



Cite this: *RSC Adv.*, 2024, **14**, 34679

## A spin-polarized analysis of the half-metallicity, mechanical, structural and optoelectronic attributes of full-Heusler $XVC\text{O}_2$ ( $X = \text{B}$ and $\text{P}$ ) alloys

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Cobalt-based Heusler alloys possess high Curie temperatures with half-metallic characteristics, which make them excellent candidates for spintronic applications. These types of Heusler alloys are perfect for the fabrication of magnetic sensors and memory-based devices. Herein, an in-depth first principles analysis of the physical attributes of  $XVC\text{O}_2$  ( $X = \text{B}$  and  $\text{P}$ ) was performed. The mBJ functional was employed to treat electron-ion interaction within their crystal structures. The crystal structure of  $XVC\text{O}_2$  ( $X = \text{B}$  and  $\text{P}$ ) was optimized, and relaxation parameters for both alloys were analyzed. Their ground-state energies at minimum volume were also computed. The Thomas Charpin methodology was employed to compute elastic constants for  $XVC\text{O}_2$  ( $X = \text{B}$  and  $\text{P}$ ), and mechanical properties of both alloys were obtained. For both alloys, metallic behavior was recorded in spin up channels, while indirect bandgaps of 0.38 eV and 1.73 eV were calculated in spin down channels for  $\text{BVC}\text{O}_2$  and  $\text{PVC}\text{O}_2$ , respectively. Both studied alloys showed 100% polarization at the Fermi level. Furthermore, their bonding character was analyzed via electron density plots. The optical characteristic obtained from a complex dielectric equation revealed higher dispersion in the visible range for  $\text{BVC}\text{O}_2$  and  $\text{PVC}\text{O}_2$ , making these materials excellent candidates for spintronics and optoelectronic devices.

Received 11th September 2024

Accepted 16th October 2024

DOI: 10.1039/d4ra06555g

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### 1. Introduction

Presently, the rapidly increasing internet speed necessitates low switching and adaptable RAM technologies for PCs and smartphones.<sup>1</sup> The existing approach to meet this need, which involves shrinking the size of chip cells while adding more transistors, will eventually become ineffective because of efficiency constraints and financial considerations.<sup>2-4</sup> Thus, appropriate semiconductor materials are essential for the development and improvement of optoelectronic devices. The necessity for material design to fulfill particular specifications in optoelectronic devices is driving this change.<sup>5</sup> Half-metallic compounds serve as foundational elements for reshaping the landscape of memory and spintronic devices, information technology and telecommunications.<sup>6-8</sup> In 1983, half-metallic ferromagnetic materials were discovered, exhibiting metallic

properties in one spin state and semiconductor traits in the other.<sup>9-11</sup> The field that uses the spin of electrons for the storage and processing of information is termed as spintronics, and it is a fairly new area of technology that still requires significant work.<sup>12</sup> Using single electron spins as sources and introducing spins into materials to produce and control electrical devices are two of the most researched applications in spintronics.<sup>13</sup> Heusler alloys, which were discovered in 1903, have captured the attention of researchers owing to their exceptional multi-functional applications in magnetic shape memory devices.<sup>14-19</sup> There are a variety of structures based on which these alloys are classified, such as full Heusler ( $X_2\text{YZ}$ ), half Heusler ( $\text{XYZ}$ ) and quaternary Heusler alloys ( $\text{XX}'\text{YZ}$ ).<sup>20,21</sup> Each alloy with these distinct structural compositions has unique features, but full Heusler alloys continue to be appropriate for many magnetic-based applications because of their remarkable characteristics.<sup>22</sup> Numerous Heusler alloys have been reported to exhibit 100% polarization at the Fermi level and investigated in the prior literature; *e.g.*, half-metallic behavior was observed in  $\text{FeRuVZ}$  ( $Z = \text{Si}$  and  $\text{Ge}$ ) Heusler alloys.<sup>23</sup> The silver-based Heusler alloys  $\text{Ag}_2\text{XGa}$  ( $X = \text{Ti}$  and  $\text{V}$ ) have reported to be useful in spintronic applications.<sup>24</sup>  $\text{TiHfFeX}$  ( $X = \text{Al}$ ,  $\text{Ga}$ , and  $\text{In}$ ) was reported to show half-metallic behaviour and considered a viable option for the construction of magnetic shape memory alloys.<sup>25</sup> Nowadays, Co-based Heusler compounds have received significant interest because of their distinct and diverse features

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compared to other Heusler compounds.<sup>26</sup> Cobalt-based Heusler alloys have been extensively studied and are particularly noteworthy as Heusler alloys possessing lower magnetization with the goal of producing high current-induced magnetic switching, ultimately leading to higher stability in the material.<sup>27–29</sup> Additionally, various Co-based alloys such as  $\text{Co}_2\text{MnX}$  ( $\text{X} = \text{Al, Ge, Si, Ga}$ ),<sup>30</sup>  $\text{Co}_2\text{VX}$  ( $\text{X} = \text{Al, Be}$ ),<sup>31</sup>  $\text{Co}_2\text{MnX}$  ( $\text{X} = \text{Ge, Sn}$ ),<sup>32</sup>  $\text{Co}_2\text{ScX}$  ( $\text{X} = \text{As, Sb, Bi}$ ),<sup>33</sup>  $\text{Co}_2\text{CrX}$  ( $\text{X} = \text{Ga, Al}$ ),<sup>34</sup>  $\text{Co}_2\text{YAl}$  ( $\text{Y} = \text{Fe, Ti}$ ),<sup>35</sup>  $\text{Co}_2\text{ZrSi}$ ,<sup>36</sup>  $\text{Co}_2\text{YX}$  ( $\text{X} = \text{P, As, Sb, and Bi}$ ),<sup>37</sup> and  $\text{Co}_2\text{YX}$  ( $\text{X} = \text{P, As, Sb, Bi}$ )<sup>38</sup> have been documented in the literature for their exceptional spintronic properties, while experimental investigations have been conducted on  $\text{Co}_2\text{Mn}_x\text{Ti}_{1-x}\text{Si}$ ,  $\text{Co}_2\text{MnGa}_{1-x}\text{Ge}_x$ , and  $\text{Co}_2\text{TiZ}$  (where  $\text{Z} = \text{Sb, Sn, Ge, Si}$ ).<sup>39</sup> Together with their magnetic properties, Heusler alloys are also known for their excellent performance in optoelectronic applications. For instance, prominent optical characteristics were observed in  $\text{Ru}_2\text{CrAl}$ ,<sup>40</sup>  $\text{Na}_2\text{SrX}$  ( $\text{Si}$  and  $\text{Ge}$ ),<sup>41</sup>  $\text{CoFeXAs}$  ( $\text{X} = \text{Mn, Cr and V}$ ),<sup>42</sup> and  $\text{Co}_{2-x}\text{V}_x\text{FeGe}$ .<sup>43</sup> They are also well-suited for high-tech structural and functional uses because of their exceptional mechanical characteristics. Heusler alloys such as  $\text{Co}_2\text{YAl}$  ( $\text{Y} = \text{Fe, Ti}$ ),<sup>35</sup>  $\text{CrCoVSB}$ <sup>44</sup> and  $\text{Co}_2\text{TaZ}$  ( $\text{Z} = \text{Si, Sn}$ )<sup>45</sup> exhibit excellent mechanical characteristics. However, their physical properties are not well understood, despite their prospective applications in a variety of technology domains. Furthermore, the investigation of Co-based Heusler alloys, in particular  $\text{XVC}\text{O}_2$  ( $\text{X} = \text{B, P}$ ), is still unexplored. Thus, to provide fundamental insights, this study attempts to explore these aspects using first principles analysis. Gaining this understanding is essential for advancements in the creation and use of these innovative materials.

