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# Preparation of $\text{HMn}_2\text{O}_4$ lithium-ion sieves with low manganese dissolution loss for improved cycling stability

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Manganese-based lithium-ion sieves have become some of the promising adsorbents for extracting  $\text{Li}^+$  from brines. However, manganese dissolution loss (MDL) severely impairs the stability and cyclicity of ion sieves. A novel ozone eluent was first developed to extract  $\text{Li}^+$  from lithium manganese oxides, which decreased MDL decreased from 5.89% to 0.11%, and after ten regeneration cycles, the adsorption capacity retained 85.39% of the initial value, which was better than 55.15% when only hydrochloric acid (HCl) was used as the eluent. Based on these phenomena, the mechanism for the  $\text{O}_3$  lowering of MDL was investigated. First, the catalytic decomposition reaction of  $\text{O}_3$  competed with the disproportionation reaction, and the involvement of  $\text{O}_3$  inhibited the occurrence of the disproportionation reaction. Additionally, the presence of  $\text{O}_3$  and reactive oxygen species provided a preferential electron acceptor compared to  $\text{Mn}^{3+}$  during the migration of electrons from the bulk phase to the surface. In this study, MDL was greatly reduced with a very simple strategy, and the cycling stability of the adsorbent was improved.

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## 1 Introduction

Owing to the strong competition in the new energy field<sup>1,2</sup> and bright prospects in the nuclear energy field,<sup>3</sup> the demand for lithium is high and continues to grow.<sup>4</sup> Although it is currently mainly extracted from ores, the rapid depletion of nonrenewable ores calls for an urgent need to draw on seawater and salt lake brine resources, which account for around 60% of the global reserves. Over the past few decades, plenty of approaches have been proposed for the extraction of lithium from salt lake brines, such as evaporative precipitation,<sup>5</sup> solvent extraction,<sup>6,7</sup> electrochemistry,<sup>8,9</sup> membrane process<sup>10–13</sup> and adsorption.<sup>14,15</sup> Among these choices, lithium-ion sieves have emerged as promising adsorbents for lithium recovery, especially for salt lake brines with low-grade and high  $\text{Mg}^{2+}/\text{Li}^+$  ratio, owing to the exceptional lithium selectivity and large uptake capacity.<sup>16</sup>

Among the inorganic metal-based adsorbents for lithium extraction, Al-based adsorbents have been utilized industrially but are generally unsatisfactory owing to their low adsorbing capacities (2–8  $\text{mg g}^{-1}$ ).<sup>17,18</sup> Ti-based and Mn-based adsorbents exhibit competitive working capacities (20–40  $\text{mg g}^{-1}$ ).<sup>19</sup> In comparison, Mn-based adsorbents are more cost-effective. Hence, a series of spinel-type lithium manganese oxides, including  $\text{LiMn}_2\text{O}_4$ ,<sup>20</sup>  $\text{Li}_4\text{Mn}_5\text{O}_{12}$  (ref. 21) and  $\text{Li}_{1.6}\text{Mn}_{1.6}\text{O}_4$ ,<sup>22</sup> were extensively studied. Notwithstanding this, the applications

were hindered owing to the non-negligible manganese dissolution loss (MDL), and tremendous efforts were directed toward improvements. Doping with cations (Fe, Co, Ni and Mg) was attempted to reduce the disproportionation of  $\text{Mn}^{3+}$ .<sup>23–25</sup> The loss thus decreased to as low as approximately 0.51%, which is encouraging for further developments. Surface coating with oxides,<sup>26,27</sup> fluorides<sup>28</sup> and carbonaceous materials<sup>29</sup> have also been explored. The coating impeded Mn loss, but the adsorption capacity also decreased simultaneously from 28.88  $\text{mg g}^{-1}$  to 25.96  $\text{mg g}^{-1}$  because of the large interfacial impedance.<sup>30</sup>

Similarly, persulfates such as  $\text{K}_2\text{S}_2\text{O}_8$ ,  $\text{Na}_2\text{S}_2\text{O}_8$  and  $(\text{NH}_4)_2\text{S}_2\text{O}_8$  were separately investigated previously as eluents for the desorption of  $\text{Li}^+$ . MLD decreased from approximately 13% to 0.2%.<sup>31</sup> However, for  $\text{K}_2\text{S}_2\text{O}_8$  and  $\text{Na}_2\text{S}_2\text{O}_8$  eluents, the concentration of  $\text{H}^+$  produced by the hydrolysis reaction was low at a temperature of less than 60 °C; therefore,  $\text{H}^+$  and  $\text{Li}^+$  cannot be exchanged adequately. Thus, the elution rate of  $\text{Li}^+$  was less than 10%. Due to the dual hydrolysis characteristic of  $(\text{NH}_4)_2\text{S}_2\text{O}_8$ , the elution rate of  $\text{Li}^+$  in  $(\text{NH}_4)_2\text{S}_2\text{O}_8$  can reach 80% at 20 °C. However, the MDL is higher than 25%. The MDL decreased significantly (below 0.5%) when the temperature was increased to 60 °C. This was due to the fact that the  $\text{SO}_4^{2-}$  generated by the activation of  $\text{S}_2\text{O}_8^{2-}$  by heat during electron migration from the interior of particles to the surface<sup>32</sup> replaces  $\text{Mn}^{3+}$  as the electron acceptor, and thus inhibits the reaction  $\text{Mn}^{3+} \rightarrow \text{Mn}^{2+}$ .<sup>33</sup> The above eluents are only effective at high temperatures, and the cost of the above treatment is too high to be employed industrially. The approaches may also bring huge

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environmental problems, against which a breakthrough is urgently needed.

It is supposed that the lithium manganese oxides are treated with a certain oxidizing eluent, which is pollution-free, effective and cheap to restrain MDL.  $O_3$ , featured with excellent oxidizing ability, is expected herein as a better electron acceptor to restrain manganese reduction. Unlike persulfate, ozone also has a strong oxidizing ability at room temperature, and does not require high-temperature activation. In contrast to hydrogen peroxide, a commonly used oxidant, the preliminary investigations verified that ozone does not damage the lithium manganese oxide structure.

In the present work, the regeneration of lithium manganese oxides with the ozone eluent was first developed. The ozone eluent, consisting of  $0.05 \text{ mol L}^{-1}$  HCl combined with  $O_3$ , not only provided a large amount of  $H^+$  to ensure that  $Li^+$  and  $H^+$  can be fully exchanged, but also limited MDL. The structure of the precursor and the manganese lithium-ion sieve with different elution agents were studied comprehensively by various techniques. The mechanisms of action of ozone were further evaluated to promote a new competitive approach for controlling the MDL.

