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# Fullerene-C<sub>60</sub> and PCBM as interlayers in regular and inverted lead-free PSCs using CH<sub>3</sub>NH<sub>3</sub>SnI<sub>3</sub>: an analysis of device performance and defect density dependence by SCAPS-1D†

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One of the challenges hindering the commercialization of perovskite solar cells (PSCs) is the presence of toxic metals such as lead in their composition. Simulation studies using SCAPS-1D have already been conducted on lead-free PSCs to find optimized solar cell parameters, having tin as the primary candidate for replacing lead in perovskites. Here, we used fullerene-C<sub>60</sub> and its derivative PCBM as interlayers in a lead-free tin-based PSC between the ETL (ZnO) and the perovskite MASl in both regular and inverted configurations of PSCs using SCAPS-1D software. To the best of our knowledge, this is the first simulation study reporting the impact of using fullerene-C<sub>60</sub> and PCBM as interlayers in lead-free PSCs. The defect density ( $N_t$ ) of the perovskite material is varied, allowing us to observe its influence on the power conversion efficiency (PCE). Using an  $N_t$  value of  $10^{17} \text{ cm}^{-3}$  without the interlayer, the PCE was 6.90% and 3.72% for regular and inverted devices. Using PCBM as an interlayer improves the efficiency of both simulated PSCs, achieving a maximum PCE of 8.11% and 5.26% for the regular and inverted configurations, respectively. Decreasing the  $N_t$  from  $10^{17} \text{ cm}^{-3}$  to  $10^{16} \text{ cm}^{-3}$  caused a significant increase in efficiency, reaching 13.38% (n-i-p) and 10.00% (p-i-n). Finally, using the optimized parameters and an ideal  $N_t$  value ( $10^{13} \text{ cm}^{-3}$ ), both PSCs achieved a PCE close to 30%.

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## 1 Introduction

The Perovskite-based solar cells as light-absorbing materials (PSCs) are considered an emerging photovoltaic technology with great potential due to the high power conversion efficiency (PCE) already achieved, exceeding 25%, and also due to the lower production costs compared to silicon-based solar cells.<sup>1</sup> Planar PSCs can be fabricated in regular (n-i-p) and inverted (p-i-n) configurations depending on whether the light is irradiated first onto the electron transport layer (ETL) or the hole transport layer (HTL). There are still challenges for PSCs to be reproducible and commercially viable, including the low stability of PSCs in the presence of air and moisture and the presence of toxic metals such as lead in their composition.<sup>2</sup>

Tin is one of the main candidates for replacing lead in PSCs due to their similar electronic configuration. In addition, the high optical absorption coefficients of tin and its high tolerance

to defects in the absorber material structure enable devices to deliver enhanced performance. Despite the similarities between these two metals and the non-toxicity of Sn<sup>2+</sup> ions, the greater stability of tin in its oxidation state Sn<sup>4+</sup> makes the device highly sensitive to the environment.<sup>3-5</sup>

One of the alternatives to reduce the use of lead in PSCs is the Pb-Sn mixed perovskites. The binding energy of the electron-hole pairs of mixed perovskites is lower compared to lead-only PSCs. As a result, energy losses during exciton diffusion and dissociation are reduced in Pb-Sn PSCs, potentially enhancing the PCE. Better results in Pb-Sn mixed PSCs are found when they are in an inverted configuration.<sup>6</sup>

In order to understand why Pb-Sn mixed PSCs in regular configuration (n-i-p) do not provide good results when compared to inverted PSCs (iPSCs), Hamada *et al.*<sup>7</sup> fabricated planar solar cells in regular and inverted configurations using a Pb-Sn mixed perovskite as the light-absorbing layer. It has been observed that both Pb and Sn strongly bind to the surface of the ETL TiO<sub>2</sub>, forming Ti-O-Pb and Ti-O-Sn bonds. However, while the Ti-O-Pb bonds help reduce charge recombination by acting as a surface passivation layer on the ETL, Ti-O-Sn bonds increase the trap density and the charge recombination in the absorber material. This fact can explain why Sn-

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only-based PSCs still exhibit low efficiency compared to Pb-based ones, especially in the regular configuration since the perovskite layer is deposited directly on the ETL in this structure. The authors used a carboxylic acid fullerene as a passivation layer between the perovskite and ETL in regular PSC to mitigate the charge recombination in the device, which increased the PCE from 5.14% to 7.91%.

Lead-free PSCs, such as Sn-based PSCs, have been extensively studied. Some experimental works have already been related, but PCE remains low compared to Pb-based PSCs. Therefore, various strategies have been employed to enhance the efficiency of these devices. One approach involves incorporating different additives, such as SnF<sub>2</sub>, into the perovskite layer to suppress Sn<sup>2+</sup> oxidation within the device.<sup>8–10</sup>

Composition engineering is another method widely applied in Sn-based PSCs,<sup>4,11</sup> as exemplified by the pioneering work of Hao *et al.*<sup>12</sup> The authors achieved a PCE of 5.73% using composition and bandgap engineering in an n-i-p PSC, using a perovskite composed of halide anions mixture, CH<sub>3</sub>NH<sub>3</sub>-SnIBr<sub>2</sub>. Nishimura *et al.*<sup>13</sup> tested different proportions of ethylammonium iodide (EAI) in the perovskite (FA<sub>0.9</sub>-EA<sub>0.1</sub>)<sub>0.98</sub>EDA<sub>0.01</sub>SnI<sub>3</sub> doped with GeI<sub>2</sub> to achieve improved alignment of band levels between the absorber and charge extraction layers, thereby enhancing the efficiency in lead-free PSCs to 13%. Zhu *et al.*<sup>14</sup> use the trimethylthiourea as an additive in the spin coating stage of FASnI<sub>3</sub> films and achieved higher experimental efficiency in lead-free PSCs of 14%. Finally, interface engineering is also employed to improve the stability of PSCs. In this method, the charge transfer between the different interfaces of the device is optimized to reduce trap states between the absorber material and the charge extraction layers, which can improve the quality of perovskite film and the charge mobility in the device.<sup>15</sup> Better deposition methods of perovskite films on ETL/HTL are also necessary to enhance PSC performance since the film quality of perovskite directly influences the number of defects present in the material, which impacts the efficiency of the solar cell.<sup>16,17</sup>

Fullerene-C<sub>60</sub> and its derivatives, especially [6,6]-phenyl-C<sub>61</sub>-butyric acid methyl ester (PCBM), are extensively used as ETLs in PSCs due to their efficient electron-accepting properties, which assist in electron extraction since they have the level of their lowest unoccupied molecular orbitals (LUMO) close to the conduction band level of perovskites.<sup>18</sup> Their use also enables the decrease in charge recombination between the solar cell layers due to the capability of fullerene derivatives to passivate trap states in the device.<sup>19–21</sup> The passivation of perovskite films using fullerene derivatives is a very used strategy in Pb-based PSCs<sup>22,23</sup> and they have also been used as interlayers and additives in Pb-based PSCs.<sup>24–30</sup> The interlayers can be considered a crucial factor for enhancing the PCE in photovoltaic devices due to their potential to directly influence the success of charge transfer between the layers of PSCs.<sup>31</sup>

Previous experimental studies employing fullerene derivatives as interfacial layers between perovskite and ETL have indicated that the optimal interlayer thickness is typically around 10 to 15 nm.<sup>25,32–34</sup> Li *et al.*<sup>35</sup> discuss in their work that despite some experimental findings suggesting that the device

efficiency is maximized with fullerene derivative interlayers of approximately 40 nm, their study indicates that ultrathin films of PCBM, as thin as 5 nm, yield superior results when applied as interlayers. Seo *et al.*<sup>36</sup> discussed in their work that a thinner PCBM layer may enhance the overall performance of the solar cell as long as this layer can adequately cover the perovskite film's surface.