## 2. Computational analysis

For several years, researchers in the field of condensed matter physics have employed density functional theory to assess the electronic properties of atoms and molecules.<sup>46</sup> The codes based on DFT have received significant attention in the past few years given that the results compiled through this software provide an easy way to evaluate the physical characteristics of a material without consuming a lot of time. Density functional theory employs different functionals to explain the energy of a system in the form of electron density.<sup>47</sup> To evaluate the physical traits of the  $\text{XVC}\text{O}_2$  ( $\text{X} = \text{B, P}$ ) full-Heusler alloys, we employed the Wien2K algorithm, which is a DFT-based code. For the expansion of the wave function, the FP-LAPW approach<sup>48</sup> was employed, which is already built in the Wien2K code. In the muffin-tin region, the potential is variable, and in the interstitial region, the potential is constant, which are the two sections that the FP-LAPW approach separates the crystal structure into and the mathematical expressions are as follows:

$$V(r) = \begin{cases} \sum_{lm} V_{lm}(r) Y_{lm}(\theta, \phi) r R_{MT} & \\ \sum_k V_{kikr} r > R_{MT} & \end{cases} \quad (1)$$

The expansion of the wave function in the unit cell was achieved by using a linear combination of the plane waves in the interstitial

area and the spherical harmonics in the muffin-tin region. The GGA potential was used for the crystal relaxation, and the mBJ functional was used to evaluate the electrical and optical characteristics of  $\text{XVC}\text{O}_2$  ( $\text{X} = \text{B, P}$ ). The mBJ functional is as follows:

$$V_X^{\text{mBJ}}(r) = c V_X^{\text{BR}}(r) + (3c - 2) \frac{1}{\pi} \sqrt{\frac{5}{12}} \sqrt{\frac{2t(r)}{\rho(r)}} \quad (2)$$

where  $V_X^{\text{BR}}$  is the Becke Roussel potential and  $c$  is mathematically stated as:

$$c = \alpha + \beta \left( \frac{1}{V_{\text{cell}}} \int \frac{\nabla \rho(r)}{\rho(r)} \right)^{\frac{1}{2}} \quad (3)$$

where  $\alpha$  and  $\beta$  can be attuned according to our required calculations given that they are the free parameters in the Wien2K software. For accurate SCF calculations, several parameters were tuned such as the  $\text{RMT} \times K_{\text{max}} = 7$ ,  $l_{\text{max}} = 12$  and  $G_{\text{max}} = 14$  (a.u)<sup>-1</sup>. The muffin-tin radii for “B”, “P”, “V” and “Co” were tuned as 1.80, 1.85, 2.06 and 2.17 (a.u)<sup>-1</sup>, respectively. To avoid charge leakage via overlapping spheres, the cut-off energy was selected as -8 Ry. To ensure accuracy in the SCF calculations, a large mesh of 2000K points was selected together with the energy convergence of 0.0001 Ry. The crystal structures and the relevant structural data for these structures were obtained through VESTA.<sup>49</sup> The optical interactions of the materials were evaluated using the Kramers-Kronig complex equations.

## 3. Results and discussion

### 3.1 Structure and stability

An in-depth analysis of crystal structures is critical because it gives information on the symmetry, atom arrangement, chemical reactions, and optimal performance of materials. Knowing the structural properties of a material reveals important information regarding its use in various applications. Our studied alloys possess cubic symmetry with the space group of  $Fm\bar{3}m225$ . In this three-dimensional structure of  $\text{XVC}\text{O}_2$  ( $\text{X} = \text{B, P}$ ), each V atom is bonded to six equivalent “B” or “P” atoms and eight equivalent “Co” atoms, creating a body-centred cubic geometry. The atomic bond lengths were computed using the VESTA and observed to be 2.36 Å, 2.73 Å, and 2.73 Å for V-Co, V-B, and V-P, respectively. The crystal structures of  $\text{XVC}\text{O}_2$  ( $\text{X} = \text{B, P}$ ) are plotted in Fig. 1. To assess the ground-state energies for both Heusler alloys, their crystal structures were optimized. The volume optimization curves were plotted for the non-magnetic and ferromagnetic phases. The volume optimization curves for  $\text{BVC}\text{O}_2$  and  $\text{PVC}\text{O}_2$  revealed that these alloys are more stable in the FM phase. Fig. 1(b) and (d) demonstrate the volume optimization curves for both alloys, respectively. After volume optimization, the optimized parameters for both Heusler alloys were analysed using the Birch–Murnaghan equation, as follows:

$$E(V) = E_0 + \left[ \frac{VB}{B'(B' - 1)} \left( \frac{V_0}{V} \right)^{B'} + \frac{VB}{B'(B' - 1)} B \left( 1 - \frac{V_0}{V} \right) \right. \\ \left. - \frac{VB}{B'(B' - 1)} \right] \quad (4)$$