## 2 Materials and methods

### 2.1 Materials and reagents

Lithium hydroxide monohydrate ( $LiOH \cdot H_2O$ , 99.0%), manganese acetate tetrahydrate ( $MnC_4H_6O_4 \cdot 4H_2O$ , 99.0%), magnesium chloride ( $MgCl_2$ , 99.0%), potassium iodide (KI, 99.0%), potassium bromide (KBr, 99.0%), and potassium bromate ( $KBrO_3$ , 99.8%) were all purchased from the Shanghai Aladdin Biochemical Technology Co., Ltd. Sodium chloride ( $NaCl$ , 97.0%), potassium chloride (KCl, 97%), calcium chloride ( $CaCl_2$ , 97%), sodium thiosulfate ( $Na_2S_2O_3$ , 90%), potassium dichromate ( $K_2Cr_2O_7$ , 99.98%) sodium bicarbonate ( $NaHCO_3$ , 98%), amylum ( $(C_6H_{10}O_5)_n$ , 90.0%), and indigo carmine ( $C_{16}H_8N_2Na_2O_8S_2$ , 90.0%) were all purchased from the Sinopharm Chemical Reagent Co., Ltd. Phosphoric acid ( $H_3PO_4$ , 85%), hydrochloric acid (HCl, 36.0%), and high-purity oxygen ( $O_2$ , 99.999%) were purchased from the Nanjing Special Gas Company Co., Ltd. All reagents were directly used without any further purification or treatment.

### 2.2 Synthesis of the $LiMn_2O_4$ precursor and preparation of the $HMn_2O_4$ ion sieves

The precursor  $LiMn_2O_4$  (LMO) was synthesized according to the solid-state synthesis method.<sup>23</sup>  $MnCO_3$ ,  $LiNO_3$ , and  $LiOH \cdot H_2O$  were added to the 95% ethanol solution in a molar ratio of 2 : 0.63 : 0.39. The mixture was magnetically stirred at 500 rpm for 2 h at 25 °C to form a uniform solution. After being dried at 80 °C, the mixture was ground. The obtained powder was then placed on the corundum ceramic sheet, and calcined in the muffle furnace under the atmosphere of flowing air to gain LMO. During the calcination, the powder was first rapidly heated to 200 °C and held for 2 h, then calcined at 600 °C for 10 h.

LMO (0.15 g) was then dispersed in 150 mL of  $0.05 \text{ mol L}^{-1}$  HCl solution, where the specifically rated  $O_3$  was continuously fed in. The mixture was continuously stirred at 25 °C for 2 h. The solid was obtained through filtration and further washed three times with 200 mL deionized water, and then dried at 80 °C. The products obtained were denoted as  $O_3$ -HMO. For comparison, the product thus obtained without  $O_3$  participation was labeled as HMO.

### 2.3 Characterization

The crystal structure was analyzed *via* an X-ray diffractometer (XRD, Rigaku Miniflex 600, Japan) with  $Cu K\alpha$  radiation at 40 kV, 15 mA, a scanning rate of  $10^\circ \text{ min}^{-1}$ , and the diffraction angle from  $10^\circ$  to  $80^\circ$ . Fourier transform infrared spectroscopy (FT-IR, Thermo Nicolet8700, USA) was used to analyze the chemical bonds and structure of materials. The surface morphology and microstructure were characterized using the scanning electron microscope (SEM, Hitachi S4800, Japan) and the transmission electron microscope (TEM, JEOL JEM-2100 Plus, Japan). The elemental composition in eluted and digested samples was measured using the inductively coupled plasma optical emission spectrometer (ICP-OES, PerkinElmer Optima 3000DV, USA). X-ray photoelectron spectroscopy (XPS, Kratos AXIS Supra, Japan) was carried out to analyze the chemical composition and valence state. The specific surface area, pore size and pore volume were analyzed using the Brunauer–Emmett–Teller method (BET, Micromeritics ASAP2460, USA). Nitrogen adsorption/desorption isotherms were measured in a relative pressure range ( $p/p_0$ ) between 0 and 1.0 to clarify the adsorption properties. The indigo method was used to determine the concentration of  $O_3$  in solution.

### 2.4 Characterization of the adsorption behavior

**2.4.1 Adsorption property.** The adsorption property of HMO and  $O_3$ -HMO was evaluated respectively through the  $Li^+$  adsorption test. The lithium-ion sieve (0.1 g) was soaked in 100 mL of the  $LiOH$  solution buffered with  $NaHCO_3$  ( $pH = 11.5$ ,  $C_{Li^+} = 100 \text{ mg L}^{-1}$ ). The mixture was stirred at 25 °C (298 K) for 24 h to ensure equilibrium. The adsorption capacity was determined according to eqn (1):

$$q_e = (C_0 - C_e)V/m \quad (1)$$

where  $q_e$  refers to the adsorption capacity at equilibrium ( $\text{mg g}^{-1}$ );  $C_0$  and  $C_e$  are the initial and equilibrium concentrations of  $Li^+$  ( $\text{mg L}^{-1}$ ), respectively;  $V$  is the volume of solution (L); and  $m$  is the mass of the adsorbent applied (g).

LMO (0.1 g) was dissolved in the digestion solution constituted by ten drops of 30%  $H_2O_2$  and 20 mL of  $2 \text{ mol L}^{-1}$  HCl solution. Then, the digestion solution was diluted for the mass fractions test of  $Li^+$  and  $Mn^{2+}$ , as shown in eqn (2):

$$W_x = (C_D V_D)/m_D \quad (2)$$

where  $W_x$  is the mass fractions;  $C_D$  represents the mass concentration of the  $Li^+$  or  $Mn^{2+}$  ( $\text{mg L}^{-1}$ );  $V_D$  is the volume of digestion (L); and  $m_D$  is the mass of the LMO applied (g).



**2.4.2 Desorption experiment.** In the lithium desorption experiment, LMO was eluted using O<sub>3</sub> aerating 0.05 mol L<sup>-1</sup> HCl solution in a self-made tubular reactor. The reactor was equipped with a quartz sand core plate at the bottom, and O<sub>3</sub> was generated by an O<sub>3</sub> generator (Tonglin 3S-T15). Samples were collected at various time intervals, and a comparative analysis of MDL and the Li<sup>+</sup> extraction rate under different O<sub>3</sub> concentrations was investigated according to batch experiments. The equation for these calculations is shown as eqn (3):

$$R_x = \frac{C_x V}{m W_x} \quad (3)$$

where  $R_x$  is the mass ratio of leaching  $x$  element (Mn<sup>2+</sup> or Li<sup>+</sup>) to total  $x$  element of LMO (%);  $C_x$  is the mass concentration of  $x$  in the eluent (mg L<sup>-1</sup>);  $V$  is the volume of the eluent (L); and  $m$  is the mass of the LMO (g).

