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# Advancements in MAX phase materials: structure, properties, and novel applications

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The MAX phase represents a diverse class of nanolaminate materials with intriguing properties that have received incredible global research attention because they bridge the divide separating metals and ceramics. Despite the numerous potential applications of MAX phases, their complex structure leads to a scarcity of readily accessible pure MAX phases. As a result, in-depth research on synthesis methods, characteristics, and structure is frequently needed for appropriate application. This review provides a comprehensive understanding of the recent advancements and growth in MAX phases, focusing on their complex crystal structures, unique mechanical, thermal, electrical, crack healing, corrosion-resistant properties, as well as their synthesis methods and applications. The structure of MAX phases including single metal MAX, i-MAX and o-MAX was discussed. Moreover, recent advancements in understanding MAX phase behaviour under extreme conditions and their potential novel applications across various fields, including high-temperature coatings, energy storage, and electrical and thermal conductors, biomedical, nanocomposites, etc. were discussed. Moreover, the synthesis techniques, ranging from bottom-up to top-down methods are scrutinized for their efficacy in tailoring MAX phase properties. Furthermore, the review explores the challenges and opportunities associated with optimizing MAX phase materials for specific applications, such as enhancing their oxidation resistance, tuning their mechanical properties, and exploring their functionality in emerging technologies. Overall, this review aims to provide researchers and engineers with a comprehensive understanding of MAX phase materials and inspire further exploration into their versatile applications in materials science and engineering.

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## 1. Introduction

In the ever-evolving landscape of material science and engineering, a class of compounds has captured the imagination of scientist's worldwide, propelling research into uncharted territories. Among these compounds, MAX phases have emerged as a captivating category, drawing the attention and concentration of researchers across the globe. MAX phases represent an intriguing group of materials, serving as a link between ceramics and metals, boasting a distinctive blend of characteristics that render them as prospective options for diverse applications.<sup>1–5</sup> MAX phases have emerged as a fascinating and versatile family of materials, renowned for their exceptional combination of properties, thus rendering them a subject of extensive research and exploration. This intriguing class of materials has traversed a dynamic trajectory, experiencing both

peaks and troughs in its relatively short history, marked by shifts in nomenclature and periods of relative obscurity. Notably, MXenes, advanced materials with superior efficacy in numerous applications, are derived from MAX phases as precursors. Consequently, the precise synthesis and characterization of MAX phases become crucial processes for producing high-quality MXenes.

The foundational work in the early 1960s, spearheaded by Wolfgang Jeitschko and Hans Nowotny in Vienna, Austria, stands as a pivotal chapter in the MAX phase's saga. Their groundbreaking efforts resulted in the discovery of over 100 new carbides and nitrides,<sup>5,6</sup> including a novel class of ternary systems characterized by a composition involving a transition metal (M), a metalloid (Me), and carbon (C). Among these, the "Hagg phases" or H-phases, named for their hexagonal crystal structure, reminiscent of the carbon-stabilized  $\beta$ -manganese phase seen in  $\text{Mo}_3\text{Al}_2\text{C}$ , garnered significant attention. The compositions within this classification, such as the system of Ti–Al–C, V–Al–C, Nb–Al–C, Cr–Al–C, Ti–Sn–C, and V–Ga–C, opened new avenues for exploration.<sup>7</sup> Despite these early breakthroughs, the H-phases experienced a period of relative neglect in subsequent decades. The earliest instances,  $\text{Ti}_2\text{SC}$

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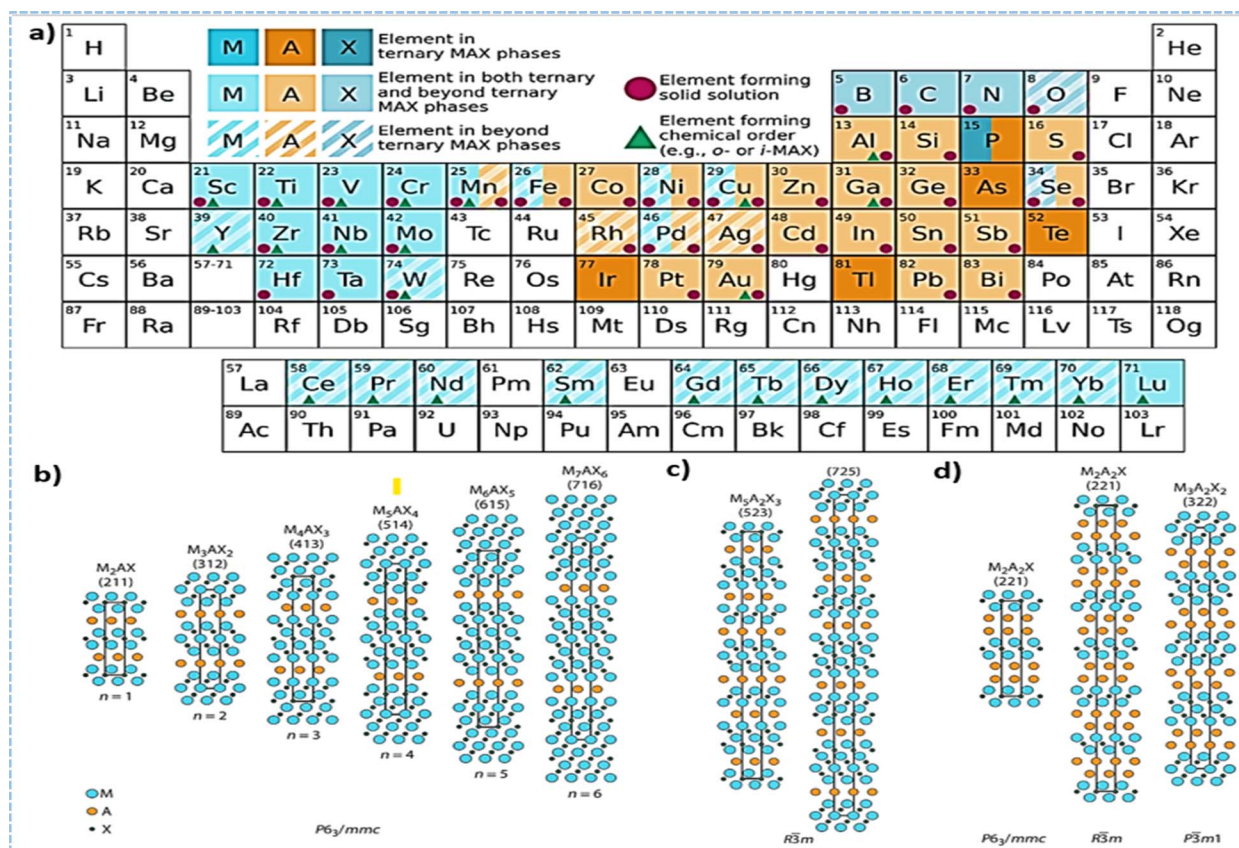


and  $\text{Zr}_2\text{SC}$ , were documented in 1960 by Helga Rohde and Hans Kudielka.<sup>8</sup> This family expanded with discoveries like  $\text{Ti}_3\text{SiC}_2$  and  $\text{Ti}_3\text{GeC}_2$ , leading to the formulation  $\text{M}_{n+1}\text{AX}_n$ , where  $n$  could equal 1 or 2.<sup>9,10</sup> Schuster, a protege of Nowotny, uncovered  $\text{Ti}_3\text{AlC}_2$  in 1994.<sup>11</sup>

In 1988, The IUPAC, which stands for the International Union of Pure and Applied Chemistry took action to clarify the organization of the periodic table, providing a numbering system for the columns that would eliminate previous ambiguities. This universal standard simplified scientific discussions and helped students navigate the elements and their characteristics without the inconsistency of earlier labeling conventions. As time progressed, MAX phases underwent significant changes with more compositions being both predicted and synthesized. This contributed to the development of a wide array of materials that could be categorized under the general formula  $\text{M}_{n+1}\text{AX}_n$  and advanced the use of the  $\text{M}_{n+1}\text{AX}_n$  notation used to describe their chemical composition shown in Fig. 1a. In this formula, "M" stands for a transition metal, "A" represents an A-group element (primarily IIIA or IVA), "X" encompasses C and/or N, and " $n$ " can vary from 1 to 3. This nomenclature, later simplified to "MAX," has since become synonymous with this group of materials. Examples of popular

MAX phases include  $\text{Ti}_3\text{SiC}_2$ ,  $\text{Ti}_3\text{AlC}_2$ ,  $\text{Ti}_2\text{AlC}$ ,  $\text{V}_2\text{AlC}$ ,  $\text{Ti}_2\text{AlN}$ , etc., each possessing a distinct combination of attributes that make them suitable for a wide array of applications.<sup>12–15</sup> The  $\text{M}_2\text{AX}$ ,  $\text{M}_3\text{AX}_2$ , and  $\text{M}_4\text{AX}_3$  phases are commonly denoted as 211, 312, and 413 phases, respectively, reflecting the value of " $n$ ". The key distinction among these phases lies in the count of M layers sandwiched between the A layers. In the crystal lattice of MAX phases, M atoms are densely arranged, while X atoms occupy octahedral sites, resulting in  $\text{M}_{n+1}\text{AX}_n$  layers that display ceramic characteristics. These layers are interspersed with A layers that possess metallic properties. Consequently, MAX phases seamlessly integrate the advantageous characteristics of both ceramics and metallic materials. Similar to metals, they demonstrate efficient thermal and electrical conductivity, can be easily machined using conventional tools, and exhibit resilience against thermal shocks. On the other hand, akin to ceramics, MAX phases showcase remarkable strength, excellent high-temperature resilience, and thermal stability.

Barsoum's influential research, notably his groundbreaking work in 1996, drew considerable focus to MAX phases, initiating a deeper investigation into their characteristics. Subsequently, there has been notable enthusiasm surrounding this material due to its unique blend of physical properties. The resurgence



**Fig. 1** (a) The periodic table displays M-elements highlighted in blue, A-elements in orange, and X-elements in grey. In ternary MAX phases, the shading is intensified, whereas in those present in both ternary and post-ternary phases, the shading is lighter. Elements contributing to solid solutions or chemical order at M-, A-, or X-sites are represented by purple circles or dark blue triangles, respectively. (b) Conventional MAX phases possessing a general  $\text{M}_{n+1}\text{AX}_n$  configuration crystallize within the  $P6_3/mmc$  symmetry group. (c) Intergrown MAX phases, exhibiting alternating  $\text{M}_{n+1}\text{X}_n$  layer thicknesses, crystallize in the  $R\bar{3}m$  space group. (d) Phases featuring dual A-layers can crystallize in one of three space groups:  $P6_3/mmc$ ,  $R\bar{3}m$ , or  $P\bar{3}m1$ . (Reproduced from ref. 11 with permission from Elsevier, copyright 2023).<sup>11</sup>

of interest in this family of materials transpired in 1996 with the publication of “Synthesis and characterization of a remarkable ceramic:  $\text{Ti}_3\text{SiC}_2$ ” by Michel W. Barsoum and collaborators. Barsoum and colleagues accomplished the synthesis of predominantly single-phase  $\text{Ti}_3\text{SiC}_2$  by reactive hot-pressing  $\text{TiSi}_2$ ,  $\text{SiC}$ , and graphite powders, resulting in fully dense material.<sup>13,14</sup> This work not only highlighted the material's distinct blend of ceramic and metallic characteristics but also acted as a catalyst for renewed attention towards the H-phases. The practical creation of compounds within the 211 phases and 312 phases, such as  $\text{Ti}_2\text{AlC}$  and  $\text{Ti}_3\text{SiC}_2$ , marked a turning point in MAX phases research.

In 2000, M. W. Barsoum's review article titled “MAX phases on new ternary transition metal carbide or nitride materials” provided a comprehensive overview. Describing MAX phases as possessing elastic rigidity, excellent thermal and electrical conductivity, lightweight, thermal shock-resistant, machinable, and resistant to oxidation, the review marked a milestone in the understanding and appreciation of these materials.<sup>5,16–19</sup>

Currently, a comprehensive inventory reveals the existence of 155 unique compositions, and this number is consistently expanding. It is crucial to emphasize that not all potential combinations display thermodynamic stability. By 2019, Sokol *et al.* cataloged 155 MAX phases,<sup>15</sup> a figure that has since more than doubled within a brief span, reaching a current count of 342 distinct compositions, with ongoing discoveries fueling continuous expansion.<sup>11</sup> For example, within the Ti–Al–C system,  $\text{Ti}_2\text{AlC}$  and  $\text{Ti}_3\text{AlC}_2$  demonstrate stability over a wide temperature range. In contrast, systems like  $\text{Cr}_2\text{AlC}$  and  $\text{Ti}_3\text{SiC}_2$  only maintain stability with a single phase such as Cr–Al–C and Ti–Si–C. The absence of a standardized definition for formulations of solid solutions that are thermodynamically stable, coupled with limited insights into maximal solubility within each system, presents significant challenges due to the multitude of potential permutations involved.<sup>20,21</sup>

Crucially, all MAX phases exhibit a hexagonal crystal lattice (space group  $P6_3/mmc$ ), comprising layers of  $\text{M}_6\text{X}$ -octahedra interconnected by shared edges, alongside layers of “A” elements positioned at the center of trigonal prisms. The M–X bonds exhibit strength due to their combined metallic-covalent character, contrasting with the relatively weaker M–A bonds. This distinctive crystal lattice, along with MAX phases' elements' position on the periodic table, contributes to their characteristic layered arrangement and imparts them with a distinctive blend of characteristics that bridge the traditional gap between ceramics and metals.

Prior to delving deeper, it is essential to precisely define the term “MAX phase”. This is a task that has proven to be more complex than initially anticipated due to the existence of numerous layered compounds with three or four components featuring transition metals, A-group elements, and X atoms, as delineated in our set parameters. A fundamental representation of a MAX phase is a layered, hexagonal, nanolaminate compound adhering to  $\text{M}_{n+1}\text{AX}_n$  chemistry, where alternating layers of  $\text{M}_{n+1}\text{AX}_n$  and layers solely comprised of the A-group element are present. A visual depiction of this crystalline structure is presented in Fig. 1a. Though it is generally accepted

that many traditional MAX phases are inherently machinable, it is still under debate whether this characteristic can be uniformly applied to all the MAX phases that have been reported thus far. Another family of compounds, the MAB phases, also warrants mention as they bear some similarities to MAX phases. MAB phases, too, are comprised of layered borides with transition metals (M), A-group elements (A), and boron (B). Yet, the most notable difference between MAX and MAB phases lies in their structural differences. While MAX phases strictly maintain the hexagonal  $P6_3/mmc$  structure, MAB phases demonstrate a much broader spectrum of both structural and compositional variations. These include orthorhombic ( $\text{M}_2\text{AB}_2$ ,  $\text{M}_3\text{AB}_4$ ,  $\text{M}_4\text{AB}_6$ ,  $\text{M}_4\text{AB}_4$ ,  $\text{M}_2\text{A}_2\text{B}_2$ ),<sup>22–25</sup> tetragonal ( $\text{M}_5\text{AB}_2$ ),<sup>26</sup> and hexagonal ( $\text{M}_2\text{AB}_2$ ,  $\text{M}_3\text{AB}_4$ )<sup>27,28</sup> symmetries. It is worth noting that the B-layers within hexagonal MAB phases create a flat honeycomb lattice—a stark contrast to the hexagonal lattice formation observed in B-based MAX phases.

Although MAX phases have integrated beneficial traits from both metals and ceramics, they are predominantly acknowledged as a class of structural ceramics renowned for their distinctive properties and applications. In contrast to conventional structural ceramics like  $\text{SiC}$  and  $\text{Si}_3\text{N}_4$ , MAX phases exhibit machinability and electrical conductivity, positioning them as viable alternatives in applications requiring intricate shapes. The integration of features from both ceramics and metals enhances their appeal, paving the way for a wide range of potential uses. Beyond their role as structural ceramics, MAX phases find utility as heating elements, nuclear materials, electrical contact materials and components such as pantograph slide plates for high-speed trains.<sup>29–33</sup> Additionally, MAX phases have shown promise in the field of energy storage and conversion due to their inherent conductivity and electrochemical stability. Recent research has concentrated on customizing the properties of MAX phases through alloying and surface modifications to enhance their performance in specific applications. The creation and analysis of MAX phases have emerged as critical research areas, holding the key to unlocking the full potential of these materials. A comprehensive understanding of their synthesis processes, crystal structures, microstructural properties, and performance under varying conditions is essential to effectively harness their capabilities and explore their applications in diverse fields.

Understanding MAX phases from a chemical perspective and their synthesis methods is a multifaceted issue. We've classified MAX phases into two broad groups, which correspond to the different elemental compositions observed in phases produced through bottom-up or top-down approaches. The first category, dubbed “classic” MAX phases are classified under space group  $P6_3/mmc$ . In this context, M stands for an early transition metal, while A signifies an A-group element, typically from groups 12 to 16 and X comprises elements such as C, N, B, and/or P. The term “classic” isn't a reflection of age but refers to Nowotny's findings where  $n = 1, 2, 3$ , later extended to include 4, 5, or 6. A recent discovery of B-containing MAX phases still fits the “classic” definition and thus belongs to this category.<sup>34</sup> Additionally, bottom-up synthesized MAX phases, this includes ternary MAX phases and alloys, which can also encompass multielement



solids with significant disorder within the M-sites,<sup>35–38</sup> conforming to hexagonal  $P6_3/mmc$  space group symmetry, and may be synthesized in a single step shown in Fig. 1b. This group includes o-MAX phases with ordered out-of-plane structures and i-MAX phases with ordered in-plane structures, typically realized through powder synthesis.<sup>39–46</sup> The i-MAX phase crystallizes in either orthorhombic  $Cmcm$  or monoclinic  $C2/c$  and  $C2/m$  symmetry, with minor differences in stacking configurations.<sup>42,46,47</sup> On the other hand, top-down synthesis, building upon the first category, introduces beyond groups 12 to 16, A-site elements are introduced. In top-down synthesized MAX phases, the distinctive feature is not their chemistry but rather the modified A-group layers. These phases usually originate from a bottom-up MAX phase precursor, where the A-layer is subsequently partially or entirely replaced after synthesis.

Additional information about various methods of synthesis like the high-temperature reaction of powder mixtures in a furnace,<sup>48,49</sup> hot isostatic pressing,<sup>50,51</sup> self-propagating high-temperature synthesis,<sup>52,53</sup> molten metal synthesis,<sup>54–56</sup> spark-plasma sintering,<sup>57–59</sup> microwave synthesis,<sup>60,61</sup> magnetron sputtering, and alternative methods.<sup>62–68</sup> However, these methods are often associated with significant drawbacks, notably in terms of time and cost, rendering them inefficient. A potential remedy to this challenge lies in Self-propagating High-temperature Synthesis (SHS). SHS stands out as a technique capable of generating over a thousand different materials, including carbides, borides, nitrides, oxides, intermetallic, and composite materials.<sup>69</sup> While high-temperature synthesis is commonly employed, certain instances exist where MAX phases can only be effectively produced through alternative methods.<sup>66,70,71</sup>

Intergrown MAX phases, a unique subgroup, are distinguished by their alternating  $M_{n+1}AX_n$  layers, each with distinct  $n$  values and thicknesses, as represented in Fig. 1c. Two prominent combinations have been noted 523 (a fusion of 211 and 312) and 725 (consisting of 312 and 413).<sup>72–74</sup> To date, five intertwined MAX phases have been identified. In the case of  $Ti_3SiC_2$ ,  $Ti_5Si_2C_3$  and  $Ti_7Si_2C_5$  emerge as secondary components.<sup>72</sup> The formation of  $Ti_5Al_2C_3$  is reported following the annealing of  $Ti_2-AlC$ .<sup>73</sup> Additionally,  $Ti_5Ge_2C_3$  and  $Ti_7Ge_2C_5$  have been observed in  $Ti_{n+1}GeC_n$  thin films, showcasing intergrown structures.<sup>74</sup> It is crucial to recognize that hybrid MAX phases, distinct from classical  $M_{n+1}AX_n$  phases, adopt the  $R3m$  space group due to the altered symmetry arising from the varying thickness and alternating stacking sequence of  $M_{n+1}AX_n$  layers.  $Mo_2Ga_2C$  ( $P6_3/mmc$ ) stands as the sole representation among the five identified double A-layer MAX phases that fits within the bottom-up synthesis category, depicted in Fig. 1d.<sup>75,76</sup> Illustrated in Fig. 1a is a summary of the elements comprising MAX phases span across a broad spectrum of the Periodic Table, this encompasses 28 variations of M-site elements, 28 A-site elements, and 6 X-site elements.

The distinctive attributes of MAX phases originate from their layered crystal structure, characterized by alternating  $M_{n+1}X_n$  layers and A layers. The M–X bonds within the  $M_{n+1}X_n$  layers are robust and can be ionic or covalent, contributing to the material's overall strength. Meanwhile, the M–A bonds between the

$M_{n+1}X_n$  layers and A layers are metallic bonds, rendering MAX phases as layered materials akin to graphite. This structural resemblance to graphite prompted researchers to explore the possibility of exfoliating MAX phases to obtain two-dimensional (2D) materials. In 2004, the mechanical exfoliation of graphite led to the discovery of graphene, a remarkable 2D material with distinct properties compared to its three-dimensional counterpart.<sup>77</sup> This breakthrough ignited significant interest in the realm of 2D materials, with subsequent discoveries including transition metal dichalcogenides (TMDs) such as  $MoS_2$ , hexagonal boron nitride (h-BN), and black phosphorus or phosphorene. Inspired by the success of graphene, researchers sought to exfoliate MAX phases to unlock their 2D potential.

Despite being weaker than intralayer bonds yet stronger than the van der Waals bonds that bind graphite layers, the metallic bonds acting as interlayer bonds in MAX phases have posed a challenge. Prior to 2011, mechanical exfoliation of MAX phases had been unsuccessful. However, a breakthrough occurred when  $Ti_3AlC_2$ , a typical MAX phase, was successfully exfoliated by specifically dissolving aluminum atoms in an HF solution, leading to the creation of 2D  $Ti_3C_2$ .<sup>78</sup> This significant achievement laid the groundwork for subsequent endeavors by research teams at Drexel University, under the leadership of Prof. Barsoum and Prof. Gogotsi, to exfoliate a range of aluminum-containing MAX phases, producing a family of 2D materials named MXenes.<sup>79–83</sup> These MXenes are created by selectively eliminating A layers from MAX phases, thereby leaving behind MX layers with a graphene-like 2D structure. This novel approach has opened up new paths for investigating the characteristics and diverse applications of MXenes in numerous domains. While several recent reviews have explored the synthesis, properties, and applications of MAX phases, they often fall short in offering a systematic evaluation of the latest developments, synthesis processes, characterization techniques and applications.<sup>83,84</sup> The existing literature lacks an in-depth examination of cutting-edge methodologies employed in the synthesis and characterization of MAX phases, leaving a gap in understanding the full spectrum of advancements in this field. Recognizing this void, our review manuscript aims to bridge the gap by providing a detailed and up-to-date exploration of the synthesis, properties, characteristics, and applications of MAX phases. By addressing the limitations of previous publications and delving into the advantages and challenges of various synthesis methods and characterization techniques, our review manuscript seeks to offer a unique and valuable contribution to the current body of knowledge on MAX phases. Through this comprehensive examination, we aim to provide researchers and practitioners with a nuanced understanding of the latest advancements in this fascinating field, fostering further innovation and progress in the synthesis and application of MAX phases.

## 2. Structure of MAX phase

### 2.1 Composition and architecture of MAX phase materials

The broad range of ternary MAX phases, denoted by the general formula  $M_{n+1}AX_n$ , showcases a remarkable spectrum of





structural and compositional variations. These MAX phases share a common space group ( $P6_3/mmc$ ) and possess a hexagonal crystalline structure. Within their unit cells, one encounters edge-sharing  $M_6X$  octahedra interspersed with layers of A elements. Remarkably, the MX layers exhibit a twinning phenomenon, where the A layer serves as a mirror plane, leading to distinctive “zig-zag” arrangements along the  $c$ -axis. The distinguishing feature among the distinguishing factor among these MAX phases is the quantity of M layers that divide the A layers with the 211, 312, 413, and 514 phases containing two, three, four, and five M layers, respectively. Exploration into quaternary MAX phases, attained by replacing elements within the M, A, or X sites reveals numerous disordered solid solutions, exhibiting unit cell and crystal structures resembling those of ternary MAX phases ( $P6_3/mmc$ ) in Fig. 2.<sup>72</sup> Remarkably, two separate ordered quaternary MAX solid solutions arise: MAX phases with out-of-plane ordering (o-MAX) and those with in-plane ordering (i-MAX), contributing to the complex structural diversity within this captivating class of materials.

**2.1.1 Solid solutions in MAX phases-single and double site variations single metal MAX (S-MAX).** Solid solutions of MAX phases involving single and double sites offer extensive compositional flexibility, enabling the synthesis of novel materials with tailored properties. These solutions open avenues for incorporating unconventional elements and enhancing phase purity, advancing the versatility and applicability of MAX phase ceramics. Initial studies by Tunca *et al.* documented 34 systems exhibiting substitutional solid solutions across M, A, and X sites, with subsequent investigations revealing an expanding inventory, including 29  $(M', M'')_{n+1}AX_n$  and 15 single-site solution MAX phases of the form  $M_{n+1}(A', A'')X_n$ .<sup>85,86</sup> These solutions offer the potential to incorporate unconventional elements like W or Fe and enhance phase purity by introducing a fourth element, as seen in the addition of Al to  $Ti_3SiC_2$ .<sup>87,88</sup> Recent research has focused on the production of nearly pure MAX phase ceramics through fifth element additions, resulting in the creation of double solid solutions  $(M', M'')_{n+1}(A', A'')X_n$ . Strategic alloying on both M and A sites has enabled the production of near-phase pure ceramics,

such as  $(Zr, Nb)_2(Al, Sn)C$  and  $(Zr, Ti)_2(Al, Sn)C$ .<sup>89–91</sup> Additionally, introducing alloying into ternary MAX phases enables the adjustment of several properties, including the coefficient of thermal expansion, high-temperature stability, hardness, toughness, and magnetic properties. Crystallographically, alloying influences lattice parameters  $a$  and  $c$ , altering the unit cell's anisotropy and distortion factors  $od$  and  $pd$ . The evolution of ZM in the 211 type varies with the partially replaced element, as observed in  $(Ti, Nb)_2AlC$  and  $Cr_2(Al, Ge)C$ .<sup>92,93</sup> Overall, these findings underscore the profound impact of alloying on MAX phase properties, supported by a statistical dispersion of host and solute atoms across all listed structures.