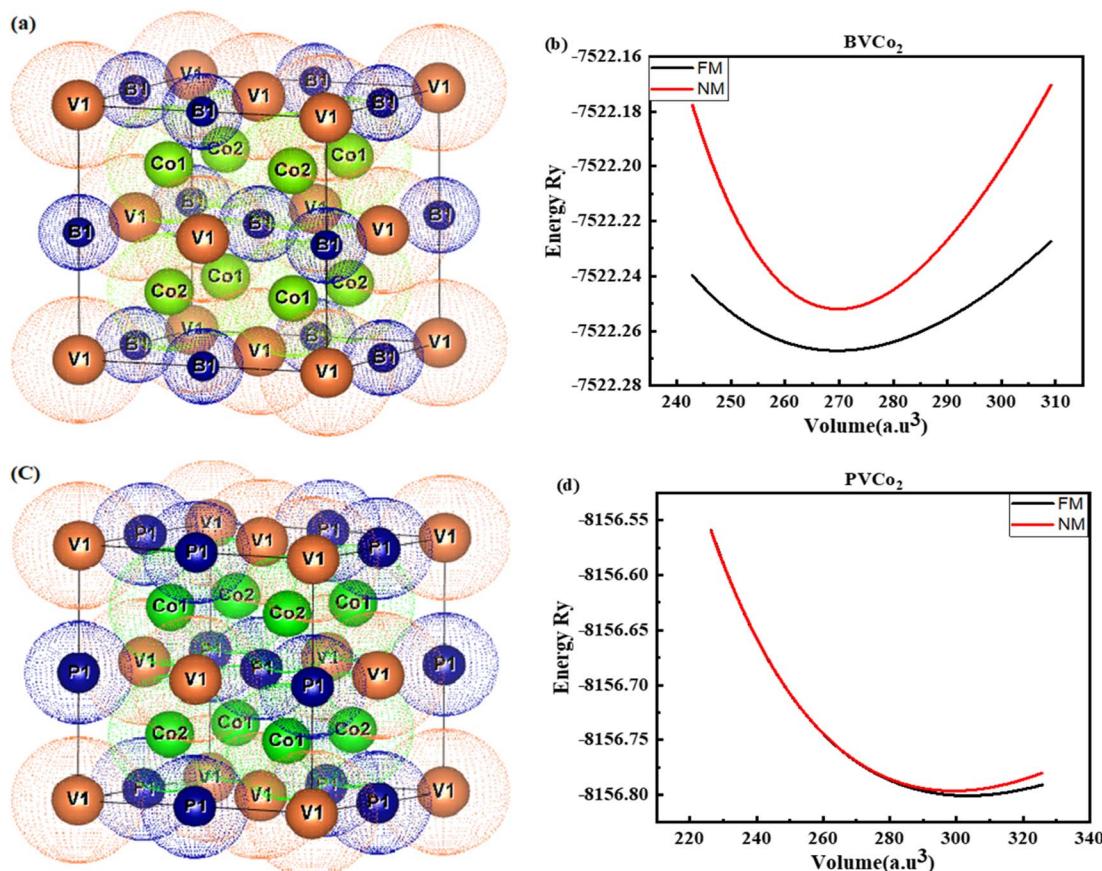


Fig. 1 (a and c) Unit cell structure and (b and d) volume optimization curves for  $\text{BVCu}_2$  and  $\text{PVCo}_2$ .

In the Birch–Murnaghan equation, the first term corresponds to the optimized ground-state energy, which is the minimum energy of the alloy at which it is stable, while the second term defines the compressional changes in the structure caused by variations in the volume and bulk modulus. The optimized bulk modulus values for both alloys depict that these alloys are very hard to compress. All the optimized lattice constants for  $\text{XVCu}_2$  ( $\text{X} = \text{B, P}$ ) are summarized in Table 1. After assessing the structural stability of both alloys, we assessed their thermodynamical stability by computing their respective formation energies. The formation energy of an alloy indicates the amount of energy that has been absorbed or released in its formation.<sup>50</sup> An alloy is considered stable if its formation energy is computed to be negative, whereas the formation energy is positive for an unstable alloy.<sup>51</sup> The formation energy for  $\text{XVCu}_2$  ( $\text{X} = \text{B, P}$ ) was calculated as follows:

$$E_F = E_{\text{total}} - (2E_{\text{Co}} + E_V + E_{\text{B/P}}) \quad (5)$$

Table 1 Optimized lattice parameters for  $\text{XVCu}_2$  ( $\text{X} = \text{B and P}$ )

Heusler alloy	$A^0$	$V_0$ (a.u <sup>3</sup> )	$B$ (GPa)	$B'$	$E_0$ (Ry)	$E_F$
$\text{BVCu}_2$	5.42	272.28	255.55	4.02	-7522.267	-2.73
$\text{PVCo}_2$	5.64	283.13	184.07	6.92	-8156.800	-2.79

where,  $E_{\text{total}}$  represents the ground-state energy for  $\text{XVCu}_2$  ( $\text{X} = \text{B, P}$ ) and  $E_{\text{Co}}$ ,  $E_V$  and  $E_{\text{B/P}}$  are the energies of the discrete atoms Co, V and B/P, respectively. The computed formation energy for  $\text{BVCu}_2$  is slightly lower than that of  $\text{PVCo}_2$ , which infers that it possesses slightly higher thermo-dynamical stability.

### 3.2 Elastic attributes

The ability of these two materials to endure external stress and revert to their original form was assessed based on their mechanical properties.<sup>52,53</sup> In the first principles calculations of a material, multiple methods can be employed to compute its elastic constant.<sup>54</sup> The method we employed to evaluate the elastic constants of  $\text{XVCu}_2$  ( $\text{X} = \text{B, P}$ ) is the Thomas Charpin method.<sup>55</sup> This technique includes applying slight strains to a crystal in a systematic manner and computing its subsequent stress responses to determine its elastic constants. Because the Heusler alloys under investigation have cubic symmetry, their mechanical properties could be adequately addressed using only three elastic constants ( $C_{11}$ ,  $C_{12}$ , and  $C_{44}$ ). It is critical that these elastic constants fully justify Born's stability criterion, which requires that all computed elastic constants should be greater than zero. If Born's stability criterion fails to be satisfied, then further mechanical traits of the desired compound cannot be assessed. The evaluated elastic constants and the related properties for  $\text{XVCu}_2$  ( $\text{X} = \text{B, P}$ ) are presented in Table 2. The  $C_{11}$



Table 2 Mechanical parameters of  $\text{BVC}_{\text{O}_2}$  and  $\text{PVC}_{\text{O}_2}$  alloys

Mechanical properties	$\text{BVC}_{\text{O}_2}$	$\text{PVC}_{\text{O}_2}$
$C_{11}$	340.33	389.2
$C_{12}$	239.09	230.1
$C_{44}$	142.022	110.34
(Bulk modulus) $B$	272.28	283.13
(Young's modulus) $Y$	252.85	260.6
(Shear modulus) $S$	93.96	96.7
(Anisotropy factor) $A$	2.80	1.38
(Pugh's ratio) $B/G$	2.90	2.92
(Poisson's ratio) $\nu$	0.33	0.34
(Cauchy pressure) $C_p$	97.06	119.76
(Hardness factor) $H_v$	10.77	10.37
(Machinability index) $\mu_m$	1.92	2.56
(Compressional waves) $v_t$ (m s $^{-1}$ )	6553.53	6677.58
(Transverse waves) $v_t$ (m s $^{-1}$ )	3183.79	3235.79
(Mean velocity) $v_m$ (m s $^{-1}$ )	3577.43	3636.37
(Melting temperature) $T_m$ (K)	2564.35	2853.17
(Debye temperature) $\theta_D$ (K)	575.21	561.87