The amount of dissolved O<sub>3</sub> was determined using the indigo method. After the addition of LMO, the eluent composed of hydrochloric acid-ozone (HCl-O<sub>3</sub>) was sampled at different time points, and added to a 25 mL volumetric flask containing 1 mL of standard indigo solution and 5 mL of NaH<sub>2</sub>PO<sub>4</sub>·H<sub>3</sub>PO<sub>4</sub> buffer (pH = 2). The eluent was added until the blue color had clearly decolorized and then diluted to 25 mL, recording the volume of deionized water used. Samplers, along with one blank without O<sub>3</sub>, were collected for absorbance measurement. The O<sub>3</sub> concentration of the eluent can be described as follows in eqn (4):

$$C_{O_3} = \frac{25 M_{O_3} \Delta A}{\epsilon b V} \quad (4)$$

where  $C_{O_3}$  is the concentration of dissolved O<sub>3</sub> in the HCl-O<sub>3</sub> eluent (g mL<sup>-1</sup>); 25 is the volume of the volumetric flask (mL);  $M_{O_3}$  is the molar mass of O<sub>3</sub> (g mol<sup>-1</sup>);  $\Delta A$  is difference absorbance between sample and blank (L mol<sup>-1</sup> cm<sup>-1</sup>);  $b$  is the thickness of the cuvette (cm); and  $V$  is the volume of the eluent (mL).

**2.4.3 Adsorption selectivity.** To test the selectivity of the prepared adsorbent towards Li<sup>+</sup>, a concentrated artificial brine system was utilized, as shown in Table 1. In the competitive adsorption process, 0.15 g of adsorbent was dispersed in 150 mL of the concentrated artificial brine with a pH of 10.5. The mixture was subjected to magnetic stirring for 24 hours to reach adsorption equilibrium. Following this, the saturated adsorbed O<sub>3</sub>-HMO was filtered, washed, and dried. Then, the saturated adsorbed O<sub>3</sub>-HMO and O<sub>3</sub>-HMO were each separately dissolved in H<sub>2</sub>O<sub>2</sub>-HCl digestion solution. The resulting solutions were then diluted for elemental analysis. To evaluate the selectivity performance, the distribution coefficient ( $K_d$ ) and separation factor ( $\alpha_M^{Li}$ ) were calculated according to eqn (5) and (6), respectively:

$$k_d = \frac{C_0 - C_e}{C_e} \times \frac{V \times 1000}{m} \quad (5)$$

**Table 1** Composition of the artificial brine used in this work

Cation	Li <sup>+</sup>	Na <sup>+</sup>	K <sup>+</sup>	Mg <sup>2+</sup>	Ca <sup>2+</sup>
Concentration	682	27 855	9239	71 013	879

$$\alpha_M^{Li} = \frac{k_d(Li)}{k_d(M)} (M = Na^+, K^+, Mg^{2+}, Ca^{2+}) \quad (6)$$

where  $K_d$  is the distribution coefficient of metal ions in solution (mL g<sup>-1</sup>);  $\alpha_M^{Li}$  is the separation factor;  $C_0$  and  $C_e$  represent the mass concentrations of HMO digestion solution and adsorbed saturated HMO digestion solution (mg L<sup>-1</sup>), respectively;  $V$  denotes the volume of the adsorption solution (L); and  $m$  signifies the mass of adsorption-saturated HMO (g).

## 2.5 Cyclic performance

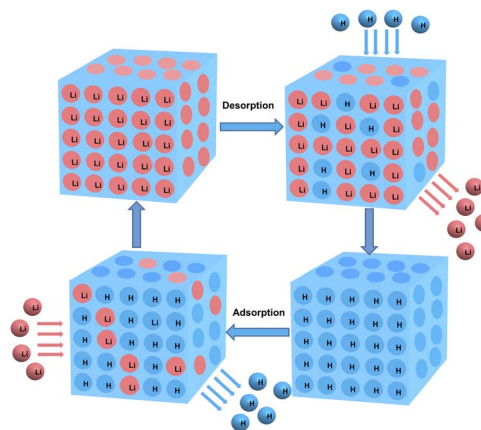
As illustrated in Fig. 1, the adsorption-saturated O<sub>3</sub>-HMO was eluted using O<sub>3</sub>-aerating 0.05 mol L<sup>-1</sup> HCl solution for regeneration. The regenerated O<sub>3</sub>-HMO was used in the subsequent adsorption step. Continuous, repetitive adsorption-desorption experiments were conducted to evaluate the cyclic performance.

## 3 Results and discussion

### 3.1 Characterization of LMO, HMO and O<sub>3</sub>-HMO

The XRD patterns of LMO, HMO and O<sub>3</sub>-HMO are illustrated in Fig. 2a. The characteristic peaks of LMO match well with JCPDS 35-0782, which corresponds to the spinel-structured LiMn<sub>2</sub>O<sub>4</sub>. Both HMO and O<sub>3</sub>-HMO retained the spinel structure after desorption, indicating that the addition of O<sub>3</sub> aeration did not affect the crystalline nature. In addition, since the ionic radius of H<sup>+</sup> is smaller than Li<sup>+</sup>, all of the peaks shifted to a higher degree after elution. Moreover, the intensity of the (111) peak, which correlates positively with the amount of crystalline lithium,<sup>34</sup> was weaker after elution. This result verifies that the ion exchange reaction between H<sup>+</sup> and Li<sup>+</sup> occupying the tetrahedral (8a) sites proceeds topotactically.

The FT-IR spectra of LMO, HMO and O<sub>3</sub>-HMO are shown in Fig. 2b. The absorption bands occurring at 3446 cm<sup>-1</sup> and 1632 cm<sup>-1</sup> in LMO correspond to the stretching and bending vibrations of -OH, respectively, which also occur in HMO and O<sub>3</sub>-HMO at similar positions. Compared to LMO, a new peak appeared at 910 cm<sup>-1</sup> for HMO and 909 cm<sup>-1</sup> for O<sub>3</sub>-HMO, which is attributed to the asymmetric conjugate vibration of H<sup>+</sup>.



**Fig. 1** Schematic diagram of the cyclic application of ion sieves.



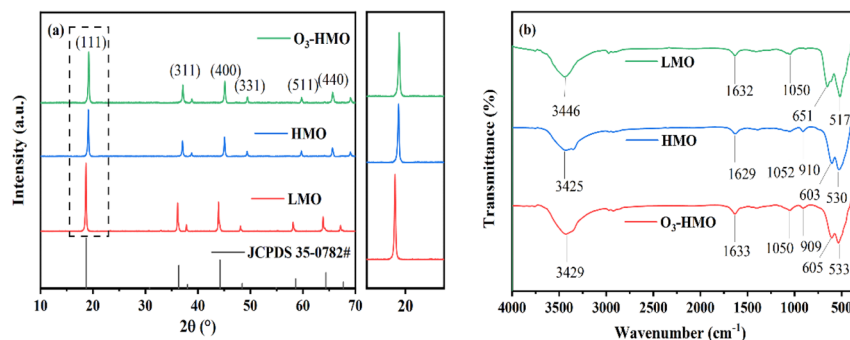


Fig. 2 The powder XRD patterns of (a) LMO, HMO and O<sub>3</sub>-HMO; (b) FT-IR spectra of LMO, HMO and O<sub>3</sub>-HMO.

