref. 51), the molecular structure of rhodamine B and its dimer formation viewed from different

Table 1 Parameters of adsorption kinetic models (PFO and PSO) for rhodamine B on OSB

Pseudo-first-order: $q_t = q_c(1 - e^{-k_1 t})$					Pseudo-second-order: $q_t = \frac{q_c^2 k_2 t}{1 + q_c k_2 t}$			
$q_{e,exp}(\text{mg g}^{-1})$	$q_{e1,cal}(\text{mg g}^{-1})$	$K_1(\text{min}^{-1})$	R^2	χ^2	$q_{e2,cal}(\text{mg g}^{-1})$	$K_2(\text{g mg}^{-1} \text{min}^{-1})$	R^2	χ^2
2.445	2.404	0.886	0.768	0.004	2.446	0.9311	0.986	0.0002
Intraparticle-diffusion: $q_t = K_{int} t^{1/2} + C$								
$K_{int,1}(\text{mg g}^{-1} \text{min}^{-1/2})$	$C_1 \text{ mg g}^{-1}$	R^2	$K_{int,2}(\text{mg g}^{-1} \text{min}^{-1/2})$	$C_2 \text{ mg g}^{-1}$	R^2	$K_{int,3}(\text{mg g}^{-1} \text{min}^{-1/2})$	$C_3 \text{ mg g}^{-1}$	R^2
0.141	1.857	0.945	0.012	2.350	0.953	-0.001	2.456	0.974



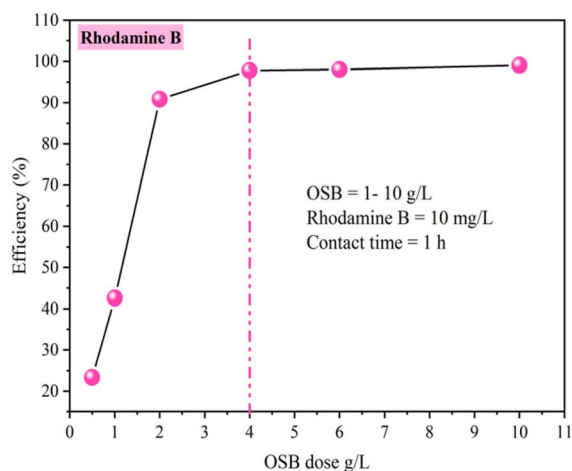


Fig. 5 Data illustrating the influence of OSB adsorbent on rhodamine B removal efficiency.

directions present dimensions such as 0.5 width and 1.22 height. These dimensions allow them to pass easily into the pores of the OSB.

3.2.2. Impact of adsorbent dose. Fig. 5 presents the variation in the rhodamine B removal efficiencies using a different dose on the biochar prepared in this study. The results clearly demonstrate that the removal efficiency is enhanced with each additional dose of biochar, which is attributable to the increase in the count of effective interactions sites.¹⁴ The optimal dose of OSB was found to be 4 g L⁻¹, achieving remarkable removal efficiency (97.79%). This indicates the performance of biochar in rhodamine B removal, making it a promising material for water treatment applications.

3.2.3. Impact of initial pH. The correlation between the initial pH of the solution and the efficiency of dye removal is illustrated in Fig. 6. From the results, the alteration in the

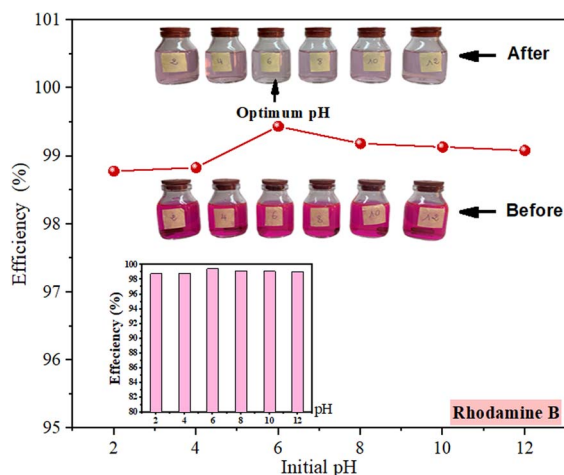


Fig. 6 Rhodamine B removal efficiencies as a function of initial pH of treated solutions ([rhodamine B]₀ = 10 mg L⁻¹; pH = 2 to 12; OSB = 4 g L⁻¹; contact time = 1 h; T = 20 °C).