and  $C_{12}$  elastic constants define the directional changes in the materials, whereas  $C_{44}$  defines the forces that cause deformity in their shape. The bulk modulus is the most important term in the assessment of mechanical qualities given that it defines the ability of a material to resist volumetric changes with an increase in the external pressure.<sup>56</sup> According to the computed results, it can be seen that  $\text{PVC}_{\text{O}_2}$  possesses a larger bulk modulus than  $\text{BVC}_{\text{O}_2}$ , which implies that  $\text{PVC}_{\text{O}_2}$  is more resistant to the volumetric changes caused *via* external stresses. The ability of a material to stretch or compress with the application of force is measured through its Young's modulus.<sup>57</sup> The attained results of Young's modulus imply that  $\text{PVC}_{\text{O}_2}$  is a rigid material in comparison  $\text{BVC}_{\text{O}_2}$  and is not easily stretched or compressed. The deformation caused in the shape of materials can be analysed through the shear modulus.<sup>58</sup>  $\text{PVC}_{\text{O}_2}$  offers a higher shear modulus value than  $\text{BVC}_{\text{O}_2}$ , which indicates that causing an irregularity in the shape of  $\text{PVC}_{\text{O}_2}$  is difficult compared to  $\text{BVC}_{\text{O}_2}$ . The anisotropy factor is computed to determine the directional dependency of the properties of a material. In the case of  $A = 1$  or  $A = 0$ , the attributes of a material are not affected by the change in direction, which is referred to as an isotropic material. Deviation of the anisotropy factor from zero or unity results in anisotropic behavior, implying that the properties of a material may vary depending on the direction.<sup>59</sup> The anisotropy value of both Heusler alloys implies anisotropic behaviour, as depicted by their anisotropy values. Brittle materials cannot tolerate tension and rapidly break, whereas ductile materials handle external stresses exceedingly well. The  $B/G$  ratio, referred to as "Pugh's ratio", determines how ductile or brittle a material is. An alloy or a compound is considered brittle if  $B/G < 1.75$ , otherwise it is ductile. A larger  $B/G$  ratio denotes a greater capacity to tolerate deformation, whereas a lower ratio implies a propensity for fracture.<sup>60</sup> Both  $\text{XVC}_{\text{O}_2}$  ( $X = \text{B}, \text{P}$ ) Heusler alloys showed  $B/G$  higher than 1.75, indicating that both alloys are ductile materials. Furthermore, Poisson's ratio can aid in determining if a material is brittle or ductile. According to Poisson's criteria,

material brittleness is defined as  $\nu < 0.26$ , and ductility is defined as  $\nu > 0.26$ .<sup>61</sup> The evaluated results of Poisson's ratio depicts that both alloys are ductile. The type of bonding between the atoms of a material can be judged by the Cauchy pressure. In the case of ionic bonding, the Cauchy pressure is evaluated to be positive, whereas for covalent bonding, the  $C_p$  value is negative.<sup>60</sup> The reported Cauchy pressure values for both alloys revealed ionic bonding between their atoms. The hardness factor reflects the capacity of a material to withstand indentation and scratches. Higher hardness factor values indicate that a material is more resistant to scratching, whereas lower values indicate that it can be easily deformed.<sup>62</sup> The computed hardness factor values for both studied alloys revealed their higher resistance to scratching. The ratio of the bulk modulus to shear deformation of a material, or machinability index, illustrates how easy or workable it is.<sup>63</sup> Lower values of the machinability index show the difficulty in handling a material, whereas higher values imply that it is easy to handle. Both alloys revealed lower machinability index values. In the case of both Heusler alloys, we also evaluated elastic sound waves using their mechanical properties. Waves in a material can propagate in two different ways, *i.e.*, transverse waves and compressional waves. Transverse waves move through materials perpendicularly, whereas compressional waves move parallel across the medium. In the case of both studied Heusler alloys, it is noticeable that the compressional waves were dominant compared to transverse waves. Furthermore, the mean velocities for  $\text{XVC}_{\text{O}_2}$  ( $X = \text{B}, \text{P}$ ) were also computed and mathematically stated as follows:

$$v_m = \left[ \frac{1}{3} \left( \frac{2}{v_t^3} + \frac{1}{v_l^3} \right) \right]^{-\frac{1}{3}} \quad (6)$$

The mean velocity defines the average speed at which a wave passes through a material. It provides significant information regarding the ability of a material to stretch, compress and revert to its original state. The temperature at which a material melts is referred to as the melting temperature.<sup>64</sup> A material with stronger bonding between its atoms or molecules will have a greater melting temperature given that more heat energy is required to dissolve these tight connections, enabling the material to change from solid to liquid form. The calculated results of the melting temperature for  $\text{XVC}_{\text{O}_2}$  ( $X = \text{B}, \text{P}$ ) imply the strong bonding of their atoms with each other. The Debye temperature is an extremely important term in the field of solid-state physics given that it provides detailed insight about the specific heat, stiffness, thermal conductivity and phonons of materials<sup>65</sup> and is computed as follows:

$$\theta_D = \frac{h}{k_B} \left[ \frac{3n}{4\pi} \left( \frac{N_A \rho}{M} \right) \right]^{\frac{1}{3}} v_m \quad (7)$$

According to the Debye temperature results for  $\text{XVC}_{\text{O}_2}$  ( $X = \text{B}, \text{P}$ ), the specific heat capacity of these alloys will change very slowly below this temperature.



### 3.3 Electro-magnetic properties

The nature of a material and its uses in the field of optoelectronic devices can be assessed by its electronic properties. Magnetic materials, which behave like a conductor in one spin channel and insulator or a semiconductor in the other spin channel, are termed half-metallic materials.<sup>66</sup> These half-metallic materials show significant potential in spintronic-related applications. The electronic properties of  $XVC_{2}$  ( $X = B, P$ ) such as band structure, TDOS and PDOS were computed using the mBJ approximation. The band structure profiles for  $XVC_{2}$  ( $X = B, P$ ) were analyzed for high symmetry point (W-L- $\Gamma$ -X-W-K) in the first Brillouin zone. The Fermi line, which separates the conduction and valence band, is represented by  $E_F$ . Fig. 2(a) shows the band structure profile of  $BVC_{2}$  for the spin-up channel and it is clearly seen that the dispersion curves in its conduction band overlap with the dispersion curves present in its valence band, revealing its metallic behavior. Fig. 2(b) shows the plot of the band structure of the spin-down channel for  $BVC_{2}$ . In the spin-down channel, a visible gap was observed in both intermediate bands with an indirect bandgap of 0.38 eV. In the case of  $PVC_{2}$ , metallic behavior was observed in the spin-up channel, as shown in Fig. 2(c), while a direct bandgap of 1.73 eV was observed in the spin-down state, as presented in Fig. 2(d). In the case of both studied alloys, half metallic behavior was observed, which implies that these alloys are

perfect for efficiently generating and controlling the spin polarized currents.