**2.1.2 Out-of-plane direction MAX phases (o-MAX).** This review manuscript focuses on a comprehensive examination of out-of-plane (o-MAX) phase structures, providing an insightful exploration into their unique properties and practical applications. The MAX-phase family has expanded, leading to the discovery of novel microstructures, with the out-of-plane ordered microstructure standing out as a defining subgroup known as o-MAX phases. Characterized by a general formula of  $(M_1, M_2)_{n+1}AlC_n$ , with  $n$  being either 2 or 3, o-MAX phases exhibit a distinctive ordering of M layers. Within these structures, two  $M_1$  layers enclose either one or two  $M_2$  layers in each M layer, forming a characteristic arrangement. The pioneering discovery of the first o-MAX phase,  $(Cr_{2/3}Ti_{1/3})_3AlC_2$ , arose from a solid-state reaction between  $Cr_2AlC$  and  $TiC$ .<sup>43</sup> The ordered arrangement of Cr and Ti atoms in  $(Cr_{2/3}Ti_{1/3})_3AlC_2$  was revealed through diffraction techniques utilizing neutrons and X-rays (XRD) analyses. Rietveld refinement provided more precise localization of Ti and Cr atoms within the 2a and 4f Wyckoff sites, respectively. The emergence of the M site ordered structure was explained by notable variations in electronegativity and covalent radius between Ti and Cr atoms. These differences made the formation of a  $(Cr, Ti)_3AlC_2$ -type solid solution challenging, while the ordered quaternary  $(Cr_{2/3}Ti_{1/3})_3AlC_2$  structure emerged more readily.<sup>94</sup> A similar M site ordering was later discovered in  $(Cr_{1/2}V_{1/2})_{n+1}AlC_n$  MAX phases with  $n$  values of two and three. Refinements using neutron diffraction showcased the distinct occupancy of V atoms in the 2a and 4f Wyckoff sites in  $(Cr_{1/2}V_{1/2})_3AlC_2$  and  $(Cr_{1/2}V_{1/2})_4AlC_3$ , revealing varying occupancies in the 4e and 4f Wyckoff sites.<sup>95</sup>

Additionally, out-of-plane ordering was observed in  $(MoTi)_{n+1}AlC_n$  ( $n = 2$  or  $3$ ) MAX phases. Diagrams illustrating the 312- and 413-unit cells depicted outer M layers “sandwiching” middle M layers, with the ordering influenced by the ratio of M elements. However, incomplete ordering was observed due to partial intermixing, as evidenced by neutron diffraction analysis. The out-of-plane chemical order in  $M_3AX_2$  and  $M_4AX_3$  o-MAX phases displayed M element specificity. In  $M_3AX_2$ , the first M element (Mo, Ti, Cr) occupied the 4f Wyckoff site, adjacent to the Al layer, while the second M element (Ti, Sc, Zr, V) occupied the 2a Wyckoff site shown in Fig. 3a.<sup>95,96</sup> The emergence of o-MAX phases is suggested to arise from the introduction of a second M element, which disrupts the energetically unfavorable stacking of the first M element. This is particularly relevant for M elements like Mo and Cr, whose binary carbides do not form crystals with the rock salt structure,

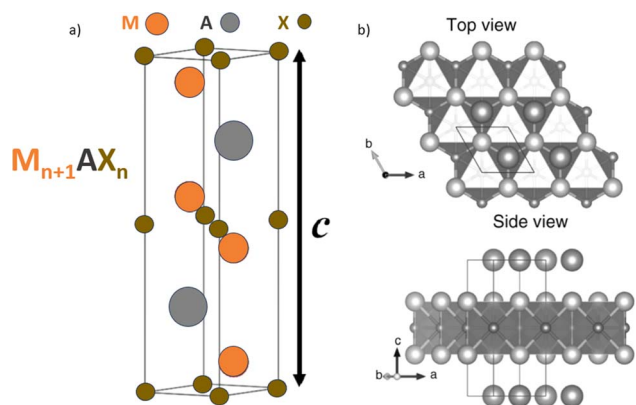


Fig. 2 (a) Unit cell and (b) crystal structure of MAX-phases. (Reproduced from ref. 72 with permission from American Physical Society, copyright 2004).<sup>72</sup>

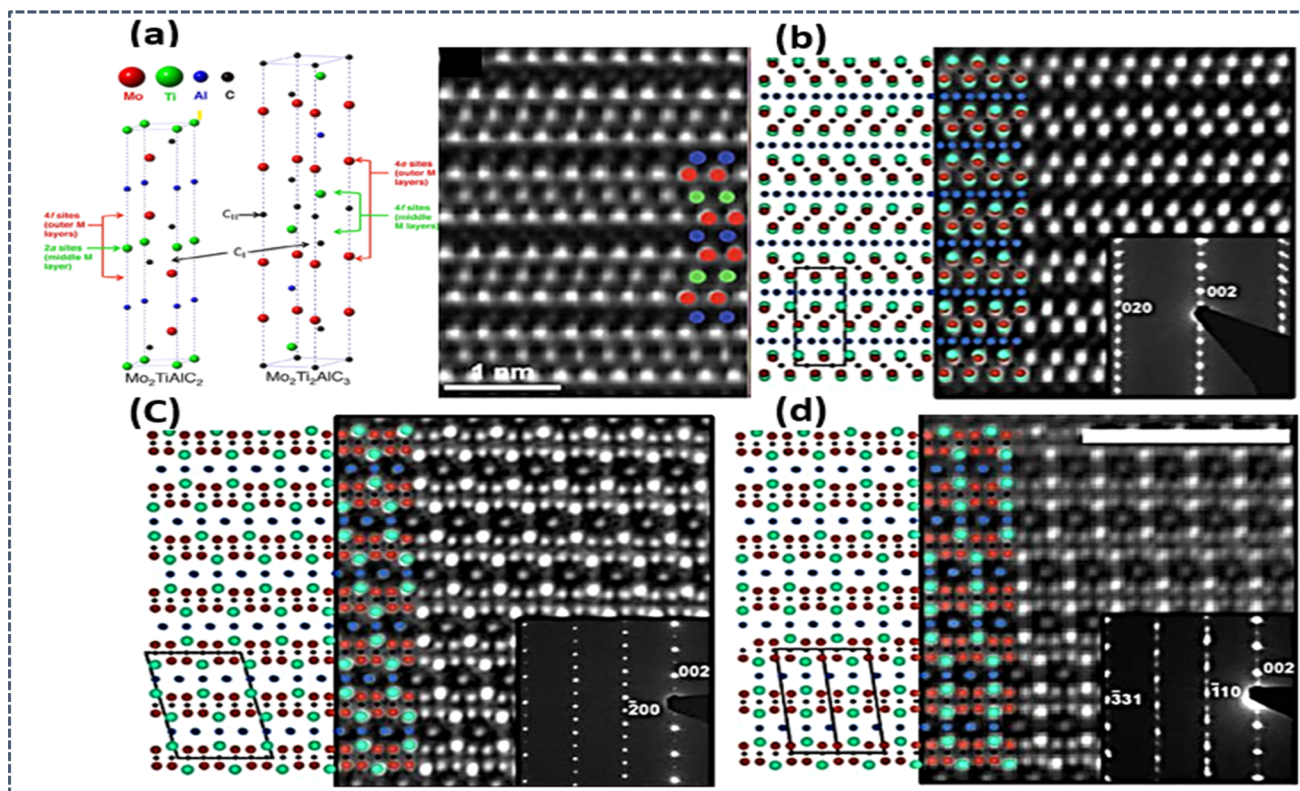


Fig. 3 (a) o-MAX phase microstructure STEM analyses of  $(\text{MoTi})_{n+1}\text{AlC}_n$  ( $n = 2$  or  $3$ ) MAX phases, with HAADF-STEM images and EDS maps. HRSTEM of  $\text{Mo}_2\text{ScAlC}_2$  and  $\text{Mo}_2\text{Ti}_2\text{AlC}_3$  o-MAX. Reprinted with permission<sup>95,96</sup> and microstructures of traditional and i-MAX phases are depicted, featuring schematic illustrations and HAADF-STEM images. Images (b–d) show  $(\text{V}_{2/3}\text{Zr}_{1/3})_2\text{AlC}$  i-MAX phase viewed along  $[010]$ ,  $[110]$ , and  $[100]$  zone axes. Reprinted with permission.<sup>101</sup>

thus avoiding the occupation of center layers. Another noteworthy o-MAX phase,  $(\text{Mo}_2\text{Sc})\text{AlC}_2$ , demonstrated clear interleaving of Sc layers between two layers of Mo. The stability of this phase was attributed to electronic configurations, with Sc atoms likely donating electrons to C atoms and Mo atoms attracting electrons from the Al layer.<sup>96,98</sup> As of now, only six o-MAX phases, including  $(\text{Cr}_{2/3}\text{Ti}_{1/3})_3\text{AlC}_2$ ,  $(\text{Cr}_{1/2}\text{V}_{1/2})_3\text{AlC}_2$ ,  $(\text{Cr}_{1/2}\text{V}_{1/2})_4\text{AlC}_3$ ,  $(\text{MoTi})_3\text{AlC}_2$ ,  $(\text{MoTi})_4\text{AlC}_3$ , and  $(\text{Mo}_2\text{Sc})\text{AlC}_2$ , have been synthesized. Notably, Al is consistently found occupying the A site, while C occupies the X site in all o-MAX phases. Interestingly, no o-MAX phases have been experimentally identified within the 211 MAX phase, despite theoretical predictions. This absence may be attributed to the singular Wyckoff site in the 211 phase, and the ordering of which would lead to the formation of a superlattice, thereby decreasing configurational entropy.<sup>99</sup> Finally, they exploration of o-MAX phases continues to unravel their unique structural intricacies and holds promise for further advancements in materials science.

**2.1.3 In-plane ordered MAX phases (i-MAX).** The i-MAX phase structure represents a captivating realm in materials science, particularly within the domain of in-plane configurations. This phase structure entails a meticulous exploration of its intriguing characteristics, unveiling a complex and intricate framework. Researchers delve into the subtle nuances of i-MAX

phases, deciphering their unique properties and behavior. Navigating through fundamental principles to recent advancements, we offer a concise yet thorough overview of the structural nuances and promising functionalities exhibited by i-MAX phases. The seminal discovery of the  $(\text{Mo}_{2/3}\text{Sc}_{1/3})_2\text{AlC}$  compound marked the inception of a novel ordering known as the i-MAX phase has emerged, featuring a 211 stoichiometry and an in-plane organization of the M elements. In contrast to the conventional 211-type MAX structures, the i-MAX crystal structure presents a more intricate unit cell that extends in-plane along both  $a$  and  $b$  axes. Within this structure, non-equivalent M-sites demonstrate comparable stability under both monoclinic (space group 15 –  $C2/c$ ) and orthorhombic (space group 63 –  $Cmcm$ ) descriptions. The structural exploration extends beyond  $(\text{Mo}_{2/3}\text{Sc}_{1/3})_2\text{AlC}$  to encompass other i-MAX phases such as  $(\text{V}_{2/3}, \text{Zr}_{1/3})_2\text{AlC}$ ,  $(\text{Mo}_{2/3}, \text{Y}_{1/3})_2\text{AlC}$ , and  $(\text{Cr}_{2/3}, \text{Zr}_{1/3})_2\text{AlC}$ .<sup>100,101</sup> HAADF-STEM images expose the in-plane chemical arrangement within these i-MAX phases, emphasizing the unique atomic arrangements and the Kagomé-like pattern formed by Al atom columns shown in Fig. 3b–d.<sup>97</sup> The crystallographic diversity of i-MAX phases manifests in two structures:  $C2/c$  monoclinic and  $Cmcm$  orthorhombic, elucidated through a close interplay of experimental synthesis, characterization, and computational stability assessment using density functional theory (DFT).<sup>43,102</sup> Anticipating the potential to derive





attractive MXene 2D-derivatives, theoretical predictions on ordered MAX phases encompassing 24 structures.<sup>103,104</sup> These predictions hinge on key parameters, including the formation enthalpy ( $\Delta H_{\text{ep}}$ ) and the temperature at which the transition from order to disorder occurs ( $T_{\text{disorder}}$ ).<sup>100,105</sup> The latter parameter underscores the necessity for  $T_{\text{disorder}}$  to exceed the synthesis temperature for the experimental realization of ordered structures.<sup>106</sup> Sokol *et al.* offer an overview of around 30 i-MAX phases, revealing the discovery of rare-earth-containing phases for the first time.<sup>15</sup> Notably, all known i-MAX phases thus far have been synthesized using Al or Ga as A-elements and C as X-element, emphasizing the need for further exploration into other A-elements and X-elements. Despite the wealth of discovered (i-MAX) phases, the absence of high phase purity bulk i-MAX ceramics precludes a comprehensive understanding of their intrinsic material properties. Theoretical and empirical analyses have laid the foundation for formulating rules governing i-MAX formation, encompassing criteria such as a ratio of 2 : 1 for  $M_1 : M_2$ , substantial differences in the sizes of the two metals, with  $M_2$  being larger, an electron population favoring bonding orbitals, and a small-sized A element.<sup>100,107,108</sup> The first three criteria are deemed particularly crucial, while intermixing of M elements can be anticipated. However, further investigations are required to elucidate the impact of deviations from the ideal 2 : 1 ratio on stability and the implications for the transformation of i-MAX into i-MXene structures. It is noteworthy that despite the diverse crystal structures observed in intermediate (i-MAX) phases, the resulting i-MXene structures remain identical, highlighting the intriguing consistency in the transformation process.

Also, this manuscript explores the intriguing domain of MAX phases, with a particular emphasis on their rare-earth (RE)

variations, often referred to as RE-i-MAX phases. The structural attributes of these RE-i-MAX phases have been extensively scrutinized, owing to their distinctive and auspicious characteristics. Inspired by the recent revelation of RE-i-MAX phases and the possibility of employing these magnetic phases serve as precursor materials in layered compounds to synthesize 2D magnetic MXenes, the investigation focused on the  $(\text{Mo}_{2/3}\text{RE}_{1/3})_2\text{AlC}$  unit cell, comprising 48 atoms – 16 Mo, 8 RE (Nd, Sm, Gd, Tb, Dy, Ho, Er, Tm, or Lu), 12 Al, and 12 C atoms – and crystallizing in the  $C2/c$  (#15) space group.<sup>109,110</sup> Owing to their analogous structures, a schematic representation valid for any RE element is depicted in Fig. 4a. Additionally, the quality and structure of monocrystalline samples were scrutinized *via* scanning transmission electron microscopy (STEM) shown in Fig. 4b.<sup>111</sup> The precise arrangement of atoms in the samples affirmed the  $C2/c$  crystalline structure. Furthermore, the alternation of one bright RE atom and two less bright Mo atoms is discernible from the line profile in the inset of the second panel. The inclusion of rare-earth elements introduces a layer of complexity, ushering in distinct electronic and magnetic properties that augment their utility. For instance, the integration of RE elements can alter the electronic and magnetic traits of MAX phases, thereby widening their potential applications in domains such as spintronics, energy storage, and catalysis. Additionally, the varying sizes and electronegativities of RE elements compared to other MAX phase constituents contribute to the emergence of unique crystal structures, which have been thoroughly explored through both computational and experimental studies.

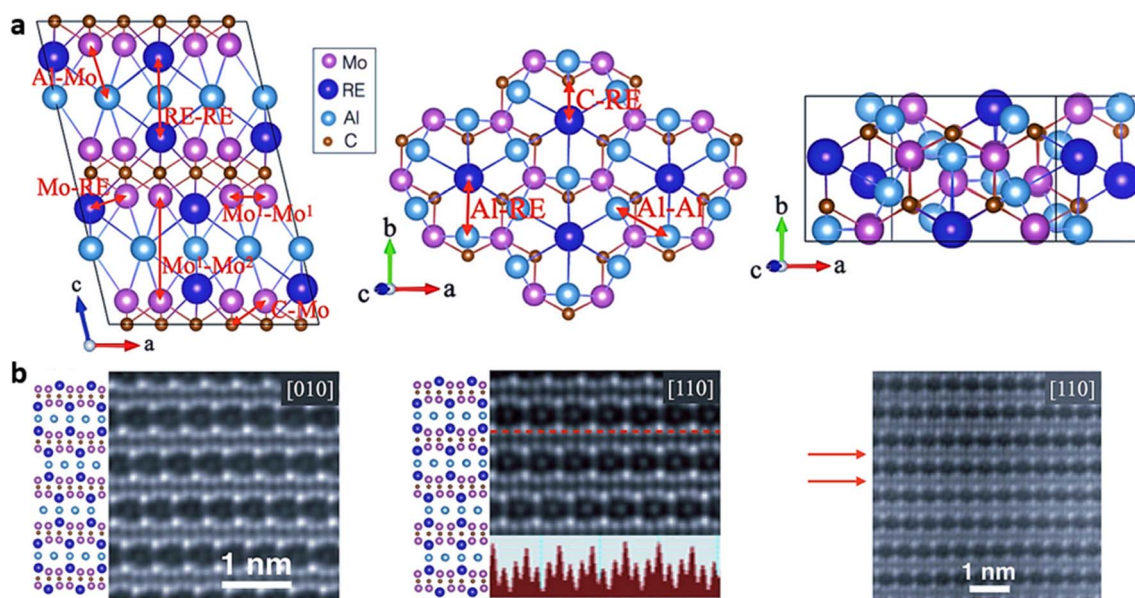


Fig. 4 (a) Schematic depiction of the conventional monoclinic  $C2/c$  unit cell for  $(\text{Mo}_{2/3}\text{RE}_{1/3})_2\text{AlC}$ , with specific interatomic bonds highlighted by red arrows. (b) High-resolution STEM images of  $(\text{Mo}_{2/3}\text{Dy}_{1/3})_2\text{AlC}$  single crystals along  $[010]$  and  $[110]$  zone axes, accompanied by corresponding schematics for the  $C2/c$  monoclinic structure. Inset exhibits the line-profile of Z contrast along the red dashed line, and the area with a stacking fault is indicated by red arrows. (Reproduced from ref. 109 and 111 with permission from American Physical Society, copyright 2019).<sup>109,111</sup>



Table 1 presents a list of synthesized MAX phases. It is observed that the number of single metal MAX phases surpasses that of o-MAX and i-MAX phases (Table 1). The structures of i-MAX and o-MAX are notably more intricate compared to single metal MAX phases. The synthesized single metal MAX, o-MAX, and i-MAX phases are outlined in Table 1.

### 3. Properties of MAX phases

MAX phases are a unique class of layered ternary carbides and nitrides with the general formula  $M_{n+1}AX_n$  (where M is an early transition metal, A is an A-group element, and X is carbon and/or nitrogen). These materials combine the best properties of metals and ceramics, making them highly desirable for various applications. They exhibit high strength and hardness, excellent damage tolerance, and remarkable fracture toughness, allowing them to withstand mechanical stresses without cracking. The unique properties of MAX phases arise from their layered structure, where 'M' layers (metallic) alternate with 'A' layers (group elements) and 'X' layers (carbon/nitrogen). This structure enables a combination of metallic and ceramic characteristics. MAX phases can deform plastically at relatively low temperatures due to the presence of basal slip systems, which facilitate dislocation movement. This is unusual for ceramics and contributes to their damage tolerance. The strong covalent bonding in the 'M-X' layers provides thermal stability, while the metallic bonding in the 'M' layers ensures good electrical and thermal conductivity. Their high thermal conductivity and stability enable them to maintain performance at elevated temperatures, while their good electrical conductivity makes them suitable for electromagnetic shielding. MAX phases are also known for their corrosion and oxidation resistance, ensuring long-term stability in harsh environments. Additionally, they offer excellent thermal shock resistance and are machinable using conventional tools, unlike most ceramics. Below Fig. 5 provides a comprehensive summary of the properties of MAX phases, which are a class of layered ternary carbides and nitrides. The unique layered structure of MAX phases contributes to their distinctive combination of properties, making them ideal for use in coatings, high-temperature components, electrical contacts, and other demanding applications.

The future of MAX phases depends on substantial research and development efforts. One key area is exploring new combinations of M, A, and X elements to discover MAX phases with enhanced properties. Additionally, developing nanostructured MAX phases can further improve their mechanical and thermal properties. Another promising direction is creating hybrid materials by combining MAX phases with other materials to produce composites with tailored properties for specific applications. These advancements will likely expand the potential uses of MAX phases across various industries, driving innovation and improving performance in numerous high-demand areas.

#### 3.1 Electrical and thermal properties

Electronic and thermal properties play a crucial role in understanding the behavior of MAX phases. These materials exhibit

good electrical conductivity, with variations observed among different compositions. Variations in electronic conductivity are evident across different MAX compositions, with  $Ti_4AlN_3$  exhibiting notably lower conductivity attributed to reduced charge carrier mobility resulting from scattering by vacancies. Moreover, the microstructure plays a pivotal role in determining electronic conductivity, as demonstrated by the stark contrast in conductivity between  $Ti_2AlC$  samples synthesized *via* different methods. Lattice defects such as vacancies, dislocations, stacking faults, and grain boundaries in self-propagating high-temperature synthesis (SHS)/pressurized by hot isostatic pressing (PHIP)-synthesized  $Ti_2AlC$  lead to increased electron-scattering and higher electrical resistivity. Similar to metals, the electronic resistivity of MAX phases shows a linear increase with temperature, described by a characteristic temperature coefficient of resistivity. For instance, the electronic resistivity of  $Ti_2AlC$  rises from  $0.36 \times 10^{-6} \Omega m$  at 300 K to approximately  $1.0 \times 10^{-6} \Omega m$  at 1200 K shown in Fig. 6a and b. Conversely, the electrical conductivity of MAX phases generally decreases as temperature rises, reflecting their thermally dependent behavior.<sup>159</sup>

Thermal properties of MAX phases, encompassing thermal expansion coefficients, heat capacity, and conductivity, provide insights into their behavior under varying temperature conditions. While most MAX phases exhibit thermal expansion coefficients within the range of  $7\text{--}10 \times 10^{-6} K$ , exceptions such as  $Cr_2AlC$  display significantly higher values. Notably,  $Cr_2AlC$  and  $Ti_2AlC$  demonstrate lower heat capacities at room temperature compared to other MAX phases, indicating distinctive thermal behavior. Regarding thermal conductivity at room temperature,  $Ta_4AlC_3$  stands out as the highest among the mentioned MAX phases. Similar to electronic attributes, the thermal behavior of MAX phases alters with temperature, as demonstrated by the temperature-dependent heat capacity and thermal conductivity of  $Ti_2AlC$ . The linear increase in thermal conductivity with temperature mirrors the trend observed in electronic resistivity. Furthermore, the contribution of electrons and phonons to total thermal conductivity varies with temperature, with electrons dominating at room temperature. Phonon contributions become more significant in Al-containing MAX phases due to the strong binding of aluminum atoms facilitating coherent vibrations with neighboring atoms. The relationship between thermal conductivity and temperature differs among various MAX phases, with some demonstrating a decrease in thermal conductivity as temperature rises, while others display slight increases, underscoring the complex interplay of factors influencing thermal behavior in Table 2.