medium's pH does not significantly affect the proportion of rhodamine B removed by OSB. Even under strongly acidic (pH = 2) or basic (pH = 12) conditions, the removal performance of rhodamine B decreases by 0.7 to 0.3%, respectively, than that of the optimum pH (99.45% at pH = 6), implying that the biochar as prepared exhibits a high degree of pH tolerance. This finding is supported by the literature.⁵²

When plotted on a small scale, the graph indicates a tendency that firstly increases and then decreases (Fig. 6). On the other hand, at reduced pH levels, the abundant H⁺ ions encourage the protonation of the functional groups in the surface of adsorbent, resulting in a more positively-charged surface and consequently repelling positively-charged dye molecules.² Specifically, rhodamine B dye is a xanthene dye existing in cationic form as rhodamine BH⁺ in the pH range from 1.0 to 3.0 and zwitterion rhodamine B ± at pH > 4.0.^{51,53} When the positive charges are located on the =N⁺ groups and the negative ones on the COO⁻ group in the molecule of this dye.⁵⁴ According to ref. 2, the H⁺ ions also compete with rhodamine B molecules, which exist in monomeric and cationic forms,⁵⁵ for occupying the adsorption sites. Conversely, as the pH of the solution increases (pH > p*H*_{pzc} (5.52)), the charge at the adsorbent's surface becomes negative, resulting from the adsorption of OH groups and chemical functionalities deprotonation, thus enhancing the adsorption through electrostatic attraction. The slight decline in the efficiency of removal at higher pH values (pH > 8) is attributed to the formation of hydrated rhodamine B ions, which form larger molecular structures (dimers) that obstruct the dye's entry into the material's pores.^{2,55} However, the overall removal efficiency fluctuates within a 1% range, remaining within the acceptable error bar tolerance. Thus, while the electrostatic effect is present, it does not have a strong influence on the adsorption process. This outcome is in accordance with the findings of (ref. 56).

The electrostatic interactions, hydrophobic interactions, pore-filling, hydrogen bonding, π-π and n-π interactions are the main interaction that can occur between organic pollutants and biochar.⁵⁰ For rhodamine B, the electrostatic forces do not have a strong effect on the process. According to (ref. 57), the hydrogen bonding and π-π interaction are the primary mechanism applicable in rhodamine B adsorption onto biochar. The hydrogen bonds occur between the OH, COOH, and NH groups in the prepared biochar (OSB) as H donor and the oxygen, nitrogen atoms rhodamine B as H acceptor.^{50,58} Additionally, rhodamine B has a carboxyl group (-COOH) as the H-donor, which can interact with oxygen, nitrogen-containing biochar as an H acceptor.⁵⁷ π-π interactions are the interactions that occur between a π-electron donor and π-electron acceptor.⁵⁹ The aromatic groups of dye can interact with the aromatic ring of biochar *via* π-π stacking.⁵⁸ On the other hand, the π-π interaction can occur between the oxygen-containing OH groups of the prepared biochar and the benzene ring in the dye.⁵⁸ The n-π interactions are another type of electron donor-acceptor interaction that can occur between the oxygen in the carbonyl groups (electron donors) of the OSB prepared in this work (FTIR spectroscopy results) and the aromatic rings (electron acceptors) of rhodamine B.⁶⁰ The pore-filling mechanism



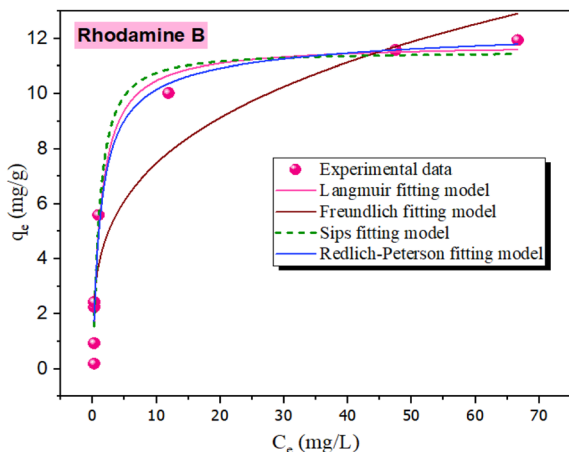


Fig. 7 Modeling of experimental data at equilibrium (OSB = 4 g L⁻¹, T = 20 °C; rhodamine B = 1–100 mg L⁻¹).