This further confirmed the occurrence of the ion exchange reaction between H<sup>+</sup> and Li<sup>+</sup>, and is consistent with the results of the XRD diffraction spectra. After elution, the absorption bands in the 400–700 cm<sup>−1</sup> range caused by the asymmetric stretching vibrations of the Mn(III)–O bond and Mn(IV)–O bond in the manganese-oxygen octahedra were shifted due to the disproportionation of Mn<sup>3+</sup>. However, the shift of the peaks was not significant, indicating that the skeletal structure of the [MnO<sub>6</sub>] octahedron is still stable after acid treatment.<sup>33</sup>

The crystal structures and morphologies of LMO, HMO and O<sub>3</sub>-HMO collected by SEM and TEM characterization are shown in Fig. 3. No marked differences were observed between the morphologies of LMO, HMO and O<sub>3</sub>-HMO (Fig. 3a–c), indicating that the acid treatment did not destroy the spinel structure of LMO, but weakened the agglomeration of ion sieves for better dispersion. All three samples exhibited clumped structures with sharp-edged grains, suggesting that the O<sub>3</sub>-aerated delithiation process had little impact on the structure. As shown in Fig. 3d–f, 0.478 nm, 0.476 nm and 0.475 nm are associated with the interplanar crystal spacing of the (311) planes in LMO,

HMO and O<sub>3</sub>-HMO, respectively. The regular and conspicuous lattice fringes manifest that HMO and O<sub>3</sub>-HMO possess good crystallinity, which is consistent with the XRD results.

Fig. 4 depicts the nitrogen adsorption–desorption isotherm curve and pore size distribution curve of the precursor (Fig. 4a) and ion sieves (Fig. 4b–c). The adsorption–desorption isotherm curve of the precursor and ion sieves belong to the type III and type II isotherms classified by IUPAC, respectively. Since there is a significant reduction of the 30–60 nm pores caused by the agglomeration phenomenon, the pore size after elution was mainly below 10 nm, which coincides with the results of the SEM analysis. This is the main reason for the reduction in the average pore size. Furthermore, this decrease resulted from the lattice contraction, which is consistent with the fact that all of the XRD peaks were shifted to a higher degree. The surface area, average pore diameter and pore volume of LMO, HMO and O<sub>3</sub>-HMO were analyzed and are summarized in Table 2. It can be observed that the BET surface area and pore volume of HMO and O<sub>3</sub>-HMO are all larger than LMO. The increase in the pore volume is due to Li<sup>+</sup> being discharged from the three-

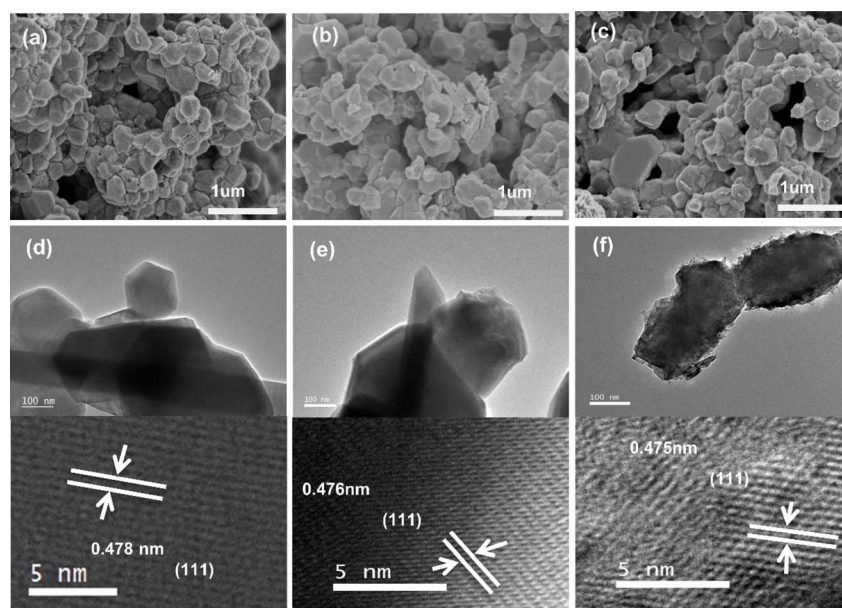


Fig. 3 SEM images of (a) LMO, (b) HMO and (c) O<sub>3</sub>-HMO; TEM images of (d) LMO, (e) HMO, and (f) O<sub>3</sub>-HMO.



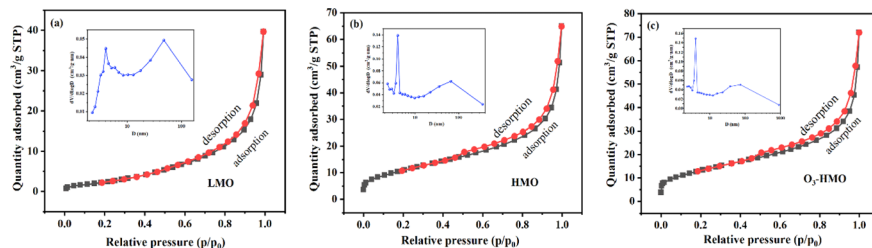


Fig. 4 Nitrogen adsorption-desorption isotherms and pore volume distribution insets: (a) LMO, (b) HMO and (c) O<sub>3</sub>-HMO.

Table 2 Pore structure parameters of LMO, HMO and O<sub>3</sub>-HMO

Samples	BET surface area (m <sup>2</sup> g <sup>-1</sup> )	Average pore diameter (nm)	Pore volume (cm <sup>3</sup> g <sup>-1</sup> )
LMO	10.220	22.899	0.0585
HMO	40.628	8.430	0.0856
O <sub>3</sub> -HMO	48.101	7.371	0.0886

dimensional channels of the spinel structure, and this is also the reason for the increase in the specific surface area of the ion sieve. In addition, the agglomeration of the sample is weakened and the dispersion is better after elution. Thus, HMO and O<sub>3</sub>-HMO have a larger specific surface area compared to LMO, which is consistent with the SEM results.

The XPS spectra of LMO, HMO and O<sub>3</sub>-HMO were recorded to ascertain the surface chemical states and content changes of Mn O and Li before and after delithiation. Fig. 5a and b show the Li 1s spectra and O 1s spectra of LMO, HMO and O<sub>3</sub>-HMO, respectively. The characteristic peaks of Li 1s that appeared in LMO were not detected in HMO and O<sub>3</sub>-HMO. As depicted in Fig. 5b, the intensity of [MnO<sub>6</sub>] decreases compared to the peaks before the ion exchange reaction, while the peak of -OH is enhanced and shifted by 0.2–0.3 eV. These observations indicate that the Li<sup>+</sup>/H<sup>+</sup> exchange delithiation process was completed, and H<sup>+</sup> existed on the surface in the form of -OH groups.<sup>35</sup> The Mn 2p<sub>3/2</sub> results are presented in Fig. 5c. The peaks at 642.7 eV and 641.3 eV, assigned to Mn(IV) and Mn(III), respectively, were found in all three samples. Slight shifts were observed in the delithiated samples. This suggests that the structural transformation of Li-Mn-O to H-Mn-O alters the

chemical environment of Mn. An increase in the proportion of surface Mn(IV) and the corresponding decline in surface Mn(III) were observed in the fitting curve of HMO. This result followed the disproportionation reaction of Mn(III). In the fitting curve of O<sub>3</sub>-HMO, the proportion of Mn(III) also decreased compared to LMO. Whereas only a tiny portion of Mn(II) was detected after elution with 0.05 mol L<sup>-1</sup> HCl solution containing O<sub>3</sub> dosages, this finding indicates that there are other reasons for the decrease in the Mn(III) content.