#### 3.2 Mechanical properties in ambient temperature condition

MAX phases possess a distinctive microstructure and chemical bonding that contribute to their impressive mechanical properties at ambient temperatures. These materials typically exhibit elevated Young's modulus, flexural and compressive strength, as well as fracture toughness, although they tend to have relatively low hardness and shear modulus. The robust



Table 1 Summary of various MAX phase types and their corresponding structural properties

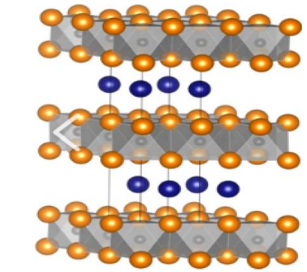
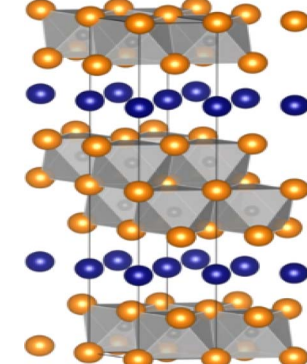
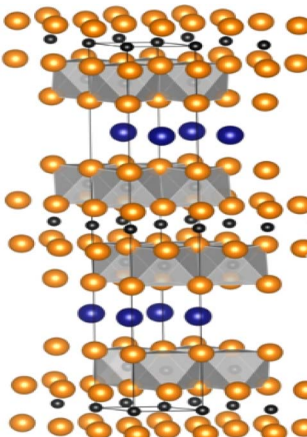
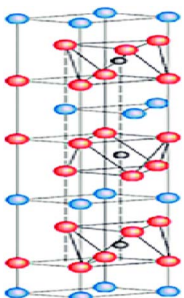
Types	Single metal MAX	Structure
211	$\text{Ti}_2\text{AlC}$ , <sup>112</sup> $\text{Ti}_2\text{GaC}$ , <sup>113</sup> $\text{Ti}_2\text{GeC}$ , <sup>114</sup> $\text{Ti}_2\text{SiC}$ , $\text{Zr}_2\text{SiC}$ , $\text{Hf}_2\text{AlC}$ , <sup>115</sup> $\text{Hf}_2\text{GaC}$ , $\text{Hf}_2\text{GeC}$ , $\text{Hf}_2\text{InC}$ , $\text{Hf}_2\text{SiC}$ , $\text{V}_2\text{AlC}$ , <sup>112</sup> $\text{V}_2\text{AuC}$ , $\text{V}_2\text{CdC}$ , $\text{V}_2\text{ZnC}$ , $\text{V}_2\text{GaC}$ , $\text{Nb}_2\text{AlC}$ , $\text{Nb}_2\text{AuC}$ , <sup>116</sup> $\text{Nb}_2\text{CdC}$ , $\text{Nb}_2\text{GaC}$ , <sup>113</sup> $\text{Nb}_2\text{InC}$ , <sup>117</sup> $\text{Nb}_2\text{IrC}$ , $\text{Nb}_2\text{TlC}$ , $\text{Nb}_2\text{ZnC}$ , $\text{Ta}_2\text{AlC}$ , $\text{Ta}_2\text{AuC}$ , $\text{Ta}_2\text{GaC}$ , $\text{Ta}_2\text{InC}$ , $\text{Ta}_2\text{ZnC}$ , $\text{Cr}_2\text{AuC}$ , <sup>118</sup> $\text{Cr}_2\text{GaC}$ , $\text{Cr}_2\text{ZnC}$ , $\text{Mo}_2\text{AlC}$ , $\text{Mo}_2\text{ZnC}$ , $\text{Ti}_2\text{AlN}$ , $\text{Ti}_2\text{GaN}$ , $\text{Hf}_2\text{AlN}$ , $\text{V}_2\text{ZnN}$	
312	$\text{Ti}_3\text{AlC}_2$ , $\text{Ti}_3\text{AuC}_2$ , $\text{Ti}_3\text{CdC}_2$ , $\text{Ti}_3\text{GaC}_2$ , $\text{Ti}_3\text{GeC}_2$ , $\text{Ti}_3\text{InC}_2$ , $\text{Ti}_3\text{IrC}_2$ , <sup>119</sup> $\text{Ti}_3\text{SiC}_2$ , <sup>120</sup> $\text{Ti}_3\text{TlC}_2$ , $\text{Ti}_3\text{ZnC}_2$ , $\text{Zr}_3\text{AlC}_2$ , <sup>121</sup> $\text{Hf}_3\text{AlC}_2$ , <sup>115</sup> $\text{Hf}_3\text{AuC}_2$ , $\text{Hf}_3\text{CdC}_2$ , $\text{Hf}_3\text{CuC}_2$ , $\text{Hf}_3\text{GaC}_2$ , $\text{Hf}_3\text{GeC}_2$ , $\text{Hf}_3\text{InC}_2$ , <sup>122</sup> $\text{Hf}_3\text{IrC}_2$ , $\text{Hf}_3\text{PbC}_2$ , <sup>123</sup> $\text{Hf}_3\text{SiC}_2$ , $\text{Hf}_3\text{SnC}_2$ , <sup>104</sup> $\text{Hf}_3\text{TlC}_2$ , $\text{Hf}_3\text{ZnC}_2$ , $\text{V}_3\text{AlC}_2$ , $\text{V}_3\text{AuC}_2$ , $\text{V}_3\text{CdC}_2$ , $\text{V}_3\text{GaC}_2$ , $\text{V}_3\text{ZnC}_2$ , $\text{Nb}_3\text{AlC}_2$ , $\text{Nb}_3\text{AuC}_2$ , $\text{Nb}_3\text{CdC}_2$ , $\text{Nb}_3\text{GaC}_2$ , $\text{Nb}_3\text{GeC}_2$ , $\text{Nb}_3\text{InC}_2$ , $\text{Nb}_3\text{IrC}_2$ , $\text{Nb}_3\text{TlC}_2$ , $\text{Nb}_3\text{ZnC}_2$ , $\text{Ta}_3\text{AlC}_2$ , <sup>124</sup> $\text{Ta}_3\text{AuC}_2$ , $\text{Ta}_3\text{CdC}_2$ , $\text{Ta}_3\text{GaC}_2$ , $\text{Ta}_3\text{IrC}_2$ , $\text{Ta}_3\text{ZnC}_2$ , $\text{Ti}_3\text{AlN}_2$ , $\text{Ti}_3\text{ZnN}_2$ , $\text{Hf}_3\text{AlN}_2$	
413	$\text{Ti}_4\text{AlC}_3$ , $\text{Ti}_4\text{AsC}_3$ , $\text{Ti}_4\text{AuC}_3$ , $\text{Ti}_4\text{CdC}_3$ , $\text{Ti}_4\text{GaC}_3$ , <sup>125</sup> $\text{Ti}_4\text{GeC}_3$ , <sup>126</sup> $\text{Ti}_4\text{InC}_3$ , $\text{Ti}_4\text{IrC}_3$ , $\text{Ti}_4\text{SiC}_3$ , <sup>127</sup> $\text{Ti}_4\text{TlC}_3$ , $\text{Ti}_4\text{ZnC}_3$ , $\text{Zr}_4\text{AlC}_3$ , $\text{Zr}_4\text{CdC}_3$ , $\text{Zr}_4\text{GaC}_3$ , $\text{Zr}_4\text{InC}_3$ , $\text{Zr}_4\text{IrC}_3$ , $\text{Zr}_4\text{SiC}_3$ , $\text{Zr}_4\text{ZnC}_3$ , $\text{Hf}_4\text{AlC}_3$ , $\text{Hf}_4\text{AuC}_3$ , $\text{Hf}_4\text{BiC}_3$ , $\text{Hf}_4\text{CdC}_3$ , $\text{Hf}_4\text{GaC}_3$ , $\text{Hf}_4\text{GeC}_3$ , $\text{Hf}_4\text{InC}_3$ , $\text{Hf}_4\text{IrC}_3$ , $\text{Hf}_4\text{PbC}_3$ , $\text{Hf}_4\text{SiC}_3$ , $\text{Hf}_4\text{SnC}_3$ , $\text{Hf}_4\text{TlC}_3$ , $\text{Hf}_4\text{ZnC}_3$ , $\text{V}_4\text{AlC}_3$ , <sup>128</sup> $\text{V}_4\text{GaC}_3$ , $\text{V}_4\text{ZnC}_3$ , $\text{Nb}_4\text{AlC}_3$ , <sup>129</sup> $\text{Nb}_4\text{AuC}_3$ , $\text{Nb}_4\text{CdC}_3$ , $\text{Nb}_4\text{GaC}_3$ , $\text{Nb}_4\text{GeC}_3$ , $\text{Nb}_4\text{InC}_3$ , $\text{Nb}_4\text{IrC}_3$ , $\text{Nb}_4\text{SnC}_3$ , $\text{Nb}_4\text{TlC}_3$ , $\text{Ta}_4\text{AlC}_3$ , <sup>130</sup> $\text{Ta}_4\text{AuC}_3$ , $\text{Ta}_4\text{CdC}_3$ , $\text{Ta}_4\text{GaC}_3$ , $\text{Ta}_4\text{InC}_3$ , $\text{Ta}_4\text{IrC}_3$ , $\text{Ta}_4\text{TlC}_3$ , $\text{Ta}_4\text{ZnC}_3$ , $\text{Ti}_4\text{AlN}_3$ , <sup>131</sup> $\text{Ti}_4\text{GaN}_3$	
212, 314, 211, 222	$\text{Hf}_2\text{InB}_2$ , $\text{Hf}_2\text{SnB}_2$ , $\text{Zr}_2\text{TlB}_2$ , $\text{Zr}_2\text{PbB}_2$ , $\text{Zr}_2\text{InB}_2$ , $\text{Ti}_2\text{InB}_2$ , $\text{Hf}_3\text{PB}_4$ , $\text{Zr}_3\text{CdB}_4$ , $\text{Hf}_2\text{BiB}$ , $\text{Hf}_2\text{PbB}$ , $\text{Hf}_2\text{B}_2\text{F}_2$ , $\text{Hf}_2\text{B}_2\text{Cl}_2$ , $\text{Zr}_2\text{B}_2\text{F}_2$ , $\text{Zr}_2\text{B}_2\text{FCl}_2$	

Table 1 (Contd.)

Types o-MAX		Structure
312	$(\text{Cr}_{2/3}\text{V}_{1/3})_3\text{AlC}_2$ , <sup>132</sup> $(\text{Cr}_{2/3}\text{Ti}_{1/3})_3\text{AlC}_2$ , <sup>133</sup> $(\text{Mo}_2\text{Ti})\text{AlC}_2$ , <sup>134,135</sup> $\text{Cr}_2\text{TiAlC}_2$ , <sup>136</sup> $(\text{Cr}_{0.75}\text{V}_{0.25})_2\text{VAlC}_2$ , <sup>a137</sup> $(\text{Mo}_2\text{Sc})\text{AlC}_2$ (ref. 138)	
413	$(\text{Cr}_2\text{V}_2)\text{AlC}_3$ , <sup>132</sup> $(\text{Mo}_2\text{Ti}_2)\text{AlC}_3$ , <sup>134</sup> $\text{Cr}_{2+x}\text{Ti}_{2-x}\text{AlC}_3$ ( $x = 0.5$ ), <sup>a139</sup> $(\text{Cr}_{0.7}\text{V}_{0.3})_2(\text{Cr}_{0.2}\text{V}_{0.8})_2\text{AlC}_3$ , <sup>a137</sup> $\text{Mo}_2\text{Nb}_2\text{AlC}_3$ <sup>a</sup> (ref. 140)	
Types i-MAX		Structure
211	$(\text{Mo}_{2/3}\text{Sm}_{1/3})_2\text{AlC}$ , $(\text{Mo}_{2/3}\text{Nd}_{1/3})_2\text{AlC}$ , $(\text{Mo}_{2/3}\text{Gd}_{1/3})_2\text{AlC}$ , $(\text{Mo}_{2/3}\text{Tb}_{1/3})_2\text{AlC}$ , $(\text{Mo}_{2/3}\text{Ho}_{1/3})_2\text{AlC}$ , $(\text{Mo}_{2/3}\text{Dy}_{1/3})_2\text{AlC}$ , $(\text{Mo}_{2/3}\text{Er}_{1/3})_2\text{AlC}$ , $(\text{Mo}_{2/3}\text{Tm}_{1/3})_2\text{AlC}$ , $(\text{Mo}_{2/3}\text{Lu}_{1/3})_2\text{AlC}$ , $(\text{Mn}_{2/3}\text{Sc}_{1/3})_2\text{GaC}$ , $(\text{Cr}_{2/3}\text{Sc}_{1/3})_2\text{GaC}$ , $(\text{Mo}_{2/3}\text{Ce}_{1/3})_2\text{AlC}$ , $(\text{Mo}_{2/3}\text{Pr}_{1/3})_2\text{AlC}$ , <sup>141</sup> $(\text{Mo}_{2/3}\text{Gd}_{1/3})_2\text{GaC}$ , $(\text{Mo}_{2/3}\text{Tb}_{1/3})_2\text{GaC}$ , $(\text{Mo}_{2/3}\text{Dy}_{1/3})_2\text{GaC}$ , $(\text{Mo}_{2/3}\text{Er}_{1/3})_2\text{GaC}$ , $(\text{Mo}_{2/3}\text{Ho}_{1/3})_2\text{GaC}$ , $(\text{Mo}_{2/3}\text{Tm}_{1/3})_2\text{GaC}$ , $(\text{Mo}_{2/3}\text{Lu}_{1/3})_2\text{GaC}$ , $(\text{Mo}_{2/3}\text{Y}_{1/3})_2\text{AlC}$ , $(\text{Cr}_{2/3}\text{Sc}_{1/3})_2\text{AlC}$ , $(\text{Mo}_{2/3}\text{Y}_{1/3})_2\text{AlC}$ , $(\text{Cr}_{2/3}\text{Y}_{1/3})_2\text{AlC}$ , $(\text{Mo}_{2/3}\text{Sc}_{1/3})_2\text{GaC}$ , $(\text{Cr}_{2/3}\text{Zr}_{1/3})_2\text{AlC}$ , <sup>142</sup> $\text{W}_{4/3}\text{Sc}_{2/3}\text{AlC}$ , $\text{W}_{4/3}\text{Y}_{2/3}\text{AlC}$ , <sup>143</sup> $\text{W}_{4/3}\text{Gd}_{2/3}\text{AlC}$ , $\text{W}_{4/3}\text{Tb}_{2/3}\text{AlC}$ , $\text{W}_{4/3}\text{Dy}_{2/3}\text{AlC}$ , $\text{W}_{4/3}\text{Ho}_{2/3}\text{AlC}$ , $\text{W}_{4/3}\text{Tm}_{2/3}\text{AlC}$ , $\text{W}_{4/3}\text{Lu}_{2/3}\text{AlC}$ , <sup>144</sup> $\text{Mo}_{4/3}\text{Sc}_{2/3}\text{AlC}$ , <sup>145</sup> $\text{V}_{4/3}\text{Zr}_{2/3}\text{AlC}$ , <sup>146</sup> $\text{Mo}_{4/3}\text{Y}_{2/3}\text{AlC}$ , <sup>147</sup> $\text{Mo}_{4/3}\text{Ce}_{2/3}\text{AlC}$ , $\text{Mo}_{4/3}\text{Dy}_{2/3}\text{AlC}$ , $\text{Mo}_{4/3}\text{Ho}_{2/3}\text{AlC}$ , $\text{Mo}_{4/3}\text{Er}_{2/3}\text{AlC}$ , $\text{Mo}_{4/3}\text{Tm}_{2/3}\text{AlC}$ , $\text{Mo}_{4/3}\text{Eu}_{2/3}\text{AlC}$ , $\text{Mo}_{4/3}\text{Pr}_{2/3}\text{AlC}$ , $\text{Mo}_{4/3}\text{Nd}_{2/3}\text{AlC}$ , $\text{Mo}_{4/3}\text{Sm}_{2/3}\text{AlC}$ , <sup>148</sup> $\text{Cr}_{4/3}\text{Sc}_{2/3}\text{GaC}$ , <sup>149</sup> $\text{V}_{4/3}\text{Sc}_{2/3}\text{AlC}$ , <sup>150</sup> $\text{Cr}_{4/3}\text{Sc}_{2/3}\text{AlC}$ , $\text{Cr}_{4/3}\text{Y}_{2/3}\text{AlC}$ , <sup>151</sup> $\text{Cr}_{4/3}\text{Zr}_{2/3}\text{AlC}$ , <sup>152</sup> $\text{Cr}_{4/3}\text{Gd}_{2/3}\text{AlC}$ , $\text{Cr}_{4/3}\text{Tb}_{2/3}\text{AlC}$ , <sup>153</sup> $\text{Cr}_{4/3}\text{Dy}_{2/3}\text{AlC}$ , $\text{Cr}_{4/3}\text{Ho}_{2/3}\text{AlC}$ , $\text{Cr}_{4/3}\text{Er}_{2/3}\text{AlC}$ , $\text{Cr}_{4/3}\text{Tm}_{2/3}\text{AlC}$ , $\text{Cr}_{4/3}\text{Lu}_{2/3}\text{AlC}$ , $\text{Mn}_{4/3}\text{Sc}_{2/3}\text{GaC}$ , <sup>133</sup> $\text{Mo}_{4/3}\text{Sc}_{2/3}\text{GaC}$ , $(\text{Mo}_{2/3}\text{Y}_{2/3}\text{GaC})$ , <sup>154</sup> $\text{Mo}_{4/3}\text{Gd}_{2/3}\text{GaC}$ , $\text{Mo}_{4/3}\text{Tb}_{2/3}\text{GaC}$ , $\text{Mo}_{4/3}\text{Dy}_{2/3}\text{GaC}$ , $\text{Mo}_{4/3}\text{Ho}_{2/3}\text{GaC}$ , $\text{Mo}_{4/3}\text{Er}_{2/3}\text{GaC}$ , $\text{Mo}_{4/3}\text{Tm}_{2/3}\text{GaC}$ , $\text{Mo}_{4/3}\text{Yb}_{2/3}\text{GaC}$ , $\text{Mo}_{4/3}\text{Lu}_{2/3}\text{GaC}$ , <sup>155</sup> $(\text{W}_{0.5}\text{Mo}_{0.5})_{4/3}\text{Y}_{2/3}\text{AlC}$ , <sup>b</sup> $\text{W}_{2/3}\text{Mo}_{2/3}\text{Gd}_{2/3}\text{AlC}$ , <sup>b</sup> $(\text{W}_{0.5}\text{Mo}_{0.5})_{4/3}\text{Tb}_{2/3}\text{AlC}$ , <sup>b</sup> $(\text{W}_{0.5}\text{Mo}_{0.5})_{4/3}\text{Dy}_{2/3}\text{AlC}$ , <sup>b</sup> $(\text{W}_{0.5}\text{Mo}_{0.5})_{4/3}\text{Ho}_{2/3}\text{AlC}$ , <sup>b</sup> $(\text{W}_{0.5}\text{Mo}_{0.5})_{4/3}\text{Er}_{2/3}\text{AlC}$ , <sup>b156</sup> $\text{Nb}_2(\text{Al}_{0.2}\text{Au}_{0.8})\text{C}$ , <sup>b157</sup> $\text{Ti}_3(\text{Al}_{1/3}\text{Cu}_{2/3})\text{C}_2$ (ref. 158)	<p><math>M'_{4/3}M''_{2/3}AX</math> (<math>C2/m</math>)</p> <p><math>M'_{4/3}M''_{2/3}AX</math> (<math>C2/c</math>)</p> <p><math>M'_{4/3}M''_{2/3}AX</math> (<math>Cmcm</math>)</p>

<sup>a</sup> Partial mixing or off-stoichiometry in contrast to the ideal o-MAX phase. <sup>b</sup> Solid solution i-MAX (in-plane metal ordering).





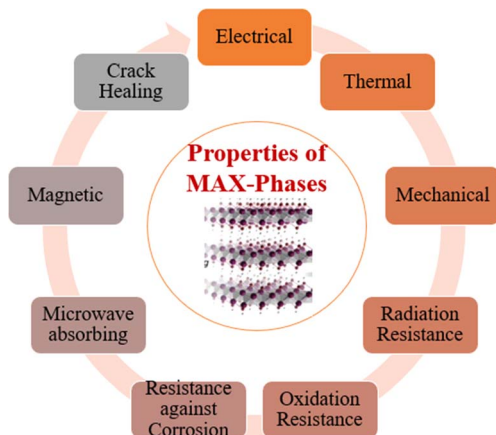


Fig. 5 Overview of MAX-phase properties.

covalent bonds formed between M-site and A-site elements largely contribute to their high Young's modulus, strength, and fracture toughness. Conversely, the weaker bonds between the MX layer and A layer lead to a lower shear modulus. Despite their robust mechanical characteristics, MAX phases maintain a relatively low density, ranging from 4.1 to 5 g cm<sup>-3</sup>, rendering them elastically stiff. Consequently, their specific stiffness values, notably high when calculated as the ratio of Young's modulus to density. For instance, Ti<sub>2</sub>AlC MAX phases exhibit Specific stiffness values marginally below those of Si<sub>3</sub>N<sub>4</sub> ceramics but roughly three times higher than Ti metal.<sup>166</sup> Notably, Ta-containing MAX phases go against the low-density trend, with Ta<sub>2</sub>AlC and Ta<sub>4</sub>AlC<sub>3</sub> boasting densities reaching up to 11.64 g cm<sup>-3</sup> and 13.18 g cm<sup>-3</sup>, respectively. Despite their high stiffness, MAX phases exhibit relatively lower hardness compared to other ceramic materials like ZrO<sub>2</sub>-based or ZrO<sub>2</sub> toughened Al<sub>2</sub>O<sub>3</sub>, having hardness values within the limited range of 2–5 GPa.<sup>167,168</sup> Their Young's modulus, ranging from 282 GPa to 340 GPa, positions them between ZrO<sub>2</sub> and Al<sub>2</sub>O<sub>3</sub> ceramics but significantly higher than most metals like Ti<sub>6</sub>Al<sub>4</sub>V alloy.<sup>167</sup> While MAX phases exhibit lower flexural strength compared to some structural ceramics, they demonstrate excellent crack propagation resistance, as evidenced by their high fracture toughness values. These properties are similar to those observed in structural Si<sub>3</sub>N<sub>4</sub> ceramics, which exhibit an interlocking microstructure.<sup>169</sup> While MAX phases generally exhibit favorable mechanical properties at room temperature, there is still potential for enhancement in certain aspects such as hardness and flexural strength. Drawing from strategies commonly employed in ceramic materials, various strengthening and toughening mechanisms have been explored for MAX phases. Notably, a novel MAX phase solid solution, Ti<sub>3</sub>(Al<sub>0.8</sub>Si<sub>0.2</sub>Sn<sub>0.2</sub>)C<sub>2</sub>, incorporating three A-site elements, has been synthesized. This solid solution exhibits improved flexural strength and Vickers hardness, measuring 649 ± 27 MPa and 6.4 ± 0.12 GPa, respectively, surpassing those of single-phase counterparts like Ti<sub>3</sub>AlC<sub>2</sub> or Ti<sub>3</sub>(AlSn<sub>0.2</sub>)C<sub>2</sub>. The observed enhancement is credited to solid solution reinforcement.<sup>170</sup>

Particle toughening techniques have been employed to enhance fracture toughness, exemplified by ZrC particles-

reinforced Ti<sub>3</sub>AlC<sub>2</sub> composites. The incorporation of 20 vol% ZrC resulted in a notable enhanced fracture toughness, rising from 7.8 ± 0.4 MPa m<sup>-1/2</sup> for monolithic Ti<sub>3</sub>AlC<sub>2</sub> to 11.5 ± 1.0 MPa m<sup>-1/2</sup> for the composite.<sup>171</sup> Similarly, ZrO<sub>2</sub> particles were utilized to improve fracture toughness in ZrO<sub>2</sub>/Ti<sub>3</sub>AlC<sub>2</sub> composites, attributed to transformation toughening effects.<sup>172</sup> Moreover, the addition of ZrO<sub>2</sub> led to enhancements in flexural strength and Vickers hardness, further underscoring the influence of composition on mechanical behavior. Notably, in ternary MAX phases with similar microstructures, the substitution of Ti with V or Cr has been shown to significantly enhance bulk modulus by up to 36%.<sup>173</sup> These findings highlight the multifaceted approaches and the pivotal role of composition in tailoring mechanical properties of MAX phases. MAX phases with their distinctive layered nanolaminate structure exhibit remarkable mechanical properties characterized by kinking nonlinear elastic (KNE) behavior. Recent investigations, exemplified by the work of Bei *et al.*, have elucidated the intricate deformation mechanisms of Ti<sub>3</sub>AlC<sub>2</sub> MAX phase under compression.<sup>160</sup> The observed microstructures near critical cracks unveil a range of mechanisms for energy dissipation, such as grain bending, pull-out, push-in, *trans*-granular fracture, grain decohesion, crack deflection along grain boundaries, and the creation of kink bands (KBs) and delamination. These KBs, arising from dislocation glide, demonstrate continuous propagation within the lamella, indicative of the complex nature of mechanical responses in MAX phases. Additionally, studies on Nb<sub>2</sub>AlC MAX phase by Zhang *et al.* reveal shear deformation in laminated grains alongside *trans*-granular fracture, with crack propagation aligned parallel to the layer orientation.<sup>174</sup> These findings underscore the recurring nature of KBs and shear deformation across various MAX phases such as Ti<sub>2</sub>AlC, Cr<sub>2</sub>AlC, and Ta<sub>4</sub>AlC<sub>3</sub>, underscoring their pivotal role in governing mechanical deformation processes.<sup>159,175,176</sup> Table 3 presents an overview of ambient-temperature mechanical characteristics across selected MAX phases.

### 3.3 Mechanical properties in elevated temperature condition

Outstanding mechanical performance at elevated temperatures is a defining characteristic of MAX materials, garnering considerable attention in research endeavors. These materials commonly exhibit a brittle-plastic transition temperature (BPTT), delineating their behavior. Below this threshold, which varies among MAX phases, temperature fluctuations have negligible effects on strength, and brittle fracture akin to traditional ceramics is observed. Conversely, above the BPTT, MAX phases display pronounced plastic deformation resembling conventional metals.<sup>180</sup> Bai *et al.* conducted comprehensive flexural and compressive assessments on Ti<sub>3</sub>AlC<sub>2</sub> MAX phase across a temperature gradient, revealing distinct behaviors.<sup>159</sup> At room temperature (RT) through 900 °C, Ti<sub>3</sub>AlC<sub>2</sub> exhibited typical brittle fracture, transitioning to plastic deformation at 950 °C without a discernible yield point. The BPTT, determined through flexural testing, fell between 900 and 950 °C, while in compression testing, it ranged from 800 to 900 °C,



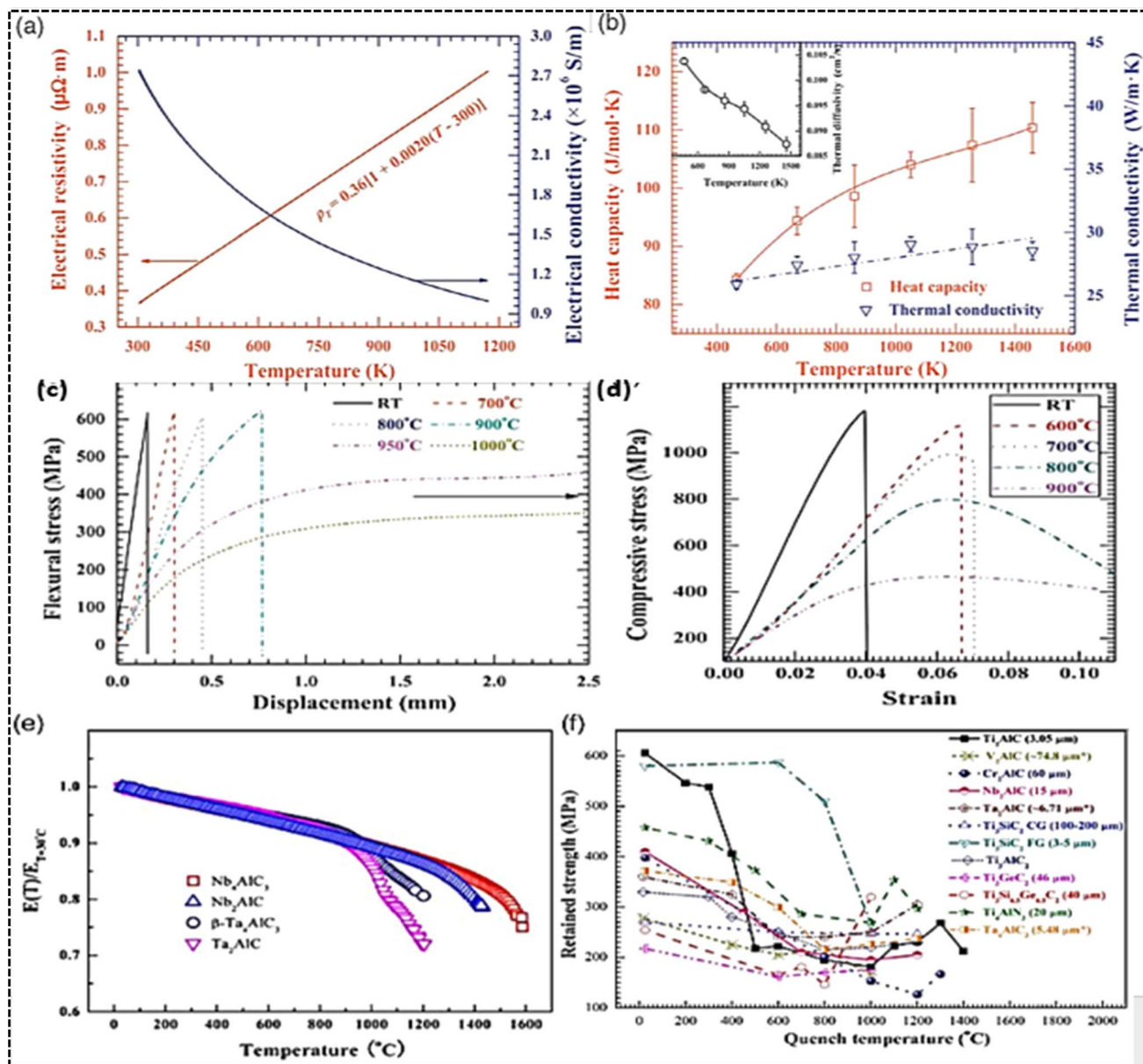


Fig. 6 MAX phases electrical and thermal characteristics: (a)  $\text{Ti}_2\text{AlC}$ 's electronic conductivity and resistivity as a function of temperature. (b) Thermal conductivity, heat capacity, and diffusivity variations in  $\text{Ti}_2\text{AlC}$  across temperatures. Mechanical properties of MAX phases: graphs illustrating deformation characteristics under flexural and compressive stress of  $\text{Ti}_2\text{AlC}$  from ambient conditions to increased temperatures are shown. (c and d). Mechanical behaviours of MAX phases (e and f). (Reproduced from ref. 159 with permission from Elsevier, copyright 2013).<sup>159</sup> (Reproduced from ref. 160 with permission from American Ceramic Society, copyright 2012).<sup>160</sup>

indicating phase-specific variability shown in Fig. 6c and d. Furthermore, it was evident that temperature increments below the BPTT did not significantly affect flexural or compressive strength, whereas beyond this threshold, a rapid strength decline ensued. Variations in BPTT were also observed among different MAX phases, exemplified by  $\text{Nb}_4\text{AlC}_3$ 's remarkable retention of ambient strength up to 1400  $^\circ\text{C}$ , contrasting with the lower BPTT of  $\text{Cr}_2\text{AlC}$ , situated between 800 and 900  $^\circ\text{C}$ .<sup>161,181</sup> Moreover, the decline in Young's modulus with rising temperatures shown in Fig. 6e mirrored the trend observed in strength, underscoring the interplay between mechanical properties and temperature in MAX materials.<sup>159,161,176</sup>