can be controlled by the diffusion of rhodamine B molecule on the surface and inside the biochar pores. The hydrophobic interactions can be applied between the hydrophobic groups of biochar and the hydrophobic groups of rhodamine B.⁵⁹

3.2.4. Adsorption isotherms study. To study the adsorption at equilibrium (Fig. 7), a set of rhodamine B solutions with concentration varying from 1 mg L⁻¹ to 100 mg L⁻¹ and an adsorbent concentration fixed at 4 g L⁻¹ was used. The results demonstrated an improvement in the capacity of adsorption as the initial rhodamine B content increased.

To get more information about the adsorption process and to determine the maximum adsorption capacity of rhodamine on OSB, the adjustment of experimental data at equilibrium is recommended. Thus, Langmuir⁶¹ (eqn (9)), Freundlich⁶² (eqn (10)), Redlich Peterson⁶³ (eqn (11)), and Sips⁶⁴ (eqn (12)) isothermal models were applied in this research paper.

$$\text{Langmuir : } q_e = \frac{Q_{\max} K_L C_e}{1 + K_L C_e} \quad (9)$$

$$\text{Freundlich : } q_e = K_F C_e^{\frac{1}{n}} \quad (10)$$

$$\text{Redlich – Peterson : } q_e = \frac{K_{RP} C_e}{1 + a_{RP} C_e^{\beta}} \quad (11)$$

$$\text{Sips : } q_e = \frac{q_s K_s C_e^{1/n_s}}{1 + K_s C_e^{1/n_s}} \quad (12)$$

The related parameters of these models are: Langmuir adsorption capacity (Q_{\max} (mg g⁻¹)), the Langmuir constant (K_L (L mg⁻¹)), Freundlich constants (K_F (mg g⁻¹)/(mg L⁻¹)^{1/n}, and n (dimensionless)), Redlich–Peterson constants (K_{RP} (L g⁻¹) and a_{RP} (mg L⁻¹)^{-β}), where β must be between 0 and 1, Sips adsorption capacity (q_s (mg g⁻¹)), Sips constant (K_s (L mg⁻¹)), and the adsorbent's heterogeneity (n_s).

Based on the findings outlined in Table 2, the Langmuir model, with a high determination coefficient ($R^2 = 0.972$) and lower error value ($\chi^2 = 0.784$), showed the greatest consistency with the experimental data compared to the other fitted models. This suggests that rhodamine B was adsorbed on the homogeneous adsorbent surface-forming monolayers,⁵⁸ with a Q_{\max} (maximum adsorption capacity of Langmuir) of 11.82 mg g⁻¹. For comparison, this capacity is higher than that obtained when using the activated raw materials such as treated banana peel (9.52 mg g⁻¹),⁶⁵ cinnamon wood biochar (2.01 mg g⁻¹)⁶⁶ and comparable with a capacity obtained with a coconut shell-derived biochar with Fe–N co-modification of 12.41 mg g⁻¹.⁶⁷

The dimensionless parameter R_L is used to determine whether adsorption is favorable or not,⁶⁸ and the equation for calculating R_L is as follows (eqn (13))

$$R_L = \frac{1}{1 + C_0 K_L} \quad (13)$$

where K_L (L mg⁻¹) is Langmuir's constant (dimensionless).

Adsorption is favorable when R_L lies between 0 and 1, is unfavorable if R_L exceeds 1, and is irreversible when R_L is 0.⁶⁹ For the adsorption of rhodamine B on OSB, the R_L : 0 < R_L (0.013 to 0.562) < 1; as a result, the adsorption process is favorable. This hypothesis is also confirmed by the fitting results of Freundlich isotherm (Table 2), which indicate a value of $1/n$ less than 1 (0.288 < 1), reflecting a favorable adsorption of the tested dye on OSB.