On the contrary, we also obtained the TDOS plots for  $XVC_{2}$  ( $X = B, P$ ) in the energy range of -6 eV to 6 eV, as presented in Fig. 3. The total density of states corresponds to the different energy levels that electrons can occupy. Fig. 3(a) illustrates the TDOS plot of  $BVC_{2}$  for both spin states. The TDOS plot in the spin-up channel indicates 100% polarization at the Fermi level, while a clear bandgap is noticed in the spin-down channel. In the case of the  $PVC_{2}$  alloy, a bandgap in the spin-down channel was observed, while metallic character was observed in the spin-up state. Together with TDOS, we also assessed the PDOS for  $XVC_{2}$  ( $X = B, P$ ), as displayed in Fig. 4. It was observed that for  $BVC_{2}$ , the B-p state showed the highest involvement in the conduction band with small contributions from the V-d and Co-d states in both spin channels, while V-d and Co-d showed the highest contribution in the valence band, as presented in Fig. 4(a). In the case of  $PVC_{2}$ , the P-p and Co-d states show the highest contribution in the conduction band with the minor contribution of the V-d state in both spin channels. In the conduction band, V-d and Co-d states prominently contribute, with a small contribution from the P-p state, as depicted in Fig. 4(b).

The response of a material when it interacts with an external magnetic field is analysed by its magnetic traits. The magnetic moments for  $XVC_{2}$  ( $X = B, P$ ) are listed in Table 3. In the case of

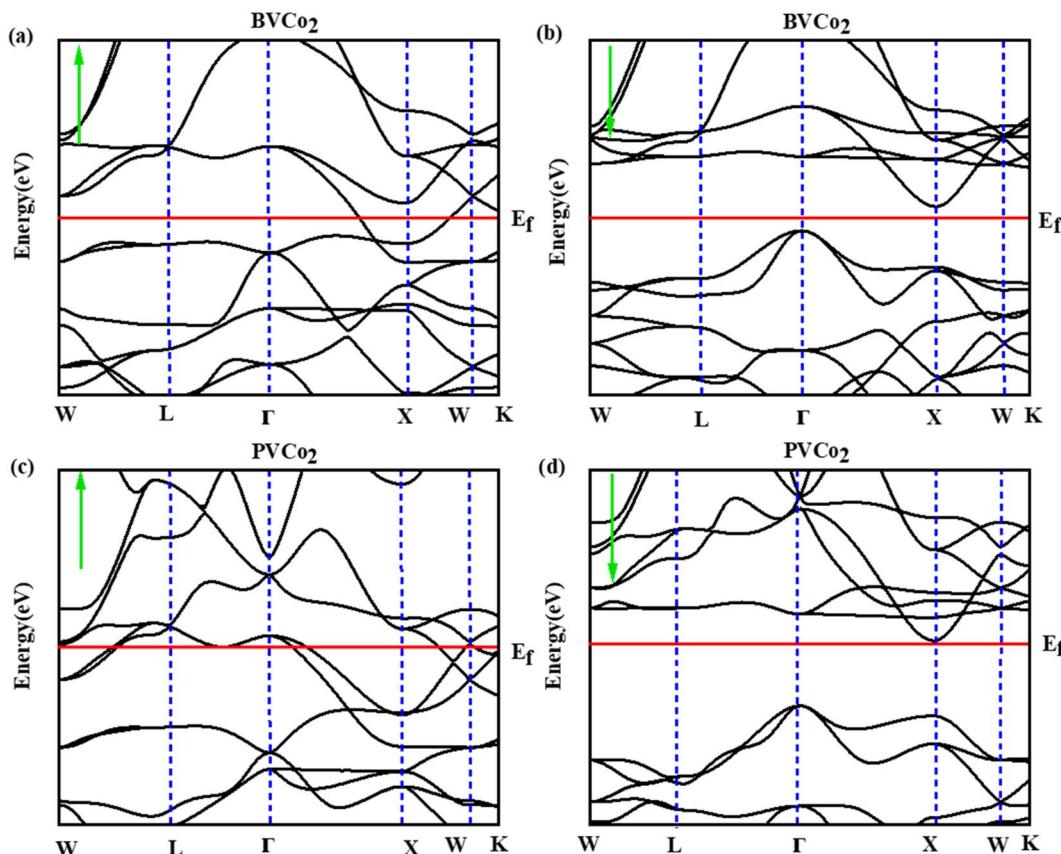
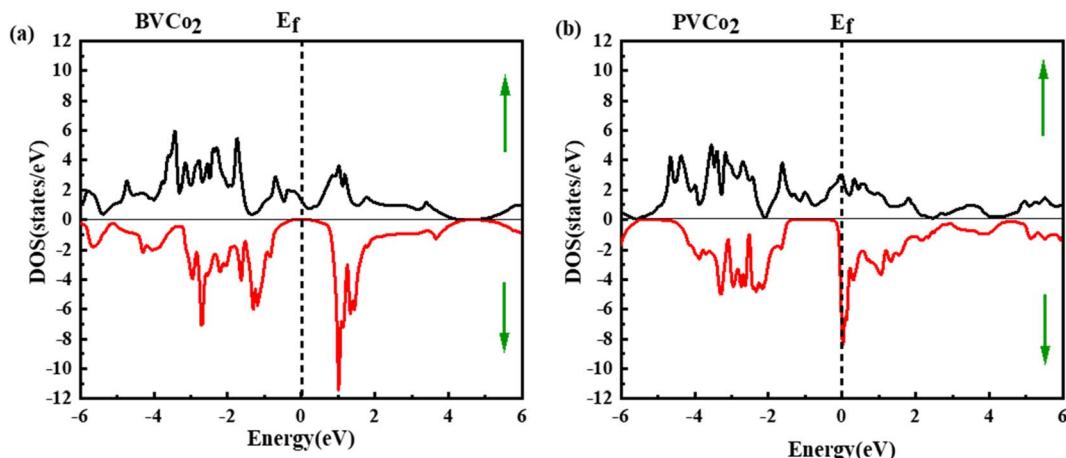
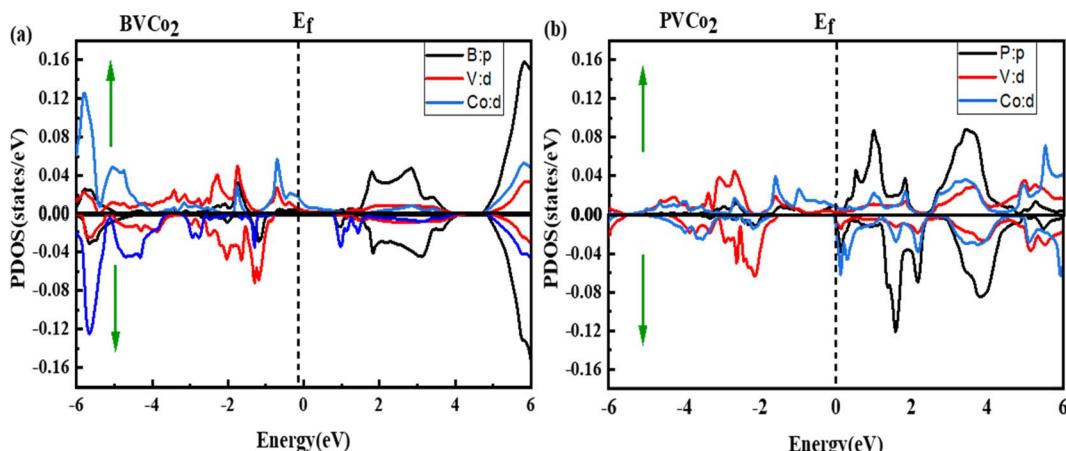