### 3.2 Desorption performance of LMO with a new type of eluent

**3.2.1 Effect of eluents with different O<sub>3</sub> concentrations on MDL.** The relationship between the MDL of LMO and different O<sub>3</sub> concentrations during the delithiation process is depicted in Fig. 6. The results from the desorption experiments reveal that MDL exhibited a rapid upward trend, reaching 5% and then gradually increasing until the end (5.89%) with no O<sub>3</sub> aeration. However, when the O<sub>3</sub> concentration was controlled within the range of 1.67–5.00 g mg L<sup>-1</sup>, the MDL remained below 0.4%. Notably, when the concentration of O<sub>3</sub> was 2.50 mg L<sup>-1</sup>, the MDL was the lowest, measuring less than 0.12%. Conversely, the MDL with an O<sub>3</sub> concentration of 5.83 mg L<sup>-1</sup> was unsatisfactory, showing an accelerated rising trend along with the delithiation process. An interesting observation was the pink coloration of the eluent during this process. Further analysis *via* UV-Vis spectroscopy of the filtered eluent confirmed the presence of an adsorption band at 460–580 nm with a maximum adsorption at 525 nm, corresponding to the permanganate ion. The generation of permanganate ions was further identified

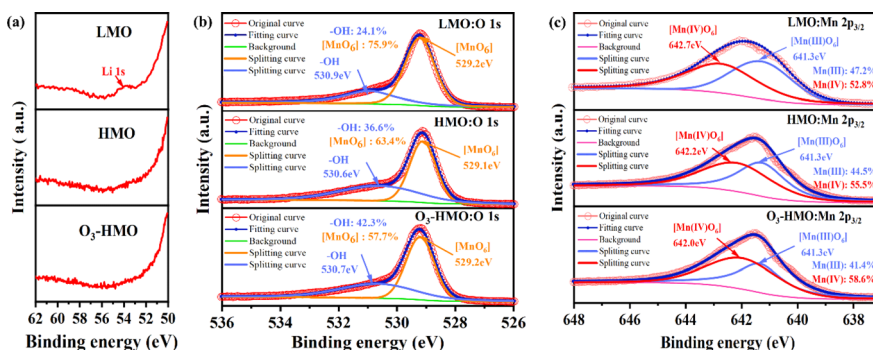


Fig. 5 The XPS fitted splitting for LMO, HMO and O<sub>3</sub>-HMO: (a) Li 1s, (b) O 1s, (c) Mn 2p<sub>3/2</sub>.

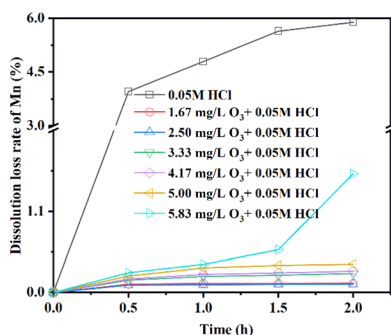


Fig. 6 The MDL of LMO under 0.05 mol L<sup>-1</sup> HCl + *R* mg L<sup>-1</sup> O<sub>3</sub> (*R* = 0, 1.67, 2.50, 3.33, 4.17, 5.00, and 5.83).

through literature investigation, which indicated that many elements, including manganese, can be oxidized to their highest oxidation state. Therefore, we concluded that a lower O<sub>3</sub> concentration of 1.67–5 mg L<sup>-1</sup> significantly reduces MDL, and a high O<sub>3</sub> concentration can lead to the formation of soluble permanganate ions, but can still reduce MDL.

Table 3 summarizes the final lithium extraction and MDL of LMO obtained with different O<sub>3</sub> concentrations. As discussed, the variation of the O<sub>3</sub> concentration had a significant effect on inhibiting MDL. The comparison of the adsorption properties and MDL using eluents consisting of HCl and O<sub>3</sub> with other modification methods is shown in Table 4. Based on the table, it can be seen that LMO retains low MDL and excellent adsorption capacity by using the eluent consisting of HCl and O<sub>3</sub>.

**3.2.2 The mode of action of O<sub>3</sub>.** In order to systematically verify the key role of O<sub>3</sub> in reducing MDL, under the condition of

the O<sub>3</sub> concentration being set to 2.50 mg L<sup>-1</sup>, the change in dissolved O<sub>3</sub> concentration after adding LMO powder was explored by the indigo method. As depicted in Fig. 7, there was a sudden decrease in the dissolved O<sub>3</sub> concentration when the LMO powder was introduced into the O<sub>3</sub>-saturated eluent, and then it finally approached zero. Meanwhile, the MDL initially increased and then stabilized at 0.15% throughout the desorption process. The above results indicate that O<sub>3</sub> reduces MDL significantly.

### 3.3 Mechanism exploration

Based on the finding that the addition of O<sub>3</sub> significantly reduced the MDL, the following explanations were provided. The sharp decrease in the concentration of dissolved O<sub>3</sub>, as depicted in Fig. 7, discloses that the addition of the LMO led to the decomposition of O<sub>3</sub>, and the crystal structure of the LMO remained unchanged after extraction. This process is closely similar to the catalytic decomposition reaction of O<sub>3</sub> on the surface of transition metal oxides. Transition metal oxides with multiple oxidation states, such as manganese, iron, copper, cobalt, nickel, *etc.*, especially manganese oxides, exhibit good catalytic properties for O<sub>3</sub> decomposition.<sup>40</sup> Ma *et al.*<sup>41</sup> found that the electron conduction between coexisting Mn(IV) and Mn(III) oxygen vacancies in the M-OMS-2 catalyst is crucial for the catalytic decomposition of O<sub>3</sub>. According to their findings, the decomposition reaction of O<sub>3</sub> on the surface of LMO proceeded according to the following formulas:<sup>42</sup>

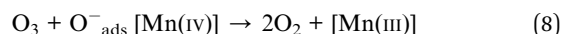
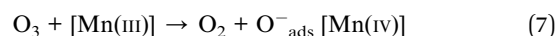


Table 3 The adsorption and MDL performance of products after using the eluent with different O<sub>3</sub> fluxes