3.2.5. Thermodynamic study. This section of work is centered on the thermodynamic parameters that are instrumental in elucidating the spontaneity, endothermic or

Table 2 Parameters estimated for rhodamine B non-linear adsorption isotherm models

Langmuir : $q_e = \frac{Q_{\max} K_L C_e}{1 + K_L C_e}$					Freundlich : $q_e = K_F C_e^{\frac{1}{n}}$				
K_L (L mg ⁻¹)	Q_{\max} (mg g ⁻¹)	R^2	χ^2	K_F (mg g ⁻¹)/(mg L ⁻¹) ^{1/n}	n	R^2	χ^2		
0.780	11.821	0.972	0.784	3.855	3.475	0.900	2.806		
Redlich – Peterson : $q_e = \frac{K_{RP} C_e}{1 + a_{RP} C_e^{\beta}}$					Sips : $q_e = \frac{q_s K_s C_e^{1/n_s}}{1 + K_s C_e^{1/n_s}}$				
K_{RP} (L g ⁻¹)	a_{RP} (mg L ⁻¹) ^{-β}	β	R^2	χ^2	q_s (mg g ⁻¹)	K_s (L mg ⁻¹)	n_s	R^2	χ^2
9.833	0.933	0.97	0.973	0.9074	11.524	0.944	0.852	0.973	0.9073



exothermic characteristics, and the irregularity of the solid-liquid phase in the adsorption process. Furthermore, these parameters can be applied to expound the mechanisms of adsorption, thereby differentiating between the processes governed by physical and chemical interactions.⁷⁰ The parameters include ΔG° (Gibbs free energy), ΔH° (enthalpy change) and ΔS° (entropy change). The utilization of eqn (14)–(16) is integral to deriving the estimates for ΔG° , ΔH° , and ΔS° in this context.

$$\Delta G^\circ = \Delta H^\circ - T\Delta S^\circ \quad (14)$$

$$\Delta G^\circ = -RT \ln(K_c) \quad (15)$$

By replacing eqn (14) in eqn (15), the equation obtained is named the Van't Hoff relation (eqn (16)).

$$\ln(K_c) = -\frac{\Delta H^\circ}{R} \times \frac{1}{T} + \frac{\Delta S^\circ}{R} \quad (16)$$

where ΔG° (kJ mol^{-1}) denotes the Gibbs energy change, ΔH° (kJ mol^{-1}) is the enthalpy change, and ΔS° (J (mol K)^{-1}) is the entropy change. R ($8.314 \text{ J (mol K)}^{-1}$) denotes the ideal gas constant, while T is the temperature of solution in K.

The K_c equilibrium constant is dimensionless, calculated as a function of K_L (L mg^{-1}) (the Langmuir isotherm constant for each temperature); this constant was calculated using eqn (17), as noted by (ref. 71).

$$K_c = K_L \times M_{\text{adsorbate}} \times 55.5 \times 10^3 \quad (17)$$

where $M_{\text{adsorbate}}$ presents the molar mass of rhodamine B and 55.5 mol L^{-1} expresses the molarity of water.

Fig. 8a shows the results of the determination of K_L (L mg^{-1}) from the adsorption curves of rhodamine B on OSB in the equilibrium state at 20, 30, 40 and 50 °C, while Fig. 8b shows the representation of the Van't Hoff straight-line plot.

The ΔG° value is varied from -29.26 to $-24.21 \text{ kJ mol}^{-1}$ (Table 3), and all Gibbs energy changes are negative, indicating the spontaneous and favorable nature of the adsorption process.

The ΔG° values varied from -29.26 to $-24.21 \text{ kJ mol}^{-1}$ (Table 3) and all Gibbs energy changes values were negative, indicating the spontaneous and favorable nature of the adsorption process.^{72,73} Considering the values of ΔH° (>0) in Table 3 and Fig. 8b, the adsorption of rhodamine B is endothermic,⁷⁴ accompanied by heat absorption from the surroundings, contributing to an increase in the internal energy of the system. Additionally, the system exhibits a positive value of (ΔS°), which reflects the increased randomness and disorder at the adsorbent/adsorbate phase throughout the adsorption,^{72,73} implying that rhodamine B molecules are not structured in a specific manner upon adsorption.