The use of fullerene derivatives as interlayers or additives in mixed Sn–Pb PSCs has been addressed in some studies, such as the work by Rajagopal *et al.*,<sup>20</sup> where a fluoroalkyl-substitute fullerene was employed as an additive in the mixed perovskite, helping in defect passivation within the material and reducing trap states and charge recombination. Meanwhile, in the work of Hu *et al.*<sup>18</sup> three fullerene derivatives (IPH, IPB and PCBM) was used as interlayers between the Pb–Sn mixed perovskite and the ETL (fullerene-C<sub>60</sub>). The authors observed that using IPH derivative as an interlayer presented promising results in the device's parameters. However, the use of fullerene derivatives as interlayers or additives in lead-free PSCs still needs to be explored. For example, Chen *et al.*<sup>37</sup> synthesized three new multifunctional ionic fullerene halides and used them in small quantities as additives in the perovskite FASnI<sub>3</sub> to improve perovskite film quality in inverted PSCs. The device using the fullerene derivative C<sub>60</sub>-RNH<sub>3</sub>-Br achieved an efficiency of 11.74% due to its grain boundary passivation effect.

Although experimental and theoretical studies aiming to reduce the use of Pb in PSCs have already been described, many parameters can still be modified to achieve better solar cell efficiency. In solar cell simulations, it is possible to modify the parameters in the interfaces between the layers, evaluating the influence of possible defects, which can save both time and financial resources during the device construction process in the laboratory.<sup>38,39</sup> One of the software used in PSC simulations is the Solar Cell Capacitance Simulator in One Dimension (SCAPS-1D) developed by Niemegeers and Burgelman's research group.<sup>40</sup> SCAPS-1D is free software based on Poisson's equation that enables the simulation of thin-film polycrystalline heterojunction solar cells and permits the introduction of different input parameters for a simulation, making it a valuable tool for assisting in the design and investigation of new solar cells.

The PSCs simulations using SCAPS-1D have been employed in many works involving the methylammonium lead iodide perovskite (MAPI) or mixed perovskites.<sup>41–45</sup> In recent years, simulation studies in SCAPS-1D have been performed specifically about lead-free PSCs<sup>46–51</sup> and many of them have used fullerene-C<sub>60</sub> and its derivatives as ETLs.<sup>52–54</sup>

Some simulation works in SCAPS-1D were found using interlayers between ETL/HTL and the perovskite. For example, in the work of Karthick *et al.*,<sup>55</sup> a regular Pb-based PSC using bismuth iodide as an interface layer between HTL and MAPI perovskite, was simulated and achieved a PCE of 24%. Mohandes *et al.*<sup>56</sup> used fullerene-C<sub>60</sub> as an interlayer between ETL and Pb-based perovskite with a mixed composition of anions and cations. They optimized the different parameters and achieved a PCE of 31.2% for a regular PSC using ZnO/C<sub>60</sub> as ETL and interlayer, respectively, when the value of a defect density ( $N_t$ ) in the perovskite layer was  $2.0 \times 10^{14} \text{ cm}^{-3}$ .



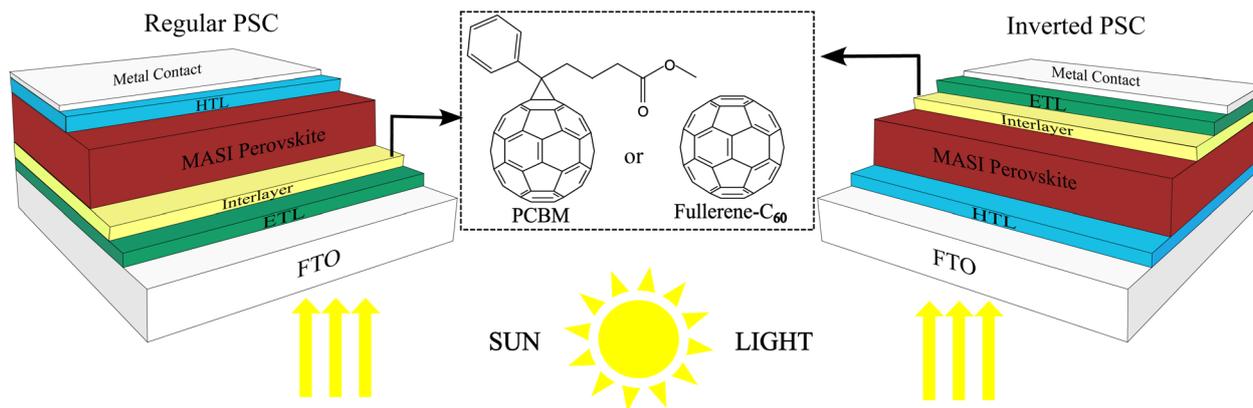


Fig. 1 Interface engineering using fullerene-C<sub>60</sub> and PCBM as interlayers between ETL and perovskite.

In our research, we did not find any studies involving simulations in SCAPS-1D using fullerene-C<sub>60</sub> and its derivative PCBM as an interlayer between the ETL and the perovskite in lead-free PSCs, such as CH<sub>3</sub>NH<sub>3</sub>SnI<sub>3</sub> (MASI). Besides that, the number of studies using simulations of devices in a regular configuration (n-i-p) is lower when compared to those using an inverted configuration (iPSCs). This occurs because, experimentally, the inverted configuration has advantages in solar devices, such as the low temperatures required for processing and lower hysteresis.<sup>57</sup>

In this way, our work aims to investigate how the device efficiency in regular and inverted configurations can be optimized using fullerene-C<sub>60</sub> and its derivative PCBM as interlayers between an inorganic ETL and the light-absorbing layer in lead-free PSCs using MASI through SCAPS-1D simulations (Fig. 1).

## 2 Materials and methods

Hao *et al.*<sup>12</sup> used composition engineering to optimize regular lead-free PSCs, thus achieving a PCE of 5.23% in their device using MASI perovskite (Spiro-MeOTAD/MASI/TiO<sub>2</sub>/FTO). Here, we use this solar cell as a means of validation and reference to simulate regular PSCs. We perform modifications, such as the inclusion of interlayers and changes in the ETL/HTL, in order to optimize the PSC. The solar cell developed by Hao *et al.*<sup>12</sup> has also been used as a reference model in other simulation studies using SCAPS-1D.<sup>38,39</sup>

For simulations of inverted PSCs, we use the work of Wang *et al.*<sup>58</sup> as a reference, where an iPSC with the configuration PEDOT:PSS/MASI/PCBM/BCP was fabricated using the method of ion exchange and insertion reactions for layer deposition with a time of 60 minutes, achieving a PCE of 7.78%. The control iPSC using the one-step deposition method in this study achieved an efficiency of only 1.62%, even using the same HLT/ETL and SnF<sub>2</sub> as an additive. This PCE was similar to those achieved by the iPSC using the new method with a time of 20 minutes (1.39%). Our simulation used as a validation method did not consider the method of ion exchange/insertion reactions for layer deposition and achieved an efficiency close to the control device of 1.18%. All the output parameters obtained

with our simulation are very close to the device using the new method with 20 minutes time described in Wang *et al.*<sup>58</sup> as shown in Table 1.

The thicknesses used to simulate the PSCs were 350 nm to MASI perovskite in regular and inverted configurations, and 200 nm to both HTLs (PEDOT:PSS and Spiro-MeOTAD), based on information from Hao *et al.*<sup>12</sup> and Wang *et al.*<sup>58</sup> The thickness used for the ETLs was 30 nm to TiO<sub>2</sub> and 50 nm to PCBM. Finally, the value of  $N_t$  used in the simulations is  $4.5 \times 10^{17} \text{ cm}^{-3}$ .

The output parameters obtained in our simulations and those described in the reference articles of Hao *et al.*<sup>12</sup> and Wang *et al.*<sup>58</sup> are presented in Table 1. The output parameters from simulated PSCs in both configurations are close to the experimental values.