O <sub>3</sub> concentration (mg L <sup>-1</sup> )	Manganese dissolution rate (%)	Lithium extraction rate (%)
0	5.89	98.2
1.67	0.126	97.9
2.50	0.113	99.2
3.33	0.257	99.7
4.17	0.289	99.1
5.00	0.383	98.9
5.83	1.61	98.3

Table 4 The comparison of the MDL using the eluent in this work with other modification methods

Adsorbent	Modified mode	C <sub>Li</sub> (mg L <sup>-1</sup> )	Eluted temperature (°C)	Eluent	q <sub>e</sub> (mg g <sup>-1</sup> )	Mn (%)	Ref.
LiMn <sub>2</sub> O <sub>4</sub>	SiO <sub>2</sub> coating	100	—	HCl	33.9	3.9%	36
Li <sub>1.6</sub> Mn <sub>1.6</sub> O <sub>4</sub>	Surface fluorination	350	25	HCl	31.86	1.58%	37
Li <sub>1.6</sub> Mn <sub>1.6</sub> O <sub>4</sub>	Zirconium coating	150	25	HCl	25.96	0.349%	30
Li <sub>1.6</sub> Mn <sub>1.6</sub> O <sub>4</sub>	Mg doping	600	—	HCl	45.8	4.32%	38
LiMn <sub>2</sub> O <sub>4</sub>	Fe doping	50	25	HCl	34.8	0.51%	23
Li <sub>1.6</sub> Mn <sub>1.6</sub> O <sub>4</sub>	Al and S co-doping	42	25	HCl	33.7	3%	39
LiMn <sub>2</sub> O <sub>4</sub>	—	347	80	Na <sub>2</sub> S <sub>2</sub> O <sub>8</sub>	25.72	0.18%	31
LiMn <sub>2</sub> O <sub>4</sub>	—	174	80	Na <sub>2</sub> S <sub>2</sub> O <sub>8</sub>	—	0.5%	34
LiMn <sub>2</sub> O <sub>4</sub>	—	100	25	HCl + O <sub>3</sub>	33.2	0.11%	This work



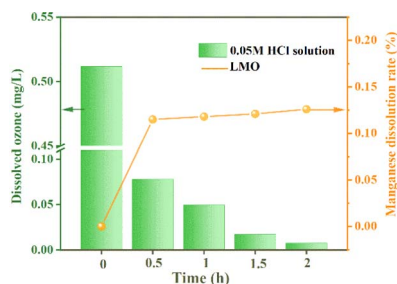
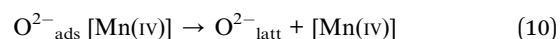
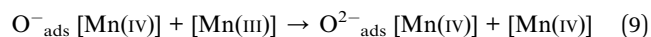


Fig. 7 Dissolved O<sub>3</sub> concentration and MDL after adding LMO.

The proportion of Mn(III) on the surface of synthesized LMO was as high as 47.2%, indicating an abundance of surface oxygen vacancies. This high proportion led to a significant catalytic degradation effect on O<sub>3</sub>. The adsorption of O<sub>3</sub> on the Mn(III) oxygen vacancies on the LMO surface occurred rapidly, and decomposed to oxygen and active oxygen species O<sup>-</sup><sub>ads</sub> [Mn(IV)]. Then, O<sub>3</sub> reacted with active oxygen species O<sup>-</sup><sub>ads</sub> [Mn(IV)] to generate oxygen and Mn(III).<sup>43</sup> At the same time, Mn(III) inside the spinel structure was forced to release an electron to become Mn(IV) due to the exchange of H<sup>+</sup> and Li<sup>+</sup>. The electron freely migrated to the crystal surface and was captured by the surface Mn to dissolve as Mn(II).<sup>32,44</sup> Thus, on the surface, the conversion of Mn(III) → O<sup>-</sup><sub>ads</sub> [Mn(IV)] → Mn(III) and the disproportionation reaction 2Mn(III) → Mn(II) competed with each other.

According to formulas (7) and (8), the ratio of Mn(III) in O<sub>3</sub>-HMO should be the same as in LMO. However, the peak splitting results of Mn 2p<sub>3/2</sub> indicate that the ratio of Mn(III) in O<sub>3</sub>-HMO (Mn(III): 41.4%) greatly decreases compared to LMO (Mn(III): 47.2%). This observation suggests that other reactions

besides formulas (7) and (8) also take place. The catalytic reaction mentioned above illustrates that the content of Mn(III) is closely related to the density of oxygen vacancies. Therefore, the decrease in Mn(III) content also implies a decrease in oxygen vacancies after the reaction, which aligns with the XPS results. Hence, we hypothesize that during the reaction, a portion of the formed oxygen vacancies adsorb oxygen without further reacting with O<sub>3</sub> to generate oxygen, but instead convert into lattice oxygen. The proposed reaction mechanism is as follows:



In addition to the aforementioned speculations, the delithiation process is accompanied by electron transfer. When electrons migrate from the interior of the particle to the surface, Mn(III) accepts the electrons and triggers a disproportionation reaction that results in the MDL. The emergence of O<sub>3</sub> and reactive oxygen species O<sup>-</sup><sub>ads</sub> provides a preferential option as electron acceptors. We hypothesize that the following reactions occur:

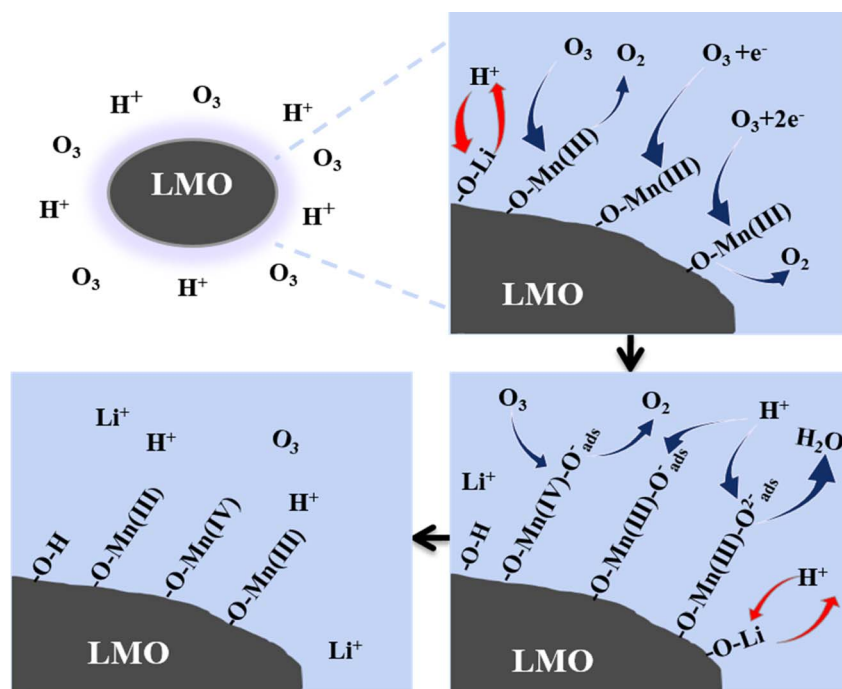
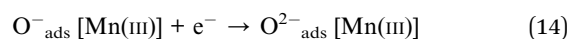


Fig. 8 Mechanism of the Li<sup>+</sup> extraction process using the HCl-O<sub>3</sub> eluent.