3.2.6. Reuses and regeneration. The determination of the lifespan of an adsorbent (potential for reuses and regeneration) is crucial from both economic and environmental perspectives.⁵⁶ Adsorption tests for the reusability of the adsorbent were conducted under the same operational conditions and with the same concentrations of adsorbent and rhodamine B in the solutions. The results outlined in Fig. 9 show that the

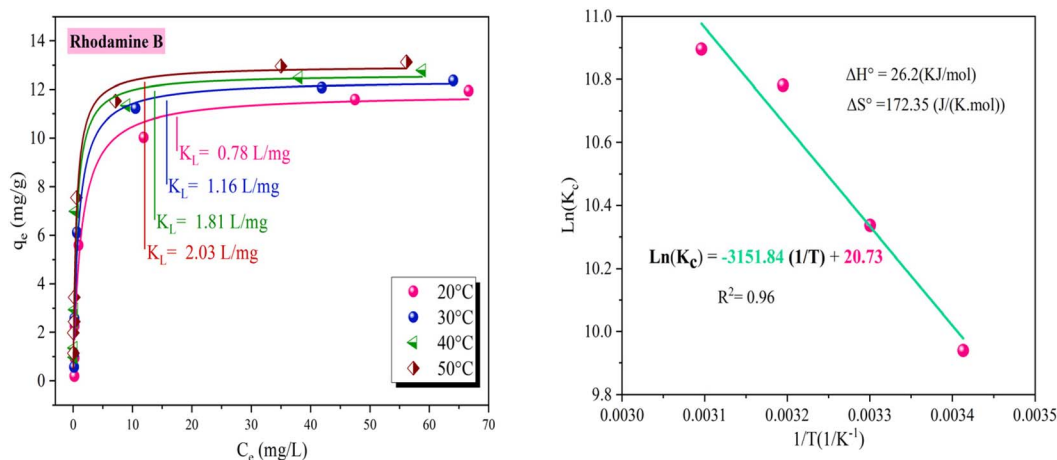


Fig. 8 Adsorption behavior of rhodamine B on OSB across different temperatures ([OSAC] = 1 g L^{-1} , [rhodamine B]₀ = $10\text{--}400 \text{ mg L}^{-1}$, $T = 20\text{--}50 \text{ }^\circ\text{C}$, contact time = 1 h).

Table 3 Thermodynamic parameters of rhodamine B adsorption on OSB ([OSB] = 1 g L^{-1} , [rhodamine B]₀ = $10\text{--}400 \text{ mg L}^{-1}$, contact time = 1 h)

T (K)	K_L (L mg^{-1})	K_c	Van't Hoff equation	ΔG° (kJ mol^{-1})	ΔH° (kJ mol^{-1})	ΔS° ($\text{J K}^{-1} \text{ mol}^{-1}$)
298	0.78	20 736.78	$y = -3151.84x + 20.73$	-24.21	26.2	172.35
303	1.16	30 839.31		-26.04		
313	1.81	48 119.95		-28.06		
323	2.03	53 968.79		-29.26		



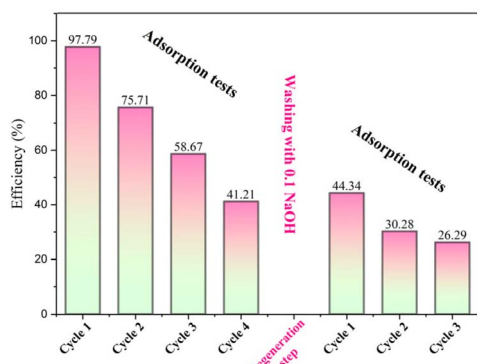


Fig. 9 Efficiency of rhodamine B removal over multiple cycles and regeneration of OSB.

effectiveness of removing rhodamine B by the prepared biochar in this study decreases with each cycle, from 97.79% in cycle 1 to 41.21% in cycle 4. After the regeneration of the biochar with NaOH (0.1 M), the efficiency increased by 3.13%, which indicates the release of some adsorption sites. However, the efficiency remained relatively low (<50%), suggesting the formation of strong chemical bonds that are difficult to break. Consequently, biochar derived from olive stones (OSB) was tested over four successive cycles, achieving efficiencies exceeding 50%. This indicates the potential use of this type of waste, with simple pyrolysis, for adsorption purposes.