Fig. 2 Band structure profiles for  $BVC_{2}$  (a and b) and  $PVC_{2}$  (c and d).



Fig. 3 Total DOS for (a)  $\text{BVCO}_2$  and (b)  $\text{PVCO}_2$ .Fig. 4 Partial density of states for (a)  $\text{BVCO}_2$  and (b)  $\text{PVCO}_2$ .

the  $\text{BVCO}_2$  alloy, the major contribution was observed from its “Co” atom, whereas the contributions from the “B” and “V” atoms are extremely low. The magnetic moment in the interstitial region for  $\text{BVCO}_2$  is negative, which implies that the direction of the magnetic moment is opposite to the external magnetic field, and thus the collective magnetic moment for  $\text{BVCO}_2$  was computed as  $2\mu_B$ . In the case of the  $\text{PVCO}_2$  alloy, the major contribution was noticed from the “V” and “Co” atoms, while a very small contribution is noticed from the “P” atom. The total magnetic moment for  $\text{PVCO}_2$  was computed as  $2.81\mu_B$ .

Table 3 Calculated partial and total magnetic moments for  $\text{BVCO}_2$  and  $\text{PVCO}_2$ 

Alloys	Magnetic moment ( $\mu_B$ )					
	B	P	V	Co	Interstitial	Total
$\text{BVCO}_2$	0.0251	—	0.050	1.029	-0.134	2.00
$\text{PVCO}_2$	—	0.049	0.795	0.957	0.056	2.81

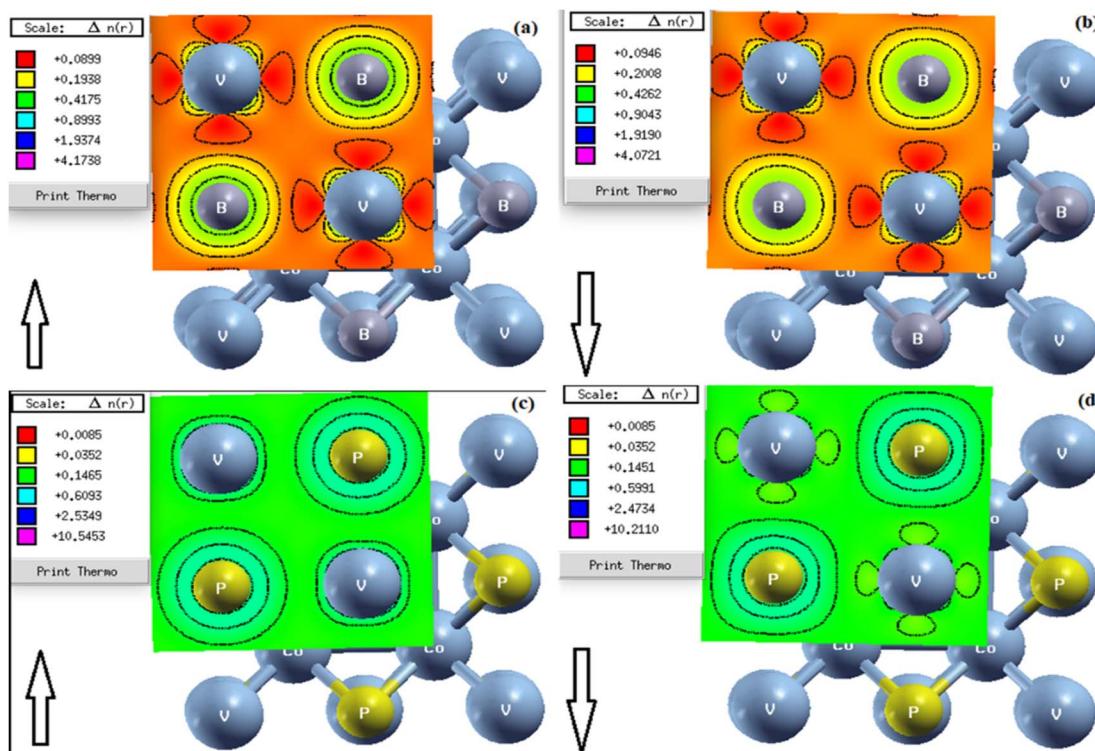
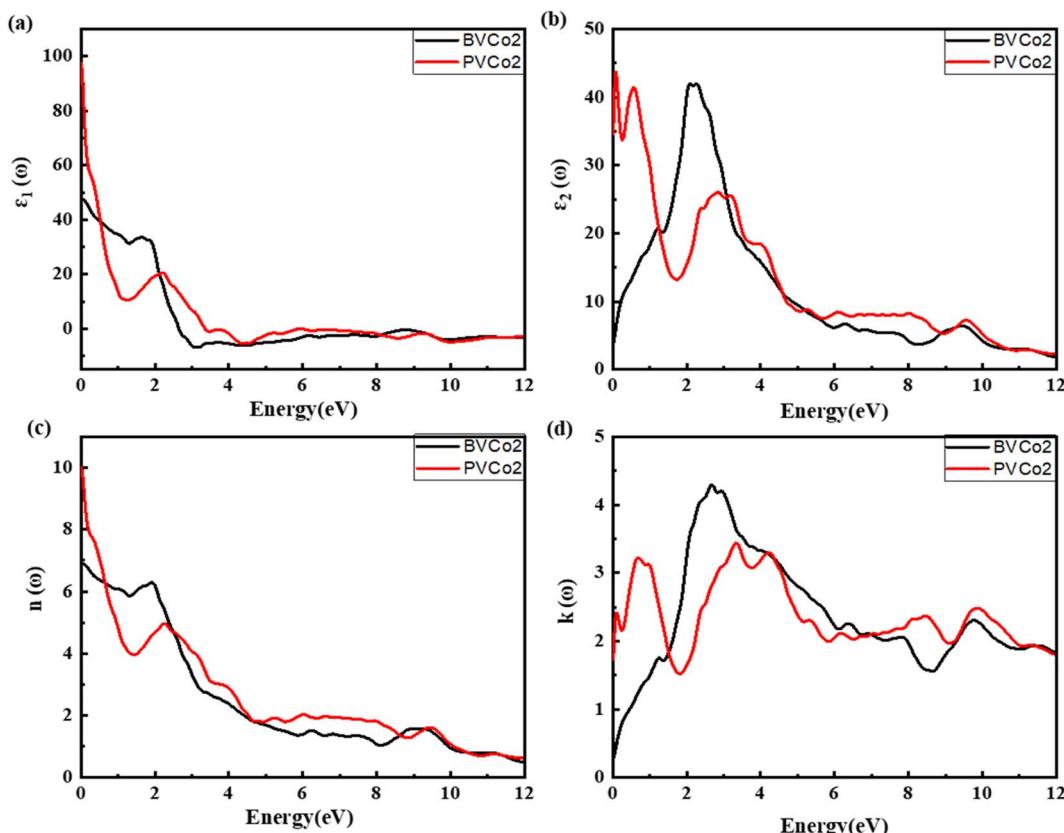
### 3.4 Bonding nature