The overall role of  $O_3$  in the desorption process can be summarized as follows: during the ion exchange process,  $O_3$  undergoes catalytic decomposition and replaces the surface Mn as the electron group on the LMO surface, which is simultaneously accompanied by partial oxidation of Mn(III) to Mn(IV). The mechanism is shown in Fig. 8.

### 3.4 Static adsorption behavior of lithium-ion sieves

The pH of the solution has a vital influence on the adsorption properties. As shown in Fig. 9a, the adsorption capacity of  $O_3$ -HMO at different initial pH solutions was investigated. The adsorption capacity of  $O_3$ -HMO gradually increased with increasing alkalinity. The enhancement of alkalinity was accompanied by the increase of  $OH^-$  concentration, which was conducive to neutralizing the released  $H^+$ , and further facilitated ion exchange between  $Li^+/H^+$ . Another crucial reason was that the adsorbent surface possessed more negative charges at a high pH.<sup>45</sup> Therefore, the electrostatic attraction between  $Li^+$  and the surface of the adsorbent increased with initial pH, which resulted in a greater adsorption affinity for  $Li^+$  and could further enhance the adsorption capacity. The temperature of

the solution also has a vital influence on the adsorption properties. As shown in Fig. 9b, the adsorption capacity of  $O_3$ -HMO was investigated at different initial temperature solutions. The increase of solution temperature would enhance the adsorption capacity, indicating that the adsorption process is an endothermic reaction.

As shown in Fig. 10a, HMO and  $O_3$ -HMO were immersed in a  $NaHCO_3$  buffered LiOH solution ( $pH = 11.5$ ,  $C_{Li^+} = 100 \text{ mg L}^{-1}$ ) at  $25^\circ\text{C}$  for adsorption. Within the initial 2 h, the adsorption capacity reached about 85% of the saturated adsorption capacity, and equilibrium was achieved within 24 hours. To investigate the adsorption kinetics, the adsorption data in Fig. 10a were fitted by pseudo-first-order and pseudo-second-order kinetic models,<sup>46,47</sup> represented by eqn (16) and (17), respectively. The results in Fig. 10b and c show that the corresponding fitting parameters obtained from the pseudo-second-order kinetic model were superior to those from the pseudo-first-order kinetic model, indicating that the pseudo-second-order kinetic model provides a more accurate description of  $Li^+$  adsorption, which belongs to the chemisorption process. Table 5 lists the specific fitting parameters of the adsorption isotherms.

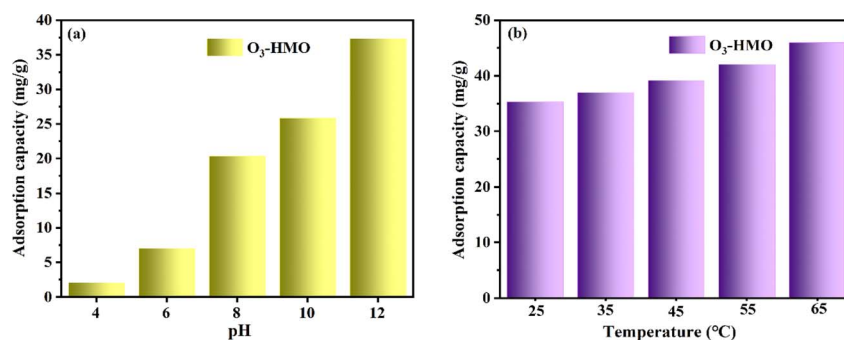


Fig. 9 Effects of different conditions on the adsorption capacity of  $O_3$ -HMO: (a) pH ( $C_{Li^+} = 100 \text{ mg L}^{-1}$ ,  $T = 25^\circ\text{C}$ ), (b) temperature ( $C_{Li^+} = 100 \text{ mg L}^{-1}$ ,  $pH = 11.5$ ).

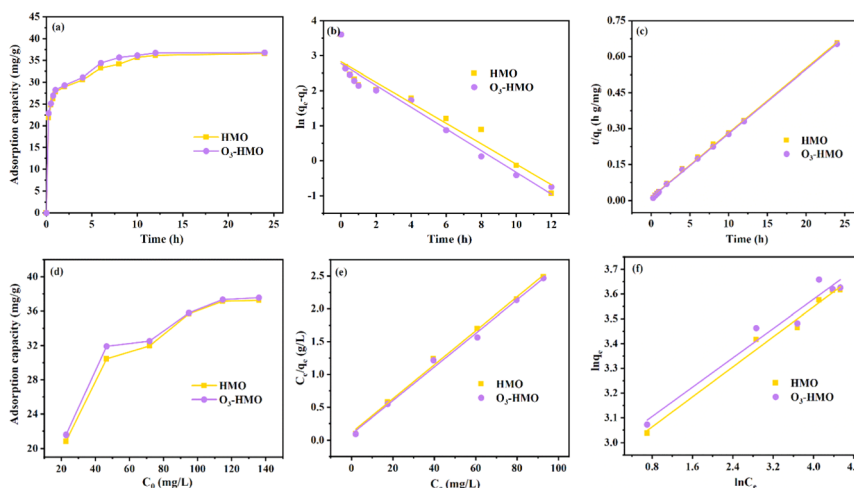


Fig. 10 (a) Variation in the adsorption capacity with time. (b) Pseudo-first-order kinetic model and (c) pseudo-second-order kinetic model. (d) Variation in the adsorption capacity with different initial lithium concentrations. (e) Langmuir isothermal model and (f) Freundlich isothermal model.





Table 5 Pseudo-first-order kinetic and pseudo-second-order kinetic parameters

Material	$q_{e,exp}$	Pseudo-first-order			Pseudo-second-order		
		$k_1$ ( $h^{-1}$ )	$q_{e,cal}$ ( $mg\ g^{-1}$ )	$R^2$	$k_2$ ( $g\ mg^{-1}\ h^{-1}$ )	$q_{e,cal}$ ( $mg\ g^{-1}$ )	$R^2$
HMO	36.54	0.2931	16.91	0.92442	0.06	37.05	0.9989
O <sub>3</sub> -HMO	36.78	0.3112	16.05	0.9401	0.07	37.30	0.9994