Evaluation of mechanical properties at elevated temperatures is crucial for assessing the viability of MAX phases as high-temperature materials. Thermal shock behavior, in particular, is a key aspect in this regard, wherein samples are rapidly quenched from elevated temperatures to room temperature to measure retained strength. Bai *et al.* conducted a study on  $\text{Ti}_2\text{AlC}$  and compared its thermal shock behavior with other MAX phases.<sup>182</sup> Their findings delineate four distinct regions: There's a fragile damage zone up to 300  $^\circ\text{C}$ , a robust damage zone between 300  $^\circ\text{C}$  and 500  $^\circ\text{C}$ , a steady damage zone from 500  $^\circ\text{C}$  to 1000  $^\circ\text{C}$ , and an area where strength unexpectedly rebounds above 1000  $^\circ\text{C}$  shown in Fig. 6f. Similar trends were



Table 2 Electrical and thermal characteristics of certain representative MAX phases

MAX phases	Properties						Ref.
	Electrical conductivity at RT ( $\times 10^6 \Omega^{-1} \text{ m}^{-1}$ )	Electrical resistivity ( $\times 10^{-6} \Omega \text{ m}$ )	Temperature resistivity coefficient ( $\text{K}^{-1}$ )	Thermal expansion coefficient ( $\times 10^{-6} \text{ K}$ )	Heat capacity at room temp. ( $\text{J mol}^{-1} \text{ K}^{-1}$ )	Thermal conductivity at room temp, ( $\text{W m}^{-1} \text{ K}^{-1}$ )	
Nb <sub>4</sub> AlC <sub>3</sub>	1.33	0.75	0.0025	7.2	158	13.5	161
Ta <sub>4</sub> AlC <sub>3</sub>	2.59	0.39	0.0035	8.2 $\pm$ 0.3	185	38.4	162
Ti <sub>4</sub> AlN <sub>3</sub>	0.5	2	0.0075	9.7 $\pm$ 0.2	150	12	161
Ti <sub>3</sub> AlC <sub>2</sub>	3.48	0.29	0.0031	9	—	—	162 and 163
Ti <sub>2</sub> AlC	2.5	0.4	0.002	8.2	87.2	27.0	164
Ti <sub>2</sub> AlC	4.42	0.23	0.00295	—	—	—	164
Cr <sub>2</sub> AlC	3.45	0.29	0.0028	13.3	84.4	17.9	165

observed in other MAX phases, highlighting the significance of grain size. Coarse-grained MAX phases exhibit superior thermal shock resistance compared to fine-grained counterparts. Notably, coarse-grained Ti<sub>3</sub>SiC<sub>2</sub> retained its strength even at 1400 °C quenching temperature, whereas fine-grained samples experienced significant strength loss at lower temperatures.<sup>183</sup> MAX phases demonstrate enhanced thermal shock resistance compared to traditional ceramics due to their micro-scale ductility and exceptional tolerance to damage similar to metals, attributed to the generation of kink bands and delamination during quenching processes.<sup>182</sup>

### 3.4 Property of radiation resistance

Several MAX phases, such as Ti<sub>3</sub>AlC<sub>2</sub> and Ti<sub>3</sub>SiC<sub>2</sub>, exhibit promising potential for applications in nuclear settings, serving as either fuel matrices or protective coatings due to their resilience to high temperatures and radiation damage.<sup>184,185</sup> Various types of radiation sources, methods such as heavy ions, neutrons, and protons are frequently utilized to evaluate the radiation resilience of MAX phases. The interaction between these radiation sources and MAX phases can trigger various

microstructural changes, including lattice distortions, phase shifts, micro-strain, amorphization, as well as the creation of vacancies and dislocations. Both the direct impact of incident radiation beams and secondary effects stemming from displaced atoms can contribute to radiation-induced damage, disrupting electronic interactions or bonds within MAX phases. For instance, Bowden *et al.* conducted experiments on Zr<sub>3</sub>AlC<sub>2</sub>, Nb<sub>4</sub>AlC<sub>3</sub>, and (Zr<sub>0.5</sub>, Ti<sub>0.5</sub>)<sub>3</sub>AlC<sub>2</sub>, revealing an expansion in the *c* lattice parameter following proton irradiation at elevated temperatures.<sup>186</sup> Deng *et al.* investigated the impact of C<sup>4+</sup> ions on Ti<sub>3</sub>AlC<sub>2</sub>, observing an increase in micro-strain with higher irradiation fluence and a sequential transformation from the  $\alpha$  phase to the  $\beta$  and  $\gamma$ -fcc phases. Transmission electron microscopy studies by Deng *et al.* also demonstrated the formation of defect clusters or loops in irradiated Ti<sub>2</sub>AlC and Ti<sub>3</sub>AlC<sub>2</sub> MAX phases.<sup>187</sup> Notably, Nappé *et al.* documented partial amorphization of Ti<sub>3</sub>SiC<sub>2</sub> MAX phase upon irradiation with Xe ions, as evidenced by decreased X-ray diffraction peak intensities.<sup>188</sup> Similarly, Whittle *et al.* observed amorphization in Ti<sub>3</sub>AlC<sub>2</sub> and Ti<sub>3</sub>SiC<sub>2</sub> through diffuse scattering halos in selected-area electron diffraction patterns following irradiation with Kr cations.<sup>185</sup> These findings collectively underscore the

Table 3 Mechanical characteristics of selected typical MAX phases at ambient temperature

MAX phase	Density ( $\text{g cm}^{-3}$ )	Young's modulus (GPa)	Vickers hardness (GPa)	Compressive strength (MPa)	Flexural strength (MPa)	Fracture toughness ( $\text{MPa m}^{-1/2}$ )	Reference
<b>211 phase</b>							
Ti <sub>2</sub> AlC	~4.1	—	5.8 $\pm$ 0.5	952 $\pm$ 6	432 $\pm$ 12	6.5 $\pm$ 0.2	164
V <sub>2</sub> AlC	~4.0	—	2.2 $\pm$ 0.1	527 $\pm$ 12	270 $\pm$ 12	5.7 $\pm$ 0.2	176
Cr <sub>2</sub> AlC	5.17	~282	~4.9	949 $\pm$ 22	469 $\pm$ 27	6.2 $\pm$ 0.3	175
Nb <sub>2</sub> AlC	6.44	~294	4.5 $\pm$ 0.3	—	481 $\pm$ 42	5.9 $\pm$ 0.3	174
Ta <sub>2</sub> AlC	11.46	292	4.4 $\pm$ 0.1	~804	360 $\pm$ 19	7.7 $\pm$ 0.2	177
<b>312 phase</b>							
Ti <sub>3</sub> SiC <sub>2</sub>	~4.5	~320	~4.0	~600	260 $\pm$ 20	—	178
Ti <sub>3</sub> AlC <sub>2</sub>	4.21	297	2.7–3.2	760	340	6.9–7.2	179
Ti <sub>3</sub> GeC <sub>2</sub>	5.22	340	5.0	1277	—	—	180
<b>413 phase</b>							
Ti <sub>4</sub> AlN <sub>3</sub>	4.6	310 $\pm$ 2	2.5	475 $\pm$ 15	350 $\pm$ 15	—	161
Nb <sub>4</sub> AlC <sub>3</sub>	6.97	306	2.6 $\pm$ 0.2	515 $\pm$ 44	346 $\pm$ 38	7.1 $\pm$ 0.3	162
Ta <sub>4</sub> AlC <sub>3</sub>	13.18	324	5.1 $\pm$ 0.1	821 $\pm$ 97	372 $\pm$ 20	7.7 $\pm$ 0.5	162



intricate responses of MAX phases to radiation exposure, emphasizing the need for further exploration to harness their full potential in nuclear applications.

In exploring the radiation resistance mechanisms of MAX phases, numerous factors contribute to their ability to endure radiation damage. One such exemplar is  $\text{Ti}_3\text{AlC}_2$ , where researchers have observed a sequential phase transformation during irradiation, transitioning successively through  $\alpha$ ,  $\beta$ ,  $\gamma$ , and finally to an fcc phase shown in Fig. 7. Particularly noteworthy is the reversibility of this phase evolution, demonstrated at elevated temperatures between 500 °C to 800 °C. Higher irradiation temperatures are found to support more thorough

phase recovery. Additionally,  $\text{Ti}_3\text{AlC}_2$  can maintain its lattice structure even when subjected to irradiation-induced defects, thanks to the low formation energy of Ti–Al antisite defects and carbon interstitials, allowing it to accommodate such defects effectively prevents amorphization. Moreover, the saturation of vacancy intensity beyond  $5 \times 10^{15}$  fluence, rather than exhibiting a linear increase, further fortifies  $\text{Ti}_3\text{AlC}_2$ 's resistance to amorphization and radiation damage. This suite of inherent traits collectively endows  $\text{Ti}_3\text{AlC}_2$  with exceptional resilience against irradiation and amorphization. Exploring how variations in irradiation temperature, ranging from 350 to 600 °C, affect the crystallographic stability of  $\text{Ti}_3\text{AlC}_2$ , through exposure

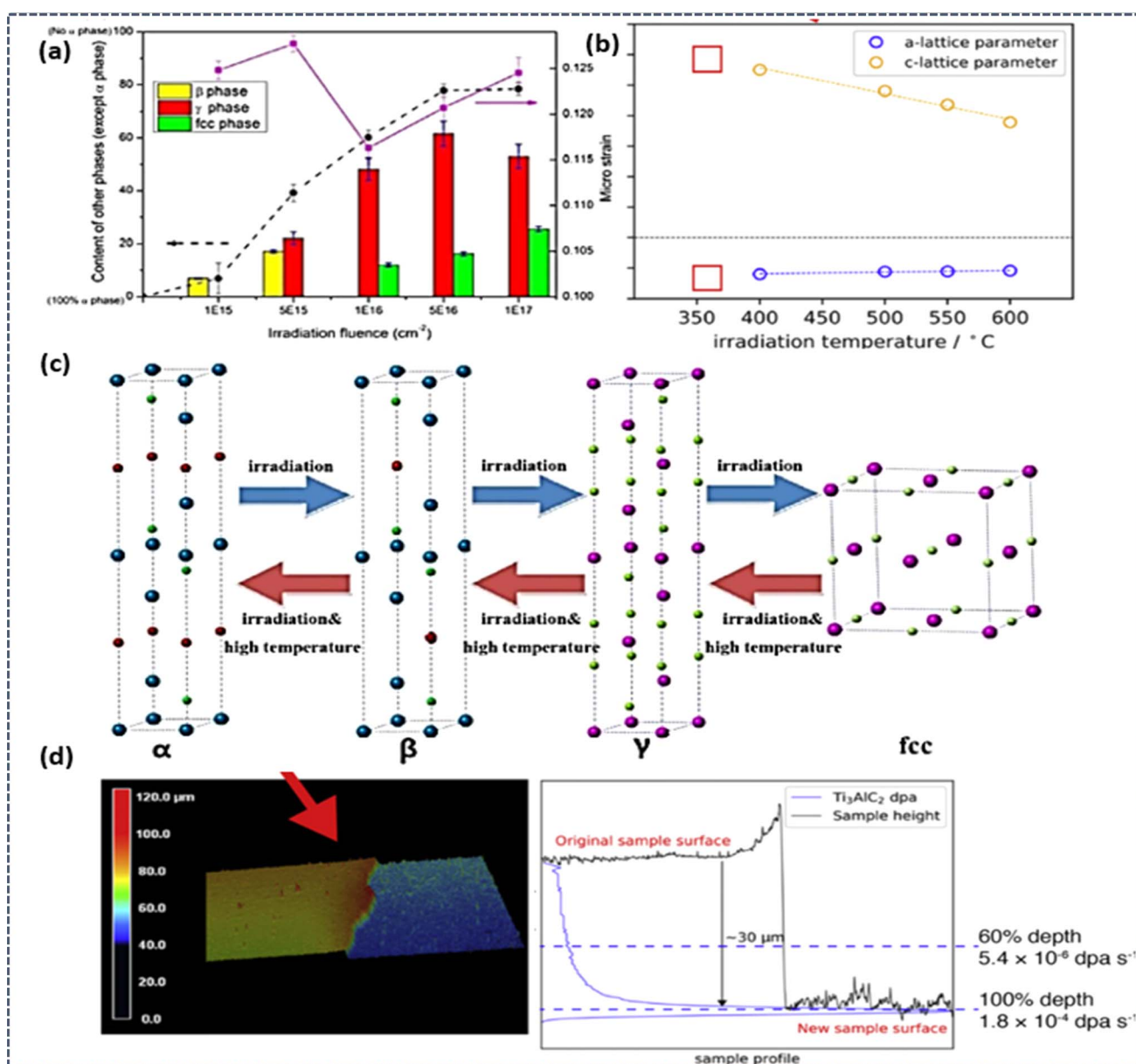


Fig. 7 Behavior of MAX phases under irradiation: (a) micro strain and phase component shifts in  $\text{Ti}_3\text{AlC}_2$  upon  $\text{C}^{4+}$  ion irradiation at room temperature across various fluences. (b) Proton irradiation induced defects cause lattice strain in MAX phase materials. (c) Phase transformation sequences and recovery in  $\text{Ti}_3\text{AlC}_2$  post-irradiation at high temperature. (d)  $\text{Ti}_3\text{AlC}_2$  has low defect recovery rate, causing the irradiated surface to exfoliate at low irradiation temperature. (Reproduced from ref. 187 with permission from Elsevier, copyright 2020).<sup>187</sup> (Reproduced from ref. 189 with permission from Elsevier, copyright 2019).<sup>189</sup>



to 2 MeV protons at a fluence of  $2.25 \times 10^{18}$  protons  $\text{cm}^{-2}$ , shows that as the irradiation temperature increases, the recovery of defects reduces the extent of anisotropic lattice alterations. However, diminished recovery at lower temperatures results in surface exfoliation and heightened damage rates. Consequently, these findings suggest that the practical application of these compositions in reactor environments may be chiefly suitable for high-temperature conditions.<sup>189</sup>

### 3.5 Property of oxidation resistance

The outstanding ability to resist high-temperature oxidation displayed by Al-containing MAX phases, like  $\text{Ti}_2\text{AlC}$ ,  $\text{Ti}_3\text{AlC}_2$ ,  $\text{V}_2\text{AlC}$ , and  $\text{Cr}_2\text{AlC}$ , underscores their promising applications in elevated temperature environments.<sup>190–193</sup> The resistance arises because of the tendency of loosely bonded aluminum components to migrate towards the surface under high temperatures. This migration facilitates the creation of a dense and uninterrupted layer of  $\text{Al}_2\text{O}_3$ , effectively blocking the inward diffusion

of  $\text{O}^{2-}$ .<sup>194,195</sup> Several factors, such as particle size, composition of the solid solution, and oxidation temperature, greatly impact the oxidation characteristics of MAX phases. For instance, increase in weight per unit of surface area initially with oxidation time at lower temperatures like 800 °C and 900 °C before reaching a plateau, while at higher temperatures like 1000 °C and 1100 °C, weight gain continues to increase as oxygen atoms penetrate deeply, establishing an advanced oxidation front shown in Fig. 8. Cubic and parabolic oxidation kinetics are observed, characterized by  $(\Delta W/S)^3 = k_{\text{ct}}$  and  $(\Delta W/S)^2 = k_{\text{pt}}$ , respectively, with cubic kinetics associated with the formation of a dense and continuous  $\text{Al}_2\text{O}_3$  layer indicative of excellent oxidation resistance. Conversely, discontinuous  $\text{Al}_2\text{O}_3$  layer formation, often accompanied by a  $\text{TiO}_2$  layer, leads to parabolic kinetics and weaker oxidation resistance.<sup>195,196</sup> Cross-sectional observations *via* SEM reveal an increase in oxide layer thickness from  $\sim 7 \mu\text{m}$  at 24 hours to  $\sim 200 \mu\text{m}$  at 500 hours of oxidation at 800 °C for  $\text{Ti}_3\text{AlC}_2$ , highlighting compositional

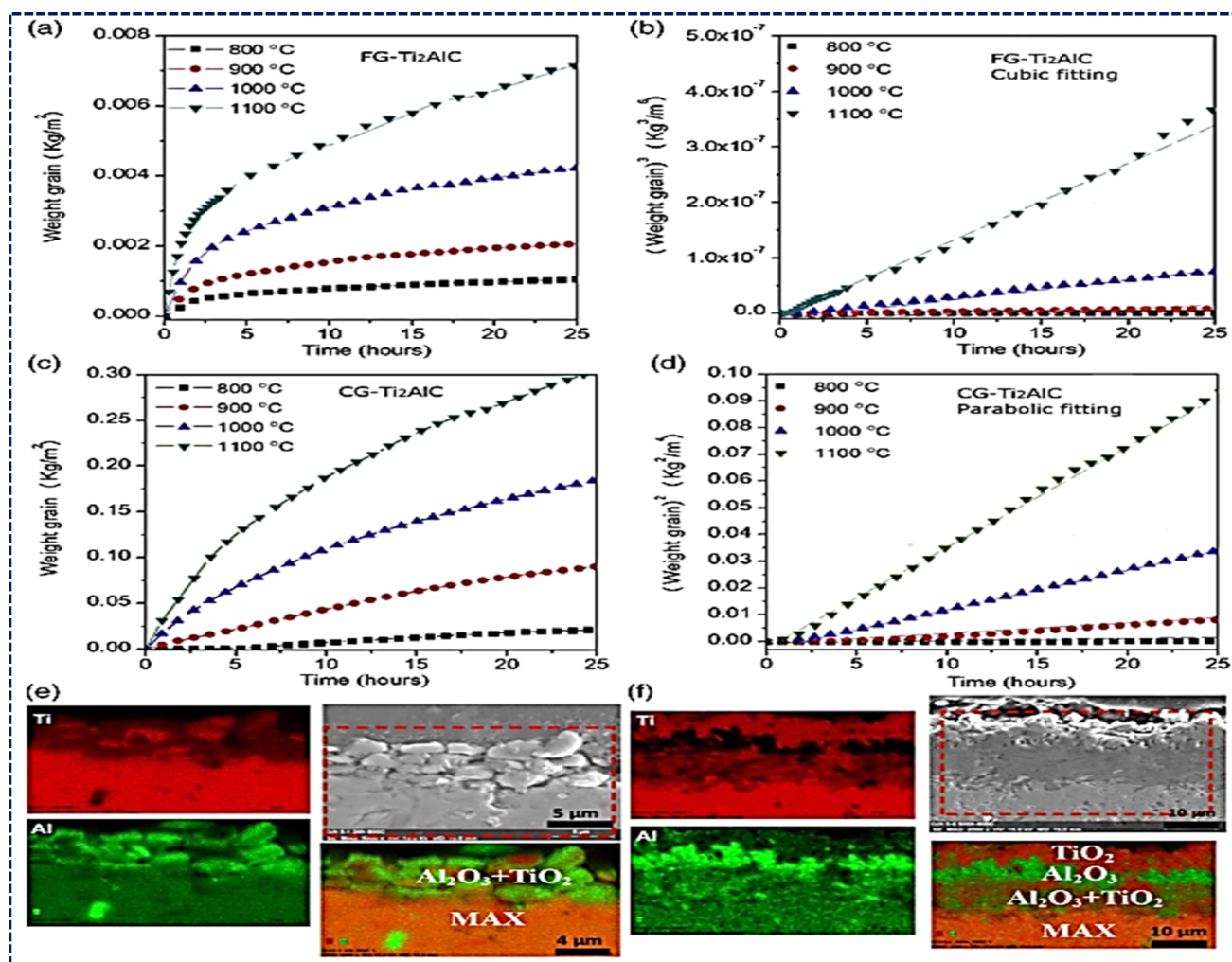


Fig. 8 MAX phases' oxidation behavior: (a and c) increase in weight per unit surface area over time due to oxidation for fine-grained (FG) and coarse-grained (CG)  $\text{Ti}_2\text{AlC}$  MAX phases at elevated temperatures. (b and d) Fitting of corresponding oxidation kinetics. (Reproduced from ref. 195 with permission from Elsevier, copyright 2020).<sup>195</sup> (e and f) SEM cross-section views of the oxide layer on  $\text{Ti}_3\text{AlC}_2$  MAX phase oxidized for 24 h (e) and 500 h (f) at 800 °C. (Reproduced from ref. 194 with permission from John Wiley and Sons, copyright 2019).<sup>194</sup>



changes driven by inward  $O^{2-}$  diffusion and outward  $Ti^{4+}$  and  $Al^{3+}$  diffusion during oxidation shown in Fig. 8.

Grain size plays a pivotal role in modifying the oxidation resistance of MAX phases, with coarse-grained structures exhibiting significantly enhanced resistance compared to their fine-grained counterparts. For instance, fine-grained  $Ti_2AlC$  displays cubic oxidation kinetics, with a cubic rate constant of  $8.3 \times 10^{-13} \text{ kg}^3 \text{ m}^{-6} \text{ s}^{-1}$  at  $1000^\circ\text{C}$ , while coarse-grained  $Ti_2AlC$  follows parabolic oxidation kinetics shown in Fig. 6d, with a rate constant of  $4.0 \times 10^{-7} \text{ kg}^2 \text{ m}^{-4} \text{ s}^{-1}$  under the same conditions.<sup>191,195</sup> This disparity results from fine-grained  $Ti_2AlC$  having a higher density of grain boundaries and more Al diffusion pathways, which promote the creation of a protective  $Al_2O_3$  layer. Conversely, in coarse-grained  $Ti_2AlC$ , Al diffusion and the formation of the protective  $Al_2O_3$  layer are constrained. Drouelle *et al.* conducted a comparative study on the oxidation resistance of  $Ti_3AlC_2$  and  $Ti_3(Al_{0.8}Sn_{0.2})C_2$  solid solution, revealing that the oxidation kinetics of  $Ti_3(Al_{0.8}Sn_{0.2})C_2$  are notably higher than those of  $Ti_3AlC_2$ .<sup>194</sup> This disparity is attributed to the facile diffusion of Sn atoms in  $Ti_3(Al_{0.8}Sn_{0.2})C_2$ , leading to the formation of nonprotective and rapidly growing  $SnO_2$  oxide at approximately  $460^\circ\text{C}$ . Bei *et al.* have also obtained similar results, supporting the important impact of solid solution composition and grain size on the oxidation behavior of MAX phases.<sup>197</sup>

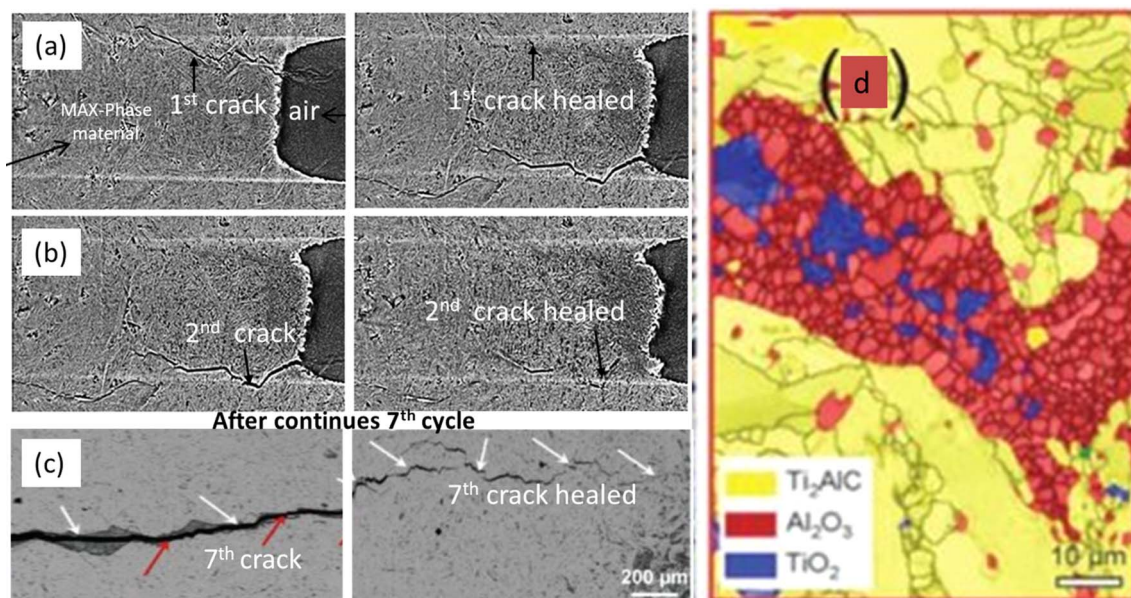
### 3.6 Crack healing properties

The scientific community has shown considerable interest in the crack healing capabilities of MAX phase materials because of their distinct blend of metallic and ceramic characteristics. These materials, which form a class of layered ceramics,

demonstrate exceptional high-temperature mechanical strength, thermal stability, and outstanding oxidation resistance. This review endeavors to provide a thorough summary of the fundamental mechanisms accountable for the crack healing characteristics observed in MAX phase materials. Our focus will encompass a detailed examination of various contributing factors such as microstructural evolution, interfacial chemistry, and mechanical characteristics.