The values of input parameters used in our work, summarized in Tables 2–4 were taken from reference studies.<sup>38,39,46</sup> The parameters referring to the HTLs PEDOT:PSS, Spiro-MeOTAD, and the ETL TiO<sub>2</sub> are presented in Table S1 in ESI (ESI).†

In our work, we simulated PSCs in regular and inverted configurations using fullerene-C<sub>60</sub> and PCBM as interlayers, varying their thickness from 5 nm to 15 nm. First, the HTLs (Spiro-MeOTAD, PEDOT:PSS and CuI) and the ETLs (TiO<sub>2</sub> and ZnO) are optimized. The MASI thickness varied between 150–800 nm, and the  $N_t$  of perovskite varied from  $4.5 \times 10^{13} \text{ cm}^{-3}$  to  $4.5 \times 10^{17} \text{ cm}^{-3}$ .

## 3 Results and discussion

Here, we discuss the main results obtained by optimizing different parameters in both configurations of PSCs using

Table 1 Output parameters of experimental n-i-p and p-i-n PSCs<sup>12,58</sup> and of simulated PSCs in SCAPS-1D.  $V_{oc}$  is the open circuit voltage,  $J_{sc}$  is the short circuit current density, FF is the fill factor and PCE is the device's power conversion efficiency

PSC	$V_{oc}$ (V)	$J_{sc}$ (mA cm <sup>-2</sup> )	FF (%)	PCE (%)
Hao <i>et al.</i> (2014) <sup>12</sup>	0.68	16.30	48.00	5.23
SCAPS-1D simulation	0.68	17.87	49.99	6.12
Wang <i>et al.</i> (2020) <sup>58</sup>	0.61	6.52	35.00	1.39
SCAPS-1D simulation	0.55	5.84	37.15	1.18



**Table 2** Input parameters used for simulations in SCAPS-1D.  $E_g$  is the materials bandgap,  $\epsilon_r$  is the relative permittivity,  $\chi$  is the electron affinity,  $N_c$  and  $N_v$  are the effective conduction and valence band density,  $\mu_e$  and  $\mu_h$  are the electron and hole mobility,  $N_D$  and  $N_A$  are the donor and acceptor concentration and  $N_t$  is the defect density of the material

	FTO <sup>39</sup>	HTL	Perovskite	ETL	ETLs/Interlayers	PCBM <sup>46</sup>
Parameters/Materials	FTO <sup>39</sup>	CuI <sup>55,59–61</sup>	MASI <sup>12,38</sup>	ZnO <sup>46,60</sup>	C <sub>60</sub> (ref. 46, 62 and 63)	PCBM <sup>46</sup>
Thickness (nm)	500	Variable	Variable	30	Variable	Variable
$E_g$ (eV)	3.50	2.98	1.30	3.20	1.70	2.00
$\chi$ (eV)	4.00	2.10	4.17	4.26	3.90	3.90
$\epsilon_r$	9.00	6.50	8.20	9.00	4.20	4.00
$N_c$ (cm <sup>-3</sup> )	$2.20 \times 10^{18}$	$2.80 \times 10^{19}$	$1.0 \times 10^{18}$	$2.00 \times 10^{18}$	$8.00 \times 10^{19}$	$1.00 \times 10^{21}$
$N_v$ (cm <sup>-3</sup> )	$1.80 \times 10^{19}$	$1.00 \times 10^{19}$	$1.0 \times 10^{18}$	$1.80 \times 10^{19}$	$8.00 \times 10^{19}$	$2.00 \times 10^{20}$
$\mu_e$ (cm <sup>2</sup> V <sup>-1</sup> s <sup>-1</sup> )	20	100	1.6	100.00	0.08	0.02
$\mu_h$ (cm <sup>2</sup> V <sup>-1</sup> s <sup>-1</sup> )	10	2.00	1.6	5.00	$3.5 \times 10^{-3}$	0.02
$N_A$ (cm <sup>-3</sup> )	—	$1.00 \times 10^{18}$	$3.2 \times 10^{16}$	—	—	—
$N_D$ (cm <sup>-3</sup> )	$2.00 \times 10^{19}$	—	—	$1.50 \times 10^{17}$	$2.60 \times 10^{17}$	$1.00 \times 10^{20}$
$N_t$ (cm <sup>-3</sup> )	$1.00 \times 10^{15}$	$1.00 \times 10^{15}$	Variable	$1.00 \times 10^{15}$	$1.00 \times 10^{14}$	$1.00 \times 10^{14}$

**Table 3** Input parameters of interface defect layers.<sup>64</sup>

Parameters and units	ETL/MASI	HTL/MASI
Defect type	Acceptor	Acceptor
Capture cross section for electrons and holes (cm <sup>2</sup> )	$1.0 \times 10^{-17}$ $1.0 \times 10^{-18}$	$1.0 \times 10^{-18}$ $1.0 \times 10^{-19}$
Energetic distribution	Single	Single
Energy level with respect to $E_v$ (above $E_v$ , eV)	Above the highest EV	Above the highest EV
Total density (cm <sup>-3</sup> )	$1.0 \times 10^9$	$1.0 \times 10^9$

**Table 4** Work function of different back metal contacts<sup>65</sup>

Back metal contact	Ag	Cu	Au	Ni	Pt
Work function	4.26	4.65	5.10	5.15	5.65

version 3.3.08 of SCAPS-1D. All the simulations were realized using AM 1.5 G solar spectrum irradiance with 300 K of temperature.

### 3.1 Optimization of HTL and ETL in n-i-p and p-i-n PSCs, using $N_t = 4.5 \times 10^{17} \text{ cm}^{-3}$

Initially, the ETL and HTL were varied to analyze how the changes can influence the efficiency in solar cells of Hao *et al.*<sup>12</sup> and Wang *et al.*<sup>58</sup> in both configurations, considering the interfacial defects and using a high value of  $N_t$  ( $4.5 \times 10^{17} \text{ cm}^{-3}$ ) in the absorber material. Table S2† shows the PCE variation observed when Spiro-MeOTAD/CuI and PEDOT:PSS/CuI were employed as HTLs in regular and inverted PSCs, respectively, using different ETLs (TiO<sub>2</sub> and ZnO).

In both configuration simulations, the HTLs (Spiro-MeOTAD, PEDOT:PSS, and CuI) presented a thickness of 200 nm, and ETLs (TiO<sub>2</sub> and ZnO) were 30 nm thick. The perovskite MASI thickness stays at 350 nm (Fig. 2). The transparent conductive oxide layer (TCO), in our case the fluorine-doped tin oxide (FTO), was omitted for the simulations of inverted PSCs since the HTL/FTO interface can be considered an ohmic contact.<sup>44</sup>

The organic HTL PEDOT:PSS presents difficulties in its application in solar cells, especially related to its low conductivity and defects in film morphology deposition, which leads to high charge recombination and consequently low values of FF and PCE.<sup>66</sup> As related in other studies, despite Spiro-MeOTAD being one of the most used HTLs in planar PSCs, its use also finds difficulties related to this HTL environmental stability and during the solar cell fabrication process as well. In addition to it, Spiro-MeOTAD synthesis is expensive and this HTL is also commonly used with additives that interfere in the PSCs stability, despite increasing its conductivity.<sup>46</sup>

Inorganic HTLs such as CuI, Cu<sub>2</sub>O, and CuSCN have low cost and high stability, which makes them good candidates for replacement of organic HTLs.<sup>57</sup> In particular, CuI has a large bandgap with an energy level close to perovskite and higher hole mobility of 0.5 to 2 cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup>.<sup>67</sup> However, these HTLs need low thickness to win the high device series resistance, which causes a challenge in regular PSC construction. Because of that, iPSCs are considered an excellent solution to overcome this problem.<sup>54</sup>

The simulated PSCs using CuI demonstrate superior performance in both regular and inverted configurations in all simulations compared to those using organic HTLs Spiro-MeOTAD and PEDOT:PSS with ZnO as the ETL, which is attributed to the higher hole mobility of CuI compared to organic HTLs. Considering the previously mentioned advantages of the inorganic HTL over the organic HTLs, we use CuI as HTL in the remaining simulations for both configurations. The next topic will discuss the optimization of CuI thickness.