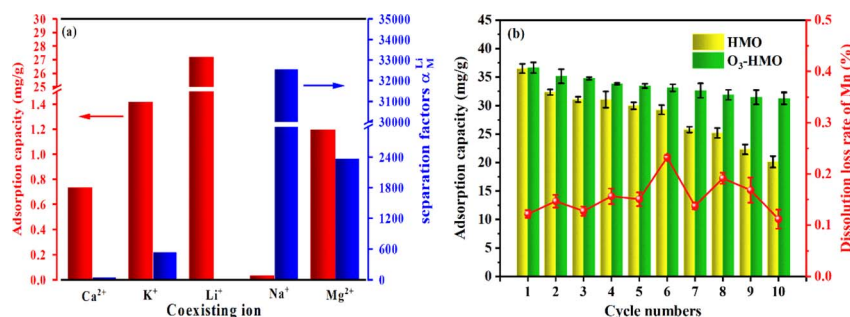


Fig. 11 Recovery of Li<sup>+</sup> from artificial brine via O<sub>3</sub>-HMO: (a) adsorption selectivity towards Li<sup>+</sup>, Na<sup>+</sup>, K<sup>+</sup>, Mg<sup>2+</sup> and Ca<sup>2+</sup>; (b) dissolution loss of Mn and Li<sup>+</sup> adsorption capacity in the cycling process.

$$\ln(q_e - q_t) = \ln q_e - k_1 t \quad (16)$$

$$\frac{t}{q_t} = \frac{t}{q_e} + \frac{1}{k_2 q_e^2} \quad (17)$$

where  $q_e$  is the adsorption capacity ( $mg\ g^{-1}$ );  $q_t$  is the adsorption capacity at different times ( $mg\ g^{-1}$ );  $t$  is the adsorption time;  $k_1$  ( $h^{-1}$ ) and  $k_2$  ( $g\ mg^{-1}\ h^{-1}$ ) are the rate constants of the pseudo-first-order and pseudo-second-order kinetic models, respectively.

As shown in Fig. 10d, HMO and O<sub>3</sub>-HMO were immersed in different lithium concentration solutions ( $pH = 11.5$ ,  $C_0 = 20$ – $135\ mg\ L^{-1}$ ) at  $25\ ^\circ C$  for adsorption to investigate the effect of  $C_0$  on the equilibrium adsorption capacity. The results indicate that the equilibrium adsorption capacity increased sharply with the increase of  $C_0$ , but the adsorption capacity was close to saturation when  $C_0$  reached about  $110\ mg\ L^{-1}$ . The adsorption data in Fig. 10d were fitted by Langmuir and Freundlich models<sup>48,49</sup> to examine the uptake behavior, presented as eqn (18) and (19), respectively. The fitted curves in Fig. 10e and f demonstrate that the Li<sup>+</sup> adsorption process aligns well with a monolayer Langmuir-type adsorption with a correlation coefficient. This indicates that the adsorption behavior of Li<sup>+</sup> on the HMO particles hinges on the completion of the chemisorption monolayer.

$$\frac{C_e}{q_e} = \frac{C_e}{q_m} + \frac{1}{k_L q_m} \quad (18)$$

$$\ln q_e = \frac{1}{n} \ln C_e + \ln k_F \quad (19)$$

where  $C_e$  denotes the equilibrium concentration of Li<sup>+</sup> ( $mg\ L^{-1}$ );  $q_e$  is the equilibrium adsorption capacity ( $mg\ g^{-1}$ );  $q_m$  is the theoretical maximum adsorption capacity ( $mg\ g^{-1}$ );  $k_L$  represents the constant of the Langmuir isotherm ( $L\ mg^{-1}$ ); and  $k_F$  and  $n$  are the parameters of the Freundlich equation ( $L\ g^{-1}$ ).

### 3.5 Selectivity and cyclic performance

The selective adsorption results are depicted in Fig. 11a. The equilibrium adsorption capacity of O<sub>3</sub>-HMO for highly concentrated competing cations in artificial brine water did not exceed  $1.5\ mg\ g^{-1}$ . However, the adsorption capacity of Li<sup>+</sup> reached  $27.2\ mg\ g^{-1}$ . Although it was below the adsorption capacity in the NaHCO<sub>3</sub>-buffered LiOH solution owing to the lower pH,<sup>50</sup> it still exhibited a much higher  $q_e$  than the other coexisting cations. The high selectivity of the lithium-ion sieve for Li<sup>+</sup> originates from the “ion sieve effect”, which is the three-dimensional channel that theoretically only allows Li<sup>+</sup> and ions with a smaller radius to pass through. Thus, the lithium-ion sieve can screen and memorize the target Li<sup>+</sup> ions. Although the ionic radius of Mg<sup>2+</sup> ( $0.072\ nm$ ) is similar to that of Li<sup>+</sup> ( $0.076\ nm$ ), the separation factor of Li<sup>+</sup> to Mg<sup>2+</sup> is still as high as 2367. This is because the hydration energy of Mg<sup>2+</sup> ( $-1830\ kJ\ mol^{-1}$ ) is much larger than the hydration energy of Li<sup>+</sup> ( $-475\ kJ\ mol^{-1}$ ), resulting in a higher dehydration barrier for entry into the 16c–8a–16c channel. This further demonstrates that O<sub>3</sub>-HMO exhibits excellent selectivity for lithium recovery in high Mg<sup>2+</sup>/Li<sup>+</sup> ratio saline systems.

Regenerability and excellent structural stability are crucial for further industrial applications. Fig. 11b presents the cyclic performance of LMO treated with O<sub>3</sub>-HCl or HCl. The MDL of LMO eluted with O<sub>3</sub>-HCl was consistently lower than 0.3%, far below the 5.89% observed for the HCl-treated sample in this article. Although there was a gradual decrease in the Li<sup>+</sup> uptake, the tenth adsorption capacity remained at about 85.39% of the original capacity. The good cyclic stability and low MDL prove that O<sub>3</sub> in combination with HCl is a better method than using HCl alone.

## 4 Conclusions

In this study, a novel eluent consisting of  $0.05\ mol\ L^{-1}$  HCl combined with O<sub>3</sub> was used to address the issue of MDL.



Notably, the introduction of this eluent did not alter the spinel crystal structure of the material. By optimizing the O<sub>3</sub> concentration of 2.50 mg L<sup>-1</sup>, the MDL of LMO fell from 5.89% (without O<sub>3</sub> dosage) to a mere 0.11%. The material also exhibited excellent stability during cyclic tests. Even after 10 adsorption-desorption cycles, the adsorption capacity of LMO remained above 31.27 mg g<sup>-1</sup> and the MDL remained below 0.3%, owing to the beneficial effects of O<sub>3</sub> on the LMO. Furthermore, the HMO demonstrated remarkable selectivity for Li<sup>+</sup> even in the presence of various coexisting ions. The application of the HCl-O<sub>3</sub> eluent represents a promising strategy to prevent MDL and improve the cycling stability. In addition, LMO has the problem of high loss and difficult recovery, as it exists in the form of a powder. Therefore, further work needs to be carried out to select suitable composite materials and form technologies to immobilize the powdery material into different forms to facilitate its industrial application.

## Author contributions

Longyan Song: experimental design, conceptualization, methodology, formal analysis, writing – original draft. Minxia Liu: methodology, formal analysis, investigation. Min Nian: investigation. Gang Yang: conceptualization, writing – review & editing.

## Conflicts of interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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