The crack propagates along the basal planes of the hexagonal  $Ti_2AlC$ 's randomly oriented lamellar grains, creating a zigzag pattern and leaving smooth cleavage fracture surfaces locally. When the crack deflects perpendicular to the basal planes, it produces a stair-like fracture surface. Features such as local crack branching, crack bridging, and grain pull-out are characteristic of this material. The high toughness of  $Ti_2AlC$  is attributed to the simultaneous operation of multiple deformation and cracking mechanisms. The local variations in crack opening are influenced by the differences in grain orientations along the crack path, affecting the local deformation and failure processes. This Fig. 9 illustrates the progression of crack growth and healing steps in  $Ti_2AlC$  at  $1500 \text{ K}$  in air from 1st to 8th cycle and provides an SEM image of the healed-damage zone, obtained using electron backscatter diffraction, highlighting the microstructural changes associated with the healing process.<sup>198</sup>

Previous research within the Ti–Al–C system has revealed the capacity of MAX phases to “heal” cracks. This self-healing process entails subjecting  $Ti_2AlC$  or  $Ti_3AlC_2$  to heat treatment in an oxidative environment, resulting in the deposition of  $TiO_2$  and  $Al_2O_3$  oxidation products within the cracks. This in turn (partially) restores the strength of the material.<sup>199</sup> Similar observations have been reported for  $Cr_2AlC$ , thus indicating



**Fig. 9** Images depict the fracture and crack healing process in  $Ti_2AlC$  from the 1st to the 8th cycle. (a) Shows the first crack and its healed state. (b) Illustrates the second crack and its healed state. (c) Displays the crack path after seven healing cycles and subsequent fracture, with red arrows pointing to the remnants of the crack. (d) Presents an SEM image of the healed-damage zone captured using electron backscatter diffraction. (Reproduced from ref. 198 with permission from Springer Nature, copyright 2016).<sup>198</sup>





a wider applicability of the crack healing phenomenon within the MAX phase family.<sup>200</sup> In an attempt to identify additional MAX phases that could exhibit this self-healing behavior, Farle *et al.* highlighted several thermodynamic and mechanical requirements. As a result,  $V_2AlC$ ,  $Ti_3SiC_2$ , and  $Zr_2AlC$  were identified as promising candidates for further investigation.<sup>201</sup> A more recent study showcased the crack healing abilities of  $Ti_2SnC$ , specifically in response to thermal shock-induced cracks.<sup>202,203</sup> Treatment of these materials in air led to the formation of  $TiO_2$ ,  $SnO_2$ , and metallic Sn, which effectively filled the cracks and restored the material's strength. This example serves to underscore the broader application of crack healing beyond commonly studied elements such as Al and Si. A thorough exploration of the crack healing capabilities in MAX phase materials could lead to the development of highly resilient, durable materials with numerous potential applications in high-temperature environments.

### 3.7 Magnetic properties

Since the pioneering synthesis of the first magnetic MAX phase, characterized by a heteroepitaxial single-crystal thin film comprising  $(Cr_{0.75}Mn_{0.25})_2GeC$ ,<sup>204</sup> the exploration of magnetic MAX materials has flourished. Subsequent investigations have unveiled a diverse array of magnetic MAX phases, such as  $(V, Mn)_3GaC_2$ ,  $Cr_2AlC$ ,  $Cr_2GeC$ , and  $Mn_2GaC$ ; and  $(Cr, Mn)_2AlC$ ,  $Cr_2GeC$ , and  $(Cr, Mn)_2GaC$ ; and  $(Mo, Mn)_2GaC$ , predominantly centered around chromium and manganese substitutions.<sup>205</sup> A significant breakthrough occurred when Tao and colleagues introduced rare earth (RE) elements into  $Mo_2AlC$ -based i-MAX phases, leading to the discovery of a novel class of magnetic i-MAX phases denoted as  $(Mo_{2/3}RE_{1/3})_2AlC$ , with RE comprising Ce, Pr, Nd, Sm, Gd, Tb, Dy, Ho, Er, Tm, and Lu.<sup>206</sup> These innovative phases exhibited a distinctive microstructure characterized *via* quasi-2D magnetic frustrated triangular lattice bilayers on top of a Mo honeycomb configuration, resulting in complex magnetic orders arising from intricate intra- and in-plane magnetic interactions. More recently, the exploration of magnetic MXenes has emerged, with notable works such as the synthesis of  $Ti_3C_2$  MXene containing a small fraction of silicon carbide, exhibiting a combination of ferromagnetic and diamagnetic properties suitable for potential applications in spintronics devices.<sup>207</sup> Additionally, investigations into the magnetic transitions of MAX phases, exemplified by the transition observed in  $Cr_2TiC_{2-x}$ , have shed light on the complex magnetism inherent in these materials. Theoretical studies have played a pivotal role in elucidating the magnetic properties of MAX phases, offering insights into their stability and electronic structures. For instance, theoretical predictions have highlighted Fe-based MAX phases, particularly  $Fe_3AlC_2$ , as promising candidates for ferromagnetic behavior, although experimental confirmation remains elusive.<sup>208</sup> Computational approaches, such as density functional theory (DFT) and DFT + U methods, have enabled researchers to unravel the underlying mechanisms governing magnetism in MAX phases, revealing the dominant contribution in Cr-containing MAX phases of Cr 3d valence electrons to the magnetic moments.<sup>130</sup> Furthermore, theoretical calculations have elucidated the

influence of structural factors, such as intercalated nonmagnetic slabs, on the magnetic properties of MAX phases, exemplified by the enhanced magnetic moments observed in  $(Cr_2Ti)AlC_2$  compared to  $Cr_2AlC$  due to the larger interatomic distances between out-plane Cr atoms. Bulk Mn- and Fe-substituted  $Cr_2AlC$  samples were prepared for the study Fig. 10 shows the magnetization data for the Mn (a) and Fe (b) substituted samples,  $(Cr_{1-x}Mn_x)_2AlC$  and  $(Cr_{1-x}Fe_x)_2AlC$ , with nominal compositions ranging from  $x = 0$  to  $x = 0.15$  and  $x = 0$  to  $x = 0.075$ , respectively.<sup>209</sup> These multifaceted investigations underscore the intricate interplay between composition, structure, and magnetism in MAX phases, paving the way for the design and exploration of novel magnetic materials with tailored properties and functionalities.

### 3.8 Resistance against corrosion in liquid metals

The evaluation of MAX phase materials for potential applications in lead-cooled fast reactors (LFRs) of Generation IV necessitates a thorough understanding of their corrosion resistance in contact with heavy liquid metal (HLM) primary coolants such as lead (Pb) and lead-bismuth eutectic (LBE). Unlike conventional stainless steels, which are susceptible to dissolution corrosion when most MAX phases come into contact with liquid LBE, they behave inertly at high temperatures ( $>450$  °C) and low HLM oxygen concentrations ( $CO < 10$ –8 mass%).<sup>210</sup> This inherent liquid metal corrosion (LMC) resistance renders MAX phases highly promising for structural components in Gen-IV LFRs. Recent experiments involving commercially available MAX phase ceramics, exposed to liquid Pb and LBE at reactor-relevant temperature ranges, such as Maxthal® 312 and Maxthal® 211, have shown no corrosion effects that would jeopardize their structural integrity. Notably,  $Ti_3SiC_2$  exhibited thin rutile  $TiO_2$  formation, while  $Ti_2AlC$  ceramic showed dissolution of the  $TiAl$  phase resulting in LBE ingress.<sup>211</sup> Lapauw *et al.* (2019) conducted stability tests on 11 MAX phase ceramics in oxygen-depleted liquid LBE at 500 °C, revealing either intrinsic resistance to LBE attack or passivation *via* nanometric  $Al_2O_3$  or  $SiO_2$  oxide scales.<sup>133,212</sup> The susceptibility of MAX phases to LBE interaction was observed in  $Ti_2SnC$  and Zr-rich MAX phases, emphasizing the significance of phase purity on LMC resistance. Despite local LBE interaction with MAX phase grains, surface integrity was maintained, with attacked Zr-rich MAX phase grains transforming into MAX phase solid solutions. Additionally, experiments conducted under fast-flowing LBE conditions resulted in the formation of oxide scales on MAX phase ceramics, while reference structural materials such as solution-annealed 316L stainless steels showed erosion damage shown in Fig. 11, further highlighting the favorable corrosion resistance properties of MAX phases in liquid metal environments (Table 4).<sup>123,133</sup>

### 3.9 Microwave absorbing properties

In the realm of microwave absorbing materials, while carbon materials have traditionally held sway, their susceptibility to oxidation under high temperatures has constrained their



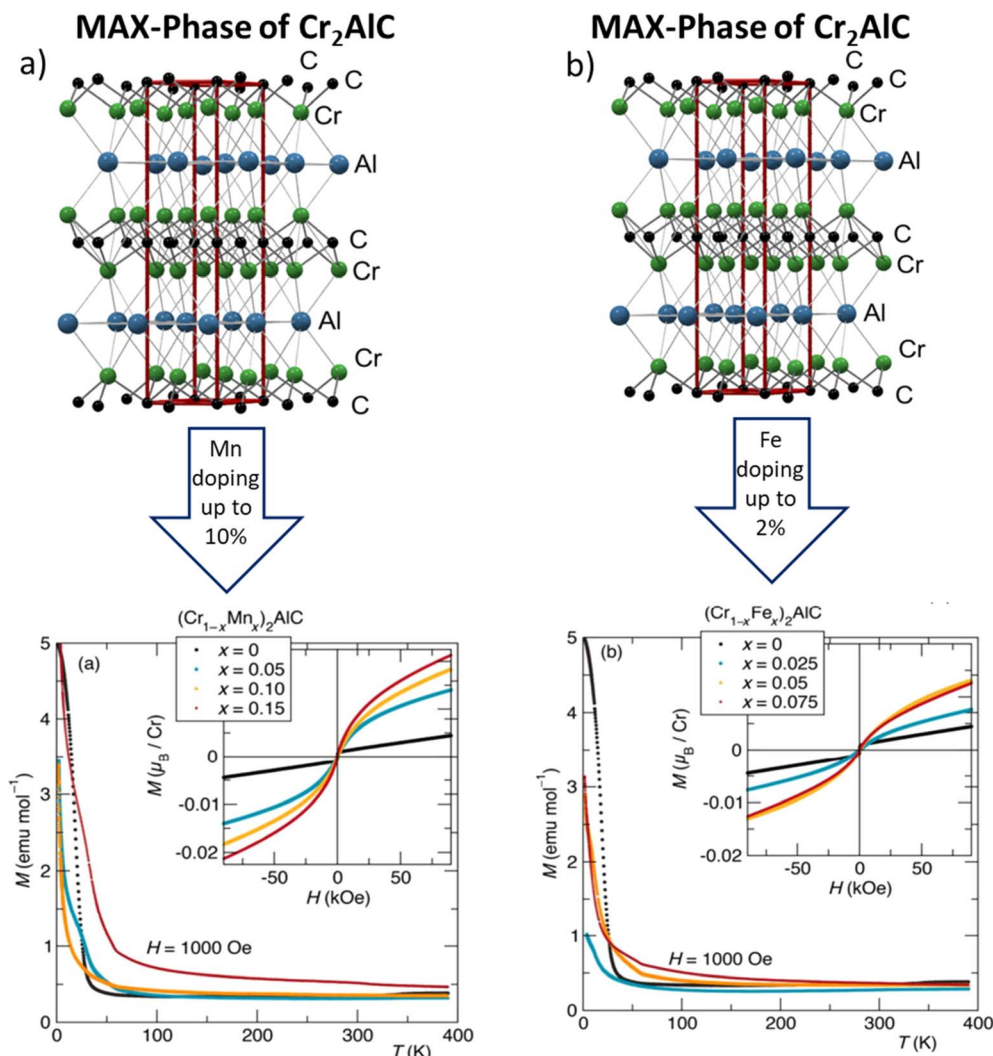


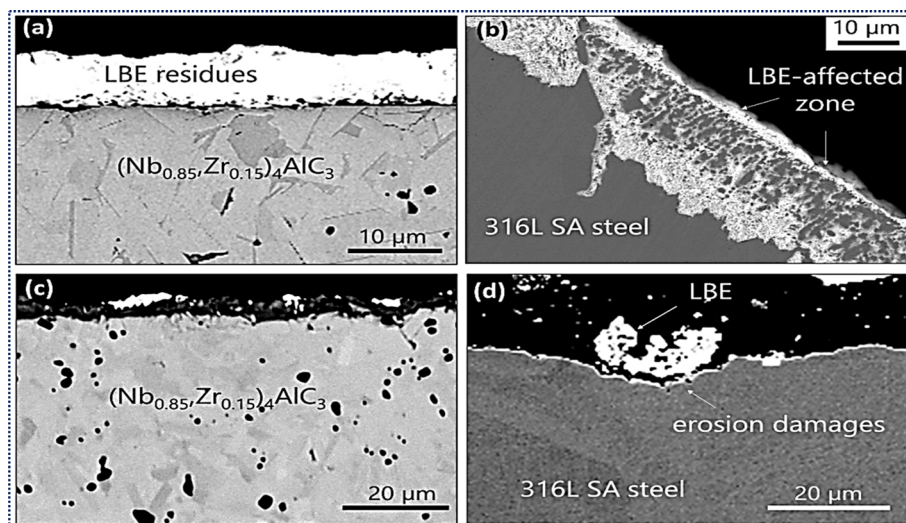
Fig. 10 Magnetization data for the Mn (a) and Fe (b) substituted samples,  $(\text{Cr}_{1-x}\text{Mn}_x)_2\text{AlC}$  and  $(\text{Cr}_{1-x}\text{Fe}_x)_2\text{AlC}$ , with nominal compositions. (Reproduced from ref. 209 with permission from The Royal Society of Chemistry, copyright 2017).<sup>209</sup>

widespread application. However, MAX phases, renowned for their exceptional thermal stability and versatile properties, have emerged as promising contenders for microwave absorption, particularly in elevated temperature settings. Beginning with the investigation of  $\text{Ti}_3\text{SiC}_2$  MAX phase's microwave dielectric properties, researchers have delved into understanding its potential. Studies by Li *et al.* revealed the influence of  $\text{Ti}_3\text{SiC}_2$  purity on its microwave absorbing characteristics, with higher purity variants exhibiting superior complex permittivity and dielectric loss.<sup>218</sup> Subsequent research efforts have focused on enhancing  $\text{Ti}_3\text{SiC}_2$  purity through Al doping, yielding notable improvements in permittivity.<sup>219</sup> Moreover, the incorporation of  $\text{Ti}_3\text{SiC}_2$  into composite materials has yielded intriguing results. For instance,  $\text{Ti}_3\text{SiC}_2$ /cordierite composites demonstrated effective microwave absorption, achieving significant absorption bandwidths. Additionally, the exploration of other MAX phases, such as  $(\text{Cr}_{2/3}\text{Ti}_{1/3})_3\text{AlC}_2$ , has unveiled further potential.<sup>220,221</sup> Yao *et al.*'s investigation into  $(\text{Cr}_{2/3}\text{Ti}_{1/3})_3\text{AlC}_2$ 's microwave absorption properties underscored the importance of particle size and matrix thickness in influencing absorption

efficacy. Notably, at specific thicknesses and frequencies,  $(\text{Cr}_{2/3}\text{Ti}_{1/3})_3\text{AlC}_2$  showcased remarkable microwave absorption capabilities, suggesting its viability for practical applications in the X-band frequency range.<sup>222</sup>

The future path of MAX phases is poised for remarkable advancements in their electrical and thermal properties. As researchers continue to explore these materials, a deeper understanding of the mechanisms underlying their conductivity and thermal behaviors will be achieved. Variations in electronic conductivity, influenced by composition and microstructural factors, will likely be fine-tuned for specific applications, improving performance in various technological fields. For example, minimizing lattice defects such as vacancies and dislocations will reduce electron scattering, thereby enhancing electrical conductivity. The temperature-dependent nature of MAX phases' resistivity and conductivity will be harnessed to develop materials with tailored properties for high-temperature electronics and thermal management systems. Innovations in synthesis methods, such as optimizing self-propagating high-temperature synthesis (SHS) and hot isostatic pressing (PHIP),





**Fig. 11** Materials exposed for 1000 hours at 500 °C to oxygen-deficient, static LBE: (a) solid solution in the MAX phase  $(\text{Nb}_{0.85}, \text{Zr}_{0.15})_4\text{AlC}_3$ , (b) stainless steel 316L SA. Materials subjected for 1000 hours at 500 °C to fast-slowing, oxygen-deficient LBE: (c)  $(\text{Nb}_{0.85}, \text{Zr}_{0.15})_4\text{AlC}_3$  (d) 316L SA stainless steel;  $4\text{AlC}_3$  MAX phase solid solution. (Reprinted from ref. 213 with permission from Elsevier, copyright 2021).<sup>213</sup>

**Table 4** Summary of literature studies on the exposure of MAX phases to liquid Pb and LBE

MAX phase	Pb/LBE	Time (kh)	<i>T</i> (°C)	Flow	Interaction	CO (wt%)	Ref.
$\text{Ti}_3\text{AlC}_2$	LBE	3.5	500	Static	Local GB penetration	$10^{-10}$	133
$(\text{Ti}, \text{Nb})_2\text{AlC}$	LBE	3.5	500	Static	No interaction	$10^{-10}$	133
$\text{Nb}_2\text{AlC}$	LBE	3.5	500	Static	No interaction	$10^{-10}$	133
$\text{Nb}_4\text{AlC}_3$	LBE	3.5	500	Static	No interaction	$10^{-10}$	133
$(\text{Nb}_{0.85}\text{Zr}_{0.15})_4\text{AlC}_3$	LBE	1	500	Static	No interaction	$\sim 10^{-11}$	133
				$\sim 8 \text{ ms}^{-1}$	3–4 $\mu\text{m}$ $\text{Nb}_2\text{O}_5$ -based scale	$5 \times 10^{-9}$	
$\text{Ti}_3\text{SiC}_2$	LBE	1	700	Static	No interaction	$5 \times 10^{-6}$	214
	LBE	3	550/650	Static	$\text{TiO}_2$ (rutile)	$10^{-6}/10^{-8}$	130
	LBE	1/3	550/650	Static	$\text{TiO}_2$ (rutile), local surface disintegration	$10^{-6}/10^{-8}$	211
		5/10	700				
	LBE	3.5	500	Static	No interaction	$10^{-10}$	133
	Pb	1	650/800	—	No interaction	$^a 10^{-12}$	215
	Pb	0.5	550/600	Static	$\text{TiO}_2$ (rutile) formation	$10^{-6}/10^{-8}$	216
		2/4	750				
	Pb	2	500	$1 \text{ ms}^{-1}$	Thin oxide layer	$10^{-6}$	217
$\text{Zr}_2\text{AlC}$	LBE	1	500	Static	Penetration of LBE into MAX phase resulting in the formation of $\text{Zr}_2(\text{Al}, \text{Bi}, \text{Pb})\text{C}$	$\sim 10^{-11}$	133
				$\sim 8 \text{ ms}^{-1}$	Mild $\text{ZrO}_2$ formation	$5 \times 10^{-9}$	
$\text{Zr}_3\text{AlC}_2$	LBE	1	500	Static	Penetration of LBE into MAX phase resulting in the formation of $\text{Zr}_3(\text{Al}, \text{Bi}, \text{Pb})\text{C}$	$\sim 10^{-11}$	133
				$\sim 8 \text{ ms}^{-1}$	Severe $\text{ZrO}_2$ formation	$5 \times 10^{-9}$	
$\text{Ti}_2\text{AlC}$	LBE	1/3 5/10	550/650 700	Static	$\text{TiO}_2$ (rutile) & $\text{Al}_2\text{O}_3$ formation (CO = $10^{-6}$ ) dissolution of secondary phases (CO = $10^{-8}$ , $T = 650, 750$ °C)	$10^{-6}/10^{-8}$	211
	LBE	3.5	500	Static	No interaction	$10^{-10}$	133
	Pb	1	650/800	—	No interaction	$^a 10^{-12}$	215
$(\text{Zr}_{0.8}, \text{Ti}_{0.2})_2\text{AlC}$ & $(\text{Zr}_{0.8}, \text{Ti}_{0.2})_3\text{AlC}_2$	LBE	1	500	Static	When LBE penetrates the MAX phase, the intermetallic $(\text{Zr}_{0.8}, \text{Ti}_{0.2})_{n+1}(\text{Al}, \text{Pb}, \text{Bi})\text{Cn}$ production dissolves	$10^{-11}$	133
$\text{Ti}_2\text{SnC}$	LBE	1	500	Static	LBE penetration through grain boundaries with secondary Sn phase attacked at grain boundaries	$10^{-11}$	133

<sup>a</sup> Denotes a calculated CO value.





will lead to more consistent and high-quality MAX phase materials with superior electrical and thermal conductivities. Additionally, the interplay between electrons and phonons in thermal conductivity will be better understood, allowing for the design of MAX phases with enhanced heat dissipation capabilities. As these materials continue to be refined, their applications in fields like aerospace, energy, and electronics will expand, leveraging their unique combination of metallic and ceramic properties.

## 4. Synthesis of MAX phases

### 4.1 Synthesis techniques (bottom-up vs. top-down approaches)

Synthesis techniques play a pivotal role in defining the characteristics of MAX phases, with bottom-up and top-down approaches offering distinct pathways for material synthesis and customization. The characterization of MAX phases, innovative materials bridging the gap between metals and ceramics with their distinctive layered structure, heavily relies on the

synthesis techniques applied. These methods, classified as either bottom-up or top-down approaches, significantly influence the elemental composition and structural attributes of the resultant materials. Traditional MAX phases, adhering to the space group  $P6_3/mmc$  and comprising an early transition metal (M), an A-group element (A) from groups 12 to 16, and additional elements like carbon, nitrogen, boron, or phosphorus(x), are commonly synthesized through bottom-up methodologies. While upholding Nowotny's seminal findings, this category has evolved to encompass materials with higher  $n$  values and, more recently, boron-containing phases, emphasizing the adaptability of the approach in generating intricate compositions.<sup>223</sup> Bottom-up synthesis encompasses direct techniques such as powder metallurgy and thin film deposition, yielding a wide array of MAX phases, including ternary compositions, alloys, and multi-element solids with significant disorder on the M sites, such as high entropy MAX phases. This method facilitates the inclusion of A-site elements beyond conventional groups, thereby expanding the spectrum of achievable material

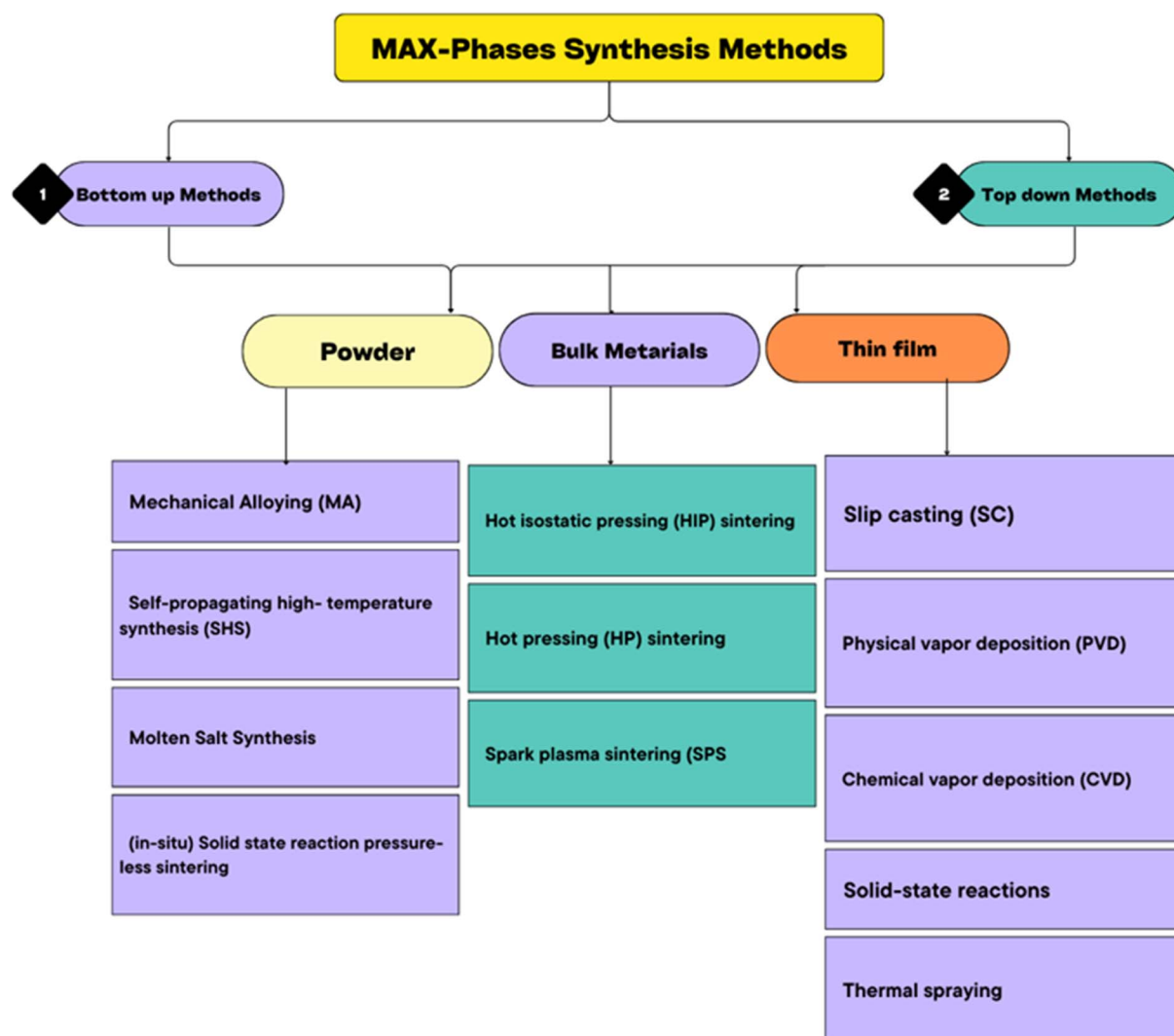


Fig. 12 An illustration of the methods used to synthesize MAX phases presented in a flowchart format.



properties.<sup>224,225</sup> Conversely, top-down synthesized MAX phases involve modifying the A-group layers post-synthesis, rather than altering their initial chemical composition.<sup>226</sup> Derived from a bottom-up synthesized precursor, these materials undergo partial or complete replacement of the A-layer through subsequent treatments, demonstrating the method's potential for tailoring material properties. The dichotomy between bottom-up and top-down synthesis of MAX phases underscores the versatility and complexity of these materials, highlighting the crucial role of synthesis techniques in shaping their structure, composition, and ultimately, their properties.<sup>227</sup>

Over the past two decades, significant endeavors have been invested in advancing the synthesis and characterization of MAX phases. Fig. 12 provides a detailed flowchart depicting the various synthesis methods employed to produce MAX-phase materials. Addressing the synthesis of MAX phase ceramics proves to be a noteworthy challenge, with a limited selection of commercially available powder sources in the market, encompassing compositions such as  $\text{Ti}_3\text{SiC}_2$ ,  $\text{Ti}_2\text{AlC}$ ,  $\text{Ti}_3\text{AlC}_2$ ,  $\text{V}_2\text{AlC}$ , and  $\text{Nb}_2\text{AlC}$ . Notably, the absence of commercially available bulk MAX phase ceramics has been conspicuous. The synthesis approaches for MAX phases can be broadly categorized into powder, bulk, and thin film methods, with a comprehensive overview presented in Table 5. It is interesting to note that a majority of observed MAX phases are commonly produced in a highly polycrystalline form, although a few instances report thin single crystalline layers<sup>245</sup> or single-crystalline platelets.<sup>246</sup> The synthesis of bulk single crystals has become a pivotal strategy for exploring the anisotropic physical properties of MAX phases. However, until recently, the synthesis of bulk single crystals presented a considerable challenge, impeding in-depth investigations into their physical properties. A significant breakthrough in 2011, led by the LMGP team, successfully developed a method for producing single crystal MAX phases,<sup>247,248</sup> unlocking new avenues for research in a field that already commands intense international interest and research activity.