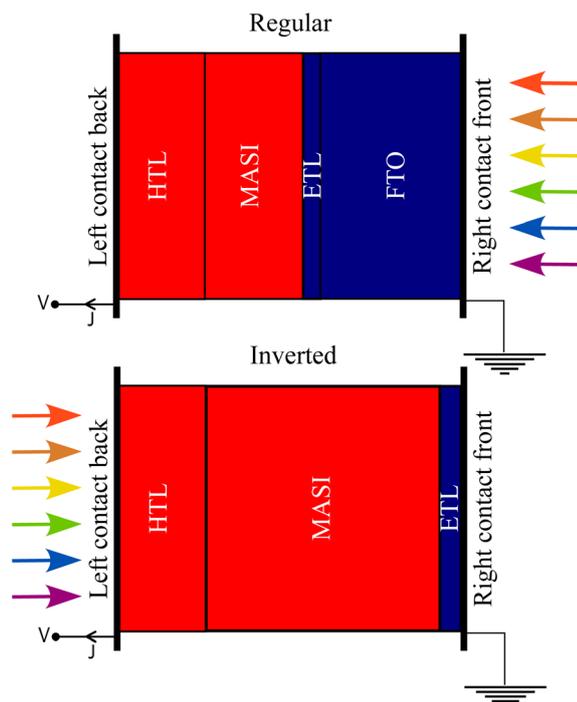


Fig. 2 Simulated PSCs in SCAPS-1D: regular n-i-p and inverted p-i-n.

A higher PCE is observed when zinc oxide replaced titanium dioxide in regular PCS in all simulations (Table S2†). While  $\text{TiO}_2$  boasts a good electron transfer capacity, its utilization requires high processing temperatures.<sup>68,69</sup> Additionally, the Ti–O–Sn bond can contribute to increased charge recombination, as discussed earlier in this work.<sup>7</sup> ZnO is a good alternative to  $\text{TiO}_2$  due to its similar band energy alignment and the fact that it does not require high-temperature processing.<sup>70</sup>

Table 5 shows the output parameters of n-i-p and p-i-n PSCs simulated in SCAPS-1D, varying the ETLs and using CuI/Spiro-MeOTAD as HTLs for regular PSCs and CuI/PEDOT:PSS as HTLs for inverted PSCs.

The simulated device CuI/MASI/ZnO showed better results than the device using  $\text{TiO}_2$  in both configurations (6.89% and 1.35% for regular and inverted PSCs, respectively) due to the greater electron mobility of ZnO compared to  $\text{TiO}_2$ .<sup>56</sup>

Table 5 Output parameters of current–voltage (JV) curves simulated of PSCs with n-i-p and p-i-n configurations, varying the HTLs and ETLs, fixing  $N_t$  in  $4.5 \times 10^{17} \text{ cm}^{-3}$  and the perovskite thickness in 350 nm. The thickness of HTL/ETL is 200 nm and 30 nm, respectively

Simulated PSCs	HTL/ETL	$V_{oc}$ (V)	$J_{sc}$ ( $\text{mA cm}^{-2}$ )	FF (%)	PCE (%)
n-i-p <sup>a</sup>	Spiro/ $\text{TiO}_2$	0.68	17.87	49.99	6.12
n-i-p	CuI/ $\text{TiO}_2$	0.68	12.23	52.40	6.54
n-i-p	CuI/ZnO	0.68	18.70	53.82	6.89
p-i-n <sup>a</sup>	PEDOT/PCBM	0.55	5.84	37.15	1.18
p-i-n	CuI/ $\text{TiO}_2$	0.66	4.15	38.87	1.06
p-i-n	CuI/ZnO	0.62	4.83	45.04	1.35

<sup>a</sup> Simulations based on reference PSCs configurations. Regular PSC ref.: Spiro/ $\text{TiO}_2$ , PCE = 5.23%;<sup>12</sup> iPSC ref.: PEDOT:PSS/PCBM, PCE = 1.39%.<sup>58</sup>

Jayan and Sebastian<sup>46</sup> studied the effect of different HTLs and ETLs on the efficiency of regular MASI PSCs using SCAPS-1D software. The study achieved a PCE of 18.18% using CuI and ZnO as HTL/ETL. However, the authors used an ideal  $N_t$  of  $2.5 \times 10^{13} \text{ cm}^{-3}$  and did not perform the study for iPSCs. The influence of different values of  $N_t$  will be discussed in the last topic of this work.

Several simulation studies have already evaluated the relationship between the PSC efficiency and the defect density values ( $N_t$ ), both in the light-absorbing layer and at the device interfaces, varying it between  $10^{13}$  and  $10^{19} \text{ cm}^{-3}$ .<sup>39,71–74</sup> It is observed that the lower the defect density in the absorber material, the higher its charge diffusion length ( $L$ ), and this reduces charge recombination and increases the device efficiency.

The charge diffusion length of the device is given by the square root of the product obtained between the diffusion coefficient ( $D$ ) and the carrier lifetime ( $\tau$ ), which is the average time required for a carrier to recombine, given in cm, as shown in the eqn (1) and  $D$  is given by the eqn (2) in  $\text{cm}^2 \text{ s}^{-1}$ .

$$L = \sqrt{D\tau} \quad (1)$$

$$D = \frac{\mu k_B T}{q} \quad (2)$$

where  $\mu$  is the charge mobility (electrons and holes), in our case, both present the value of  $1.6 \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$ ,  $k_B$  is Boltzmann constant,  $T$  is the temperature, in our simulation 300 K, and  $q$  is the charge magnitude ( $1.6 \times 10^{19} \text{ C}$ ).

The carrier lifetime  $\tau$  is given in the eqn (3).

$$\tau = \frac{1}{\sigma V_{th} N_t} \quad (3)$$

where,  $\sigma$  is capture cross-section ( $2 \times 10^{-14} \text{ cm}^2$ ) and  $V_{th}$  is the thermal velocity ( $1 \times 10^7 \text{ cm s}^{-1}$ ).<sup>42</sup>

As shown by the formulas above, the defect density of the light-absorbing material is related to the value of the charge diffusion length of the device. Despite defect density values between  $10^{13} \text{ cm}^{-3}$  and  $10^{15} \text{ cm}^{-3}$  being ideal for achieving better output parameters in PSCs, studies about defect density in experimental cells have shown that values between  $10^{16} \text{ cm}^{-3}$  and  $10^{17} \text{ cm}^{-3}$  are commonly found in these devices.<sup>75,76</sup> Here, we perform simulations using an  $N_t$  closer to those found in experimental solar cells.

### 3.2 Influence of MASI/CuI thickness and the different back contact metals on n-i-p and p-i-n PSCs

Due to the results presented in the last topic, all simulations are realized using CuI as HTL and ZnO as ETL. The ZnO thickness was 30 nm in all simulations, and the influence of HTL and MASI thickness will be evaluated.

The thickness of CuI was varied from 200 nm to 30 nm, keeping the MASI thickness at 350 nm for both regular and inverted PCSs. There were no changes in the efficiencies of both configurations with varying thicknesses of the inorganic HTL. In the work of Wang *et al.* (2017),<sup>77</sup> the authors fabricated an iPSC using CuI as the HTL with thicknesses of 20, 40, and 60 nm



and found the optimal output parameters at a thickness of 40 nm. Based on this finding, we adopted a thickness of 40 nm for the HTL in our study.

Subsequently, we evaluated the MASI thickness influence in solar cell's PCE, varying the thickness from 150 nm to 800 nm in regular and inverted PSCs with an  $N_t$  at  $4.5 \times 10^{17} \text{ cm}^{-3}$  and using the configuration  $\text{CuI}(40 \text{ nm})/\text{MASI}/\text{ZnO}(30 \text{ nm})$ .