The atomic bonding of the studied  $\text{BVCO}_2$  and  $\text{PVCO}_2$  alloys for both spin channels is presented in Fig. 5. Their bonding nature was analysed for the [110] plane. The yellow and red regions indicate an increase in the electron density, while the blue and green regions imply a lower electron density. In the case of  $\text{BVCO}_2$ , covalent bonding was observed in the V and B atoms in both spin channels, while for  $\text{PVCO}_2$ , ionic bonding was observed in the P and V atoms in the spin up channel and covalent bonding was noticed between the P and V atoms in the spin down channel.

### 3.5 Optical attributes

The optical traits of bulk materials can be analysed when they interact with external electromagnetic waves. This interaction results in a few important optical characteristics that make it simple to assess the potential of a material for use in the field of optoelectronics. The optical properties of the  $\text{BVCO}_2$  and  $\text{PVCO}_2$  alloys were examined through a set of complex equations known as the Kramers–Kronig equations. These equations are divided into two segments, real and imaginary parts, as follows:



Fig. 5 Contour plots for (a and b)  $\text{BVCo}_2$  and (c and d)  $\text{PVCo}_2$ .Fig. 6 (a) Real and (b) imaginary parts, (c) refractive index and (d) extinction coefficient for  $\text{BVCo}_2$  and  $\text{PVCo}_2$ .

$$\varepsilon_1(\omega) = 1 + \frac{2p}{\pi} \int_0^\infty \frac{\omega' \varepsilon_2(\omega')}{\omega'^2 - \omega^2} d\omega' \quad (8)$$

The real part elaborates the ability of a material to disperse or polarize incident light.<sup>67</sup> The “P” in the mathematical expression of the real part is Cauchy’s principle value. On the contrary, the imaginary part provides detailed information regarding the absorption and scattering power of a material,<sup>68</sup> as follows:

$$\varepsilon_2(\omega) = \frac{h' e^2}{\pi \omega^2 m^2} \sum_{v,c} \int_{BZ} \left[ M_{cv}(k) \right]^2 \delta[\omega_{cv}(k) - \omega] d^3k \quad (9)$$

where  $M_{cv}$  is the dipole matrix. The optical characteristics of the BVC<sub>0.2</sub> and PVC<sub>0.2</sub> alloys were analysed in the energy range of 0 to 12 eV, and their real part is drawn in Fig. 6(a). In both alloys, a declining trend was observed with an increase in the incident energy. The static value for BVC<sub>0.2</sub> was observed to be 47.5, which gradually declined, and then increased to the peak at 1.89 eV in the visible region. After this peak value, a sharp decline was observed, which was followed by a linear trend as the energy increased. In the case of PVC<sub>0.2</sub>, the static value was noticed as 97.25, which then declined drastically and the peak was observed at 2.24 eV. With an increase in the photon energy, the real part of PVC<sub>0.2</sub> showed a linear trend. In the case of both alloys, the maximum polarization was noticed in the visible region. Fig. 6(b) shows the plot of the imaginary component of

the dielectric function for both the PVC<sub>0.2</sub> and BVC<sub>0.2</sub> alloys. In the case of BVC<sub>0.2</sub>, the maximum scattering and absorption were observed in the visible region at 2.24 eV, which gradually declined when the energy increased, and another noticeable peak at 9.42 eV was detected in the UV region. The graphical pattern of the imaginary part for PVC<sub>0.2</sub> showed the maximum value at 0.095 eV, followed by another peak at 0.55 eV, which declined in the visible region and prominent peaks appeared at 2.87 eV and 9.61 eV. The bending of light when it passes through a material is determined through the refractive index, as represented in Fig. 6(c) for PVC<sub>0.2</sub> and BVC<sub>0.2</sub>. In the case of BVC<sub>0.2</sub>, the static refractive index was observed to be 6.90, which showed a sharp decline, and a peak at 1.94 eV was noticed in the visible region. Several smaller peaks appeared as the photon energy increased and a minor peak in the UV region was observed at 9.12 eV. The refractive index for PVC<sub>0.2</sub> has a static value of 10.01, which shows a drop. A peak was observed in the visible region at 1.94 eV, and another notable peak was detected in the UV region at 9.51 eV. The extinction coefficient, which is illustrated in Fig. 6(d), indicates how strongly a material absorbs light or other electromagnetic radiation at a given wavelength. The maximum extinction coefficient peak for BVC<sub>0.2</sub> was found to be in the visible region at 2.68 eV. After this peak value, the extinction coefficient displayed a decreasing behavior with an increase in the photon energy and another minor peak was observed at 9.80 eV. In the case of PVC<sub>0.2</sub>, significant extinction coefficient peaks were observed