3.3. Single coagulation–flocculation treatment

3.3.1. Effect of FeCl_3 dose. It is crucial to account for the impact of the coagulant dosage when selecting the optimal dose for the coagulation–flocculation process. The optimum dose is determined in an approach that minimizes cost and generation of sludge and optimizes the removal performance of the treatment process.⁷⁵ For this purpose, rhodamine B removal efficiency (10 mg L⁻¹) was monitored as a function of coagulant (FeCl_3) dose (Fig. 10). As presented, the dye removal efficiency improved as the coagulant dosage increased, and the best

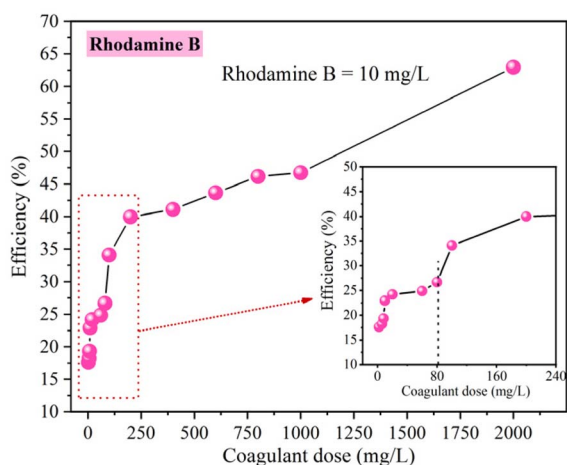


Fig. 10 Impact of FeCl_3 dosage on coagulation–flocculation treatment efficiency.

removal efficiency (62.95%) was registered with a high coagulant dose of 2000 mg L⁻¹. As stated by (ref. 76), a high dosage of coagulant provides the structure (bridging) of hydroxide precipitates to capture colloidal particles, increasing the collision efficiency and producing more solid flocs. On the other hand, (ref. 77) showed that when the re-stabilization of the colloid in the system will occur due to the high amount of coagulant, then the leading coagulation mechanism is charge neutralization. According to the results presented in Fig. 10, no decrease in the removal efficiency was recorded with the coagulant dosage increasing from 10 to 2000 mg L⁻¹.

3.3.2. Effect of initial pH. pH is a key factor in the coagulation process, influencing the charge of particles and solubility

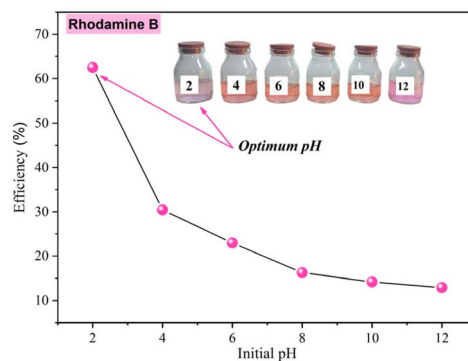


Fig. 11 Unveiling the influence of pH on rhodamine B removal by FeCl_3 .

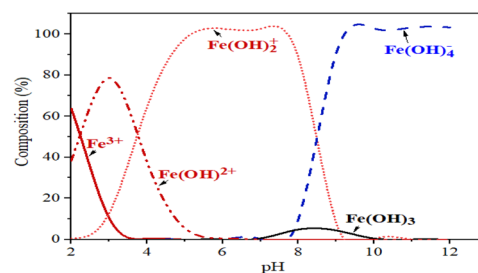


Fig. 12 Iron(III) speciation as a function of pH for an FeCl_3 solution (80 mg L⁻¹).

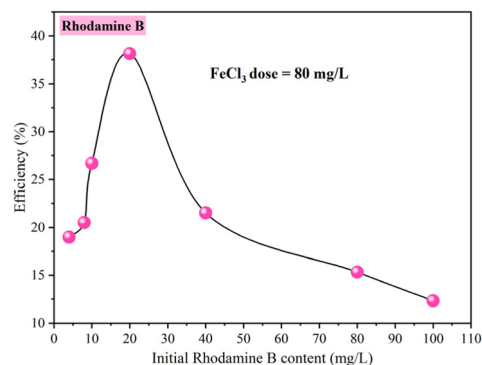


Fig. 13 Effect of initial rhodamine B content on coagulation–flocculation ($[\text{rhodamine B}]_0 = 5\text{--}100$ mg L⁻¹).