In both configurations, the decrease in the perovskite thickness reduces the light absorption rate, negatively impacting the device efficiency. However, very high thicknesses can increase the recombination of charges in the material.<sup>78</sup> Devices with thicker perovskite exhibit significant charge extraction losses, and charge recombination occurs due to the comparatively slow speed of charge transport between the carrier layers compared to the light absorption rate.<sup>79</sup>

In a planar PSC, for optimal results, the charge diffusion value should be greater than the perovskite thickness.<sup>80,81</sup> Table 6 shows the  $L$  and  $\tau$  values to different  $N_t$  values, calculated from the described equations discussed in Subsection 3.1.

It is related in many studies involving simulated iPSCs that the PCE increases with perovskite thickness. However, these studies use a low  $N_t$  value.<sup>44,52,81</sup> Fig. 3 shows the device efficiency variation as a function of perovskite thickness, using different  $N_t$  values ranging from  $4.5 \times 10^{13}$  to  $4.5 \times 10^{17} \text{ cm}^{-3}$  for both regular and inverted PSCs.

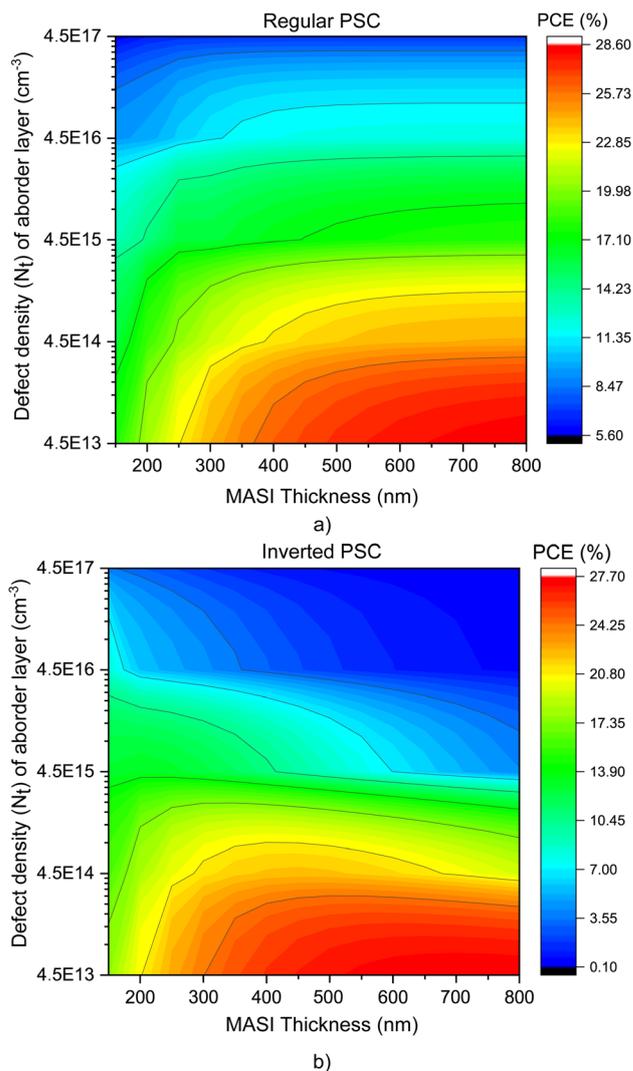
It is possible to observe in Fig. 4 and in Table S3 in ESI† the variation of the output parameters ( $V_{oc}$ ,  $J_{sc}$ , FF and PCE) as the MASI thickness increases.

When low values of  $N_t$  were used ( $10^{13} \text{ cm}^{-3}$  and  $10^{14} \text{ cm}^{-3}$ ), the device's PCE increased with the perovskite thickness in both configurations. Regular PSCs maintained the pattern of increasing efficiency as the thickness increased, regardless of the defect density ( $N_t$ ), as shown in Fig. 3. The thickness of n-i-p PSCs was optimized to 400 nm. As discussed by Lin *et al.*<sup>82</sup> when the perovskite thickness decreases in regular PSCs, there is an increase in the hysteresis effect, leading to lower PCE values with very thin absorber layers.

On the other hand, unlike regular PSCs, the efficiency of iPSCs decreases as the thickness of the MASI perovskite increases when high values of  $N_t$  are employed (Fig. 3b). Considering the perovskite thickness between 150 to 800 nm, the highest PCE in iPSC was 3.72% using MASI with 150 nm thick. This behavior is attributed to non-radiative recombination linked to defects within the perovskite film.<sup>42</sup> Fig. 5 shows that the charge recombination increased as the MASI thickness increased in iPSCs. As depicted in eqn (4), Shockley–Read–Hall

**Table 6** Values of  $L$  and  $\tau$  according to the  $N_t$  variation.  $N_t$  is the defect density of light-absorbing material,  $L$  is the charge diffusion length and  $\tau$  is the charge carrier lifetime

$N_t \text{ (cm}^{-3}\text{)}$	$L \text{ (nm)}$	$\tau \text{ (s)}$
$4.5 \times 10^{13}$	676.50	$1.11 \times 10^{-7}$
$4.5 \times 10^{14}$	213.93	$1.11 \times 10^{-8}$
$4.5 \times 10^{15}$	67.65	$1.11 \times 10^{-9}$
$4.5 \times 10^{16}$	21.40	$1.11 \times 10^{-10}$
$4.5 \times 10^{17}$	6.76	$1.11 \times 10^{-11}$



**Fig. 3** Contour graphs of the PCE values varying the MASI thickness and defect density of the absorber layer of regular (a) and inverted (b) PSCs.

recombination is directly associated with the carrier lifetime ( $\tau$ ) which, in turn, correlates with defect density ( $N_t$ ).

$$R_{\text{SRH}} = \frac{np - n_i^2}{\tau_{\text{nr}}(n + p)} \quad (4)$$

where  $n$  and  $p$  are electron and hole densities, respectively and  $n_i$  is intrinsic carrier density.

Sun *et al.*<sup>83</sup> achieved an efficiency of 7.40% in an experimental iPSC using MAPI with approximately 50 nm thick. The relationship between the perovskite thickness and exciton diffusion was analyzed using the Internal quantum efficiency (IQE) measurements to understand the PCE value observed in the device, concluding that the relationship between the two observed parameters was ideal. The authors emphasized that the value of  $L$  was close to the MAPI thickness. In our simulations using a high value of  $N_t$  ( $4.5 \times 10^{17} \text{ cm}^{-3}$ ), the perovskite thickness of p-i-n PSC was optimized to 150 nm.



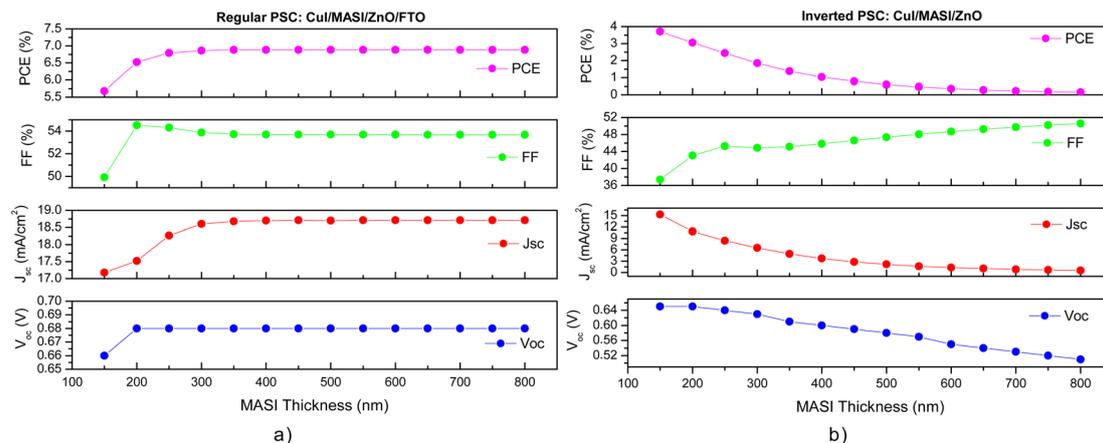


Fig. 4 PCE, FF,  $J_{sc}$  and  $V_{oc}$  of n-i-p (a) and p-i-n (b) PSCs, varying the MASI thickness, using ZnO and CuI as ETL/HTL (30 nm) and  $N_t$  of MASI in  $4.5 \times 10^{17} \text{ cm}^{-3}$ .