## 4.2 MAX phase powders

In the realm of MAX phase powder synthesis, various production methodologies have been explored, each contributing to the versatility of the field. The self-propagating high-temperature synthesis (SHS) technique has found application in the production of Maxthal 211 and 312, showcasing its efficacy.<sup>229,230</sup> Microwave synthesis and molten salt routes have also been pivotal in MAX phase powder synthesis. Notably, molten salt synthesis from elemental powders has proven successful in obtaining MAX phase powders like  $\text{Ti}_2\text{AlC}$ ,  $\text{Ti}_3\text{AlC}_2$ , and  $\text{Cr}_2\text{AlC}$ .<sup>231,249,250</sup> The use of different molten salt compositions, such as KBr, NaCl/KCl mixtures, and NaCl/KCl, allows for the tailored synthesis of specific phases. Moreover, electrosynthesis emerges as a viable approach, enabling the transformation of oxide/carbon precursors into MAX phase powders in molten salt environments. For instance,  $\text{TiO}_2/\text{Al}_2\text{O}_3/\text{C}$  precursor pellets can be used to produce  $\text{Ti}_3\text{AlC}_2$  powder at 900 °C and 3.1 V in molten  $\text{CaCl}_2$ , whereas  $\text{Cr}_2\text{AlC}$  precursor pellets can be used to produce  $\text{Cr}_2\text{AlC}$  powder at 700 °C and 3 V in molten NaCl- $\text{CaCl}_2$ .<sup>251,252</sup> Alternatively, method for producing MAX phase powder is through the comminution of bulk materials that have undergone reactive synthesis, further diversifying the available synthesis routes.

## 4.3 MAX phase bulk ceramics

In recent years, the development of bulk processing techniques for MAX phase ceramics has seen significant advancements. Powder metallurgy stands out as the predominant method, necessitating a meticulous fusion of the starting powder constituents. Within this domain, various approaches have emerged, ranging from conventional methods like CS or microwave sintering conducted under protective atmospheres to more sophisticated techniques such as hot isostatic pressing (HIP),<sup>233–235</sup> hot pressing (HP),<sup>236,237</sup> spark plasma sintering (SPS),<sup>238,239</sup> single-crystal growth<sup>253</sup> and mechanical alloying (MA). Haemers *et al.* provided a comprehensive review of the

Table 5 Synthesis of various forms of MAX phases

Category	Method	Example	Reference
Powder	Mechanical alloying (MA)	$\text{Ti}_3\text{SiC}_2$	228
	Self-propagating high-temperature synthesis (SHS)	$\text{Ti}_3\text{AlC}_2$	229
		$\text{Ti}_2\text{AlC}$	230
	Molten salt synthesis	$\text{Ti}_3\text{AlC}_2$	231
	( <i>In situ</i> ) solid state reaction pressure-less sintering	$\text{Ti}_3\text{SiC}_2$	232
Bulk materials (polycrystalline MAX and its composites)	Hot isostatic pressing (HIP) sintering	$\text{Ti}_3\text{SnC}_2$ , $\text{Ti}_2\text{SnC}$	233
		$\text{Hf}_2\text{PbC}$ , $\text{Zr}_2\text{PbC}$	234
		$\text{V}_2\text{AlC}$	235
	Hot pressing (HP) sintering	$\text{Cr}_2\text{AlC}$	236
		$\text{Nb}_2\text{AlC}$	237
	Spark plasma sintering (SPS)	$\text{Ti}_3\text{SiC}_2$	238
		$\text{Ti}_2\text{AlC}$	239
	Slip casting (SC)	$\text{Ti}_3\text{AlC}_2$	240
Thin film	Physical vapor deposition (PVD)	$\text{Ti}_3\text{GeC}_2$ , $\text{Ti}_2\text{GeC}$	241
	Chemical vapor deposition (CVD)	$\text{Ti}_3\text{SiC}_2$	242
	Solid-state reactions	$\text{Ti}_2\text{AlN}$	243
	Thermal spraying	$\text{Ti}_2\text{AlC}$	244



synthesis protocols for the most prevalent layered carbide and nitride MAX phases, shedding light on the intricate processes involved.<sup>254,255</sup> Bulk synthesis techniques are often categorized based on their synthesis routes, distinguishing between pressure less methods like CS and SHS, and pressure-assisted techniques like HIP, HP, and SPS. Among these, the latter group has demonstrated greater efficacy in synthesizing various members of the MAX phase family, particularly those of higher orders like Nb<sub>4</sub>AlC<sub>3</sub>, which have been exclusively reported through HP or SPS synthesis routes.

Notably, the synthesis of MAX phases involves complex thermodynamic considerations, especially regarding the temperature requirements for the formation of different MAX phase compositions. For instance, MAX phases with a higher 'n' in the M<sub>n+1</sub>AX<sub>n</sub> formula demand elevated formation temperatures compared to those with smaller 'n' layers in the same ternary system. This nuanced understanding has enabled the targeted synthesis of specific MAX phases like Ti<sub>3</sub>AlC<sub>2</sub>, Nb<sub>4</sub>AlC<sub>3</sub>, and Ta<sub>4</sub>AlC<sub>3</sub> through annealing processes tailored to their respective ternary systems.<sup>243</sup> However, at elevated temperatures, MAX phase decomposition becomes a competing reaction, leading to the breakdown of M<sub>n+1</sub>AX<sub>n</sub> into M<sub>n+1</sub>X<sub>n</sub> and A components.

The M-A bond, the weakest in MAX phases, tends to break first at high temperatures, leading to outward diffusion of the A-element. Pressure-assisted techniques offer a notable advantage by enclosing the material in a die/punch system or metal capsule, thus reducing A-element loss. This assertion finds support in a study where a ternary powder mixture was embedded in Al<sub>4</sub>C<sub>3</sub>, resulting in a significant enhancement in Ti<sub>3</sub>AlC<sub>2</sub> formation during pressure less sintering.<sup>256</sup> To discuss synthesis routes and process parameters, the ternary Ti-Al-C system is chosen, housing two extensively researched MAX phases: Ti<sub>2</sub>AlC and Ti<sub>3</sub>AlC<sub>2</sub>. Self-propagating high-temperature synthesis (SHS) emerges as the most cost-effective method for MAX phase production, being efficient in time and energy, requiring minimal infrastructure, and scalable for industrial use. Although exothermal, with the powder bed igniting and a reaction front advancing through it, SHS often yields competing phases like TiC.<sup>257</sup> While commonly employing elemental powders, alternative combinations like M-oxides, Al, and Al<sub>4</sub>C<sub>3</sub> have been explored, albeit with limited process control and product predictability. Conventional sintering, conducted under protective atmospheres or vacuum, offers better control and scalability. It has been successfully applied to various ternary and quaternary MAX phases. Pressure less sintering can be coupled with mechanical alloying (MA) to introduce elements like Cu into MAX phase structures, as demonstrated by Lyu *et al.*<sup>258</sup>

Furthermore, microwaves offer an alternative heat source. During microwave sintering, grain orientation in the Ti<sub>2</sub>AlN MAX phase was shown to be favored during growth, although the underlying mechanism remains incompletely understood.<sup>259</sup> Hot isostatic pressing (HIP) and reactive hot pressing (HP) have been extensively employed in the synthesis of high purity, dense Ti<sub>2</sub>AlC and Ti<sub>3</sub>AlC<sub>2</sub> on a laboratory scale within the Ti-Al-C system. Key process parameters include the chemistry and stoichiometric ratio of the starting powders, sintering

temperature (typically ranging from 1200 °C to 1500 °C), dwell time (0.5 to 16 hours), pressure (30 to 70 MPa), and optionally, a heat treatment at lower temperatures. While elemental powders are commonly used as starting materials, binary compounds like TiC<sub>x</sub>, Al<sub>4</sub>C<sub>3</sub>, and TiH<sub>2</sub> are also utilized.<sup>260</sup> When compared to fine pure Ti powder, TiH<sub>2</sub> is a less pyrophoric and more cost-effective source of Ti,<sup>261</sup> dehydrogenating *in situ* around 600 °C. Although Al<sub>4</sub>C<sub>3</sub> is noted for its effectiveness as a source of Al and C in the Ti-Al-C MAX phase synthesis, this carbide's hygroscopic nature causes parasitic phases like Al<sub>2</sub>O<sub>3</sub> to exist in the finished product.<sup>262</sup> Processing cycles that are comparatively slow limit HP and HIP and a restricted amount of material per run, rendering these techniques, particularly HIP, costly. Because Spark Plasma Sintering (SPS), sometimes called PDS or FAST, has shorter dwell durations of only a few minutes and higher heating and cooling rates, it can speed up processing. Furthermore, SPS synthesis temperatures have been observed to be normally 50–200 °C lower than those of hot pressing. As an illustration, another research team combined mechanical alloying (MA) with SPS at 1050 °C to synthesize dense Ti<sub>3</sub>AlC.<sup>263</sup> It is uncertain whether this inconsistency with traditional methods such as HP or HIP is due to the process's nature, increased diffusion caused by current flow, or simply a result of the temperature measurement technique used.

#### 4.4 MAX phase thin film

In the realm of MAX phase coating synthesis, the exploration of various deposition techniques has been pivotal, particularly from the perspective of thin films. Notably, three primary methods have gained prominence: physical vapor deposition (PVD) utilizing elemental dc sputtering, cathodic arc deposition or magnetron sputtering,<sup>241</sup> and chemical vapor deposition (CVD).<sup>242</sup> Additionally, solid-state reaction synthesis has been employed both between thin films and at film-bulk interfaces. An informative study of MAX phase thin films is given by Eklund *et al.*, with a focus on the synthesis of innovative MAX phase coatings.<sup>243</sup> The thermal substitution reaction of a Ti<sub>3</sub>SiC<sub>2</sub> coating with noble metals like Au and Ir is one interesting direction, yielding coatings like Ti<sub>3</sub>AuC<sub>2</sub>, Ti<sub>3</sub>Au<sub>2</sub>C<sub>2</sub>, and Ti<sub>3</sub>IrC<sub>2</sub>.<sup>264</sup> A comparative analysis between bulk and thin film processing reveals distinct disparities. The primary difference is the synthesis temperature, as MAX phase production occurs at substantially lower temperatures for thin films (*e.g.*, PVD of Cr<sub>2</sub>AlC at 450 °C),<sup>243</sup> compared to the 1200–1400 °C range reported for bulk synthesis.<sup>244,265</sup> This temperature contrast is attributed to the additional energetic flux resulting from atomic bombardment during thin film deposition. Another differentiating factor lies in the thermodynamic state of the formed material. Bulk techniques typically aim for a near-equilibrium state, assuming greater stability of the produced MAX phases compared to competing phases. However, certain thin film processes yield MAX phase compounds marked as 'metastable', such as Ti<sub>4</sub>SiC<sub>3</sub>, Ti<sub>4</sub>GeC<sub>3</sub>, and Ti<sub>3</sub>SnC<sub>2</sub>.<sup>266</sup> Although these MAX phases are considered intrinsically stable based on the Cauchy-Born criterion, their synthesis proves challenging in bulk, where specific techniques or additives are required. Notably,





Thorsteinsson *et al.* reported the thin film synthesis of the magnetic MAX phase  $\text{Mn}_2\text{GaC}$ , an achievement not replicated in bulk synthesis to date, underscoring the unique capabilities and challenges inherent in thin film MAX phase synthesis.<sup>267</sup>

Additionally, there is another type of MAX phase known as MAX phase composite material, which we discuss in this article. The synthesis of MAX phase composite materials presents an intriguing avenue for material scientists, offering enhanced properties and structural versatility. In this review, we delve into the synthesis methodologies, focusing particularly on the High-Pressure (HP) process as a primary approach. Notably, Zhang *et al.* demonstrated the fabrication of  $\text{Cu}/\text{Ti}_3\text{AlC}_2$  composites *via* HP, shedding light on their structural stability.<sup>268</sup> Through XRD analysis, it was revealed that Cu and  $\text{Ti}_3\text{AlC}_2$  could coexist below 850 °C, with moderate reactivity observed between 850 and 950 °C, and substantial reaction beyond 950 °C. The diffusion of Al from  $\text{Ti}_3\text{AlC}_2$  into Cu, initiating the formation of  $\text{Cu}(\text{Al})$  solid solution, marked the commencement of the process. Moreover, the ability of  $\text{Ti}_3\text{AlC}_2$  to withstand some Al loss while preserving its structural integrity underscores its robust nature. Additionally, we explore bulk procedures and solid-state reaction techniques, which bear resemblance to each other and differ from Physical Vapor Deposition (PVD). The unique attributes of PVD, such as the capability to supply energy for film growth through methods other than temperature, like energetic growth or ion bombardment, facilitate the deposition of thin-film MAX phases even at low substrate temperatures. This comprehensive examination illuminates the diverse pathways available for the synthesis of MAX phase composites, offering valuable insights for further advancements in material engineering.

## 5. Advanced application of MAX phases

In recent years, the quest for overcoming the hurdles to MAX phase commercialization has intensified, with researchers and industry players alike focusing on innovative solutions. Notably, advancements in materials synthesis, processing techniques, and characterization methods have propelled the exploration of MAX phases into new realms of possibility. For instance, since the late 1990s, following Kanthal Corp.'s acquisition of the MAX technology, significant progress has been achieved in pushing the boundaries of MAX phases' applications. Particularly noteworthy are the advancements in  $\text{Ti}_2\text{AlC}$  heating elements, which underwent thorough testing, displaying exceptional stability over roughly 8000 cycles between room temperature and 1350 °C, thanks to the development of a protective oxide layer.<sup>269</sup> Furthermore,  $\text{Ti}_2\text{AlC}$  has emerged as a superior alternative to traditional steel nozzles in corrosive environments, demonstrating its versatility and potential. Despite these breakthroughs, the widespread availability of MAX phase products remains limited. However, instances such as the adoption of  $\text{Cr}_2\text{AlC}$  pantographs in electric high-speed trains underscore the incremental progress towards broader commercialization.<sup>270</sup>

Nonetheless, challenges persist, including the scarcity of economically viable high-purity powders, the intricate nature of

the vast MAX phase family, and the protracted qualification processes required for critical applications. This review manuscript aims to delve into these recent advancements, offering insights into the evolving landscape of MAX phase utilization and charting a course toward future breakthroughs and commercialization prospects across various industries. Overall, the diverse properties of MAX phases make them promising candidates for a wide range of applications across industries, driving ongoing research and innovation in materials science and engineering is shown in Fig. 13. Here are some notable examples:

### 5.1 Material for high-temperature structural applications

High-temperature structural materials in MAX phase compounds delves into the fascinating realm of MAX phase materials, highlighting their remarkable properties and potential applications in extreme environments. This succinct review offers insights into the structural stability, thermal conductivity, and oxidation resistance of MAX phases, elucidating their pivotal role in advancing aerospace, energy, and automotive industries. Given the remarkable attributes displayed by  $\text{Al}_2\text{O}_3$  scale-forming MAX phases, their utilization in extreme conditions and high-temperature environments is becoming increasingly evident. One particularly promising avenue lies in incorporating  $\text{Ti}_2\text{AlC}$ ,  $\text{Ti}_3\text{AlC}_2$ , and  $\text{Cr}_2\text{AlC}$  into components utilized within gas turbine engines, with the potential to significantly improve efficiency and performance. These MAX phases offer substantially higher operating temperatures compared to conventional Ni/Co superalloys, potentially enabling operations at temperatures exceeding 1400 °C.<sup>271</sup> This advancement is critical for components like combustor liners, blades, and vanes, which endure temperatures surpassing 1600 °C, along with exposure to oxidizing atmospheres, corrosive particles, and intense thermal and mechanical stresses. Additionally, their compatibility with thermal barrier coatings (TBCs) further enhances their utility by reducing thermal stresses and extending system longevity. Boatemaa *et al.* conducted a study where they incorporated 20 vol%  $\text{Ti}_2\text{AlC}$  into  $\text{Al}_2\text{O}_3$  and investigated the crack healing shown in Fig. 14a–d behavior of the composite at elevated temperatures.<sup>271,273</sup> They observed that surface cracks induced by Vickers indentation were filled with newly formed  $\text{Al}_2\text{O}_3$  after annealing above 800 °C, leading to a restoration of bending strength to about 90% of the undamaged composite after annealing at 1000 °C for 15 minutes, with full strength recovery achieved after 1 hour of annealing. Moreover, the abundance of constituent elements such as Ti, Al, and C in MAX phases presents a sustainable and cost-effective alternative to superalloys, which often rely on strategic elements with limited availability and environmental concerns. Recent research has highlighted the exceptional oxidation resistance exhibited by Al-containing MAX phases, illustrated by oxidation-induced crack healing inclusions observed in  $\text{Ti}_2\text{AlC}$  and  $\text{Ti}_3\text{AlC}_2$  composites. Long-term oxidation studies on  $\text{Ti}_3\text{AlC}_2$  have further demonstrated the maintenance of structural integrity and protective capabilities even after prolonged exposure to high temperatures. Additionally, the fabrication of  $\text{Cr}_2\text{AlC}$  foams using sacrificial template



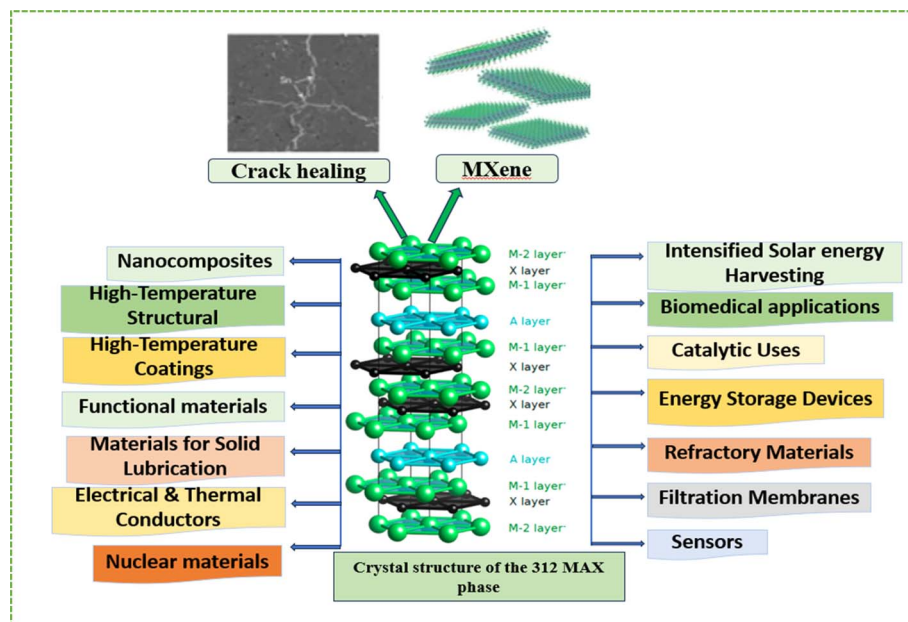


Fig. 13 The overview of multi-applications of MAX-phases.

techniques has demonstrated their potential as robust heat exchangers and catalyst supports, underscoring the versatility and promise of MAX phases in high-temperature applications.<sup>274</sup> These findings collectively emphasize the transformative potential of  $\text{Al}_2\text{O}_3$  scale-forming MAX phases in driving materials innovation for extreme environments and high-temperature applications.

## 5.2 High-temperature coatings

In the domain of cutting-edge materials, High-Temperature Coatings (HTCs) applied on MAX phases have emerged as

a promising frontier. MAX phases, with their unique combination of metallic and ceramic properties, present a fertile ground for innovative coating technologies. MAX phase coatings have garnered attention as protective layers for refractory alloys and as bond-coat layers within Thermal Barrier Coating (TBC) systems. The Coefficient of Thermal Expansion (CTE) plays a pivotal role in both applications, aiming to mitigate stresses and prevent coating spallation. While  $\text{Cr}_2\text{AlC}$ , with its higher CTE ranging from  $12.0$  to  $13.3 \times 10^{-6} \text{ K}^{-1}$ , is deemed more suitable for metallic systems,  $\text{Ti}_2\text{AlC}$  and  $\text{Ti}_3\text{AlC}_2$  with CTE values between  $8.2$  and  $9.0 \times 10^{-6} \text{ K}^{-1}$ , align better with TBC

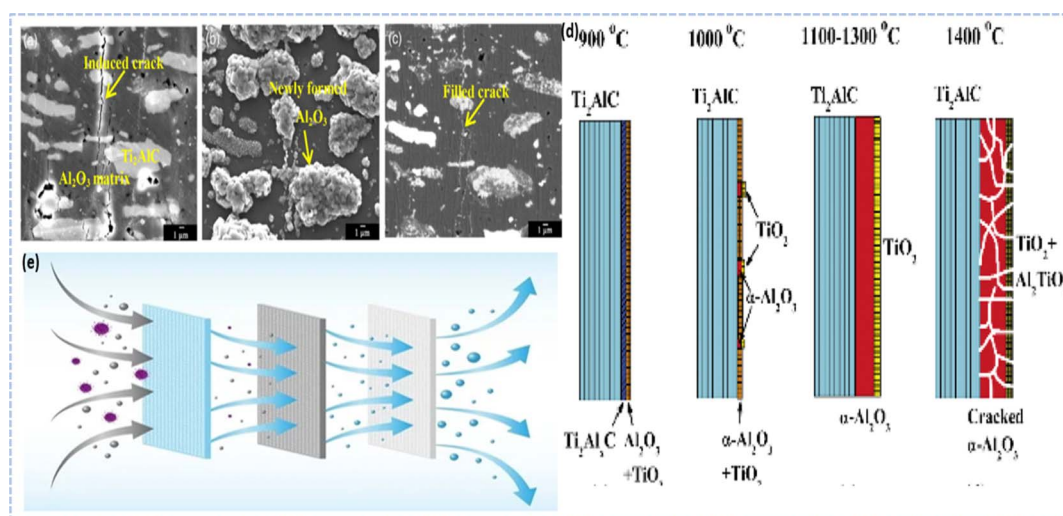


Fig. 14 Examples of MAX phases applications: (a–c) SEM images showcasing  $\text{Al}_2\text{O}_3$ – $\text{Ti}_2\text{AlC}$  composite before and after 1 hour oxidation at  $1000^\circ \text{C}$  in air. (a) Crack initiation prior to oxidation, (b) post-oxidation with visible cracks, and (c) a polished surface revealing filled cracks. (Reproduced from ref. 271 with permission from John Wiley and Sons, copyright 2018).<sup>271</sup> (d) Schematic illustrating microstructural evolution during  $\text{Ti}_2\text{AlC}$  oxidation. (e) Creating a membrane by combining  $\text{Ti}_2\text{AlN}$  MAX phase with cellulose acetate for the removal of dye, protein, and lead ions. (Reproduced from ref. 272 with permission from Elsevier, copyright 2022).<sup>272</sup>



compounds. Notably, advanced turbine disks can be shielded against Type I and II Low Temperature Hot Salt Corrosion (LTHC).<sup>275,276</sup> For instance,  $\text{Cr}_2\text{AlC}$  coatings applied on a low  $\gamma'$  solvus and high refractory content alloy, referred to as LSHR and developed by NASA, effectively prevented hot corrosion pitting and substantially enhanced low cycle fatigue resistance by up to 90%. A novel fabrication technique was employed to produce dense, single-phase  $\text{Cr}_2\text{AlC}$  MAX phase coatings, thereby circumventing columnar structures. These coatings demonstrated exceptional resistance to oxidation, enduring temperatures up to 1100 °C, with the oxidation process manifesting two distinct stages due to the formation of dense  $\text{Al}_2\text{O}_3$  and  $(\text{Cr}, \text{Al})_2\text{O}_3$  layers shown in Fig. 15.<sup>277</sup> Recent advancements include the deposition of  $\text{Cr}_2\text{AlC}$  bond-coats on Inconel 738 substrates, succeeded by the application of porous yttria-stabilized zirconia as an external TBC. Under conditions akin to a gas turbine environment, the system endured surface and substrate temperatures of 1400 °C and 1050 °C, respectively, albeit failing after 745 cycles, mainly attributed to the open porosity of the  $\text{Cr}_2\text{AlC}$  bond-coat layer, oxidation of secondary phases, and inter-diffusion.<sup>274</sup> Moreover, future endeavors aim to address the challenges in transferring MAX phase coatings as bond-coats, with  $\text{Ti}_2\text{AlC}$  showing promising potential for such applications.