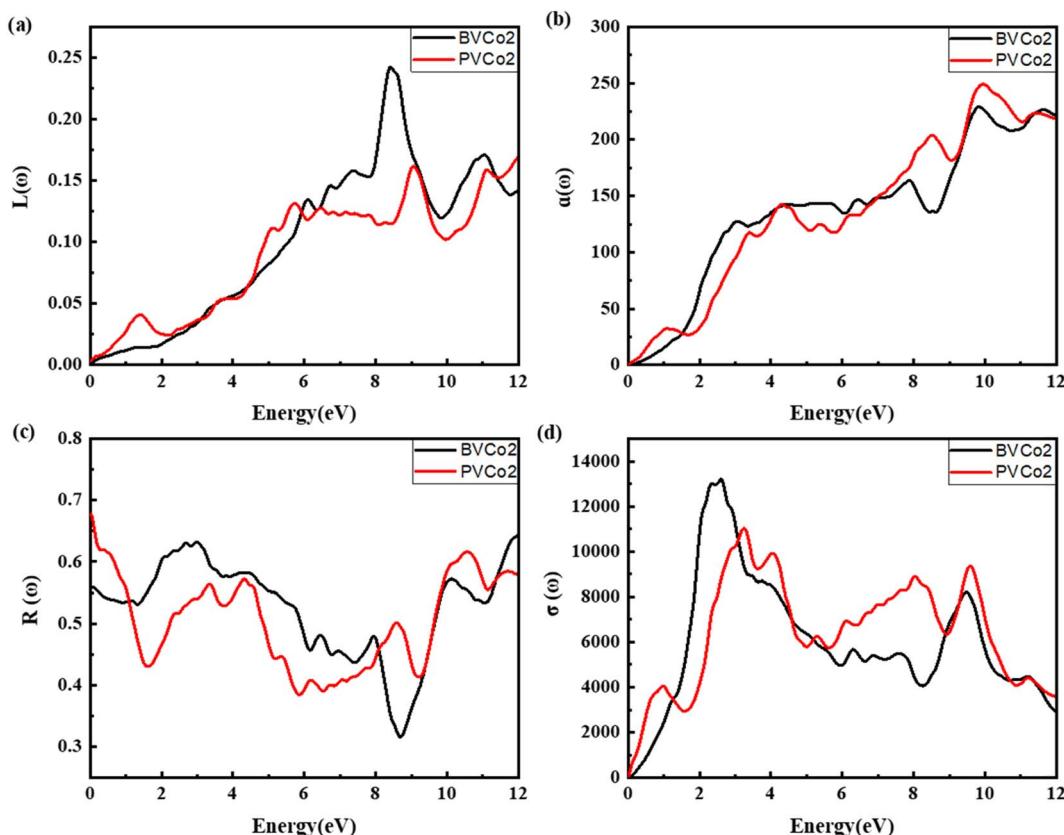


Fig. 7 (a) Energy loss, (b) absorption coefficient, (c) reflectivity and (d) optical conductivity of BVC<sub>0.2</sub> and PVC<sub>0.2</sub>.



throughout the electromagnetic spectrum at 0.74 eV, 4.25 eV, 8.53 eV, and 9.80 eV with the maximum peak at 3.31 eV. In the case of  $\text{BVC}\text{O}_2$ , its extinction coefficient reveals the strong absorption of light in the visible spectrum, whereas for  $\text{PVC}\text{O}_2$ , the highest absorption occurs in the UV region.

The energy loss for  $\text{PVC}\text{O}_2$  and  $\text{BVC}\text{O}_2$  is represented in Fig. 7(a), which corresponds to the amount of energy that is lost when electrons interact with a material. In the case of  $\text{BVC}\text{O}_2$ , the important energy loss peaks were seen at 6.13 eV and 11.06 eV and the maximum energy loss peak was noticed at 8.42 eV. In the case of  $\text{PVC}\text{O}_2$ , a minor energy loss peak was noticed at 1.40 eV. With an increase in energy, some major peaks appeared and the highest peak was detected at 9.07 eV. The absorption spectra of  $\text{PVC}\text{O}_2$  and  $\text{BVC}\text{O}_2$  are presented in Fig. 7(b), which provide information regarding their ability to absorb incident light when they interact with electromagnetic waves. The minor absorption peak for  $\text{BVC}\text{O}_2$  was noticed at 3.03 eV, while with an increase in energy, another peak at 7.85 eV emerged, and the maximum absorption was noticed in the UV region at 9.83 eV. In the case of  $\text{PVC}\text{O}_2$ , peaks were visible at 1.12 eV, 4.34 eV, and 8.55 eV, and the highest absorption was noticed at 9.94 eV. Optical reflectivity is another crucial optical characteristic to assess given that it reveals the amount of light that is reflected or transmitted into a given material. The optical reflectivity of  $\text{PVC}\text{O}_2$  and  $\text{BVC}\text{O}_2$  is displayed in Fig. 7(c). The  $R(0)$  for  $\text{BVC}\text{O}_2$  was observed at 0.55, and with an increase in energy, several prominent peaks appeared at 3.38 eV, 4.36 eV, and 8.61 eV, and the maximum reflectivity was observed at 10.57 eV. In the case of  $\text{PVC}\text{O}_2$ , the static value of the optical reflectivity was noticed at 0.67, which gradually declined in the visible region, and then increased to the peak at 3.00 eV. More prominent peaks appeared for  $\text{PVC}\text{O}_2$  at 7.95 eV and 10.08 eV with an increase in energy, while the maximum peak was seen at 11.95 eV. It can be concluded from the optical reflectivity plot for both alloys that these materials become highly reflective in the UV region, indicating that more light is reflected, and then transmitted. The optical conductivity for  $\text{PVC}\text{O}_2$  and  $\text{BVC}\text{O}_2$  is reported in Fig. 7(d), which corresponds to the quantity of electrons becoming conductive when they absorb the incident light. The maximum optical conductivity peaks for  $\text{PVC}\text{O}_2$  and  $\text{BVC}\text{O}_2$  were noticed at 3.25 eV and 2.65 eV, respectively, indicating that for  $\text{PVC}\text{O}_2$ , the electrons become extremely conductive in the UV spectrum, whereas for  $\text{BVC}\text{O}_2$ , they become extremely conductive in the visible region.

## 4. Conclusions

The half-metallic behavior of Heusler alloys has attracted significant attention in recent decades given that these materials have demonstrated an excellent output for magnetic shape memory devices. In this study, using the mBJ functional and FP-LAPW approach, the physical characteristics of  $\text{PVC}\text{O}_2$  and  $\text{BVC}\text{O}_2$  were determined. The volume optimization curves, ground-state energies and negative formation energies for both alloys revealed that they are completely stable in non-magnetic and magnetic phases. Also, their computed elastic constants and mechanical properties completely satisfy the mechanical

stability criteria. The elastic properties of both alloys indicate that they are ductile and require a higher melting temperature for phase transitioning. The electronic properties revealed half-metallic behavior for both alloys, which is extremely desirable in spintronic applications. Also, high polarization and dispersion in the visible and UV spectrum were observed for  $\text{BVC}\text{O}_2$  and  $\text{PVC}\text{O}_2$ . Thus, the optical traits of these materials revealed that they are suitable for application in optoelectronic and spintronic devices.

## Data availability

Data will be available upon request.

## Conflicts of interest

The authors have no competing conflict of interest.

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