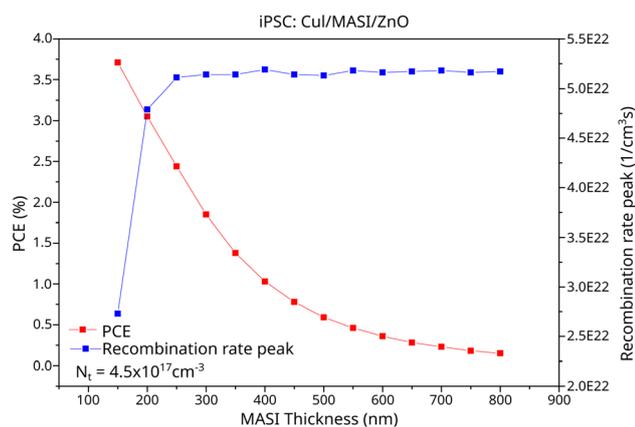


Fig. 5 PCE values and recombination rate peak based on MASI thickness variation in inverted PSC.

The output parameters of the PSCs were evaluated in both configurations by varying the metals used as back contacts. The work function values of these metals are summarized in Table 4. Fig. S1† shows that in contrast to regular PSCs, inverted PSCs present higher PCE when metals with lower work functions are used.

Yue *et al.*<sup>84</sup> built an iPSC using MAPI and measured its performance with metal cathodes with different work function values. They observed that metals with low work functions, such as Ca, Mg, Al, and Ag, resulted in superior device performance. The authors concluded that employing metals with high work functions, such as Au, caused a misalignment of energy levels within the light-absorbing layer towards the cathode, creating an upward band bend that hindered effective electron transport and consequently reduced solar cell efficiency. Similarly, Gong *et al.*<sup>85</sup> conducted simulation work using MAPI perovskite to investigate the impact of metal cathodes on iPSCs, and they also concluded that metals like Au and Pt could generate an energy barrier towards the cathode.

Fig. 6 illustrates the band diagrams of iPSCs with CuI/MASI/ZnO configuration simulated in our study with different metal

contacts. Similar to lead perovskites, it is possible to observe the upward curve of the energy levels from the tin perovskite towards the back contact metal as the work function of metals increases. Based on these results, the back contact metals selected for the remaining simulations are Au and Ag for regular and inverted PSCs, respectively.

### 3.3 Fullerene- $C_{60}$ and PCBM as interlayers in n-i-p and p-i-n MASI PSCs

In all simulations, fullerene- $C_{60}$  and its derivative PCBM were utilized as interlayers between the ETL and the perovskite layer to enhance device performance in both regular and inverted configurations. The PSCs are simulated using an  $N_t$  of  $4.5 \times 10^{17} \text{ cm}^{-3}$  and CuI and ZnO as HTL/ETL, respectively. The interlayer thickness varied from 5 to 15 nm, with the best results observed when the PCBM thickness was 15 nm due to the passivation effect reaching more trap states at the interface between the ETL and the perovskite layer as the interlayer thickness increased,<sup>86</sup> Table 7.

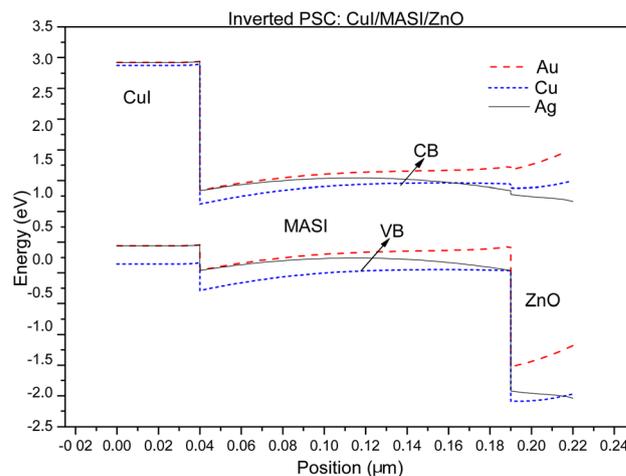


Fig. 6 Band diagrams of lead-free iPSCs using metal contacts with different work function values.

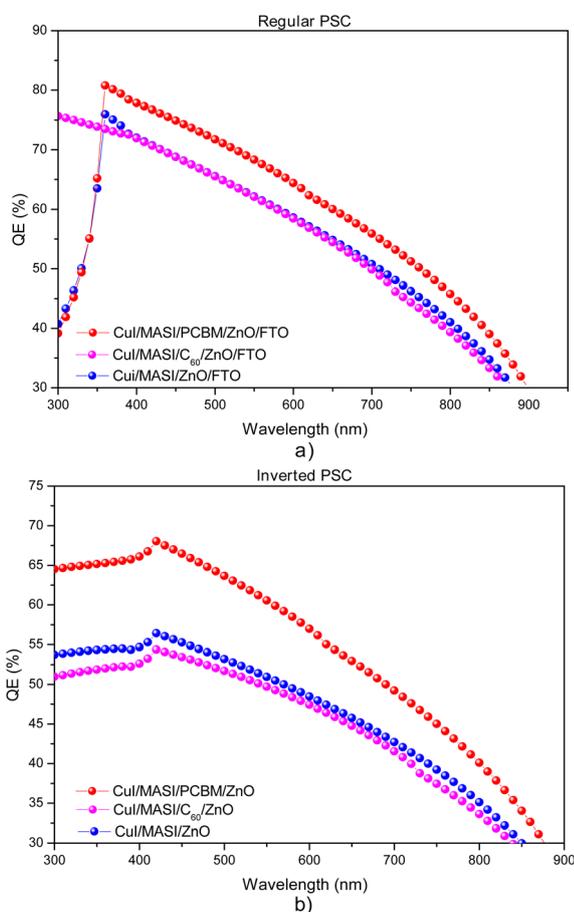


**Table 7** Influence of interlayers in PSCs n-i-p and p-i-n, using CuI (40 nm) and ZnO (30 nm) as HTL/ETL.  $N_t$  is varied between  $4.5 \times 10^{17} \text{ cm}^{-3}$  and  $4.5 \times 10^{16} \text{ cm}^{-3}$ . The MASI thickness was 150 nm to p-i-n PSCs in both values of  $N_t$  and it varied in n-i-p PSCs (400 and 700 nm, respectively)