### 5.3 Filtration membranes

The distinctive layered structure of MAX phases provides a promising framework for developing advanced filtration membranes with superior performance characteristics. These membranes possess the capability to selectively separate molecules based on various attributes such as size, charge, or other properties, rendering them suitable for applications in water purification, gas separation, and industrial processes. The

initial phase of the current study involved synthesizing  $\text{Ti}_2\text{AlN}$  MAX phase using the reactive sintering method and subsequently characterizing it shown in Fig. 14e. The hexagonal crystalline structure of the MAX phase was confirmed *via* X-ray diffraction analysis. Incorporating the MAX phase into cellulose acetate membranes enhanced their hydrophilicity and overall performance. An optimal nanocomposite membrane containing 0.75 weight% of MAX phase exhibited a significant three-fold increase in permeability during the filtration of dye solutions and pure water. Furthermore, this optimized membrane demonstrated a remarkable 92.7% improvement in flux recovery ratio, along with high removal efficiencies for various contaminants, including reactive dyes and proteins. The nanocomposite membrane also exhibited substantial rejection rates for common salts like sodium sulfate and sodium chloride, highlighting its potential as an effective membrane material for diverse membrane technology applications.<sup>278</sup>

### 5.4 Materials for solid lubrication

Exploring the frontier of solid lubricant materials, MAX phases emerge as a promising avenue for enhanced tribological performance. With their unique combination of metallic and ceramic properties, MAX phases offer exceptional resistance to wear and friction, making them ideal candidates for various engineering applications. MAX phases possess remarkable attributes such as high damage tolerance, thermal shock resistance, machinability, and a ductile–brittle transition occurring above 1000 °C, in addition to their layered hexagonal structure. These distinctive characteristics render MAX phases highly promising candidates for solid lubricant materials, with potential applications spanning MAX-based composites, monolithic bulk MAX, and MAX coatings.<sup>15</sup> Among the various MAX phases,  $\text{Ti}_3\text{SiC}_2$  and  $\text{Cr}_2\text{AlC}$  have garnered significant

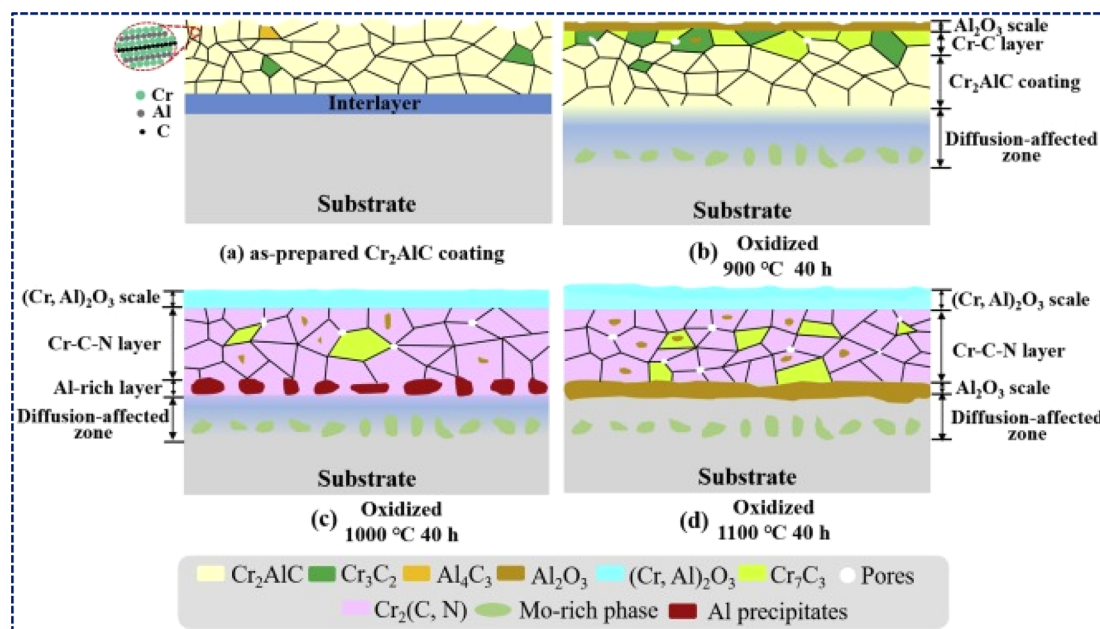


Fig. 15 Oxidation mechanisms of  $\text{Cr}_2\text{AlC}$  MAX phase coatings at 900–1100 °C. (Reproduced from ref. 277 with permission from Elsevier, copyright 2020).<sup>277</sup>





attention in research endeavors. For instance, investigations by Shi *et al.* unveiled the pivotal role of  $\text{Ti}_3\text{SiC}_2$  content in modulating the tribological properties of NiAl matrix, with an optimal  $\text{Ti}_3\text{SiC}_2$  content of 10 wt% resulting in a composite exhibiting a low friction coefficient of 0.60 and a minimal wear rate of  $5.45 \times 10^{-5} \text{ mm}^3 (\text{N m})^{-1}$ , where micro ploughing and delamination were identified as dominant wear mechanisms.<sup>279</sup> Similarly, Shamsipoor *et al.* highlighted the influence of  $\text{Cr}_2\text{AlC}$  purity on wear performance, with a maximum  $\text{Cr}_2\text{AlC}$  phase content of 68.05% showcasing superior wear resistance among all samples. Moreover, the synthesis of a  $\text{Ti}_3\text{SiC}_2$ - $\text{TiSi}_2$ - $\text{TiC}$  composite *via* Spark Plasma Sintering (SPS) demonstrated inherent self-lubricating behavior.<sup>280</sup> Furthermore, the deposition of  $\text{Ti}_2\text{AlC}$  coating onto an Inconel substrate using the cold-spray technique revealed a substantially reduced friction coefficient of 0.603 at 600 °C compared to 0.766 at room temperature, with a corresponding 40% decrease in volume loss at elevated temperatures, underscoring the potential of  $\text{Ti}_2\text{AlC}$  coatings as high-temperature tribological coatings.<sup>281</sup> Insights from Magnus *et al.* elucidated the intrinsic lubricity of  $\text{Ti}_3\text{SiC}_2$ - $\text{TiSi}_2$ - $\text{TiC}$  composites, delineating various wear mechanisms such as graphitization, Tri biofilm spallation, grain pull-out, fracture, and re-graphitization, indicative of the complex interplay of chemical and physical reactions during wear processes.<sup>282</sup> Another study focuses on creating self-lubricating nanocomposite coatings, using Ag-doped  $\text{Cr}_2\text{AlC}$ , exhibiting reduced friction and wear for aerospace and marine applications. Incorporating Ag led to unique structures with enhanced self-lubrication, notably reducing friction below 500 °C and promoting plastic strain accommodation without extensive cracking even at higher temperatures shown in Fig. 16.<sup>283</sup>

### 5.5 Electrical and thermal conductors

This comprehensive review delves into the captivating domain of MAX phases, examining their distinctive amalgamation of electrical and thermal conductive traits. MAX phases, defined by their stratified crystalline arrangement, showcase

compelling attributes in facilitating the flow of both electricity and heat. Their commendable electrical and thermal conductivity renders them apt for diverse applications like electrical connectors and thermal dissipators in electronic apparatuses. The amalgamation of metallic and ceramic attributes in MAX phases enables effective heat dispersion and enhanced electrical functionality.

$\text{Ti}_3\text{SiC}_2$  has emerged as a promising candidate for ohmic contacts on 4H-SiC owing to its desirable linear current-voltage characteristics. This material offers the advantage of facile processing through a one-step method involving the sputter-deposition of Ti onto SiC substrates.<sup>284</sup> This innovative approach opens avenues for the direct synthesis of oxygen-barrier capping layers subsequent to the deposition of the primary contact. By circumventing exposure to air, it effectively mitigates risks associated with oxidation, contamination, or the necessity for additional cleaning steps, thereby augmenting the long-term stability of the device. Additionally,  $\text{Ti}_2\text{AlN}$  has garnered attention as an ohmic contact material for GaN-based devices, demonstrating favorable ohmic behavior with a contact resistivity falling within the range of  $10^{-4} \Omega \text{ cm}^{-2}$ .<sup>285</sup>

Beyond electronic applications, MAX phases have been explored for their potential as heat exchangers capable of operating at elevated temperatures ( $\sim 850$  °C), surpassing the capabilities of conventional metallic systems.<sup>286</sup> This niche arises from the fact that ceramics remain the sole alternative for such high-temperature environments. However, the widespread adoption of MAX phases for this purpose has been impeded by inherent limitations, including poor mechanical properties, challenging machinability, low thermal conductivity, and coefficient of thermal expansion (CTE). Despite these drawbacks, MAX phases exhibit a remarkable capacity to withstand high temperatures, reaching up to 1400 °C, coupled with superior thermal shock resistance, mechanical robustness, chemical inertness, and machinability compared to materials like SiC and other advanced ceramics.<sup>287</sup> This research unveils a novel economical method for producing high-purity MAX phases,

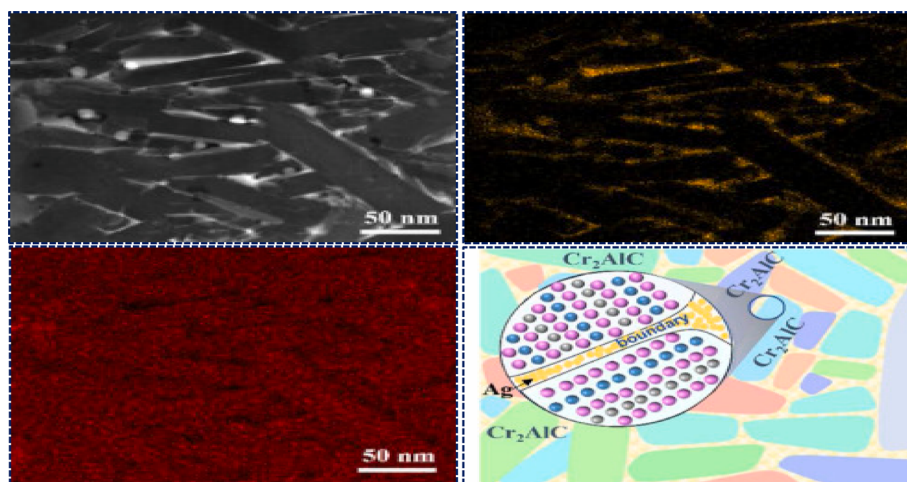


Fig. 16 The cross-sectional images and schematics representation of the Ag doped  $\text{Cr}_2\text{AlC}$  nanocomposite coatings. (Reproduced from ref. 283 with permission from Elsevier, copyright 2024).<sup>283</sup>



offering a promising avenue for refining synthesis techniques to yield low-cost, high-conductivity MAX phases in the times ahead. Notably, the  $\text{Ti}_3\text{AlC}_2$ -coated stainless steel 304 exhibits remarkable characteristics, displaying minimal corrosion and interfacial contact resistance. These findings position it as a highly viable option for deployment in simulated Proton Exchange Membrane Fuel Cell (PEMFC) environments, holding significant potential for advancing clean energy technologies shown in Fig. 17.<sup>288,289</sup>

Nevertheless, the primary drawback hindering their broader application remains their intermediate thermal conductivity, typically ranging between 12 and 60  $\text{W m}^{-1} \text{K}^{-1}$ . While this level of thermal conductivity is deemed acceptable for many applications, it falls short when compared to the thermal conductivity of SiC compounds, which can reach up to 125  $\text{W m}^{-1} \text{K}^{-1}$ .<sup>287</sup> This thermal disparity underscores a key area for further research and development aimed at enhancing the thermal transport properties of MAX phases, potentially through the exploration of novel synthesis techniques or compositional modifications, to unlock their full potential in high-temperature heat exchange applications and beyond.

## 5.6 Nuclear materials

MAX phases, a class of materials characterized by a unique combination of metallic and ceramic properties, have emerged as promising candidates for various nuclear applications. Their exceptional thermal and mechanical properties, coupled with good radiation tolerance, make them suitable for reactor structural components, fuel cladding, and even as matrix

materials for nuclear waste immobilization. MAX phases including  $\text{Ti}_3\text{SiC}_2$ ,  $\text{Ti}_2\text{AlC}$ ,  $\text{Ti}_3\text{AlC}_2$ ,  $\text{Cr}_2\text{AlC}$ ,  $\text{V}_2\text{AlC}$ ,  $\text{Zr}_2\text{AlC}$ ,  $\text{Zr}_3\text{AlC}_2$ , and  $\text{Nb}_4\text{AlC}_3$  have attracted considerable attention due to their remarkable radiation tolerance, resistance to oxidation and corrosion, mechanical strength, and chemical stability. These characteristics position them as promising candidates for accident-tolerant fuel (ATF) claddings in third-generation light-water reactors (LWRs) and anticipated fourth-generation fission plants.<sup>290</sup> This Fig. 18 illustrates the stages from MAX-phase formation to MAX-phase tubes, which are utilized in fuel production for nuclear reactors, followed by steps of spent fuel storage, fuel reproduction, and fuel fabrication.<sup>291</sup> Traditional zirconium alloys, historically employed as cladding materials, have raised concerns regarding their performance in scenarios like Loss of Coolant Accidents (LOCAs). In response, MAX phases emerge as an appealing alternative or coating material due to their superior resistance to oxidation and corrosion. Coatings composed of dense, highly pure MAX phases can be applied at low temperatures, safeguarding the integrity of zircaloy substrates.

Moreover, in the realm of Generation IV reactor development, particularly in lead-fast reactor designs, MAX phases demonstrate favorable traits including radiation tolerance, corrosion resistance, mechanical stability, and compatibility with lead alloy coolants. These reactors, utilizing fast neutrons ( $>1 \text{ MeV}$ ) for fission reactions, enhance fuel efficiency, facilitating the use of depleted uranium and transmutation of long-lived nuclear waste. The demanding operational conditions of Generation IV reactors necessitate materials capable of

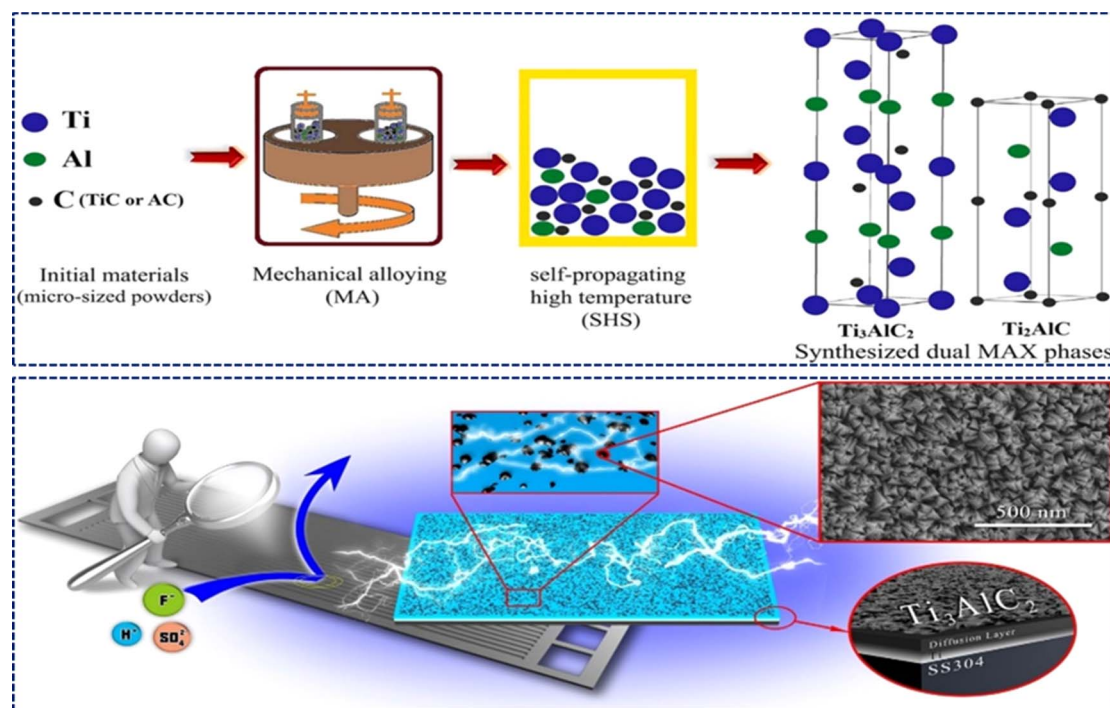


Fig. 17 Schematic representation illustrating the synthesis process of low-cost  $\text{Ti}_3\text{AlC}_2$ - $\text{Ti}_2\text{AlC}$  dual MAX phase, highlighting the use of economical raw materials and innovative compositions for achieving high-electrical conductivity. (Reproduced from ref. 288 with permission from Elsevier, copyright 2023).<sup>288</sup> (Reproduced from ref. 289 with permission from Elsevier, copyright 2019).<sup>289</sup>

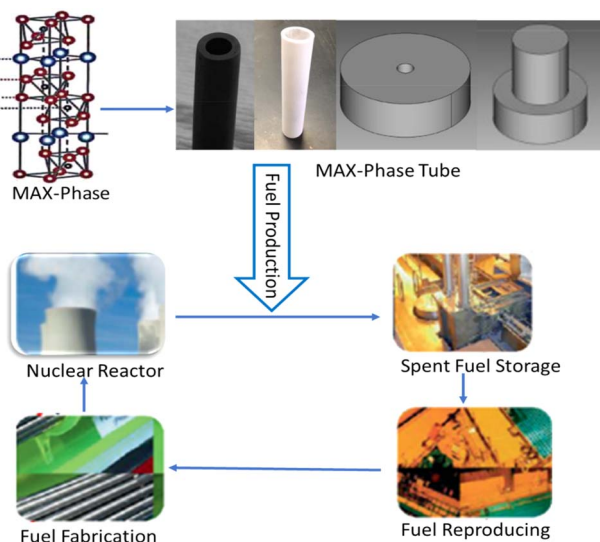


Fig. 18 Schematic representation of the fuel production process using MAX-phase materials. (Reproduced from ref. 291 with permission from Elsevier, copyright 2020).<sup>291</sup>

withstanding prolonged exposure to elevated temperatures, corrosive environments, and high neutron fluences. MAX phases, renowned for their high-temperature capabilities, damage tolerance, and resistance to radiation-induced amorphization, emerge as compelling options for nuclear applications. Extensive research validates the exceptional radiation damage tolerance of MAX phases like  $\text{Ti}_3\text{AlC}_2$  and  $\text{Ti}_3\text{SiC}_2$ , which display resistance to amorphization up to 25 displacement per atom (dpa), with complete amorphization anticipated only beyond 100 dpa.<sup>292</sup> Additionally, MAX phases exhibit comparably low neutron activation, positioning them as competitive alternatives to conventional materials such as SiC and Alloy 617 to enhance safety and efficiency for next-generation reactor components.<sup>293</sup>

### 5.7 Intensified solar energy harvesting

MAX phases are highly promising for utilization within Intensified Solar Power (ISP) systems owing to their distinctive blend of thermal robustness, mechanical resilience, and resistance to corrosion. When incorporated into various ISP components like receiver tubes or heat storage materials, MAX phases can endure the extreme temperatures and challenging operational environments encountered during concentrated solar energy capture. Furthermore, their inherent spectral selectivity, as evidenced by reflectance spectra analyses, could bolster the effectiveness of solar energy absorption and thermal regulation within ISP setups. ISP systems facilitate the conversion of solar energy into electricity without emitting greenhouse gases and offer the advantage of thermal energy retention. These systems concentrate solar radiation onto a receiver *via* mirrors, and the resultant heat is conveyed by a heat transfer fluid (HTF) to a steam turbine for electricity generation.<sup>294</sup> Efficiency in energy conversion, typical of thermal processes, improves with higher temperatures and combined cycle configurations. ISP

combined cycles ideally operate within the temperature range of 1000–1500 K, with heat transferred by HTFs like air, molten salts, minerals, or synthetic oils. Alternative nonoxide ceramics such as SiC and  $\text{ZrB}_2$  have also been proposed for solar receivers due to their elevated degradation thresholds.<sup>295–297</sup> Particularly, porous SiC volumetric receivers have garnered attention due to heightened heat transfer per unit volume coupled with minimal pressure drops.<sup>298</sup> MAX phases demonstrate potential in two distinct sections of CSP systems: the solar receiver and the storage tank. An ideal solar receiver should possess exceptional oxidation resistance, along with attributes like high absorptance in the ultraviolet-visible-near infrared (UV-vis-NIR) spectrum and low thermal emission in the infrared (IR) spectrum.<sup>299</sup> The reflectance spectra of mirror-polished MAX phase samples reveal intrinsic spectral selectivity across the full range of wavelengths measured. While  $\text{Ti}_2\text{AlC}$  and  $\text{Ti}_3\text{AlC}_2$  exhibit similar infrared spectra,  $\text{Cr}_2\text{AlC}$  displays a slightly lower reflectance and a blue shifted rise front. The corrosion resistance of  $\text{Ti}_3\text{AlC}_2$  proves inferior, evidenced by significant degradation and complete disintegration after 672 hours of exposure, highlighting its susceptibility to corrosion in solar salt environments. Microscopic analysis suggests the absence of a continuous  $\text{Al}_2\text{O}_3$  scale, emphasizing the material's vulnerability to corrosion shown in Fig. 19.<sup>300</sup> However, the extent of  $\text{Ti}_2\text{AlC}$  and  $\text{Cr}_2\text{AlC}$ 's potential for CSP applications remains insufficiently researched. Despite both MAX phases exhibiting excellent resistance to high concentrated flux,  $\text{Ti}_2\text{AlC}$  displays higher light scattering due to surface oxidation. Their thermal performance varies within the range of 0.56–0.68 and 0.60–0.67, respectively, for the chosen flux levels. In terms of volumetric receivers with open and controlled porosity, MAX phase foams hold promise due to their minimal oxidation and exceptional thermal shock resilience compared to SiC, yet empirical testing remains pending. Moreover, they could serve as structural materials for storage tanks owing to their superb compatibility with molten solar salts. Recent studies by K. Van Loo *et al.* have evaluated the compatibility of various MAX phases, SiC grades, and reference metallic structural materials with a molten salt (40 wt%  $\text{KNO}_3$  and 60 wt%  $\text{NaNO}_3$ ) for 1000 hours at 600 °C, with  $\text{Cr}_2\text{AlC}$  exhibiting superior corrosion resistance attributable to the formation of a micrometric-thin, protective layer of  $\text{Cr}_7\text{C}_3$ .<sup>301</sup> Despite promising attributes, challenges such as corrosion resistance in solar salt environments remain to be addressed for widespread adoption of MAX phases in CSP applications. Nonetheless, ongoing research and development efforts are poised to unlock the full potential of MAX phases in advancing the sustainability and performance of ISP technology.

### 5.8 MXene formation building blocks

MAX phases serve as valuable precursors for MXenes, offering a robust platform for tailored material synthesis with diverse functionalities. By selectively etching the 'A' layers from MAX phases, MXenes with tunable surface chemistries and unique structural properties can be obtained. This process preserves the inherent mechanical strength and thermal stability of MAX





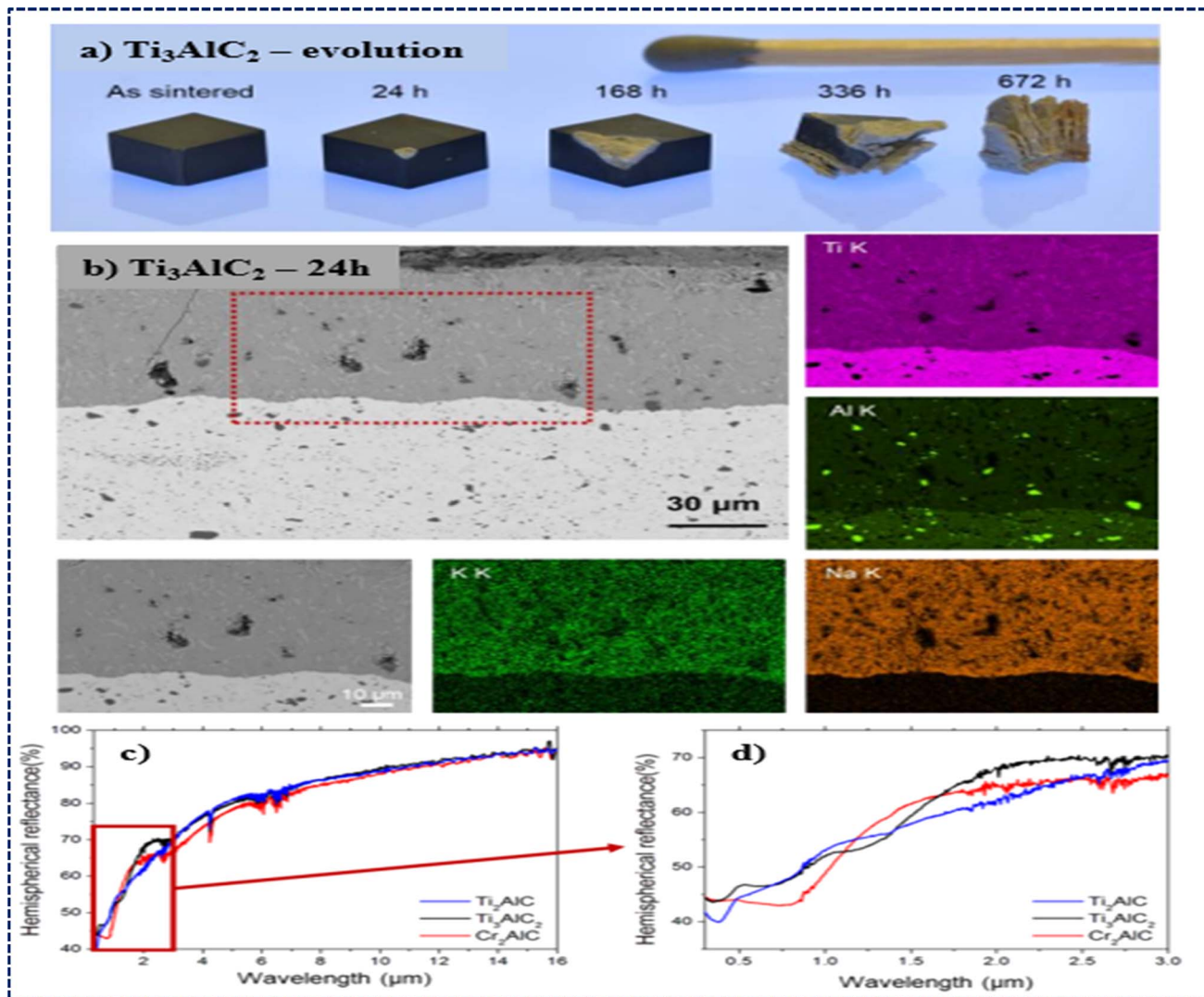


Fig. 19 (a) Images of samples before and after corrosion in solar salt at various intervals: as-sintered, and after 24, 168, 336, and 672 h. (b) Micrograph of corroded sample after 24 h with corresponding EDS elemental maps of the rectangular zone. (c) Hemispherical reflectance spectra of MAX samples in the 0.3–16  $\mu\text{m}$  range, and (d) detail of the solar spectrum range. Reprinted with permission. (Reproduced from ref. 300 with permission from John Wiley and Sons, copyright 2017).<sup>300</sup>

phases while unlocking new opportunities for applications energy storage, hybrid-ion capacitors, Li/Na-ion batteries, water purification, photo- and electrocatalysis, as well as sensors.<sup>302–304</sup> Fig. 20 shown the various processes for MXene synthesis.<sup>305</sup> The advancement in MXene preparation techniques not only forms the foundation for investigating MXene surface terminations but also offers diverse avenues for tailoring MXene performance as functional materials. However, the use of F-containing solutions in MXene synthesis poses hazards, necessitating the exploration of nonhazardous synthesis routes.<sup>282</sup> In a recent breakthrough, Li *et al.* introduced a general Lewis acidic etching method, which circumvents the need for hazardous HF solutions. This method facilitates the etching of MAX phases through direct redox reactions between the A site element and the cation of the Lewis acid molten salt.<sup>306</sup> Consequently, various MXenes can be synthesized from unconventional MAX-phase precursors with A

site elements such as Si, Zn, and Ga. A plethora of MXenes have already been synthesized from precursor MAX phases, including  $\text{Ti}_2\text{C}$ ,  $\text{V}_2\text{C}$ ,  $(\text{Ti}_{0.5}\text{Nb}_{0.5})_2\text{C}$ ,  $(\text{V}_{0.5}\text{Cr}_{0.5})_3\text{C}_2$ ,  $\text{Ti}_3\text{CN}$ ,  $\text{Nb}_4\text{C}_3$ , among others. The development of MAX phases plays a pivotal role in advancing MXene synthesis. For instance, the discovery of the first i-MAX phase  $(\text{Mo}_{2/3}\text{Sc}_{1/3})_2\text{AlC}$  led to the synthesis of the first  $\text{Mo}_{1.33}\text{C}$  MXene with ordered metal divacancies, exhibiting exceptional properties such as low resistivity ( $33.2 \mu\Omega \text{ m}^{-1}$ ) and high volumetric capacitance ( $1150 \text{ F cm}^{-3}$ ).<sup>307</sup> The continual discovery of new MAX phases broadens the scope of potential MXene synthesis, offering prospects for further advancements in materials science. Furthermore, the ability to control the synthesis parameters allows for precise manipulation of MXene properties, such as surface chemistry, interlayer spacing, and electrical conductivity, enabling targeted design for specific applications.



of the system presents a potential solution, albeit with limitations on the use of conventional ceramic foams. MAX phases offer a compelling alternative in this regard due to their favorable electrical conductivity, thermal stability, and exceptional mechanical strength. The integration of MAX phases into catalytic systems not only promises enhanced performance but also underscores the versatility and untapped potential of these intriguing materials across diverse scientific and industrial domains. As research continues to unravel the myriad capabilities of MAX phases, their role as catalysts is poised to expand, driving innovation and advancement in catalysis-driven processes and technologies.