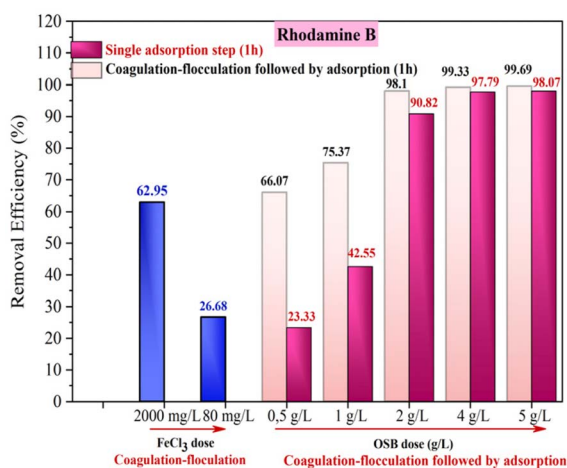


Fig. 14 Comparison of rhodamine B removal efficiencies by coagulation–flocculation, adsorption and combined coagulation–flocculation followed by adsorption.

of coagulants. In this work, the impact of the initial pH of the sample was studied at pH values from 2 to 12 for a rhodamine B solution of 10 mg L^{-1} and a coagulant content of 80 mg L^{-1} . From the results presented in Fig. 11, pH 2 can be considered as the optimum pH when the removal efficiency is the best, and the treatment is more effective in acidic pH when 62.95% of rhodamine B is removed at $\text{pH} = 2$. However, the effectiveness of the treatment gradually decreases with increasing pH.

The initial pH significantly influences the removal of rhodamine B through coagulation–flocculation using ferric

chloride (FeCl_3). At lower pH levels, the efficiency of rhodamine B removal increases due to enhanced coagulation mechanisms. As mentioned above, rhodamine B dye is in the cationic form as rhodamine BH^+ at $\text{pH} 1.0\text{--}3.0$ and in the zwitterionic form as rhodamine B^\pm at $\text{pH} > 4.0$. Using the concept at acidic pH, ferric ions hydrolyze to form ferric ions and positively-charged ferric hydroxides, mainly Fe^{3+} , $\text{Fe}(\text{OH})^{2+}$, and $\text{Fe}(\text{OH})_2^+$ (Fig. 12). The electrostatic attraction of rhodamine B molecules is less favorable at such a low pH. However, at low pH, the high removal efficiency of rhodamine B may be related to the potential influence of other forces, such as hydrogen bonding and hydrophobic interactions, to exert a greater influence than electrostatic interaction. Additionally, the process of sweep flocculation becomes more effective at lower pH levels as the precipitation of ferric hydroxides traps the dye particles within the flocs, thus improving the overall removal efficiency. Studies have shown that optimal removal occurs at an initial pH of about 3.5, where charge neutralization and sweep flocculation are most effective, leading to dye removal efficiencies as high as 96.53% (ref. 78). Further, (ref. 79) reported that the mechanisms driving this process include the adsorption of rhodamine B onto the ferric hydroxides and the subsequent formation of flocs, which are more stable and larger at lower pH, thus facilitating their removal from the solution.

3.3.3. Effect of rhodamine B content. The effect of initial rhodamine B content was analyzed at varying doses from 5 mg L^{-1} to 100 mg L^{-1} . Fig. 13 shows the tendency of the removal effectiveness, where an increase in the removal of dye was registered at 36.15% when its concentration increased to 20 mg L^{-1} . Then, a second stage is seen where the removal

Table 4 Comparison of adsorption and coagulation–flocculation processes for rhodamine B removal

Adsorption						
Adsorbent	Time (min)	Adsorbent (mg L^{-1})	pH	Rhodamine B concentration (mg L^{-1})	Efficiency (%)	References
Peanut shell biochar	60	0.325	3	1	94	80
St. John's wort (<i>Hypericum perforatum</i>)	45	2000	7	20	80	81
Olive stone biochar	60	4000	6	10	97.79	This study
Coagulation–flocculation						
Coagulant	Time	Coagulant dose (mg L^{-1})	pH	Rhodamine B concentration	Efficiency (%)	References
Bentonite sodium	1 min flash mixing + 10 min slow	200	9	$10 \text{ (g L}^{-1}\text{)}$	53.7	82
alginate bentonite + sodium alginate	mixing + 30 min sedimentation	20	9	$10 \text{ (g L}^{-1}\text{)}$	1.8	82
FeCl_3	3 min flash mixing + 17 min slow mixing + 40 min sedimentation	160 + 4	9	$10 \text{ (g L}^{-1}\text{)}$	91.5	82
		2000	2	$10 \text{ (mg L}^{-1}\text{)}$	62.95	This study
Coagulation–flocculation followed by adsorption						
Coagulant	Adsorbent	Coagulant dose (mg L^{-1})	Adsorbent dose (g L^{-1})	Rhodamine B concentration (mg L^{-1})	Efficiency (%)	References
FeCl_3	Olive stone biochar	80	2	10	98.10	This study