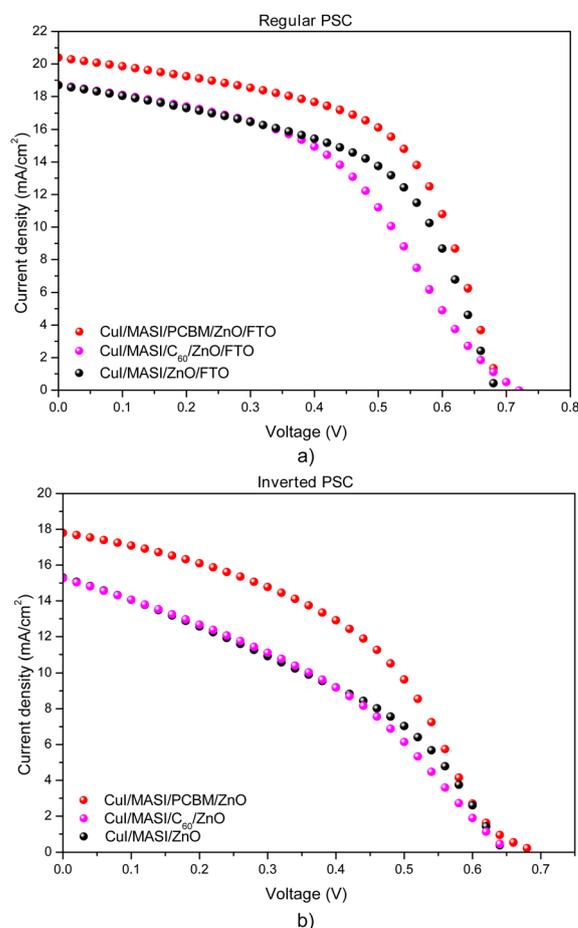
Defect density $N_t$ ( $\text{cm}^{-3}$ )	PSC n-i-p	Interlayer thickness (nm)	PCE (%)	PSC p-i-n	Interlayer thickness (nm)	PCE (%)
$4.5 \times 10^{17}$	CuI/MASI/ZnO/FTO	—	6.90	CuI/MASI/ZnO	—	3.72
	CuI/MASI/C <sub>60</sub> /ZnO/FTO	5	5.68	CuI/MASI/C <sub>60</sub> /ZnO	5	3.33
	CuI/MASI/C <sub>60</sub> /ZnO/FTO	10	5.76	CuI/MASI/C <sub>60</sub> /ZnO	10	3.41
	CuI/MASI/C <sub>60</sub> /ZnO/FTO	15	6.10	CuI/MASI/C <sub>60</sub> /ZnO	15	3.66
	CuI/MASI/PCBM/ZnO/FTO	5	8.06	CuI/MASI/PCBM/ZnO	5	5.22
	CuI/MASI/PCBM/ZnO/FTO	10	8.09	CuI/MASI/PCBM/ZnO	10	5.24
	CuI/MASI/PCBM/ZnO/FTO	15	8.11	CuI/MASI/PCBM/ZnO	15	5.26
$4.5 \times 10^{16}$	CuI/MASI/ZnO	—	11.85	CuI/MASI/ZnO	—	8.22
	CuI/MASI/PCBM/ZnO	15	13.38	CuI/MASI/PCBM/ZnO	15	10.00
	CuI/MASI/C <sub>60</sub> /ZnO	15	11.05	CuI/MASI/C <sub>60</sub> /ZnO	15	8.15

The simulations show that the PCE values for devices with interlayers are higher when PCBM is used instead of fullerene-C<sub>60</sub> in both configurations, as observed in the quantum efficiency (QE) graph in Fig. 7, which represents the ratio between the number of charges generated in the solar device to the number of incident photons, and in JV curves, Fig. 8. This fact can be attributed to the energy difference between the LUMO orbitals of the interlayer and the perovskite, as shown in Fig. 9 for regular PSCs and in Fig. S2† for inverted

PSCs. Using the fullerene derivative PCBM as an interlayer with a 15 nm thickness, a n-i-p PSC exhibited a device efficiency increase of 1.21% compared to the PSC without an interlayer, reaching 8.11%. For the p-i-n PSC, an efficiency increase of 1.54% was obtained, reaching 5.26%, Table 7 and Fig. 8. Using fullerene derivatives in smaller quantities as interlayers or additives can assist in optimizing lead-free PSCs



**Fig. 7** Quantum efficiency graph of PSCs in (a) regular and (b) inverted configurations.



**Fig. 8** JV curves of PSCs using fullerene-C<sub>60</sub> and PCBM (15 nm thickness) as interlayers between ZnO and MASI in both regular (a) and inverted (b) configurations.



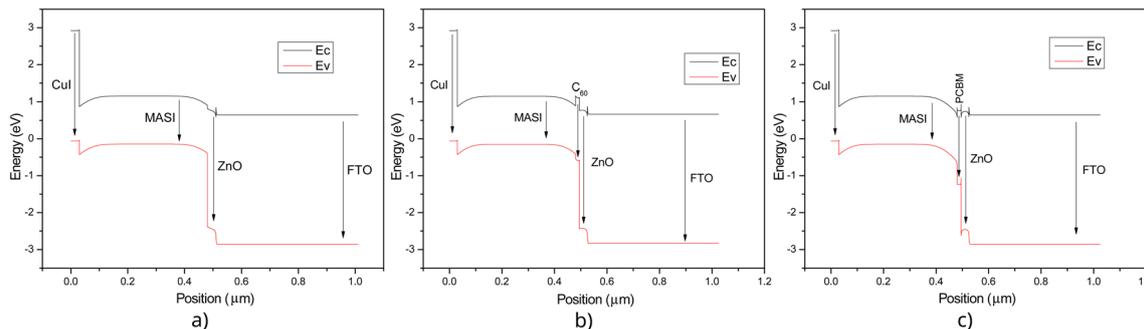


Fig. 9 Energy diagram of simulated regular PSCs. (a) Cul/MASI/ZnO, (b) Cul/MASI/C<sub>60</sub>/ZnO, (c) Cul/MASI/PCBM/ZnO, using  $N_t = 4.5 \times 10^{17} \text{ cm}^{-3}$  and MASI thickness at 400 nm.

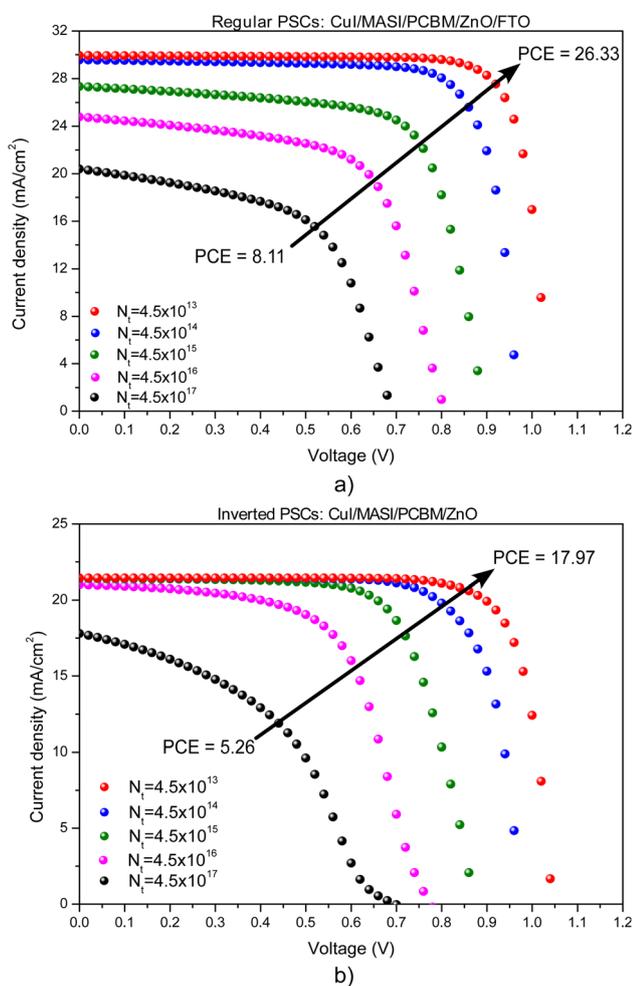


Fig. 10 Comparison of JV curves using PCBM as an interlayer at different values of defect density ( $N_t$ ) of PSCs in (a) regular and (b) inverted configurations.

by passivating possible defects in the crystal lattice formed during the deposition step.<sup>28</sup>

When fullerene-C<sub>60</sub> was used as an interlayer in regular PSCs, all results were worse compared to the devices simulated without interlayers (Table 7), in both configurations. As shown in Fig. 9C to the regular PSCs and Fig. S2 (ESI)<sup>†</sup> to the iPSCs, the

LUMO energy level of PCBM is close to the MASI perovskite, which helps in electron extraction. In simulated PSC using fullerene-C<sub>60</sub> as an interlayer a slight energy barrier to electron transfer occurs between the MASI layer and the ETL (Fig. 9 and S2<sup>†</sup>), which hampers electron mobility. The electron energy barrier at the interface perovskite/ETL is crucial as it determines how efficiently electrons can be transferred between the layers. Electron losses due to recombination occur during the transport of photogenerated charges between the various layers of the PSC. A high energy barrier can lead to significant recombination losses, reducing the current generated by the solar cell and decreasing its efficiency.<sup>87</sup>

### 3.4 Influence of defect density ( $N_t$ ) in regular and inverted PSCs using fullerene-C<sub>60</sub> and PCBM as interlayers

Here, we will evaluate how changing the defect density in perovskite layer can influence the PCE. Initially, the  $N_t$  value of perovskite MASI is changed between  $4.5 \times 10^{17} \text{ cm}^{-3}$  and  $4.5 \times 10^{13} \text{ cm}^{-3}$  in n-i-p and p-i-n PSCs, maintaining the MASI thickness in 400 nm and 150 nm for regular and inverted PSCs, respectively, and using PCBM as interlayer. As shown in Fig. 10, the JV curve increases when the  $N_t$  value decreases for both configurations.