For instance, the biocompatibility of MAX phases has been extensively studied, revealing minimal cytotoxicity and favorable cell adhesion properties, both of which are crucial for promoting tissue integration.<sup>314</sup> Similarly, investigations into the corrosion resistance of MAX phases under physiological conditions have underscored its importance in ensuring the

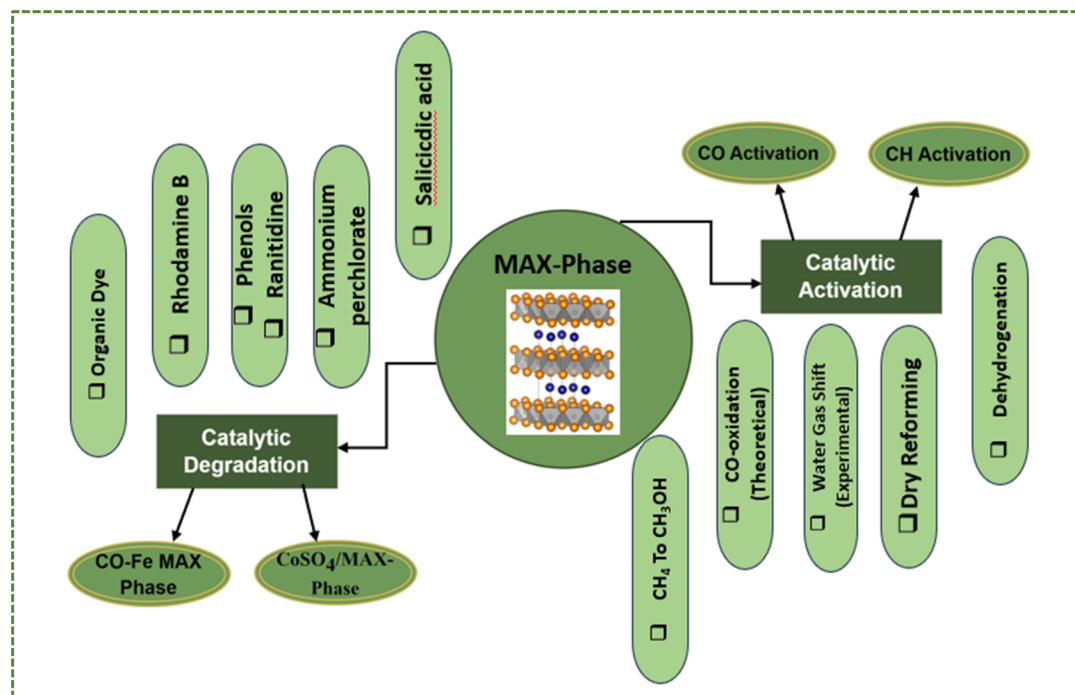


Fig. 21 Types of MAX phases used in catalytic degradation reactions and processes based on C–H and C–O activation. (Reproduced from ref. 308 with permission from The Royal society of Chemistry, copyright 2021).<sup>308</sup>

longevity and reliability of implants within the human body.<sup>315</sup> Furthermore, MAX phases exhibit an exceptional capacity to withstand harsh physiological environments, ensuring prolonged functionality and reduced risk of degradation within the human body. This robustness is essential for the longevity and effectiveness of implants, as they must endure the rigors of daily life while promoting tissue regeneration.<sup>316</sup> Moreover, MAX phases possess tailored mechanical properties that closely mimic those of natural bone, facilitating optimal load-bearing capabilities and minimizing the risk of implant failure. This similarity to bone structure not only enhances the compatibility of MAX phase implants but also promotes osseointegration, the process by which bone grows around the implant, ensuring long-term stability and functionality.<sup>317</sup> Additionally, the tunable nature of MAX phases allows for customization according to specific application requirements, offering versatility in design and performance. This adaptability opens avenues for the development of personalized biomedical implants tailored to individual patient needs, ultimately improving treatment outcomes and patient satisfaction. Furthermore, the use of MAX phases in bone tissue engineering scaffolds presents an innovative approach to regenerative medicine. By providing a supportive framework for cell growth and tissue regeneration, MAX phase scaffolds facilitate the repair of damaged or diseased bone tissue, offering a viable solution for conditions such as fractures, defects, and degenerative bone diseases.<sup>318,319</sup> Their porous structure and interconnected pore network enable efficient nutrient exchange and cell infiltration, fostering a conducive environment for tissue regeneration and integration. Moreover, MAX phase scaffolds

can be engineered to degrade gradually over time, allowing for seamless replacement by newly formed bone tissue without the need for additional surgical interventions.<sup>320</sup> This biodegradability feature eliminates the risk of long-term implant retention and alleviates concerns associated with implant removal, offering a more patient-friendly approach to bone regeneration shown in Fig. 22. Overall, the biomedical applications of MAX phases hold tremendous promise for advancing the field of orthopedics and regenerative medicine, offering innovative solutions for improving patient outcomes and quality of life.<sup>322</sup> With ongoing research and development efforts, MAX phases are poised to play a pivotal role in shaping the future of biomedical implant technology and tissue engineering strategies.

### 5.11 Energy storage devices

MAX phases exhibit excellent electronic and ionic conductivity, owing to their metallic nature and inherent crystal structure. This combination of properties renders MAX phases highly promising candidates for next-generation battery technologies. One of the most compelling features of MAX phases is their ability to maintain structural integrity even after undergoing multiple intercalations and deintercalation cycles, a crucial requirement for long-term battery performance and durability. Additionally, their inherent stability against chemical and mechanical degradation further enhances their suitability for energy storage applications. Researchers are actively exploring the incorporation of MAX phases into electrode materials for lithium-ion batteries to exploit their exceptional ion accommodation capabilities and conductivity. By leveraging these





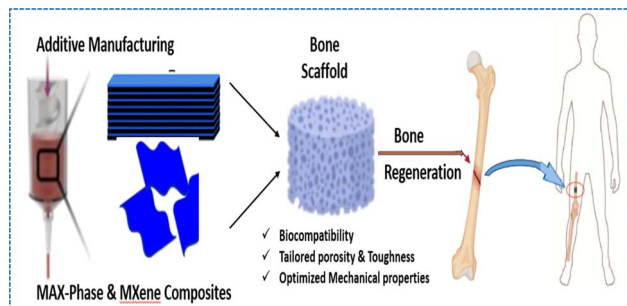


Fig. 22 Bio-medical applications for bone regeneration by MAX-phase composites. (Reproduced from ref. 321 with permission from Elsevier, copyright 2023).<sup>321</sup>

unique properties, MAX phases hold the potential to significantly enhance the energy storage capacity, efficiency, and lifespan of lithium-ion batteries, paving the way for the development of high-performance energy storage systems for diverse applications ranging from portable electronics to electric vehicles and grid-level energy storage.<sup>323,324</sup> Furthermore, the versatility of MAX phases extends beyond lithium-ion batteries, with investigations underway to explore their applicability in other types of energy storage devices such as supercapacitors and solid-state batteries.<sup>325</sup> Through continued research and development efforts, MAX phases are poised to play a pivotal role in advancing the landscape of energy storage technologies, driving innovation and sustainability in the quest for cleaner and more efficient energy solutions. MXene is developed from the MAX phase, which is being used as an energy-storing material, as shown in Fig. 23.

### 5.12 Refractory materials

MAX phases, characterized by their remarkable combination of high melting points and exceptional thermal stability, have emerged as valuable constituents in the fabrication of refractory materials tailored for demanding applications in high-temperature environments. Refractory materials play a critical role in industries where extreme heat conditions are prevalent, such as metallurgy, ceramics, and glass manufacturing. MAX phases, with their inherent resistance to thermal degradation and mechanical stress, offer a compelling solution to the challenges posed by such harsh operating conditions. These

materials are adept at withstanding temperatures well above those tolerated by conventional refractory materials, making them ideal candidates for lining furnaces, crucibles, and other high-temperature equipment. MAX phases exhibit robust mechanical properties even at elevated temperatures, ensuring structural integrity and longevity in demanding industrial settings. Their ability to endure thermal cycling without undergoing significant degradation further enhances their suitability for refractory applications. Moreover, MAX phases demonstrate excellent resistance to chemical corrosion, a crucial attribute in environments where exposure to reactive substances is common. This resistance allows MAX phase-based refractory materials to maintain their performance and integrity over extended periods, minimizing downtime and maintenance costs.

Several studies in the literature underscore the suitability and advantages of MAX phase-based refractory materials for high-temperature applications. For example, research by Smith *et al.* highlighted the superior thermal stability of MAX phases compared to traditional refractory materials, showcasing their potential for enhancing furnace performance and prolonging service life.<sup>326</sup> Similarly, investigations by Johnson and colleagues elucidated the exceptional mechanical properties of MAX phase-based refractories, emphasizing their ability to withstand mechanical stresses under extreme heat conditions, thus reducing the risk of failure and downtime in industrial operations.<sup>327</sup>

Furthermore, the versatility of MAX phases enables the engineering of refractory materials with tailored properties to meet specific application requirements, including enhanced thermal conductivity, thermal shock resistance, and erosion resistance. As such, MAX phase-based refractory materials represent a promising avenue for improving the efficiency, reliability, and safety of high-temperature processes across various industries. Continued research and development efforts in this field are expected to unlock further potential in leveraging MAX phases to advance the performance and functionality of refractory materials, driving innovation and sustainability in high-temperature applications.

### 5.13 Sensor

The electrical and thermal properties of MAX phases make them promising materials for various sensor applications. Their

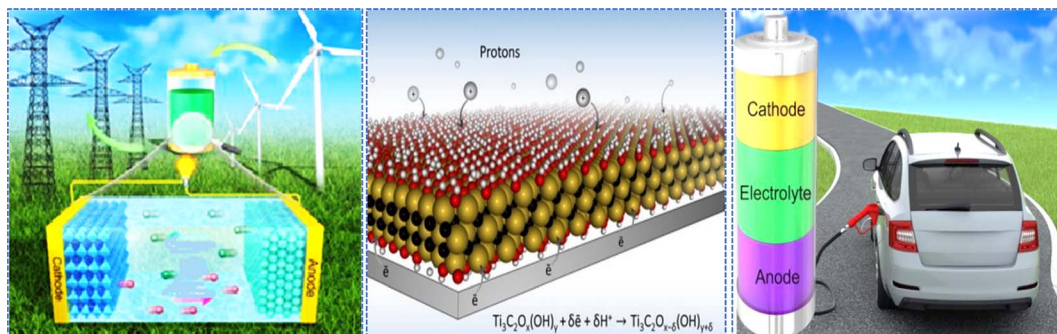


Fig. 23 Various energy storing application using MAX phases derivatives (MXene).



ability to detect changes in temperature, pressure, strain, and gas concentrations can be utilized in sensors for industrial monitoring, environmental sensing, and healthcare diagnostics. The electrical and thermal properties inherent in MAX phases render them highly promising materials for a wide array of sensor applications. MAX phases exhibit intriguing electrical conductivity, which can range from metallic to semi-conducting behavior, depending on the specific composition and environmental conditions. This tunable conductivity makes them suitable for applications where precise electrical sensing is required, such as in strain sensors, temperature sensors, and gas sensors. Additionally, MAX phases possess excellent thermal stability and high thermal conductivity, attributes that are advantageous for sensing applications involving temperature monitoring and thermal imaging. Their ability to withstand extreme temperatures while maintaining structural integrity ensures reliable and accurate sensor performance even in harsh environments. This Fig. 24 illustrates the process of combining MAX-phases with a GCE to create a MAX-phase@GCE composite, which is then applied to improve the functionality of the resulting material as a sensor.<sup>328</sup>

Overall, the unique combination of electrical and thermal properties in MAX phases positions them as promising candidates for next-generation sensor technologies across various fields, including aerospace, automotive, healthcare, and environmental monitoring.

A straightforward and environmentally friendly approach was utilized to successfully create a  $\text{Ti}_3\text{Al}_{0.5}\text{Cu}_{0.5}\text{C}_2$  MAX phase structure, leading to the development of a  $\text{Ti}_3\text{Al}_{0.5}\text{Cu}_{0.5}\text{C}_2$ -based glassy carbon electrode (GCE). Under optimized conditions, the  $\text{Ti}_3\text{Al}_{0.5}\text{Cu}_{0.5}\text{C}_2$ -based sensor showed good linearity within the range of  $0.02\text{--}50.00\ \mu\text{mol L}^{-1}$  for rutin analysis, achieving a low limit of detection (LOD) of  $0.015\ \mu\text{mol L}^{-1}$ . Moreover, the fabricated  $\text{Ti}_3\text{Al}_{0.5}\text{Cu}_{0.5}\text{C}_2$  MAX phase was effectively utilized for the detection of trace levels of rutin in mandarin and kiwi samples, with validation conducted through high-performance liquid chromatography (HPLC), thus underscoring its potential for precise electrochemical analysis of small molecules in agricultural applications.<sup>329</sup>

#### 5.14 Advanced nanocomposites

MAX phases are a versatile class of nanomaterials renowned for their unique blend of metallic and ceramic properties, making them highly coveted for applications in nanocomposites. Incorporating MAX phases into nanocomposites serves as a formidable reinforcement strategy, enhancing mechanical properties such as strength, stiffness, and fracture toughness.

This is particularly advantageous for crafting lightweight yet resilient materials suited for structural needs across diverse industries. Furthermore, harnessing the exceptional thermal conductivity of MAX phases enables the engineering of nanocomposites with superior heat dissipation capabilities, crucial for applications where efficient thermal management is paramount, such as in electronics, aerospace, and automotive sectors. Moreover, the innate resistance to corrosion exhibited by MAX phases positions them as prime candidates for augmenting the durability of nanocomposite coatings, shielding substrates from degradation in harsh environments. Additionally, the distinctive combination of metallic and ceramic traits in MAX phases facilitates the development of nanocomposites with tailored electrical and electromagnetic properties, driving advancements in electronics, telecommunications, and sensor technologies.

Recent years have witnessed MAX phases emerging as focal points in global materials research, captivating scientists with their extraordinary properties. The surge in publications on MAX phases underscores the growing interest in these nanolaminate materials, which promise a plethora of applications. This comprehensive review aims to deepen our understanding of MAX phases while highlighting recent progress and developments in the field. Covering aspects from chemical composition to microstructure, including newly-discovered structural variants, the review provides insights into synthesis methods and explores the chemical and physical properties of MAX phases. Moreover, it surveys potential applications across diverse fields such as high-temperature and nuclear materials, as well as their role as precursors for producing 2D materials like MXenes.<sup>330</sup> Despite challenges in controlling MAX phase morphology at the nanoscale, recent advancements have led to the fabrication of nanostructured MAX phases, opening doors to exciting opportunities. For instance, the synthesis of nanostructured Ti-Al-C MAX phases has facilitated the production of nanosized multilayered MXenes with enhanced electrochemical properties, paving the way for advancements in energy storage technologies. Furthermore, the synergistic combination of MAX phases with other materials, as seen in nanocomposites, has resulted in improved thermal and mechanical properties, demonstrating their potential in various engineering applications.<sup>331</sup> This Fig. 25 shows the transformation of MAX-phase materials into various forms of advanced nanocomposites, including nanofibers, nanofillers, and nanoflakes. Moving forward, continued exploration of PANI-MAX phase nanocomposites presents avenues for novel applications, particularly in the realms of photocatalysis and solar energy. As

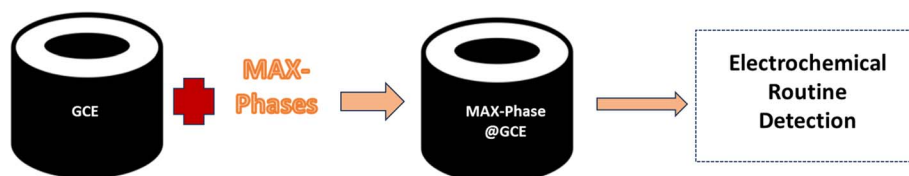


Fig. 24 Schematic of MAX-phase integration with Glassy Carbon Electrode (GCE) for enhanced performance as a sensor. (Reproduced from ref. 328 with permission from Elsevier, copyright 2022).<sup>328</sup>

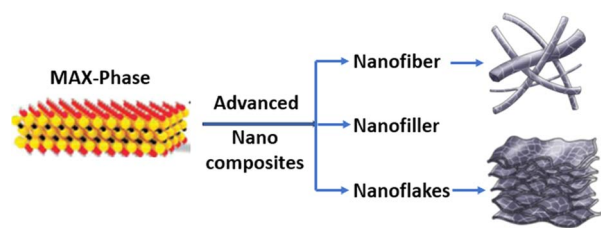


Fig. 25 Formation of advanced nanocomposites from MAX-phase materials.

research progresses, the integration of MAX phases into nanocomposites promises to drive innovation in materials science and engineering, ushering in a new era of advanced materials with tailored properties and functionalities.<sup>332</sup>

### 5.15 Functional materials

MAX phases, renowned for their diverse array of physical and chemical properties, have attracted attention as functional materials. Wang *et al.*<sup>333</sup> investigated the utilization of  $\text{Ti}_3\text{AlC}_2$  as a catalyst to enhance the reversible hydrogen storage capabilities of  $\text{MgH}_2$ . The addition of 7 wt%  $\text{Ti}_3\text{AlC}_2$  into  $\text{MgH}_2$  significantly decreased the dehydrogenation onset temperature by 70 °C compared to pristine  $\text{MgH}_2$ , with a notable reduction in the apparent activation energy of the composite. The catalytic effectiveness of  $\text{Ti}_3\text{AlC}_2$  was attributed to its capability to integrate hydrogen atoms into the interstitial sites of its Ti–Al layers.<sup>334</sup> Sun *et al.*<sup>335</sup> fabricated reticulated porous  $\text{Ti}_3\text{AlC}_2$  for use as support material in gas exhaust catalyst devices, leveraging its attributes such as thermal stability, mechanical strength, erosion resistance, low heat capacity, thermal shock resistance, and electronic conductivity, thus enabling its application in electrically heated catalysts. Furthermore, Fashandi *et al.*<sup>336</sup> synthesized thin films of  $\text{Ti}_3\text{AuC}_2$  and  $\text{Ti}_3\text{IrC}_2$ , which formed stable ohmic electrical contacts to SiC even after prolonged exposure to high temperatures in air. These MAX phases containing noble metals exhibit potential for stable electrical contacts in high-temperature power electronics or gas sensors. This Fig. 26 demonstrates the combination of MAX-phase materials, highlighting their use as functional materials to improve performance.

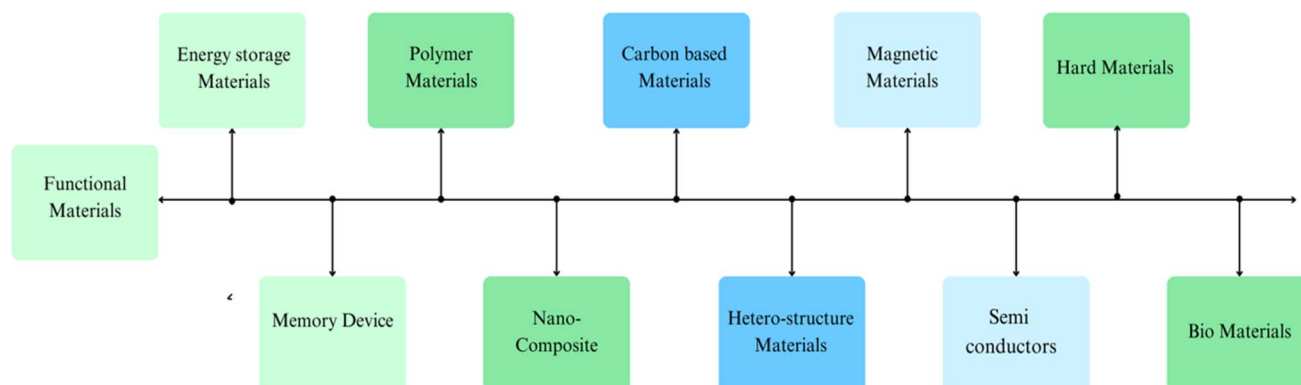


Fig. 26 Application of MAX-phase materials as functional materials.

## 6. Summary and outlook

Recent advancements in MAX phase materials have significantly expanded our understanding of their complex structures, unique properties, and diverse applications. Through innovative synthesis techniques and precise control of composition and microstructure, researchers have unlocked new possibilities for tailoring MAX phase properties to meet the demands of various industries. MAX phases, characterized by their metallic conductivity, ceramic-like hardness, and polymer-like machinability, offer exceptional performance in high-temperature environments, corrosive conditions, and demanding mechanical applications. These materials exhibit remarkable stability, strength, and resistance to degradation, positioning them as key contenders for a wide range of applications, including aerospace, energy storage, electronics, and beyond. Looking ahead, the future of MAX phase materials appears promising, with continued research and development poised to unlock even greater potential for innovation and application. Emerging techniques such as additive manufacturing and nanoscale engineering offer new avenues for fine-tuning MAX phase properties and exploring novel applications in fields such as catalysis, biomedicine, and environmental remediation. Additionally, collaborative efforts between academia, industry, and government agencies will be crucial for advancing fundamental understanding, scaling up production, and accelerating the commercialization of MAX phase materials. By addressing remaining challenges such as processing scalability, cost-effectiveness, and environmental sustainability, MAX phase materials have the potential to revolutionize various industries and pave the way for the development of next-generation materials with unprecedented performance and functionality.

This review has provided a comprehensive review of MAX phases in terms of chemical compositions, microstructures, synthesis methods, properties, and novel applications. Tremendous progress on MAX phases has been made in terms of discovering more MAX phases, characterizing their microstructures and properties, and exploring their potential applications. Future directions for MAX phases include the ongoing search for new MAX phases, the need for thorough experimental investigations into their microstructures and properties, the





improvement of synthesis methods to achieve higher purity, and the characterization of a wide range of chemical and physical properties of newly developed MAX phases. Additionally, there is vast potential for the development of MAX phases as functional materials. The field continues to see rapid growth, with an increasing number of synthesized MAX phases reported each year, exemplifying a true revitalization of the field. Phase stability calculations are also proving useful for predicting new MAX phases for future syntheses, further advancing the field and opening up new opportunities for research and development. Recently, the progress of the new MAX phase synthesis has dramatically increased from earlier. Until now, researchers have discovered about 342 MAX phases, with the majority occurring after 2018. Challenges in MAX phase materials include intricate structural complexities, limited understanding of property correlations, and scalability hurdles for novel applications. Potential solutions involve advanced characterization techniques for structural elucidation, comprehensive property modeling frameworks, and innovative synthesis strategies optimized for industrial scalability. Integration of multi-disciplinary approaches, collaboration between academia and industry, and continual research investment are vital for overcoming these challenges and unlocking the full potential of MAX phase Materials.

## 7. Future directions

Future directions in MAX phase materials study encompass exploring new synthesis routes to tailor properties, elucidating atomic-scale structural dynamics, integrating computational modeling for predictive design, advancing multi-functional applications, and enhancing sustainability through eco-friendly manufacturing processes. These efforts aim to unlock the full potential of MAX phase materials, which are known for their unique combination of metallic and ceramic properties, including high-temperature stability, electrical conductivity, and resistance to oxidation and corrosion.

Exploring new synthesis routes is essential for fine-tuning the properties of MAX phase materials to meet specific application requirements. Researchers are investigating various chemical and physical processes to develop more efficient and scalable methods for producing these materials. Understanding atomic-scale structural dynamics is crucial for optimizing performance. Advanced techniques like high-resolution electron microscopy and spectroscopy are employed to observe and manipulate the atomic arrangements and bonding characteristics within MAX phase materials.

The integration of computational modeling plays a pivotal role in the predictive design of MAX phase materials. By leveraging machine learning algorithms and high-throughput computational methods, scientists can simulate and predict the behavior of these materials under different conditions, thus accelerating the discovery of new compositions with desirable properties.

Advancing multi-functional applications is another significant focus area. MAX phase materials hold promise for a wide range of industries, including aerospace, energy, and

electronics, due to their exceptional properties. Researchers are developing innovative ways to utilize these materials in various applications, such as thermal protection systems, electrical contacts, and energy storage devices.

Enhancing sustainability through eco-friendly manufacturing processes is a critical objective. Developing green synthesis methods and recycling strategies will reduce the environmental impact of producing and using MAX phase materials. Collaborative efforts between materials scientists, engineers, and industry partners are vital for driving innovation and ensuring the successful commercialization of next-generation MAX phase materials.

Emphasis on scalability, cost-effectiveness, and commercial viability will facilitate the widespread adoption of MAX phase materials in critical sectors. Continuous refinement of processing techniques and characterization methods will enable precise control over material properties, leading to breakthroughs in performance and functionality. Ultimately, pursuing these directions will expand the fundamental understanding of MAX phase materials and accelerate their transition from the laboratory to real-world applications.

## Data availability

No primary research results, software or code have been included, and no new data were generated or analyzed as part of this review. All information cited within this review is derived from existing literature and publicly available sources.

## Conflicts of interest

There are no conflicts to declare.

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