efficiency decreased as the initial rhodamine B concentration increased above 20 mg L⁻¹.

3.4. Coagulation–flocculation followed by adsorption treatment results

In order to reduce the use of high doses of coagulant (FeCl₃), high levels of residual iron should be avoided in the treated water when using the high dose of adsorbent, which will increase the removal efficiencies. A combination of the two processes was tested.

The treatment test was begun by the coagulation–flocculation treatment while introducing a coagulant dose of 80 mg L⁻¹. This dose was chosen as it is lower than the optimum dose obtained in previous tests (FeCl₃ = 2000 mg L⁻¹, R% = 62.95%). The removal efficiency when using 80 mg L⁻¹ FeCl₃ was 26.68% (Fig. 10 and 14). The sample taken after coagulation–flocculation was subjected to adsorption tests over 4 hours of contact time. The amount of OSB used was adjusted from 0.5 g L⁻¹ to 5 g L⁻¹. Fig. 14 shows that the rhodamine B removal efficiency increases with increasing OSB dose. These efficiencies are significantly higher than those obtained after each treatment alone (Fig. 14). It can also be concluded that this combination allows the use of a low dose of coagulant compared with that required (2000 mg L⁻¹) to achieve an effective rhodamine B removal rate as well as a low dose of adsorbent (<2 g L⁻¹) to achieve a removal efficiency of over 90%. Table 4 summarizes some research work on rhodamine B removal by adsorption and coagulation–flocculation. It seems that the combination of coagulation–flocculation, followed by adsorption, significantly enhances the removal efficiency while simultaneously reducing the required adsorbent dose, underscoring the synergistic interaction between the two processes for optimized dye removal.

4. Conclusion

From the results obtained and discussed, it seems clear that in the single adsorption treatment process, the kinetics study indicated that adsorption equilibrium was achieved within one hour, resulting in an efficiency of removal of about 97.79%. The PSO kinetic model well fitted the experimental data of 4 g L⁻¹; thus, the adsorption is a chemical rather than a physical process. The Langmuir isotherm model well describes the results, which mean that rhodamine B molecules were adsorbed on the homogeneous adsorbent surface, forming monolayers. In the single coagulation–sedimentation treatment process, it seems that a high dose of FeCl₃ was recommended for reaching a high removal efficiency of 2000 mg L⁻¹ of FeCl₃ for an efficiency of 62.95%. Combining the two conventional processes, coagulation–flocculation, followed by adsorption on OSB, proved to be an effective technique as it minimizes the disadvantages of each process when used individually. This satisfactory result is based on the fact that this combination allows for the use of a lower dose of coagulant and adsorbent than that required when each process is used alone. In addition, OSB is a highly effective and recyclable adsorbent for

rhodamine B removal. Therefore, the combination of the two treatment processes is considered as a key solution for wastewater treatment, offering methods that can be easily implemented in various industrial settings.

Data availability

The authors confirm that the data used to support the findings of this study are included within the article and are available from the corresponding author upon reasonable request.

Author contributions

Meriem Chebbi: investigation, formal analysis, writing – original draft, Soufiane Youcef: writing – review & editing, Leila Youcef: supervision, conceptualization, writing – original draft, review & editing, Amina Soudani: writing – review & editing, Dridi Chafika: writing – review & editing, Amrane Sahli: formal analysis, Aya Houchet: investigation, formal analysis, Chaima Deroues: investigation, formal analysis.

Conflicts of interest

The authors state that they possess no pecuniary conflicts of interest or personal connections that might have influenced the research presented in this work.

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