Although the PCE increases with the decrease in the  $N_t$  value, we discreetly reduced the  $N_t$  value from  $4.5 \times 10^{17}$  to  $4.5 \times 10^{16} \text{ cm}^{-3}$ , maintaining an  $N_t$  value close to that found in experimental solar cells.<sup>75</sup> The MASI thickness was already optimized for different values of  $N_t$ , as discussed in Section 3.2. When PCBM is used as an interlayer, PCE significantly increased, rising from 8.11% to 13.38% for regular PSCs and from 5.26% to 10.00% for inverted PSCs, as shown in Table 7, considering 150 nm to iPSC and 700 nm to regular PSC in this simulations.

Fig. 11 compares JV curves of the devices using an  $N_t$  of  $4.5 \times 10^{17} \text{ cm}^{-3}$  and  $4.5 \times 10^{16} \text{ cm}^{-3}$  and PCBM as an interlayer between ZnO and MASI. As observed in both configurations, using a PCBM interlayer helps increase the PCE when high values of  $N_t$  are used due to its surface defect passivation effect. A lower defect density in the absorber material increases the PSC's efficiency, even without using interlayers between the ETL and the perovskite. However, using PCBM as an interlayer significantly increases the PCE value (Table 7).



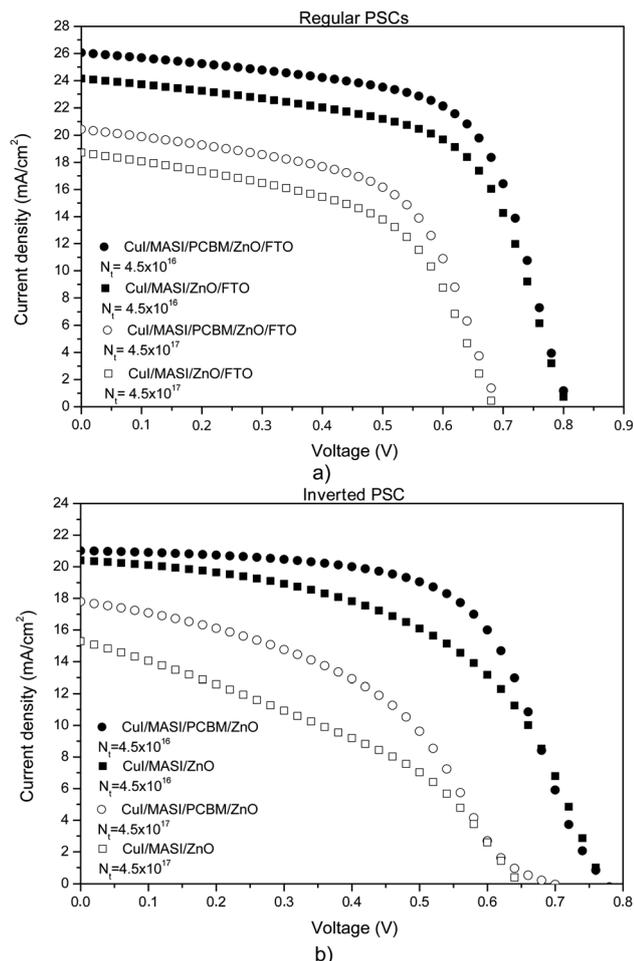


Fig. 11 JV curve of simulated PSCs in n-i-p (a) and p-i-n (b) configurations with and without interlayers using different values of  $N_t$  and PCBM as an interlayer (15 nm). Empty symbols represent PSCs using  $N_t$  of  $4.5 \times 10^{17} \text{ cm}^{-3}$ , and filled symbols represent simulated PSCs with an  $N_t$  of  $4.5 \times 10^{16} \text{ cm}^{-3}$ .

For the simulations considering an ideal  $N_t$  of  $4.5 \times 10^{13} \text{ cm}^{-3}$ , the MASI thickness of regular and inverted PSCs was 800 and 750 nm, respectively, as optimized in Subsection 3.2. Interlayers did not positively affect the PSC performance in both configurations. Lower defect densities in the perovskite material result in fewer trap states and reduced charge recombination between layers, enhancing the PCE. In this context, the interlayers play a less significant role, as the device does not require passivation of the absorber layer. The simulations using PCBM as an interlayer achieved nearly the same results as simulations without interlayers, as shown in Table S4.† However, in the simulations using fullerene- $\text{C}_{60}$  as an interlayer, the PCE significantly decreased, similar to what occurred with higher  $N_t$  values.

## 4 Conclusion

The objective of our work was to understand how the use of fullerene- $\text{C}_{60}$  and its derivative PCBM could affect lead-free PSCs using MASI in both regular and inverted configurations. We

observed from simulation results that the inorganic HTL, CuI, could be considered a good alternative to organic HTLs in lead-free PSCs for achieving improved output parameters for solar cells in both configurations. The HTL CuI and MASI perovskite thicknesses were optimized and a PCE of 6.90% and 3.72% was achieved for the regular and inverted PSCs, respectively.

Using a fullerene derivative as an interlayer could positively influence the PCE of MASI PSCs when the inorganic ETL, ZnO, is used in both configurations due to better electron extraction and defect passivation. Using PCBM as an interlayer, with 15 nm thick, in simulations with a high value of defect density ( $N_t = 4.5 \times 10^{17} \text{ cm}^{-3}$ ) in the absorber layer caused an increase in the device's efficiency, from 6.90% to 8.11%. In iPSCs with CuI/MASI/PCBM/ZnO configuration, also occurs an increase of 1.54% as compared to MASI PSC without an interlayer, and the device achieved a PCE of 5.26%.

However, when fullerene- $\text{C}_{60}$  was used as an interlayer, device performance had no positive impact, and a decrease in PCE of regular and inverted PSCs was observed compared to devices without an interlayer. This occurs due to the difference in energy level between the interlayer and MASI perovskite layer, which causes recombination losses. The optoelectronic properties of fullerene- $\text{C}_{60}$  derivatives need to be such that they do not negatively impact device performance while also serving their purpose of passivating interfacial recombination sites.

Decreasing the defect density to  $4.5 \times 10^{16} \text{ cm}^{-3}$  in the light absorbing material for devices with CuI/MASI/PCBM/ZnO configuration in n-i-p and p-i-n PSCs, better results were found and the PCE reached 13.38% for regular PSC and 10.00% for the iPSC. Considering an ideal  $N_t$  of  $4.5 \times 10^{13} \text{ cm}^{-3}$ , it was observed in both simulated PSCs that the use of PCBM as interlayer did not significantly interfere the efficiency of the solar device. As the defect density in the perovskite layer is small, the PCBM passivation effect was not that significant.

Finally, our SCAPS-1D simulations revealed that employing fullerene derivatives such as PCBM in thin layers as interlayers can positively impact lead-free PSCs using MASI, especially in the inverted configuration. We hope our findings will contribute to ongoing research efforts to enhance the efficiency and stability of MASI PSCs.

## Conflicts of interest

There are no conflicts to declare.

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